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ADEQUACY OF SERVICES REPORT

FOR

**BARRHAVEN CONSERVANCY
DEVELOPMENT CORPORATION**

BARRHAVEN CONSERVANCY WEST

CITY OF OTTAWA

PROJECT NO.: 21-1226

**JANUARY 2023
2ND SUBMISSION
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1.0 INTRODUCTION

David Schaeffer Engineering Limited (DSEL) has been retained to prepare an Adequacy of Services Report (AES) in support of the Barrhaven **Conservancy West** development area on behalf of Barrhaven Conservancy Development Corporation (BCDC).

The overall Conservancy land area is approximately 139.7 ha (all land use components) and is located within the City of Ottawa urban boundary in the Barrhaven ward. As illustrated in **Figure 1**, the subject site is located north of the Jock River, east of Highway 416, west of Borrisokane Road and south of McKenna Casey Drive.

The focus of this report is for the **Conservancy West** land area that is located west of the existing Foster Ditch which bisects the overall BCDC landholdings and consists of vacant land. The subject lands are approximately 34.15ha in area (including all right-of-ways, residential area and park areas) and the proposed development draft plan **Figure 2** is provided for reference. The development area is currently zoned Development Reserve (DR) and is planned to be developed with a mix of detached single homes, townhomes, park blocks, open spaces and a road network.

A previous draft plan application has been submitted for the BCDC landholdings to the east of this development area.

The Conservancy West development area is outside of the Jock River 100-year limit as confirmed by the Rideau Valley Conservation Authority (RVCA). Refer to the RVCA confirmation letter in **Appendix D**. The 100-year regulatory flood line is demonstrated in Drawing 1 (Grading) and Drawing 3 (Stormwater) in the **Appendix**.

The objective of this report is to provide sufficient detail to demonstrate that the proposed development area can be supported by municipal services.

1.1 Existing Conditions

The initial **Conservancy West** property topography is relatively flat with the existing ground elevations varying between 91 m and 92 m. All existing flows are either overland to the Jock River or conveyed to the Jock River by way of the O'Keefe Municipal Drain or the Foster Ditch (and their tributaries) which run north to south through the subject property. The property is within the Jock River watershed and is under the jurisdiction of the RVCA.

1.2 Summary of Pre-Consultation

The following provides a summary of the pre-consultation:

Ministry of the Environment, Conservation and Parks (MECP)

Prior consultations associated with the Conservancy Phase 1 development were previously undertaken for the approval of that phase of the development area.

A pre-consultation with the local MECP office has not yet been completed for the Conservancy West development area until the functional design details and requirements have been established with the City of Ottawa.

Rideau Valley Conservation Authority (RVCA)

Multiple consultations, analysis and submissions were coordinated with the RVCA to establish that the development area is outside of the Jock River 100-year limit. See the RVCA documentation in **Appendix D** for reference.

1.3 Existing Permits / Approvals

Key approvals associated with the advancement of development of the Barrhaven Conservancy area, are presented in the following table. The most relevant approval is the Environmental Compliance Approval (ECA) for the South Nepean Collector sanitary trunk sewer that future phases will be connecting to. The document is provided in **Appendix A** for reference.

Table 1A: Existing Permits / Approvals

Agency	Approval Type	Approval Number	Remarks
Ministry of the Environment, Conservation and Parks (MECP)	Environmental Compliance Approval	# 8129-AB7LDF (June 23, 2016)	South Nepean Collector existing approval (sanitary outlet for development area)
MECP	Environmental Compliance Approval	# 4357-CHMQEM (Sept. 1, 2022)	Sanitary and storm sewer approvals for Conservancy lands east of Borrisokane Road
MECP	Permit to take Water	#5633-C2RQPL (May 26, 2021)	Water taking from Building Excavation, Site Servicing, SWMW, In-Water Works, Poned Surface Water
Rideau Valley Conservation Authority (RVCA)	RVCA Letter of Permission under O.Reg. 174/06	RV5-4419	Letter of permission related to placement of fill within a regulated area.

1.4 Required Permits / Approvals

The City of Ottawa must approve detailed engineering design drawings and reports prior to future construction of the municipal infrastructure identified in this report. This will occur as part of the Plan of Subdivision application process and detailed design.

Based on pre-consultation with City staff, the additional approvals and permits listed in the following table are expected to be required prior to construction of the municipal infrastructure detailed herein. Please note that other permits and approvals may be required, as detailed in the other studies to be submitted as part of the Plan of Subdivision application (e.g. *Tree Conservation Report, Environmental Impact Statement, Phase 1 Environmental Site Assessment, Headwater Drainage Feature Assessment, etc.*)

Table 1B: Required Permits/Approvals

Agency	Permit/Approval Required	Trigger	Remarks
MECP	Environmental Compliance Approval	Construction of new sanitary and storm sewers throughout the subdivision.	The MECP will review the sanitary and storm sewer design through the City of Ottawa transfer of review process.
MECP	Environmental Compliance Approval	Implementation of oil-grit separator units for quality control.	The MECP will review the stormwater management appurtenance design through the City of Ottawa transfer of review process.
MECP	Permit to Take Water	Construction of proposed land uses (e.g. basements for residential homes) and services.	Pumping of groundwater may be required during construction, given groundwater conditions and proposed land uses and on-site/off-site municipal infrastructure.
City of Ottawa	MECP Form 1 – Record of Watermains Authorized as a Future Alteration.	Construction of watermains throughout the subdivision	The City of Ottawa will review the watermains on behalf of the MECP through the Form 1 – Record of Watermains Authorized as a Future Alteration.
RVCA	Permit under Ontario Regulation 174/06, RVCA's Development, Interference with Wetlands and Alterations to Shorelines and Watercourses Regulation	Grading (proposed development & potential temporary access roads) within the subject lands (i.e. crossing of Foster Ditch)	Supporting applications and documentation as required through consultation with the RVCA.
RVCA	Outlets to Jock River	In conjunction with issuance of MECP applications	Supporting applications and documentation as required through consultation with the RVCA.
RVCA	Alteration to Watercourses (O'Keefe Drain)	As necessary through consultation with the RVCA	Supporting applications and documentation as required through consultation with the RVCA.
City of Ottawa	Commence Work Notification (CWN)	Construction of new sanitary and storm sewers throughout the subdivision	The City of Ottawa will issue a commence work notification for construction of the sanitary and storm sewers once an approval is issued by the MECP.

2.0 GUIDELINES, PREVIOUS STUDIES, AND REPORTS

2.1 Existing Studies, Guidelines, and Reports

The following studies were utilized in the preparation of this report.

- Ottawa Sewer Design Guidelines,
City of Ottawa, *SDG002*, October 2012
(*City Standards*)
 - Technical Bulletin ISDTB-2014-01
City of Ottawa, February 5, 2014
(*ITSB-2014-01*)
 - Technical Bulletin PIEDTB-2016-01
City of Ottawa, September 6, 2016
(*PIEDTB-2016-01*)
 - Technical Bulletin ISTB-2018-01
City of Ottawa, March 21, 2018
(*ISTB-2018-01*)
 - Technical Bulletin ISTB-2018-04
City of Ottawa, June 27, 2018
(*ISTB-2018-04*)
- Ottawa Design Guidelines – Water Distribution
City of Ottawa, July 2010.
(*Water Supply Guidelines*)
 - Technical Bulletin ISD-2010-2
City of Ottawa, December 15, 2010.
(*ISD-2010-2*)
 - Technical Bulletin ISDTB-2014-2
City of Ottawa, May 27, 2014.
(*ISDTB-2014-2*)
 - Technical Bulletin ISTB-2018-02 / ISTB-2019-02
City of Ottawa, March 21, 2018 / July 08, 2019
(*ISTB-2018-02 / ISTB-2019-02*)
 - Technical Bulletin ISDTB-2021-03
City of Ottawa, August 18, 2021
(*ISTB-2021-03*)
- Design Guidelines for Sewage Works,
Ministry of the Environment, Conservation and Parks, 2008. (formerly MOECC)
(*MECP Design Guidelines*)

- Stormwater Planning and Design Manual, Ministry of the Environment, March 2003.
(SWMP Design Manual)
- City of Ottawa Official Plan, adopted by Council 2003.
(Official Plan)
- City of Ottawa Secondary Plan – Former Nepean – South Nepean Urban Area – Areas 9 and 10, Adopted by Council 2003.
(Secondary Plan)
- South Nepean Collector: Phase 2 Hydraulics Review / Assessment Technical Memorandum
Novatech, August 2015
(Novatech SNC Memo)
 - South Nepean Collector: Phase 2 Preliminary Design Report, Novatech, March 2016
(Novatech SNC Design Report)
- Strandherd Drive Widening Project, South Nepean Collector: Phase 3 Sanitary Flow Calculations
Novatech, May 2019
(2019 Novatech SNC Design Report)
- Hydraulic Potable Water Assessment for Barrhaven Conservancy Development Corporation, March 2021
(Stantec Hydraulic Analysis)
- Jock River Reach One Subwatershed Study
Stantec, 2007
(Jock River SWS)
- Geotechnical Investigation, Proposed Residential Development, Conservancy Lands West, Ottawa, Ontario
Paterson Group, September 27, 2019 (Project No. PG5036-1)
(Geotechnical Report)
- Environmental Impact Statement for Barrhaven Conservancy East
Kilgour & Associates Ltd., July 29, 2020
(Kilgour EIS)

- Master Infrastructure Review – Barrhaven Conservancy
David Schaeffer Engineering Ltd., July 2021
(Conservancy MIR)
- Design Brief for Barrhaven Conservancy East – Phase 2, 3, & Jock River
David Schaeffer Engineering Ltd., June 2022
(DSEL East Design Brief)
- Adequacy of Services Report - Barrhaven Conservancy East – Phase 5
David Schaeffer Engineering Ltd., December 2022
(DSEL East Ph5 Report)
- Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River): Water Distribution
System Analysis, Stantec, June 2, 2022
(*Stantec Hydraulic Analysis - East*)

3.0 WATER SUPPLY SERVICING

3.1 Existing Water Supply Services

The subject property is located adjacent to the City of Ottawa's Pressure Zone (PZ) 3SW (previously known as PZ BARR). PZ SUC services the lands that are east of the subject property, as well as south of the Jock River.

The City of Ottawa has recently reconfigured the pressure zones servicing Barrhaven and the South Urban Community (SUC) in order to improve reliability and efficiency and to increase pumping capacity to accommodate for future growth in the area. There are three pumping stations servicing Zone 3SW and Zone SUC as follows: the Fallowfield Road Pumping Station (FRPS), the Barrhaven Pumping Station (BPS) and the Ottawa South Pumping Station (OSPS).

The future watermain to be implemented through the detailed design process for the adjacent Conservancy East lands will facilitate water service to the West area. These services will be further extended to provide the requisite water supply to this development area.

3.2 Water Supply Servicing Design

Stantec Consulting Limited was retained to perform a hydraulic assessment for the Conservancy East Lands. The ***Hydraulic Potable Water Assessment for Barrhaven Conservancy Development Corporation (Stantec Hydraulic Analysis)*** prepared by Stantec (March 2021) previously supported the advancement of the Conservancy East lands east of Borrisokane road. Subsequently, as part of the detailed design for the approved phases east of Borrisokane Road, Stantec prepared an updated study "***Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River): Water Distribution System Analysis (June 2022 – Stantec Hydraulic Analysis - East)***". The analysis reviewed the system requirements of the development area on the west and east sides of Borrisokane Road but only the detailed design of the areas east of Borrisokane Road were advanced to detailed design.

Stantec has prepared an updated analysis to evaluate the distribution system with the three watermain feeds to the overall development area that were assessed in the Conservancy East design. Their "***Barrhaven Conservancy West: Water Distribution System Analysis (January 2023)***" is provided in ***Appendix B***.

The proposed water servicing layout is presented in ***Figure 3***.

The following table summarizes the relevant Water Supply Design Criteria which will be employed in the design of the subject property.

Table 2A: Water Supply Design Criteria

Design Parameter	Value
<i>Extracted from Section 4: Ottawa Design Guidelines, Water Distribution (July 2010)</i>	
Residential – Detached Single	3.4 p/unit
Residential – Townhome/ Semi	2.7 p/unit
Residential – Apartment	1.8 p/unit
Minimum Watermain Size	150 mm diameter
Minimum Depth of Cover	2.4 m from top of watermain to finished grade
During normal operating conditions desired operating pressure is within	350 kPa and 480kPa
During fire flow operating pressure must not drop below	140 kPa
Residential – Detached Single	280 L/cap/day
Residential – Rear Lane Town & Back-to-Back	2880 L/cap/day
Average Day (AVDY)	Population x Demand
Max Day (MXDY)	AVDY x 2.5
Peak Hour(PKHR)	MXDY x 2.2

Fire Flow Demand

Fire Flow requirements are established in the boundary condition request found in **Appendix B** as prepared by Stantec. Based on anticipated unit configurations and separations the City’s fire flow cap of 13,000 L/min for single dwellings and traditional townhomes as outlined in *ISDTB-2014-02* does not apply and separation of fire areas with units of ordinary construction, as well as architectural elements, will be incorporated to meet target fire flows. The fire flows will be calculated in accordance with the Fire Underwriters Survey’s Water Supply for Public Fire Protection Guideline (2020).

Boundary Conditions

To support the preparation of a hydraulic analysis for the subdivision, boundary conditions were provided by the City of Ottawa for the anticipated water demands and are summarized in the following table. See **Appendix B** for full details of the boundary condition request submitted.

Table 2B: Boundary Conditions (from *Stantec Hydraulic Analysis – West report*)

HGL (m) - Zone SUC Servicing Conditions			
Demand Scenario	Three Connections		
	Connection 1 ⁽¹⁾	Connection 2 ⁽²⁾	Connection 3 ⁽³⁾
AVDY	146.7	146.7	146.6
PKHR	141.4	141.3	141.0
AVDY +FF	139.7	138.1	139.8
MXDY +FF	137.9	136.2	137.9
(1) Ground elevation at Connection 1 (Chapman Mills Drive) = 93.10 m (2) Ground elevation at Connection 2 (Danson Gardens Grv / Darjeeling Ave) 91.80 m (3) Ground elevation at Connection 3 (Flagstaff Dr) 92.30 m As provided by the City of Ottawa via email on December 6, 2022 (J.Bougadis)			

Water Demand Calculations

A summary of water demands for the subject site is presented in the following table as derived from the criteria above and the *Stantec Hydraulic Analysis* found in **Appendix B**.

Table 2C: Water Demand Estimate

		Unit Count	Pop (¹)	AVDY ⁽²⁾ (L/s)	MXDY ⁽³⁾ (L/s)	PKHR ⁽⁴⁾ (L/s)
East	Single Family	782	2,659	-	-	-
	Townhouse	606	1,636	-	-	-
	Subtotal	1,388	4,295	13.92	34.80	76.55
West	Single Family	462	1,571	-	-	-
	Townhouse	499	1,347	-	-	-
	Subtotal	961	2,918	9.46	23.64	52.01
Totals		2,349	7,213	23.38	58.44	128.57
(1) Population per unit is 3.4 for Single Family and 2.7 for Townhomes (2) AVDY = Average Day (3) MXDY = Maximum Day (4) PKHR = Peak Hour (5) See Stantec Hydraulic Analysis in Appendix B for details.						

3.3 Summary of Hydraulic Modeling Analysis

A watermain analysis has been prepared to confirm that the network is sized adequately, which is the greater of maximum day plus fire and maximum hour. City review comments on the prior *Stantec Hydraulic Analysis - East* noted that the

preferred system configuration for the entirety of the Conservancy development area is for three connections to the existing network and those results are presented below.

System Pressures

The modeling indicates that the development can be adequately serviced by the proposed watermain network. Modeled service pressures for the development are summarized the following table. The detailed pipe and junction tables are contained in the **Stantec Hydraulic Analysis**, enclosed in **Appendix B**.

Table 2D: Summary of Available System Pressures

	AVDY Maximum Pressure		Peak Hour Demand Minimum Pressure	
	kPA	psi	kPA	psi
Conservancy West	546	79.23 (J239)	436	63.22 (J297)

Note: See model results in the Appendix C of the Stantec Hydraulic Analysis memo.

The generally accepted best practice is to design new water distribution systems to operate between 350 kPa (50 psi) and 480 kPa (70 psi) as outlined in the City of Ottawa Design Guidelines. Where pressures exceed 80psi pressure reducing valves (PRV) shall be implemented as per the Ontario Building Code.

Available Fire Flows

The minimum allowable pressure under fire flow conditions is 140 kPa (20 psi) at the location of the fire. A summary of the available fire flows is presented in the following table. The detailed fire flow reports are found in the **Stantec Hydraulic Analysis - East** enclosed in **Appendix B**.

Table 2E: Summary of Available Fire Flows

	Required Fire Flow (L/s)	Minimum Available Flow (L/s)	Junction ID
Conservancy West	217	183.84 177.61 197.95	J363 J365 J369

Note: See model results in the Appendix C of the Stantec Hydraulic Analysis. It is anticipated that the above minor flow node can be managed by procedures noted in ISDTB-2018-02 (See Section 3.2 of Stantec report)

As shown in the above table, the model predicts the majority of the network will be able to provide the required 13,000 L/min (217 L/s) fire flows. The junctions noted are marginally below this threshold but it is anticipated that at detailed design fire control measures such as ordinary construction units, firewalls and/or using the alternativ4e

hydrant spacing procedure outline in ISDTB-2018-2 can mitigate these areas (if fire flow results remain the same at detailed design). Detailed results are included in the ***Stantec Hydraulic Analysis***, enclosed in ***Appendix B***.

System Reliability

Various major watermain failure scenarios were reviewed by Stantec. Some scenarios resulted in fire flows that are within the 10,000 L/min range that can be reviewed in more thoroughly at detailed design. See discussion in Section 3.3 of the ***Stantec Hydraulic Analysis*** in ***Appendix B***.

3.4 Water Supply Conclusion

The subject lands are have been reviewed by Stantec to confirm the proposed distribution system will meet the required demands and redundancy requirements.

The network is proposed to consist of 152 mm, 203 mm, 254 mm and 305 mm watermains.

Under AVDY demand conditions the model results indicate that maximum pressures are below the allowable maximum pressure of 80 psi as per the City of Ottawa Design Guidelines. Under PKHR demand conditions the minimum pressures are within the City's system pressure requirements.

Under MXDY+FF demand conditions the assumed required fire flow of 13,000 L/min can be achieved for the majority of the proposed distribution network at full build out conditions. There are several isolated locations where the FF may be slightly less than the 13,000 L/min threshold (i.e. worst case scenario of 10,657 L/min at Junction 365) but it is assumed that these isolated locations can be managed with fire control measure as required at the detailed design stage.

Reliability assessments indicate that for AVDY+FF conditions there are some locations where system flows are slightly below the fire flow of 13,000 L/min (i.e. in the 10,000 to 11,000 L/min range). At detailed design these areas will be assessed with fire flow measures proposed to mitigate potential shortfalls.

Watermain crossings (300mm diameter) of the O'Keefe Drain and Foster Ditch will be accomplished via the implementation of a 610mm diameter steel casing (gauge 12.7mm – Grade 3) which will have 1m clearance below the culverts and extend up to 5m beyond the edge of the culverts. Pressure grout of 1:5 cement/sand ratio will surround the pipe. Details to be established at future detailed design.

Future modelling at the detailed design stage will confirm phasing of the extensions of trunk watermains and sizing of the local watermain network. The proposed water supply design will conform to all relevant City and MECP Guidelines and Policies.

4.0 WASTEWATER SERVICING

4.1 Existing Wastewater Services

Per the **South Nepean Collector (SNC) Wastewater Servicing Study and Functional Design Report** by Dillon in October 2003 (**Dillon SNC Report**), the subject property is tributary to the South Nepean Collector (SNC) sewer as urban development land.

The SNC (previously called the Jock River Collector) sewer operates north of the subject property within Strandherd Drive prior to travelling south down a Chapman Mills Drive (CMD) and then turns eastward within the future CMD right-of-way (ROW).

The **South Nepean Collector Phase 2: Hydraulics Review / Assessment** memo was prepared by Novatech Engineering Consultants on August 20, 2015 (**Novatech SNC Memo**) to provide an update to the sanitary design flows for Phase 2 of the South Nepean Collector, as previously documented in the **South Nepean Collector (SNC) – Functional Design Report and Update** by Dillon in 2012 (**Dillon SNC Report and Update**). In addition, Novatech is also currently the engineer of record for the design and implementation of the Phase 3 extension of the SNC.

4.2 South Nepean Collector Phase 3 – Preliminary Design

The 2015 **Novatech SNC Memo** contemplated that the Conservancy Phase 1 development area (north of the Fraser-Clarke Watercourse) would be serviced by the 900 mm diameter SNC sewer running adjacent to the property within the future extension of CMD. This is represented by area “A6-E” within the “**Sanitary Drainage Areas and Land Use – Fig.1**” plan within the 2015 Novatech memo (note that the actual tributary area and population varied slightly).

For the Phase 3 extension of the SNC, Novatech has prepared another review of sanitary flows within their technical memorandum titled “**Strandherd Drive Widening Project, South Nepean Collector Phase 3: Sanitary Flow Calculations**” May 30, 2019 (**2019 Novatech SNC Memo**). The memorandum, along with the design sheet calculations from the Novatech memo, are provided in **Appendix C** for reference along with DSEL annotations on key items in the figure and design sheets. The updated “**Sanitary Drainage Areas and Land Use – Fig.1**” (May 2019) plan is essentially reflective of the same tributary information that was provided in the 2015 study (the plan has been marked up to reflect the Conservancy areas as a frame of reference). The associated design sheet also reflects updated City wastewater design criteria that was not accounted for in the 2015 study and is discussed further in the following section.

Report excerpts are provided in **Appendix C** for the SNC Phase 2 analysis as well as draft information associated with the Phase 3 extension. The location of the SNC sewer is shown in **Figure 4**.

4.3 Wastewater Design

The subject property is planned to be serviced by an internal gravity sanitary sewer system that is to generally follow the local road network with select servicing easements as required to achieve efficiencies in servicing and grading designs. The wastewater servicing plan can be seen in **Drawing 4**.

Similar to the proposed Conservancy East development, this report proposes that the drainage area of the SNC sanitary sewer be expanded to include the entirety of the Conservancy property. The sewer network will connect to the off-site SNC sanitary sewer within the future CMD at existing manhole 'SANMH8' as identified in the Novatech SNC Phase 2 design Drawing No. 20 provided in **Appendix C** for reference (City contract number ISD14-2033). As noted in the prior section, the 2015 **Novatech SNC Memo** was derived flows based on the City guideline parameters of the time (namely 350 L/capita/day, infiltration allowance of 0.28 L/s/ha and commercial properties at 50,000 L/ha/d). The following table summarizes the new City design guidelines and criteria to be applied to the **Conservancy East** sewer design as well for the determination of the projected flows to be tributary to the SNC along the frontage of the Conservancy Phase 1 development area.

Table 3: Wastewater Design Criteria

Design Parameter	Value
Current Design Guidelines	
Residential - Single Family	3.4 p/unit
Residential – Townhome/ Semi	2.7 p/unit
Residential – Apartment	1.8 p/unit
Average Daily Demand	280 L/d/person
Peaking Factor	Harmon's Peaking Factor. Max 4.0, Min 2.0
Commercial / Institutional Flows	28,000 L/ha/day
Commercial / Institutional Peak Factor	1.5
Infiltration and Inflow Allowance	0.33 L/s/ha
Park Flows	28,000 L/ha/d
Park Peaking Factor	1.0
Sanitary sewers are to be sized employing the Manning's Equation	$Q = \frac{1}{n} AR^{2/3} S^{1/2}$
Minimum Sewer Size	200mm diameter
Minimum Manning's 'n'	0.013
Minimum Depth of Cover	2.5m from crown of sewer to grade
Minimum Full Flowing Velocity	0.6m/s
Maximum Full Flowing Velocity	3.0m/s
<i>Extracted from Sections 4 and 6 of the City of Ottawa Sewer Design Guidelines, October 2012, and associated Technical Bulletins.</i>	

Several design sheets are provided in **Appendix C** for reference:

- Sanitary design sheet for the lands east of Borrisokane Road;

- Design sheet and drainage plan for the recently submitted Conservancy Phase 5 development area for adjustments to that previously approved draft plan (bounded by the Foster Ditch to the west and Borrisokane Road to the east);
- Design sheet and drainage plan for Conservancy West (this current application).

Within the Conservancy East design sheet the area and flows from the lands west of Borrisokane Road are highlighted where flows enter the development area at the westward stub from MH10A. That design sheet projected a flow of 77.81 L/s.

Based on the Conservancy East Phase 5 draft plan, and updated concept plans for the Conservancy West development area, the flows shown at the eastern limit of Phase 5 (see Phase 5 design sheet in **Appendix C**) projected ~68.96 L/s at MH 532A where it outlets to the MH10A noted above. As such, downstream systems are sufficient and no negative impacts given that flows are lower than the previously projected 77.81 L/s.

Updates to the development area for Conservancy West were completed after the Phase 5 submission. The design sheet for the current Conservancy West submission shows a projected flow of 45.84 L/s to Phase 5 whereas the Phase 5 submission had estimated a flow of 56.22 L/s. Flows from Conservancy West are lower therefore no downstream impacts.

4.4 Sanitary Lift Station

As documented within the **Conservancy MIR** the design of the gravity sewers for the Conservancy development areas has been kept the sewer inverts as low as possible from its connection point at the South Nepean Collector. Despite this, the invert of the existing Foster Ditch, which is along the easternmost limit of the Conservancy West draft plan area, does impart a constraint for the sanitary sewer crossing. This constraint will necessitate the inclusion of a low lift sanitary pump station, west of the Foster Ditch, in order to provide sanitary service upstream.

Preliminary review of the requirements by Stantec indicates the following pump station characteristics:

The proposed pumping station will be of wet well type, with two submersible sewage pumps (one duty one standby) estimating a required capacity of 60 L/s +/- . The main components will be:

- Precast concrete or fiberglass wet well, 2.4 m in diameter;
- Two submersible sewage pumps with the duty point of 60 L/s at 14.8 m total dynamic head (initial estimate to be finalized at detailed design);
- Approximately 90 m long forcemain (twin), 150 mm dia., PVC SDR 26 or equal;
- Bypass chamber for pumping the sewage during wet well inspections/repairs or emergency situations;

- Precast control building with electrical and SCADA equipment;
- Permanent power supply (transformer);
- Standby Power: Generator (diesel or natural gas);
- SCADA communication tower;
- Approximately 620m² block of land for the facility based on past experience on a facility of this nature (Note: final block size may vary slightly based on the detailed design/layout of the facility);
- The proposed facility is adjacent to the Foster Ditch and future residential development. The nearest residential units would be ~35m north, ~30m west, ~12m south or ~75m to the east. Separation distances will ultimately depend on the siting of the station;
- Typical carbon filters would be added to venting to mitigate potential odor issues.

The development area and pumps station location are in close proximity to the Jock River with limited opportunity for discharge to a watercourse or storm sewer. The incoming sanitary sewer invert to the station is ~86.41m. The Foster Ditch immediately adjacent to the facility (to the east) has an invert of 90.20. The 25-year water elevation of the Jock River in this vicinity is ~91.57m and the 100-year water elevation is ~91.89m. An overflow siphon to the sanitary outlet manhole is feasible due to the relatively minor elevation difference between the inlet at the lift station versus the gravity outlet to the east of the Foster Ditch (~ +2.0 to 2.5m).

As an extra level of protection during an overflow situation, along with the gravity outlet option noted above, the sewage would have to be pumped by pumper trucks (or temporary pumps) from the wet well to the adjacent sewers or to the Foster Ditch (depending on the type of emergency). The response time for the Operators would need to be calculated based on the available storage in the wet well and within the incoming sanitary sewer. Wet well and/or sanitary sewers could be oversized to increase the available storage to accommodate the response time so that it would be within acceptable limits based on City experience. This will be discussed and addressed in detail during the preliminary station design.

4.5 Wastewater Servicing Conclusion

The subject property will be serviced by local sanitary sewers, an on-site trunk sanitary sewer, and the off-site SNC sanitary sewer per previous reports. There is residual capacity in the downstream SNC providing sufficient capacity for the peak sanitary flows for the subject property, including external commercial and community park flows. Projected flows from Conservancy West are lower than those previously estimated.

The Conservancy West area will require a low lift sanitary pumping station due to a constraint imposed by the existing Foster ditch watercourse that bisects the property which does not allow for gravity drainage all the way to the SNC connection point. Detailed design for the station will be coordinated with the City during the detailed design stage for the development area.

5.0 STORMWATER CONVEYANCE

5.1 Existing Stormwater Drainage

The subject property is within the Jock River watershed. Per the existing topography characterized in available City of Ottawa base mapping, as well as site specific survey, all flows from the subject property are ultimately conveyed to the Jock River by a series of watercourses, sheet flow and minor ditches. The Foster Ditch and the O'Keefe Municipal Drain are the main stormwater conveyances within the Conservancy West property that convey stormwater to the Jock River.

5.2 Proposed Stormwater Management Strategy

Various stormwater strategies were discussed within the Master Infrastructure Review (MIR) prepared previously. Alternatives reviewed were:

Alternative 1 – Oil and Grit Separators & Treatment Train to Naturalized Wetlands*

Alternative 2 – Stormwater Management Wetland Facilities in the Floodplain

Alternative 3 – Stormwater Management Wetland Facilities out of the Floodplain

Alternative 4 – Modified Etobicoke filtration System (MEFS)

For the purposes of this AES update for Conservancy West, Alternative 1 continues to be advanced as per the evaluation provided in the MIR and per discussions with the City of Ottawa on July 20, 2021. This alternative:

- A storm sewer system designed to capture at least the minimum design capture events in accordance with the amendment to the storm sewer and stormwater management elements of the Ottawa Design Guidelines – Sewer (Technical Bulletin PIEDTB-2016-01). The stormwater runoff will be treated before ultimately being released into the natural heritage features and the Jock River as per the ***Jock River Reach One Subwatershed Study*** prepared by Stantec in 2007 (***Jock River SWS***).
- All proposed units will be equipped with sump pumps due to local constraints;
- A treatment train approach to attain an Enhanced Level of Protection (80% total suspended solids (TSS) removal) per MECP guidelines consisting of:
 - Deep sump catchbasins;
 - The incorporation of infiltration-type LIDs within the right-of-way extending out from catchbasin locations (see ***Figure 5*** in the ***Figures & Drawings*** section). Future detailed grading will allow for the determination of suitable locations in order to yield optimal benefit from this LID. See Section 5.7 for additional LID discussion.

- Multiple oil and grit separators (OGS) units to provide TSS treatment with outlets that are above the 2-year event summer water levels on the Jock River;
- The storm systems will discharge the treated stormwater at multiple outlets located along the southern natural heritage corridor, connecting via channels. Discharge locations are demonstrated in the **Storm Tributary Area** plan in the **Figures & Drawings** section
- An on-site road network designed to maximize the available storage within right-of-ways for the 100-year design event, where possible; and
- An overland flow route designed to safely convey stormwater runoff flows in excess of the on-site road storage.

The design for the site proposes to have stormwater flows conveyed through the development area of the subject property via an underground sewer network. The stormwater runoff will be treated before ultimately being released into the natural heritage features and the Jock River as per the **Jock River Reach One Subwatershed Study** prepared by Stantec in 2007 (**Jock River SWS**).

The proposed stormwater design layout is shown on **Drawing 3** with the stormwater management design consisting of:

- A storm sewer system designed to capture at least the minimum design capture events in accordance with the amendment to the storm sewer and stormwater management elements of the Ottawa Design Guidelines – Sewer (Technical Bulletin PIEDTB-2016-01);
- Multiple oil and grit separators (OGS) designed to assist with achieving the required Enhanced Level of Protection per MECP guidelines, along with additional treatment train elements, via treatment of the stormwater captured by the storm sewer network;
- The storm systems will discharge the treated stormwater at multiple outlets located along the natural heritage corridor, connecting via naturalized channels outletting to the Jock River. Discharge locations are demonstrated in **Drawing 3**;
- Inverts of storm outlets are set at the 2-year summer water levels of the Jock River;
- An on-site road network designed to maximize the available storage within right-of-ways for the 100-year design event, where possible, with controlled release of stormwater to the minor storm system; and
- An overland flow route designed to safely convey stormwater runoff flows in excess of the on-site road storage.

Although quantity control has not typically been required for this reach of the Jock River, as per the **Jock River SWS**, the quantity of stormwater runoff exiting from the subject property will be minimized by optimizing on-site storage in the sags of the proposed road network, which in turn minimizes the size of downstream storm sewer infrastructure. It is noted that the RVCA is currently reviewing the SWM requirements within the Jock River Reach 1 area. In consideration of this, J.F. Sabourin and Associates (JFSA) has undertaken a review of the existing quantity control recommendations and the existing, and proposed, development conditions for this area. The findings are presented in the JFSA memorandum *Review of Quantity Control Requirement for Jock River Reach 1 (March 2021)* provided in **Appendix D** which concludes that quantity controls will still not be required for this reach of the Jock River.

Post-Development Stormwater Management Targets

Stormwater management requirements for the proposed alternative Stormwater management scheme have been adopted from the **Jock River SWS**, **City Standards**, and the **MECP SWMP Manual**.

Given the general criteria mentioned above, the following specific standards are anticipated for stormwater management within the subject property:

- Enhanced quality treatment will be provided for stormwater runoff from the subject property, corresponding to a long-term average TSS removal efficiency of 80%, as defined by the MECP prescribed treatment levels;
- Downstream receiving watercourses will be assessed for responses to planned stormwater management outflows, and stabilization mitigation measures will be planned as required;
- Storm sewers on local roads are to be designed to provide at least a 2-year level of service without any ponding per the City's latest Technical Bulletin PIEDTB-2016-01;
- Storm sewers on collector roads are to be designed to provide at least a 5-year level of service without any ponding per the City's latest Technical Bulletin PIEDTB-2016-01;
- For less frequent storms (i.e. larger than 2-year or 5-year), the minor system sewer capture will be restricted with the use of inlet control devices to prevent excessive hydraulic surcharges;
- Under full flow conditions, the allowable velocity in storm sewers is to be no less than 0.80 m/s and no greater than 6.0 m/s;
- For the 100-year storm and for all roads, the maximum depth of water (static and/or dynamic) on streets, rear yards, public space and parking areas shall not exceed 0.35 m at the gutter;

- The major system shall be designed with sufficient capacity to allow the excess runoff of a 100-year storm to be conveyed within the public ROW, or adjacent to the ROW, provided the water level does not touch any part of the building envelope; must remain below all building openings during the stress test event (100-year + 20%); and must maintain 15 cm vertical clearance between spill elevation on the street and the ground elevation at the nearest building envelope;
- Flow across road intersections shall not be permitted for minor storms (generally 5-year or less);
- When catchbasins are installed in rear yards, safe overland flow routes are to be provided to allow the release of excess flows from such areas. A minimum of 30 cm of vertical clearance is required between the rear yard spill elevation and the ground elevation at the adjacent building envelope;
- The product of the maximum flow depths on streets and maximum flow velocity must be less than 0.60 m²/s on all roads.

Quality Control

Per the ***Jock River SWS***, Enhanced quality treatment will be provided for stormwater runoff from the subject property, corresponding to a long-term average TSS removal efficiency of 80%, as described by the MECP prescribed treatment levels. See Section 5.3 for quality control approach and discussion.

Quantity Control

As noted in the ***Jock River SWS***, quantity control is not anticipated to be required for outlets to the Jock River, however, some quantity control may be provided by erosion storage, as erosion thresholds for any watercourses/outlets will be respected where required. As noted in Section 5.2, JFSA has reviewed the current/future development conditions contributing to this reach of the Jock River and concludes that quantity control will still not be required. See “*Review of Quantity Control Requirement for Jock River Reach 1 (JFSA March 2021)*” provided in ***Appendix D***.

5.3 Stormwater Management Design

Treatment Train Approach

JFSA previously (June 2021 memo) prepared a review of various potential stormwater quality treatment options that were investigated for the development. These included options, and combinations of options, as summarized in the following updated table. Each of the options has an expected total suspended sediment (TSS) removal capability, varying from 5% to 88%. This review assessed how the required Enhanced Level of Protection (80% TSS removal) could be achieved when the options are used in

a treatment train approach, consistent with the expected requirements of the upcoming MECP *Consolidated Linear Infrastructure* policy.

Table 1: Quality Control Alternatives – Treatment Train to achieve 80% TSS Removal									
<u>Selection and comparison of alternatives</u>									
Method	TSS Removal	Alt. 1	Alt. 2	Alt. 3	Alt. 4	Alt. 5	Alt. 6	Alt. 7	Alt. 8
Street Sweeping (Monthly)	5%								
Street Sweeping (Weekly)	10%								
Street Sweeping (Weekly with Elgin Eagle)*	88%	x							
Curb Cut with Grass Swales	75%			X					
Curb Cut with Infiltration Trenches	80%								
Catchbasin Inserts (CB Shield)*	27%		X		X	X		X	
Deep Sump Catch Basin	25%				X		X		X
Infiltration/ Filtration Trenches**	80%				X	X	X		
Infiltration at CBs, per MOE Table 3.2 (22.5m ³ /ha)	70%								X
OGS*	50%			X					X
JellyFish*	85%							X	
SWM Pond (Wet Pond)	80%		X						
Overall Performance		88.0%	85.4%	87.5%	89.1%	85.4%	85.0%	89.1%	88.8%
Treatment Train Overall Performance = 1 - (1- TSS Removal Rate Method 1) x (1- TSS Removal Rate Method 2) x (1- TSS Removal Rate Method 3 x ...)									
*) TSS Removal as documented by ETV Canada									
**) includes the use of Etobicoke infiltration or filtration systems or other permutations of the same									

The above table provides a summary of the TSS removal for the various methods that were considered. An option of infiltration LID measures located at catchbasin locations has been added as a method, and to Alternative 8 (see further discussion regarding this method below). The options, and combinations of options, have been assessed and shown to meet or exceed the required 80% TSS target.

For the development area, the updated Alternative 8 option demonstrates an estimated TSS removal of 88.8% for that particular treatment train approach which has been discussed with City staff for the approval of prior phases and will be the design being advanced. For the determination of the TSS removal of 70% for the infiltration LID at catchbasins, the *Table 3.2* of the MOECC (now MECP) publication entitled “*Stormwater Management Planning and Design Manual, March 2003*” sets the storage volume requirements for infiltration measures to achieve certain TSS removal rates.

Table 3.2 Water Quality Storage Requirements based on Receiving Waters^{1, 2}

Protection Level	SWMP Type	Storage Volume (m ³ /ha) for Impervious Level			
		35%	55%	70%	85%
<i>Enhanced</i> 80% long-term S.S. removal	Infiltration	25	30	35	40
	Wetlands	80	105	120	140
	Hybrid Wet Pond/Wetland	110	150	175	195
	Wet Pond	140	190	225	250
<i>Normal</i> 70% long-term S.S. removal	Infiltration	20	20	25	30
	Wetlands	60	70	80	90
	Hybrid Wet Pond/Wetland	75	90	105	120
	Wet Pond	90	110	130	150
<i>Basic</i> 60% long-term S.S. removal	Infiltration	20	20	20	20
	Wetlands	60	60	60	60
	Hybrid Wet Pond/Wetland	60	70	75	80
	Wet Pond	60	75	85	95
	Dry Pond (Continuous Flow)	90	150	200	240



¹Table 3.2 does not include every available SWMP type. Any SWMP type that can be demonstrated to the approval agencies to meet the required long-term suspended solids removal for the selected protection levels under the conditions of the site is acceptable for water quality objectives. The sizing for these SWMP types is to be determined based on performance results that have been peer-reviewed. The designer and those who review the design should be fully aware of the assumptions and sampling methodologies used in formulating performance predictions and their implications for the design.

²Hybrid Wet Pond/Wetland systems have 50-60% of their permanent pool volume in deeper portions of the facility (e.g., forebay, wet pond).

The required storage volume of 24.0 m³/ha is determined for the development area prorated from the above table based on an overall imperviousness of ~68%. Similar to prior phases it is anticipated that the extent of the site area for Conservancy West can be managed with the proposed LID and treatment train system. For prior phases it is noted that approximately 140 lineal meters of LID per hectare of area to be treated was required. The overall land area is ~34.15ha as noted in the introduction of this report. The system design would be such that rear yards are not tributary to the LID. Therefore, if we conservatively assume the full 34.15ha being treated this would equate to 140x34.15= 4,781 m extent of LID required. Conservancy West has approximately 5,700 m of roadway available to incorporate the LID infrastructure therefore more than sufficient roadway length is available for use.

Oil-Grit Separator Units (OGS)

As shown on **Drawing 3**, there will be multiple OGS units at various locations along the southern boundary of the property, discharging to the Jock River via naturalized

channels. By way of an MECP Certificate of Technology Assessment and manufacturer’s design report, the OGS units will demonstrate compliance with Enhanced Level of Protection requirements, with specific drainage area parameters for each area.

The manufacturer’s reported efficiency of TSS removal of the OGS units is expected to be based on a ‘fine distribution’ particle size distribution in conformance with the following table, unless otherwise approved by the City of Ottawa, RVCA, and MECP. The particle size distribution is the generic particle size distribution accepted by the City of Toronto per the *Wet Weather Flow Management Guidelines* (City of Toronto, 2006) as a typical average stormwater particle size distribution, and is an excerpt from Table 3.3 of the *Stormwater Management Practices Planning and Design Manual* (MOECC, 1994).

**Table 4: Typical Stormwater Particle Size Distribution & Settling Velocities
 (Source: *Stormwater Management Practices Planning and Design Manual*,
 MOECC, 1994)**

Particle Size (microns) (NURP 1983)	% of Particle Mass	Average Settling Velocities (m/s)
< 20	0 - 20	0.00000254
20 - 40	20 - 30	0.00001300
40 - 60	30 - 40	0.00002540
60 - 130	40 - 60	0.00012700
130 - 400	60 - 80	0.00059267
400 - 4000	80 - 100	0.00550333

To allow for flexibility as detailed design advances, it is proposed that any OGS unit can be selected, given that it:

- Meets the requirements set out in the preceding sections;
- Ensures no significant negative impact on the upstream storm sewer system – to be determined via hydraulic modelling at detailed design; and
- Demonstrates suitability for meeting Enhanced water quality targets via a MECP Certificate of Technology Assessment.

The preliminary OGS units proposed in the following table have been sized to treat the stormwater runoff for the tributary areas noted in order to meet MECP Enhanced Level of Protection criteria as part of a treatment train approach prior to discharge to the Jock River via naturalized channels as shown on **Drawing 3**. The OGS total suspended removal rates and preliminary OGS unit details have been attached for reference in **Appendix D**.

Table 5: OGS Unit ID and Design Characteristics

Area and Unit ID ⁽¹⁾⁽²⁾	Drainage Area Target (ha)	Estimated Weighted C Value	Unit Treatment Capacity (L/s)	Unit Model ⁽¹⁾
Area 1 – OGS W1	8.92	0.70	255	CDS Model 5640-10
Area 2 – OGS W2	10.75	0.69	212	CDS Model 5653-10
Area 3 – OGS W3	6.30	0.64	255	CDS Model 4040-8
Area 4 – OGS W4	8.18	0.67	255	CDS Model 5640-10
(1) Providing at minimum 80% TSS removal (until such time that criteria for the MECP’s Consolidated Linear Infrastructure approach is in force at which time only 50% is attributed to OGS units). (2) See Drawing 3 for OGS unit locations. The “W” prefix in the numbering indicates ‘West’ development area.				

The above preliminary OGS unit sizing will achieve required quality controls and, along with other treatment train elements, will have additional beneficial TSS mitigation.

Groundwater

Paterson Group has reviewed the anticipated long term groundwater condition for the development area. Paterson drawing PG5036-10B in **Appendix D** demonstrates the long term groundwater elevation across the Conservancy West development area. The elevations range from ~88.5 m in the southern areas up to ~90 m in the northern areas. The lowest storm outlet at the southern boundary is 89.35 m (OGS W1) and all storm sewers, and any infiltration-type LIDs proposed within the development area, are above the anticipated long term groundwater elevation. Profiles for the storm sewers can be seen in **Drawing 5**.

5.4 Proposed Minor System

The subject property will be serviced by an internal gravity storm sewer system that is to generally follow the local road network and proposed servicing blocks as required. The drainage will be conveyed within the underground piped sewer system to headwall outlets located along the natural heritage corridor, providing hydration to naturalized outlet channels.

Street catchbasins will collect drainage from the streets and front yards, while rear yard catchbasins will capture drainage from backyards. Perforated catch basin leads will be provided in rear yards, except the last segment where they connect to the right-of-way which will be solid pipe, per City standards.

The preliminary rational method design of the minor system captures drainage for storm events up to and including the 2-year (local) and 5-year (collector).. The following table

summarizes the standards that will be employed in the detailed design of the storm sewer network. The preliminary drainage area information can be found in **Drawing 3** and rational method design sheets are provided in **Appendix D**.

Table 6: Storm Sewer Design Criteria

Design Parameter	Value
Minor System Design Return Period	1:2 year (PIEDTB-2016-01) for local roads, without ponding 1:5 year (PIEDTB-2016-01) for collector roads, without ponding 1:100 year (PIEDTB-2016-01) for arterial road, without ponding
Major System Design Return Period	1:100 year
Intensity Duration Frequency Curve (IDF) 2-year storm event: A=732.951 B=6.199 C=0.810 5-year storm event: A = 998.071 B = 6.053 C = 0.814	$i = \frac{A}{(t_c + B)^C}$
Minimum Time of Concentration	10 minutes
Rational Method	$Q = CiA$
Storm sewers are to be sized employing the Manning's Equation	$Q = \frac{1}{n} AR^{2/3} S^{1/2}$
Runoff coefficient for paved and roof areas	0.9
Runoff coefficient for landscaped areas	0.2
Minimum Sewer Size	250 mm diameter
Minimum Manning's 'n' for pipe flow	0.013
Minimum Depth of Cover	1.5 m from crown of sewer to grade
Minimum Full Flowing Velocity	0.8 m/s
Maximum Full Flowing Velocity	6.0 m/s
Clearance from 100-Year Hydraulic Grade Line to Building Opening	0.30 m
Design Parameter	Value
Max. Allowable Flow Depth on Municipal Roads	35 cm above gutter (PIEDTB-2016-01)
Extent of Major System	To be contained within the municipal ROW or adjacent to the ROW provided that the water level must not touch any part of the building envelope and must remain below the lowest building opening during the stress test event (100-year + 20%) and 15cm vertical clearance is maintained between spill elevation on the street and the ground elevation at the nearest building envelope (PIEDTB-2016-01)
Stormwater Management Model	DDSWMM (release 2.1), SWMHYMO (v. 5.02) and XPSWMM (v. 10)

Model Parameters	Fo = 76.2 mm/hr, Fc = 13.2 mm/hr, DCAY = 4.14/hr, D.Stor.Imp. = 1.57 mm, D.Stor.Per. = 4.67 mm
Imperviousness	Based on runoff coefficient (C) where Percent Imperviousness = (C - 0.2) / 0.7 x 100%.
Design Storms	Chicago 3-hour Design Storms and 24-hour SCS Type II Design Storms. Maximum intensity averaged over 10 minutes.
Historical Events	July 1st, 1979, August 4th, 1988 and August 8th, 1996
Climate Change Street Test	20% increase in the 100-year, 3-hour Chicago storm
<i>Extracted from City of Ottawa Sewer Design Guidelines, October 2012, and ISSU, and based on recent residential subdivisions in City of Ottawa.</i>	

The peak design flows are calculated based on an average predicted runoff coefficient (C-value) of 0.68 for the development area generally in keeping with the MIR and will require updating, 0.40 for park areas and 0.25 for grassed areas. The runoff coefficients are based on the proposed building envelopes, which have been established based on zoning setbacks and driveway widths and other details (i.e. ROW treatments etc).

There are several trunk sewers proposed and the peak flows are described for the trunk sewers which correspond to the stormwater management design areas as summarized in the following table:

Table 7: Minor System Trunk Sewer Outlets

Area/Outlet # (from east to west)	Trunk Sewer Outlet Headwall	Drainage Area Target (ha)	Peak Flow (L/s) & (L/s/ha)
1 (HW1)	1200 mm diameter @ 0.11%	8.92	953 / 107
2 (HW2)	1200 mm diameter @ 0.11%	10.75	1014 / 94
3 (HW3)	975 mm diameter @ 0.11%	6.30	582 / 92
4 (HW4)	1050 mm diameter @ 0.11%	8.18	699 / 85
Note: See rational design sheet in Appendix D for details.			

The storm sewers tributary to the various outlets, and associated peak flows, are detailed in the rational method design sheet, enclosed in **Appendix D**.

The conceptual servicing layout is shown on **Drawing 2** in **Drawings**. As detailed design progresses, alignment and sizing of local storm sewers will be confirmed and additional servicing blocks may be required, potentially triggering minor amendments to

the proposed lot fabric in the concept plan. The preliminary sanitary and storm trunk plan and profiles are shown on **Drawing 5 and 6** in **Drawings**.

Hydraulic Grade Line Analysis

A preliminary hydraulic grade line (HGL) modelling analysis has been completed by JFSA to demonstrate that the HGL will be maintained below the ground surface. See the JFSA memo entitled *Barrhaven Conservancy West– Preliminary HGL Analysis (December 2022)* in **Appendix D** for details/results. The analysis has been evaluated for various scenarios for the Jock River in order to assess the appropriate HGL boundary condition:

- 5-year water level in Jock River + 100yr rain event; or
- 100-year water level in Jock River + (2/5/10 yr) rain event (deemed to be the critical event).

The HGL results in JFSA's Table 1 (**Appendix D**) demonstrate that the freeboard to the ground surface ranges from 0.50 m to 1.16 m (with an average of 0.75 m) for the critical event noted above.

An updated HGL analysis will be completed for the proposed system at the detailed design stage, based on the above noted events, including historical design storms and climate change stress test as required.

5.5 Proposed Major System

Major system conveyance, or overland flow, will be provided to accommodate flows in excess of the minor system capacity. Overland flow is accommodated by generally storing stormwater up to the 100-year design event in road sags then routing additional surface flow along the road network and service easements towards the proposed stormwater outlets, discharging to the Jock River through the natural heritage corridors, as shown on **Drawing 1**. The grading design includes a saw-toothed-road design with 0.10% minimum grade from high point to high point in order to maximize available surface storage for management of flows up to the 100-year design event where possible.

5.6 Foundation Drainage (Sump Pumps)

Due to the grade raise restrictions and the proposed storm and sanitary drainage schemes, the road centerlines do not allow for standard basements with a gravity connection to the storm sewer system. As such, because of the constraints on the subject property, sump pumps are proposed to be installed for all residential blocks and residential lots.

The City of Ottawa issued Technical Bulletin *ISTB-2018-04* and *2019-02* for the amendment of the *Ottawa Design Guidelines – Sewer, Second Edition*, October 2012 with respect to the screening criteria for the use of sump pump systems for foundation drainage in Greenfield developments on sites with clay soils. Similar to the development of Conservancy Phase 1 and the Conservancy East (Phase 2) site, **Conservancy West** has also been assessed as meeting the required criteria for the use of sump pumps.

One of the screening criterion is with respect to the hydraulic grade line (HGL) for the development wherein the system should be reviewed to demonstrate that the HGL cannot reasonably be lowered any further due to outlet restrictions. The site grading is constrained by the close proximity of the Jock River, which is the receiver of stormwater outflows, and is also constrained by grade raise restrictions for the property.

For the Barrhaven **Conservancy West** Lands the grade raise restriction varies between 1.9 m and 2.2 m. Paterson's permissible grade raise plan is contained in **Appendix E** for reference (See Section 6 for discussion). Further investigations on the property and potential surcharging or lightweight fill (LWF) underneath garages could increase the permissible grade raise and will be investigated further as part of the detailed design.

The functional grading plan for the subdivision has been prepared with the grade raise restrictions in mind with grades being kept as low as possible.

The proposed centerline of road grades, and subsequently the house grades, do not allow for standard basements with a gravity connection to the storm sewer system. As such, the subdivision will be serviced entirely by sump pumps due to site constraints imposed by grade raise restrictions, HGL elevations and the proximity to the Jock River stormwater outlet.

5.7 Low Impact Development (LID) - Infiltration

The following general Low Impact Development (LID) techniques could be considered for implementation, where possible, as part of detailed design (noting that they have to be weighed against the objectives of the City's sump pump technical bulletins):

- Rear-yard swales should be designed with minimum grades where possible, to promote infiltration;
- Rear-yard catchbasin leads should be perforated (except for the last segment connecting to the storm sewer within the ROW), to promote infiltration; and,
- Where eavestroughs are provided on residential units, they are to be directed to landscaped surfaces, to promote infiltration.
- Furthermore, the following techniques can be examined as part of detailed landscaping design of the park block; and,
- Micro-grading can be considered to promote infiltration.

The long term groundwater anticipated is demonstrated on Paterson Drawing *PG5036-10B* in **Appendix D** as previously noted. The infiltration measure noted in Section 5.2 will contribute some infiltration and quality benefits as first flush stormwater is conveyed into the filtration trench. The amount of infiltration is dependent upon the surrounding soils, but the proposed design will optimize the potential on the site. JFSA has completed a high level water budget review of the site which is provided in **Appendix D** for reference.

To assess the water budget for the site under both pre- and post-development conditions, a SWMHYMO model was developed by JFSA. This model was run using 36 years of hourly rainfall data from the Ottawa International Airport from 1967 to 2003 (excluding missing 2001 rainfall data), the average annual runoff volumes from the subject site were computed and compared. The conceptual LIDs have been included in the model through the use of ROUTE RESERVOIR commands, which represent the storage volume and infiltration rates of each of these proposed LID features. After running each of the models for the 36 years, the annual runoff and infiltration results were extracted and the annual average water budget for each scenario calculated. Full summary tables for each year and scenario have been provided in Table A1 in **Appendix D**.

The analysis concludes that with the proposed LID the existing annual water infiltration volume can be met and exceeded. The extents of the LID system can be refined at detailed design to optimize LID locations and to minimize the extent of infrastructure to be maintained.

5.8 Existing Watercourses

Foster Ditch

The Foster Ditch borders the eastern boundary of the **Conservancy West** development area. It originates south of Fallowfield Road, west of Cedarview Road and flows south until it converges with the Jock River south of McKenna Casey Drive. The ditch is approximately 3,200 m long and has been artificially straightened. This non-municipal drain is a fish bearing tributary of the Jock River with approximately 335 ha of catchment area. The surrounding land use is urban and vacant lands. Riparian vegetation is very sparse consisting of mostly grasses with a few shrubs.

As noted in the **Jock River SWS**, to ensure protection of the aquatic habitat north of the Jock River, a development setback should be provided for all of the tributaries. Further studies will determine the development setback, which will be the greater of: 1) regulatory floodplain; 2) meander belt width; and 3) aquatic setback, whichever is greater.

Coordination will be undertaken for determinations of the appropriate culvert sizes and configuration for development road crossings of the Foster.

O’Keefe Municipal Drain

The O’Keefe Drain is located east of and runs parallel to Highway 416. The drain extends from south of Fallowfield Road and enters the Jock River south of McKenna Casey Drive. The drain is approximately 3,100 m in length and has been artificially straightened through development areas to the north and to follow the depression between agricultural lands through the subject property. The predominant land use is agricultural. The riparian vegetation consists mainly of grasses and some shrubs with thicker forested patches as the reach approaches the Jock River.

Coordination will be undertaken with the City’s Drainage group for determinations of the appropriate culvert sizes and configuration for development road crossings of the OMD. Initial sizing will be as per the Engineer’s Report for the O’Keefe Drain.

5.9 Floodplain

On November 8th 2019 the RCVA gave permission to Barrhaven Conservancy Development Corporation to cut and fill on the subject property under permit RV5 44/19 pursuant to review under Section 28 of the Conservation Authorities Act, regulation 174/06. The application and approval by the RVCA was supported by a 2D HEC-RAS model prepared by JFSA. The JFSA model identified the existing and proposed 100-year water levels and permissible extent of fill placement.

The works pursuant to the above-mentioned permit were completed and accepted by the RVCA on May 31st 2020. Options to complete the fill area boundary as set by JFSA included building a structural face of fill (retaining wall) to the limits of the 100-year floodplain boundary, or, building a berm with the toe of slope at the 100-year floodplain boundary. As-builts for the fill placement were subsequently provided and approved by the RVCA, resulting in the May 31st approval noted above and the current 100-year floodplain boundary delineation. The toe of any material placed corresponds to the approved 100-year floodplain line.

5.10 Stormwater Servicing Conclusions

The stormwater runoff is designed to be captured by an internal gravity sewer system that will convey flows to multiple outlet locations equipped with end of line OGS units. A proposed treatment train arrangement of 1.0 m deep sump catchbasins to optimize catchbasin sump retention of solids, as well as select catchbasin locations with connected infiltration-type subdrains will provide the required quality control treatment to achieve the Enhanced Level of protection. Downstream of the storm outlets along the southern development boundary will be naturalized channels where treated stormwater will be conveyed through the natural heritage corridor prior to discharge to the Jock

River. It is anticipated that quantity control is not required for the Jock River. Notwithstanding, some quantity control by means of erosion storage will be included.

A preliminary Hydraulic Grade Line (HGL) modelling analysis has been completed for the **Conservancy West** development area at this time and demonstrates that the HGL is maintained below the ground surface with freeboards ranging from 0.50 m to 1.16 m for critical event conditions. Further detailed HGL review will be completed for the proposed system at the detailed design stage. Due to the grade raise restrictions, and the proposed storm and sanitary drainage layout, the road centerlines do not allow for standard basements with a gravity connection to the storm sewer system. As such, because of the constraints on the subject property, sump pumps are proposed to be installed for all residential blocks and residential lots.

The **Conservancy West** development area will be outside of the Jock River's regulatory floodplain area.

Appropriate setbacks from existing watercourse are incorporated into the draft plan based on advancement/finalizing of studies to assess the various determining criteria.

6.0 GRADING

A site grading arrangement has been developed to optimize earthworks and provide major system conveyance to the receiving outlets, and naturalized channels, which ultimately outlet to the existing Jock River drainage network. The proposed grading can be found in **Drawing 1** in **Drawings**.

The development area is outside of the Jock River regulatory flood plain limits. The site grading will be a minimum of 0.50m above the 100-year regulatory limit event of the Jock River.

6.1 Geotechnical Conditions

Paterson completed a geotechnical investigation for the Conservancy West lands as follows:

- Geotechnical Investigation – Proposed Residential Development, Conservancy Lands West (Paterson Group, October 19, 2021);

The existing ground surface across the site is relatively level with approximate ground surface elevation varying between 91 m and 92 m. The subsurface profile generally consists of an approximate 50 mm to 360 mm thick layer of topsoil underlain by a silty clay deposit.

Due to the presence of a silty clay deposit, permissible grade raise restrictions are recommended for this site. The recommended permissible grade raise varies between 1.9 m to 2.2 m. Figure PG5036-5 '*Permissible Grade Raise Plan*' by Paterson is enclosed in **Appendix E** for reference. At the time of detailed design, efforts will be made to mitigate any exceedances and detailed review and signoff by a licensed Geotechnical Engineer will be required. Where grade raises exceed the permissible levels the Engineer will recommend appropriate measures to mitigate where required (i.e. light weight fill or pre-consolidation etc).

The following additional grading criteria and guidelines will be applied to detailed design, per **City of Ottawa Guidelines**:

- Driveway slopes will have a maximum slope of 6%;
- Grading in grassed/landscaped areas to range from 2% to 3:1, with terracing required for slopes larger than 7%;
- Swales are to be 0.15m deep with 3:1 side slopes unless otherwise indicated on the drawings; and,
- Perforated pipe will be required for drainage swales if they are less than 1.5% in slope.

The geotechnical analysis of the site, published under separate cover in support of the development applications, provides additional information about the suitability of the site for the proposed services and grading scheme. At the time of detailed design, detailed review and signoff by a licensed Geotechnical Engineer will be required.

7.0 EROSION AND SEDIMENT CONTROL

Soil erosion occurs naturally and is a function of soil type, climate and topography. The extent of erosion losses is exaggerated during construction where vegetation has been removed and the top layer of soil becomes agitated.

Prior to topsoil stripping, earthworks or underground construction, erosion and sediment controls are implemented and will be maintained throughout any construction phase.

The following specific recommendations to the Contractor will be included in contract documents.

- Limit extent of exposed soils at any given time.
- Re-vegetate exposed areas as soon as possible.
- Minimize the area to be cleared and grubbed.
- Protect exposed slopes with plastic or synthetic mulches.
- Install silt fence to prevent sediment from leaving the site and entering existing watercourses, and clean and maintain throughout construction.
- Install catchbasin inserts during construction to protect from silt entering the storm sewer system.
- Install mud mats in order to prevent mud tracking onto adjacent roadways.
- No refueling or cleaning of equipment near existing watercourses.
- No material stockpiles within 30m of existing watercourses, unless otherwise permitted by RVCA and City of Ottawa.
- Provide sediment traps and basins during dewatering.
- Plan construction at proper time to avoid flooding.
- The Contractor will, at every rainfall, complete inspections to ensure proper performance.
- Erosion and sediment controls will remain in place until the working areas have been stabilized and re-vegetated.

8.0 UTILITIES

Utility services extending to the site may require connections to multiple existing infrastructure points: consultation with Enbridge gas, Hydro Ottawa, Rogers, and Bell is required as part of the development process to confirm the servicing plan for the subject lands.

9.0 CONCLUSION AND RECOMMENDATIONS

This AES provides details on the planned on-site municipal services for the subject property and demonstrates that adequate municipal infrastructure capacity is expected to be available for the planned development of the subject property.

- The subject lands have been reviewed by Stantec to confirm that servicing is feasible by City of Ottawa PZ SUC. Several alternatives were presented to confirm that servicing is feasible. The water supply network will be expanded through neighboring properties to meet the water demands of the proposed concept plan, via the trunk watermain network and local watermains identified. Detailed modelling will confirm phasing of the extensions of trunk watermains and sizing of the local watermain network.
- The subject property will be serviced by local sanitary sewers, an on-site trunk sanitary sewer, and the off-site SNC sanitary sewer as defined in previous reports. This AES continues to confirm that the expansion of the drainage areas from the **2019 Novatech SNC Memo** to include the entirety of the subject property has no negative impacts. There is residual capacity in the downstream SNC providing sufficient capacity for the peak sanitary flows for the subject property, including external commercial and community park flows. Flows projected for this development area are lower than flows previously projected in the Conservancy East development downstream.
- Stormwater service is to be provided by capturing stormwater runoff by an internal gravity sewer system that will convey flows to various outlets along the southern boundary to proposed naturalized channels. Prior to discharge from the development, any first flush stormwater will have passed through an end of line OGS unit for quality control. The OGS units will provide an Enhanced Level of Protection quality control treatment for stormwater in combination with an upstream treatment train of measures such as 1.0 m deep catchbasin sumps and LID system prior to discharge from the development. It is anticipated that quantity control will not be required for discharges to the Jock River.
- A preliminary Hydraulic Grade Line (HGL) modelling analysis has been completed at this time and demonstrates that the HGL is maintained below the

ground surface. Another detailed HGL review will be completed for the proposed system at the detailed design level.

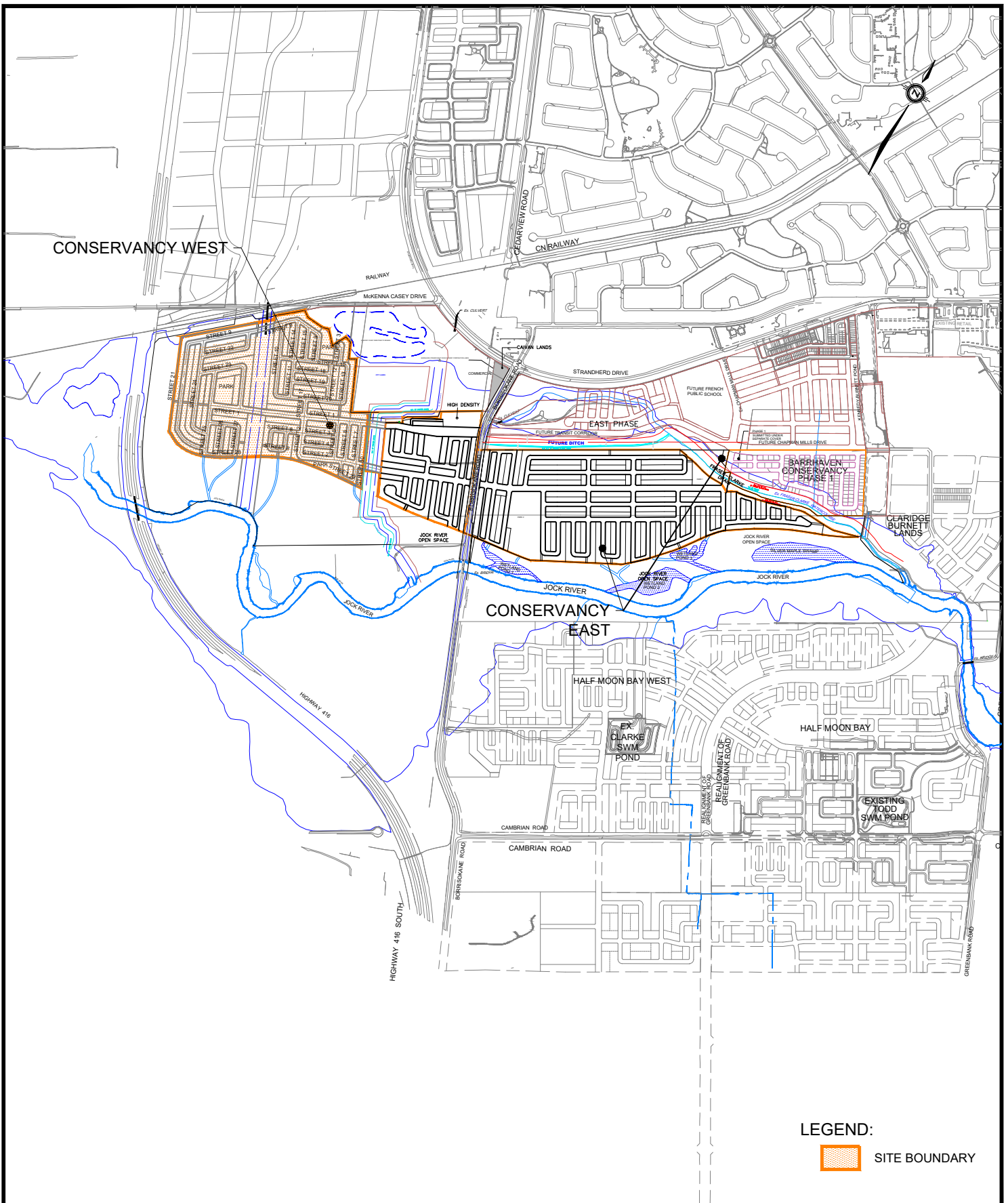
- A preliminary water budget analysis has been completed by JFSA at this time and indicates that pre-development infiltration levels can be met.
- Sump pumps are proposed to be installed for all units within residential blocks and lots;
- The site will be subject to grade raise restrictions ranging from 1.9 m to 2.2 m;
- The proposed servicing and grading plans are expected to meet all City, RVCA, and MECP requirements as set out in background studies and current standards.
- Prior to detailed design of the infrastructure presented in this report, this AES will require approval under the Planning Act as supporting information for the Plan of Subdivision application. Project-specific approvals are also expected to be required for the infrastructure presented in this report from the City of Ottawa, MECP, and Rideau Valley Conservation Authority, among other agencies.

Prepared by,
David Schaeffer Engineering Ltd.



Per: Kevin L. Murphy, P.Eng.

FIGURES & DRAWINGS



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BARRHAVEN CONSERVANCY WEST

KEY PLAN

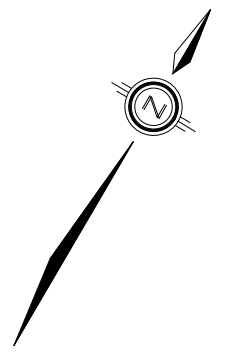
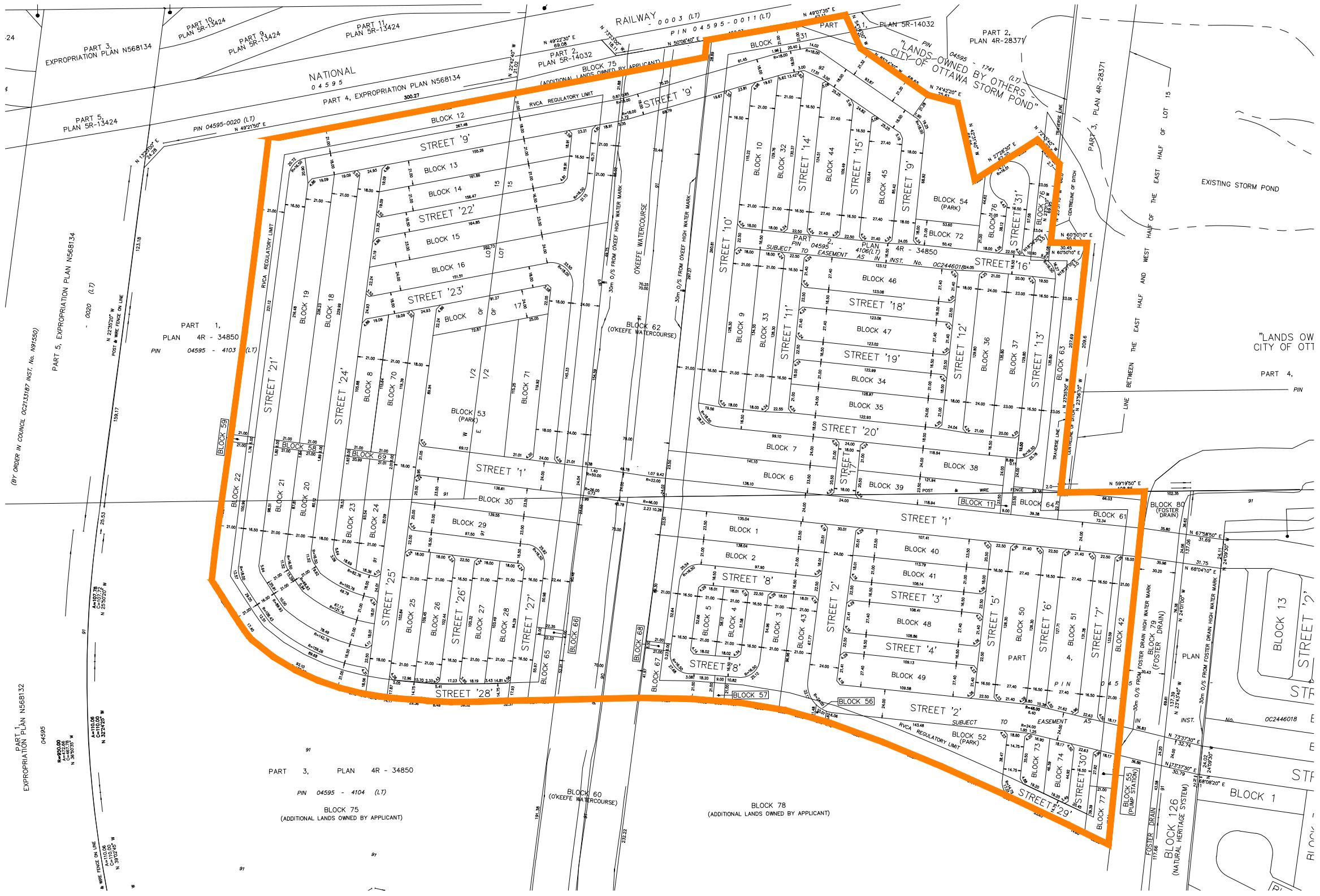
CITY OF OTTAWA

DATE: DECEMBER 2022

SCALE: 1:20000

PROJECT No.: 20-1226

FIGURE: 1



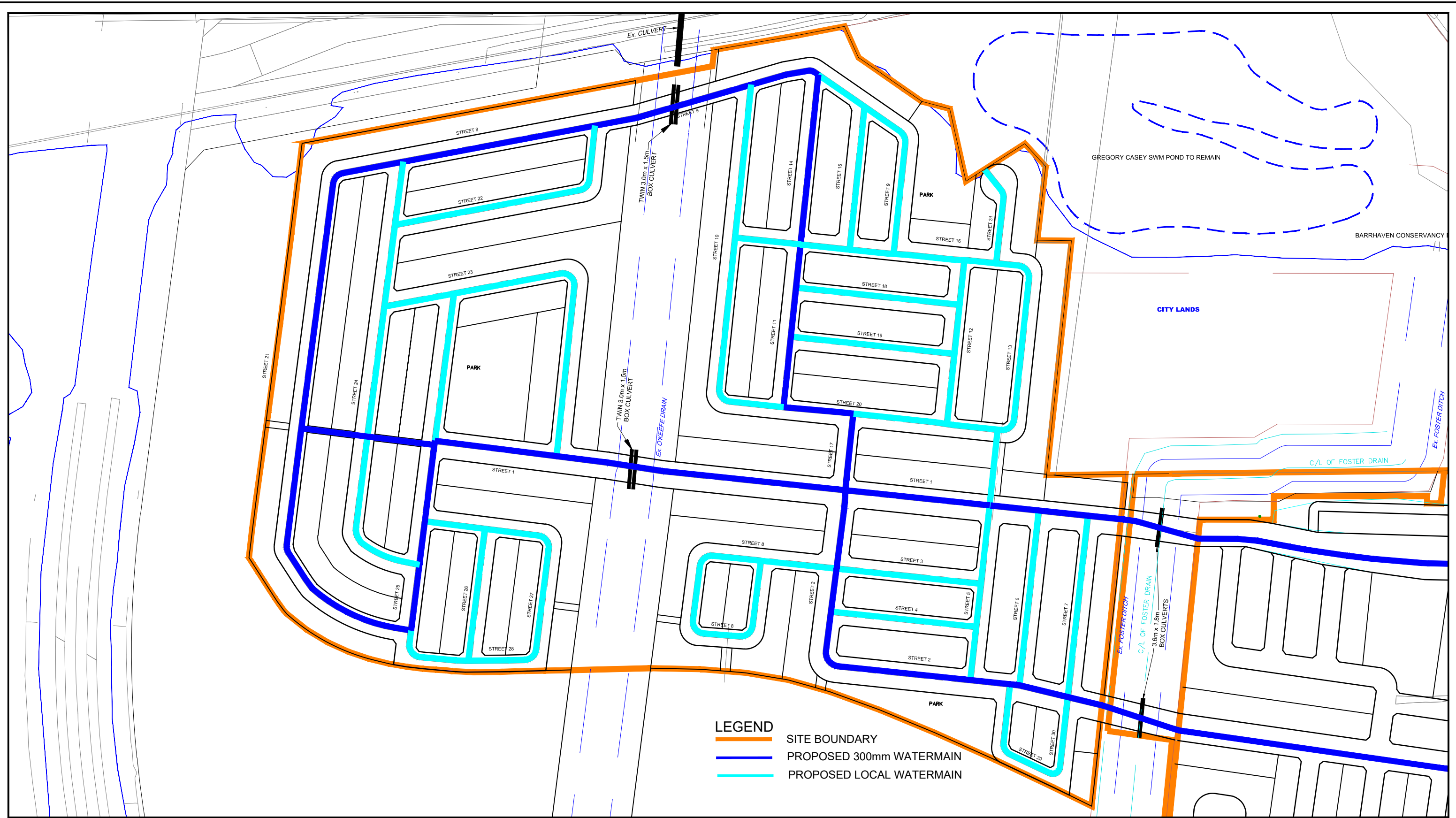
LEGEND:
 SITE BOUNDARY



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**BARRHAVEN CONSERVANCY WEST
 SUBDIVISION PLAN
 CITY OF OTTAWA**

PROJECT No.:	20-1226
SCALE:	NTS
DATE:	DECEMBER 2022
FIGURE:	2



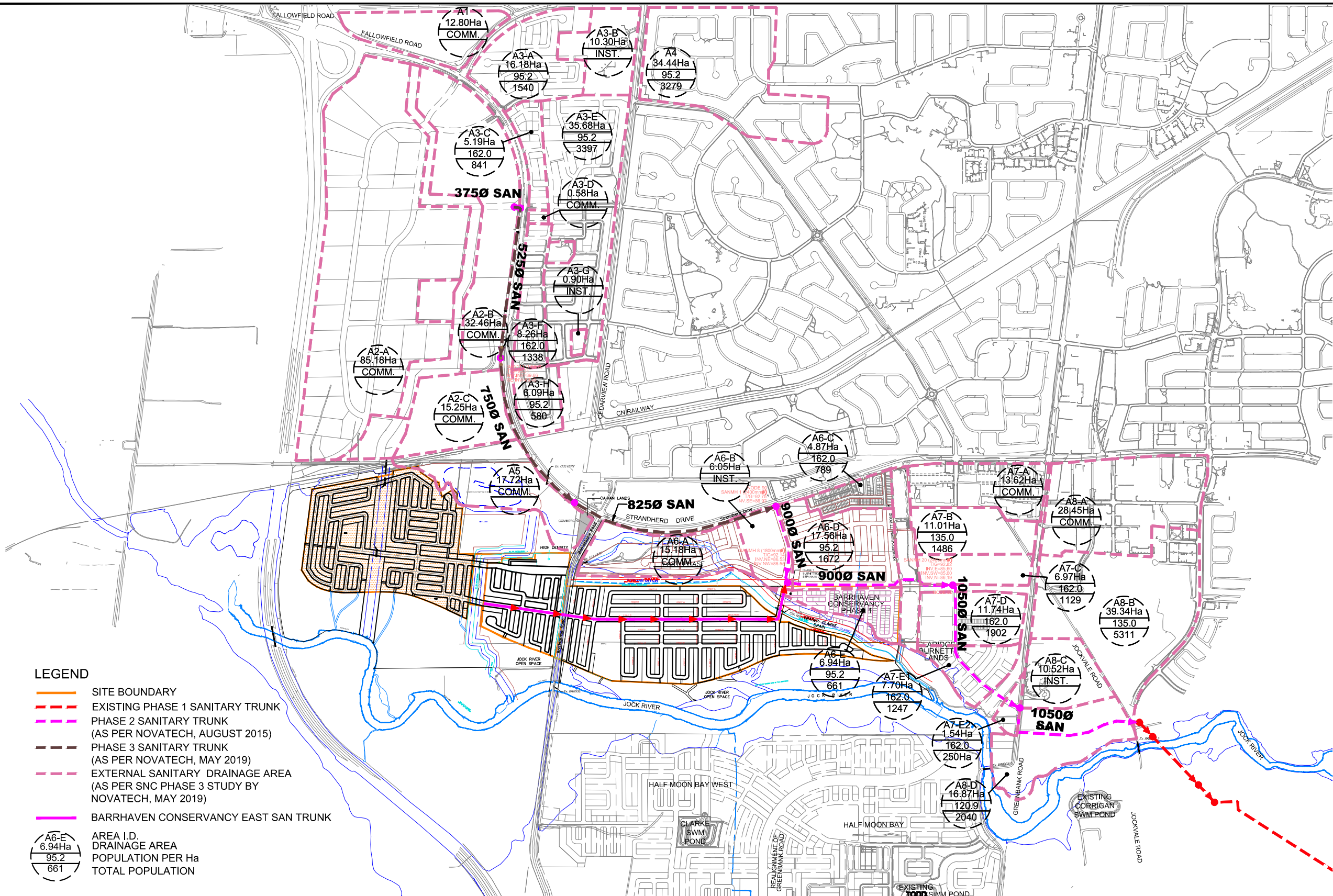
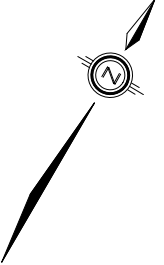
- LEGEND**
- SITE BOUNDARY
 - PROPOSED 300mm WATERMAIN
 - PROPOSED LOCAL WATERMAIN



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**BARRHAVEN CONSERVANCY WEST
 WATERMAIN SERVICING PLAN
 CITY OF OTTAWA**

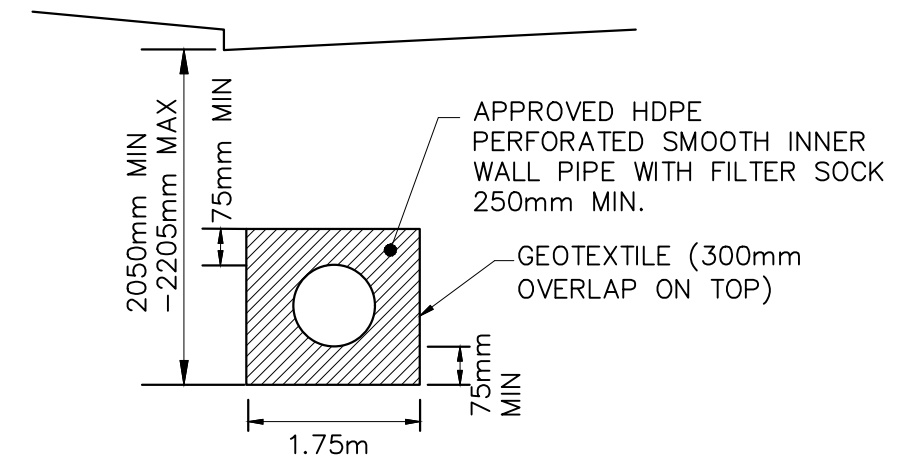
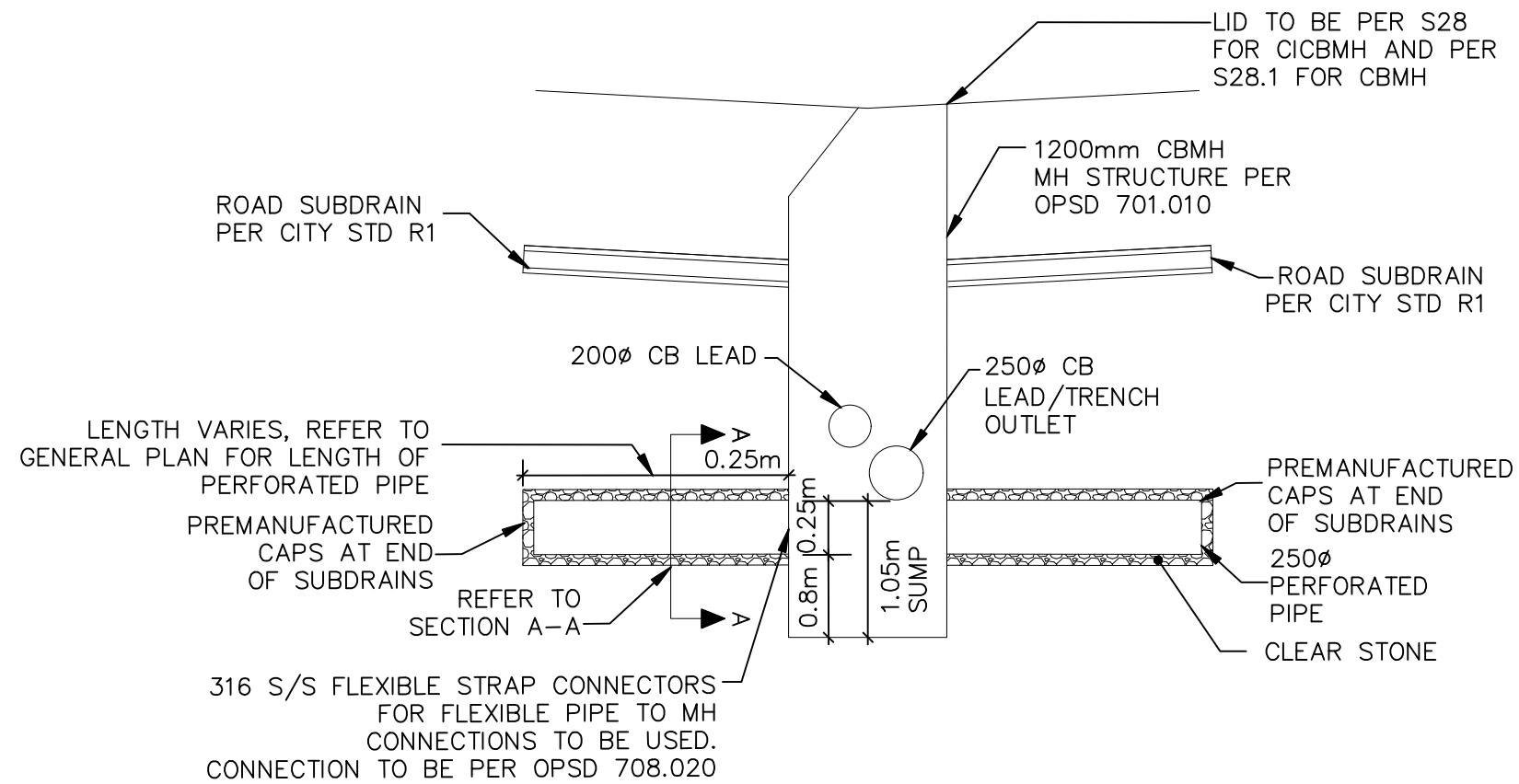
PROJECT No.:	20-1226
SCALE:	1:3000
DATE:	DECEMBER 2022
FIGURE:	3



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**BARRHAVEN CONSERVANCY WEST
EXTERNAL SANITARY SERVICING
CITY OF OTTAWA**

PROJECT No.:	20-1226
SCALE:	1:18000
DATE:	DECEMBER 2022
FIGURE:	4



SECTION A-A
SCALE: N.T.S.

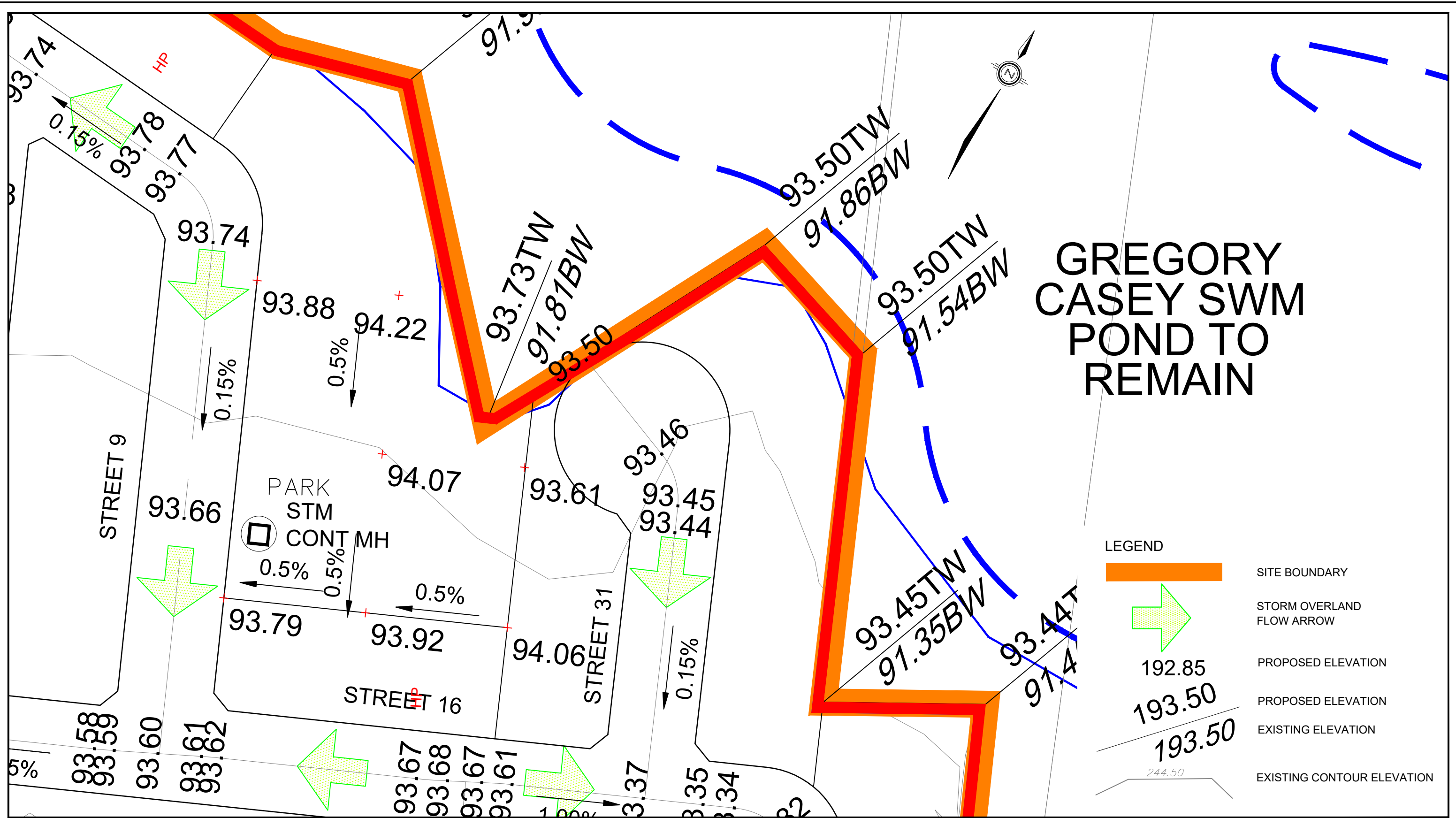
INFILTRATION TRENCH DETAIL FOR CBMHs
SCALE: N.T.S.




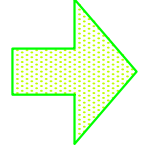
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BARRHAVEN CONSERVANCY WEST
FILTRATION SYSTEM DETAILS
CITY OF OTTAWA

PROJECT No.:	20-1226
SCALE:	NTS
DATE:	DECEMBER 2022
FIGURE:	5



GREGORY CASEY SWM POND TO REMAIN

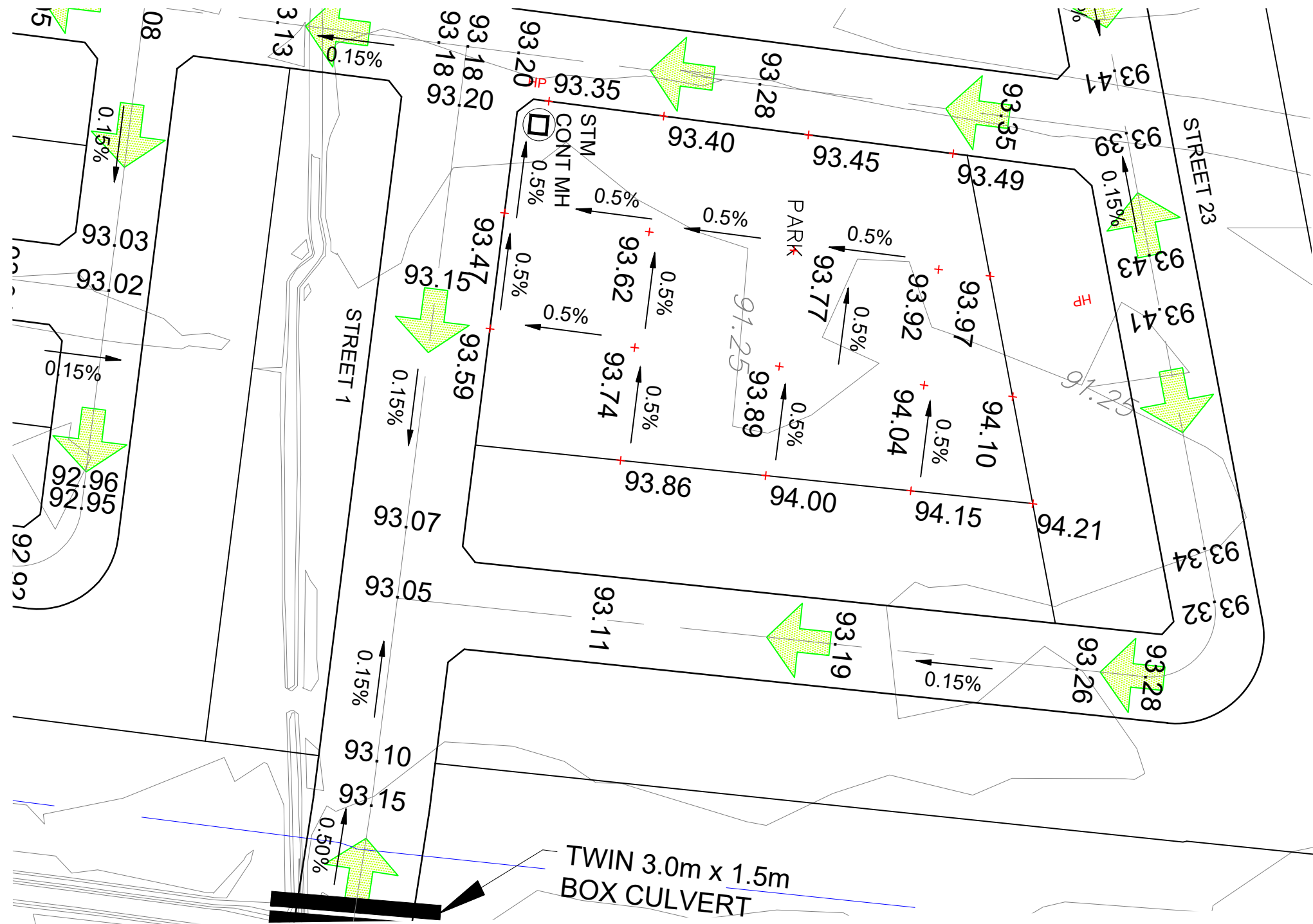
LEGEND	
	SITE BOUNDARY
	STORM OVERLAND FLOW ARROW
192.85	PROPOSED ELEVATION
193.50	PROPOSED ELEVATION
193.50	EXISTING ELEVATION
244.50	EXISTING CONTOUR ELEVATION



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BARRHAVEN CONSERVANCY
 CONCEPTUAL PARK 1 GRADING PLAN
 CITY OF OTTAWA

PROJECT No.:	20-1226
SCALE:	1:1500
DATE:	DECEMBER 2022
FIGURE:	6



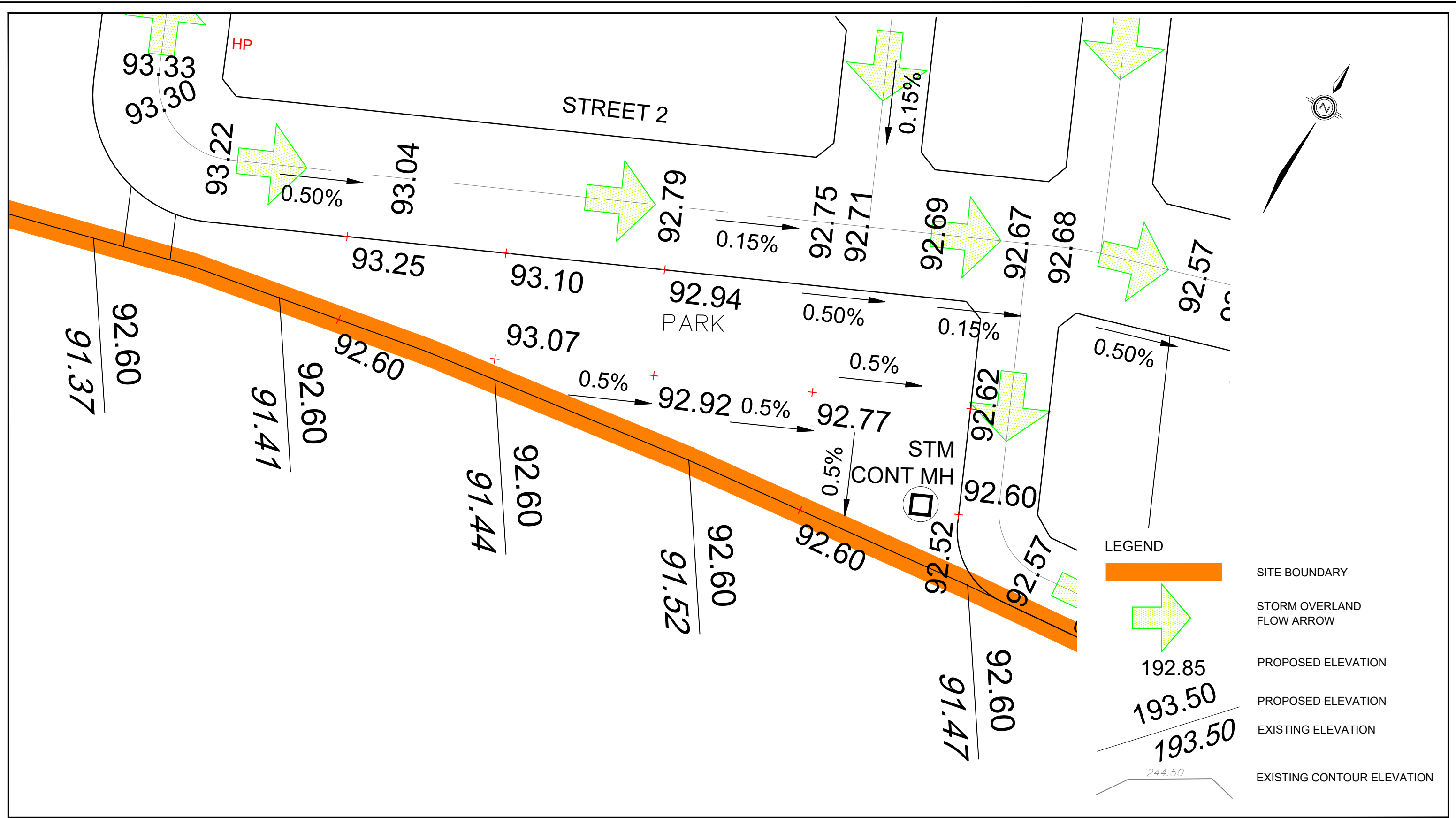
LEGEND	
	SITE BOUNDARY
	STORM OVERLAND FLOW ARROW
192.85	PROPOSED ELEVATION
193.50	PROPOSED ELEVATION
193.50	EXISTING ELEVATION
	EXISTING CONTOUR ELEVATION



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BARRHAVEN CONSERVANCY EAST
 CONCEPTUAL PARK 2 GRADING PLAN
 CITY OF OTTAWA

PROJECT No.:	1180
SCALE:	1:1000
DATE:	DECEMBER 2021
FIGURE:	7



LEGEND

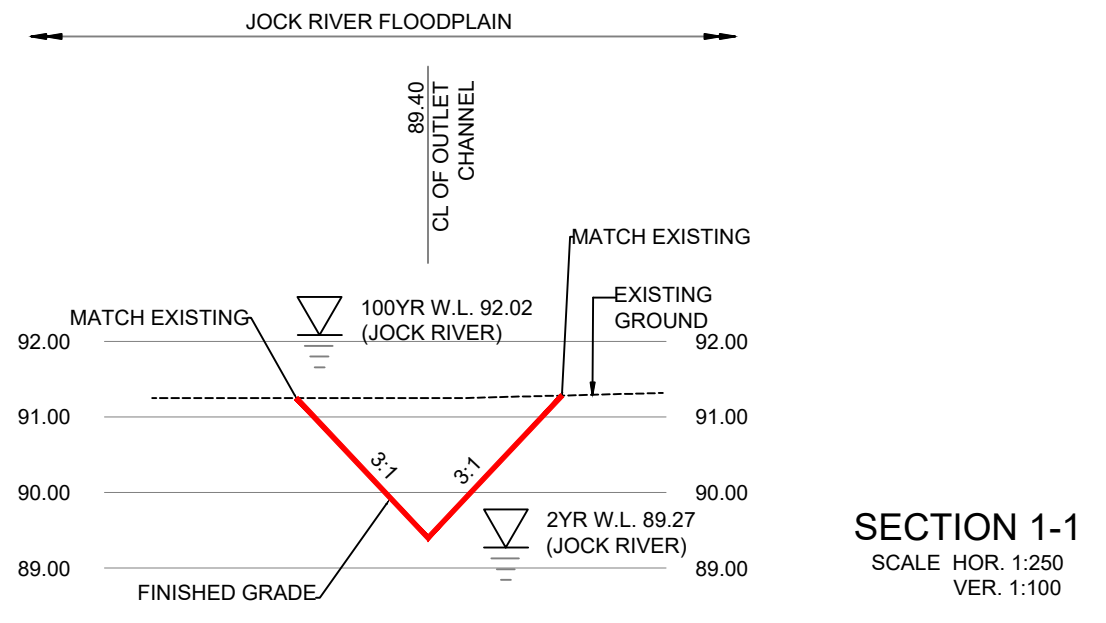
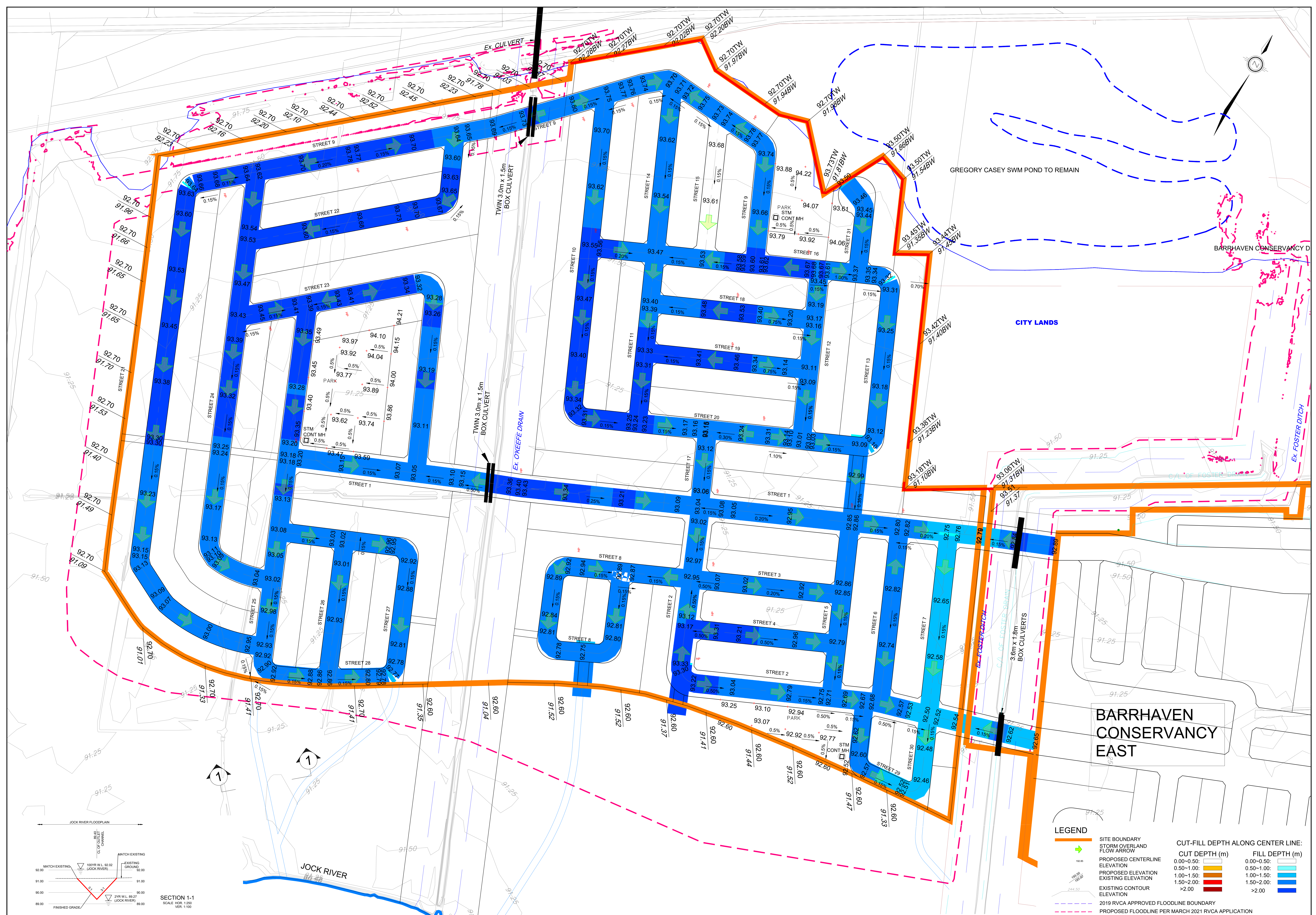
- SITE BOUNDARY
- STORM OVERLAND FLOW ARROW
- PROPOSED ELEVATION
- PROPOSED ELEVATION
- EXISTING ELEVATION
- EXISTING CONTOUR ELEVATION



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**BARRHAVEN CONSERVANCY
 CONCEPTUAL PARK 3 GRADING PLAN
 CITY OF OTTAWA**

PROJECT No.:	20-1226
SCALE:	1:1500
DATE:	DECEMBER 2022
FIGURE:	8



LEGEND

- Orange line: SITE BOUNDARY
- Green arrow: STORM OVERLAND FLOW ARROW
- Blue dashed line: PROPOSED CENTERLINE ELEVATION
- Red dashed line: PROPOSED ELEVATION
- Black dashed line: EXISTING CONTOUR ELEVATION
- Black dashed line: 2019 RVCA APPROVED FLOODLINE BOUNDARY
- Pink dashed line: PROPOSED FLOODLINE PER MARCH 2021 RVCA APPLICATION

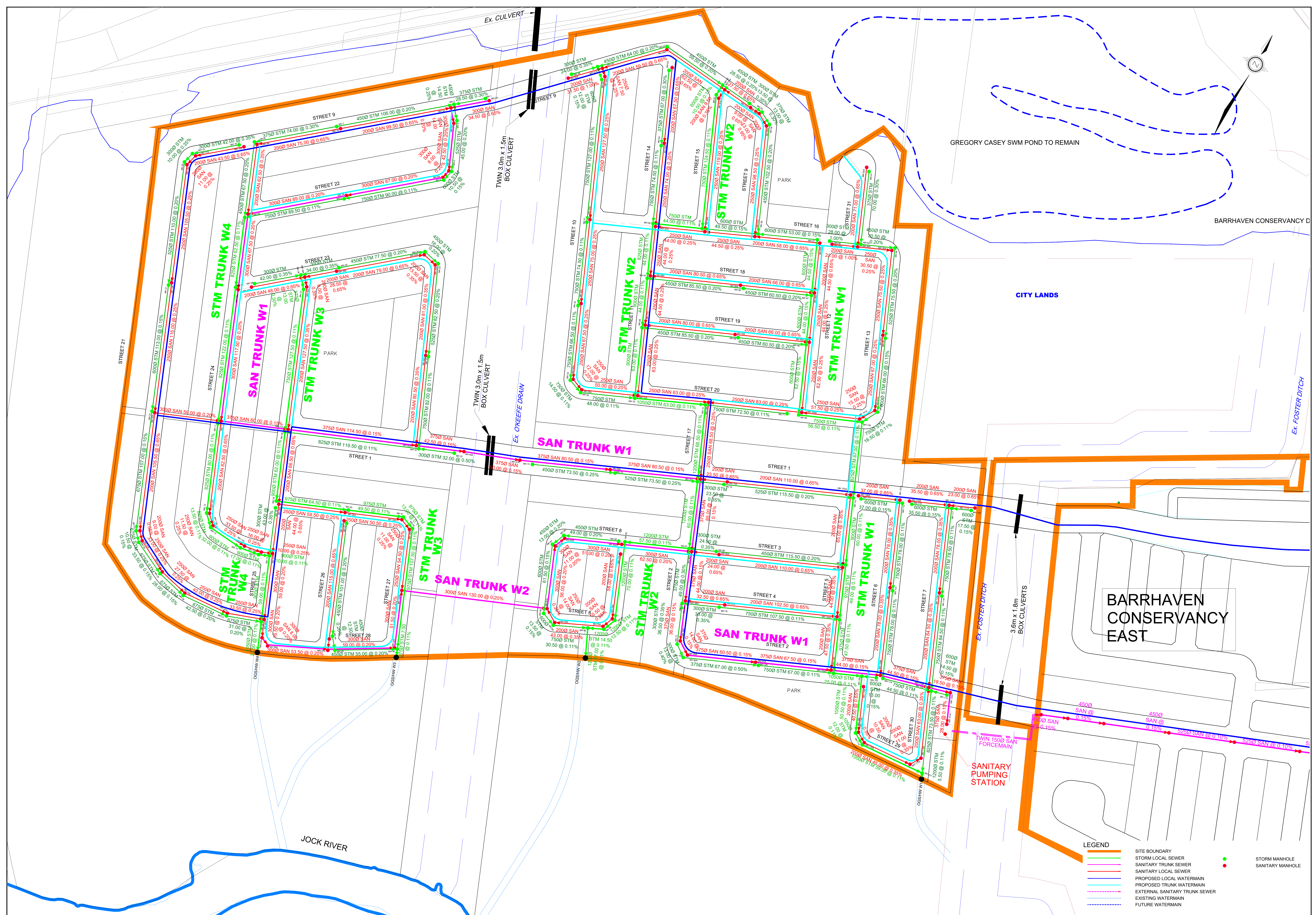
CUT-FILL DEPTH ALONG CENTER LINE:	CUT-DEPTH (m)		FILL DEPTH (m)	
	0.00-0.50	0.50-1.00	0.00-0.50	0.50-1.00
0.00-0.50	Light Blue	Light Blue	Light Blue	Light Blue
0.50-1.00	Yellow	Yellow	Light Blue	Light Blue
1.00-1.50	Orange	Orange	Light Blue	Light Blue
1.50-2.00	Red	Red	Light Blue	Light Blue
>2.00	Dark Red	Dark Red	Light Blue	Light Blue



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BARRHAVEN CONSERVANCY WEST
CONCEPTUAL GRADING PLAN
CITY OF OTTAWA

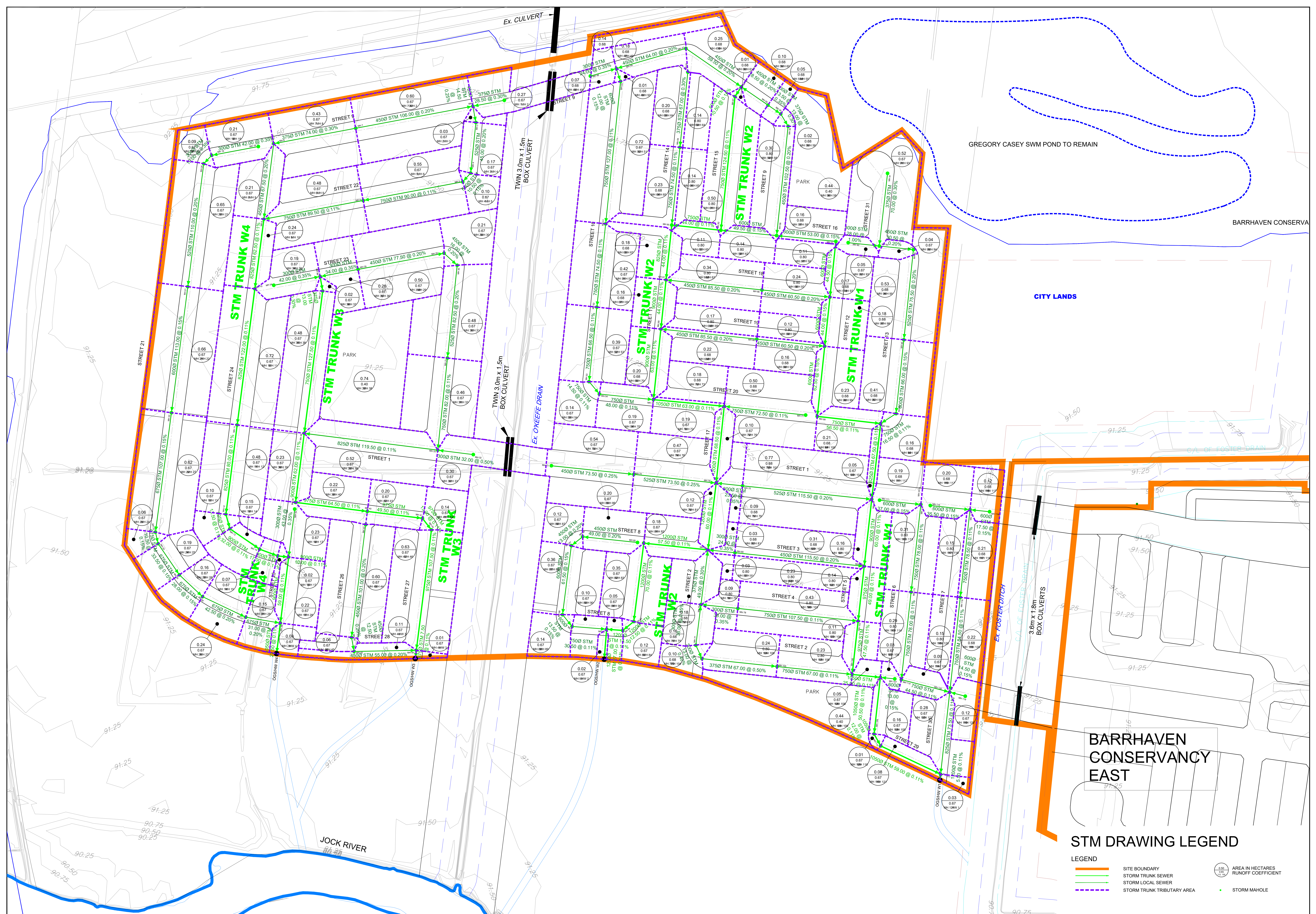
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SCALE: 1:1000
DATE: DECEMBER 2022
DRAWING No. 1



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BARRHAVEN CONSERVANCY WEST
 CONCEPTUAL SERVICING PLAN
 CITY OF OTTAWA

PROJECT No. : 20-1226
 SCALE: 1:1000
 DATE: DECEMBER 2022
 DRAWING No. 2



BARRHAVEN CONSERVANCY WEST
 STORM TRIBUTARY AREA
 CITY OF OTTAWA

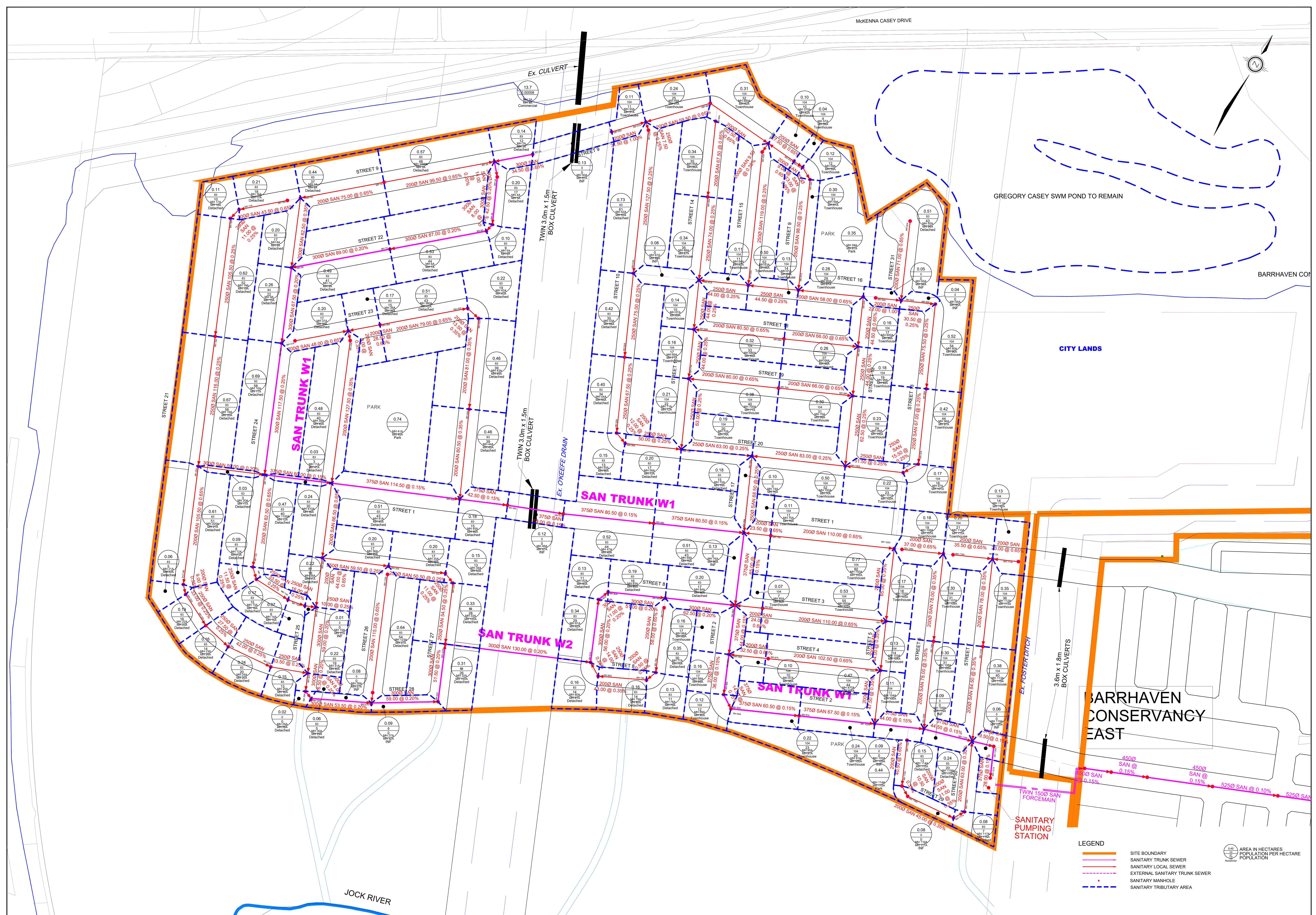
STM DRAWING LEGEND

LEGEND	
	SITE BOUNDARY
	STORM TRUNK SEWER
	STORM LOCAL SEWER
	STORM TRUNK TRIBUTARY AREA
	AREA IN HECTARES RUNOFF COEFFICIENT
	STORM MAHOLE



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PROJECT No.: 20-1226
 SCALE: 1:1000
 DATE: DECEMBER 2022
 DRAWING No. 3

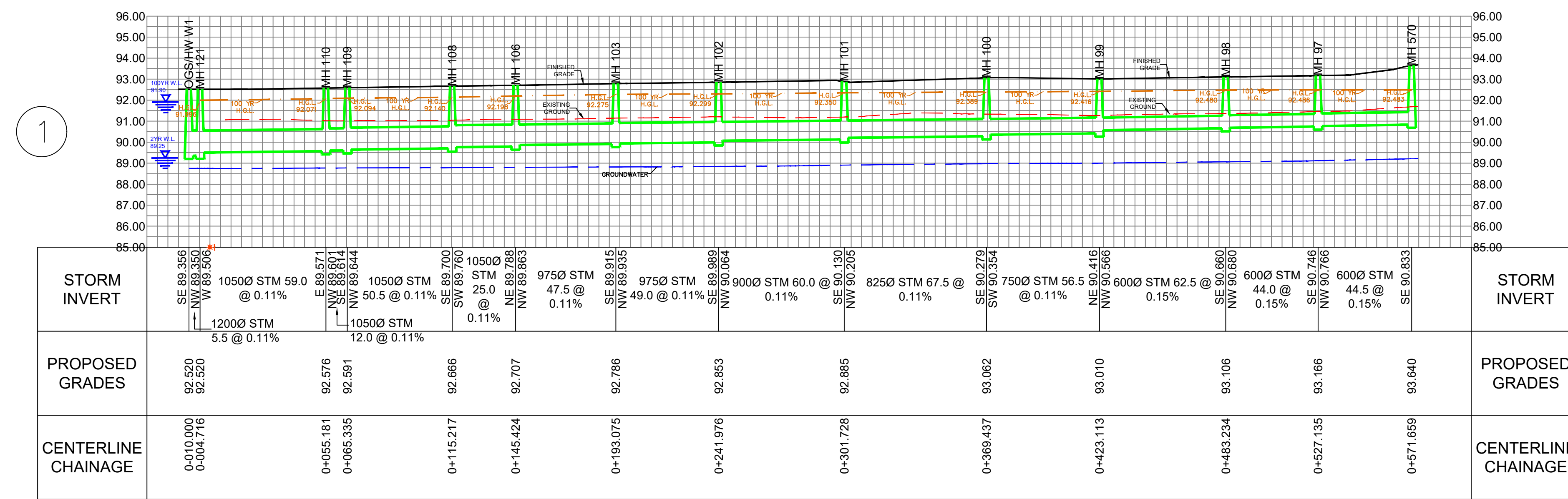


LEGEND

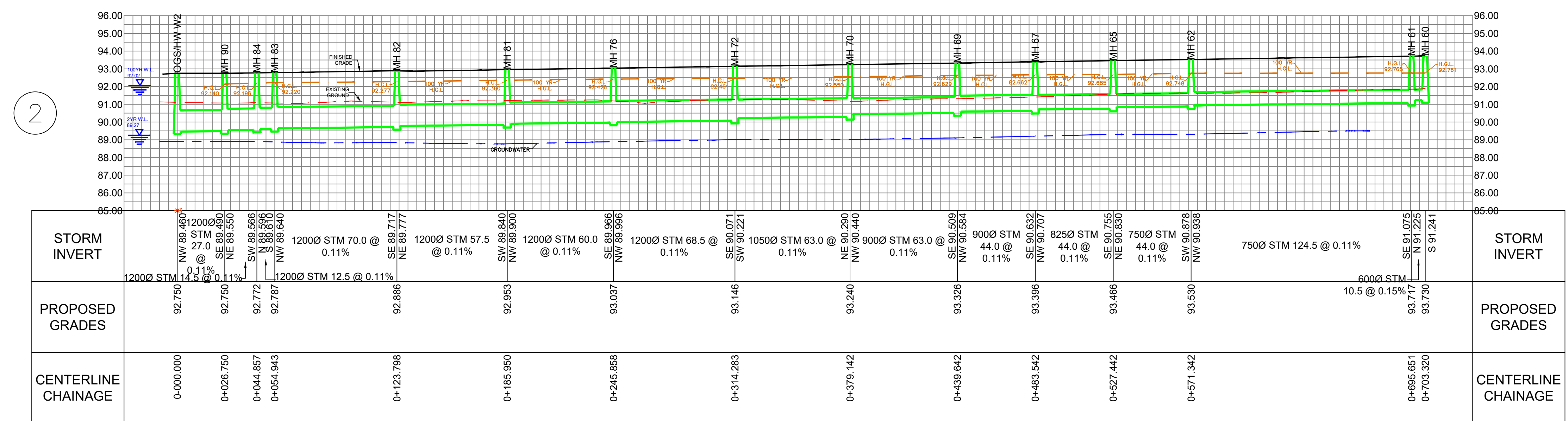
- SITE BOUNDARY
- SANITARY TRUNK SEWER
- SANITARY LOCAL SEWER
- EXTERNAL SANITARY TRUNK SEWER
- SANITARY MANHOLE
- SANITARY TRIBUTARY AREA

0.44 AREA IN HECTARES
POPULATION PER HECTARE
POPULATION

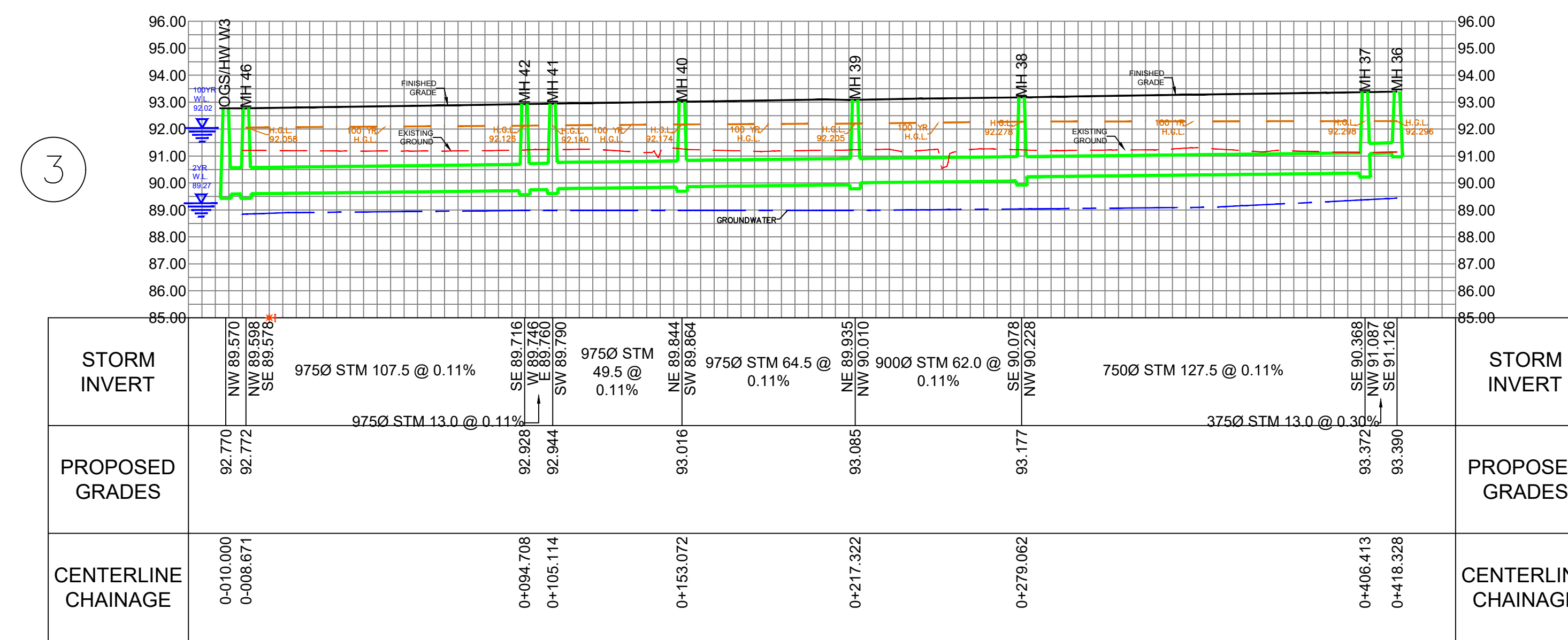
STM TRUNK W1



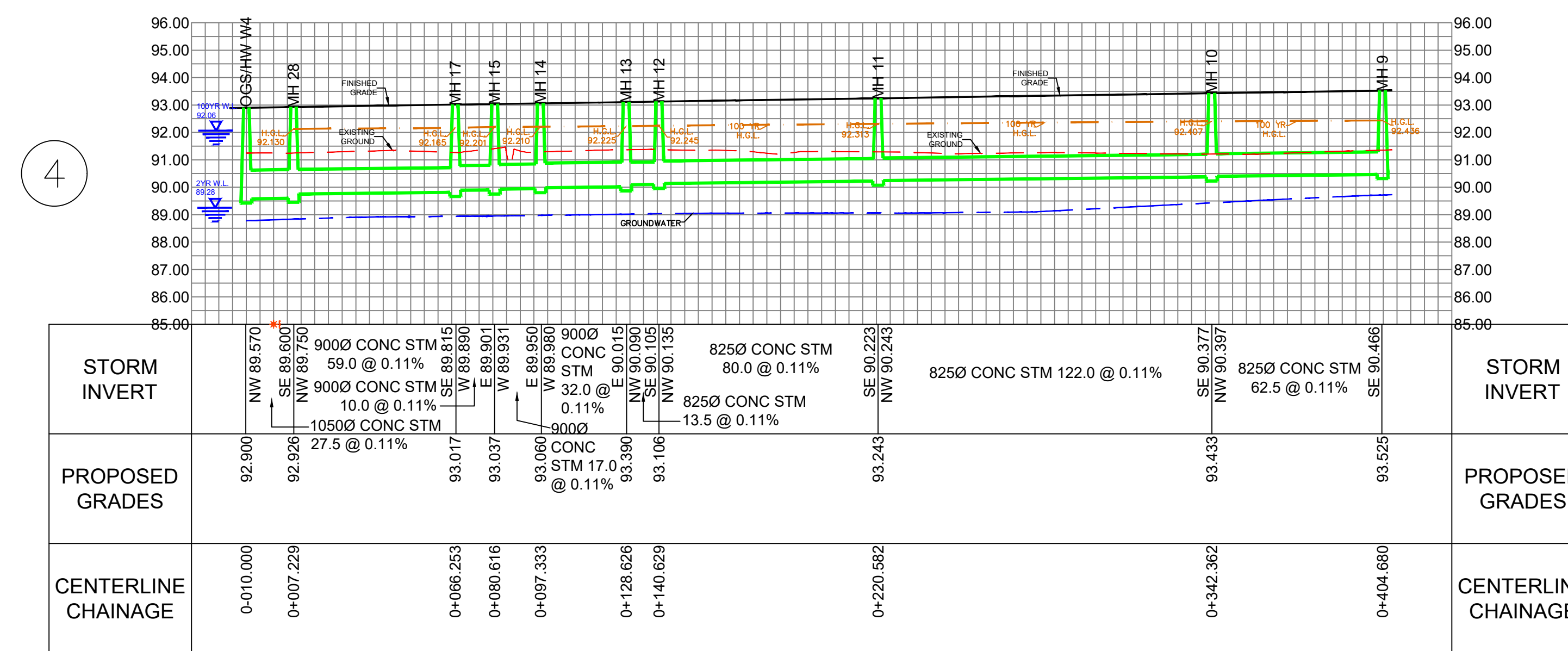
STM TRUNK W2



STM TRUNK W3



STM TRUNK W4

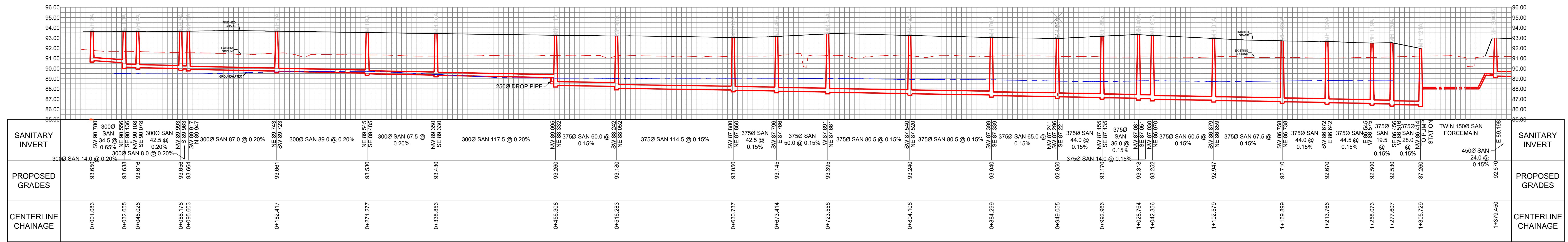


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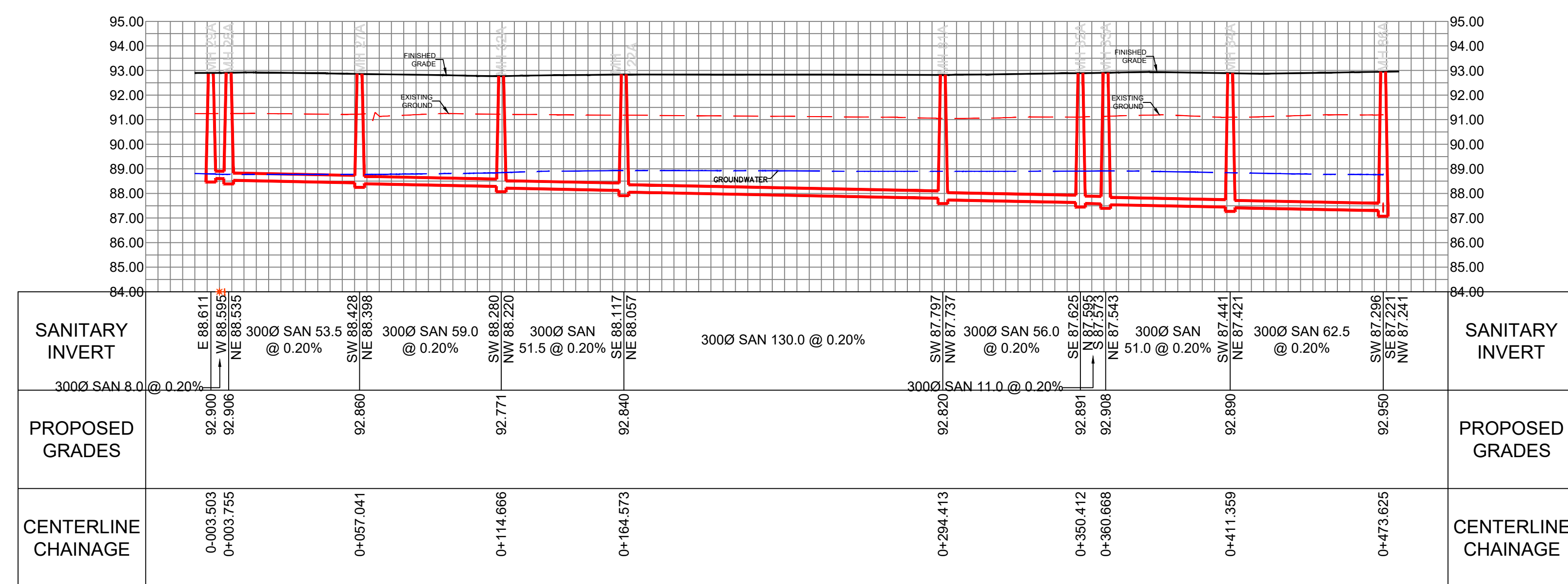
BARRHAVEN CONSERVANCY WEST STORM TRUNK PROFILES CITY OF OTTAWA

PROJECT No. : 20-1226
SCALE: 1:1500
DATE: DECEMBER 2022
DRAWING No. 5

SAN TRUNK W1



SAN TRUNK W2



SANITARY SEWER NOTE:
 WHERE SANITARY SEWER ARE PLACED BELOW THE LONG TERM GROUND WATER LEVEL AS DETERMINED BY GEOTECHNICAL ENGINEER, MH SECTIONS ARE TO BE SEALED TIGHT AND HAVE A MEMBRANE ON THE OUTSIDE PLUS BLUE SKIN WRAPPING. WATERMAIN GRADE PVC SEWER PIPE TO BE USED FOR SANITARY PIPES. GLUED PIPE SECTIONS ARE NOT PERMITTED.



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BARRHAVEN CONSERVANCY WEST
 SANITARY TRUNK PROFILES
 CITY OF OTTAWA

PROJECT No. : 20-1226
 SCALE: 1:1500
 DATE: DECEMBER 2022
 DRAWING No. 6

APPENDIX A

GENERAL

Content Copy Of Original



Ministry of the Environment and Climate Change
Ministère de l'Environnement et de l'Action en matière de changement
climatique

ENVIRONMENTAL COMPLIANCE APPROVAL

NUMBER 8129-AB7LDF

Issue Date: June 23, 2016

City of Ottawa
100 Constellation Crescent West, 6th Floor
Ottawa, Ontario
K2G 6J8

Site Location: Jockvale Road and Strandherd Drive
City of Ottawa, Ontario

You have applied under section 20.2 of Part II.1 of the Environmental Protection Act, R.S.O. 1990, c. E. 19 (Environmental Protection Act) for approval of:

sanitary sewers to be constructed in the City of Ottawa, on various vacant development lands (from Station 0+003 to Station 2+517), Greenbank Road (from Station 1+846 to Station 1+947), and Jockvale Road (from Station 2+430 to Station 2+517);

all in accordance with the application form from the City of Ottawa, dated June 22, 2016, including final plans and specifications prepared by Novatech Engineers, Planners and Landscape Architects.

In accordance with Section 139 of the Environmental Protection Act, you may by written Notice served upon me and the Environmental Review Tribunal within 15 days after receipt of this Notice, require a hearing by the Tribunal. Section 142 of the Environmental Protection Act provides that the Notice requiring the hearing shall state:

1. The portions of the environmental compliance approval or each term or condition in the environmental compliance approval in respect of which the hearing is required, and;
2. The grounds on which you intend to rely at the hearing in relation to each portion appealed.

The Notice should also include:

3. The name of the appellant;
4. The address of the appellant;
5. The environmental compliance approval number;
6. The date of the environmental compliance approval;
7. The name of the Director, and;
8. The municipality or municipalities within which the project is to be engaged in.

And the Notice should be signed and dated by the appellant.

This Notice must be served upon:

The Secretary*
Environmental Review Tribunal
655 Bay Street, Suite 1500

AND

The Director appointed for the
purposes of Part II.1 of the
Environmental Protection Act

Toronto, Ontario
M5G 1E5

Ministry of the Environment and
Climate Change
135 St. Clair Avenue West, 1st
Floor
Toronto, Ontario
M4V 1P5

*** Further information on the Environmental Review Tribunal's requirements for an appeal can be obtained directly from the Tribunal at: Tel: (416) 212-6349, Fax: (416) 326-5370 or www.ert.gov.on.ca**

The above noted activity is approved under s.20.3 of Part II.1 of the Environmental Protection Act.

DATED AT TORONTO this 23rd day of June, 2016

Gregory Zimmer, P.Eng.
Director
appointed for the purposes of Part II.1 of
the *Environmental Protection Act*

AF/
c: District Manager, MOECC Ottawa
Water Supervisor, MOECC, Ottawa
M. Rick O'Connor, City Clerk, City of Ottawa
Luc Marineau, City of Ottawa
Jonathan Knoyle, City of Ottawa
Bob Dowdall, Novatech Engineers, Planners and Landscape Architects
Edson Donnelly, Novatech Engineers, Planners and Landscape Architects

APPENDIX B
WATER SUPPLY



**BARRHAVEN CONSERVANCY WEST:
WATER DISTRIBUTION SYSTEM
ANALYSIS**
Final Report

January 13, 2023

Prepared for:
David Schaeffer Engineering Ltd.

Prepared by:
Stantec Consulting Ltd.

Project Number:
163401817

Barrhaven Conservancy West: Water Distribution System Analysis

Revision	Description	Author	Date	Quality Check	Date	Independent Review	Date
0	Draft	AMG	20221219	AP	20221219	AP	20221219
1	Final	AMG	20230111	AP	20230113	AP	20230113



Barrhaven Conservancy West: Water Distribution System Analysis

The conclusions in the Report titled **Barrhaven Conservancy West: Water Distribution System Analysis** are Stantec's professional opinion, as of the time of the Report, and concerning the scope described in the Report. The opinions in the document are based on conditions and information existing at the time the scope of work was conducted and do not take into account any subsequent changes. The Report relates solely to the specific project for which Stantec was retained and the stated purpose for which the Report was prepared. The Report is not to be used or relied on for any variation or extension of the project, or for any other project or purpose, and any unauthorized use or reliance is at the recipient's own risk.

Stantec has assumed all information received from David Schaeffer Engineering Ltd. (the "Client") and third parties in the preparation of the Report to be correct. While Stantec has exercised a customary level of judgment or due diligence in the use of such information, Stantec assumes no responsibility for the consequences of any error or omission contained therein.

This Report is intended solely for use by the Client in accordance with Stantec's contract with the Client. While the Report may be provided to applicable authorities having jurisdiction and others for whom the Client is responsible, Stantec does not warrant the services to any third party. The report may not be relied upon by any other party without the express written consent of Stantec, which may be withheld at Stantec's discretion.

Prepared by: _____
Signature
Alexandre Mineault-Guitard, M.Sc.A., ing., P.Eng.

Printed Name

Reviewed by: _____
Signature
Ana Paerez, P.Eng.

Printed Name

Approved by: _____
Signature
Ana Paerez, P.Eng.

Printed Name



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1 Introduction

To support David Schaeffer Engineering Ltd (DSEL) with their conceptual design submission for the Barrhaven Conservancy West development lands, Stantec Consulting Ltd. (Stantec) was requested to provide engineering services to complete a water distribution system analysis for this proposed development located within the City of Ottawa's (City) South Urban Community (SUC). The purpose of the analysis is to confirm associated watermain sizing and redundancy needs.

For this assignment, Stantec's scope of work included the following tasks:

1. Reviewing background information and establishing updated water demands for the Conservancy West development area based on the most current draft plan;
2. Preparing and submitting a boundary condition request to the City;
3. Updating the stand-alone hydraulic model, developed for the Conservancy East lands in a previous assignment (Stantec Consulting Ltd., 2022), to include the distribution system within the Conservancy West lands using boundary conditions provided by the City;
4. Assessing Fire Underwriters Survey (FUS) fire flow requirements;
5. Setting up and running model simulations for average day (AVDY), peak hour (PKHR), and maximum day (MXDY) plus fire flow demands to identify watermain sizing and redundancy needs required for the water distribution system within the development lands to meet design criteria; and,
6. Documenting the approach used, findings and recommendations from the analysis.

1.1 Study Area

The study area, referred to as the Barrhaven Conservancy development lands, is located in the City's southwestern suburban neighbourhood of Barrhaven. The lands are situated between Strandherd Dr to the north, the Jock River to the south, Fraser-Clark Drain to the east, and bisected by Borrisokane Rd through the western portion. The Conservancy West development lands will proceed once all phases within the East development lands have been built out. The distribution network within the Conservancy East lands was analyzed under a previous assignment (Stantec Consulting Ltd., 2022).

Based on the latest draft plan provided by DSEL (dated December 1, 2022), the proposed Conservancy West development will comprise a total of 462 single family home (SFH) units and 499 townhouse (MLT) units (consisting of a combination of back-to-back and standard townhouse units) for a total estimated population of 2,918 persons. More details on phasing and population estimates are provided in

Section 1.2.



1 Introduction

January 13, 2023

Based on a previously completed serviceability study for these lands (Stantec Consulting Ltd., 2021, Stantec Consulting Ltd., 2022), this residential community, which is currently situated adjacent to Pressure Zone 3SW (previously known as Zone BARR), is ultimately planned to be serviced by the future Zone SUC. In 2015, the City embarked on a large initiative to reconfigure the pressure zones servicing Barrhaven and the southern reaches of Ottawa (i.e., SUC).

The latest information provided by the City indicates that the pressure zone reconfiguration is planned to be completed by mid 2025. The purpose of the zone reconfiguration is to improve reliability and efficiencies, and to provide increased pumping capacity for future growth. As such, these development lands are to be serviced by two existing connections to the existing distribution network, both of which are currently part of Zone 3SW and will ultimately be part of Zone SUC, as well as a future connection located south of the Jock River. The connections include the following locations as shown in **Figure 1-1**:

1. The existing 305 mm stub extending from Chapman Mills Dr (east of Kennedy-Burnett Pond);
2. The T-junction on the existing 203 mm watermain at Danson Gardens Grv and Darjeeling Ave; and
3. A future 305 mm stub at the intersection of Flagstaff Drive and Borrisokane Road, which requires crossing the Jock River.

Previous studies analyzed the serviceability of the Barrhaven Conservancy Lands via the two (2) existing connections only, as well as with all three (3) connections. This study will only consider the three (3) connections, as it is the City's preferred option.

As previously mentioned, the development area will ultimately be serviced by the pressure Zone SUC once the reconfiguration is complete (planned by mid 2025). As such, the analysis and proposed watermain sizing and layout documented in this report only considers the Zone SUC servicing conditions.

1.2 Phasing Of Barrhaven Conservancy

For the purpose of this assessment, development within the Barrhaven Conservancy lands, as shown in **Figure 1-2**, is assumed to occur in the following phasing order:

1. Conservancy East lands – Comprising 782 SFH units, 606 MTL units, and three (3) parks for a total estimated population of 4,295 persons.
2. Conservancy West lands – Comprising 462 SFH units, 499 MTL units, and three (3) parks for a total estimated population of 2,918 persons.

Several subphases are planned for both the East and West lands, however only the ultimate buildout conditions of both phases (i.e., the buildout conditions of the Barrhaven Conservancy lands) will be analyzed herein. **Figure 1-2** also shows the proposed building types throughout the Conservancy lands.



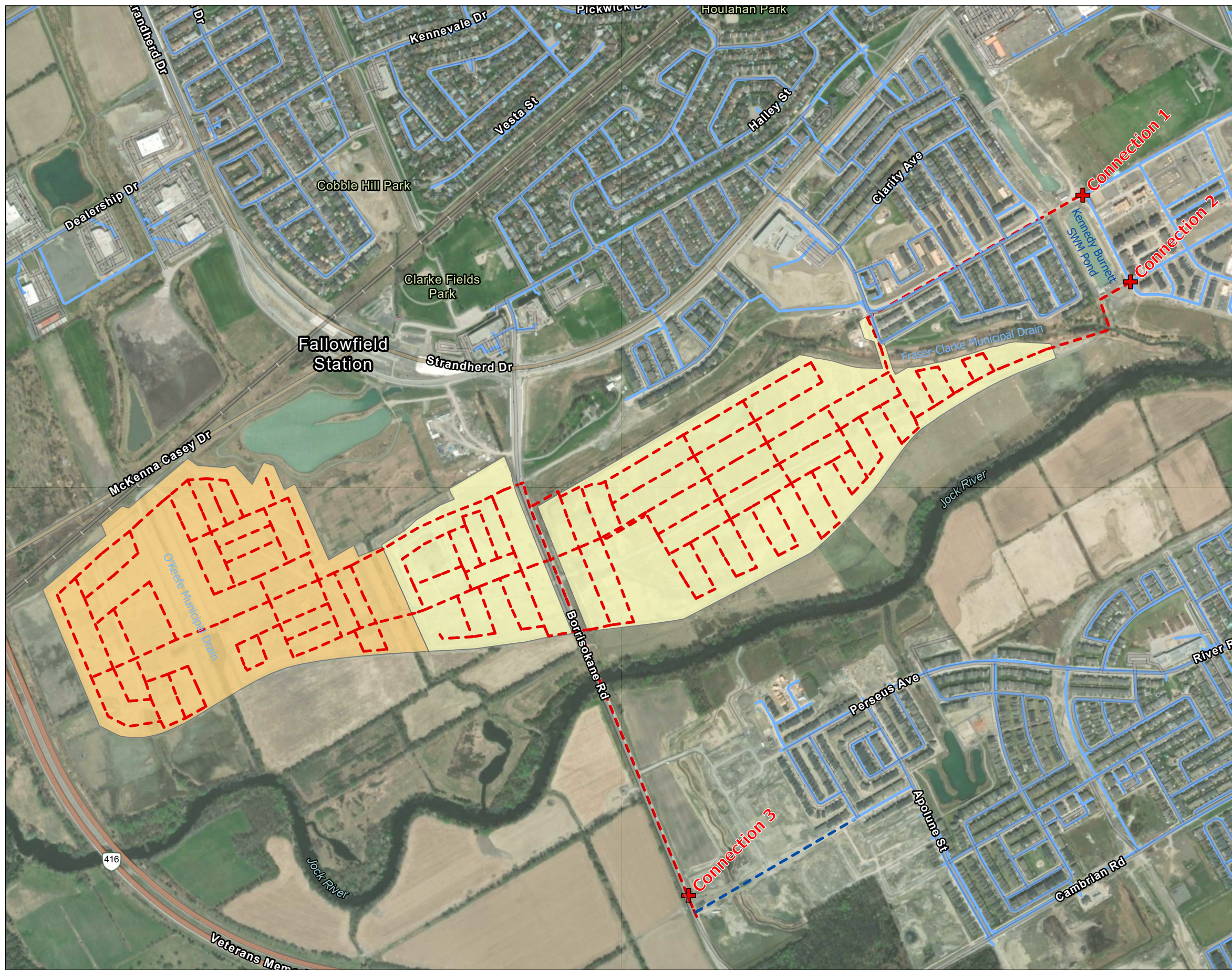
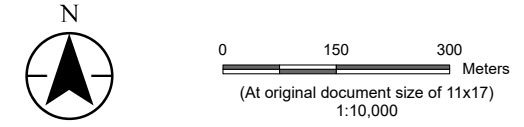


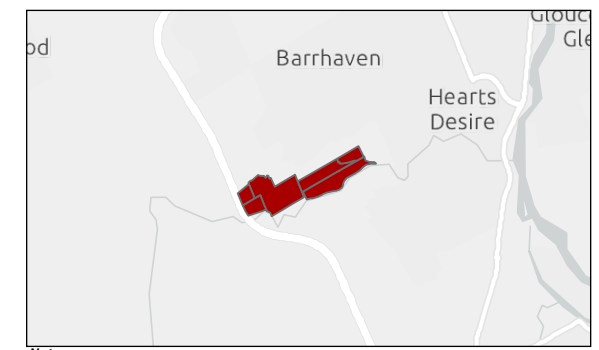
Figure No. **1-1**
Connections to Existing Water Distribution Network

Client/Project
 David Schaeffer Engineering Ltd
 Barrhaven Conservancy West: Water Distribution System Analysis

Project Location
 Ottawa, Ontario, Canada



- Legend
- Barrhaven Conservancy West
 - Barrhaven Conservancy East
 - Existing Distribution Watermain
 - Future Distribution Watermain
 - Connection Location
 - Future Watermain to Service Barrhaven Conservancy Lands



Notes

1. Coordinate System: NAD 1983 CSRS MTM 9
2. Background: Esri, Maxar, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, AeroGRID, IGN, and the GIS User Community

Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community



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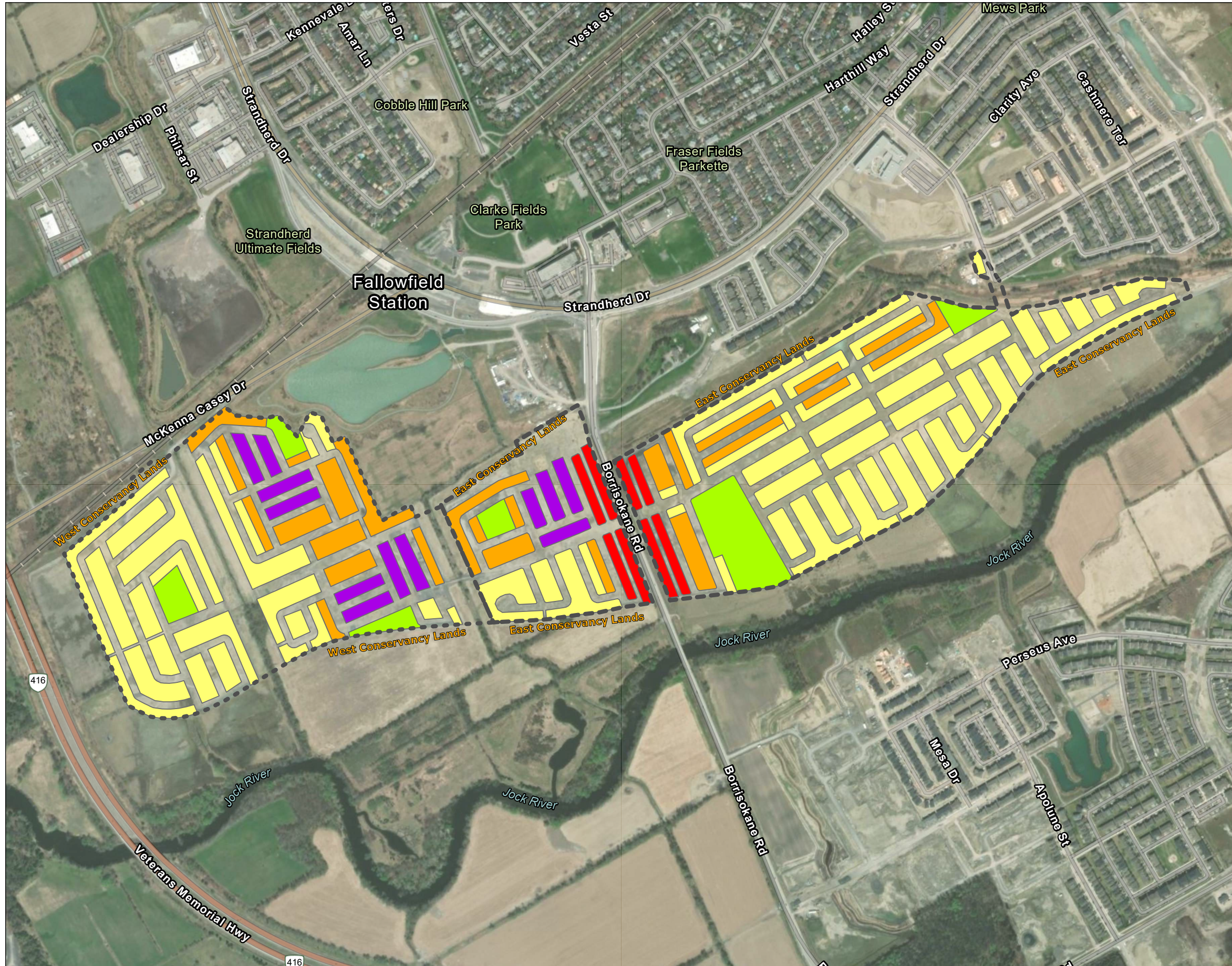


Figure No.

1-2

Title

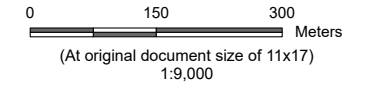
Phasing Plan of Barrhaven Conservancy Lands

Client/Project

David Schaeffer Engineering Ltd
Barrhaven Conservancy West: Water Distribution System Analysis

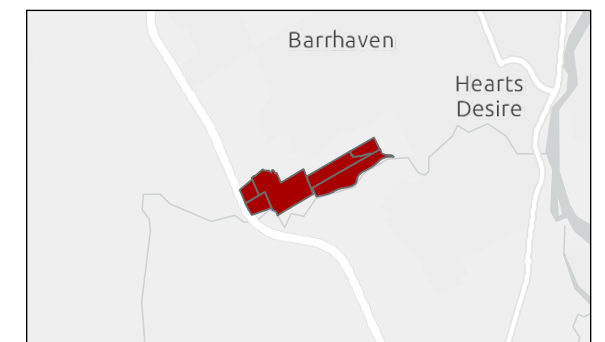
Project Location

Ottawa, Ontario, Canada



Legend

- Development Phase Boundary
- Single Family Home (SFH)
- Standard Townhouse (STND TH)
- Rear-Lane Townhouse (RLTH)
- Back-to-Back Townhouse (B2B)
- Park



Notes

1. Coordinate System: NAD 1983 CSRS MTM 9
 2. Background: Esri, Maxar, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, AeroGRID, IGN, and the GIS User Community
- Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community



2 Hydraulic Assessment

The City of Ottawa Water Design Guidelines (City of Ottawa, 2010) and criteria outlined in the 2013 Water Master Plan (WMP) were used to establish water demands, level of service and pressure objectives during normal and emergency conditions. As per the City's design guidelines and Technical Bulletin ISTB-2021-03, since this is a new development involving the design of new watermains, the design shall consider a required fire flow established using the calculation method published by the Fire Underwriters Survey (FUS).

2.1 Serviceability

2.1.1 SYSTEM PRESSURES

As per the City's Water Design Guidelines, the desired range of pressure under average day (AVDY), maximum day (MXDY) and peak hour (PKHR) demands is 345 to 552 kPa (50 to 80 psi) and no less than 276 kPa (40 psi) at ground elevation (i.e., at street level). The maximum pressure at any point in the water distribution system should not exceed 552 kPa (80 psi). Pressure reducing measures are required to service areas where pressures greater than 552 kPa (80 psi) are anticipated.

Under emergency fire conditions, the system must be able to supply appropriate fire flow while maintaining a residual pressure of 138 kPa (20 psi).

Figure 2-1 shows the elevations of each model junction within the Conservancy West lands. Proposed grades range from 92.5 m to 93.8 m, based on the grading plan provided by DSEL. Elevations in the Conservancy East lands range from 92.4 m to 93.5 m.

2.1.2 FIRE FLOWS

The City requires a fire flow assessment to be completed to demonstrate that local watermains can provide the objective fire flows. However, information regarding unit sizes and unit separation is not available at this time and as such, FUS calculations have not been completed.

As a result, the required fire flow for the governing unit design established for the Conservancy East lands (Stantec Consulting Ltd., 2022) of 13,000 L/min will be used for this analysis to ensure that the local watermains can provide this minimum fire flow at a residual pressure of 20 psi.

It is recommended that FUS calculations for the Conservancy West lands be reviewed at the detailed design stage to ensure that fire flow requirements are met across the site.



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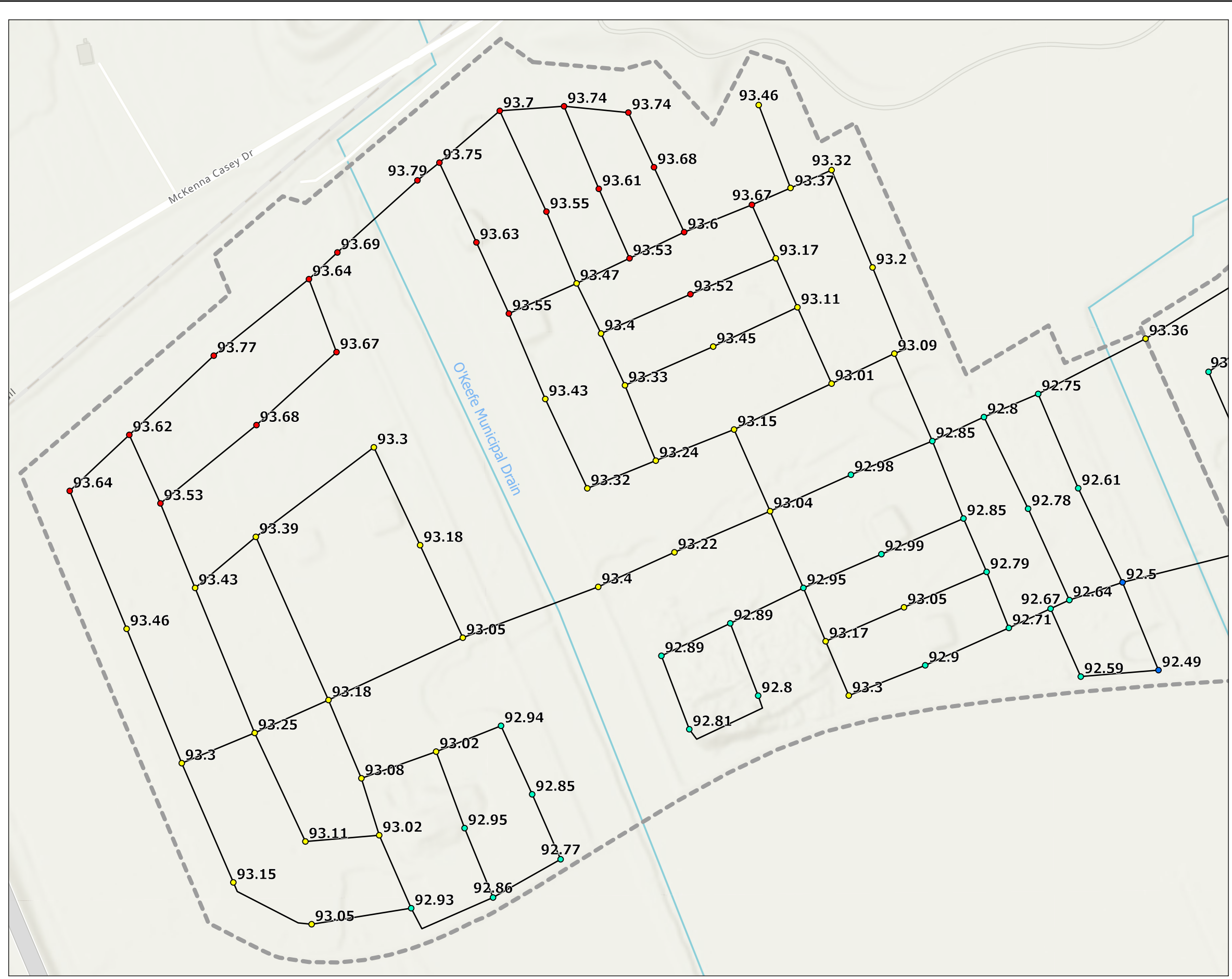


Figure No.
2-1

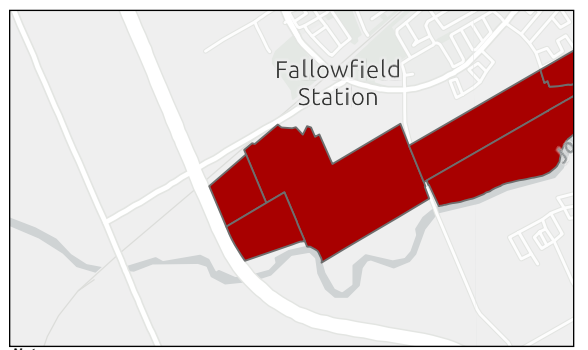
Title
Junction Elevation

Client/Project
David Schaeffer Engineering Ltd
Barrhaven Conservancy West: Water Distribution System Analysis

Project Location
Ottawa, Ontario, Canada



- Legend
- Development Phase Boundary
 - Future Watermain to Service Barrhaven Conservancy Lands
- Ground Elevation (m)
- <92.5
 - 92.5 - 93.0
 - 93.0 - 93.5
 - 93.5 - 94



Notes

1. Coordinate System: NAD 1983 CSRS MTM 9
2. Background: Esri, Maxar, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, AeroGRID, IGN, and the GIS User Community

Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community



2.2 Growth Projections

The estimated residential population for Barrhaven Conservancy lands was estimated based on projected household sizes as per population densities (or persons per unit, PPU) specified in the City's Water Design Guidelines.

Table 2-1 shows the estimated number of units per phase of these development lands and the projected populations based on the distribution of residential types. The total number of units across the entire Barrhaven Conservancy lands is estimated to be 2,349 with a residential population of 7,213 persons.

Table 2-1: Estimated Unit Counts and Populations for Barrhaven Conservancy Lands

Phase	Unit Types	Units	PPU	Population
East	Singles	782	3.4	2,659
	Towns	606	2.7	1,636
	<i>East Phase Sub-total</i>	<i>1,388</i>	-	<i>4,295</i>
West	Singles	462	3.4	1,571
	Towns	499	2.7	1,347
	<i>West Phase Sub-total</i>	<i>961</i>	-	<i>2,918</i>
Total		2,349		7,213

2.3 Demand Projections

As part of the 2022 Study (Stantec Consulting Ltd.) that analyzed the serviceability of the Conservancy East lands, the City requested that the criteria outlined in the City's Water Design Guidelines and Technical Bulletin ISTB-2021-03 were followed to establish water demands. This was considered a conservative approach, as the criteria in the City's Water Design Guidelines are more restrictive in comparison to the ones outlined in the 2013 City's Water Master Plan (WMP).

As such, the demand rates and peaking factors from the Water Design Guidelines and Technical Bulletin ISTB-2021-03 were applied to the population projections presented in **Table 2-2** based on land-use. For residential land-use, SFH and MLT units were assigned an average day (AVDY) consumption rate of 280 L/cap/d. To determine maximum day (MXDY) demands, the AVDY demands were multiplied by a residential peaking factor of 2.5. Peak hour (PKHR) demands were established by multiplying MXDY demands by a residential peaking factor of 2.2. Estimated AVDY, MXDY and PKHR demand projections are summarized in **Table 2-2**.



Table 2-2: Estimated Demand Projections for Barrhaven Conservancy Lands

Phase	Units	Population	AVDY (L/s)	MXDY (L/s)	PKHR (L/s)
East	1,388	4,295	13.92	34.80	76.55
West	961	2,918	9.46	23.64	52.01
Total	2,349	7,213	23.38	58.44	128.57

2.4 Model Development

Innovyze’s InfoWater Pro (Version 3.5, Update #1) was used as a hydraulic modelling platform for the water distribution system analysis of the proposed West Conservancy development lands, and includes the previously assessed East Conservancy lands (Stantec Consulting Ltd., 2022). The model was developed to reflect the most current draft plan for the West Conservancy lands, including the proposed watermain layout (based on proposed road alignment) and water demands.

Watermains added to the model were assigned Hazen-Williams coefficients (“C-Factors”) in accordance with the City’s Water Design Guidelines. These factors are listed in **Table 2-3**.

Table 2-3: Hazen-Williams Coefficients by Watermain Size

Watermain Diameter (mm)	Coefficient
152	100
203 - 305	110
350 - 600	120
> 600	130

2.4.1 BOUNDARY CONDITIONS

The proposed development has three (3) connection points to the existing water distribution system. The boundary conditions provided by the City include hydraulic gradeline (HGL) values for Zone SUC servicing conditions. Values are provided in **Appendix A** and summarized in **Table 2-4**, and have been simulated in the hydraulic model using fixed head reservoirs to which HGLs have been applied for the respective demand scenarios.

Note that minor changes were made to the conceptual plans following the request for boundary conditions. Those changes include a net increase of 34 units (37 additional SFH units, 3 less MTL units), which have a minimal impact on residential water demands (+0.39 L/s for AVDY, and +2.10 L/s for PKHR). As such, boundary conditions listed in **Table 2-4** were used for this study, and updated boundary conditions will be requested from the City for a subsequent submission.



Table 2-4: HGL Boundary Conditions

HGL (m) Zone SUC Servicing Conditions			
Demand Scenario	Three Connections		
	Connection 1 ⁽¹⁾	Connection 2 ⁽²⁾	Connection 3 ⁽³⁾
AVDY	146.7	146.7	146.6
PKHR	141.4	141.3	141.0
AVDY +FF ⁽⁴⁾	139.7	138.1	139.8
MXDY+FF ⁽⁴⁾	137.9	136.2	137.9

Notes

- (1) Ground elevation @ Connection 1 (Chapman Mills Dr) = 93.1 m.
- (2) Ground elevation @ Connection 2 (Danson Gardens Grv / Darjeeling Ave) = 91.8 m.
- (3) Ground elevation @ Connection 3 (Flagstaff Dr) = 92.3 m.
- (4) FF of 13,000 L/min or 216.67 L/s.

2.4.2 PROPOSED WATERMAIN SIZING & LAYOUT

The layout and sizing of the watermains within the proposed development (both East and West) is shown in **Figure 2-2**. Within the Conservancy West lands, the network is proposed to consist of 152 mm, 203 mm, 254 mm, and 305 mm, with the 305 mm watermains acting as the hydraulic backbone throughout the development lands. The 305 mm backbone watermains connect at two (2) locations to the watermains within Conservancy East lands and extend west crossing the O’Keefe municipal drain at two (2) locations. Note that **Figure 2-2** is a schematic representation of the hydraulic model layout. The specific configuration of dead-end watermains, among other infrastructure, are not presented in the figure.

The proposed watermain layout contains two (2) dead-end watermains in the Conservancy West lands (noted on **Figure 2-2**). This includes a dead-end watermain along the cul-de-sac, as well as another single looped watermain east of the O’Keefe municipal drain.

As per the City of Ottawa Water Distribution Design Guidelines, dead ends should be avoided as much as possible to limit potential water quality issues. Where dead-end watermains cannot be avoided, the guidelines specify a maximum watermain size of 150 mm, unless a larger size is needed for supply reasons. Dead-end #1 is proposed to be serviced by a 203 mm diameter watermain, whereas dead-end #2 is proposed to be serviced by a combination of 203 and 254 mm diameter watermains. These pipe sizes are recommended to meet demands under fire flow conditions. The configuration of the dead-end watermains will be as per de City’s standard details and will be reviewed at the detailed design stage.

Furthermore, the maximum number of units along a dead-end watermain should not exceed 49 to avoid the creation of a vulnerable service area. Based on the latest concept plans, each dead-end watermain within the Conservancy West lands services fewer than 49 single-family units.



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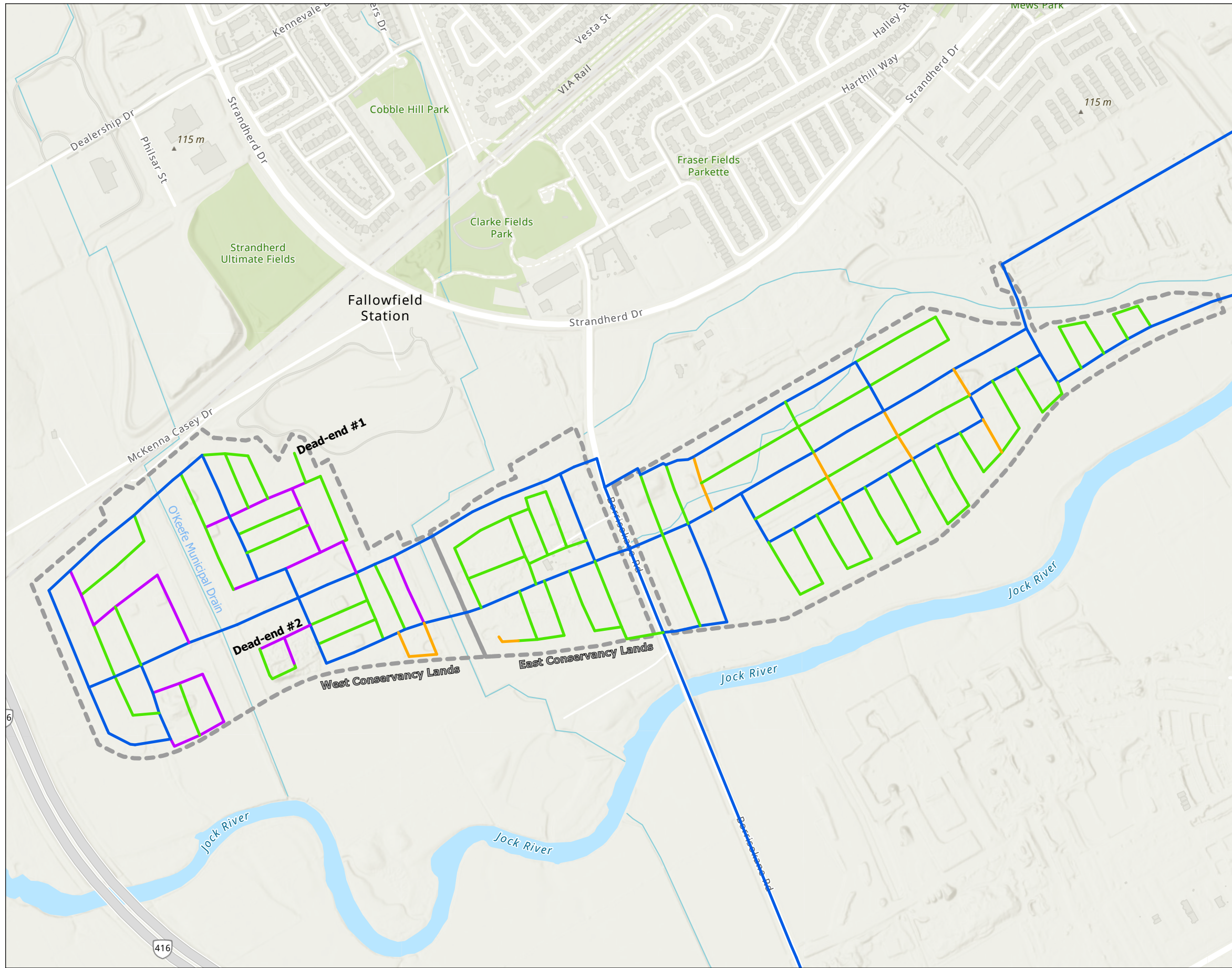
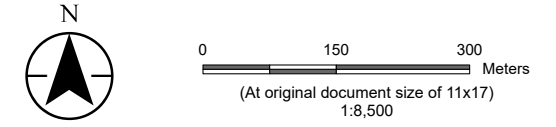


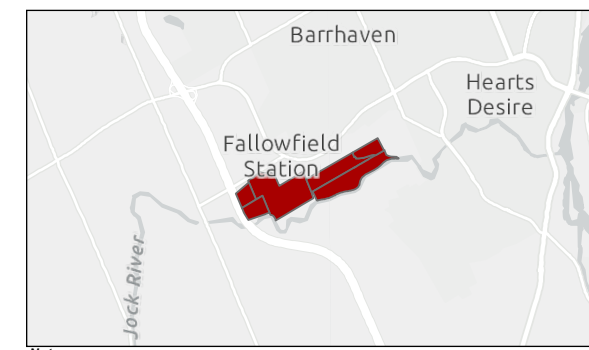
Figure No. **2-2**
 Title **Proposed Watermain Sizing & Layout**

Client/Project
 David Schaeffer Engineering Ltd
 Barrhaven Conservancy West: Water Distribution System Analysis

Project Location
 Ottawa, Ontario, Canada



- Legend
- Development Phase Boundary
 - Proposed Watermain Diameter (mm)**
 - 152
 - 203
 - 254
 - 305



Notes

1. Coordinate System: NAD 1983 CSRS MTM 9
2. Background: Esri, Maxar, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, AeroGRID, IGN, and the GIS User Community

Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community



3 Hydraulic Modelling Results

Hydraulic modelling was completed for ultimate buildout conditions of the development lands, under SUC servicing conditions, to verify how the network would respond. The following subsections present the modelling results under AVDY, PKHR, and under emergency MXDY fire flow conditions. Furthermore, a reliability analysis was performed to assess the network's performance under emergency AVDY fire flow conditions in the event of a watermain break at key points within the proposed network. **Figure B-1 (Appendix B)** provides the model system map, while detailed modelling results for all scenarios are provided in **Appendix C**.

3.1 Average Day & Peak Hour Demands

Under AVDY demands, maximum modelled pressures under buildout conditions are 78 psi. These maximum pressures are less than the City's maximum pressure objective of 80 psi.

Under PKHR demands, minimum modelled pressures under buildout conditions are 64 psi. These pressures fall within the desired pressure range of 50 to 80 psi and are thus considered acceptable.

3.2 Maximum Day Plus Fire Flow

Available fire flows across the proposed development lands must meet or exceed the RFF of 13,000 L/min (216.7 L/s) as described in **Section 2.1.2**.

Under full buildout maximum day + fire flow (MXDY+FF) conditions, model results show that fire flows greater than 13,000 L/min are achievable, with a residual pressure of 138 kPa (20 psi), in most locations within the Conservancy West lands. However, there are a few locations outlined in Table C-3 of **Appendix C** (nodes J363, J365 and J369), where the residual pressures during fire flow conditions are below 138 kPa (20 psi). The worst-case scenario occurs at node J365 where a maximum fire flow of 10,502 L/min is available at a residual pressure of 138 kPa (20 psi).

Fire flow requirements across the Conservancy West lands are to be confirmed at the detailed design stage and fire control measures are to be included as required. These fire control measures may include adding ordinary construction units, the addition of firewalls and/or using the alternative hydrant placing procedure outlined in Appendix I of ISDTB-2018-02 to avoid oversizing local pipes.

These results show that the proposed watermain sizing and layout along with fire control measures at a few locations will meet serviceability requirements.



3.3 Reliability Analysis

As per the City of Ottawa Design Guidelines, the system must be able to provide average day demand plus fire flow (AVDY+FF) while meeting serviceability requirements during a major failure (i.e., watermain break). To assess reliability and resiliency against major failures, a number of reliability scenarios were completed to confirm sufficient pressure and flow can be achieved during a major failure. These scenarios included the following and are shown in **Figure 3-1** :

1. **Break Scenario 1** – Break in the backbone watermain from Connection 1;
2. **Break Scenario 2** – Break in the backbone watermain from Connection 2;
3. **Break Scenario 3** – Break in the backbone watermain from Connection 3 (crossing the Jock River);
4. **Break Scenario 4** – Break along the southern east-west backbone watermain connecting to Conservancy East lands;
5. **Break Scenario 5** – Break along the northern east-west backbone watermain connecting to Conservancy East lands;
6. **Break Scenario 6** – Break in the south backbone watermain crossing O’Keefe municipal drain; and,
7. **Break Scenario 7** – Break in the north backbone watermain crossing O’Keefe municipal drain.

Under Break Scenario 1, all junctions meet the 13,000 L/min required fire flows, with the exception of nodes J363, J365 and J369, which can provide a minimum of 10,715 L/min. Fire flow requirements and fire flow measures are to be confirmed at the detailed design stage.

Under Break Scenario 2, all junctions meet the 13,000 L/min required fire flows, with the exception of nodes J363, J365 and J369, which can provide a minimum of 10,836 L/min. Fire flow requirements and fire flow measures are to be confirmed at the detailed design stage.

Under Break Scenario 3, all junctions meet the 13,000 L/min required fire flows, with the exception of nodes J239, J309, J313, J355, J363, J365 and J369, which can provide a minimum of 10,115 L/min. Fire flow requirements and fire flow measures are to be confirmed at the detailed design stage.

Under Break Scenario 4, all junctions meet the 13,000 L/min required fire flows, with the exception of nodes J237, J239, J241, J259, J261, J271, J285, J289, J297, J301, J309, J313, J329, J343, J345, J347, J349, J351, J353, J355, J363, J365 and J369, which can provide a minimum of 9,679 L/min. Fire flow requirements and fire flow measures are to be confirmed at the detailed design stage.

Under Break Scenario 5, all junctions meet the 13,000 L/min required fire flows, with the exception of nodes J363, J365 and J369, which can provide a minimum of 10,552 L/min. Fire flow requirements and fire flow measures are to be confirmed at the detailed design stage.

Under Break Scenario 6, all junctions meet the 13,000 L/min required fire flows, with the exception of nodes J313, J329, J331, J343, J345, J347, J349, J351, J353, J355, J363, J365 and J369, which can



3 Hydraulic Modelling Results

January 13, 2023

provide a minimum of 11,449 L/min. Fire flow requirements and fire flow measures are to be confirmed at the detailed design stage.

Under Break Scenario 7, all junctions meet the 13,000 L/min required fire flows, with the exception of nodes J305, J309, J313, J363, J365 and J369, which can provide a minimum of 11,448 L/min. Fire flow requirements and fire flow measures are to be confirmed at the detailed design stage.

At the detailed design stage, fire flow requirements across the site are to be confirmed and the required fire flow measures to meet City criteria under all watermain break scenarios are to be determined. These fire control measures may include adding ordinary construction units, the addition of firewalls and/or using the alternative hydrant placing procedure outlined in Appendix I of ISDTB-2018-02 to avoid oversizing local pipes.



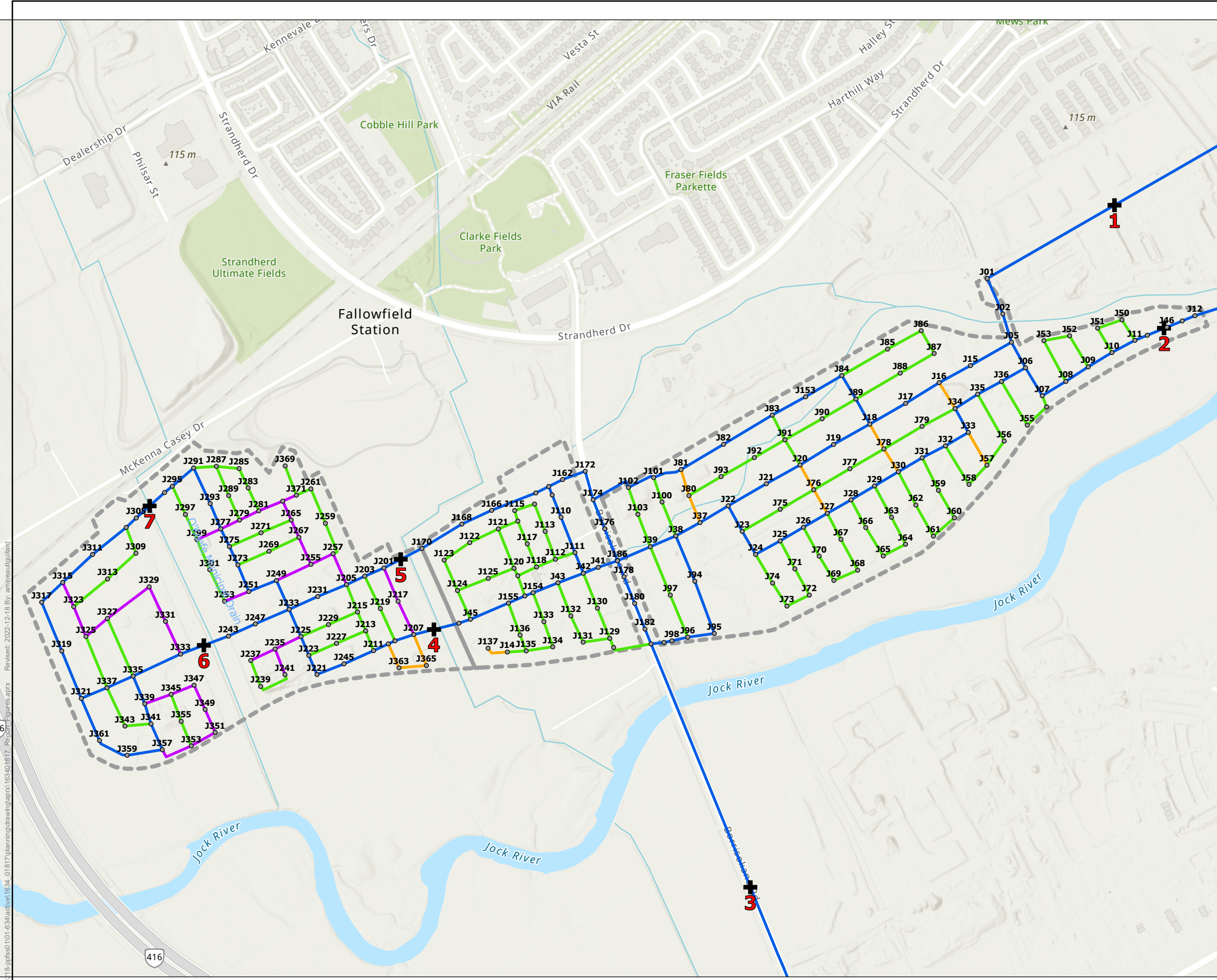
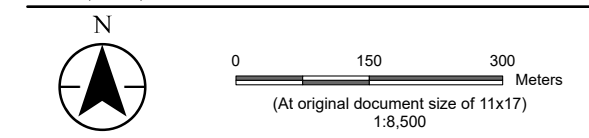
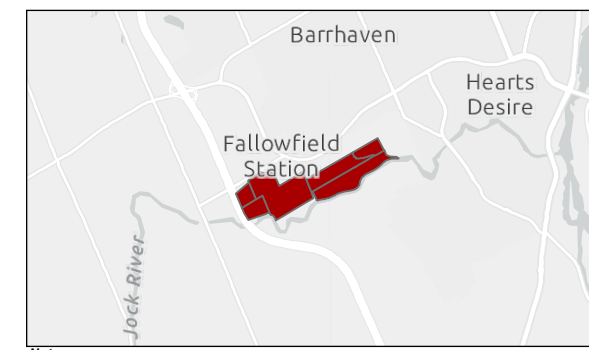


Figure No. **3-1**
 Title **Reliability Analysis Watermain Break Locations**
 Client/Project David Schaeffer Engineering Ltd
 Barrhaven Conservancy West: Water Distribution System Analysis



- Legend
- Development Phase Boundary
 - Model Node
 - Watermain Break Location/Scenario
- Proposed Watermain Diameter (mm)
- 152
 - 203
 - 254
 - 305



Notes

1. Coordinate System: NAD 1983 CSRS MTM 9
2. Background: Esri, Maxar, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, AeroGRID, IGN, and the GIS User Community

Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community



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 Revised: 2022-12-18 By: amineulqulid
 6

4 Conclusion and Recommendations

A water distribution system hydraulic analysis was completed for the Barrhaven Conservancy West development lands. The purpose of this analysis was to confirm associated watermain sizing and redundancy needs. Based on the hydraulic analysis, the following conclusions and recommendations were made:

- Based on the most current site plan layout, the estimated AVDY, MXDY and PKHR demand projections for the Conservancy West lands are 9.46 L/s, 23.64 L/s, and 52.01 L/s, respectively. With the Conservancy East lands, the total estimated AVDY, MXDY and PKHR demands for the entire development are 23.38 L/s, 58.44 L/s, and 128.57 L/s, respectively.
- Information regarding proposed unit sizes and unit spacing is not available at this time and as such, FUS calculations have not been completed. The previously fire flow objective of 13,000 L/min as established in the analysis of the Conservancy East lands (Stantec Consulting Ltd., 2022) was used for this analysis. It is recommended that the FUS calculations be reviewed during the detailed design stage to ensure that fire flow requirements are met across the site.
- Previous studies related to the Conservancy lands analyzed the serviceability of the development via two (2) and three (3) connections scenarios. This study only considered the scenario with three (3) connections. Furthermore, the analysis in this report considers the future zone SUC servicing conditions only.
- Within the Conservancy West lands, the network is proposed to consist of 152 mm, 203 mm, 254 mm, and 305 mm. The 305 mm backbone watermains connect at two (2) different locations to the Conservancy East lands network and extend west crossing the O'Keefe municipal drain at two (2) locations.
- The maximum number of units along a dead-end watermain should not exceed 49 to avoid the creation of a vulnerable service area. Based on the latest concept plans, each dead-end watermain within the Conservancy West lands services fewer than 49 single-family units.
- Under AVDY demand conditions, model results suggest that maximum pressures are below the allowable maximum pressure of 80 psi in accordance with the City of Ottawa Design Guidelines. Under PKHR demand conditions, the minimum pressures are in accordance with the City's system pressure requirements.
- Under MXDY+FF demand conditions, the assumed required fire flow of 13,000 L/min can be achieved across most of the proposed network at full build out conditions, with the exception of a few locations, where the worst-case scenario results in a maximum fire flow of 10,502 L/min available at a residual pressure of 138 kPa (20 psi). Fire flow requirements across the Conservancy West lands are to be confirmed at the detailed design stage and fire control measures are to be included as required. These fire control measures may include adding ordinary construction units, the addition of firewalls and/or using the alternative hydrant placing procedure outlined in Appendix I of ISDTB-2018-02 to avoid oversizing local pipes.



4 Conclusion and Recommendations

January 13, 2023

- To assess reliability and resiliency against major failures, a number of reliability scenarios were completed under AVDY+FF demand conditions to confirm sufficient pressure and flow can be achieved during a major failure. Under all break scenarios, some locations are slightly below the RFF of 13,000 L/min. At the detailed design stage, fire flow requirements across the site are to be confirmed and the required fire flow measures to meet City criteria under all watermain break scenarios are to be determined.



5 References

City of Ottawa. (2010). Ottawa Design Guidelines - Water Distribution. Ottawa.

City of Ottawa. (2018). Technical Bulletin ISTB-2018-02. Ottawa.

City of Ottawa. (2021). Technical Bulletin ISTB-2021-03. Ottawa.

Stantec Consulting Ltd. (2013). City of Ottawa 2013 Water Master Plan. Ottawa.

Stantec Consulting Ltd. (2021). Hydraulic Potable Water Assessment for Barrhaven Conservancy Development Corporation. Ottawa.

Stantec Consulting Ltd. (2022). Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River): Water Distribution System Analysis. Ottawa.



Appendix A Boundary Conditions

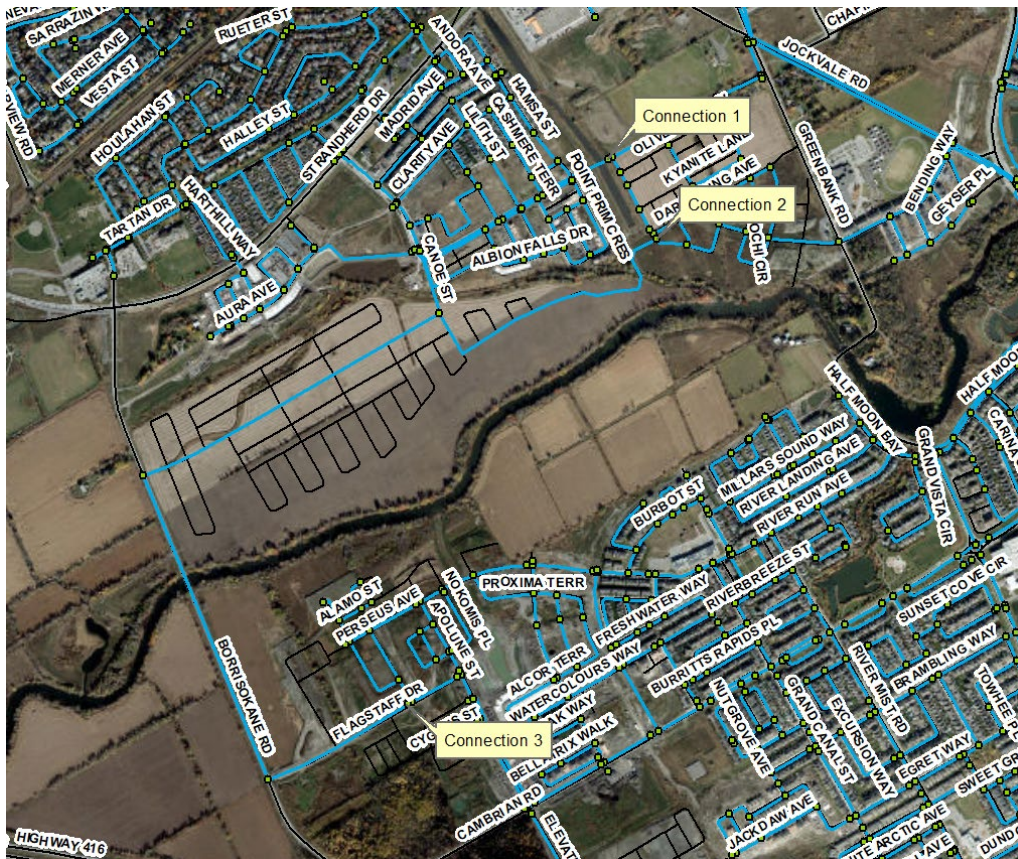


Boundary Conditions Barrhaven Conservancy West

Provided Information

Scenario	Demand	
	L/min	L/s
Average Daily Demand	1,379	22.99
Maximum Daily Demand	3,449	57.49
Peak Hour	7,588	126.47
Fire Flow Demand #1	13,000	216.67

Location



Results – SUC Zone Reconfiguration

Connection 1 – Chapman Mills Dr.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	146.7	76.2
Peak Hour	141.4	68.7
Basic Day plus Fire 1	139.7	66.3
Max Day plus Fire 1	137.9	63.7

Ground Elevation = 93.1 m

Connection 2 – Danson Gardens Grove / Darjeeling Ave.

Demand Scenario	Head (m)	Pressure¹ (psi)
Maximum HGL	146.7	78.0
Peak Hour	141.3	70.4
Basic Day plus Fire 1	138.1	65.9
Max Day plus Fire 1	136.2	63.2

Ground Elevation = 91.8 m

Connection 3 – Langstaff Dr. / Borrisokane Rd.

Demand Scenario	Head (m)	Pressure¹ (psi)
Maximum HGL	146.6	77.2
Peak Hour	141.0	69.3
Basic Day plus Fire 1	139.8	67.5
Max Day plus Fire 1	137.9	64.8

Ground Elevation = 92.3 m

Disclaimer

The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation. Fire Flow analysis is a reflection of available flow in the watermain; there may be additional restrictions that occur between the watermain and the hydrant that the model cannot take into account.

Appendix B Junction IDS



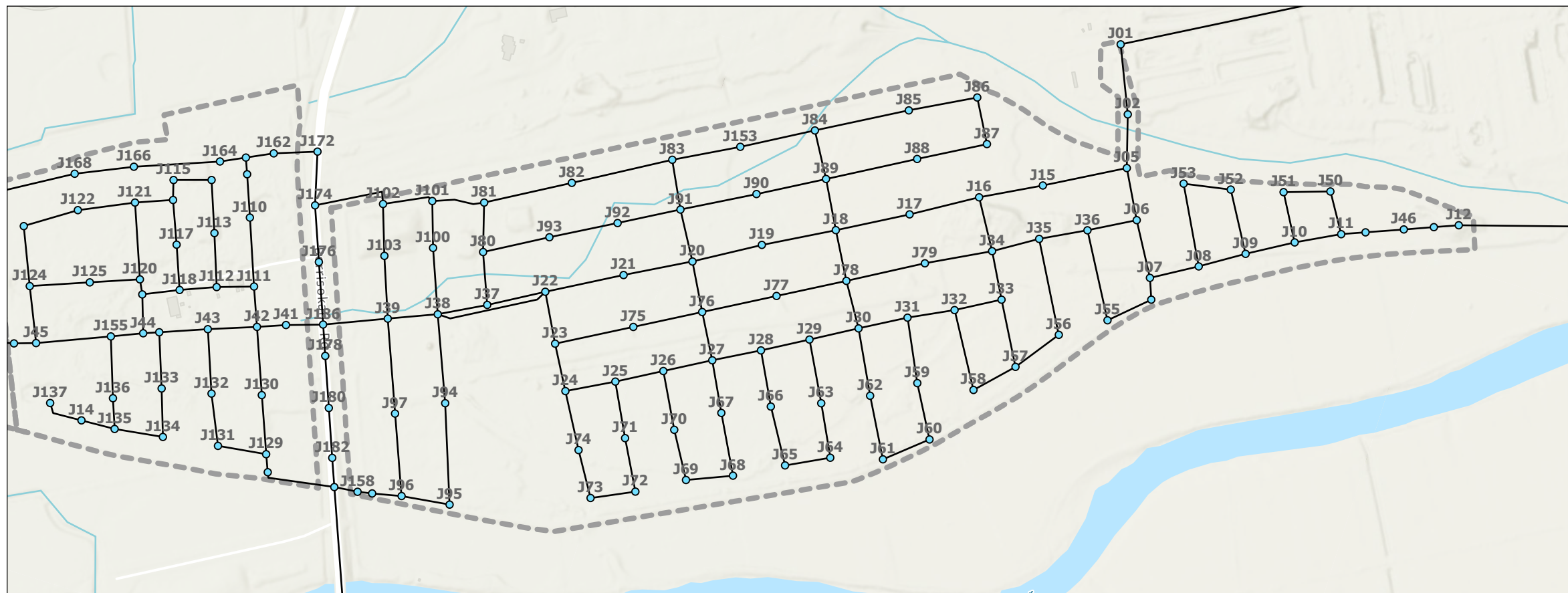
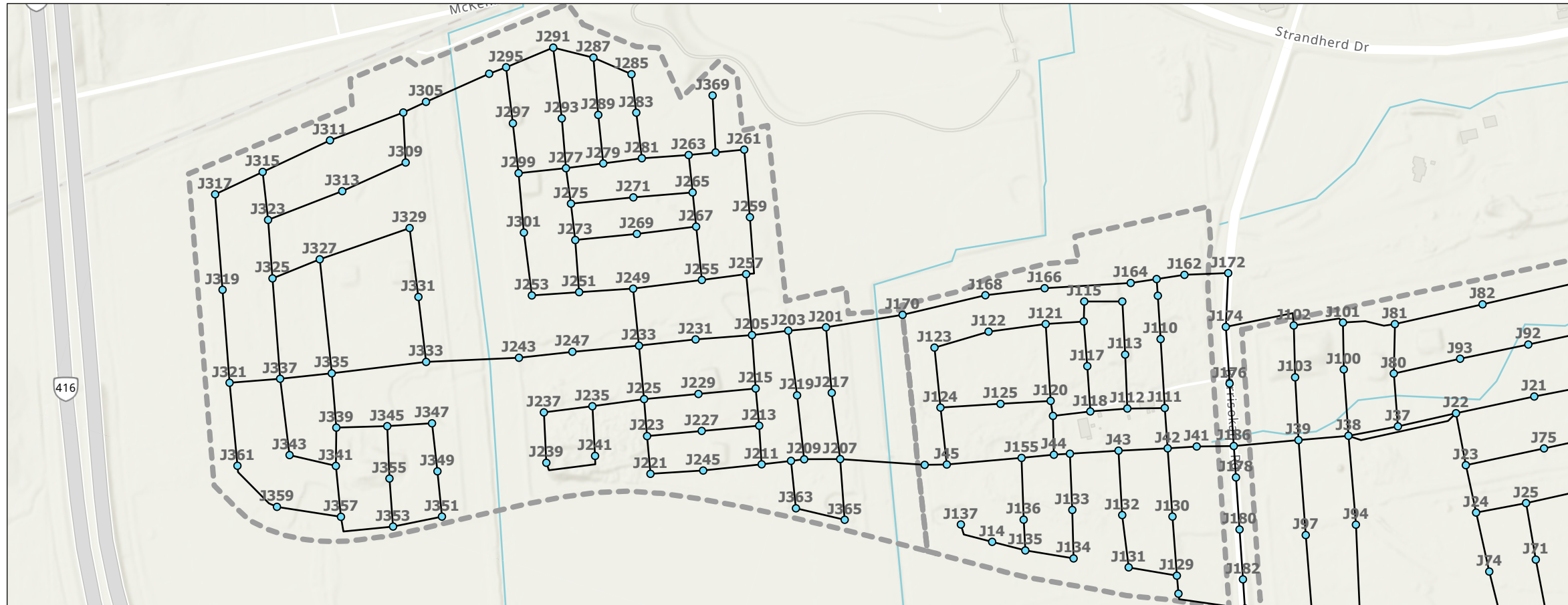


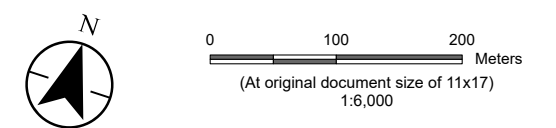
Figure No.

B-1

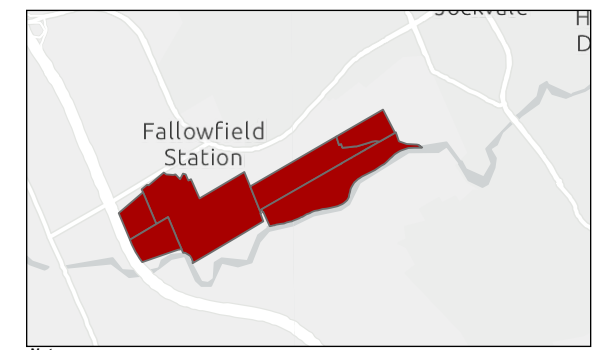
Title
Model System Map

Client/Project
David Schaeffer Engineering Ltd
Barrhaven Conservancy West: Water Distribution System Analysis

Project Location
Ottawa, Ontario, Canada



- Legend
- Development Phase Boundary
 - Future Watermain
 - Model Node



Notes

1. Coordinate System: NAD 1983 CSRS MTM 9
2. Background: Esri, Maxar, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, AeroGRID, IGN, and the GIS User Community

Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community



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Appendix C Model Results



APPENDIX C

SANITARY

MEMORANDUM

DATE: MAY 30, 2019

TO: JOSÉE VALLEE – CITY OF OTTAWA

FROM: CONRAD STANG – NOVATECH

RE: STRANDHERD DRIVE WIDENING PROJECT
SOUTH NEPEAN COLLECTOR PHASE 3: SANITARY FLOW CALCULATIONS

CC: EDSON DONNELLY – NOVATECH

See markups on:
- Figure 1
- "Sanitary Sewer Design Sheet, South Nepean Collector - Phase 2 & 3" (Dec 5, 2018 version)
- "Sanitary Sewer Design Sheet, South Nepean Collector - Phase 2 & 3" (August 20, 2015 version)

1.0 PURPOSE

This memorandum provides the sanitary sewer flow calculations and design sheet for Phase 3 of the proposed South Nepean Collector (SNC), as part of the Strandherd Drive Widening Project. Sanitary design flows have been estimated for both current-day operational flows and future development peak design flows. They are based on the latest available planning information for the vacant lands within the SNC sewershed.

2.0 BACKGROUND

In January 1998, the Master Servicing Study for the South Nepean Urban Area provided a conceptual plan for water, wastewater and stormwater infrastructure. The preferred alternative for wastewater servicing was an east/west trunk sewer alignment that was to be completed in several phases. The proposed sanitary trunk sewer was initially called the Jock River Collector, but was renamed the South Nepean Collector during the original functional design study completed in 2003.

Phase 1 of the South Nepean Collector was completed in 2005 and currently terminates at a 2400mm maintenance hole located east of Longfields Drive, north of Bren-Maur Road. Phase 2 was completed in 2016 and currently terminates at a 2400mm maintenance hole located at the intersection of Strandherd Drive and Fraser Fields Way.

Phase 3 will extend the trunk sewer along Strandherd Drive to the intersection of Kennevale Drive. Here it will connect with the existing sanitary trunk sewer that was constructed as part of the 2014 works to improve Strandherd Drive and develop the CitiGate Lands.

The sanitary sewer flows were previously documented in the *South Nepean Collector – Functional Design Report and Update* (Dillon, 2012). Novatech (2016) completed a *Hydraulics Review / Assessment* of the sanitary flows presented in the Dillon Report (attached). This was based on the latest planning information for the vacant lands within the SNC sewershed. The results of the *Hydraulics Review / Assessment* (Novatech, 2016) were similar to the results from the Dillon (2012) analysis.

3.0 DESIGN PARAMETERS AND POPULATION ESTIMATES

3.1 Design Parameters

The sanitary design flow were calculated using the parameters from the City of Ottawa Sewer Design Guidelines (October 2012), revised per Technical Bulletin ISTB-2018-01 (March 2018). These parameters are summarized in **Table 1** and **Table 2**.

Table 1: Peak Design Flow Parameters

Land Use	Average Daily Flow	Peaking Factor	Peak Extraneous Flows
Residential	280 L/cap/day	Harmon Equation, K=0.8 (1.6 min – 3.2 max)	0.33 L/s/ha
Commercial	28,000 L/ha/day	1.0 – 1.5*	
Institutional	28,000 L/ha/day	1.0 – 1.5*	
Other†	0 L/ha/day	N/A	

*Peak Factor = 1.5 if contributing area is >20%; Peak Factor = 1.0 if contributing area is <20%

†Open Space, Arterial ROW, SWM Blocks, etc. with no sanitary flow contribution (extraneous flow only)

Table 2: Operational Design Flow Parameters

Land Use	Average Daily Flow	Peaking Factor	Peak Extraneous Flows
Residential	200 L/cap/day	Harmon Equation, K=0.6 (1.2 min – 2.4 max)	0.30 L/s/ha
Commercial	17,000 L/ha/day	1.0 (non-coincident peak)	
Institutional	17,000 L/ha/day	1.0 (non-coincident peak)	

*There are no industrial areas identified within the tributary area.

$$\text{Harmon Equation} = 1 + \frac{14}{4 + \left(\frac{P}{1000}\right)^{\frac{1}{2}}} \times K$$

Where:

P = Population

K = Correction Factor:

- Peak Flow = 0.8
- Operational = 0.6

3.2 Land Use Designations & Population Estimates

Population densities and unit counts for future residential development are based on the Novatech (2016) Hydraulics Review / Assessment; refer to **Table 3**. They are based on the concept plans provided by the developers of the future residential areas.

Table 3: Residential Land Use Population Densities

Residential Land Use	Units per ha	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

The land use designations shown in **Table 4** have been applied for the areas within Phases 2 & 3 of the SNC (Node 70 to 130). The Hydraulics Analysis / Review delineated the sewershed areas and land use designations using aerial photos (existing development) and conceptual site plans (future development).

Table 4: Land Use Designations

Land Use Designation	
Secondary Plan	SNC Design
Residential	Residential (Low / Medium / High Density)
Institutional / Office	Institutional
Commercial	Commercial
Recreational	
Business Park	
Prestige Business Park	
Park/Open Space Area	Other*
Ex. Snow Disposal Facility (future commercial)	
Stormwater Management Facility	
Conservation Lands	
Arterial Right-of-Ways	

* No sanitary flow contribution - extraneous flows (inflow/infiltration) only.

The overall residential population estimate and sewershed area for Phases 2 and 3 of the SNC is provided in **Table 5** below. It is assumed that the snow dump facility at the Stranderd Drive and McKenna Casey Drive will ultimately be re-zoned for commercial development.

Table 5: Population Estimates and Areas

Existing / Future	Estimated Population / Area	Novatech (2015)
Existing	Estimated Population	6,944 persons
	Gross Residential Area	60.09 ha
	Gross Commercial / Institutional Area	64.37 ha
	<i>Total Sewershed Area</i>	124.5 ha
Future (full service)	Estimated Population	27,312 persons
	Gross Residential Area	248.48 ha
	Gross Commercial / Institutional Area	228.82 ha
	<i>Total Sewershed Area</i>	477.3 ha

4.0 SANITARY DESIGN FLOWS

The sanitary flow allocations for Phases 2 and 3 of the SNC are provided in **Table 6**. The corresponding sanitary drainage area plan is provided as **Figure 1**. Sanitary sewer flow calculations for Phases 2 and 3 and detailed sanitary sewer design sheets for Phase 3 are attached to this memorandum.

The estimated sanitary design flows from Phase 3 of the SNC (entering Node 90) are as follows:

- Present-Day Operational Design Flows (Theoretical) = 55.1 L/s
- Future Peak Design Flows = 282.5 L/s

The outlet for Phase 3 of the SNC is the existing 900mm outlet pipe at the 2400mm maintenance hole (Node 90) located at the intersection of Strandherd Drive and Fraser Fields Way. Given a minimum design slope of 0.10%, this 900mm sanitary trunk sewer would have a full flow capacity of 597.2 L/s. Therefore, the downstream sanitary trunk sewer would be at 64% capacity, based on the future peak design flow being 282.5 L/s.

ATTACHMENTS:

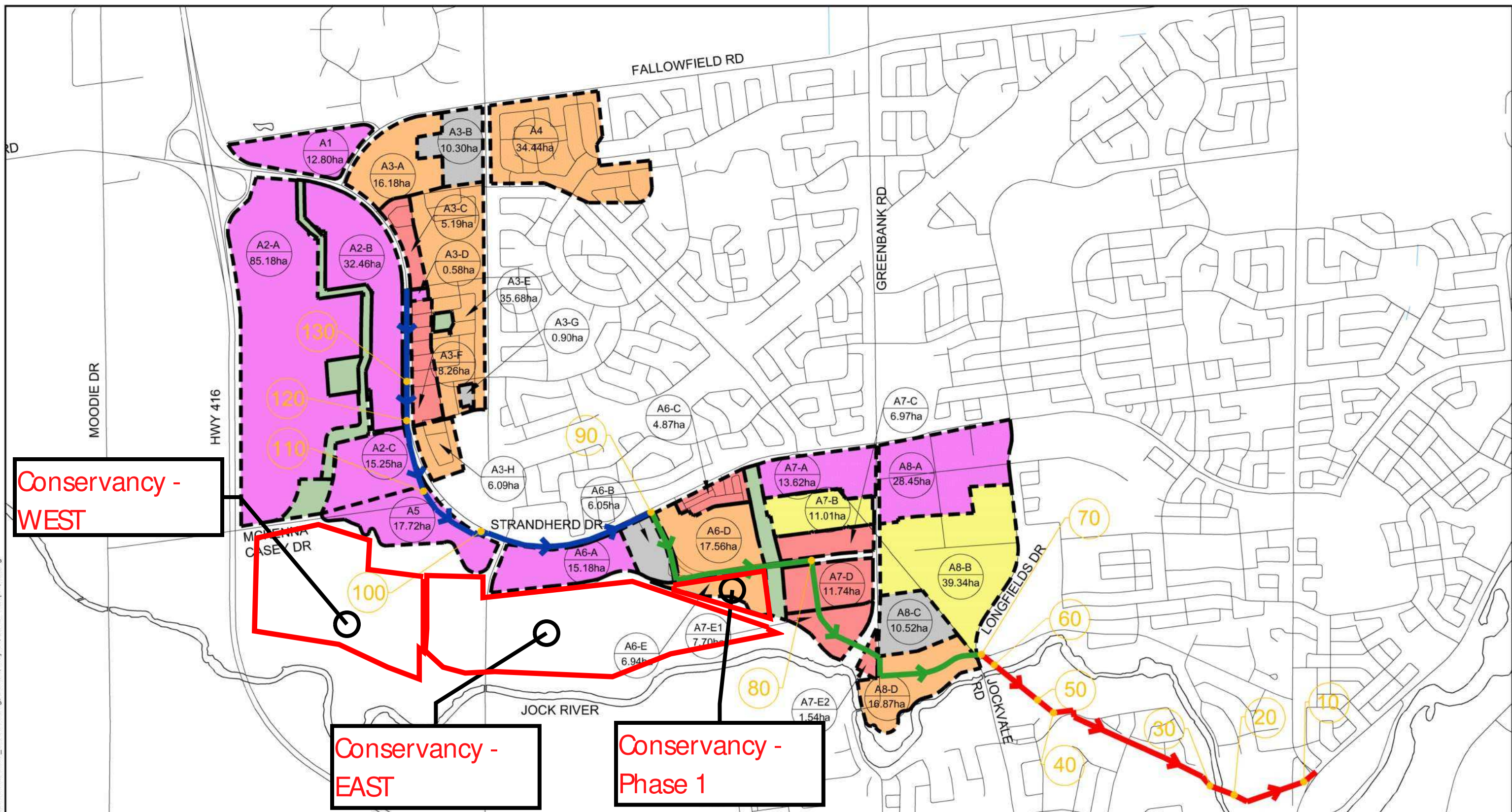
- Figure 1: Sanitary Drainage Areas and Land Use
- Sanitary Sewer Flow Calculations
- Sanitary Sewer Design Sheets (Phase 3)
- South Nepean Collector Phase 2: Hydraulics Review / Assessment (Novatech, 2016)
- Excerpts from Dillion (2012)



Table 6: Updated Allocation of Commercial, Institutional and Residential Demands to Phases 2 & 3 (Nodes 70 – 130) of the SNC by Collection Area

Collection Area	Upstream Node	Existing / Proposed Development	Existing / Proposed Land Use	Area (ha)	Estimated Number of Residential Units	Population Density (persons / ha)	Comment	Reference
A1	130	Proposed	Commercial	12.80	-	-	O'Keefe Court – Conceptual site plan shows proposed commercial.	Conceptual Plans for O'Keefe Court
A2-A	130	Proposed	Commercial	85.18	-	-	CitiGate – Analysis uses same approach as the design for CitiGate.	Detailed Servicing and SWM Report (Phase 1) (Novatech, 2014)
A2-B	130	Proposed	Commercial	32.46	-	-		
A2-C	120	Proposed	Commercial (ex. Snow dump)	15.25	-	-	Existing snow dump facility assumed to be future commercial.	Functional Design Report and Update – SNC Phase 2 and 3 (Dillon, 2012)
A3-A	130	Proposed	Low Density Residential	16.18	461	95.2	Havencrest – Existing single family units.	Havencrest Design Report (IBI, 2013)
A3-B	130	Existing	Institutional	10.30	-	-	Cedarview Middle School and Cedarview Alliance Church.	Aerial Photos / Site Visits
A3-C	130	Existing	Medium Density Residential	5.19	311	162	Existing townhouse units.	
A3-D	130	Existing	Commercial	0.58	-	-	Existing commercial buildings.	
A3-E	130	Existing	Low Density Residential	35.68	999	95.2	Existing single family units.	
A3-F	130	Existing	Medium Density Residential	8.26	496	162.0	Existing townhouse units.	
A3-G	130	Existing	Institutional	0.90	-	-	Ottawa Torah Centre Chibad.	
A3-H	120	Existing	Low Density Residential	6.09	171	95.2	Existing single family units.	
A4	130	Existing	Low Density Residential	34.44	964	95.2	Existing single family units currently serviced by Jockvale pump station; to be redirected to SNC.	
A5	110	Proposed	Commercial	17.72	-	-	Proposed commercial south of McKenna Casey Drive.	Site Visits
A6-A	100	Proposed	Commercial	15.18	-	-	Proposed commercial south of Srandherd Drive; east of Borrisokane Road.	Conceptual Plan for Lands Adjacent the Kennedy-Burnett SWMF provided by Minto (2015)
A6-B	100	Proposed	Institutional	6.05	-	-	Proposed school site on Minto property.	
A6-C	90	Existing	Medium Density Residential	4.87	292	162.0	Existing townhouse units.	Aerial Photos / Site Visits
A6-D	90	Proposed	Low Density Residential	17.56	492	95.2	Proposed single family units on lands owned by Minto / Mion.	Conceptual Plans for Lands Adjacent the Kennedy-Burnett SWMF provided by land owners.
A6-E	90	Proposed	Low Density Residential	6.94	203	95.2	Proposed single family units on lands owned by Pavic / Braovac.	
A7-A	80	Existing	Commercial	13.62	-	-	Existing large retail stores (commercial).	Aerial Photos
A7-B	80	Proposed	High Density Residential	11.01	826	135.0	Proposed high density units on lands owned by Richcraft / Trinity.	Conceptual Plans for Lands Adjacent the Kennedy-Burnett SWMF provided by land owners.
A7-C	80	Proposed	Medium Density Residential	6.97	418	162.0	Proposed Medium density units on lands owned by Mion.	
A7-D	80	Proposed	Medium Density Residential	11.74	704	162.0	Proposed Medium density units on lands owned by Caivan.	
A7-E1/E2	80	Proposed	Medium Density Residential	9.24	554	162.0	Proposed Medium density units on lands owned by Claridge.	
A8-A	80	Existing	Commercial	28.45	-	-	Existing Barrhaven Market Place (commercial).	Aerial Photos / Site Visits
A8-B	80	Proposed	High Density Residential	39.34	2951	135.0	Future development similar to Ampersands development.	Site Visits
A8-C	80	Existing	Institutional	10.52	-	-	Existing St. Joseph High School.	Aerial Photos / Site Visits
A8-D	80	Proposed	Low Density Residential	16.87	1012	162.0	Proposed 600 low density residential units.	Functional Design Report and Update – SNC Phase 2 and 3 (Dillon, 2012)

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LEGEND

	EXISTING / PROPOSED HIGH DENSITY RESIDENTIAL
	EXISTING / PROPOSED MEDIUM DENSITY RESIDENTIAL
	EXISTING / PROPOSED LOW DENSITY RESIDENTIAL
	EXISTING / PROPOSED COMMERCIAL
	EXISTING / PROPOSED INSTITUTIONAL

	OTHER LANDS (OPEN SPACE, PARKS, AND SWMFS)
	SOUTH NEPEAN COLLECTOR PHASE 1
	SOUTH NEPEAN COLLECTOR PHASE 2
	SOUTH NEPEAN COLLECTOR PHASE 3
	SOUTH NEPEAN COLLECTOR NODE ID

NOVATECH
 Engineers, Planners & Landscape Architects
 Suite 200, 240 Michael Cowpland Drive
 Ottawa, Ontario, Canada K2M 1P6

Telephone (613) 254-9643
 Facsimile (613) 254-5867
 Website www.novatech-eng.com

SOUTH NEPEAN COLLECTOR SEWER		
SANITARY DRAINAGE AREAS AND LAND USE		
SCALE	1:20 000	
DATE	JOB	FIGURE
MAY 2019	117190	FIG. 1

PROJECT #: 117190
 DESIGNED BY: CMS
 CHECKED BY: RJD
 DATE: December 5, 2018

SANITARY SEWER DESIGN SHEET

South Nepean Collector - Phase 2 & 3

Theoretical Current Operational Peak Wastewater Flow



Location			Areas				Population				Individual Design Flows			Cumulative Design Flows				
Area I.D.	Existing Land Use	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Total Gross Area (ha)	Residential Population Density (people / ha)	Individual Residential Population	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn ¹)	Commercial Peak Flow Rate ² (17,000 L/ha/d) (L/s)	Institutional Peak Flow Rate ² (17,000 L/ha/d) (L/s)	Infiltration / Inflow Rate (0.3 L/s/ha) (L/s)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (200 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)
A1	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A2-A	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A2-B	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A3-A	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A3-B	Institutional	130		10.30		10.30					0.0	2.0	3.1	0.0	2.0	3.1	0.0	5.1
A3-C	Medium Density Residential	130			5.19	5.19	162.0	841	841	2.40	0.0	0.0	1.6	0.0	2.0	4.6	4.7	11.3
A3-D	Commercial	130	0.58			0.58		841	841	2.40	0.1	0.0	0.2	0.1	2.0	4.8	4.7	11.6
A3-E	Low Density Residential	130			35.68	35.68	95.2	3397	4238	2.39	0.0	0.0	10.7	0.1	2.0	15.5	23.4	41.1
A3-F	Medium Density Residential	130			8.26	8.26	162	1338	5576	2.32	0.0	0.0	2.5	0.1	2.0	18.0	29.9	50.1
A3-G	Institutional	130		0.90		0.90			5576	2.32	0.0	0.2	0.3	0.1	2.2	18.3	29.9	50.5
A4	Low Density Residential*	130				0.00			5576	2.32	0.0	0.0	0.0	0.1	2.2	18.3	29.9	50.5
A2-C	Snow Dump Facility	120				0.00			5576	2.32	0.0	0.0	0.0	0.1	2.2	18.3	29.9	50.5
A3-H	Low Density Residential	120			6.09	6.09	95.2	580	6155	2.30	0.0	0.0	1.8	0.1	2.2	20.1	32.7	55.1
A5	Open Space	110				0.00			6155	2.30	0.0	0.0	0.0	0.1	2.2	20.1	32.7	55.1
A6-A	Open Space	100				0.00			6155	2.30	0.0	0.0	0.0	0.1	2.2	20.1	32.7	55.1
A6-B	Open Space	100				0.00			6155	2.30	0.0	0.0	0.0	0.1	2.2	20.1	32.7	55.1
A6-C	Medium Density Residential	90			4.87	4.87	162.0	789	6944	2.27	0.0	0.0	1.5	0.1	2.2	21.6	36.4	60.3
A6-D	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	0.1	2.2	21.6	36.4	60.3
A6-E	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	0.1	2.2	21.6	36.4	60.3
A7-A	Commercial	90	13.62			13.62			6944	2.27	2.7	0.0	4.1	2.8	2.2	25.6	36.4	67.1
A7-B	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	2.2	25.6	36.4	67.1
A7-C	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	2.2	25.6	36.4	67.1
A7-D	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	2.2	25.6	36.4	67.1
A7-E1/E2	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	2.2	25.6	36.4	67.1
A8-A	Commercial	80	28.45			28.45			6944	2.27	5.6	0.0	8.5	8.4	2.2	34.2	36.4	81.2
A8-B	Open Space	80				0.00			6944	2.27	0.0	0.0	0.0	8.4	2.2	34.2	36.4	81.2
A8-C	Institutional	80		10.52		10.52			6944	2.27	0.0	2.1	3.2	8.4	4.3	37.3	36.4	86.4
A8-D	Open Space	80				0.00			6944	2.27	0.0	0.0	0.0	8.4	4.3	37.3	36.4	86.4
ROW Along SNC Sewer Alignment	-	80				14.34			6944	2.27	0.0	0.0	4.3	8.4	4.3	41.6	36.4	90.7
TOTAL		80	42.65	21.72	60.09	138.80	-	6944	6944	2.27	8.4	4.3	41.6	8.4	4.3	41.6	36.4	90.7

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

Notes:

- Harmon Equation = $1 + [14 / (4 + (P/1000)^{1/2})] \times K$
 Where: P = population; K = correction factor = 0.6
- Institutional / Commercial Peaking Factor = 1.0

Reported Design Flows / Assumptions:

- Area A4: Existing single family units currently serviced by Jockvale pump station; currently not directed to SNC

PROJECT #: 117190
 DESIGNED BY: CMS
 CHECKED BY: RJD
 DATE: December 5, 2018

SANITARY SEWER DESIGN SHEET

South Nepean Collector - Phase 2 & 3

Theoretical Future Full Service Peak Wastewater Flow



Location			Areas				Population				Individual Design Flows			Cumulative Design Flows				
Area I.D.	Existing / Proposed Land Use	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Total Gross Area (ha)	Residential Population Density (people / ha)	Individual Residential Population	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn ¹)	Commercial Peak Flow Rate ² (28,000 L/ha/d) (L/s)	Institutional Peak Flow Rate ² (28,000 L/ha/d) (L/s)	Infiltration / Inflow Rate (0.33 L/s/ha) (L/s)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (280 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)
A1	Commercial	130	12.80			12.80					6.2	0.0	4.2	6.2	0.0	4.2	0.0	10.4
A2-A	Commercial	130	85.18			85.18					41.4	0.0	28.1	47.6	0.0	32.3	0.0	80.0
A2-B	Commercial	130	32.46			32.46					15.8	0.0	10.7	63.4	0.0	43.0	0.0	106.5
A3-A	Low Density Residential	130			16.18	16.18	95.2	1540	1540	3.14	0.0	0.0	5.3	63.4	0.0	48.4	15.7	127.5
A3-B	Institutional	130		10.30		10.30					0.0	3.3	3.4	63.4	3.3	51.8	15.7	134.2
A3-C	Medium Density Residential	130			5.19	5.19	162.0	841	2381	3.02	0.0	0.0	1.7	63.4	3.3	53.5	23.3	143.6
A3-D	Commercial	130	0.58			0.58					0.3	0.0	0.2	63.7	3.3	53.7	23.3	144.0
A3-E	Low Density Residential	130			35.68	35.68	95.2	3397	5778	2.75	0.0	0.0	11.8	63.7	3.3	65.5	51.5	184.0
A3-F	Medium Density Residential	130			8.26	8.26	162	1338	7116	2.68	0.0	0.0	2.7	63.7	3.3	68.2	61.8	197.0
A3-G	Institutional	130		0.90		0.90					0.0	0.3	0.3	63.7	3.6	68.5	61.8	197.6
A4	Low Density Residential	130			34.44	34.44	95.2	3279	10395	2.55	0.0	0.0	11.4	63.7	3.6	79.9	85.9	233.1
A2-C	Commercial (ex. snow dump)	120	15.25			15.25					7.4	0.0	5.0	71.1	3.6	84.9	85.9	245.5
A3-H	Low Density Residential	120			6.09	6.09	95.2	580	10974	2.53	0.0	0.0	2.0	71.1	3.6	86.9	90.0	251.7
A5	Commercial	110	17.72			17.72					8.6	0.0	5.8	79.7	3.6	92.7	90.0	266.1
A6-A	Commercial	100	15.18			15.18					7.4	0.0	5.0	87.1	3.6	97.7	90.0	278.5
A6-B	Institutional	100		6.05		6.05					0.0	2.0	2.0	87.1	5.6	99.7	90.0	282.5
A6-C	Medium Density Residential	90			4.87	4.87	162.0	789	11763	2.51	0.0	0.0	1.6	87.1	5.6	101.4	95.6	289.6
A6-D	Low Density Residential	90			17.56	17.56	95.2	1672	13435	2.46	0.0	0.0	5.8	87.1	5.6	107.1	107.2	307.0
A6-E	Low Density Residential	90			6.94	6.94	95.2	661	14096	2.44	0.0	0.0	2.3	87.1	5.6	109.4	111.7	313.8
A7-A	Commercial	90	13.62			13.62					6.6	0.0	4.5	93.7	5.6	113.9	111.7	324.9
A7-B	High Density Residential	90			11.01	11.01	135.0	1486	15582	2.41	0.0	0.0	3.6	93.7	5.6	117.6	121.7	338.5
A7-C	Medium Density Residential	90			6.97	6.97	162.0	1129	16711	2.38	0.0	0.0	2.3	93.7	5.6	119.9	129.2	348.3
A7-D	Medium Density Residential	90			11.74	11.74	162.0	1902	18613	2.35	0.0	0.0	3.9	93.7	5.6	123.7	141.6	364.6
A7-E1/E2	Medium Density Residential	90			9.24	9.24	162.0	1497	20110	2.32	0.0	0.0	3.0	93.7	5.6	126.8	151.2	377.3
A8-A	Commercial	80	28.45			28.45					13.8	0.0	9.4	107.5	5.6	136.2	151.2	400.5
A8-B	High Density Residential	80			39.34	39.34	135.0	5311	25421	2.24	0.0	0.0	13.0	107.5	5.6	149.2	184.4	446.7
A8-C	Institutional	80		10.52		10.52					0.0	3.4	3.5	107.5	9.0	152.6	184.4	453.6
A8-D	Low Density Residential	80			16.87	16.87	120.9	2040	27461	2.21	0.0	0.0	5.6	107.5	9.0	168.2	196.9	471.6
ROW Along SNC Sewer Alignment	-	80				14.34					0.0	0.0	4.7	107.5	9.0	162.9	196.9	476.3
TOTAL		80	221.24	27.77	230.38	493.73	-	27461	27461	2.21	107.5	9.0	162.9	107.5	9.0	162.9	196.9	476.3

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 - 28 (28 used)	2.7 - 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 - 60 (60 used)	2.7	162.0
High Density (apartments)	60 - 75 (75 used)	1.8	135.0

Notes:

- Harmon Equation = $1 + [14 / (4 + (P/1000)^{1/2})] \times K$
 Where: P = population; K = correction factor = 0.8
- Commercial Peaking Factor = 1.5; Institutional Peaking Factor = 1.0

Reported Design Flows / Assumptions:

- Area A4: Existing single family units currently serviced by Jockvale pump station to be redirected to SNC
- Area A8-D: proposed 600 medium density residential units

See Note (2) in the DSEL "Barrhaven Conservancy - Evaluation of SNC Flows" design sheet

THE PRIOR NOVATECH SNC DESIGN SHEET HAD FLOWS AT 423.6 L/s AFTER AREA ID "A6-E".
 THIS UPDATED NOVATECH 'PHASE 3' EVALUATION HAS A FLOW OF 313.8 L/s.
 THE DSEL EVALUATION OF SANITARY FLOWS WITH THE NEW CITY DESIGN PARAMETERS AT THIS SAME NODE (WITH CONSERVANCY WEST AND EAST INCLUDED) IS ~401.05 L/s (WHICH IS LESS THAN THE PRIOR 423.6 L/s NOTED ABOVE)

SOUTH NEPEAN COLLECTOR (PHASE 3)
SANITARY SEWER DESIGN SHEET



DECEMBER 5 2018
JOB# 117190

LOCATION			Area				Population		Cumulative Design Flows					PROPOSED SEWER						
From MH	To MH	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Total Gross Area (ha)	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn ¹)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (280 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)	Length (m)	Pipe Size (mm)	Type	Slope %	Capacity (L/s)	Full Flow Velocity (m/s)	Ratio (Q/Qfull)
SA 22	SA 21	120	146.27	11.20	105.84	263.31	10974	2.53	71.1	3.6	86.9	90.0	251.7	131.9	750	CONC	0.10	367.3	0.81	69%
SA 21	SA 20	120											251.7	90.6	750	CONC	0.10	367.3	0.81	69%
SA 20	SA 19	120											251.7	90.0	750	CONC	0.10	367.3	0.81	69%
SA 19	SA 18	120											251.7	72.1	750	CONC	0.10	367.3	0.81	69%
SA 18	SA 17	120											251.7	71.9	750	CONC	0.10	367.3	0.81	69%
SA 17	SA 16	120											251.7	71.4	750	CONC	0.10	367.3	0.81	69%
SA 16	SA 15	110	163.99	11.20	105.84	281.03	10974	2.53	79.7	3.6	92.7	90.0	266.1	73.2	750	CONC	0.10	367.3	0.81	72%
SA 15	SA 14	110											266.1	67.5	750	CONC	0.10	367.3	0.81	72%
SA 14	SA 13	110											266.1	56.6	750	CONC	0.10	367.3	0.81	72%
SA 13	SA 12	110											266.1	133.5	750	CONC	0.10	367.3	0.81	72%
SA 12	SA 11	110											266.1	150.0	750	CONC	0.10	367.3	0.81	72%
SA 11	SA 10	100	179.17	17.25	105.84	302.26	10974	2.53	87.1	5.6	99.7	90.0	282.5	97.8	750	CONC	0.10	367.3	0.81	77%
SA 10	SA 9	100											282.5	76.7	750	CONC	0.10	367.3	0.81	77%
SA 9	SA 8	100											282.5	79.7	750	CONC	0.10	367.3	0.81	77%
SA 8	SA 7	100											282.5	75.3	750	CONC	0.10	367.3	0.81	77%
SA 7	SA 6	100											282.5	84.9	750	CONC	0.10	367.3	0.81	77%
SA 6	SA 5	100											282.5	77.1	750	CONC	0.10	367.3	0.81	77%
SA 5	SA 4	100											282.5	78.9	750	CONC	0.10	367.3	0.81	77%
SA 4	SA 3	100											282.5	80.5	750	CONC	0.10	367.3	0.81	77%
SA 3	SA 2	100											282.5	150.0	750	CONC	0.10	367.3	0.81	77%
SA 2	SA 1	100											282.5	114.6	750	CONC	0.10	367.3	0.81	77%
SA 1	EX 80	100											282.5	12.4	750	CONC	0.10	367.3	0.81	77%

Design Parameters:

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles / semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row / townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

Notes:

- Harmon Equation = $1 + [14 / (4 + (P/1000)^{1/2})] \times K$
Where: P = population; K = correction factor = 0.8
- Commercial Peaking Factor = 1.5; Institutional Peaking Factor = 1.0

Reported Design Flows / Assumptions:

- Area A4: Existing single family units currently serviced by Jockvale pump station to be redirected to SNC
- Area A8-D: proposed 600 medium density residential units



MEMORANDUM

DATE: MAY 26, 2016
TO: JONATHAN KNOYLE – CITY OF OTTAWA
FROM: CONRAD STANG – NOVATECH
RE: SOUTH NEPEAN COLLECTOR PHASE 2: SANITARY FLOW CALCULATIONS
CC: EDSON DONNELLY – NOVATECH

1.0 PURPOSE

This memorandum provides the sanitary sewer flow calculations and design sheet for Phase 2 of the proposed South Nepean Collector (SNC). Sanitary design flows have been estimated for both current-day operational flows and future development peak design flows, based on the latest available planning information for the vacant lands within the SNC sewershed.

2.0 BACKGROUND

In January 1998, the Master Servicing Study for the South Nepean Urban Area provided a conceptual plan for water, wastewater and stormwater infrastructure. The preferred alternative for wastewater servicing was an east/west trunk sewer alignment that was to be completed in several phases. The proposed sanitary trunk sewer was initially called the Jock River Collector, but was renamed the South Nepean Collector during the original functional design study completed in 2003.

Phase 1 of the South Nepean Collector was completed in 2005 and currently terminates at a 2400mm maintenance hole located east of Longfields Drive, north of Bren-Maur Road. Phase 2 will extend the trunk sewer to Strandherd Drive at the intersection of the proposed transitway along the proposed extension to Chapman Mills Drive. Phase 3 will extend the trunk sewer along Strandherd Drive to the intersection of Maravista Drive.

The sanitary sewer flows were previously documented in the *South Nepean Collector – Functional Design Report and Update* (Dillon, 2012). A review of the sanitary flows provided in the Dillon Report based on the latest planning information for the vacant lands within the SNC sewershed was documented in the technical memorandum titled *South Nepean Collector Phase 2: Hydraulics Review / Assessment* (Novatech, 2015), which is attached to this memorandum. The results of the *Hydraulics Review / Assessment* (Novatech, 2015) were very similar to the results from the Dillon (2012) analysis.

3.0 DESIGN PARAMETERS AND POPULATION ESTIMATES

3.1 Design Parameters

The sanitary design flow were calculated using the parameters from the City of Ottawa Sewer Design Guidelines (October 2012), and are summarized in **Table 1** and **Table 2**.

Table 1: Peak Design Flow Parameters

Land Use	Average Daily Flow	Peaking Factor	Peak Extraneous Flows
Residential	350 L/cap/day	Harmon Equation, K=1 (2.0 min – 4.0 max)	0.28 L/s/ha
Commercial	50,000 L/ha/day	1.5	
Institutional	50,000 L/ha/day	1.5	
Other*	0 L/ha/day	N/A	

*Open Space, Arterial ROW, SWM Blocks, etc. with no sanitary flow contribution (extraneous flow only)

Table 2: Operational Design Flow Parameters

Land Use	Average Daily Flow	Peaking Factor	Peak Extraneous Flows
Residential	300 L/cap/day	Harmon Equation, K=0.6 (1.2 min – 2.4 max)	<u>Dry weather</u> 0.05-0.08 L/s/ha
Commercial	17,000 L/ha/day	1.0 (non-coincident peak)	<u>Wet Weather</u> 0.15 - 0.20 L/s/ha (typical events) 0.28 L/s/ha (large/annual events) 0.30 - 0.50 L/s/ha (extreme events)
Institutional	10,000 L/ha/day	1.0 (non-coincident peak)	

*There are no industrial areas identified within the tributary area.

$$\text{Harmon Equation} = 1 + \frac{14}{4 + \left(\frac{P}{1000}\right)^{\frac{1}{2}}} \times K$$

Where:

P = Population

K = Correction Factor:

- Peak Flow = 1

- Operational = between 0.4 to 0.6 (0.6 used)

3.2 Land Use Designations & Population Estimates

Population densities and unit counts for future residential development are based on the current concept plans for these areas, and are presented in **Table 3**.

Table 3: Residential Land Use Population Densities

Residential Land Use	Units per ha	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

The land use designations shown in **Table 4** have been applied for the areas within Phases 2 and 3 of the SNC (Node 70 to 130). The sewershed areas and land use designations were delineated using aerial photos (existing development) and conceptual site plans (future development).

Table 4: Land Use Designations

Land Use Designation	
Secondary Plan	SNC Design
Residential	Residential (Low / Medium / High Density)
Institutional / Office	Institutional
Commercial	Commercial
Recreational	
Business Park	
Prestige Business Park	
Park/Open Space Area	Other*
Ex. Snow Disposal Facility (future commercial)	
Stormwater Management Facility	
Conservation Lands	
Arterial Right-of-Ways	

* No sanitary flow contribution - extraneous flows (inflow/infiltration) only.

The overall residential population estimate and sewershed area for Phases 2 and 3 of the SNC is provided in **Table 5** below. It is assumed that the snow dump facility at the Stranderd Drive and McKenna Casey Drive will ultimately be re-zoned for commercial development.

Table 5: Population Estimates and Areas

Existing / Future	Estimated Population / Area	Novatech (2015)
Existing	Estimated Population	6,944 persons
	Gross Residential Area	60.09 ha
	Gross Commercial / Institutional Area	64.37 ha
	<i>Total Sewershed Area</i>	124.5 ha
Future (full service)	Estimated Population	27,312 persons
	Gross Residential Area	248.48 ha
	Gross Commercial / Institutional Area	228.82 ha
	<i>Total Sewershed Area</i>	477.3 ha

4.0 SANITARY DESIGN FLOWS

The sanitary flow allocations for Phases 2 and 3 of the SNC are provided in **Table 6**. The corresponding sanitary drainage area plan is provided as **Figure 1**. Sanitary sewer flow calculations for Phases 2 and 3 and detailed sanitary sewer design sheets for Phase 2 are attached to this memorandum.

The estimated sanitary design flows from Phases 2 and 3 of the SNC (entering Node 70) are as follows:

- Present-Day Operational Design Flows (Theoretical) = 72.5 L/s
- Future Peak Design Flows = 634.2 L/s

The outlet for Phase 2 of the SNC is the existing 1050mm outlet pipe at the 2400mm maintenance hole (Node 70) located east of Longfields Drive, north of Bren-Maur Road. Given a minimum design slope of 0.10%, this sanitary trunk sewer would have a full flow capacity of 900.5 L/s. Therefore, the downstream sanitary trunk sewer would be at 70% capacity, based on the future peak design flow being 634.2 L/s.

ATTACHMENTS:

- Figure 1: Sanitary Drainage Areas and Land Use
- Sanitary Sewer Flow Calculations
- Sanitary Sewer Design Sheets (Phase 2)
- South Nepean Collector Phase 2: Hydraulics Review / Assessment (Novatech, 2015)

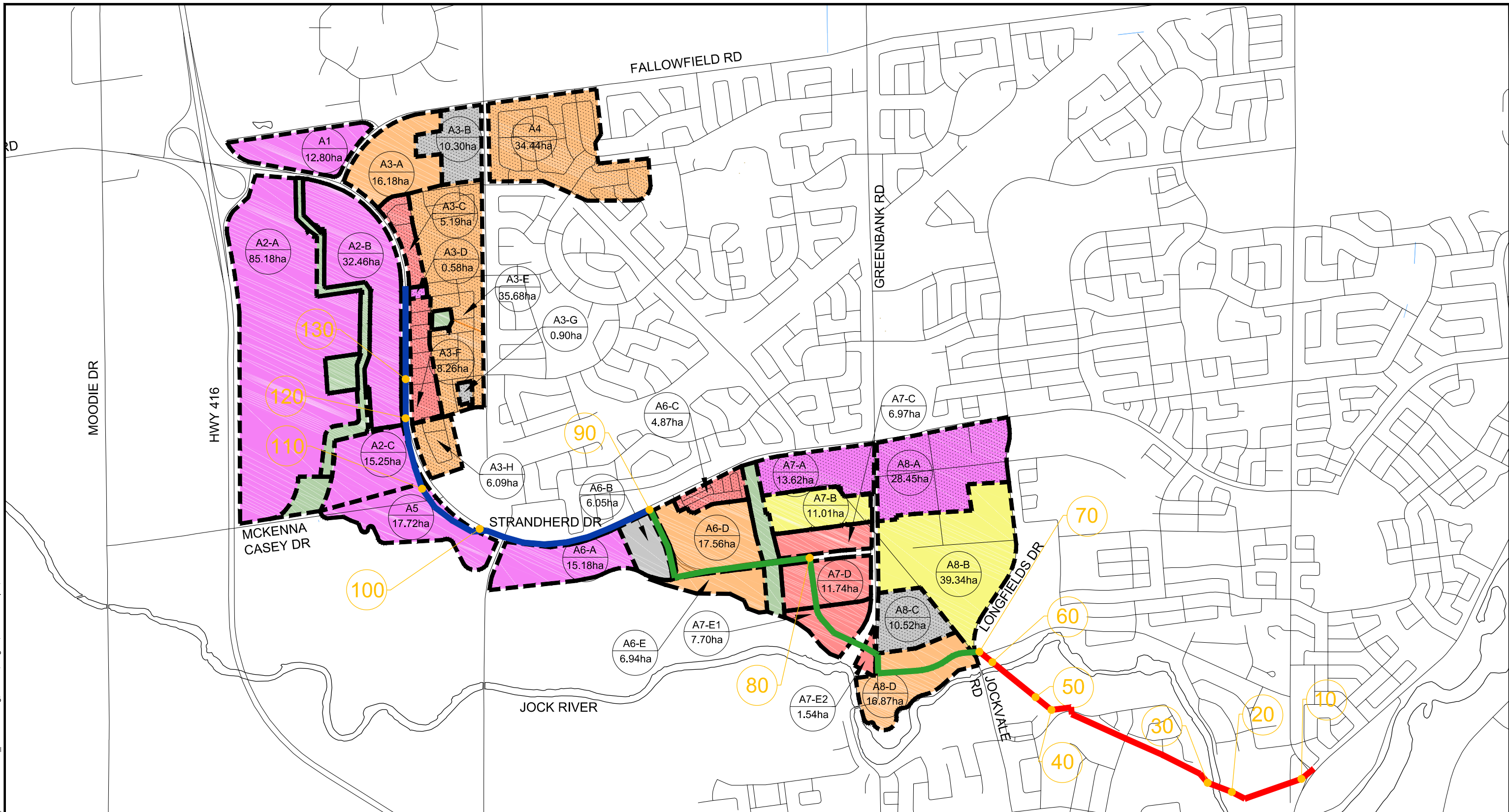


Table 6: Updated Allocation of Commercial, Institutional and Residential Demands to Phases 2 & 3 (Nodes 70 – 130) of the SNC by Collection Area

Collection Area	Upstream Node	Existing / Proposed Development	Existing / Proposed Land Use	Area (ha)	Estimated Number of Residential Units	Population Density (persons / ha)	Comment	Reference
A1	130	Proposed	Commercial	12.80	-	-	O'Keefe Court – Conceptual site plan shows proposed commercial.	Conceptual Plans for O'Keefe Court
A2-A	130	Proposed	Commercial	85.18	-	-	CitiGate – Analysis uses same approach as the design for CitiGate.	Detailed Servicing and SWM Report (Phase 1) (Novatech, 2014)
A2-B	130	Proposed	Commercial	32.46	-	-		
A2-C	120	Proposed	Commercial (ex. Snow dump)	15.25	-	-	Existing snow dump facility assumed to be future commercial.	Functional Design Report and Update – SNC Phase 2 and 3 (Dillon, 2012)
A3-A	130	Proposed	Low Density Residential	16.48	461	95.2	Havencrest – Existing single family units.	Havencrest Design Report (IBI, 2013)
A3-B	130	Existing	Institutional	10.30	-	-	Cedarview Middle School and Cedarview Alliance Church.	Aerial Photos / Site Visits
A3-C	130	Existing	Medium Density Residential	5.19	311	162	Existing townhouse units.	
A3-D	130	Existing	Commercial	0.58	-	-	Existing commercial buildings.	
A3-E	130	Existing	Low Density Residential	35.68	999	95.2	Existing single family units.	
A3-F	130	Existing	Medium Density Residential	8.26	496	162.0	Existing townhouse units.	
A3-G	130	Existing	Institutional	0.90	-	-	Ottawa Torah Centre Chibad.	
A3-H	120	Existing	Low Density Residential	6.09	171	95.2	Existing single family units.	
A4	130	Existing	Low Density Residential	34.44	964	95.2	Existing single family units currently serviced by Jockvale pump station; to be redirected to SNC.	
A5	110	Proposed	Commercial	17.72	-	-	Proposed commercial south of McKenna Casey Drive.	Site Visits
A6-A	100	Proposed	Institutional	20.70	-	-	Proposed school site on Minto property.	Conceptual Plan for Lands Adjacent the Kennedy-Burnett SWMF provided by Minto (2015)
A6-B	90	Existing	Medium Density Residential	4.87	292	162.0	Existing townhouse units.	Aerial Photos / Site Visits
A6-C	90	Proposed	Low Density Residential	10.11	283	95.2	Proposed single family units on lands owned by Minto.	Conceptual Plans for Lands Adjacent the Kennedy-Burnett SWMF provided by land owners.
A6-D	90	Proposed	Low Density Residential	5.59	157	95.2	Proposed single family units on lands owned by Mion.	
A6-E	90	Proposed	Low Density Residential	7.24	203	95.2	Proposed single family units on lands owned by Pavic / Braovac.	
A7-A	80	Existing	Commercial	13.62	-	-	Existing large retail stores (commercial).	Aerial Photos
A7-B	80	Proposed	High Density Residential	11.01	826	135.0	Proposed high density units on lands owned by Richcraft / Trinity.	Conceptual Plans for Lands Adjacent the Kennedy-Burnett SWMF provided by land owners.
A7-C	80	Proposed	Medium Density Residential	6.97	418	162.0	Proposed Medium density units on lands owned by Mion.	
A7-D	80	Proposed	Medium Density Residential	11.74	704	162.0	Proposed Medium density units on lands owned by Caivan.	
A7-E1/E2	80	Proposed	Medium Density Residential	9.24	554	162.0	Proposed Medium density units on lands owned by Claridge.	
A8-A	80	Existing	Commercial	28.45	-	-	Existing Barrhaven Market Place (commercial).	Aerial Photos / Site Visits
A8-B	80	Proposed	High Density Residential	39.34	2951	135.0	Future development similar to Ampersands development.	Site Visits
A8-C	80	Existing	Institutional	10.52	-	-	Existing St. Joseph High School.	Aerial Photos / Site Visits
A8-D	80	Proposed	Low Density Residential	16.87	1012	162.0	Proposed 600 low density residential units.	Functional Design Report and Update – SNC Phase 2 and 3 (Dillon, 2012)

Attachment 1
Sanitary Drainage Areas and Land Use

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LEGEND

- | | | | |
|--|--|--|--|
| | EXISTING / PROPOSED HIGH DENSITY RESIDENTIAL | | OTHER LANDS (OPEN SPACE, PARKS, AND SWMFS) |
| | EXISTING / PROPOSED MEDIUM DENSITY RESIDENTIAL | | SOUTH NEPEAN COLLECTOR PHASE 1 |
| | EXISTING / PROPOSED LOW DENSITY RESIDENTIAL | | SOUTH NEPEAN COLLECTOR PHASE 2 |
| | EXISTING / PROPOSED COMMERCIAL | | SOUTH NEPEAN COLLECTOR PHASE 3 |
| | EXISTING / PROPOSED INSTITUTIONAL | | SOUTH NEPEAN COLLECTOR NODE ID |



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**SOUTH NEPEAN COLLECTOR SEWER
 SANITARY DRAINAGE AREAS AND LAND USE**

SCALE 1:20 000

DATE MAY 2016 JOB 115075 FIGURE FIG. 1

Attachment 2
Sewer Flow Calculations

PROJECT #: 115075
 DESIGNED BY: CMS
 CHECKED BY: MJP
 DATE: August 20, 2015

SANITARY SEWER DESIGN SHEET

South Nepean Collector - Phase 2 & 3

Theoretical Current Operational Peak Wastewater Flow



Location			Areas				Population				Individual Design Flows			Cumulative Design Flows				
Area I.D.	Existing Land Use	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Total Gross Area (ha)	Residential Population Density (people / ha)	Individual Residential Population	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn ¹)	Commercial Peak Flow Rate ² (17,000 L/ha/d) (L/s)	Institutional Peak Flow Rate ² (10,000 L/ha/d) (L/s)	Infiltration / Inflow Rate (0.05 L/s/ha) (L/s)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (300 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)
A1	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A2-A	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A2-B	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A3-A	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A3-B	Institutional	130		10.30		10.30					0.0	1.2	0.5	0.0	1.2	0.5	0.0	1.7
A3-C	Medium Density Residential	130			5.19	5.19	162.0	841	841	2.71	0.0	0.0	0.3	0.0	1.2	0.8	7.9	9.9
A3-D	Commercial	130	0.58			0.58		841	841	2.71	0.1	0.0	0.0	0.1	1.2	0.8	7.9	10.0
A3-E	Low Density Residential	130			35.68	35.68	95.2	3397	4238	2.39	0.0	0.0	1.8	0.1	1.2	2.6	35.1	39.0
A3-F	Medium Density Residential	130			8.26	8.26	162	1338	5576	2.32	0.0	0.0	0.4	0.1	1.2	3.0	44.9	49.2
A3-G	Institutional	130		0.90		0.90			5576	2.32	0.0	0.1	0.0	0.1	1.3	3.0	44.9	49.4
A4	Low Density Residential*	130				0.00			5576	2.32	0.0	0.0	0.0	0.1	1.3	3.0	44.9	49.4
A2-C	Snow Dump Facility	120				0.00			5576	2.32	0.0	0.0	0.0	0.1	1.3	3.0	44.9	49.4
A3-H	Low Density Residential	120			6.09	6.09	95.2	580	6155	2.30	0.0	0.0	0.3	0.1	1.3	3.4	49.1	53.8
A5	Open Space	110				0.00			6155	2.30	0.0	0.0	0.0	0.1	1.3	3.4	49.1	53.8
A6-A	Open Space	100				0.00			6155	2.30	0.0	0.0	0.0	0.1	1.3	3.4	49.1	53.8
A6-B	Open Space	100				0.00			6155	2.30	0.0	0.0	0.0	0.1	1.3	3.4	49.1	53.8
A6-C	Medium Density Residential	90			4.87	4.87	162.0	789	6944	2.27	0.0	0.0	0.2	0.1	1.3	3.6	54.6	59.6
A6-D	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	0.1	1.3	3.6	54.6	59.6
A6-E	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	0.1	1.3	3.6	54.6	59.6
A7-A	Commercial	90	13.62			13.62			6944	2.27	2.7	0.0	0.7	2.8	1.3	4.3	54.6	63.0
A7-B	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	1.3	4.3	54.6	63.0
A7-C	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	1.3	4.3	54.6	63.0
A7-D	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	1.3	4.3	54.6	63.0
A7-E1/E2	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	1.3	4.3	54.6	63.0
A8-A	Commercial	80	28.45			28.45			6944	2.27	5.6	0.0	1.4	8.4	1.3	5.7	54.6	70.0
A8-B	Open Space	80				0.00			6944	2.27	0.0	0.0	0.0	8.4	1.3	5.7	54.6	70.0
A8-C	Institutional	80		10.52		10.52			6944	2.27	0.0	1.2	0.5	8.4	2.5	6.2	54.6	71.8
A8-D	Open Space	80				0.00			6944	2.27	0.0	0.0	0.0	8.4	2.5	6.2	54.6	71.8
ROW Along SNC Sewer Alignment	-	80				14.34			6944	2.27	0.0	0.0	0.7	8.4	2.5	6.9	54.6	72.5
TOTAL		80	42.65	21.72	60.09	138.80	-	6944	6944	2.27	8.4	2.5	6.9	8.4	2.5	6.9	54.6	72.5

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

Notes:

- Harmon Equation = $1 + [14 / (4 + (P/1000)^{1/2})] \times K$
 Where: P = population; K = correction factor = 0.6
- Institutional / Commercial Peaking Factor = 1.0

Reported Design Flows / Assumptions:

- Area A4: Existing single family units currently serviced by Jockvale pump station; currently not directed to SNC

PROJECT #: 115075
 DESIGNED BY: CMS
 CHECKED BY: MJP
 DATE: August 20, 2015

SANITARY SEWER DESIGN SHEET

South Nepean Collector - Phase 2 & 3

Theoretical Future Full Service Peak Wastewater Flow



Location			Areas				Population				Individual Design Flows			Cumulative Design Flows				
Area I.D.	Existing / Proposed Land Use	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Total Gross Area (ha)	Residential Population Density (people / ha)	Individual Residential Population	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn ¹)	Commercial Peak Flow Rate ² (50,000 L/ha/d) (L/s)	Institutional Peak Flow Rate ² (50,000 L/ha/d) (L/s)	Infiltration / Inflow Rate (0.28 L/s/ha) (L/s)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (350 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)
A1	Commercial	130	12.80			12.80					11.1	0.0	3.6	11.1	0.0	3.6	0.0	14.7
A2-A	Commercial	130	85.18			85.18					73.9	0.0	23.9	85.1	0.0	27.4	0.0	112.5
A2-B	Commercial	130	32.46			32.46					28.2	0.0	9.1	113.2	0.0	36.5	0.0	149.8
A3-A	Low Density Residential	130			16.18	16.18	95.2	1540	1540	3.67	0.0	0.0	4.5	113.2	0.0	41.1	22.9	177.2
A3-B	Institutional	130		10.30		10.30		1540	1540	3.67	0.0	8.9	2.9	113.2	8.9	43.9	22.9	189.0
A3-C	Medium Density Residential	130			5.19	5.19	162.0	841	2381	3.53	0.0	0.0	1.5	113.2	8.9	45.4	34.0	201.6
A3-D	Commercial	130	0.58			0.58		2381	2381	3.53	0.5	0.0	0.2	113.7	8.9	45.6	34.0	202.2
A3-E	Low Density Residential	130			35.68	35.68	95.2	3397	5778	3.19	0.0	0.0	10.0	113.7	8.9	55.5	74.6	252.8
A3-F	Medium Density Residential	130			8.26	8.26	162	1338	7116	3.10	0.0	0.0	2.3	113.7	8.9	57.9	89.4	269.9
A3-G	Institutional	130		0.90		0.90		7116	7116	3.10	0.0	0.8	0.3	113.7	9.7	58.1	89.4	270.9
A4	Low Density Residential	130			34.44	34.44	95.2	3279	10395	2.94	0.0	0.0	9.6	113.7	9.7	67.8	123.7	314.9
A2-C	Commercial (ex. snow dump)	120	15.25			15.25		10395	10395	2.94	13.2	0.0	4.3	127.0	9.7	72.0	123.7	332.4
A3-H	Low Density Residential	120			6.09	6.09	95.2	580	10974	2.91	0.0	0.0	1.7	127.0	9.7	73.7	129.6	340.0
A5	Commercial	110	17.72			17.72		10974	10974	2.91	15.4	0.0	5.0	142.4	9.7	78.7	129.6	360.3
A6-A	Commercial	100	15.18			15.18		10974	10974	2.91	13.2	0.0	4.3	155.5	9.7	82.9	129.6	377.8
A6-B	Institutional	100		6.05		6.05		10974	10974	2.91	0.0	5.3	1.7	155.5	15.0	84.6	129.6	384.7
A6-C	Medium Density Residential	90			4.87	4.87	162.0	789	11763	2.88	0.0	0.0	1.4	155.5	15.0	86.0	137.4	393.9
A6-D	Low Density Residential	90			17.56	17.56	95.2	1672	13435	2.83	0.0	0.0	4.9	155.5	15.0	90.9	153.8	415.2
A6-E	Low Density Residential	90			6.94	6.94	95.2	661	14096	2.81	0.0	0.0	1.9	155.5	15.0	92.9	160.2	423.6
A7-A	Commercial	90	13.62			13.62		14096	14096	2.81	11.8	0.0	3.8	167.4	15.0	96.7	160.2	439.2
A7-B	High Density Residential	90			11.01	11.01	135.0	1486	15582	2.76	0.0	0.0	3.1	167.4	15.0	99.8	174.3	456.4
A7-C	Medium Density Residential	90			6.97	6.97	162.0	1129	16711	2.73	0.0	0.0	2.0	167.4	15.0	101.7	184.9	468.9
A7-D	Medium Density Residential	90			11.74	11.74	162.0	1902	18613	2.68	0.0	0.0	3.3	167.4	15.0	105.0	202.4	489.7
A7-E1/E2	Medium Density Residential	90			9.24	9.24	162.0	1497	20110	2.65	0.0	0.0	2.6	167.4	15.0	107.6	215.9	505.8
A8-A	Commercial	80	28.45			28.45		20110	20110	2.65	24.7	0.0	8.0	192.0	15.0	115.5	215.9	538.5
A8-B	High Density Residential	80			39.34	39.34	135.0	5311	25421	2.55	0.0	0.0	11.0	192.0	15.0	126.6	262.4	596.0
A8-C	Institutional	80		10.52		10.52		25421	25421	2.55	0.0	9.1	2.9	192.0	24.1	129.5	262.4	608.1
A8-D	Low Density Residential	80			16.87	16.87	120.9	2040	27461	2.52	0.0	0.0	4.7	192.0	24.1	134.2	279.8	630.2
ROW Along SNC Sewer Alignment	-	80				14.34			27461	2.52	0.0	0.0	4.0	192.0	24.1	138.2	279.8	634.2
TOTAL		80	221.24	27.77	230.38	493.73	-	27461	27461	2.52	192.0	24.1	134.2	192.0	24.1	138.2	279.8	634.2

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

Notes:

- Harmon Equation = $1 + [14 / (4 + (P/1000)^{1/2})] \times K$
 Where: P = population; K = correction factor = 1.0
- Institutional / Commercial Peaking Factor = 1.5

Reported Design Flows / Assumptions:

- Area A4: Existing single family units currently serviced by Jockvale pump station to be redirected to SNC
- Area A8-D: proposed 600 medium density residential units

THIS PRIOR NOVATECH SNC DESIGN SHEET HAD DESIGN FLOWS AT 423.6 L/S AFTER AREA ID "A6-E".

THE DSEL EVALUATION WITH NEW PARAMETERS AT THIS SAME NODE WITH CONSERVANCY WEST AND EAST INCLUDED IS ~401.05 < 423.6 L/S

Attachment 3
Sanitary Sewer Design Sheets (Phase 2)

**SOUTH NEPEAN COLLECTOR (PHASE 2)
SANITARY SEWER DESIGN SHEET**



MAY 26, 2016
JOB# 115075

LOCATION			Area					Population				Individual Design Flows			Cumulative Design Flows				PROPOSED SEWER							
From MH	To MH	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Right-of-Way (ha)	Total Gross Area (ha)	Residential Population Density (people / ha)	Individual Residential Population	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn ¹)	Commercial Peak Flow Rate ² (50,000 L/ha/d) (L/s)	Institutional Peak Flow Rate ² (50,000 L/ha/d) (L/s)	Infiltration / Inflow Rate (0.28 L/s/ha) (L/s)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (350 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)	Length (m)	Pipe Size (mm)	Type	Slope %	Capacity (L/s)	Full Flow Velocity (m/s)	Ratio (Q/Qfull)
MHSA 1	MHSA 2	90	192.79	17.25	174.17	0.00	384.21	1678	20110	20110	2.65	167.352	14.97	107.58	167.4	15.0	107.6	215.9	505.8	57.3	900	CONC	0.10	597.2	0.91	85%
MHSA 2	MHSA 3	90																	505.8	57.3	900	CONC	0.10	597.2	0.91	85%
MHSA 3	MHSA 4	90																	505.8	73.9	900	CONC	0.10	597.2	0.91	85%
MHSA 4	MHSA 5	90																	505.8	34.6	900	CONC	0.10	597.2	0.91	85%
MHSA 5	MHSA 6	90																	505.8	42.8	900	CONC	0.10	597.2	0.91	85%
MHSA 6	MHSA 7	90																	505.8	84.4	900	CONC	0.10	597.2	0.91	85%
MHSA 7	MHSA 8	90																	505.8	16.5	900	CONC	0.10	597.2	0.91	85%
MHSA 8	MHSA 9	90																	505.8	85.4	900	CONC	0.10	597.2	0.91	85%
MHSA 9	MHSA 10	90																	505.8	70.6	900	CONC	0.10	597.2	0.91	85%
MHSA 10	MHSA 11	90																	505.8	70.6	900	CONC	0.10	597.2	0.91	85%
MHSA 11	MHSA 12	90																	505.8	77.8	900	CONC	0.10	597.2	0.91	85%
MHSA 12	MHSA 13	90																	505.8	77.8	900	CONC	0.10	597.2	0.91	85%
MHSA 13	MHSA 14	90																	505.8	77.8	900	CONC	0.10	597.2	0.91	85%
MHSA 14	MHSA 15	90																	505.8	25.4	900	CONC	0.10	597.2	0.91	85%
MHSA 15	MHSA 16	90																	505.8	34.2	900	CONC	0.10	597.2	0.91	85%
MHSA 16	MHSA 17	90																	505.8	86.7	900	CONC	0.10	597.2	0.91	85%
MHSA 17	MHSA 18	90																	505.8	34.3	900	CONC	0.10	597.2	0.91	85%
MHSA 18	MHSA 19	90																	505.8	68.6	900	CONC	0.10	597.2	0.91	85%
MHSA 19	MHSA 20	90																	505.8	65.5	900	CONC	0.10	597.2	0.91	85%
MHSA 20	MHSA 21	80	221.24	27.77	230.38	14.34	493.73	256	7351	27461	2.52	192.049	24.11	138.24	192.0	24.1	138.2	279.8	634.2	18.2	1050	CONC	0.10	900.9	1.01	70%
MHSA 21	MHSA 22	80																	634.2	81.9	1050	CONC	0.10	900.9	1.01	70%
MHSA 22	MHSA 23	80																	634.2	84.7	1050	CONC	0.10	900.9	1.01	70%
MHSA 23	MHSA 24	80																	634.2	77.4	1050	CONC	0.10	900.9	1.01	70%
MHSA 24	MHSA 25	80																	634.2	45.5	1050	CONC	0.10	900.9	1.01	70%
MHSA 25	MHSA 26	80																	634.2	35.8	1050	CONC	0.10	900.9	1.01	70%
MHSA 26	MHSA 27	80																	634.2	83.3	1050	CONC	0.10	900.9	1.01	70%
MHSA 27	MHSA 28	80																	634.2	74.4	1050	CONC	0.10	900.9	1.01	70%
MHSA 28	MHSA 29	80																	634.2	77.3	1050	CONC	0.10	900.9	1.01	70%
MHSA 29	MHSA 30	80																	634.2	83.8	1050	CONC	0.10	900.9	1.01	70%
MHSA 30	MHSA 31	80																	634.2	42.3	1050	CONC	0.10	900.9	1.01	70%
MHSA 31	MHSA 32	80																	634.2	100.6	1050	CONC	0.10	900.9	1.01	70%
MHSA 32	MHSA 33	80																	634.2	13.9	1050	CONC	0.10	900.9	1.01	70%
MHSA 33	MHSA 34	80																	634.2	99.9	1050	CONC	0.10	900.9	1.01	70%
MHSA 34	MHSA 35	80																	634.2	99.9	1050	CONC	0.10	900.9	1.01	70%
MHSA 35	MHSA 36	80																	634.2	88.7	1050	CONC	0.10	900.9	1.01	70%
MHSA 36	MHSA 37	80																	634.2	88.8	1050	CONC	0.10	900.9	1.01	70%
MHSA 37	MHSA 38	80																	634.2	90.3	1050	CONC	0.10	900.9	1.01	70%
MHSA 38	MHSA 39	80																	634.2	87.5	1050	CONC	0.10	900.9	1.01	70%

Design Parameters:

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles / semis)	26 - 28 (28 used)	2.7 - 3.4 (3.4 used)	95.2
Medium Density (row / townhouse)	50 - 60 (60 used)	2.7	162.0
High Density (apartments)	60 - 75 (75 used)	1.8	135.0

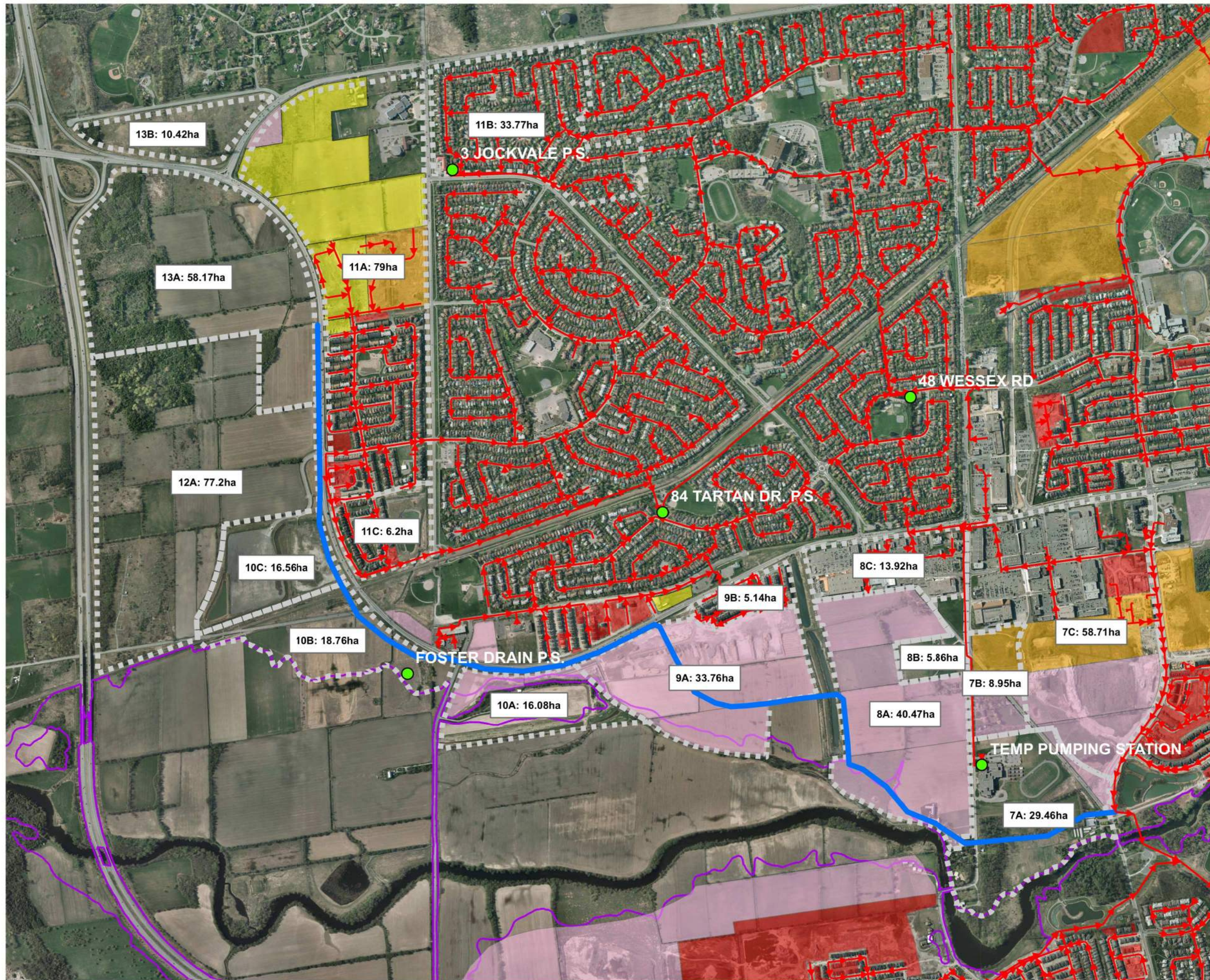
Notes:

1. Harmon Equation = $1 + [14 / (4 + (P/1000)^{1/2})] \times K$
Where: P = population; K = correction factor = 1.0
2. Institutional / Commercial Peaking Factor = 1.5

Reported Design Flows / Assumptions:

1. Area A4: Existing single family units currently serviced by Jockvale pump station to be redirected to SNC
2. Area A8-D: proposed 600 medium density residential units

Figure 01
Existing Sanitary Network and Collection Areas



- Pump Station
 - Existing Sanitary Main (With Flow Direction)
 - Proposed Alignment for South Nepean Collector
 - Collection Area
- DEVELOPMENT STATUS**
- Registered
 - Draft Approved
 - Pending
 - No Plan
 - Floodplain

NOT TO SCALE



MAP DRAWING INFORMATION:
DATA PROVIDED BY THE CITY OF OTTAWA

MAP CREATED BY: BC
MAP CHECKED BY: MBM
MAP PROJECTION: NO PROJECTION

FILE LOCATION: \\Dillon.ca\dillon_dfs\Ottawa\Ottawa_GA\CAD\2011\115681\Design_GIS\MXD\Figure01c_ExistingSanitaryNetwork.mxd

Table 5.1: Allocation of Commercial/Institutional and Residential Demands to SNC by Collection Area

Collection Area	Discharging Node	Estimated from GIS			City of Ottawa VURL Data			Other Space ¹ (ha)	Population (PE)	Residential Density (PE/net ha)	Comments	Additional Source(s)
		Gross Institutional/Commercial (ha)	Gross Residential (ha)	Gross Area (ha)	Net Residential (ha)	Units (#)	Unit Density (#/ha)					
7A	70	13.5	7.4	29.5	4.0	605	0.3	9.1	1637	4.25	Flow calculations include St Joseph H.S. Pump Station firm capacity of 7.0 L/s Additional 600 units (TAC)	3.4ppu (TAC)
7B		0.0	9.24	9.24	6.23	1474	136.7	3.0	3321	638.8	Population from split VURL allocated by area. VURL parcel id 323 - inconsistency between net and gross reported area.	2.7ppu (TAC)
8A		0.0	40.0	40.0	24.1	4462	185.1	15.9	12047.4	499.9		2.7ppu (TAC)
8B		5.9	0.0	5.9	0.0	0	0	0.0			Future Commercial area	
8C		13.9	0.0	13.9	0.0	0	0	0.0			Commercial area includes Home Depot	
9A	80	0.0	33.8	33.8	18.6	635	34.1	15.2	2210	116.2		3.4ppu (TAC)
10A	90	0.0	16.1	16.1	9.7	451	28.0	6.4	1533.4	158.0	Assume net population = 60% gross.	3.4ppu (TAC)
10B	100	18.8	0.0	35.3	0.0	0	0	16.5			Allocated as potential future I/C use as directed by TAC	
10C	110	16.6	0.0	35.3	0.0	0	0	18.7			Area includes current Municipal Snow Dump. Flow allowance is made for potential future I/C use	
11C		0.0	6.2	6.2	Note 2			2.5	306	82.7	This area is south of '11 block' in the existing development	From IBI Apr 2010 Report Figure 1
11A	120	12.5	66.5	79.0				26.6	3923	98.3	Institutional includes 4.38ha church site and 6.89 ha institution at northeast corner, as well and Claridge Commercial (0.56ha) and DCR/Phoenix Commercial (0.64ha)	From IBI Apr2010 Report Figure 1
11B		0.0	37.0	37.0				14.8	1550	69.8	Presently serviced by Jockvale pump station; to be redirected to SNC.	Estimated from 2011 Census Block data
12A		77.2	0.0	77.2				0.0			Allow sanitary peak flow 79.0 L/s	Novatech, Employment Lands Report, Revised Jan 2012
13A	130	58.5	0.0	58.5				0.0			Allow sanitary peak flow 62.8 L/s plus Collection Area 13B, total 82.2 L/s	
13B		12.5	0.0	12.5			0.0			Allow sanitary peak flow 19.4 L/s; gravity discharge to Collection Area 13A	IBI/Novatech	

Notes:

1. Other space includes other residential space accounting for the difference between gross area (measured with GIS) and net area (provided in VURL data), such as sidewalks, roads, greenspace, etc.
2. Collection Area 11A and 11B population and land use as identified under Additional Source(s). Other space reported as 60% of gross residential area, consistent with VURL average.

SOUTH NEPEAN COLLECTOR SEWER

SANITARY SEWER DESIGN SHEET - Operational Service (Average Flow Design Parameters)

TRIBUTARY AREA	Design Factors	LOCATION		AREA (ha)						INDIVIDUAL		CUMULATIVE		RESIDENTIAL		COMMERCIAL & INSTITUTION			INFL. INFLOW	PEAK DESIGN	FROPOSED SEWER									OPERATIONAL DESIGN								
		FROM	TO	Gross ICI	Net ICI	Other ICI space (Green, Sidewalks, roads)	Gross RESIDENTIAL Area	Net Residential Area	Other Res (Green, Sidewalks, roads)	TOTAL AREA (Gross ICI plus Gross Residential)	POP	DENSITY (po./ha.)	POP	AREA (ha.)	PEAKING FACTOR	RESIDENT. FLOW (L/s)	PEAKING FACTOR	CUM. AREA	I.C.I. FLOW (l/s)	Q(p) (L/s)	FLOW Q(d) (L/s)	LENGTH (m)	GROUND ELEVATION (m)	DEPTH OF COVER (m)	PIPE SIZE (m)	INVERT 1 (m)	INVERT 2 (m)	PIPE TYPE	GRADE	CAPACITY (L/s)	Q(d)/Q(c)	VELOCITY at capacity (m/s)	DEPTH (m)	VELOCITY (m/s)				
		13A	1			0.0	0.0	0.0	0.0	0.0	0.0	0		0	0.0	4.50	0.00	1.00	0.00	0.00	0.00	0.00																
13B	1		Node 130	0.0	0.0	0.0	0.0	0.0	0.0	0		0	0.0	4.50	0.00	1.00	0.00	0.00	0.00	0.00																		
12A	1		Node 130	0.0	0.0	0.0	0.0	0.0	0.0	0		0	0.0	4.50	0.00	1.00	0.00	0.00	0.00	0.00																		
11A	1			12.5	9.4	3.1	66.5	8.0	58.5	79.0	1196	148.76	1196	79.0	3.75	15.57	1.00	12.50	2.00	3.95	21.52																	
11B	1		Node 120	0.0	0.0	0.0	37.0	22.2	14.8	37.0	1550	69.82	2746	116.0	3.47	33.13	1.00	12.50	2.00	5.80	40.93																	
11C	1		Node 120	0.0	0.0	0.0	6.2	3.7	2.5	6.2	306	82.26	3052	122.2	3.44	36.41	1.00	12.50	2.00	6.11	44.82	531.89	93.60	4.42	0.750	88.96	88.43	Conc.	0.10%	353.24	0.13	0.80	0.20	0.58				
10C	1		Node 110	16.6	12.5	4.2	0.0	0.0	0.0	16.6	0		0	0.0	4.66	6.94	1.00	29.10	4.66	6.94	48.01																	
10B	1		Node 110	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0		0	0.0	4.66	6.94	1.00	29.10	4.66	6.94	48.01																	
10A	1		Node 100	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0		0	0.0	4.66	6.94	1.00	29.10	4.66	6.94	48.01																	
9A	1		Node 90	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0		0	0.0	4.66	6.94	1.00	29.10	4.66	6.94	48.01																	
8A	1		Node 80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0		0	0.0	4.66	6.94	1.00	29.10	4.66	6.94	48.01																	
8B	1			5.9	4.4	1.5	0.0	0.0	0.0	5.9	0		0	0.0	4.66	6.94	1.00	35.00	5.60	7.24	49.25																	
8C	1			13.9	10.4	3.5	0.0	0.0	0.0	13.9	0		0	0.0	4.66	6.94	1.00	48.90	7.82	7.93	52.17																	
7A	1			13.5	10.1	3.4	16.0	1.4	14.6	29.5	17	12.14	3069	188.1	3.43	36.59	1.00	62.40	9.98	9.41	55.93																	
7B	1		Node 70	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0		0	0.0	3.43	36.59	1.00	62.40	9.98	9.41	55.93	1448.98	91.24	6.01	1.050	85.63	84.18	Conc.	0.10%	864.51	0.06	1.00	0.18	0.56				
										188.1																												
										DEFAULTS																												
										q=AVERAGE DAILY FLOW										300 L/CAP.D																		
										I=UNIT OF PEAK EXTR.FLOW										0.050 L/Ha.s																		
										Mannings 'n'										0.013																		
										q=AVERAGE COMMERCIAL AND INSTITUTIONAL										0.16 L/Ha.s																		
DESIGN	D.J.G.																																					
CHECKED																																						
TODAY:	7/18/2012																																					



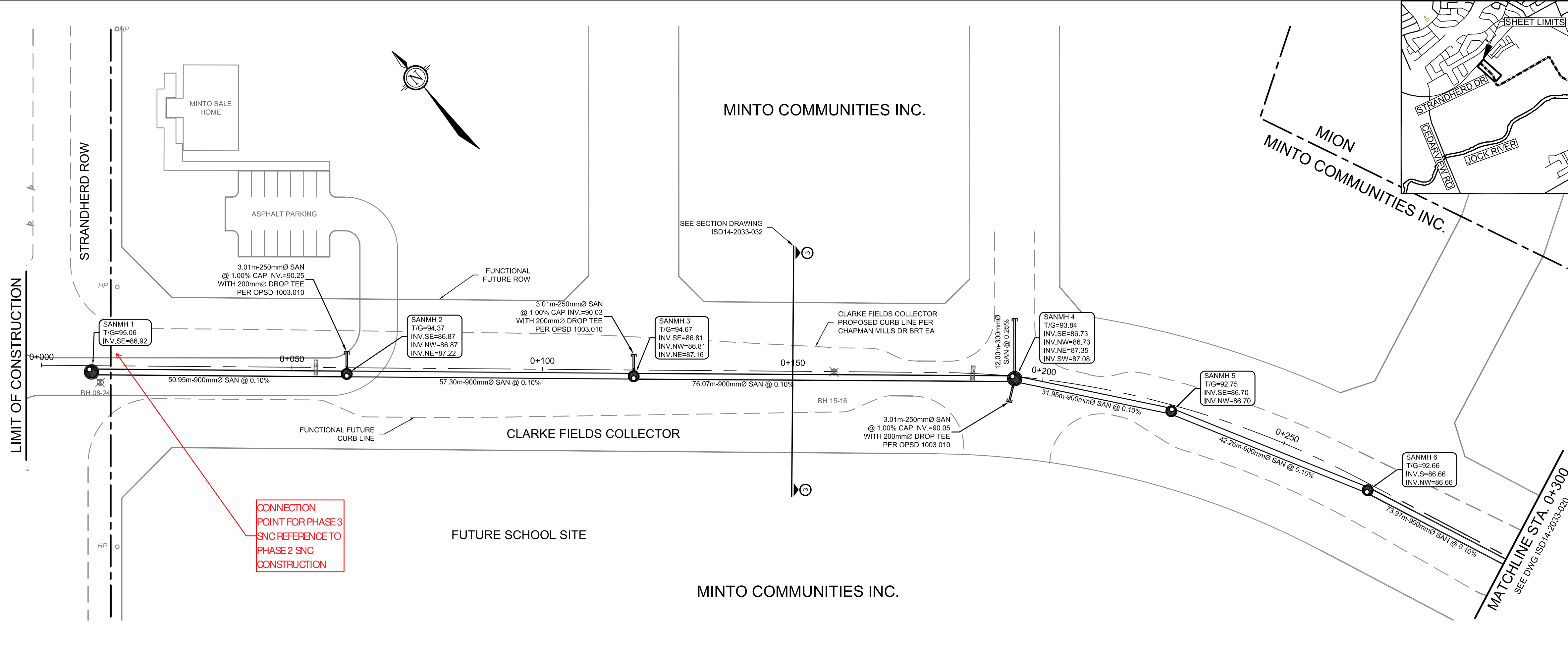
Project 11-5681

**SOUTH NEPEAN COLLECTOR SEWER
SANITARY SEWER DESIGN SHEET - Full Service (Peak Flow Design Parameters)**

TRIBUTARY AREA	Design Factors	LOCATION		AREA (ha)							INDIVIDUAL		CUMULATIVE		RESIDENTIAL		COMMERCIAL & INSTITUTION			INFL. INFLOW (L/s)	PEAK DESIGN FLOW Q(d) (L/s)	PROPOSED SEWER							PEAK DESIGN										
		FROM	TO	Gross ICI	Net ICI	Other ICI space (Green, Sidewalks, roads)	Gross RESIDENTIAL Area	Net Residential Area	Other Res (Sidewalks, roads)	TOTAL AREA (Gross ICI plus Gross Residential)	POP	DENSITY (pers/net ha.)	POP	Total I/C and Res AREA (ha.)	PEAKING FACTOR	RESIDENT. FLOW (L/s)	PEAKING FACTOR	I/C CUM. AREA	I/C FLOW (l/s)			Q(p) (L/s)	FLOW Q(d) (L/s)	LENGTH (m)	GROUND ELEVATION (m)	DEPTH OF COVER (m)	PIPE SIZE (m)	INVERT 1 (m)	INVERT 2 (m)	PIPE TYPE	GRADE	CAPACITY (L/s)	Q(d)Q(c)	VELOCITY at capacity (m/s)	DEPTH (m)	VELOCITY (m/s)			
13A	1			58.5	43.9	14.6	0.0	0.0	0.0	58.5	0	0	58.5	4.50	0.00	1.50	58.50	50.90	16.38	67.28																			
13B	1		Node 130	12.5	9.4	3.1	0.0	0.0	0.0	12.5	0	0	71.0	4.50	0.00	1.50	71.00	61.77	19.88	81.65																			
12A	1	Node 130		77.2	57.9	19.3	0.0	0.0	0.0	77.2	0	0	148.2	4.50	0.00	1.50	148.20	128.93	41.50	170.43																			
11A	1			12.5	9.4	3.1	66.5	39.9	26.6	79.0	3923	98.32	3923	227.2	3.34	53.09	1.50	160.70	139.81	63.62	256.52																		
11B	1		Node 120	0.0	0.0	0.0	37.0	22.2	14.8	37.0	1550	69.82	5473	264.2	3.21	71.13	1.50	160.70	139.81	73.98	284.92	531.89	93.60	4.42	0.750	88.96	88.43	Conc.	0.10%	353.24	0.81	0.80	0.53	0.90					
11C	1	Node 120		0.0	0.0	0.0	6.2	3.7	2.5	6.2	306	82.26	5779	270.4	3.19	74.59	1.50	160.70	139.81	75.71	290.11																		
10C	1		Node 110	16.6	12.5	4.2	0.0	0.0	0.0	16.6	0	0	5779	287.0	3.19	74.59	1.50	177.30	154.25	80.36	309.20	497.82	93.44	4.76	0.750	88.43	87.93	Conc.	0.10%	353.24	0.88	0.80	0.55	0.91					
10B	1	Node 110	Node 100	18.8	14.1	4.7	0.0	0.0	0.0	18.8	0	0	5779	305.8	3.19	74.59	1.50	196.10	170.61	85.62	330.82	603.17	93.03	4.95	0.750	87.93	87.33	Conc.	0.10%	353.24	0.94	0.80	0.58	0.92					
10A	1	Node 100	Node 90	0.0	0.0	0.0	16.1	9.7	6.4	16.1	1533	158.04	7312	321.9	3.09	91.48	1.50	196.10	170.61	90.13	352.22	430.49	93.75	6.03	0.825	87.33	86.90	Conc.	0.10%	455.17	0.77	0.85	0.55	0.95					
9A	1	Node 90	Node 80	0.0	0.0	0.0	33.8	18.6	15.2	33.8	2161	116.18	9473	355.7	2.98	114.28	1.50	196.10	170.61	99.60	384.48	1268.65	92.37	5.84	0.900	86.90	85.63	Conc.	0.10%	573.71	0.67	0.90	0.55	0.97					
8A	1	Node 80		0.0	0.0	0.0	40.0	24.1	15.9	40.0	12047	499.88	21520	395.7	2.62	228.45	1.50	196.10	170.61	110.80	509.85																		
8R	1			5.9	4.4	1.5	0.0	0.0	0.0	5.9	0	0	21520	401.6	2.62	228.45	1.50	202.00	175.74	112.45	516.64																		
8C	1			13.9	10.4	3.5	0.0	0.0	0.0	13.9	0	0	21520	415.5	2.62	228.45	1.50	215.90	187.83	116.34	532.62																		
7A	1			13.5	10.1	3.4	16.5	5.2	11.3	30.0	1637	314.81	23157	445.5	2.59	242.84	1.50	229.40	199.58	124.74	567.6																		
7B	1		Node 70	0.0	0.0	0.0				9.2	3980	638.84	27137	454.7	2.52	277.05	1.50	229.40	199.58	127.32	603.94	1448.98	91.24	6.01	1.050	85.63	84.18	Conc.	0.10%	864.51	0.70	1.00	0.64	1.07					
										225.3			454.7																										
DEFAULTS																											4,781.0												
															q=AVERAGE DAILY FLOW		350		L/CAP.D																				
															I=UNIT OF PEAK EXTR.FLOW		0.280		L/Ha.s																				
															Mannings 'n'		0.013																						
															q=AVERAGE COMMERCIAL AND INSTITUTIONAL		0.58		L/Ha.s																				
DESIGN CHECKED TODAY:	DJG																																						
		7/18/2012																																					



Project 11-5681



CITY OF OTTAWA
SOUTH NEPEAN COLLECTOR (SNC)
SEWER PHASE 2 - STRANDHERD DRIVE
TO JOCKVALE ROAD

PLAN AND PROFILE
STA. 0+000 TO 0+300

Contract No. **ISD14-2033** Dwg. No. **019**
 Sheet 19 of 51

Asset No. _____
 Asset Group **ISD**

Wayne Newell, P.Eng. General Manager
 Jonathan Knoyle, P.Eng. Senior Engineer

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PROFESSIONAL ENGINEER
M.A. BISSETT
 PROVINCE OF ONTARIO

Des. **RJD** Chk'd. **ERD**
 Dwn. **NCS** Chk'd. **RJD**
 Utility Circ. No. _____ Index No. _____
 Const. Inspector _____

Scale: HORIZONTAL 1:500
 VERTICAL 1:100

NOTE: The location of utilities is approximate only, the exact location should be determined by consulting the municipal authorities and utility companies concerned. The contractor shall prove the location of utilities and shall be responsible for adequate protection from damage.

No.	Description	By	Date (dd/mm/yy)
1.	ISSUED FOR PRELIMINARY DESIGN CIRCULATION	ERD	21/12/15
2.	CHANGES TO ORIENTATION ACROSS KB SWM FACILITY	ERD	16/02/16
3.	ISSUED FOR PRELIMINARY DESIGN REPORT	ERD	02/03/16
4.	ISSUED FOR FINAL DESIGN CIRCULATION	ERD	29/04/16
5.	ISSUED FOR MOECC ECA APPLICATION	ERD	26/05/16
6.	ISSUED FOR TENDER	ERD	20/06/16
7.	ISSUED FOR CONSTRUCTION	ERD	30/08/16
8.	SEWER ALIGNMENT SHIFT ON GREENBANK	ERD	16/09/16
9.	REVISED PER MION SERVICING	ERD	08/12/16

LEGEND

EXISTING ITEMS

- WATERMAIN
- WATERMAIN VALVE
- STORM SEWER
- STORM MH
- CATCH BASIN & LEAD
- CULVERT
- STORM STRUCTURE
- SANITARY SEWER
- SANITARY MH

PROPOSED ITEMS

- SANITARY SEWER
- SANITARY MH & LID
- CULVERT
- FUTURE STRUCTURE T/G ADJUSTMENT

- NOTES:**
- CONCRETE PRESSURE PIPE SHALL BE AWWA C301 (L) CL-16. FITTING SHALL BE DESIGNED TO THE SAME CRITERIA AS THE ADJACENT PIPE.
 - CONTRACTOR TO PROVIDE PIPE CLASS CALCULATIONS, AS PER AWWA C304 (DESIGN OF PRESTRESSED CONCRETE CYLINDER PIPE), BY THE PIPE MANUFACTURER, SIGNED AND SEALED BY A PROFESSIONAL ENGINEER LICENSED IN THE PROVINCE OF ONTARIO.
 - PIPE EMBEDMENT SHALL BE AS PER CITY OF OTTAWA DETAIL S6. SAND MAY BE USED AS PIPE COVER MATERIAL ABOVE THE SPRINGLINE.
 - A CLOTH DIAPER APPROVED BY THE PIPE MANUFACTURE SHALL BE PLACED AROUND EACH EXTERIOR JOIN RECESS AND FASTENED IN PLACE WITH EITHER WIRE OR STEEL STRAPPING STITCHED INTO ITS EDGES.
 - THE JOINT SHALL BE FILLED WITH MORTAR IN ONCE CONTINUOUS OPERATION AND PATTED OR MANIPULATED TO SETTLE THE MORTAR AND EXPEL AND ENTRAPPED AIR.
 - INTERIOR JOINTS SHALL BE FILLED WITH MORTAR AFTER BACKFILLING AND FINISHED SMOOTH WITH A TROWEL. CEMENT USED SHALL MEET THE REQUIREMENTS OF TYPE HS CEMENT (HIGH-SULPHATE-RESISTANCE), OR APPROVED EQUIVALENT.
 - THE INTERIOR OF THE JOINTS SHALL BE PROTECTED FROM CORROSION WITH EPOXY AND ZINC COATING APPLIED DURING FABRICATION.
 - THE INTERIOR STRUCTURAL CONCRETE CORE SHALL BE MANUFACTURED WITH TYPE HS CEMENT (HIGH-SULPHATE-RESISTANCE), OR APPROVED EQUIVALENT.
 - SEE MANHOLE DETAIL DRAWINGS ISD14-2033-36 TO ISD14-2033-45 FOR ADDITIONAL DETAILS

MAINTENANCE HOLE DATA

MH ID	STATION	OFFSET	STRUCTURE	COVER	T/G ELEV.	LOW. INV.
1	0+010.00	1.25R	OPSD 701.013	S24/S25	95.06	86.92
2	0+060.95	1.25R	OPSD 701.012	S24/S25	94.37	86.87
3	0+118.25	1.25R	OPSD 701.012	S24/S25	94.67	86.81
4	0+194.38	0.46R	OPSD 701.013	S24/S25	93.84	86.73
5	0+226.51	1.25R	OPSD 701.012	S24/S25	92.75	86.70
6	0+269.14	1.25R	OPSD 701.012	S24/S25	92.66	86.66

SANITARY SEWER PIPE DATA

CONNECTED STRUCTURES & INVERTS	DIA (mm)	LENGTH (m)	MATERIAL
SANMH 1 = 86.92 SANMH 2 = 86.87	900	50.95	AWWA C-301 (L)
SANMH 2 = 86.87 SANMH 3 = 86.81	900	57.30	AWWA C-301 (L)
SANMH 3 = 86.81 SANMH 4 = 86.73	900	76.07	AWWA C-301 (L)
SANMH 4 = 86.73 SANMH 5 = 86.70	900	31.95	AWWA C-301 (L)
SANMH 5 = 86.70 SANMH 6 = 86.66	900	42.26	AWWA C-301 (L)
SANMH 6 = 86.66 SANMH 7 = 86.59	900	73.97	AWWA C-301 (L)

STATION	EXISTING ELEVATION	CHAINAGE	DESCRIPTION	INVERT ELEVATION
0+000	83.47	0+000	SANMH 1 (2400mm ²) T/G=95.06 INV. SE=86.92	86.92
0+050	82.75	0+050	SANMH 2 (1800mm ²) T/G=94.37 INV. SE=86.87 INV. NW=86.87 INV. NE=87.22	86.87
0+110	82.72	0+110	SANMH 3 (1800mm ²) T/G=94.67 INV. SE=86.81 INV. NW=86.81 INV. NE=87.16	86.81
0+170	82.51	0+170	SANMH 4 (2400mm ²) T/G=93.84 INV. SE=86.73 INV. NW=86.73 INV. NE=87.08	86.73
0+230	82.45	0+230	SANMH 5 (1800mm ²) T/G=92.75 INV. SE=86.70 INV. NW=86.70	86.70
0+290	82.36	0+290	SANMH 6 (1800mm ²) T/G=92.66 INV. S=86.66 INV. NW=86.66	86.66
0+300	82.29	0+300	SANMH 7 (1800mm ²) T/G=92.66 INV. NW=86.59	86.59

AS-BUILT

THESE AS-BUILT PLANS HAVE BEEN PREPARED BASED ON INFORMATION PROVIDED BY OTHERS. THE DESIGN PROFESSIONAL HAS NOT VERIFIED THE ACCURACY AND/OR THE COMPLETENESS OF THIS INFORMATION AND SHALL NOT BE RESPONSIBLE FOR ANY ERRORS OR OMISSIONS WHICH MAY BE INCORPORATED HEREIN AS A RESULT.



CITY OF OTTAWA
SOUTH NEPEAN COLLECTOR (SNC)
SEWER PHASE 2 - STRANDHERD DRIVE
TO JOCKVALE ROAD

PLAN AND PROFILE
STA. 0+300 TO 0+600

Contract No. **ISD14-2033** Dwg. No. **020**
Sheet 20 of 51

Asset No. _____
Asset Group **ISD**

Wayne Newell, P.Eng. General Manager
Jonathan Knoyle, P.Eng. Senior Engineer

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Scale: HORIZONTAL 1:500
VERTICAL 1:100

NOTE: The location of utilities is approximate only, the exact location should be determined by consulting the municipal authorities and utility companies concerned. The contractor shall prove the location of utilities and shall be responsible for adequate protection from damage.

No.	Description	By	Date (dd/mm/yyyy)
1	ISSUED FOR PRELIMINARY DESIGN CIRCULATION	FRN	21/12/15
2	CHANGES TO ORIENTATION ACROSS KB SWM FACILITY	ERD	16/02/16
3	ISSUED FOR PRELIMINARY DESIGN REPORT	ERD	02/03/16
4	ISSUED FOR FINAL DESIGN CIRCULATION	ERD	29/04/16
5	ISSUED FOR MOECC ECA APPLICATION	ERD	26/05/16
6	ISSUED FOR TENDER	ERD	20/06/16
7	ISSUED FOR CONSTRUCTION	ERD	30/08/16
8	SEWER ALIGNMENT SHIFT ON GREENBANK	ERD	16/09/16
9	REVISED PER MION SERVICING	ERD	08/12/16
10	MINTO LANDS MANHOLE UPDATE	ERD	24/04/17
11	ISSUED FOR AS-BUILT	ERD	28/09/17

LEGEND

EXISTING ITEMS
WATERMAIN
WATERMAIN VALVE
STORM SEWER
STORM MH
CATCH BASIN & LEAD
CULVERT
STORM STRUCTURE
SANITARY SEWER
SANITARY MH

PROPOSED ITEMS
SANITARY SEWER
SANITARY MH & LID
CULVERT
FUTURE STRUCTURE T/G
ADJUSTMENT

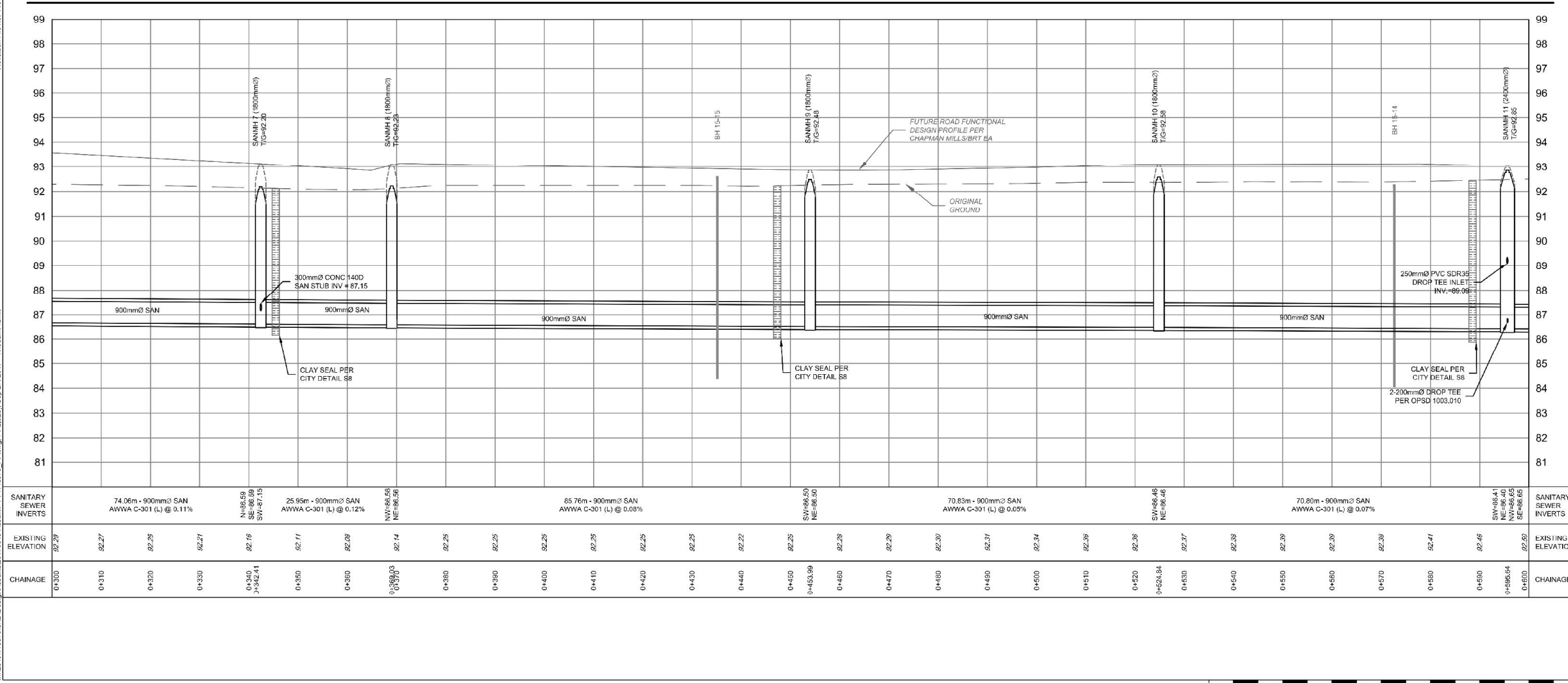
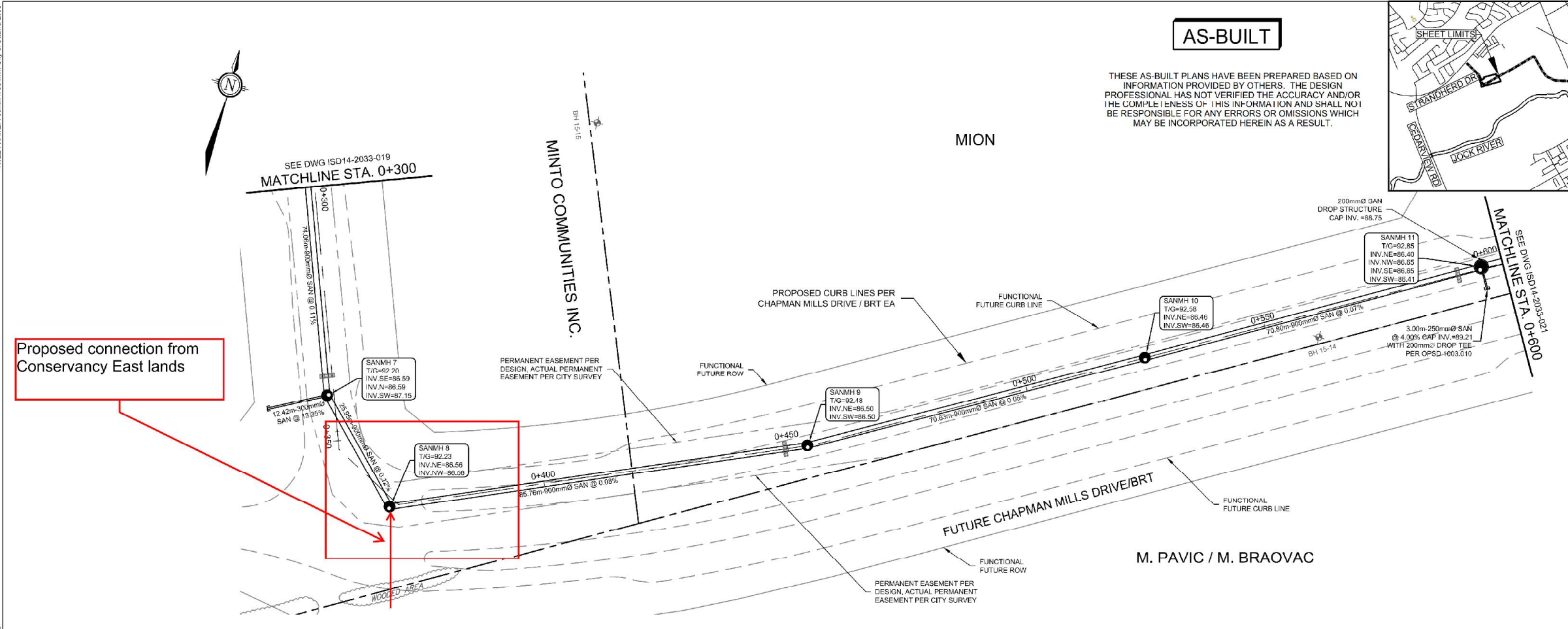
- NOTES:**
- CONCRETE PRESSURE PIPE SHALL BE AWWA C301 (L) CL-16. FITTING SHALL BE DESIGNED TO THE SAME CRITERIA AS THE ADJACENT PIPE.
 - CONTRACTOR TO PROVIDE PIPE CLASS CALCULATIONS, AS PER AWWA C304 (DESIGN OF PRESTRESSED CONCRETE CYLINDER PIPE), BY THE PIPE MANUFACTURER. SIGNED AND SEALED BY A PROFESSIONAL ENGINEER LICENSED IN THE PROVINCE OF ONTARIO.
 - PIPE EMBEDMENT SHALL BE AS PER CITY OF OTTAWA DETAIL S6. SAND MAY BE USED AS PIPE COVER MATERIAL ABOVE THE SPRINGLINE.
 - A CLOTH DIAPER APPROVED BY THE PIPE MANUFACTURER SHALL BE PLACED AROUND EACH EXTERIOR JOINT RECESS AND FASTENED IN PLACE WITH EITHER WIRE OR STEEL STRAPPING STITCHED INTO ITS EDGES.
 - THE JOINT SHALL BE FILLED WITH MORTAR IN ONCE CONTINUOUS OPERATION AND PATTED OR MANIPULATED TO SETTLE THE MORTAR AND EXPEL AND ENTRAPPED AIR.
 - INTERIOR JOINTS SHALL BE FILLED WITH MORTAR AFTER BACKFILLING AND FINISHED SMOOTH WITH A TROWEL. CEMENT USED SHALL MEET THE REQUIREMENTS OF TYPE HS CEMENT (HIGH-SULPHATE-RESISTANCE), OR APPROVED EQUIVALENT.
 - THE INTERIOR OF THE JOINTS SHALL BE PROTECTED FROM CORROSION WITH EPOXY AND ZINC COATING APPLIED DURING FABRICATION.
 - THE INTERIOR STRUCTURAL CONCRETE CORE SHALL BE MANUFACTURED WITH TYPE HS CEMENT (HIGH-SULPHATE-RESITANCE), OR APPROVED EQUIVALENT.
 - SEE MANHOLE DETAIL DRAWINGS ISD14-2033-36 TO ISD14-2033-45 FOR ADDITIONAL DETAILS

MAINTENANCE HOLE DATA

MH ID	STATION	OFFSET	STRUCTURE	COVER	T/G ELEV	LOW. INV.
7	0+342.41	1.41R	OPSD 701.012	S24/S25	92.20	86.59
8	0+389.03	1.50R	OPSD 701.012	S24/S25	92.23	86.56
9	0+453.99	0.07L	OPSD 701.012	S24/S25	92.48	86.50
10	0+524.84	0.04L	OPSD 701.012	S24/S25	92.58	86.46
11	0+595.64	0.41L	OPSD 701.013	S24/S25	92.85	86.40

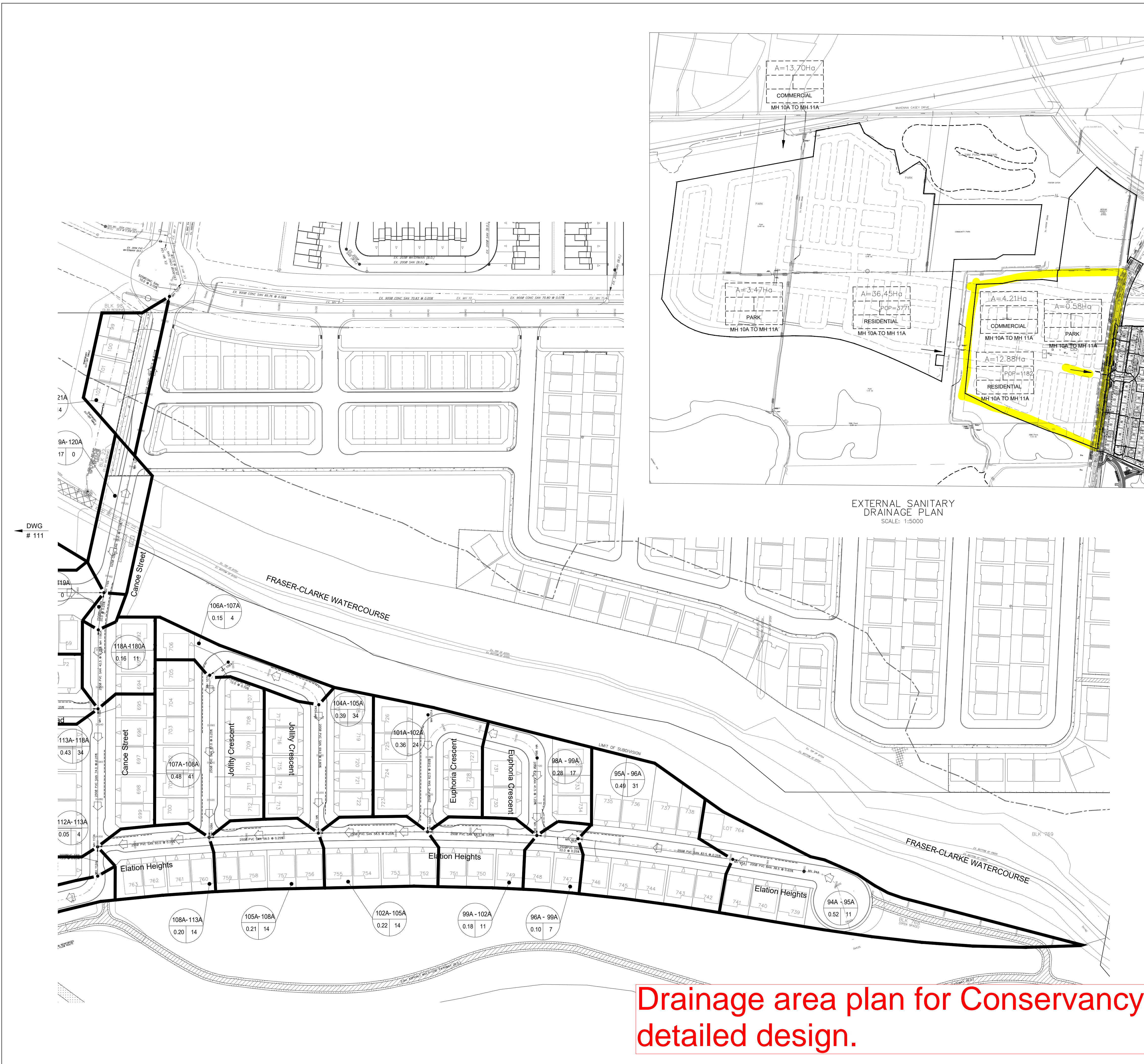
SANITARY SEWER PIPE DATA

CONNECTED STRUCTURES & INVERTS	DIA (mm)	LENGTH (m)	MATERIAL
SANMH 6 = 86.68 SANMH 7 = 86.59	900	74.06	AWWA C-301 (L)
SANMH 7 = 86.59 SANMH 8 = 86.56	900	25.95	AWWA C-301 (L)
SANMH 8 = 86.56 SANMH 9 = 86.50	900	85.76	AWWA C-301 (L)
SANMH 10 = 86.46 SANMH 9 = 86.50	900	70.83	AWWA C 301 (L)
SANMH 10 = 86.46 SANMH 11 = 86.41	900	70.80	AWWA C-301 (L)
SANMH 11 = 86.40 SANMH 12 = 86.32	900	78.15	AWWA C-301 (L)

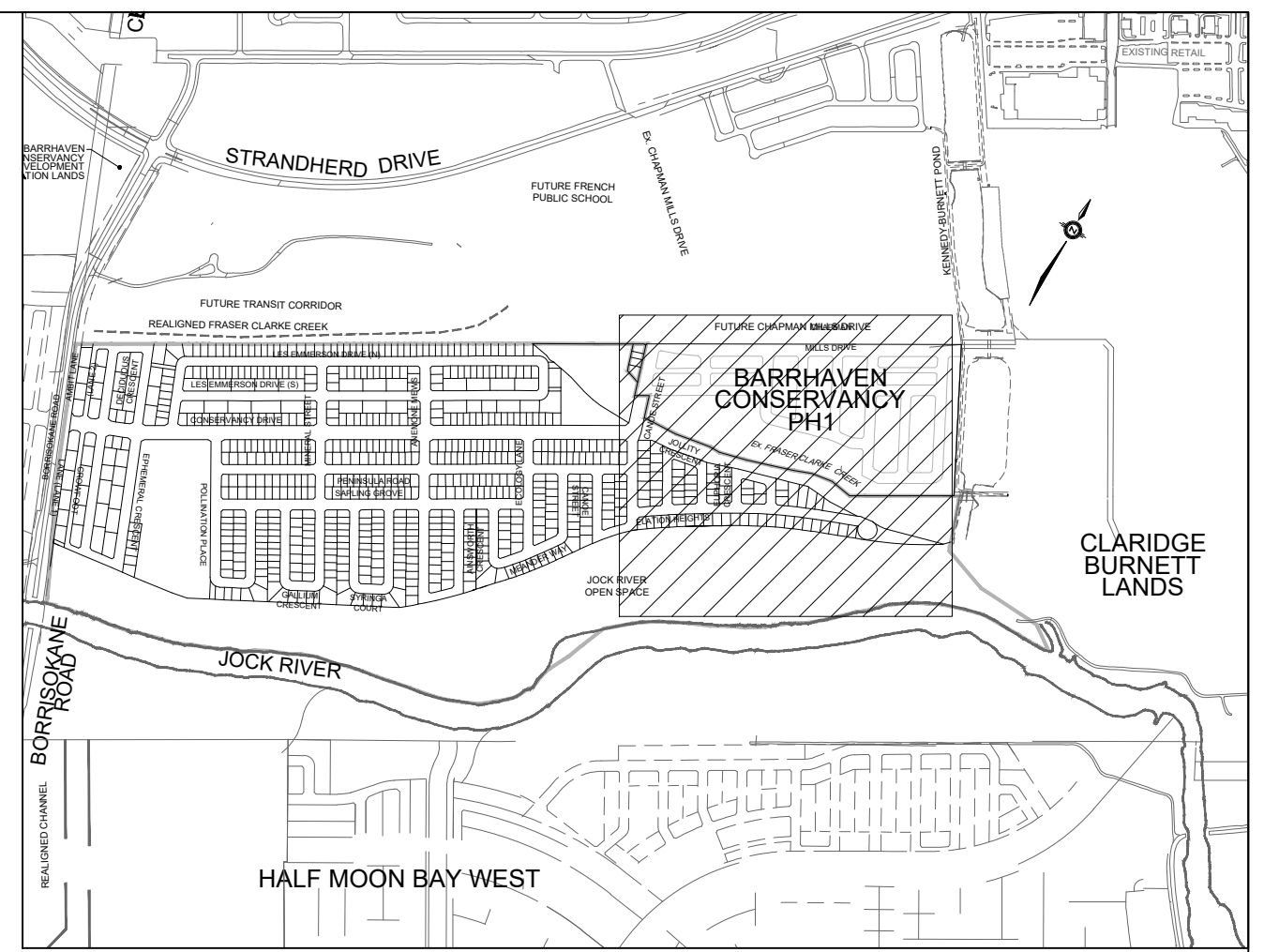


STATION	EXISTING ELEVATION	CHAINAGE	STRUCTURE	COVER	T/G ELEV	LOW. INV.
0+300	82.29	0+300	SANMH 7	1.41R	92.20	86.59
0+310	82.27	0+310	SANMH 8	1.50R	92.23	86.56
0+320	82.25	0+320	SANMH 9	0.07L	92.48	86.50
0+330	82.21	0+330	SANMH 10	0.04L	92.58	86.46
0+340	82.16	0+340	SANMH 11	0.41L	92.85	86.40
0+350	82.08	0+350				
0+360	82.05	0+360				
0+370	82.02	0+370				
0+380	82.00	0+380				
0+390	82.00	0+390				
0+400	82.00	0+400				
0+410	82.00	0+410				
0+420	82.00	0+420				
0+430	82.00	0+430				
0+440	82.00	0+440				
0+450	82.00	0+450				
0+460	82.00	0+460				
0+470	82.00	0+470				
0+480	82.00	0+480				
0+490	82.00	0+490				
0+500	82.00	0+500				
0+510	82.00	0+510				
0+520	82.00	0+520				
0+530	82.00	0+530				
0+540	82.00	0+540				
0+550	82.00	0+550				
0+560	82.00	0+560				
0+570	82.00	0+570				
0+580	82.00	0+580				
0+590	82.00	0+590				
0+600	82.00	0+600				

TITLE FRAME: 700mm x 634mm, City of Ottawa 2008
Novatech File No. 115075
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Drainage area plan for Conservancy East detailed design.



LEGEND

- SANITARY DRAINAGE BOUNDARY
- SANITARY SUB-DRAINAGE BOUNDARY
- UPSTREAM MH TO DOWNSTREAM MH 43A - 44A
- AREA IN HECTARES 0.78 61
- POPULATION 107
- UPSTREAM MH TO DOWNSTREAM MH 43A - 44A
- AREA IN OTHER PHASES IN HECTARES 0.78 61
- POPULATION 107
- EXTERNAL AREA IN HECTARES A=53.63
- EXTERNAL POPULATION POP=5739
- DENSITY (PERSONS/HECTARE) RESIDENTIAL
- EXTERNAL LAND USE RESIDENTIAL
- MAINTENANCE HOLE
- CAP
- EXISTING SANITARY MAINTENANCE HOLE

TOPOGRAPHIC INFORMATION
 TOPOGRAPHIC INFORMATION PROVIDED BY J.D. BARNES LIMITED,
 PROJECT No. 16-10-127-00, SURVEY DATED APRIL 10, 2018.

LEGAL INFORMATION
 M-PLAN PROVIDED BY J.D. BARNES, PROJECT No.
 16-10-127-00, RECEIVED ON AUGUST 2, 2022.

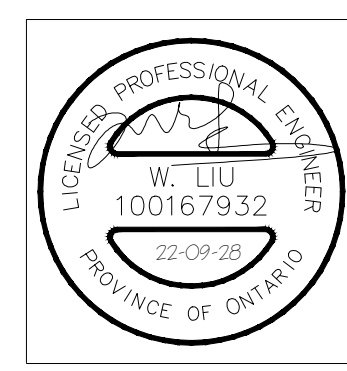
NOT FOR CONSTRUCTION

ELEVATION NOTE
 ELEVATIONS SHOWN ON THIS PLAN ARE RELATED TO GEODETIC DATUM
 AND ARE REFERRED TO THE PUBLISHED BENCH MARK No. D011964U3710
 ELEVATION = 71.724m

No.	BY	DATE	DESCRIPTION
7	W.L.	22-09-28	RETAINING WALL UPDATES
6	W.L.	22-09-27	WATERMAIN AND CUP UPDATES
5	W.L.	22-08-31	CITY COMMENTS AND TRANSPORTATION UPDATES
4	W.L.	22-08-10	REVISED STREET NAME & LOT 99 SIGHT TRIANGLE
3	W.L.	22-06-28	3rd SUBMISSION
2	W.L.	22-04-22	2nd SUBMISSION
1	W.L.	21-12-22	1st SUBMISSION

CITY OF OTTAWA

PROJECT No. 20-1180



SANITARY DRAINAGE PLAN

BARRHAVEN
 CONSERVANCY
 DEVELOPMENT
 CORPORATION

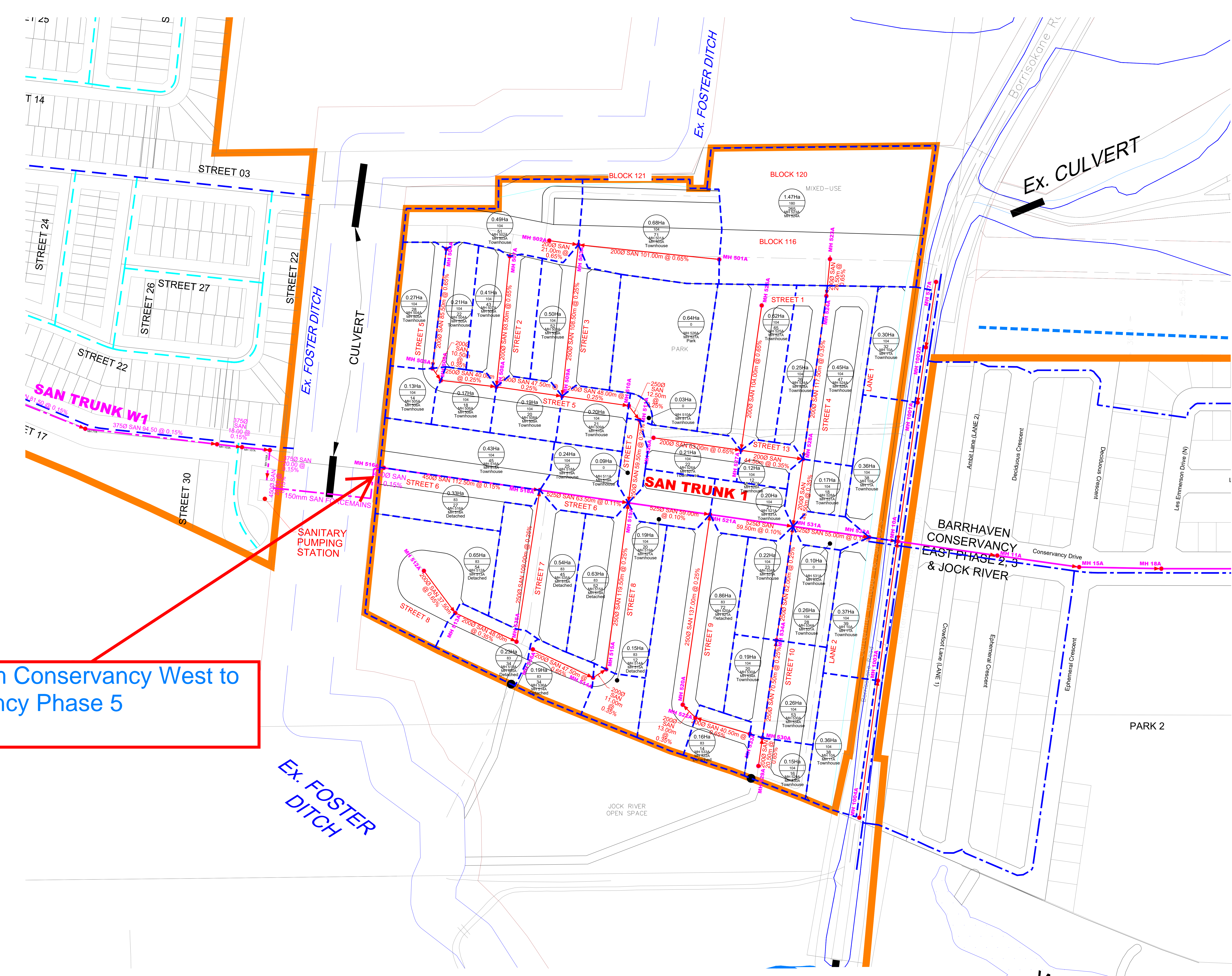
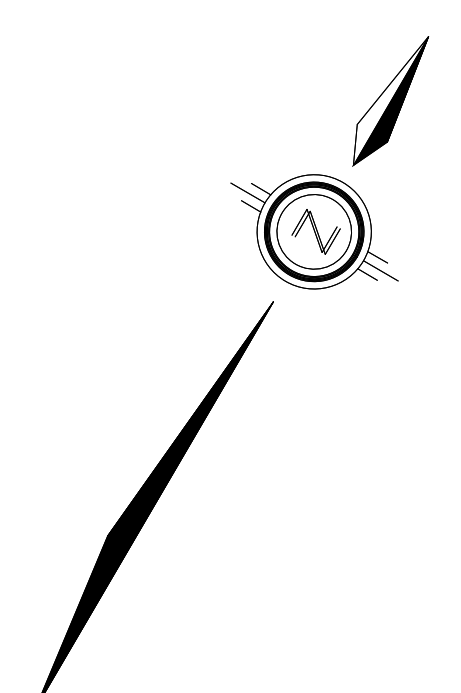
BARRHAVEN
 CONSERVANCY EAST
 PHASE 2, 3 & JOCK RIVER



120 Iber Road, Unit 103
 Stittville, ON K2S 1E9
 Tel. (613) 836-0856
 Fax. (613) 836-7183
 www.DSEL.ca

DRAWN BY: A.K./R.A./V.W.	CHECKED BY: W.L.	SHEET NO.
DESIGNED BY: W.L.	CHECKED BY: C.M.	112
SCALE: 1:1000	DATE: DECEMBER 2021	

CITY PLAN No. 18754
 CITY FILE No. D07-16-20-0021



Flows from Conservancy West to Conservancy Phase 5

Design Sheet for Conservancy Phase 5.
Updated draft plan submission in December 2022

LEGEND	
	SITE BOUNDARY
	SANITARY TRUNK SEWER
	SANITARY LOCAL SEWER
	EXTERNAL SANITARY TRUNK SEWER
	SANITARY MANHOLE
	SANITARY TRIBUTARY AREA
	AREA IN HECTARES POPULATION PER HECTARE
	POPULATION AREA TYPE

SANITARY SEWER CALCULATION SHEET

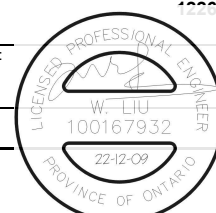


Manning's n=0.013

LOCATION			RESIDENTIAL AREA AND POPULATION						PEAK		COMM		INSTIT		PARK		C+H		INFILTRATION				PIPE					
STREET	FROM M.H.	TO M.H.	AREA (ha)	UNITS	POP.	CUMULATIVE		PEAK FACT.	PEAK FLOW (l/s)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	PEAK FLOW (l/s)	TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	DIST (m)	DIA (mm)	SLOPE (%)	CAP. (FULL) (l/s)	RATIO Q act/Q cap	VEL.		
						AREA (ha)	POP.																			(FULL) (m/s)	(ACT) (m/s)	
Centerline7 - 30																												
To STREET '16', Pipe 94A - 95A	92A	94A	0.51		43	0.51	43	3.66	0.51				0.00	0.00	0.00	0.00	0.51	0.51	0.15	0.66	71.0	200	0.65	26.44	0.02	0.84	0.35	
STREET '13'																												
Contribution From STREET '16', Pipe 94A - 95A						0.51	43					0.00	0.00	0.00	0.00	0.51	0.51											
	95A	96A	0.52		54	1.03	97	3.60	1.13				0.00	0.00	0.00	0.00	0.52	1.03	0.29	1.43	75.5	250	0.25	29.73	0.05	0.61	0.31	
To STREET '20', Pipe 97A - 101A	96A	97A	0.42		44	1.45	141	3.56	1.63				0.00	0.00	0.00	0.42	1.45	0.41	2.04	67.0	250	0.25	29.73	0.07	0.61	0.34		
STREET '19'																												
To STREET '11', Pipe 71A - 72A	70A	71A	0.38		40	0.38	40	3.67	0.48				0.00	0.00	0.00	0.38	0.38	0.11	0.58	80.0	200	0.65	26.44	0.02	0.84	0.34		
To STREET '12', Pipe 99A - 100A	70A	99A	0.30		31	0.30	31	3.68	0.37				0.00	0.00	0.00	0.30	0.30	0.09	0.46	66.0	200	0.65	26.44	0.02	0.84	0.32		
STREET '18'																												
To STREET '11', Pipe 69A - 71A	68A	69A	0.32		33	0.32	33	3.68	0.39				0.00	0.00	0.00	0.32	0.32	0.09	0.48	80.5	200	0.65	26.44	0.02	0.84	0.32		
To STREET '12', Pipe 98A - 99A	68A	98A	0.26		27	0.26	27	3.69	0.32				0.00	0.00	0.00	0.26	0.26	0.07	0.40	66.0	200	0.65	26.44	0.02	0.84	0.30		
STREET '14'																												
To STREET '11', Pipe 67A - 69A	65A	66A	0.34		35	0.34	35	3.67	0.42				0.00	0.00	0.00	0.34	0.34	0.10	0.51	67.5	200	0.65	26.44	0.02	0.84	0.33		
	66A	67A	0.34		35	0.68	70	3.63	0.82				0.00	0.00	0.00	0.34	0.68	0.19	1.02	74.0	250	0.25	29.73	0.03	0.61	0.28		
STREET '15'																												
Contribution From STREET '9', Pipe 490A - 62A						0.31	32					0.00	0.00	0.00	0.00	0.31	0.31											
Contribution From STREET '9', Pipe 570A - 62A						0.10	10					0.00	0.00	0.00	0.00	0.10	0.41											
To STREET '16', Pipe 64A - 67A	62A	63A				0.41	42	3.66	0.50				0.00	0.00	0.00	0.00	0.41	0.12	0.62	9.5	200	0.35	19.40	0.03	0.62	0.28		
	63A	64A	0.50		52	0.91	94	3.60	1.10				0.00	0.00	0.00	0.50	0.91	0.26	1.36	119.0	250	0.25	29.73	0.05	0.61	0.31		
STREET '16'																												
Contribution From Centerline7 - 30, Pipe 92A - 94A						0.00						0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	23.0	200	1.00	32.80	0.00	1.04	0.06	
To STREET '13', Pipe 95A - 96A	94A	95A				0.51	43	3.66	0.51				0.00	0.00	0.00	0.00	0.51	0.15	0.66	30.5	250	0.25	29.73	0.02	0.61	0.24		
STREET '17'																												
Contribution From STREET '9', Pipe 59A - 61A	60A	61A	0.28		29	0.28	29	3.69	0.35				0.00	0.00	0.00	0.28	0.28	0.08	0.43	58.0	200	0.65	26.44	0.02	0.84	0.30		
	61A	64A	0.13		14	0.87	90	3.60	1.05				0.00	0.00	0.35	0.81	1.09	0.35	1.44	44.5	250	0.25	29.73	0.05	0.61	0.31		

DESIGN PARAMETERS					
Park Flow =	9300	L/ha/da	0.10764	I/s/ha	
Average Daily Flow =	280	l/p/day			
Comm/Inst Flow =	28000	L/ha/da	0.3241	I/s/ha	
Industrial Flow =	35000	L/ha/da	0.40509	I/s/ha	
Max Res. Peak Factor =	4.00				
Commercial/Inst./Park Peak Factor =	1.00				
Institutional =	0.32	I/s/ha			
Industrial Peak Factor =	as per MOE Graph				
Extraneous Flow =	0.286	L/s/ha			
Minimum Velocity =	0.600	m/s			
Manning's n =	0.013	(Conc)	0.013	(Pvc)	0.013
Townhouse coeff=	2.7				
Single house coeff=	3.4				

Designed:	M.S.	PROJECT:	1226 - Barrhaven Conservancy West
Checked:	W.L./V.W.	LOCATION:	City of Ottawa
Dwg. Reference:	Sanitary Drainage Plan	File Ref:	W-110 100167932 22-12-09
		Date:	09 Dec 2022
		Sheet No	5
		of	8



SANITARY SEWER CALCULATION SHEET



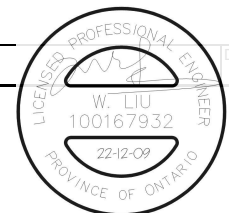
Manning's n=0.013

LOCATION			RESIDENTIAL AREA AND POPULATION						COMM		INSTIT		PARK		C+H	INFILTRATION				PIPE									
STREET	FROM M.H.	TO M.H.	AREA (ha)	UNITS	POP.	CUMULATIVE		PEAK FACT.	PEAK FLOW (l/s)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	PEAK FLOW (l/s)	TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	DIST (m)	DIA (mm)	SLOPE (%)	CAP. (FULL) (l/s)	RATIO Q act/Q cap	VEL.			
						AREA (ha)	POP.																			(FULL) (m/s)	(ACT) (m/s)		
Contribution From STREET '7', Pipe 113A - 119A						1.06	111				0.00		0.00		0.00		1.06	45.78											
Contribution From Centerline6 - 29, Pipe 118A - 119A						0.47	40				0.00		0.00		0.44		0.91	46.69											
To Centerline4 - 1004, Pipe 120A - 121A						31.46	2903	2.96	27.88		13.70		0.00	1.53	4.60	0.00	46.69	13.35	45.84		19.5	375	0.15	67.91	0.68	0.61	0.66		
Centerline4 - 1004																													
Contribution From STREET '2', Pipe 119A - 120A						31.46	2903				13.70		0.00	1.53	4.60	0.00	46.69	46.69	0.00										
→ 120A 121A						31.46	2903	2.96	27.88		13.70		0.00	1.53	4.60	0.00	46.69	13.35	45.84		28.0	375	0.15	67.91	0.68	0.61	0.66		

Projected flow of 45.84 L/s which is less than the previously projected 56.22 L/s from the Phase 5 draft plan update submission.

DESIGN PARAMETERS			
Park Flow =	9300	L/ha/da	0.10764 l/s/ha
Average Daily Flow =	280	l/p/day	
Comm/Inst Flow =	28000	L/ha/da	0.3241 l/s/ha
Industrial Flow =	35000	L/ha/da	0.40509 l/s/ha
Max Res. Peak Factor =	4.00		
Commercial/Inst./Park Peak Factor =	1.00		
Institutional =	0.32	l/s/ha	
Industrial Peak Factor =	as per MOE Graph		
Extraneous Flow =	0.286	L/s/ha	
Minimum Velocity =	0.600	m/s	
Manning's n = (Conc)	0.013	(Pvc)	0.013
Townhouse coeff=	2.7		
Single house coeff=	3.4		

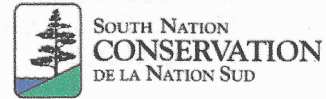
Designed:	M.S.	PROJECT:	1226 - Barrhaven Conservancy West
Checked:	W.L./V.W.	LOCATION:	City of Ottawa
Dwg. Reference:	Sanitary Drainage Plan	File Ref:	
Date:	09 Dec 2022	Sheet No of	8 / 8



APPENDIX D

STORMWATER

Conservation Partners Partenaires en conservation



May 31, 2020

City of Ottawa
110 Laurier Avenue,
Ottawa, ON K1P 1J1

Attention: Doug James

Subject: **Barrhaven Conservancy Development Corporation
Status of As-Built Grading
Related: RVCA Permit # RV5-4419 and RV5-1718)
Vacant land on the north side of the Jock River generally bounded by
Highway 416 and the Fraser Clarke Creek, City of Ottawa**

Dear Mr. James:

The RVCA has reviewed information recently submitted by David Schaeffer Engineering Ltd. including as-built grades in support of works approved by the Rideau Valley Conservation Authority under Section 28 of the Conservation Authorities Act (Permit File Number: RV5-4419 and RV5-1718). The RVCA offers the following comments related to future development proposed for the area within the scope of approved the permits.

The subject lands as identified as part of Lots 11, 12, 13, 14, 15 former geographic Township of Nepean, Concessions 3 & 4, now in the City of Ottawa have been addressed through the general placement of fill and the formal construction of a berm around the perimeter of four blocks within the subject lands. The site specific elevations of the berm have been reviewed by the RVCA and are generally accepted as being appropriate as removing these lands from the floodplain in accordance with the aforementioned approved permits.

The detailed grading plans submitted by David Schaeffer Engineering Ltd. titled "As Constructed plan of Berms and Cut Areas – Barrhaven Conservancy", dated May 27, 2020, prepared by Adam Fobert, P.Eng. of DSEL, DSEL File Number 16891 using the following resources:

- Orthoimagery Survey, dated April 20, 2020, acquired and processed by First Base Solutions a division of JD Barnes Ltd and certified by Chris Fox, O.L.S., A.L.S., P. Eng. of JD Barnes Ltd, file reference number 2037OTTA0001; ·
- Topographic Detail of Part of Lot 13, 14, & 15 Concession 3&4, dated May 6, 2020, certified by Chris Fox, O.L.S., A.L.S., P. Eng. of JD Barnes Ltd, file reference number 16-10-127-00; ·

- Contractor as-built collected by the Tomlinson Group of Companies of Phase 1 dated May 15, 2020, reviewed by Jeremy Chouindard, EIT and certified by Stephen Pichette, P.Eng. of DSEL

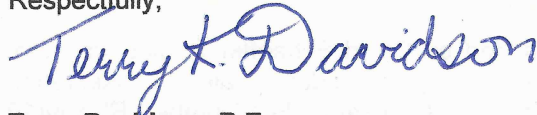
The above information indicates that land within the berm have generally been raised to exceed the flood elevation cross sections throughout the project area. However, it is noted that as this is considered an active construction site the presence of lower areas to manage construction, on-site erosion and sediment control show lower elevations. These areas will be addressed through the construction process, as sufficient material is presently stockpiled for this purpose to ensure. For the purposes of the floodplain, these areas are considered removed by virtue of the berm.

Conclusion:

The grade modifications, including construction of the berm and filling behind the berm, as documented in the above noted "as constructed" plans, have been completed in accordance with the plans approved by the RVCA under permits RV5-4419 and RV5-1718.

Please feel free to contact our office with any questions or comments you may have.

Respectfully,



Terry Davidson, P.Eng
Director of Engineering and Regulations
Rideau Valley Conservation Authority
613-692-3571 x1107
terry.davidson@rvca.ca

attach: Technical memorandum by Evelyn Liu, M.Asc., P.Eng. Water Resources
 Engineer, RVCA dated May 29, 2020

STORM SEWER CALCULATION SHEET (RATIONAL METHOD)



Local Roads Return Frequency = 2 years
 Collector Roads Return Frequency = 5 years
 Arterial Roads Return Frequency = 10 years

Manning 0.013

LOCATION			AREA (Ha)																FLOW					SEWER DATA										
			2 YEAR				5 YEAR				10 YEAR				100 YEAR				Time of Conc.	Intensity 2 Year	Intensity 5 Year	Intensity 10 Year	Intensity 100 Year	Peak Flow Q (l/s)	DIA. (mm) (actual)	DIA. (mm) (nominal)	TYPE	SLOPE (%)	LENGTH (m)	CAPACITY (l/s)	VELOCITY (m/s)	TIME OF LOW (min)	RATIO Q/Q full	
Location	From Node	To Node	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	(min)	(mm/h)	(mm/h)	(mm/h)	(mm/h)	Q (l/s)	(actual)	(nominal)	(%)	(m)	(l/s)	(m/s)	LOW (min)	Q/Q full		
Contribution From STREET '17', Pipe 72 - 76					13.48					0.49					0.00			0.00	20.16															
Contribution From STREET '1', Pipe 74 - 76					0.00					1.88					0.00			0.00	12.60															
Contribution From STREET '1', Pipe 75 - 76					0.00					0.17					0.00			0.00	10.48															
	76	81			0.00	13.48	0.12	0.67	0.22	2.76				0.00	0.00		0.00	0.00	20.16	51.77	69.90	81.80	119.34	891	1200	1200	CONC	0.11	60.0	1293.0625	1.1433	0.8746	0.689	
To STREET '8', Pipe 81 - 82					13.48					2.76					0.00			0.00	21.04															
STREET '29'																																		
Contribution From STREET '2', Pipe 106 - 108					8.87					2.78					0.00			0.00	19.37															
Contribution From STREET '2', Pipe 107 - 108					0.00					0.06					0.00			0.00	10.26															
	108	109	0.16	0.67	0.30	9.17			0.00	2.84			0.00	0.00			0.00	0.00	19.37	53.07	71.67	83.88	122.40	725	1050	1050	CONC	0.11	50.5	905.6791	1.0459	0.8047	0.801	
	109	110	0.01	0.67	0.02	9.19	0.44	0.40	0.49	3.33			0.00	0.00			0.00	0.00	20.17	51.76	69.88	81.77	119.31	708	1050	1050	CONC	0.11	12.0	905.6791	1.0459	0.1912	0.782	
	110	121	0.08	0.67	0.15	9.34			0.00	3.33			0.00	0.00			0.00	0.00	20.36	51.46	69.47	81.29	118.60	712	1050	1050	CONC	0.11	59.0	905.6791	1.0459	0.9401	0.786	
Contribution From STREET '2', Pipe 114 - 120					1.33					0.53					0.00			0.00	14.73															
Contribution From STREET '7', Pipe 118 - 120					1.48					0.60					0.00			0.00	13.95															
Contribution From STREET '2', Pipe 119 - 120					0.00					0.22					0.00			0.00	10.29															
	120	121	0.28	0.67	0.52	3.34			0.00	1.36			0.00	0.00			0.00	0.00	14.73	62.41	84.43	98.88	144.41	323	825	825	CONC	0.11	73.5	476.0801	0.8906	1.3755	0.678	
	121	OGS W1	0.03	0.67	0.06	12.73			0.00	4.68			0.00	0.00			0.00	0.00	21.30	50.03	67.52	79.00	115.24	953	1200	1200	CONC	0.11	5.5	1293.0625	1.1433	0.0802	0.737	

Definitions:
 Q = 2.78 AIR, where
 Q = Peak Flow in Litres per second (L/s)
 A = Areas in hectares (ha)
 I = Rainfall Intensity (mm/h)
 R = Runoff Coefficient

Notes:
 1) Ottawa Rainfall-Intensity Curve
 2) Min. Velocity = 0.80 m/s

Designed: M.S.	PROJECT: 1226 - Barrhaven Conservancy West
Checked: W.L./V.W.	LOCATION: City of Ottawa
Dwg. Reference:	File Ref: Date: 09 Dec 2022
	Sheet No. SHEET 7 OF 7



**CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION
BASED ON THE RATIONAL RAINFALL METHOD
BASED ON A FINE PARTICLE SIZE DISTRIBUTION**



Project Name: Conservancy West

Engineer: DSEL

Location: Ottawa, ON

Contact: K. Murphy

OGS #: W1

Report Date: 7-Dec-22

Area 8.92 ha
Weighted C 0.70
CDS Model 5640 (OFFLINE)

Rainfall Station # 215
Particle Size Distribution FINE
CDS Treatment Capacity 255 l/s

<u>Rainfall Intensity¹</u> <u>(mm/hr)</u>	<u>Percent Rainfall Volume¹</u>	<u>Cumulative Rainfall Volume</u>	<u>Total Flowrate (l/s)</u>	<u>Treated Flowrate (l/s)</u>	<u>Operating Rate (%)</u>	<u>Removal Efficiency (%)</u>	<u>Incremental Removal (%)</u>
1.0	10.6%	19.8%	17.4	17.4	6.8	96.9	10.3
1.5	9.9%	29.7%	26.0	26.0	10.2	95.9	9.5
2.0	8.4%	38.1%	34.7	34.7	13.6	95.0	8.0
2.5	7.7%	45.8%	43.4	43.4	17.0	94.0	7.2
3.0	5.9%	51.7%	52.1	52.1	20.4	93.0	5.5
3.5	4.4%	56.1%	60.8	60.8	23.8	92.0	4.0
4.0	4.7%	60.7%	69.4	69.4	27.2	91.0	4.2
4.5	3.3%	64.0%	78.1	78.1	30.6	90.1	3.0
5.0	3.0%	67.1%	86.8	86.8	34.1	89.1	2.7
6.0	5.4%	72.4%	104.1	104.1	40.9	87.1	4.7
7.0	4.4%	76.8%	121.5	121.5	47.7	85.2	3.7
8.0	3.5%	80.3%	138.9	138.9	54.5	83.2	2.9
9.0	2.8%	83.2%	156.2	156.2	61.3	81.3	2.3
10.0	2.2%	85.3%	173.6	173.6	68.1	79.3	1.7
15.0	7.0%	92.3%	260.4	254.9	100.0	68.7	4.8
20.0	4.5%	96.9%	347.2	254.9	100.0	51.5	2.3
25.0	1.4%	98.3%	434.0	254.9	100.0	41.2	0.6
30.0	0.7%	99.0%	520.7	254.9	100.0	34.4	0.2
35.0	0.5%	99.5%	607.5	254.9	100.0	29.4	0.1
40.0	0.5%	100.0%	694.3	254.9	100.0	25.8	0.1

87.0

Removal Efficiency Adjustment² = 6.5%

Predicted Net Annual Load Removal Efficiency = 80.5%

Predicted Annual Rainfall Treated = 97.1%

1 - Based on 42 years of hourly rainfall data from Canadian Station 6105976, Ottawa ON

2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.

3 - CDS Efficiency based on testing conducted at the University of Central Florida

4 - CDS design flowrate and scaling based on standard manufacturer model & product specifications



**CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION
BASED ON THE RATIONAL RAINFALL METHOD
BASED ON A FINE PARTICLE SIZE DISTRIBUTION**



Project Name: Conservancy West

Engineer: DSEL

Location: Ottawa, ON

Contact: K. Murphy

OGS #: W2

Report Date: 7-Dec-22

Area 10.75 ha
Weighted C 0.69
CDS Model 5653 (OFFLINE)

Rainfall Station # 215
Particle Size Distribution FINE
CDS Treatment Capacity 396 l/s

<u>Rainfall Intensity¹</u> <u>(mm/hr)</u>	<u>Percent Rainfall Volume¹</u>	<u>Cumulative Rainfall Volume</u>	<u>Total Flowrate (l/s)</u>	<u>Treated Flowrate (l/s)</u>	<u>Operating Rate (%)</u>	<u>Removal Efficiency (%)</u>	<u>Incremental Removal (%)</u>
1.0	10.6%	19.8%	20.6	20.6	5.2	97.4	10.3
1.5	9.9%	29.7%	30.9	30.9	7.8	96.6	9.6
2.0	8.4%	38.1%	41.2	41.2	10.4	95.9	8.0
2.5	7.7%	45.8%	51.6	51.6	13.0	95.1	7.3
3.0	5.9%	51.7%	61.9	61.9	15.6	94.4	5.6
3.5	4.4%	56.1%	72.2	72.2	18.2	93.6	4.1
4.0	4.7%	60.7%	82.5	82.5	20.8	92.9	4.3
4.5	3.3%	64.0%	92.8	92.8	23.4	92.1	3.1
5.0	3.0%	67.1%	103.1	103.1	26.0	91.4	2.8
6.0	5.4%	72.4%	123.7	123.7	31.2	89.9	4.8
7.0	4.4%	76.8%	144.3	144.3	36.4	88.4	3.8
8.0	3.5%	80.3%	165.0	165.0	41.6	86.9	3.1
9.0	2.8%	83.2%	185.6	185.6	46.8	85.4	2.4
10.0	2.2%	85.3%	206.2	206.2	52.0	83.9	1.8
15.0	7.0%	92.3%	309.3	309.3	78.0	76.5	5.3
20.0	4.5%	96.9%	412.4	396.5	100.0	67.5	3.1
25.0	1.4%	98.3%	515.5	396.5	100.0	54.0	0.8
30.0	0.7%	99.0%	618.6	396.5	100.0	45.0	0.3
35.0	0.5%	99.5%	721.7	396.5	100.0	38.6	0.2
40.0	0.5%	100.0%	824.8	396.5	100.0	33.7	0.2

90.0

Removal Efficiency Adjustment² = 6.5%

Predicted Net Annual Load Removal Efficiency = 83.5%

Predicted Annual Rainfall Treated = 98.8%

1 - Based on 42 years of hourly rainfall data from Canadian Station 6105976, Ottawa ON

2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.

3 - CDS Efficiency based on testing conducted at the University of Central Florida

4 - CDS design flowrate and scaling based on standard manufacturer model & product specifications



**CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION
BASED ON THE RATIONAL RAINFALL METHOD
BASED ON A FINE PARTICLE SIZE DISTRIBUTION**



Project Name: Conservancy West

Engineer: DSEL

Location: Ottawa, ON

Contact: K. Murphy

OGS #: W3

Report Date: 7-Dec-22

Area 6.30 ha
Weighted C 0.64
CDS Model 4040 (OFFLINE)

Rainfall Station # 215
Particle Size Distribution FINE
CDS Treatment Capacity 170 l/s

<u>Rainfall Intensity¹</u> <u>(mm/hr)</u>	<u>Percent Rainfall Volume¹</u>	<u>Cumulative Rainfall Volume</u>	<u>Total Flowrate (l/s)</u>	<u>Treated Flowrate (l/s)</u>	<u>Operating Rate (%)</u>	<u>Removal Efficiency (%)</u>	<u>Incremental Removal (%)</u>
1.0	10.6%	19.8%	11.2	11.2	6.6	97.0	10.3
1.5	9.9%	29.7%	16.8	16.8	9.9	96.0	9.5
2.0	8.4%	38.1%	22.4	22.4	13.2	95.1	8.0
2.5	7.7%	45.8%	28.0	28.0	16.5	94.1	7.2
3.0	5.9%	51.7%	33.6	33.6	19.8	93.2	5.5
3.5	4.4%	56.1%	39.2	39.2	23.1	92.2	4.0
4.0	4.7%	60.7%	44.8	44.8	26.4	91.3	4.3
4.5	3.3%	64.0%	50.4	50.4	29.7	90.3	3.0
5.0	3.0%	67.1%	56.0	56.0	33.0	89.4	2.7
6.0	5.4%	72.4%	67.3	67.3	39.6	87.5	4.7
7.0	4.4%	76.8%	78.5	78.5	46.2	85.6	3.7
8.0	3.5%	80.3%	89.7	89.7	52.8	83.7	3.0
9.0	2.8%	83.2%	100.9	100.9	59.4	81.8	2.3
10.0	2.2%	85.3%	112.1	112.1	66.0	79.9	1.7
15.0	7.0%	92.3%	168.1	168.1	98.9	70.5	4.9
20.0	4.5%	96.9%	224.2	169.9	100.0	53.2	2.4
25.0	1.4%	98.3%	280.2	169.9	100.0	42.6	0.6
30.0	0.7%	99.0%	336.3	169.9	100.0	35.5	0.2
35.0	0.5%	99.5%	392.3	169.9	100.0	30.4	0.1
40.0	0.5%	100.0%	448.4	169.9	100.0	26.6	0.1

87.4

Removal Efficiency Adjustment² = 6.5%

Predicted Net Annual Load Removal Efficiency = 80.9%

Predicted Annual Rainfall Treated = 97.4%

1 - Based on 42 years of hourly rainfall data from Canadian Station 6105976, Ottawa ON

2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.

3 - CDS Efficiency based on testing conducted at the University of Central Florida

4 - CDS design flowrate and scaling based on standard manufacturer model & product specifications



**CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION
BASED ON THE RATIONAL RAINFALL METHOD
BASED ON A FINE PARTICLE SIZE DISTRIBUTION**



Project Name: Conservancy West

Engineer: DSEL

Location: Ottawa, ON

Contact: K. Murphy

OGS #: W4

Report Date: 7-Dec-22

Area 8.18 ha
Weighted C 0.67
CDS Model 5640 (OFFLINE)

Rainfall Station # 215
Particle Size Distribution FINE
CDS Treatment Capacity 255 l/s

<u>Rainfall Intensity¹</u> <u>(mm/hr)</u>	<u>Percent Rainfall Volume¹</u>	<u>Cumulative Rainfall Volume</u>	<u>Total Flowrate (l/s)</u>	<u>Treated Flowrate (l/s)</u>	<u>Operating Rate (%)</u>	<u>Removal Efficiency (%)</u>	<u>Incremental Removal (%)</u>
1.0	10.6%	19.8%	15.2	15.2	6.0	97.1	10.3
1.5	9.9%	29.7%	22.9	22.9	9.0	96.3	9.5
2.0	8.4%	38.1%	30.5	30.5	12.0	95.4	8.0
2.5	7.7%	45.8%	38.1	38.1	14.9	94.6	7.3
3.0	5.9%	51.7%	45.7	45.7	17.9	93.7	5.6
3.5	4.4%	56.1%	53.3	53.3	20.9	92.9	4.0
4.0	4.7%	60.7%	60.9	60.9	23.9	92.0	4.3
4.5	3.3%	64.0%	68.6	68.6	26.9	91.1	3.0
5.0	3.0%	67.1%	76.2	76.2	29.9	90.3	2.7
6.0	5.4%	72.4%	91.4	91.4	35.9	88.6	4.8
7.0	4.4%	76.8%	106.7	106.7	41.8	86.9	3.8
8.0	3.5%	80.3%	121.9	121.9	47.8	85.1	3.0
9.0	2.8%	83.2%	137.1	137.1	53.8	83.4	2.4
10.0	2.2%	85.3%	152.4	152.4	59.8	81.7	1.8
15.0	7.0%	92.3%	228.5	228.5	89.7	73.2	5.1
20.0	4.5%	96.9%	304.7	254.9	100.0	58.7	2.7
25.0	1.4%	98.3%	380.9	254.9	100.0	47.0	0.7
30.0	0.7%	99.0%	457.1	254.9	100.0	39.1	0.3
35.0	0.5%	99.5%	533.3	254.9	100.0	33.5	0.2
40.0	0.5%	100.0%	609.4	254.9	100.0	29.4	0.2

88.5

Removal Efficiency Adjustment² = 6.5%

Predicted Net Annual Load Removal Efficiency = 82.0%

Predicted Annual Rainfall Treated = 97.9%

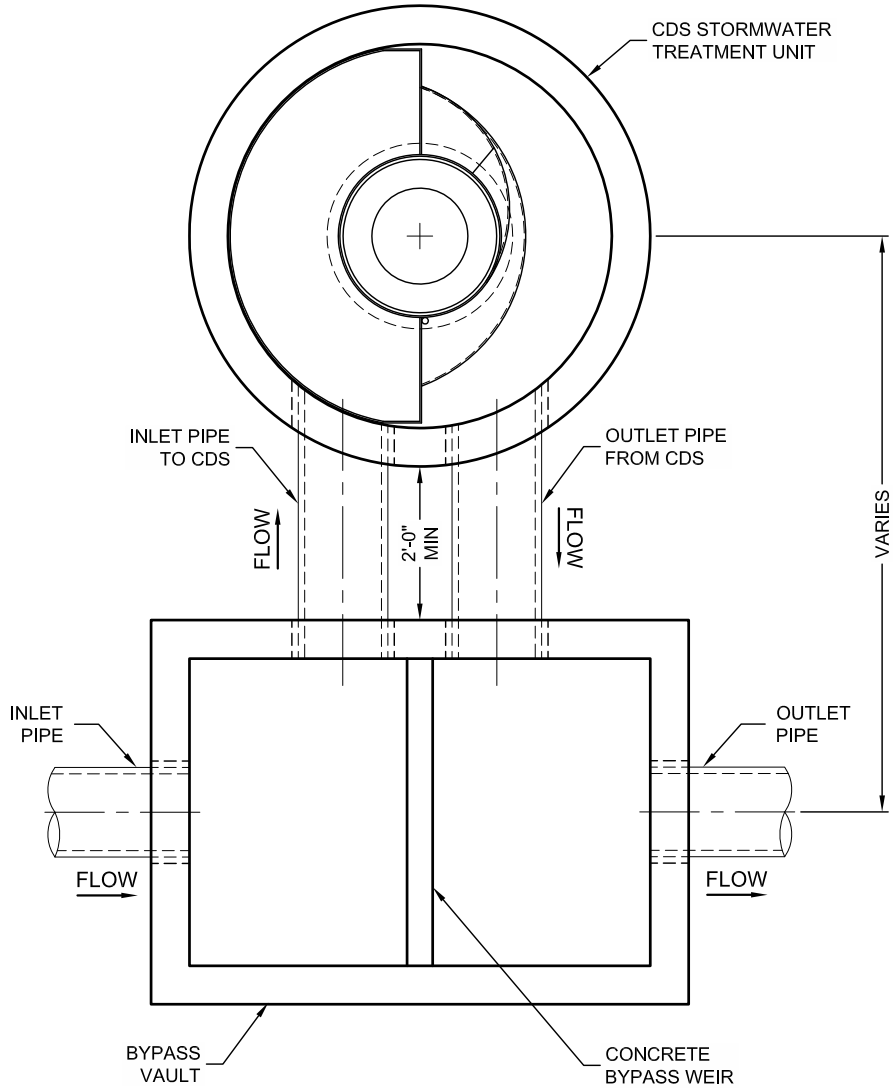
1 - Based on 42 years of hourly rainfall data from Canadian Station 6105976, Ottawa ON

2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.

3 - CDS Efficiency based on testing conducted at the University of Central Florida

4 - CDS design flowrate and scaling based on standard manufacturer model & product specifications

I:\STORMWATER\COM\WOPS\22 CDS\40 STANDARD DRAWINGS\OFFLINE LAYOUTS DWG\OFFLINE CDS-C LAYOUT BYPASS VAULT STRUCTURED.WG 3/12/2013 3:35 PM



THIS PRODUCT MAY BE PROTECTED BY ONE OR MORE OF THE FOLLOWING U.S. PATENTS: 5,788,848; 6,641,720; 6,511,595; 6,581,783; RELATED FOREIGN PATENTS, OR OTHER PATENTS PENDING.

CONTECH
ENGINEERED SOLUTIONS LLC

www.ContechES.com

9025 Centre Pointe Dr., Suite 400, West Chester, OH 45069

800-338-1122 513-645-7000 513-645-7993 FAX

CDS STORMWATER TREATMENT SYSTEM
TYPICAL OFFLINE LAYOUT
WITH BYPASS VAULT STRUCTURE

DATE:03/12/13

SCALE: NONE

PROJECT No.: N/A

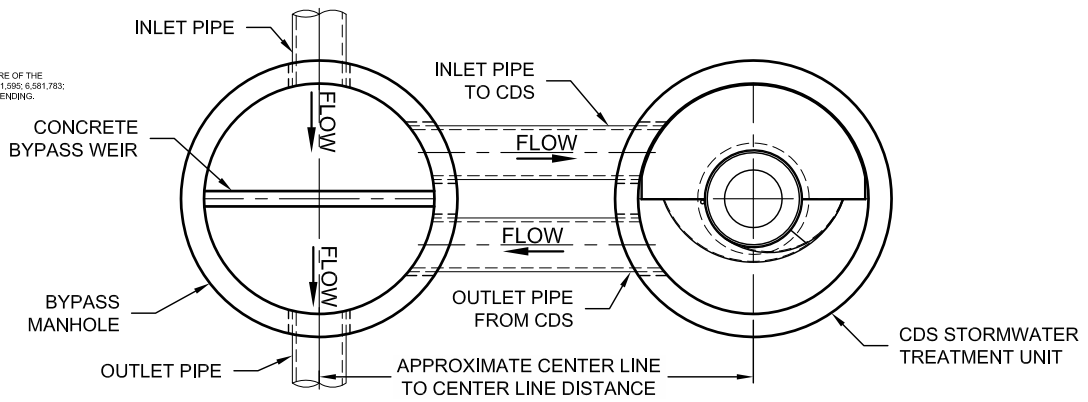
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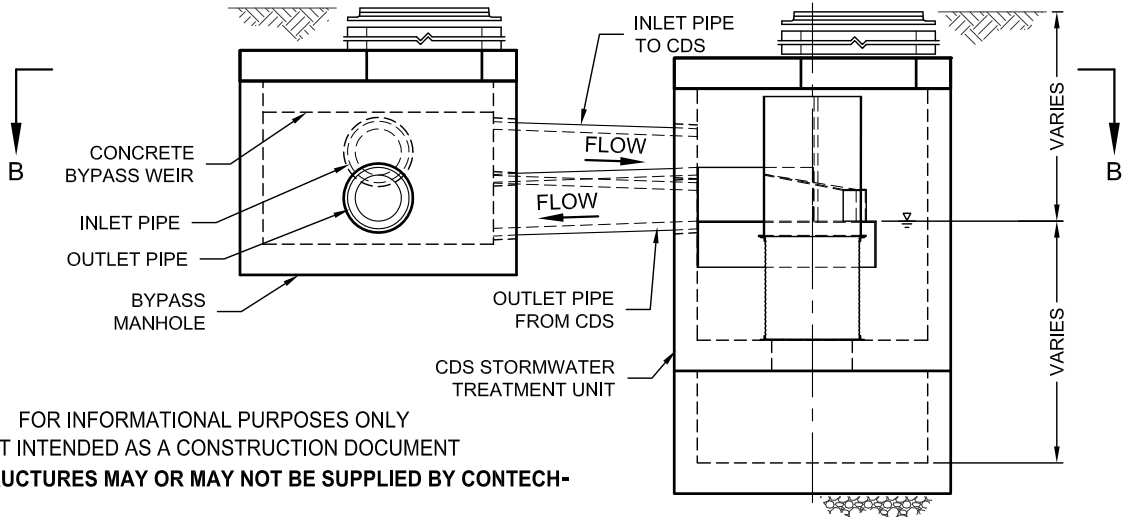


THIS PRODUCT MAY BE PROTECTED BY ONE OR MORE OF THE FOLLOWING U.S. PATENTS: 5,788,848; 6,641,720; 6,511,995; 6,581,783; RELATED FOREIGN PATENTS, OR OTHER PATENTS PENDING.



PLAN VIEW B-B

N.T.S.



ELEVATION VIEW

N.T.S.

FOR INFORMATIONAL PURPOSES ONLY
NOT INTENDED AS A CONSTRUCTION DOCUMENT

- BYPASS STRUCTURES MAY OR MAY NOT BE SUPPLIED BY CONTECH-

CDS CONCENTRIC OFFLINE SPECIFICATIONS

CDS MODEL	CDS INSIDE DIAMETER (ft/mm)	RECOMMENDED PIPE SIZE (in/mm)	TYPICAL BYPASS MANHOLE INSIDE DIAMETER (ft/mm)	APPROXIMATE CENTER LINE TO CENTER LINE DISTANCE (ft/mm)
2015-4-C	4/1219	10/250	4/1219	9/2743
2015-5-C	5/1524	10/250	5/1524	9.5/2896
2020-5-C	5/1524	12/300	5/1524	10/3048
2025-5-C	5/1524	12/300	5/1524	10/3048
3020-6-C	6/1829	15/375	6/1829	11/3353
3025-6-C	6/1829	15/375	6/1829	11/3353
3030-6-C	6/1829	18/450	6/1829	11/3353
3035-6-C	6/1829	18/450	6/1829	11/3353
4030-8-C	8/2438	24/600	8/2438	13/3962
4040-8-C	8/2438	24/600	8/2438	13/3962
4045-8-C	8/2438	24/600	8/2438	13/3962
5640-10-C	10/3048	30/750	10/3048	15/4572
5653-10-C	10/3048	30/750	10/3048	15/4572
5668-10-C	10/3048	30/750	10/3048	15/4572
5678-10-C	10/3048	30/750	10/3048	15/4572

NOTE: BYPASS AND JUNCTION MANHOLE DIAMETERS ARE ASSUMED BASED ON THE TREATMENT CAPACITY OF THE CDS SYSTEM. THESE DIAMETERS MAY CHANGE DEPENDING ON SPECIFIC SITE CONDITIONS. CONTACT YOUR CONTECH ENGINEERED SOLUTIONS DESIGN ENGINEER.

C:\USERS\BLANKENSHIP\DESKTOP\TEMP1 - ECHELON\OFFLINE_CDS-C LAYOUT BYPASS MANHOLE STRUCTURE-C.DWG 3/4/2014 1:47 PM



www.ContechES.com

200 Enterprise Drive, Scarborough, ME 04074

877-907-8676 207-885-9830 207-885-9825 FAX

**CDS STORMWATER TREATMENT SYSTEM
TYPICAL OFFLINE LAYOUT
WITH BYPASS MANHOLE STRUCTURE**

DATE: 3/4/14

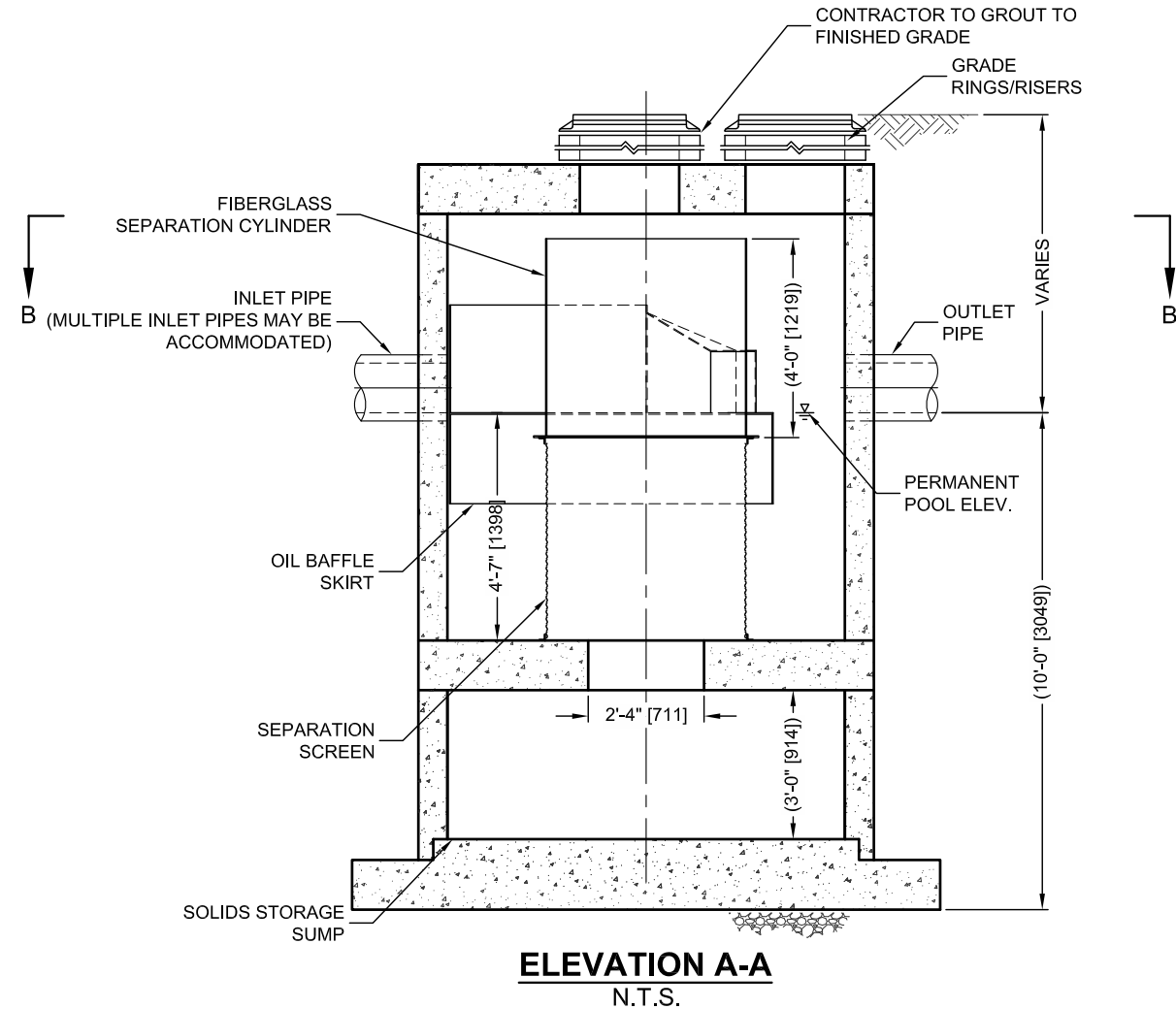
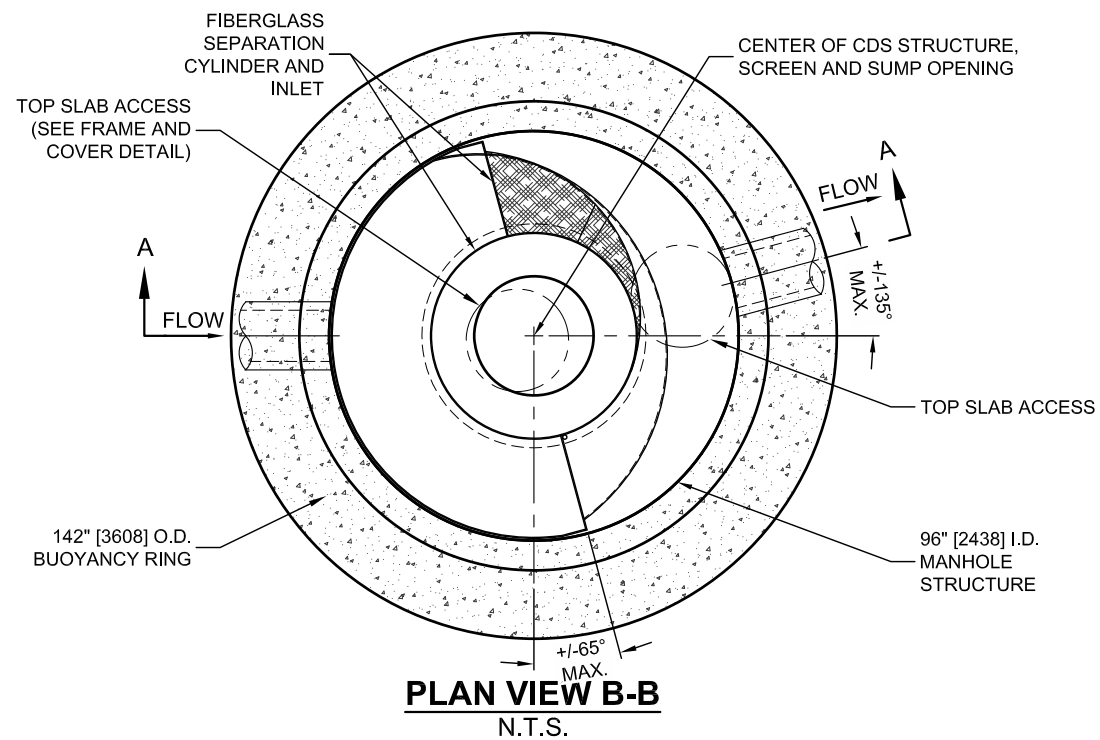
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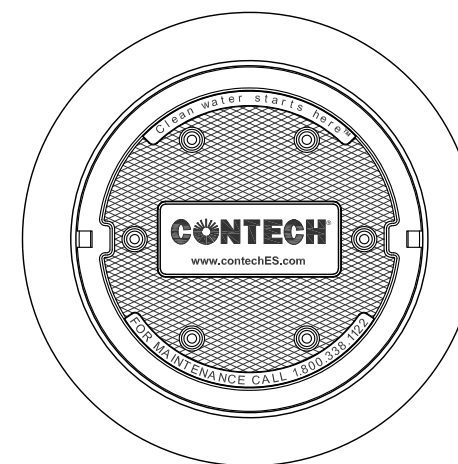
DRAWN: DWB

CHECKED:

Z:\4.0 MANUFACTURERS\CONTECH PRODUCT INFO\TREATMENT\CDS\DRAWINGS ECHELOMIN LINE-PDF\2022 - PMSU UPDATED CONTECH DRAWINGS - HUDA\8\CDS4040-8-C-DTL.DWG 6/2/2022 12:44 PM



CDS PMSU4040-8-C DESIGN NOTES	
THE STANDARD CDS PMSU4040-8-C CONFIGURATION IS SHOWN. ALTERNATE CONFIGURATIONS ARE AVAILABLE AND ARE LISTED BELOW. SOME CONFIGURATIONS MAY BE COMBINED TO SUIT SITE REQUIREMENTS.	
CONFIGURATION DESCRIPTION	
GRATED INLET ONLY (NO INLET PIPE)	
GRATED INLET WITH INLET PIPE OR PIPES	
CURB INLET ONLY (NO INLET PIPE)	
CURB INLET WITH INLET PIPE OR PIPES	
SEPARATE OIL BAFFLE (SINGLE INLET PIPE REQUIRED FOR THIS CONFIGURATION)	
SEDIMENT WEIR FOR NJDEP / NJCAT CONFORMING UNITS	



FRAME AND COVER
(DIAMETER VARIES)
N.T.S.

SITE SPECIFIC DATA REQUIREMENTS			
STRUCTURE ID			
WATER QUALITY FLOW RATE (CFS OR L/s)			*
PEAK FLOW RATE (CFS OR L/s)			*
RETURN PERIOD OF PEAK FLOW (YRS)			*
SCREEN APERTURE (2400 OR 4700)			*
PIPE DATA:	I.E.	MATERIAL	DIAMETER
INLET PIPE 1	*	*	*
INLET PIPE 2	*	*	*
OUTLET PIPE	*	*	*
RIM ELEVATION			
ANTI-FLOTATION BALLAST		WIDTH	HEIGHT
		*	*
NOTES/SPECIAL REQUIREMENTS:			
* PER ENGINEER OF RECORD			

GENERAL NOTES

1. CONTECH TO PROVIDE ALL MATERIALS UNLESS NOTED OTHERWISE.
2. DIMENSIONS MARKED WITH () ARE REFERENCE DIMENSIONS. ACTUAL DIMENSIONS MAY VARY.
3. FOR FABRICATION DRAWINGS WITH DETAILED STRUCTURE DIMENSIONS AND WEIGHTS, PLEASE CONTACT YOUR CONTECH ENGINEERED SOLUTIONS LLC REPRESENTATIVE. www.contechES.com
4. CDS WATER QUALITY STRUCTURE SHALL BE IN ACCORDANCE WITH ALL DESIGN DATA AND INFORMATION CONTAINED IN THIS DRAWING.
5. STRUCTURE SHALL MEET AASHTO HS20 AND CASTINGS SHALL MEET HS20 (AASHTO M 306) LOAD RATING, ASSUMING GROUNDWATER ELEVATION AT, OR BELOW, THE OUTLET PIPE INVERT ELEVATION. ENGINEER OF RECORD TO CONFIRM ACTUAL GROUNDWATER ELEVATION.
6. PVC HYDRAULIC SHEAR PLATE IS PLACED ON SHELF AT BOTTOM OF SCREEN CYLINDER. REMOVE AND REPLACE AS NECESSARY DURING MAINTENANCE CLEANING.

INSTALLATION NOTES

- A. ANY SUB-BASE, BACKFILL DEPTH, AND/OR ANTI-FLOTATION PROVISIONS ARE SITE-SPECIFIC DESIGN CONSIDERATIONS AND SHALL BE SPECIFIED BY ENGINEER OF RECORD.
- B. CONTRACTOR TO PROVIDE EQUIPMENT WITH SUFFICIENT LIFTING AND REACH CAPACITY TO LIFT AND SET THE CDS MANHOLE STRUCTURE (LIFTING CLUTCHES PROVIDED).
- C. CONTRACTOR TO ADD JOINT SEALANT BETWEEN ALL STRUCTURE SECTIONS, AND ASSEMBLE STRUCTURE.
- D. CONTRACTOR TO PROVIDE, INSTALL, AND GROUT PIPES. MATCH PIPE INVERTS WITH ELEVATIONS SHOWN.
- E. CONTRACTOR TO TAKE APPROPRIATE MEASURES TO ASSURE UNIT IS WATER TIGHT, HOLDING WATER TO FLOWLINE INVERT MINIMUM. IT IS SUGGESTED THAT ALL JOINTS BELOW PIPE INVERTS ARE GROUTED.



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CDS PMSU4040-8-C
INLINE CDS
STANDARD DETAIL



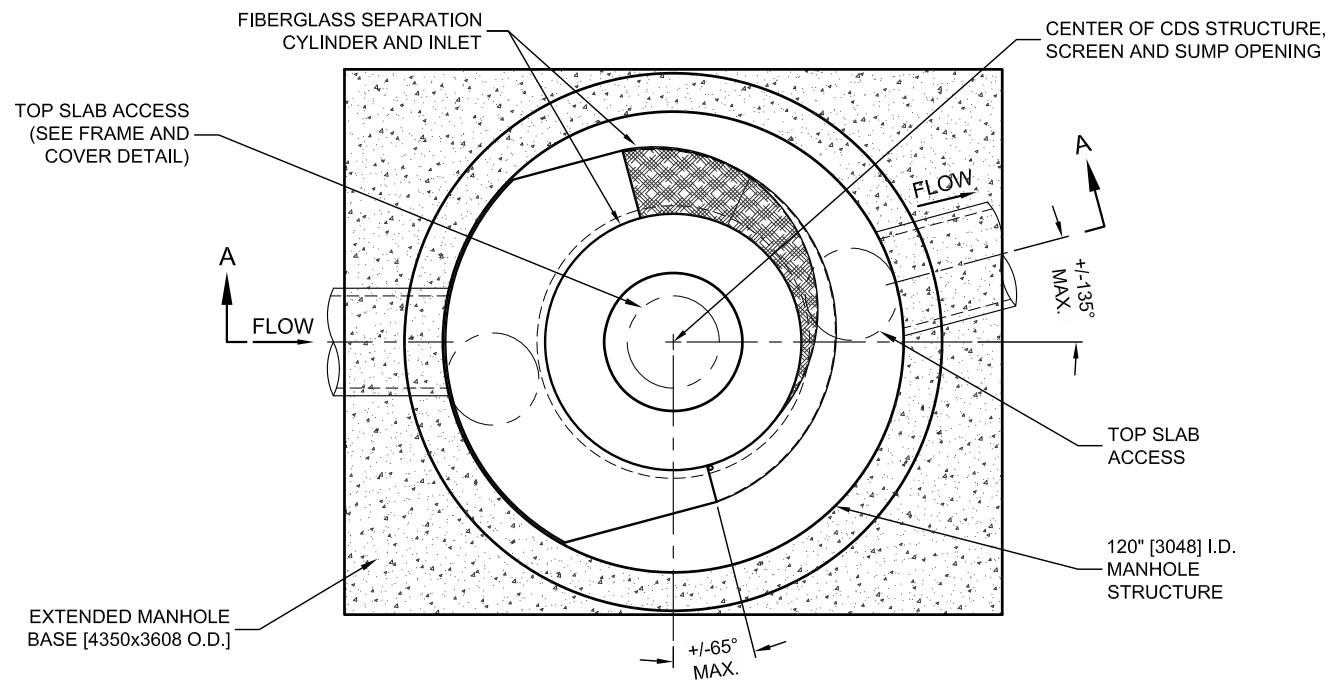
THIS PRODUCT MAY BE PROTECTED BY ONE OR MORE OF THE FOLLOWING U.S. PATENTS: 6,788,848; 6,641,722; 6,511,502; 6,581,783; RELATED FOREIGN PATENTS, OR OTHER PATENTS PENDING.

CDS PMSU5640-10-C DESIGN NOTES

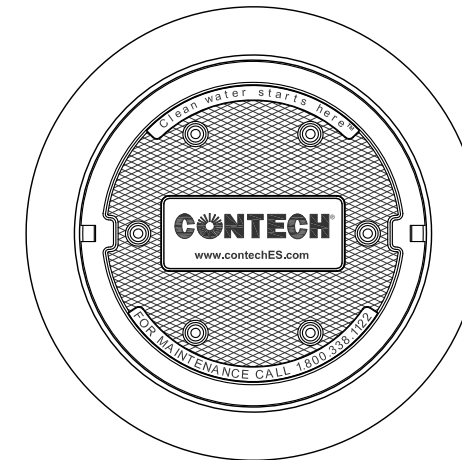
THE STANDARD CDS PMSU5640-10-C CONFIGURATION IS SHOWN. ALTERNATE CONFIGURATIONS ARE AVAILABLE AND ARE LISTED BELOW. SOME CONFIGURATIONS MAY BE COMBINED TO SUIT SITE REQUIREMENTS.

CONFIGURATION DESCRIPTION

- GRATED INLET ONLY (NO INLET PIPE)
- GRATED INLET WITH INLET PIPE OR PIPES
- CURB INLET ONLY (NO INLET PIPE)
- CURB INLET WITH INLET PIPE OR PIPES
- CUSTOMIZABLE SUMP DEPTH AVAILABLE
- ANTI-FLOTATION DESIGN AVAILABLE UPON REQUEST



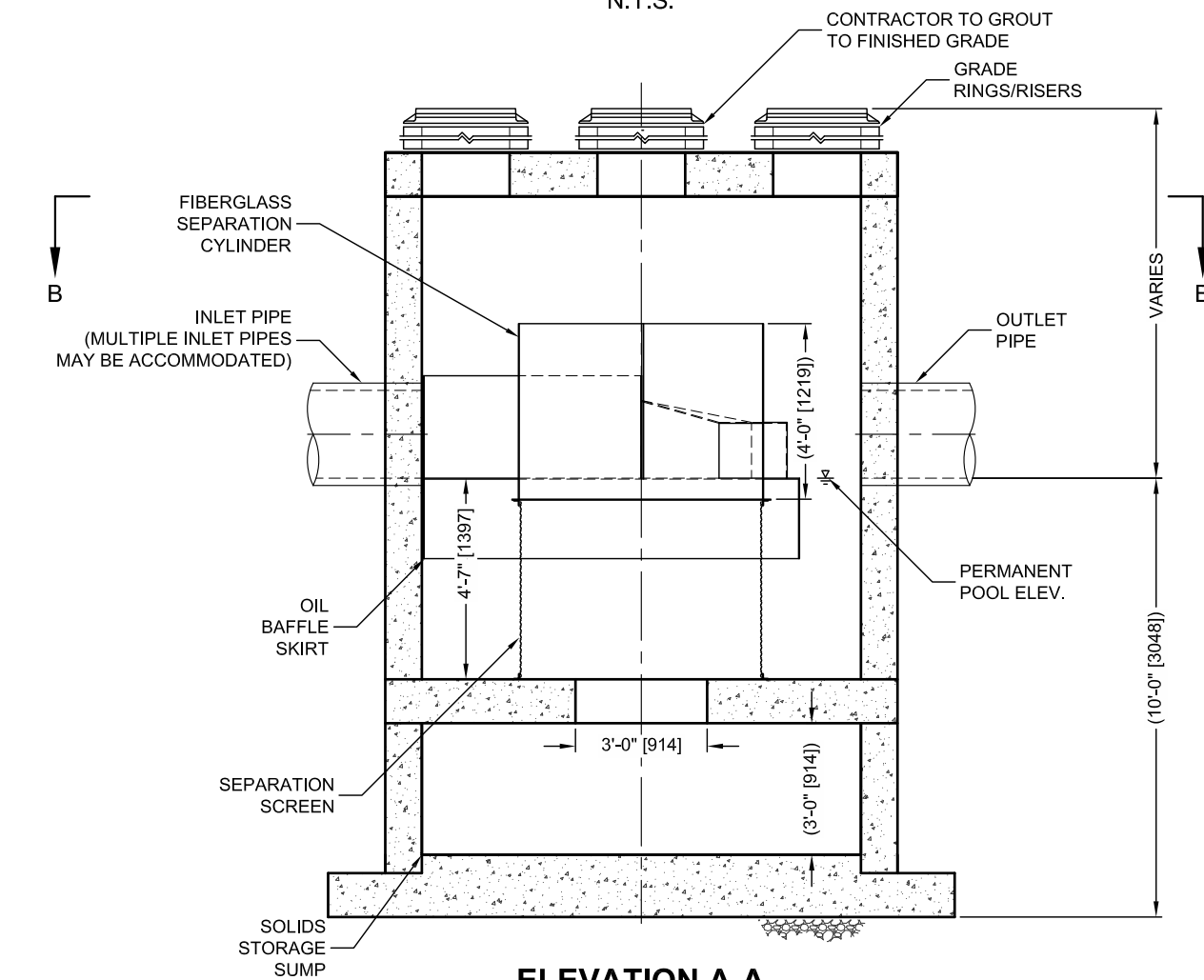
PLAN VIEW B-B
N.T.S.



FRAME AND COVER
(DIAMETER VARIES)
N.T.S.

SITE SPECIFIC DATA REQUIREMENTS

STRUCTURE ID				
WATER QUALITY FLOW RATE (CFS OR L/s)				*
PEAK FLOW RATE (CFS OR L/s)				*
RETURN PERIOD OF PEAK FLOW (YRS)				*
SCREEN APERTURE (2400 OR 4700)				*
PIPE DATA:	I.E.	MATERIAL	DIAMETER	
INLET PIPE 1	*	*	*	
INLET PIPE 2	*	*	*	
OUTLET PIPE	*	*	*	
RIM ELEVATION				*
ANTI-FLOTATION BALLAST	WIDTH	HEIGHT		
	*	*		
NOTES/SPECIAL REQUIREMENTS:				
* PER ENGINEER OF RECORD				



ELEVATION A-A
N.T.S.

GENERAL NOTES

1. CONTECH TO PROVIDE ALL MATERIALS UNLESS NOTED OTHERWISE.
2. DIMENSIONS MARKED WITH () ARE REFERENCE DIMENSIONS. ACTUAL DIMENSIONS MAY VARY.
3. FOR FABRICATION DRAWINGS WITH DETAILED STRUCTURE DIMENSIONS AND WEIGHTS, PLEASE CONTACT YOUR CONTECH ENGINEERED SOLUTIONS LLC REPRESENTATIVE. www.contechES.com
4. CDS WATER QUALITY STRUCTURE SHALL BE IN ACCORDANCE WITH ALL DESIGN DATA AND INFORMATION CONTAINED IN THIS DRAWING.
5. STRUCTURE SHALL MEET AASHTO HS20 AND CASTINGS SHALL MEET HS20 (AASHTO M 306) LOAD RATING, ASSUMING GROUNDWATER ELEVATION AT, OR BELOW, THE OUTLET PIPE INVERT ELEVATION. ENGINEER OF RECORD TO CONFIRM ACTUAL GROUNDWATER ELEVATION.
6. PVC HYDRAULIC SHEAR PLATE IS PLACED ON SHELF AT BOTTOM OF SCREEN CYLINDER. REMOVE AND REPLACE AS NECESSARY DURING MAINTENANCE CLEANING.

INSTALLATION NOTES

- A. ANY SUB-BASE, BACKFILL DEPTH, AND/OR ANTI-FLOTATION PROVISIONS ARE SITE-SPECIFIC DESIGN CONSIDERATIONS AND SHALL BE SPECIFIED BY ENGINEER OF RECORD.
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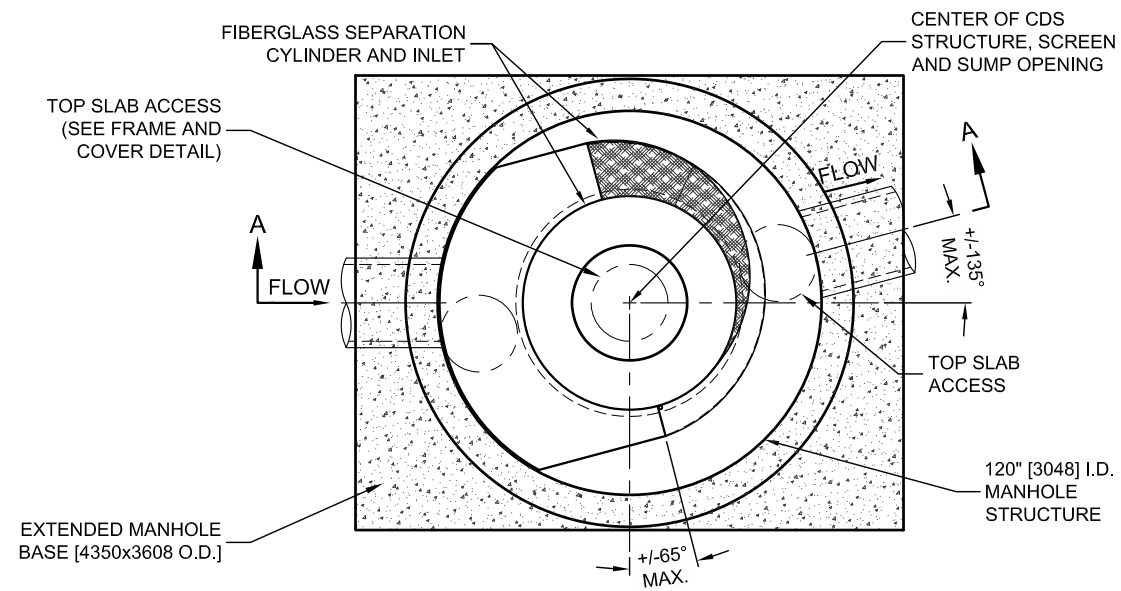


CDS PMSU5653-10-C DESIGN NOTES

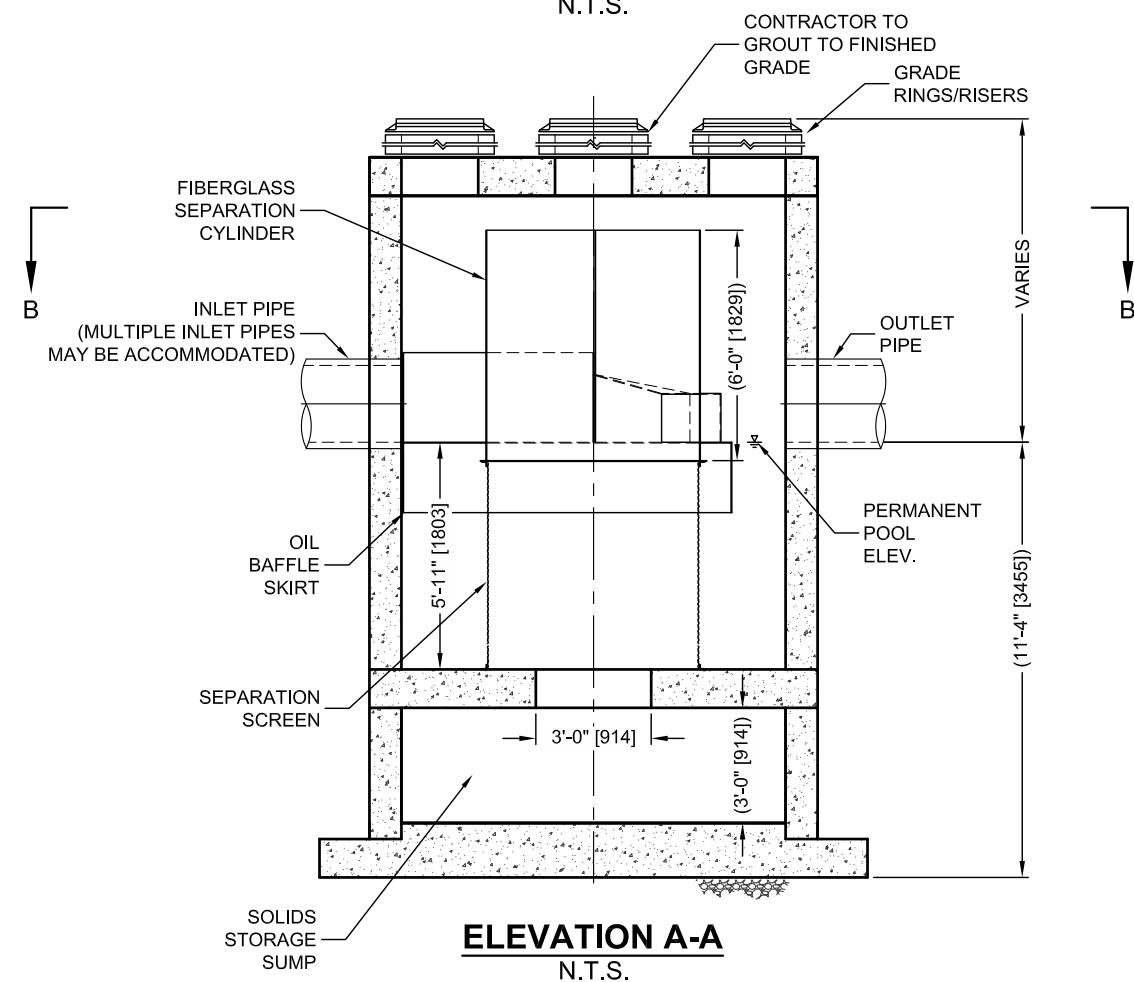
THE STANDARD CDS PMSU5653-10-C CONFIGURATION IS SHOWN. ALTERNATE CONFIGURATIONS ARE AVAILABLE AND ARE LISTED BELOW. SOME CONFIGURATIONS MAY BE COMBINED TO SUIT SITE REQUIREMENTS.

CONFIGURATION DESCRIPTION

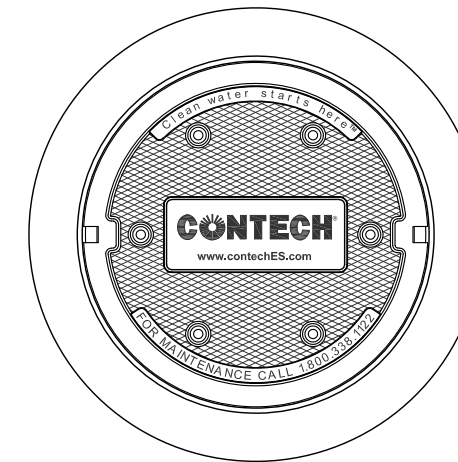
- GRATED INLET ONLY (NO INLET PIPE)
- GRATED INLET WITH INLET PIPE OR PIPES
- CURB INLET ONLY (NO INLET PIPE)
- CURB INLET WITH INLET PIPE OR PIPES
- CUSTOMIZABLE SUMP DEPTH AVAILABLE
- ANTI-FLOTATION DESIGN AVAILABLE UPON REQUEST



PLAN VIEW B-B
N.T.S.



ELEVATION A-A
N.T.S.



FRAME AND COVER
(DIAMETER VARIES)
N.T.S.

SITE SPECIFIC DATA REQUIREMENTS

STRUCTURE ID				
WATER QUALITY FLOW RATE (CFS OR L/s)				*
PEAK FLOW RATE (CFS OR L/s)				*
RETURN PERIOD OF PEAK FLOW (YRS)				*
SCREEN APERTURE (2400 OR 4700)				*
PIPE DATA:	I.E.	MATERIAL	DIAMETER	
INLET PIPE 1	*	*	*	
INLET PIPE 2	*	*	*	
OUTLET PIPE	*	*	*	
RIM ELEVATION				*
ANTI-FLOTATION BALLAST	WIDTH	HEIGHT		
	*	*		
NOTES/SPECIAL REQUIREMENTS:				
* PER ENGINEER OF RECORD				

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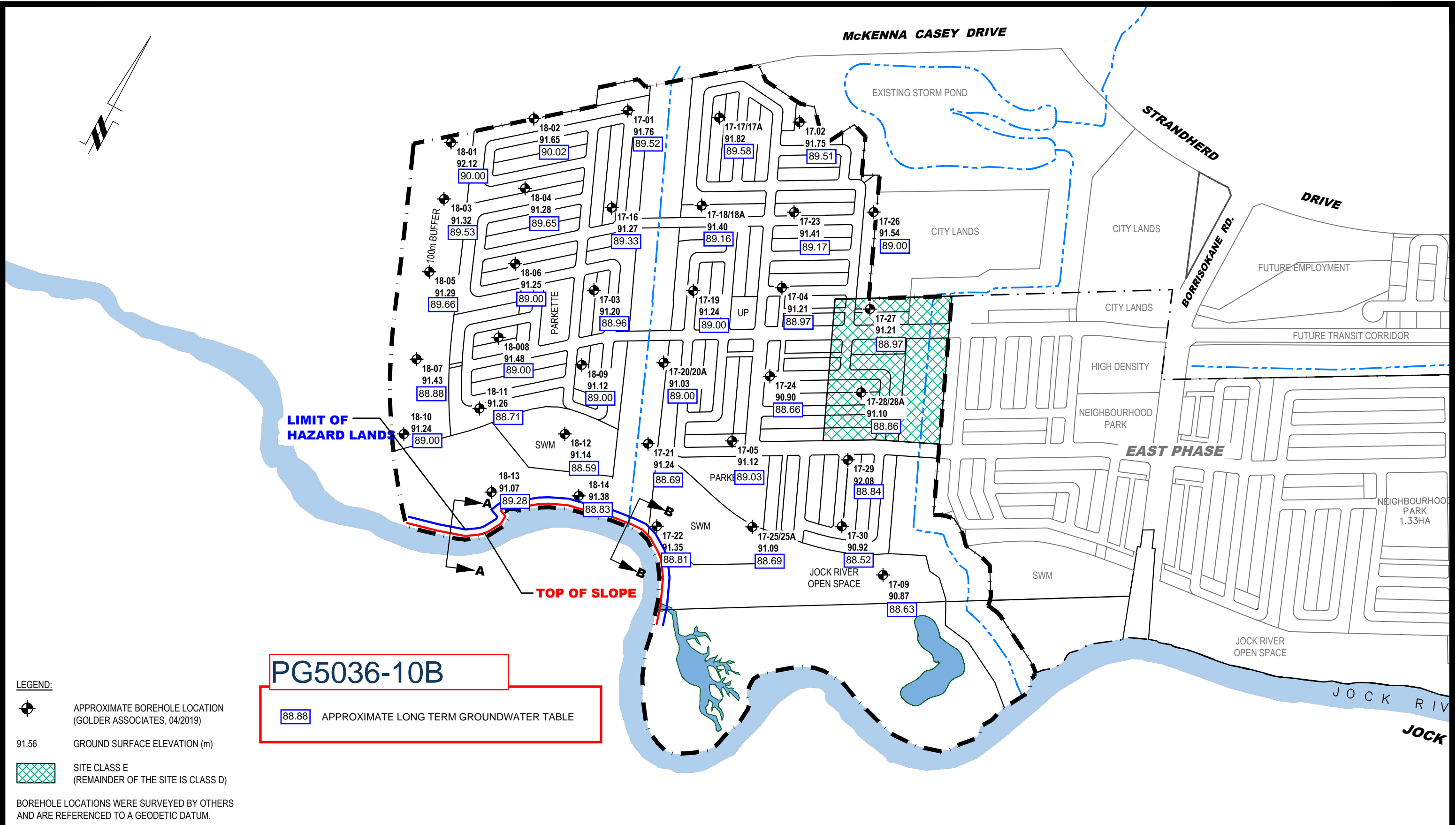
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- LEGEND:**
- APPROXIMATE BOREHOLE LOCATION (GOLDER ASSOCIATES, 04/2019)
 - 91.56 GROUND SURFACE ELEVATION (m)
 - SITE CLASS E (REMAINDER OF THE SITE IS CLASS D)

BOREHOLE LOCATIONS WERE SURVEYED BY OTHERS AND ARE REFERENCED TO A GEODETIC DATUM.

patersongroup
consulting engineers

154 Colonnade Road South
Ottawa, Ontario K2E 7J5
Tel: (613) 226-7381 Fax: (613) 226-6344

NO.	REVISIONS	DATE	INITIAL

CAIVAN COMMUNITIES
GEOTECHNICAL INVESTIGATION
PROP. RESIDENTIAL DEVELOPMENT - CONSERVANCY LANDS WEST
OTTAWA, ONTARIO

TEST HOLE LOCATION PLAN

Scale:	1:6000	Date:	09/2019
Drawn by:	MPG	Report No.:	PG5036-2
Checked by:	SD	PG5036-4	Revision No.:
Approved by:	SD		

plaudocad drawings\geotechnical\pg5036\pg5036-3\fig_west_land.dwg

December 13, 2022

Project Number: 1474

David Schaeffer Engineering Ltd
120 Iber Road, Unit 103
Ottawa, Ontario
K2S 1E9

Attention: Kevin Murphy, P.Eng

Subject: Barrhaven Conservancy West – Preliminary HGL Analysis

Introduction

Barrhaven Conservancy West Development is located in Barrhaven, Ontario, north of the Jock River, east of Highway 416 and west of the Foster Drain. The proposed development is approximately **34.15 ha** that will primarily comprise of single and townhouse residential lots. The following outlines the preliminary hydraulic grade line (HGL) assessment for the site, to ensure that the proposed minor system within the development is adequately sized to safely convey flows to the Jock River under various conditions. As such the following memo outlines the approach taken in assessing the development's HGL and summarises the findings of this analysis.

Analysis Approach

Preliminary hydraulic grade line calculations for the proposed Barrhaven Conservancy West development were completed using PCSWMM modelling software. Pipe data, storm sewer layout and Rational Method flows in the storm sewer are as provided by DSEL. The Rational Method flows were calculated based on the 2-, 5- or 10-year level of service requirements, and the 100-year flows in the hydraulic grade line calculations were estimated as 14% greater than the Rational Method flows, to account for the additional flows captured by catchbasin grates, lead pipes and/or inlet control devices under the higher surface water depths of the 100-year storm.

The 14% increase in flows for the 100-year event is based on the assumption that the head on a lead pipe/ICD will increase by 35 cm (maximum allowable major system ponding depth) during the 100-Year event. Taking a typical 250 mm lead pipe and assuming that the head on the pipe is just below the top of the grate (assumed at 1.38 m) results in a peak flow of 209 L/s, then assuming that the head is increased by 35 cm during the 100-Year (head of 1.730 m) the flow through the lead pipe would increase to 234.5 L/s, which results in a 12% increase in peak flows. It is important to note that a 12% increase is observed when the same calculations are applied to the various lead pipe and ICD sizes. An additional 2% is added as a safety factor to allow some flexibility in the design, as it is likely that not all lead pipes will have a head of 1.38 m (just below the top of MH) for the level of service specified.

The proposed storm sewer infrastructure data was extracted from DSEL's detailed drawings and incorporated into a PCSWMM model, and flows derived by DSEL's rational method calculations were then applied to each Maintenance Hole (MH) in the model as steady flows (using the baseflow option). Exit losses were applied to all storm sewer pipes in the system based on the angle of the downstream connection.

As with all other works completed for the Barrhaven Conservancy development phases, the preliminary HGL analysis was completed under two conditions:

- 100-year rainfall event on the development and a 5-year spring water level on the Jock River
- Level of service (2/5/10-year) rainfall event on the development and a 100-year spring water level on the Jock River

Note that the water level along the Jock River through the length of this development varies, and as such the nearest corresponding upstream water surface elevation calculated by RVCA’s HEC-RAS floodplain mapping model of the Jock River was applied at each of the respective storm sewer outlets. Also, note that assuming a 5-year spring water level on the Jock River for a 100-year rainfall event on the development is an inherently conservative assumption, as the critical storm for the proposed development is a summer (intense rainfall) event while the critical storm for the Jock River is a spring (snowmelt + rainfall) event. A preliminary Single Station Flood Frequency analysis was completed by JFSA using only summer flows (from May 15 to October 31) based on historical flow data recorded at the Moodie Drive Water Survey Canada gauge. This analysis found that the 100-year summer flow on the Jock River is around **99 m³/s**, while the 5-year spring flow is around **123 m³/s**, therefore the downstream boundary condition applied is conservative.

Within the proposed development, Oil and Grit Separators (OGS) units in conjunction with LID measures will be implemented to ensure the site meets quality control requirements. Preliminary OGS units and associated by-pass weir elevations have also been included in the model, based on similar drainage areas and imperviousness seen in Barrhaven Conservancy Phase 2. **Table 1** below outlines the assumed OGS sizes and configurations based on similar drainage areas and imperviousness found in Barrhaven Conservancy Phase 2. Note that the trunk sewers for this development phase have been numbered 1-4 progressing from east to west (Foster Creek to Highway 416).

Trunk System	Area (ha)	Runoff Coefficient	CDS Model	CDS Inlet/Outlet Pipe (mm)	Weir Height (mm)
Trunk 1	8.92	0.7	PMSU 5640 -10	750	660
Trunk 2	10.75	0.69	PMSU 5640 -10	750	660
Trunk 3	6.3	0.64	PMSU 4045 -8	675	650
Trunk 4	8.18	0.67	PMSU 5640 -10	750	660
Total	34.15	0.68			

Results

The maximum HGL obtained at each MH has been extracted from the level of service (2/5/10-year) event / 100-year Jock River water level scenario and the 100-year event / 5-year Jock River water level scenario, with the results from this analysis provided in **Tables 1 & 2**, respectively. As all proposed units within this development will have sump pumps, the simulated HGL was compared against the top of MH elevation to ensure that all storm sewers infrastructure is sufficiently sized and is not surcharging to the major system during the assessed events.

From this analysis, it was found that the critical scenario for HGL within the development was the level of service development event and 100-year water level on the Jock River scenario. Based on this scenario, no MHs will have an HGL elevation above the top of MH (minimum freeboard of **0.50 m** at **MH-109**), with an average freeboard of **0.75 m** from the top of MH throughout the proposed development.

For the 100-year event and 5-year water level on the Jock River, no MHs will have HGL elevations above the top of MH (minimum freeboard of **1.14 m** at **MH-101**), with an average freeboard of **1.37 m** from the top of MH throughout the proposed development. As such it can be concluded that the proposed storm sewer infrastructure is sufficiently sized, to safely convey minor system flows from the development under various extreme conditions.

Conclusion

A preliminary HGL analysis for the West Phase of the Barrhaven Conservancy Development was completed using PCSWMM based on storm sewer and flow details provided by DSEL. From this analysis, it was found that the proposed storm sewer infrastructure is sufficiently sized to convey all minor system flows to the Jock River and will not result in any MHs surcharging to the street under extreme events such as 100-year rainfall events on the development and a 5-year spring water level on the Jock River and a level of service (2/5/10 Year) rainfall event on the development and a 100-year spring water level on the Jock River, with the former being the more critical scenario for the HGL within the development.

Yours truly,
J.F Sabourin and Associates Inc.



Jonathon Burnett, P.Eng
Water Resources Engineer



cc: J.F Sabourin, M.Eng, P.Eng
Director of Water Resources Projects

Figures

Figure 1: PCSWMM Model Overview

Tables

Table 1: HGL Result Tables - Level of service (2/5/10-year) BCDC Development & 100-Year Jock River

Table 2: HGL Result Tables - 100-Year BCDC Development & 5-Year Jock River

Attachments

Attachment A: DSEL Rational Method Calculations

Modelling Files – Provided Electronically

PCSWMM BCDC-West_HGL_v02.0-5YrDev-100YrJock.inp
BCDC-West_HGL_v02.0-100YrDev-5YrJock.inp



- Legend**
- Junctions
 - Conduits
 - ▲ Outfalls
 - Development Plan

J.F. Sabourin and Associates Inc.
 WATER RESOURCES AND ENVIRONMENTAL CONSULTANTS
 52 Springbrook Drive (613) 836-3884
 Ottawa, ON, K2S 1B9 www.jfsa.com



SCALE : 1:3,500
 0 50 100 150 200 m

PROJECT :
 Barrhaven Conservancy Development
 Phase 3

TITLE :
 Figure 1:
 Preliminary HGL Analysis
 Model Overview

PROJECT	1474 -17
DRAWN:	JB
DATE:	DEC 2022

Table 1: BCDC West - Preliminary HGL Analysis
Level of Service (2/5/10 Year) BCDC Development & 100-Year Jock River

MH-ID	Invert Elevation	Top of MH (m)	Max HGL (m)	Freeboard (m)
MH-10	90.38	93.43	92.41	1.02
MH-100	90.28	93.06	92.39	0.67
MH-101	90.13	92.89	92.35	0.54
MH-102	89.99	92.85	92.30	0.55
MH-103	89.92	92.79	92.28	0.52
MH-106	89.79	92.71	92.20	0.51
MH-108	89.70	92.67	92.14	0.53
MH-109	89.61	92.59	92.09	0.50
MH-11	90.22	93.24	92.31	0.93
MH-110	89.57	92.58	92.07	0.51
MH-12	90.11	93.13	92.25	0.88
MH-121	89.36	92.52	92.00	0.52
MH-13	90.02	93.11	92.23	0.89
MH-14	89.95	93.06	92.21	0.85
MH-15	89.90	93.04	92.20	0.84
MH-17	89.82	93.02	92.17	0.86
MH-28	89.60	92.93	92.13	0.80
MH-36	91.13	93.39	92.30	1.09
MH-37	90.37	93.37	92.30	1.07
MH-38	90.08	93.18	92.28	0.90
MH-39	89.94	93.08	92.21	0.88
MH-40	89.84	93.02	92.17	0.85
MH-41	89.76	92.94	92.14	0.80
MH-42	89.72	92.93	92.13	0.80
MH-46	89.58	92.77	92.06	0.71
MH-570	90.83	93.64	92.48	1.16
MH-60	91.24	93.73	92.76	0.97
MH-61	91.08	93.72	92.77	0.95
MH-62	90.88	93.53	92.75	0.78
MH-65	90.76	93.47	92.69	0.78
MH-67	90.63	93.40	92.66	0.74
MH-69	90.51	93.33	92.63	0.70
MH-70	90.29	93.24	92.55	0.69
MH-72	90.07	93.15	92.46	0.69
MH-76	89.97	93.04	92.43	0.61
MH-81	89.84	92.95	92.36	0.59
MH-82	89.72	92.89	92.28	0.61
MH-83	89.61	92.79	92.22	0.57
MH-84	89.57	92.77	92.20	0.57
MH-9	90.47	93.52	92.44	1.08
MH-90	89.49	92.75	92.14	0.61
MH-97	90.75	93.17	92.49	0.68
MH-98	90.66	93.11	92.48	0.63
MH-99	90.42	93.01	92.42	0.59
			Min	0.50
			Max	1.16
			Average	0.75

Note: Analysis assumes 100 year spring water level on the Jock River

Model Name:BCDC-West_HGL_v02.0-5YrDev-100YrJock.inp

**Table 2: BCDC West - Preliminary HGL Analysis
100-Year BCDC Development & 5-Year Jock River**

MH-ID	Invert Elevation	Top of MH (m)	Max HGL (m)	Freeboard (m)
MH-10	90.38	93.43	91.81	1.62
MH-100	90.28	93.06	91.81	1.25
MH-101	90.13	92.89	91.75	1.14
MH-102	89.99	92.85	91.70	1.15
MH-103	89.92	92.79	91.66	1.14
MH-106	89.79	92.71	91.56	1.15
MH-108	89.70	92.67	91.48	1.19
MH-109	89.61	92.59	91.42	1.17
MH-11	90.22	93.24	91.68	1.56
MH-110	89.57	92.58	91.39	1.19
MH-12	90.11	93.13	91.60	1.54
MH-121	89.36	92.52	91.30	1.22
MH-13	90.02	93.11	91.57	1.55
MH-14	89.95	93.06	91.54	1.52
MH-15	89.90	93.04	91.53	1.51
MH-17	89.82	93.02	91.49	1.54
MH-28	89.60	92.93	91.44	1.49
MH-36	91.13	93.39	91.66	1.73
MH-37	90.37	93.37	91.66	1.71
MH-38	90.08	93.18	91.64	1.54
MH-39	89.94	93.08	91.54	1.55
MH-40	89.84	93.02	91.49	1.53
MH-41	89.76	92.94	91.46	1.48
MH-42	89.72	92.93	91.44	1.49
MH-46	89.58	92.77	91.36	1.41
MH-570	90.83	93.64	91.93	1.71
MH-60	91.24	93.73	92.27	1.46
MH-61	91.08	93.72	92.27	1.46
MH-62	90.88	93.53	92.24	1.29
MH-65	90.76	93.47	92.17	1.31
MH-67	90.63	93.40	92.13	1.27
MH-69	90.51	93.33	92.10	1.23
MH-70	90.29	93.24	91.98	1.26
MH-72	90.07	93.15	91.87	1.28
MH-76	89.97	93.04	91.84	1.20
MH-81	89.84	92.95	91.74	1.21
MH-82	89.72	92.89	91.64	1.25
MH-83	89.61	92.79	91.56	1.23
MH-84	89.57	92.77	91.54	1.23
MH-9	90.47	93.52	91.85	1.67
MH-90	89.49	92.75	91.46	1.29
MH-97	90.75	93.17	91.94	1.23
MH-98	90.66	93.11	91.92	1.19
MH-99	90.42	93.01	91.85	1.16
			Min	1.14
			Max	1.73
			Average	1.37

Note: Analysis assumes 5 year spring water level on the Jock River

Model Name:BCDC-West_HGL_v02.0-100YrDev-5YrJock



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Ottawa, ON
Paris, ON
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Montréal, QC
Québec, QC

Attachment A

DSEL Rational Method Calculations

STORM SEWER CALCULATION SHEET (RATIONAL METHOD)



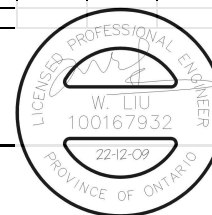
Local Roads Return Frequency = 2 years
 Collector Roads Return Frequency = 5 years
 Arterial Roads Return Frequency = 10 years

Manning 0.013

LOCATION			AREA (Ha)																FLOW					SEWER DATA													
			2 YEAR				5 YEAR				10 YEAR				100 YEAR				Time of Conc.	Intensity 2 Year	Intensity 5 Year	Intensity 10 Year	Intensity 100 Year	Peak Flow	DIA. (mm) (actual)	DIA. (mm) (nominal)	TYPE	SLOPE (%)	LENGTH (m)	CAPACITY (l/s)	VELOCITY (m/s)	TIME OF LOW (min)	RATIO Q/Q full				
Location	From Node	To Node	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	(min)	(mm/h)	(mm/h)	(mm/h)	(mm/h)	Q (l/s)	(actual)	(nominal)		(%)	(m)	(l/s)	(m/s)	LOW (min)	Q/Q full				
Contribution From STREET '17', Pipe 72 - 76					13.48					0.49					0.00				0.00	20.16																	
Contribution From STREET '1', Pipe 74 - 76					0.00					1.88					0.00				0.00	12.60																	
Contribution From STREET '1', Pipe 75 - 76					0.00					0.17					0.00				0.00	10.48																	
	76	81			0.00	13.48	0.12	0.67	0.22	2.76					0.00	0.00		0.00	20.16	51.77	69.90	81.80	119.34	891	1200	1200	CONC	0.11	60.0	1293.0625	1.1433	0.8746	0.689				
To STREET '8', Pipe 81 - 82					13.48					2.76					0.00			0.00	21.04																		
STREET '29'																																					
Contribution From STREET '2', Pipe 106 - 108					8.87					2.78					0.00				0.00	19.37																	
Contribution From STREET '2', Pipe 107 - 108					0.00					0.06					0.00				0.00	10.26																	
	108	109			0.16	0.67	0.30	0.67	0.00	9.17	0.44	0.40	0.49	3.33			0.00	0.00	19.37	53.07	71.67	83.88	122.40	725	1050	1050	CONC	0.11	50.5	905.6791	1.0459	0.8047	0.801				
	109	110			0.01	0.67	0.02	0.67	0.00	9.19			0.00	3.33			0.00	0.00	20.17	51.76	69.88	81.77	119.31	708	1050	1050	CONC	0.11	12.0	905.6791	1.0459	0.1912	0.782				
	110	121			0.08	0.67	0.15	0.67	0.00	9.34			0.00	3.33			0.00	0.00	20.36	51.46	69.47	81.29	118.60	712	1050	1050	CONC	0.11	59.0	905.6791	1.0459	0.9401	0.786				
Contribution From STREET '2', Pipe 114 - 120					1.33					0.53					0.00			0.00	14.73																		
Contribution From STREET '7', Pipe 118 - 120					1.48					0.60					0.00			0.00	13.95																		
Contribution From STREET '2', Pipe 119 - 120					0.00					0.22					0.00			0.00	10.29																		
	120	121			0.28	0.67	0.52	0.67	0.00	3.34			0.00	1.36			0.00	0.00	14.73	62.41	84.43	98.88	144.41	323	825	825	CONC	0.11	73.5	476.0801	0.8906	1.3755	0.678				
	121	OGS W4			0.03	0.67	0.06	0.67	0.00	12.73			0.00	4.68			0.00	0.00	21.30	50.03	67.52	79.00	115.24	953	1200	1200	CONC	0.11	5.5	1293.0625	1.1433	0.0802	0.737				

Definitions:
 Q = 2.78 AIR, where
 Q = Peak Flow in Litres per second (L/s)
 A = Areas in hectares (ha)
 I = Rainfall Intensity (mm/h)
 R = Runoff Coefficient

Notes:
 1) Ottawa Rainfall-Intensity Curve
 2) Min. Velocity = 0.80 m/s



Designed: M.S.	PROJECT: 1226 - Barrhaven Conservancy West
Checked: W.L./V.W.	LOCATION: City of Ottawa
Dwg. Reference:	File Ref:
Date: 09 Dec 2022	Sheet No. SHEET 7 OF 7

Attachment B

PCSWMM Model Input Files

```

00001> [TITLE]
00002> ;;Project Title/Notes
00003>
00004> [OPTIONS]
00005> ;;Option Value
00006> FLOW UNITS LPS
00007> INFILTRATION HORTON
00008> FLOW_ROUTING DYNWAVE
00009> LINK_OFFSETS DEPTH
00010> MIN_SLOPE 0
00011> ALLOW_PONDING NO
00012> SKIP_STEADY_STATE NO
00013>
00014> START_DATE 12/05/2022
00015> START_TIME 00:00:00
00016> REPORT_START_DATE 12/05/2022
00017> REPORT_START_TIME 00:00:00
00018> END_DATE 12/06/2022
00019> END_TIME 00:00:00
00020> SWEEP_START 01/01
00021> SWEEP_END 12/31
00022> DRY_DAYS 0
00023> REPORT_STEP 00:01:00
00024> WET_STEP 00:05:00
00025> DRY_STEP 00:05:00
00026> ROUTING_STEP 5
00027> RULE_STEP 00:00:00
00028>
00029> INERTIAL_DAMPING PARTIAL
00030> NORMAL_FLOW_LIMITED BOTH
00031> FORCE_MAIN_EQUATION H-W
00032> VARIABLE_STEP 0.75
00033> LENGTHENING_STEP 0
00034> MIN_SURFAREA 0
00035> MAX_TRIALS 8
00036> HEAD_TOLERANCE 0.0015
00037> SYS_FLOW_TOL 5
00038> LAT_FLOW_TOL 5
00039> MINIMUM_STEP 0.5
00040> THREADS 6
00041>
00042> [FILES]
00043> ;;Interfacing Files
00044> USE HOTSTART "C:\OneDrive\J.F. Sabourin and Associates Inc\JFSA-OTTAWA-SERVER - Documents\PROJ\1474(03)-21\202
00045>
00046> [EVAPORATION]
00047> ;;Data Source Parameters
00048> ;;-----
00049> CONSTANT 0.0
00050> DRY_ONLY NO
00051>
00052> [JUNCTIONS]
00053> ;;Name Elevation MaxDepth InitDepth SurDepth Aponded
00054> ;;-----
00055> 1 89.599 3.33 0 0 0
00056> 2 89.577 3.192 0 0 0
00057> 3 89.489 3.26 0 0 0
00058> 4 89.355 3.164 0 0 0
00059> MH-10 90.377 3.053 0 0 0
00060> MH-100 90.279 2.781 0 0 0
00061> MH-101 90.13 2.76 0 0 0
00062> MH-102 89.989 2.861 0 0 0
00063> MH-103 89.915 2.875 0 0 0
00064> MH-106 89.788 2.922 0 0 0
00065> MH-108 89.7 2.97 0 0 0
00066> MH-109 89.614 2.976 0 0 0
00067> MH-11 90.223 3.017 0 0 0
00068> MH-110 89.571 3.009 0 0 0
00069> MH-12 90.105 3.025 0 0 0
00070> MH-121 89.356 3.164 0 0 0
00071> MH-13 90.015 3.095 0 0 0
00072> MH-14 89.95 3.11 0 0 0
00073> MH-15 89.901 3.139 0 0 0
00074> MH-17 89.815 3.205 0 0 0
00075> MH-28 89.6 3.33 0 0 0
00076> MH-36 91.126 2.264 0 0 0
00077> MH-37 90.368 3.002 0 0 0
00078> MH-38 90.078 3.102 0 0 0
00079> MH-39 89.935 3.145 0 0 0
00080> MH-40 89.844 3.176 0 0 0
00081> MH-41 89.76 3.18 0 0 0
00082> MH-42 89.716 3.214 0 0 0
00083> MH-46 89.578 3.192 0 0 0
00084> MH-570 90.833 2.807 0 0 0
00085> MH-60 91.241 2.489 0 0 0
00086> MH-61 91.075 2.645 0 0 0
00087> MH-62 90.878 2.652 0 0 0
00088> MH-65 90.755 2.715 0 0 0
00089> MH-67 90.632 2.768 0 0 0

```


00090>	MH-69	90.509	2.821	0	0	0			
00091>	MH-70	90.29	2.95	0	0	0			
00092>	MH-72	90.071	3.079	0	0	0			
00093>	MH-76	89.966	3.074	0	0	0			
00094>	MH-81	89.84	3.11	0	0	0			
00095>	MH-82	89.717	3.173	0	0	0			
00096>	MH-83	89.61	3.18	0	0	0			
00097>	MH-84	89.566	3.204	0	0	0			
00098>	MH-9	90.466	3.054	0	0	0			
00099>	MH-90	89.49	3.26	0	0	0			
00100>	MH-97	90.746	2.424	0	0	0			
00101>	MH-98	90.66	2.45	0	0	0			
00102>	MH-99	90.416	2.594	0	0	0			
00103>	OGS1	89.599	3.331	0	0	0			
00104>	OGS2	89.577	3.193	0	0	0			
00105>	OGS3	89.489	3.261	0	0	0			
00106>	OGS4	89.355	3.165	0	0	0			
00107>									
00108>	[OUTFALLS]								
00109>	;;Name	Elevation	Type	Stage Data	Gated	Route To			
00110>	;;-----								
00111>	MH-1001	89.57	FIXED	92.06	NO				
00112>	MH-2000	89.57	FIXED	92.02	NO				
00113>	MH-3000	89.46	FIXED	92.02	NO				
00114>	MH-4001	89.35	FIXED	91.9	NO				
00115>									
00116>	[CONDUITS]								
00117>	;;Name	From Node	To Node	Length	Roughness	InOffset	OutOffset	InitFlow	MaxF
00118>	;;-----								
00119>	1	MH-28	OGS1	0.735	0.013	0	0	0	0
00120>	2	OGS1	1	0.753	0.013	0	0	0	0
00121>	3	MH-46	OGS2	0.93	0.013	0	0	0	0
00122>	4	OGS2	2	0.9	0.013	0	0	0	0
00123>	5	MH-90	OGS3	0.89	0.013	0	0	0	0
00124>	6	OGS3	3	0.977	0.013	0	0	0	0
00125>	7	MH-121	OGS4	0.782	0.013	0	0	0	0
00126>	8	OGS4	4	0.747	0.013	0	0	0	0
00127>	STM-100-101	MH-100	MH-101	67.5	0.013	0	0.075	0	0
00128>	STM-10-11	MH-10	MH-11	122	0.013	0	0.02	0	0
00129>	STM-101-102	MH-101	MH-102	60	0.013	0	0.075	0	0
00130>	STM-102-103	MH-102	MH-103	49	0.013	0	0.02	0	0
00131>	STM-103-106	MH-103	MH-106	47.5	0.013	0	0.075	0	0
00132>	STM-106-108	MH-106	MH-108	25	0.013	0	0.06	0	0
00133>	STM-108-109	MH-108	MH-109	50.5	0.013	0	0.03	0	0
00134>	STM-109-110	MH-109	MH-110	12	0.013	0	0.03	0	0
00135>	STM-110-121	MH-110	MH-121	59	0.013	0	0.15	0	0
00136>	STM-11-12	MH-11	MH-12	80	0.013	0	0.03	0	0
00137>	STM-12-13	MH-12	MH-13	13.5	0.013	0	0.075	0	0
00138>	STM-121-4001_2	4	MH-4001	4.324	0.013	0	0	0	0
00139>	STM-13-14	MH-13	MH-14	32	0.013	0	0.03	0	0
00140>	STM-14-15	MH-14	MH-15	17	0.013	0	0.03	0	0
00141>	STM-15-17	MH-15	MH-17	10	0.013	0	0.075	0	0
00142>	STM-17-28	MH-17	MH-28	59	0.013	0	0.15	0	0
00143>	STM-28-1001_2	1	MH-1001	26.301	0.013	0	0	0	0
00144>	STM-36-37	MH-36	MH-37	13	0.013	0	0.719	0	0
00145>	STM-37-38	MH-37	MH-38	127.5	0.013	0	0.15	0	0
00146>	STM-38-39	MH-38	MH-39	62	0.013	0	0.075	0	0
00147>	STM-39-40	MH-39	MH-40	64.5	0.013	0	0.02	0	0
00148>	STM-40-41	MH-40	MH-41	49.5	0.013	0	0.03	0	0
00149>	STM-41-42	MH-41	MH-42	13	0.013	0	0.03	0	0
00150>	STM-42-46	MH-42	MH-46	107.5	0.013	0	0.02	0	0
00151>	STM-46-2000_2	2	MH-2000	6.468	0.013	0	0	0	0
00152>	STM-570-97	MH-570	MH-97	44.5	0.013	0	0.02	0	0
00153>	STM-60-61	MH-60	MH-61	10.5	0.013	0	0.15	0	0
00154>	STM-61-62	MH-61	MH-62	124.5	0.013	0	0.06	0	0
00155>	STM-62-65	MH-62	MH-65	44	0.013	0	0.075	0	0
00156>	STM-65-67	MH-65	MH-67	44	0.013	0	0.075	0	0
00157>	STM-67-69	MH-67	MH-69	44	0.013	0	0.075	0	0
00158>	STM-69-70	MH-69	MH-70	63	0.013	0	0.15	0	0
00159>	STM-70-72	MH-70	MH-72	63	0.013	0	0.15	0	0
00160>	STM-72-76	MH-72	MH-76	68.5	0.013	0	0.03	0	0
00161>	STM-76-81	MH-76	MH-81	60	0.013	0	0.06	0	0
00162>	STM-81-82	MH-81	MH-82	57.5	0.013	0	0.06	0	0
00163>	STM-82-83	MH-82	MH-83	70	0.013	0	0.03	0	0
00164>	STM-83-84	MH-83	MH-84	12.5	0.013	0	0.03	0	0
00165>	STM-84-90	MH-84	MH-90	14.5	0.013	0	0.06	0	0
00166>	STM-90-3000_2	3	MH-3000	25.761	0.013	0	0	0	0
00167>	STM-9-10	MH-9	MH-10	62.5	0.013	0	0.02	0	0
00168>	STM-97-98	MH-97	MH-98	44	0.013	0	0.02	0	0
00169>	STM-98-99	MH-98	MH-99	62.5	0.013	0	0.15	0	0
00170>	STM-99-100	MH-99	MH-100	56.5	0.013	0	0.075	0	0
00171>									
00172>	[WEIRS]								
00173>	;;Name	From Node	To Node	Type	CrestHt	Qcoeff	Gated	EndCon	EndCoe
00174>	;;-----								
00175>	STM-121-4001_1	MH-121	4	TRANSVERSE	0.66	1.8	NO	0	2
00176>	STM-28-1001_1	MH-28	1	TRANSVERSE	0.66	1.8	NO	0	2
00177>	STM-46-2000_1	MH-46	2	TRANSVERSE	0.65	1.8	NO	0	2
00178>	STM-90-3000_1	MH-90	3	TRANSVERSE	0.66	1.8	NO	0	2

00181>	;;Link	Shape	Geom1	Geom2	Geom3	Geom4	Barrels	Culvert
00182>	;;							
00183>	1	CIRCULAR	0.75	0	0	0	1	
00184>	2	CIRCULAR	0.75	0	0	0	1	
00185>	3	CIRCULAR	0.675	0	0	0	1	
00186>	4	CIRCULAR	0.675	0	0	0	1	
00187>	5	CIRCULAR	0.75	0	0	0	1	
00188>	6	CIRCULAR	0.75	0	0	0	1	
00189>	7	CIRCULAR	0.75	0	0	0	1	
00190>	8	CIRCULAR	0.75	0	0	0	1	
00191>	STM-100-101	CIRCULAR	0.825	0	0	0	1	
00192>	STM-10-11	CIRCULAR	0.825	0	0	0	1	
00193>	STM-101-102	CIRCULAR	0.9	0	0	0	1	
00194>	STM-102-103	CIRCULAR	0.975	0	0	0	1	
00195>	STM-103-106	CIRCULAR	0.975	0	0	0	1	
00196>	STM-106-108	CIRCULAR	1.05	0	0	0	1	
00197>	STM-108-109	CIRCULAR	1.05	0	0	0	1	
00198>	STM-109-110	CIRCULAR	1.05	0	0	0	1	
00199>	STM-110-121	CIRCULAR	1.05	0	0	0	1	
00200>	STM-11-12	CIRCULAR	0.825	0	0	0	1	
00201>	STM-12-13	CIRCULAR	0.825	0	0	0	1	
00202>	STM-121-4001_2	CIRCULAR	1.2	0	0	0	1	
00203>	STM-13-14	CIRCULAR	0.9	0	0	0	1	
00204>	STM-14-15	CIRCULAR	0.9	0	0	0	1	
00205>	STM-15-17	CIRCULAR	0.9	0	0	0	1	
00206>	STM-17-28	CIRCULAR	0.9	0	0	0	1	
00207>	STM-28-1001_2	CIRCULAR	1.05	0	0	0	1	
00208>	STM-36-37	CIRCULAR	0.375	0	0	0	1	
00209>	STM-37-38	CIRCULAR	0.75	0	0	0	1	
00210>	STM-38-39	CIRCULAR	0.9	0	0	0	1	
00211>	STM-39-40	CIRCULAR	0.975	0	0	0	1	
00212>	STM-40-41	CIRCULAR	0.975	0	0	0	1	
00213>	STM-41-42	CIRCULAR	0.975	0	0	0	1	
00214>	STM-42-46	CIRCULAR	0.975	0	0	0	1	
00215>	STM-46-2000_2	CIRCULAR	0.975	0	0	0	1	
00216>	STM-570-97	CIRCULAR	0.6	0	0	0	1	
00217>	STM-60-61	CIRCULAR	0.6	0	0	0	1	
00218>	STM-61-62	CIRCULAR	0.75	0	0	0	1	
00219>	STM-62-65	CIRCULAR	0.75	0	0	0	1	
00220>	STM-65-67	CIRCULAR	0.825	0	0	0	1	
00221>	STM-67-69	CIRCULAR	0.9	0	0	0	1	
00222>	STM-69-70	CIRCULAR	0.9	0	0	0	1	
00223>	STM-70-72	CIRCULAR	1.05	0	0	0	1	
00224>	STM-72-76	CIRCULAR	1.2	0	0	0	1	
00225>	STM-76-81	CIRCULAR	1.2	0	0	0	1	
00226>	STM-81-82	CIRCULAR	1.2	0	0	0	1	
00227>	STM-82-83	CIRCULAR	1.2	0	0	0	1	
00228>	STM-83-84	CIRCULAR	1.2	0	0	0	1	
00229>	STM-84-90	CIRCULAR	1.2	0	0	0	1	
00230>	STM-90-3000_2	CIRCULAR	1.2	0	0	0	1	
00231>	STM-9-10	CIRCULAR	0.825	0	0	0	1	
00232>	STM-97-98	CIRCULAR	0.6	0	0	0	1	
00233>	STM-98-99	CIRCULAR	0.6	0	0	0	1	
00234>	STM-99-100	CIRCULAR	0.75	0	0	0	1	
00235>	STM-121-4001_1	RECT_OPEN	0.5	1.8	0	0		
00236>	STM-28-1001_1	RECT_OPEN	0.5	1.8	0	0		
00237>	STM-46-2000_1	RECT_OPEN	0.5	1.8	0	0		
00238>	STM-90-3000_1	RECT_OPEN	0.5	1.8	0	0		

00240>	[LOSSES]					
00241>	;;Link	Kentry	Kexit	Kavg	Flap Gate	Seepage
00242>	;;					
00243>	1	0	4	0	NO	0
00244>	2	0	1.33	0	NO	0
00245>	3	0	4	0	NO	0
00246>	4	0	1.33	0	NO	0
00247>	5	0	4	0	NO	0
00248>	6	0	1.33	0	NO	0
00249>	7	0	4	0	NO	0
00250>	8	0	1.33	0	NO	0
00251>	STM-100-101	0	0.035	0	NO	0
00252>	STM-10-11	0	0.035	0	NO	0
00253>	STM-101-102	0	0.02	0	NO	0
00254>	STM-102-103	0	0.02	0	NO	0
00255>	STM-103-106	0	1.33	0	NO	0
00256>	STM-106-108	0	1.33	0	NO	0
00257>	STM-108-109	0	0.32	0	NO	0
00258>	STM-109-110	0	0.32	0	NO	0
00259>	STM-110-121	0	0.95	0	NO	0
00260>	STM-11-12	0	0.16	0	NO	0
00261>	STM-12-13	0	0.39	0	NO	0
00262>	STM-13-14	0	0.08	0	NO	0
00263>	STM-14-15	0	0.08	0	NO	0
00264>	STM-15-17	0	1.33	0	NO	0
00265>	STM-17-28	0	0.02	0	NO	0
00266>	STM-36-37	0	0.11	0	NO	0
00267>	STM-37-38	0	0.035	0	NO	0

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00268> STM-38-39      0      1.33      0      NO      0
00269> STM-39-40      0      0.02      0      NO      0
00270> STM-40-41      0      0.47      0      NO      0
00271> STM-41-42      0      0.39      0      NO      0
00272> STM-42-46      0      0.02      0      NO      0
00273> STM-570-97    0      0.02      0      NO      0
00274> STM-60-61      0      0.21      0      NO      0
00275> STM-61-62      0      1.33      0      NO      0
00276> STM-62-65      0      1.33      0      NO      0
00277> STM-65-67      0      0.02      0      NO      0
00278> STM-67-69      0      0.02      0      NO      0
00279> STM-69-70      0      1.33      0      NO      0
00280> STM-70-72      0      1.33      0      NO      0
00281> STM-72-76      0      0.035     0      NO      0
00282> STM-76-81      0      1.33      0      NO      0
00283> STM-81-82      0      1.33      0      NO      0
00284> STM-82-83      0      0.39      0      NO      0
00285> STM-83-84      0      0.39      0      NO      0
00286> STM-84-90      0      1.33      0      NO      0
00287> STM-9-10       0      0.02      0      NO      0
00288> STM-97-98      0      0.02      0      NO      0
00289> STM-98-99      0      1.33      0      NO      0
00290> STM-99-100     0      1.33      0      NO      0
00291>
00292> [INFLOWS]
00293> ;;Node

```

Node	Constituent	Time Series	Type	Mfactor	Sfactor	Baseline	Pattern
00295> MH-10	FLOW	" "	FLOW	1.0	1	61	
00296> MH-100	FLOW	" "	FLOW	1.0	1	192	
00297> MH-101	FLOW	" "	FLOW	1.0	1	120	
00298> MH-102	FLOW	" "	FLOW	1.0	1	62	
00299> MH-103	FLOW	" "	FLOW	1.0	1	52	
00300> MH-106	FLOW	" "	FLOW	1.0	1	81	
00301> MH-108	FLOW	" "	FLOW	1.0	1	46	
00302> MH-11	FLOW	" "	FLOW	1.0	1	19	
00303> MH-121	FLOW	" "	FLOW	1.0	1	227	
00304> MH-13	FLOW	" "	FLOW	1.0	1	2	
00305> MH-17	FLOW	" "	FLOW	1.0	1	36	
00306> MH-28	FLOW	" "	FLOW	1.0	1	253	
00307> MH-37	FLOW	" "	FLOW	1.0	1	121	
00308> MH-38	FLOW	" "	FLOW	1.0	1	351	
00309> MH-39	FLOW	" "	FLOW	1.0	1	5	
00310> MH-40	FLOW	" "	FLOW	1.0	1	4	
00311> MH-41	FLOW	" "	FLOW	1.0	1	1	
00312> MH-42	FLOW	" "	FLOW	1.0	1	57	
00313> MH-46	FLOW	" "	FLOW	1.0	1	42	
00314> MH-570	FLOW	" "	FLOW	1.0	1	25	
00315> MH-61	FLOW	" "	FLOW	1.0	1	129	
00316> MH-62	FLOW	" "	FLOW	1.0	1	150	
00317> MH-65	FLOW	" "	FLOW	1.0	1	102	
00318> MH-67	FLOW	" "	FLOW	1.0	1	52	
00319> MH-69	FLOW	" "	FLOW	1.0	1	56	
00320> MH-70	FLOW	" "	FLOW	1.0	1	227	
00321> MH-72	FLOW	" "	FLOW	1.0	1	38	
00322> MH-76	FLOW	" "	FLOW	1.0	1	135	
00323> MH-81	FLOW	" "	FLOW	1.0	1	54	
00324> MH-82	FLOW	" "	FLOW	1.0	1	9	
00325> MH-9	FLOW	" "	FLOW	1.0	1	328	
00326> MH-90	FLOW	" "	FLOW	1.0	1	61	
00327> MH-97	FLOW	" "	FLOW	1.0	1	63	
00328> MH-98	FLOW	" "	FLOW	1.0	1	68	
00329> MH-99	FLOW	" "	FLOW	1.0	1	18	

```

00330>
00331> [REPORT]
00332> ;;Reporting Options
00333> INPUT YES
00334> CONTROLS NO
00335> SUBCATCHMENTS ALL
00336> NODES ALL
00337> LINKS ALL
00338>
00339> [TAGS]

```

```

00340> Node MH-10 MH
00341> Node MH-100 MH
00342> Node MH-101 MH
00343> Node MH-102 MH
00344> Node MH-103 MH
00345> Node MH-106 MH
00346> Node MH-108 MH
00347> Node MH-109 MH
00348> Node MH-11 MH
00349> Node MH-110 MH
00350> Node MH-12 MH
00351> Node MH-121 MH
00352> Node MH-13 MH
00353> Node MH-14 MH
00354> Node MH-15 MH
00355> Node MH-17 MH
00356> Node MH-28 MH

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```

00357> Node      MH-36      MH
00358> Node      MH-37      MH
00359> Node      MH-38      MH
00360> Node      MH-39      MH
00361> Node      MH-40      MH
00362> Node      MH-41      MH
00363> Node      MH-42      MH
00364> Node      MH-46      MH
00365> Node      MH-570     MH
00366> Node      MH-60      MH
00367> Node      MH-61      MH
00368> Node      MH-62      MH
00369> Node      MH-65      MH
00370> Node      MH-67      MH
00371> Node      MH-69      MH
00372> Node      MH-70      MH
00373> Node      MH-72      MH
00374> Node      MH-76      MH
00375> Node      MH-81      MH
00376> Node      MH-82      MH
00377> Node      MH-83      MH
00378> Node      MH-84      MH
00379> Node      MH-9       MH
00380> Node      MH-90      MH
00381> Node      MH-97      MH
00382> Node      MH-98      MH
00383> Node      MH-99      MH
00384> Node      MH-1001     MH
00385> Node      MH-2000     MH
00386> Node      MH-3000     MH
00387> Node      MH-4001     MH
00388>
00389> [MAP]
00390> DIMENSIONS      361167.0976      5012598.77375      362012.5884      5013304.82525
00391> UNITS            Meters
00392>
00393> [COORDINATES]
00394> ;;Node          X-Coord          Y-Coord
00395> ;;-----
00396> 1                361397.805          5012655.104
00397> 2                361514.378          5012694.566
00398> 3                361651.362          5012795.237
00399> 4                361972.422          5012832.031
00400> MH-10            361229.473          5012901.573
00401> MH-100           361770.387          5013075.776
00402> MH-101           361797.145          5013013.577
00403> MH-102           361821.057          5012958.819
00404> MH-103           361840.671          5012914.024
00405> MH-106           361859.784          5012870.375
00406> MH-108           361882.782          5012880.618
00407> MH-109           361903.056          5012834.317
00408> MH-11           361276.266          5012789.141
00409> MH-110           361913.458          5012828.108
00410> MH-12            361307.29           5012715.44
00411> MH-121           361972.037          5012832.911
00412> MH-13            361316.727          5012706.114
00413> MH-14            361348.591          5012703.619
00414> MH-15            361365.578          5012706.457
00415> MH-17            361374.51           5012710.416
00416> MH-28            361397.42           5012656.019
00417> MH-36            361274.201          5012939.975
00418> MH-37            361282.629          5012930.004
00419> MH-38            361331.549          5012812.424
00420> MH-39            361355.516          5012755.515
00421> MH-40            361414.729          5012780.453
00422> MH-41            361460.146          5012799.578
00423> MH-42            361472.228          5012794.652
00424> MH-46            361513.992          5012695.483
00425> MH-570           361657.22           5013191.185
00426> MH-60            361513.921          5013272.732
00427> MH-61            361513.285          5013262.473
00428> MH-62            361563.864          5013148.92
00429> MH-65            361523.763          5013131.057
00430> MH-67            361541.625          5013090.956
00431> MH-69            361559.487          5013050.854
00432> MH-70            361585.105          5012993.338
00433> MH-72            361642.459          5013019.665
00434> MH-76            361670.332          5012957.093
00435> MH-81            361693.64           5012902.065
00436> MH-82            361641.33           5012878.765
00437> MH-83            361668.398          5012814.088
00438> MH-84            361663.904          5012802.313
00439> MH-9             361205.529          5012959.106
00440> MH-90            361650.936          5012796.131
00441> MH-97            361675.279          5013150.488
00442> MH-98            361693.086          5013110.361
00443> MH-99            361718.45           5013053.203
00444> OGS1            361398.117          5012655.795
00445> OGS2            361514.896          5012695.296

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00446> OGS3          361650.404      5012795.416
00447> OGS4          361972.786      5012832.684
00448> MH-1001       361408.013      5012630.867
00449> MH-2000       361516.888      5012688.605
00450> MH-3000       361662.443      5012771.982
00451> MH-4001       361974.157      5012828.07
00452>
00453> [VERTICES]
00454> ;;Link          X-Coord          Y-Coord
00455> ;;-----
00456>
```

```

00001> [TITLE]
00002> ;;Project Title/Notes
00003>
00004> [OPTIONS]
00005> ;;Option          Value
00006> FLOW_UNITS         LPS
00007> INFILTRATION       HORTON
00008> FLOW_ROUTING       DYNWAVE
00009> LINK_OFFSETS       DEPTH
00010> MIN_SLOPE          0
00011> ALLOW_PONDING      NO
00012> SKIP_STEADY_STATE NO
00013>
00014> START_DATE         12/05/2022
00015> START_TIME         00:00:00
00016> REPORT_START_DATE 12/05/2022
00017> REPORT_START_TIME 00:00:00
00018> END_DATE           12/06/2022
00019> END_TIME           00:00:00
00020> SWEEP_START        01/01
00021> SWEEP_END          12/31
00022> DRY_DAYS           0
00023> REPORT_STEP        00:01:00
00024> WET_STEP           00:05:00
00025> DRY_STEP           00:05:00
00026> ROUTING_STEP       5
00027> RULE_STEP          00:00:00
00028>
00029> INERTIAL_DAMPING   PARTIAL
00030> NORMAL_FLOW_LIMITED BOTH
00031> FORCE_MAIN_EQUATION H-W
00032> VARIABLE_STEP     0.75
00033> LENGTHENING_STEP  0
00034> MIN_SURFAREA      0
00035> MAX_TRIALS         8
00036> HEAD_TOLERANCE    0.0015
00037> SYS_FLOW_TOL      5
00038> LAT_FLOW_TOL      5
00039> MINIMUM_STEP      0.5
00040> THREADS            6
00041>
00042> [FILES]
00043> ;;Interfacing Files
00044> USE HOTSTART "C:\OneDrive\J.F. Sabourin and Associates Inc\JFSA-OTTAWA-SERVER - Documents\PROJ\1474(03)-21\202
00045>
00046> [EVAPORATION]
00047> ;;Data Source      Parameters
00048> ;;-----
00049> CONSTANT           0.0
00050> DRY_ONLY           NO
00051>
00052> [JUNCTIONS]
00053> ;;Name             Elevation  MaxDepth  InitDepth  SurDepth  Aponded
00054> ;;-----
00055> 1                  89.599    3.33      0           0           0
00056> 2                  89.577    3.192     0           0           0
00057> 3                  89.489    3.26      0           0           0
00058> 4                  89.355    3.164     0           0           0
00059> MH-10             90.377    3.053     0           0           0
00060> MH-100            90.279    2.781     0           0           0
00061> MH-101            90.13     2.76      0           0           0
00062> MH-102            89.989    2.861     0           0           0
00063> MH-103            89.915    2.875     0           0           0
00064> MH-106            89.788    2.922     0           0           0
00065> MH-108            89.7      2.97      0           0           0
00066> MH-109            89.614    2.976     0           0           0
00067> MH-11             90.223    3.017     0           0           0
00068> MH-110            89.571    3.009     0           0           0
00069> MH-12             90.105    3.025     0           0           0
00070> MH-121            89.356    3.164     0           0           0
00071> MH-13             90.015    3.095     0           0           0
00072> MH-14             89.95     3.11      0           0           0
00073> MH-15             89.901    3.139     0           0           0
00074> MH-17             89.815    3.205     0           0           0
00075> MH-28             89.6      3.33      0           0           0
00076> MH-36             91.126    2.264     0           0           0
00077> MH-37             90.368    3.002     0           0           0
00078> MH-38             90.078    3.102     0           0           0
00079> MH-39             89.935    3.145     0           0           0
00080> MH-40             89.844    3.176     0           0           0
00081> MH-41             89.76     3.18      0           0           0
00082> MH-42             89.716    3.214     0           0           0
00083> MH-46             89.578    3.192     0           0           0
00084> MH-570            90.833    2.807     0           0           0
00085> MH-60             91.241    2.489     0           0           0
00086> MH-61             91.075    2.645     0           0           0
00087> MH-62             90.878    2.652     0           0           0
00088> MH-65             90.755    2.715     0           0           0
00089> MH-67             90.632    2.768     0           0           0

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00090>	MH-69	90.509	2.821	0	0	0
00091>	MH-70	90.29	2.95	0	0	0
00092>	MH-72	90.071	3.079	0	0	0
00093>	MH-76	89.966	3.074	0	0	0
00094>	MH-81	89.84	3.11	0	0	0
00095>	MH-82	89.717	3.173	0	0	0
00096>	MH-83	89.61	3.18	0	0	0
00097>	MH-84	89.566	3.204	0	0	0
00098>	MH-9	90.466	3.054	0	0	0
00099>	MH-90	89.49	3.26	0	0	0
00100>	MH-97	90.746	2.424	0	0	0
00101>	MH-98	90.66	2.45	0	0	0
00102>	MH-99	90.416	2.594	0	0	0
00103>	OGS1	89.599	3.331	0	0	0
00104>	OGS2	89.577	3.193	0	0	0
00105>	OGS3	89.489	3.261	0	0	0
00106>	OGS4	89.355	3.165	0	0	0

00107>

00108> [OUTFALLS]

;;Name	Elevation	Type	Stage Data	Gated	Route To
00111>	MH-1001	89.57	FIXED	91.35	NO
00112>	MH-2000	89.57	FIXED	91.3	NO
00113>	MH-3000	89.46	FIXED	91.3	NO
00114>	MH-4001	89.35	FIXED	91.17	NO

00115>

00116> [CONDUITS]

;;Name	From Node	To Node	Length	Roughness	InOffset	OutOffset	InitFlow	MaxF
00119>	1	MH-28	OGS1	0.735	0.013	0	0	0
00120>	2	OGS1	1	0.753	0.013	0	0	0
00121>	3	MH-46	OGS2	0.93	0.013	0	0	0
00122>	4	OGS2	2	0.9	0.013	0	0	0
00123>	5	MH-90	OGS3	0.89	0.013	0	0	0
00124>	6	OGS3	3	0.977	0.013	0	0	0
00125>	7	MH-121	OGS4	0.782	0.013	0	0	0
00126>	8	OGS4	4	0.747	0.013	0	0	0
00127>	STM-100-101	MH-100	MH-101	67.5	0.013	0	0.075	0
00128>	STM-10-11	MH-10	MH-11	122	0.013	0	0.02	0
00129>	STM-101-102	MH-101	MH-102	60	0.013	0	0.075	0
00130>	STM-102-103	MH-102	MH-103	49	0.013	0	0.02	0
00131>	STM-103-106	MH-103	MH-106	47.5	0.013	0	0.075	0
00132>	STM-106-108	MH-106	MH-108	25	0.013	0	0.06	0
00133>	STM-108-109	MH-108	MH-109	50.5	0.013	0	0.03	0
00134>	STM-109-110	MH-109	MH-110	12	0.013	0	0.03	0
00135>	STM-110-121	MH-110	MH-121	59	0.013	0	0.15	0
00136>	STM-11-12	MH-11	MH-12	80	0.013	0	0.03	0
00137>	STM-12-13	MH-12	MH-13	13.5	0.013	0	0.075	0
00138>	STM-121-4001_2	4	MH-4001	4.324	0.013	0	0	0
00139>	STM-13-14	MH-13	MH-14	32	0.013	0	0.03	0
00140>	STM-14-15	MH-14	MH-15	17	0.013	0	0.03	0
00141>	STM-15-17	MH-15	MH-17	10	0.013	0	0.075	0
00142>	STM-17-28	MH-17	MH-28	59	0.013	0	0.15	0
00143>	STM-28-1001_2	1	MH-1001	26.301	0.013	0	0	0
00144>	STM-36-37	MH-36	MH-37	13	0.013	0	0.719	0
00145>	STM-37-38	MH-37	MH-38	127.5	0.013	0	0.15	0
00146>	STM-38-39	MH-38	MH-39	62	0.013	0	0.075	0
00147>	STM-39-40	MH-39	MH-40	64.5	0.013	0	0.02	0
00148>	STM-40-41	MH-40	MH-41	49.5	0.013	0	0.03	0
00149>	STM-41-42	MH-41	MH-42	13	0.013	0	0.03	0
00150>	STM-42-46	MH-42	MH-46	107.5	0.013	0	0.02	0
00151>	STM-46-2000_2	2	MH-2000	6.468	0.013	0	0	0
00152>	STM-570-97	MH-570	MH-97	44.5	0.013	0	0.02	0
00153>	STM-60-61	MH-60	MH-61	10.5	0.013	0	0.15	0
00154>	STM-61-62	MH-61	MH-62	124.5	0.013	0	0.06	0
00155>	STM-62-65	MH-62	MH-65	44	0.013	0	0.075	0
00156>	STM-65-67	MH-65	MH-67	44	0.013	0	0.075	0
00157>	STM-67-69	MH-67	MH-69	44	0.013	0	0.075	0
00158>	STM-69-70	MH-69	MH-70	63	0.013	0	0.15	0
00159>	STM-70-72	MH-70	MH-72	63	0.013	0	0.15	0
00160>	STM-72-76	MH-72	MH-76	68.5	0.013	0	0.03	0
00161>	STM-76-81	MH-76	MH-81	60	0.013	0	0.06	0
00162>	STM-81-82	MH-81	MH-82	57.5	0.013	0	0.06	0
00163>	STM-82-83	MH-82	MH-83	70	0.013	0	0.03	0
00164>	STM-83-84	MH-83	MH-84	12.5	0.013	0	0.03	0
00165>	STM-84-90	MH-84	MH-90	14.5	0.013	0	0.06	0
00166>	STM-90-3000_2	3	MH-3000	25.761	0.013	0	0	0
00167>	STM-9-10	MH-9	MH-10	62.5	0.013	0	0.02	0
00168>	STM-97-98	MH-97	MH-98	44	0.013	0	0.02	0
00169>	STM-98-99	MH-98	MH-99	62.5	0.013	0	0.15	0
00170>	STM-99-100	MH-99	MH-100	56.5	0.013	0	0.075	0

00171>

00172> [WEIRS]

;;Name	From Node	To Node	Type	CrestHt	Qcoeff	Gated	EndCon	EndCoe	
00175>	STM-121-4001_1	MH-121	4	TRANSVERSE	0.66	1.8	NO	0	2
00176>	STM-28-1001_1	MH-28	1	TRANSVERSE	0.66	1.8	NO	0	2
00177>	STM-46-2000_1	MH-46	2	TRANSVERSE	0.65	1.8	NO	0	2
00178>	STM-90-3000_1	MH-90	3	TRANSVERSE	0.66	1.8	NO	0	2

00181>	;;Link	Shape	Geom1	Geom2	Geom3	Geom4	Barrels	Culvert
00182>	;;							
00183>	1	CIRCULAR	0.75	0	0	0	1	
00184>	2	CIRCULAR	0.75	0	0	0	1	
00185>	3	CIRCULAR	0.675	0	0	0	1	
00186>	4	CIRCULAR	0.675	0	0	0	1	
00187>	5	CIRCULAR	0.75	0	0	0	1	
00188>	6	CIRCULAR	0.75	0	0	0	1	
00189>	7	CIRCULAR	0.75	0	0	0	1	
00190>	8	CIRCULAR	0.75	0	0	0	1	
00191>	STM-100-101	CIRCULAR	0.825	0	0	0	1	
00192>	STM-10-11	CIRCULAR	0.825	0	0	0	1	
00193>	STM-101-102	CIRCULAR	0.9	0	0	0	1	
00194>	STM-102-103	CIRCULAR	0.975	0	0	0	1	
00195>	STM-103-106	CIRCULAR	0.975	0	0	0	1	
00196>	STM-106-108	CIRCULAR	1.05	0	0	0	1	
00197>	STM-108-109	CIRCULAR	1.05	0	0	0	1	
00198>	STM-109-110	CIRCULAR	1.05	0	0	0	1	
00199>	STM-110-121	CIRCULAR	1.05	0	0	0	1	
00200>	STM-11-12	CIRCULAR	0.825	0	0	0	1	
00201>	STM-12-13	CIRCULAR	0.825	0	0	0	1	
00202>	STM-121-4001_2	CIRCULAR	1.2	0	0	0	1	
00203>	STM-13-14	CIRCULAR	0.9	0	0	0	1	
00204>	STM-14-15	CIRCULAR	0.9	0	0	0	1	
00205>	STM-15-17	CIRCULAR	0.9	0	0	0	1	
00206>	STM-17-28	CIRCULAR	0.9	0	0	0	1	
00207>	STM-28-1001_2	CIRCULAR	1.05	0	0	0	1	
00208>	STM-36-37	CIRCULAR	0.375	0	0	0	1	
00209>	STM-37-38	CIRCULAR	0.75	0	0	0	1	
00210>	STM-38-39	CIRCULAR	0.9	0	0	0	1	
00211>	STM-39-40	CIRCULAR	0.975	0	0	0	1	
00212>	STM-40-41	CIRCULAR	0.975	0	0	0	1	
00213>	STM-41-42	CIRCULAR	0.975	0	0	0	1	
00214>	STM-42-46	CIRCULAR	0.975	0	0	0	1	
00215>	STM-46-2000_2	CIRCULAR	0.975	0	0	0	1	
00216>	STM-570-97	CIRCULAR	0.6	0	0	0	1	
00217>	STM-60-61	CIRCULAR	0.6	0	0	0	1	
00218>	STM-61-62	CIRCULAR	0.75	0	0	0	1	
00219>	STM-62-65	CIRCULAR	0.75	0	0	0	1	
00220>	STM-65-67	CIRCULAR	0.825	0	0	0	1	
00221>	STM-67-69	CIRCULAR	0.9	0	0	0	1	
00222>	STM-69-70	CIRCULAR	0.9	0	0	0	1	
00223>	STM-70-72	CIRCULAR	1.05	0	0	0	1	
00224>	STM-72-76	CIRCULAR	1.2	0	0	0	1	
00225>	STM-76-81	CIRCULAR	1.2	0	0	0	1	
00226>	STM-81-82	CIRCULAR	1.2	0	0	0	1	
00227>	STM-82-83	CIRCULAR	1.2	0	0	0	1	
00228>	STM-83-84	CIRCULAR	1.2	0	0	0	1	
00229>	STM-84-90	CIRCULAR	1.2	0	0	0	1	
00230>	STM-90-3000_2	CIRCULAR	1.2	0	0	0	1	
00231>	STM-9-10	CIRCULAR	0.825	0	0	0	1	
00232>	STM-97-98	CIRCULAR	0.6	0	0	0	1	
00233>	STM-98-99	CIRCULAR	0.6	0	0	0	1	
00234>	STM-99-100	CIRCULAR	0.75	0	0	0	1	
00235>	STM-121-4001_1	RECT_OPEN	0.5	1.8	0	0		
00236>	STM-28-1001_1	RECT_OPEN	0.5	1.8	0	0		
00237>	STM-46-2000_1	RECT_OPEN	0.5	1.8	0	0		
00238>	STM-90-3000_1	RECT_OPEN	0.5	1.8	0	0		

00240>	[LOSSES]					
00241>	;;Link	Kentry	Kexit	Kavg	Flap Gate	Seepage
00242>	;;					
00243>	1	0	4	0	NO	0
00244>	2	0	1.33	0	NO	0
00245>	3	0	4	0	NO	0
00246>	4	0	1.33	0	NO	0
00247>	5	0	4	0	NO	0
00248>	6	0	1.33	0	NO	0
00249>	7	0	4	0	NO	0
00250>	8	0	1.33	0	NO	0
00251>	STM-100-101	0	0.035	0	NO	0
00252>	STM-10-11	0	0.035	0	NO	0
00253>	STM-101-102	0	0.02	0	NO	0
00254>	STM-102-103	0	0.02	0	NO	0
00255>	STM-103-106	0	1.33	0	NO	0
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00257>	STM-108-109	0	0.32	0	NO	0
00258>	STM-109-110	0	0.32	0	NO	0
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00260>	STM-11-12	0	0.16	0	NO	0
00261>	STM-12-13	0	0.39	0	NO	0
00262>	STM-13-14	0	0.08	0	NO	0
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00264>	STM-15-17	0	1.33	0	NO	0
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00267>	STM-37-38	0	0.035	0	NO	0


```

00268> STM-38-39      0      1.33      0      NO      0
00269> STM-39-40      0      0.02      0      NO      0
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00271> STM-41-42      0      0.39      0      NO      0
00272> STM-42-46      0      0.02      0      NO      0
00273> STM-570-97    0      0.02      0      NO      0
00274> STM-60-61      0      0.21      0      NO      0
00275> STM-61-62      0      1.33      0      NO      0
00276> STM-62-65      0      1.33      0      NO      0
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00283> STM-81-82      0      1.33      0      NO      0
00284> STM-82-83      0      0.39      0      NO      0
00285> STM-83-84      0      0.39      0      NO      0
00286> STM-84-90      0      1.33      0      NO      0
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00288> STM-97-98       0      0.02      0      NO      0
00289> STM-98-99       0      1.33      0      NO      0
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```

```

00292> [INFLOWS]
00293> ;;Node
00294> ;;-----
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00297> MH-101     FLOW      ""      FLOW      1.0      1      137
00298> MH-102     FLOW      ""      FLOW      1.0      1      71
00299> MH-103     FLOW      ""      FLOW      1.0      1      59
00300> MH-106     FLOW      ""      FLOW      1.0      1      92
00301> MH-108     FLOW      ""      FLOW      1.0      1      52
00302> MH-11      FLOW      ""      FLOW      1.0      1      22
00303> MH-121     FLOW      ""      FLOW      1.0      1      259
00304> MH-13      FLOW      ""      FLOW      1.0      1      2
00305> MH-17      FLOW      ""      FLOW      1.0      1      41
00306> MH-28      FLOW      ""      FLOW      1.0      1      288
00307> MH-37      FLOW      ""      FLOW      1.0      1      138
00308> MH-38      FLOW      ""      FLOW      1.0      1      400
00309> MH-39      FLOW      ""      FLOW      1.0      1      6
00310> MH-40      FLOW      ""      FLOW      1.0      1      5
00311> MH-41      FLOW      ""      FLOW      1.0      1      1
00312> MH-42      FLOW      ""      FLOW      1.0      1      65
00313> MH-46      FLOW      ""      FLOW      1.0      1      48
00314> MH-570     FLOW      ""      FLOW      1.0      1      29
00315> MH-61      FLOW      ""      FLOW      1.0      1      147
00316> MH-62      FLOW      ""      FLOW      1.0      1      171
00317> MH-65      FLOW      ""      FLOW      1.0      1      116
00318> MH-67      FLOW      ""      FLOW      1.0      1      59
00319> MH-69      FLOW      ""      FLOW      1.0      1      64
00320> MH-70      FLOW      ""      FLOW      1.0      1      259
00321> MH-72      FLOW      ""      FLOW      1.0      1      43
00322> MH-76      FLOW      ""      FLOW      1.0      1      154
00323> MH-81      FLOW      ""      FLOW      1.0      1      62
00324> MH-82      FLOW      ""      FLOW      1.0      1      10
00325> MH-9       FLOW      ""      FLOW      1.0      1      374
00326> MH-90      FLOW      ""      FLOW      1.0      1      70
00327> MH-97      FLOW      ""      FLOW      1.0      1      72
00328> MH-98      FLOW      ""      FLOW      1.0      1      78
00329> MH-99      FLOW      ""      FLOW      1.0      1      21
00330>

```

```

00331> [REPORT]
00332> ;;Reporting Options
00333> INPUT      YES
00334> CONTROLS   NO
00335> SUBCATCHMENTS ALL
00336> NODES     ALL
00337> LINKS     ALL
00338>

```

```

00339> [TAGS]
00340> Node      MH-10      MH
00341> Node      MH-100     MH
00342> Node      MH-101     MH
00343> Node      MH-102     MH
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00345> Node      MH-106     MH
00346> Node      MH-108     MH
00347> Node      MH-109     MH
00348> Node      MH-11      MH
00349> Node      MH-110     MH
00350> Node      MH-12      MH
00351> Node      MH-121     MH
00352> Node      MH-13      MH
00353> Node      MH-14      MH
00354> Node      MH-15      MH
00355> Node      MH-17      MH
00356> Node      MH-28      MH

```

```

00357> Node      MH-36      MH
00358> Node      MH-37      MH
00359> Node      MH-38      MH
00360> Node      MH-39      MH
00361> Node      MH-40      MH
00362> Node      MH-41      MH
00363> Node      MH-42      MH
00364> Node      MH-46      MH
00365> Node      MH-570     MH
00366> Node      MH-60      MH
00367> Node      MH-61      MH
00368> Node      MH-62      MH
00369> Node      MH-65      MH
00370> Node      MH-67      MH
00371> Node      MH-69      MH
00372> Node      MH-70      MH
00373> Node      MH-72      MH
00374> Node      MH-76      MH
00375> Node      MH-81      MH
00376> Node      MH-82      MH
00377> Node      MH-83      MH
00378> Node      MH-84      MH
00379> Node      MH-9       MH
00380> Node      MH-90      MH
00381> Node      MH-97      MH
00382> Node      MH-98      MH
00383> Node      MH-99      MH
00384> Node      MH-1001     MH
00385> Node      MH-2000     MH
00386> Node      MH-3000     MH
00387> Node      MH-4001     MH
00388>
00389> [MAP]
00390> DIMENSIONS      361167.0976      5012598.77375      362012.5884      5013304.82525
00391> UNITS            Meters
00392>
00393> [COORDINATES]
00394> ;;Node          X-Coord          Y-Coord
00395> ;;-----
00396> 1                361397.805          5012655.104
00397> 2                361514.378          5012694.566
00398> 3                361651.362          5012795.237
00399> 4                361972.422          5012832.031
00400> MH-10            361229.473          5012901.573
00401> MH-100           361770.387          5013075.776
00402> MH-101           361797.145          5013013.577
00403> MH-102           361821.057          5012958.819
00404> MH-103           361840.671          5012914.024
00405> MH-106           361859.784          5012870.375
00406> MH-108           361882.782          5012880.618
00407> MH-109           361903.056          5012834.317
00408> MH-11            361276.266          5012789.141
00409> MH-110           361913.458          5012828.108
00410> MH-12            361307.29           5012715.44
00411> MH-121           361972.037          5012832.911
00412> MH-13            361316.727          5012706.114
00413> MH-14            361348.591          5012703.619
00414> MH-15            361365.578          5012706.457
00415> MH-17            361374.51           5012710.416
00416> MH-28            361397.42           5012656.019
00417> MH-36            361274.201          5012939.975
00418> MH-37            361282.629          5012930.004
00419> MH-38            361331.549          5012812.424
00420> MH-39            361355.516          5012755.515
00421> MH-40            361414.729          5012780.453
00422> MH-41            361460.146          5012799.578
00423> MH-42            361472.228          5012794.652
00424> MH-46            361513.992          5012695.483
00425> MH-570           361657.22           5013191.185
00426> MH-60            361513.921          5013272.732
00427> MH-61            361513.285          5013262.473
00428> MH-62            361563.864          5013148.92
00429> MH-65            361523.763          5013131.057
00430> MH-67            361541.625          5013090.956
00431> MH-69            361559.487          5013050.854
00432> MH-70            361585.105          5012993.338
00433> MH-72            361642.459          5013019.665
00434> MH-76            361670.332          5012957.093
00435> MH-81            361693.64           5012902.065
00436> MH-82            361641.33           5012878.765
00437> MH-83            361668.398          5012814.088
00438> MH-84            361663.904          5012802.313
00439> MH-9             361205.529          5012959.106
00440> MH-90            361650.936          5012796.131
00441> MH-97            361675.279          5013150.488
00442> MH-98            361693.086          5013110.361
00443> MH-99            361718.45           5013053.203
00444> OGS1            361398.117          5012655.795
00445> OGS2            361514.896          5012695.296

```

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00446> OGS3          361650.404      5012795.416
00447> OGS4          361972.786      5012832.684
00448> MH-1001       361408.013      5012630.867
00449> MH-2000       361516.888      5012688.605
00450> MH-3000       361662.443      5012771.982
00451> MH-4001       361974.157      5012828.07
00452>
00453> [VERTICES]
00454> ;;Link          X-Coord          Y-Coord
00455> ;;-----
00456>
```


December 13, 2022

Project Number: 1474

David Schaeffer Engineering Ltd
120 Iber Road, Unit 103
Ottawa, Ontario
K2S 1E9

Attention: Kevin Murphy, P.Eng

Subject: Barrhaven Conservancy West – Preliminary Water Balance

Introduction

Barrhaven Conservancy West Development is located in Barrhaven, Ontario, north of the Jock River, east of Highway 416 and west of the Foster Drain. The proposed development is approximately **34.15 ha** that will primarily comprise of single and townhouse residential lots. The following memo outlines how the proposed development will match/exceed the existing water budget through the use of LIDs.

Water Balance Overview

A pre-and post-development water balance has been completed for the site based on continuous hydrologic model simulations. As such a SWMHYMO model was developed that reflects the hydrologic conditions of these lands under pre-development, post-development without LIDs and post-development with LIDs conditions. These models were run using 36 years of hourly rainfall data from the Ottawa International Airport from 1967 to 2003 (excluding 2001 - missing rainfall data), and the average annual runoff volumes from the subject site were computed and compared. **Table A1 in Attachment A** outlines the continuous modelling parameters for both pre and post-development conditions. The following section outlines the modelling approach for each scenario and the results of this analysis.

Pre-Development

Based on the Soil Survey Complex mapping from the Ontario Ministry of Agriculture, Food, and Rural Affairs (OMAFRA) the site primarily consists of Carsonby - Silt (Type C) and Brandon -Silty Clay- (Type D) Soils. This was confirmed by Paterson Groups through onsite field investigations and boreholes which also reported Silt and Silty Clays through the majority of the site.

Based on the Southern Ontario Land Resource Information System (SOLRIS) the site consists primarily of tilled lands and hedgerows. Based on the underlying Land Use Type and Soil Classification at each location within a subcatchment, a Curve Number (CN) was calculated, based on applicable values outlined in **Tables A2 and A3** in the SWMHYMO Manual. Each Curve Number was then weighted based on the total area within the subcatchment to determine the weighted CN for that subcatchment. The CN value calculated was then converted to CN*, as CN* values have been shown to correlate well with measured flows and perform well in continuous SWMHYMO modelling (as discussed in the July 1989 INTERHYMO / OTTHYMO 89 Manual), when compared to conventional CN. Full details of the derivation of CN under existing conditions have been outlined in **Table A2 and Figures A1 & A2 in Attachment A**.

For this area, the time to peak (T_p) has been calculated based on existing topography. Flow paths have been discretized based on the topographic data using GIS tools and the longest major flow path within the subcatchment identified; refer to **Figure A3 in Attachment A** for the flow paths discretized for these lands. The upstream and downstream topographic elevations and flow lengths were identified for this subcatchment and used in the calculations. For these lands, the Federal Aviation Administration (FAA) method was determined to be the most appropriate method to calculate the T_p . Full details of these calculations have been provided in **Table A3 in Attachment A**, along with other time-to-peak values using alternative T_p calculation methods. This site under pre-development conditions has been represented in SWMHYMO using a CONTINUOUS NASHYD command, with all continuous parameters outlined in **Table A1 of Attachment A**. Note that the pre-development areas have been represented as 2 individual areas (east and west of the Okeefe drain) with the results of both areas added together to provide the full site pre-development water budget.

Post-Development – Without LIDs

Under post-development conditions, the site will have 4 individual storm sewer outlets, as such the development lands have been broken into these 4 discrete areas (with a total drainage area of 34.15 ha, matching existing conditions). Based on the development conceptual plan, the 34.15 ha site will have a total imperviousness of 68%, see figure A4 in Attachment A for an overview of the proposed development plan. These developed lands have been represented using CONTINUOUS STANDHYD commands in SWMHYMO. This scenario has been provided to quantify the average annual reduction in infiltration volume throughout the site due to the increase in impervious area.

In order to best represent infiltration over a long simulation period, and to provide a consistent comparison between pre- and post-development conditions, the SCS procedure was used to simulate infiltration over the subject site for both pre-and post-development conditions. Under post-development conditions, soils in the development areas will be defined by the characteristics of topsoil, which has a CN of 79 ($CN^* = 71$) for urban lawns in fair condition.

Post-Development – With LIDs

As mentioned above the proposed development will have LIDs implemented throughout the site to offset any deficit in annual infiltration volume produced by the increase in the impervious area due to the development. For this analysis, it is assumed that the development will have infiltration LIDs implemented at the road catch basins. Runoff captured by the road catch basins will be directed to an infiltration trench, where it can infiltrate before discharging to the storm sewer system (see *Figure 5* in *DSEL Figures & Drawings* package for more details about the proposed LID configuration). A conceptual design of these LIDs systems has been completed but will be refined at detailed design when detailed grading is available, to yield optimal benefit from this LID approach. **Table 1** below outlines the parameters of these conceptual LIDs based on the current development plan. Each of the LID clusters have been represented in the model as single lumped ROUTE RESERVOIR commands, with the outflow of each command reflective of the soil infiltration rate and the volume reflective of the storage volume within each LID.

Soil Infiltration & Draw Down Time

Based on the Paterson Groups' geotechnical Investigation, the site consists of soil that typically has infiltration rates in the range of **9 mm/hr - 25 mm/hr**. As such it has been assumed that this site will have an infiltration rate of 9mm/hr with a safety factor of 2.5 (3.6 mm/hr). Based on a trench height of 0.4 m (with a void ratio of 0.4) these trenches will have a draw downtime of approximately **45 hours**. Note that in this analysis it is assumed that only the bottom of the trench can infiltrate, which is a conservative assumption.

Table 1: Proposed LID Summary

Parameter	OGS W1	OGS W2	OGS W3	OGS W4
Area (ha)	8.92	10.75	6.30	8.18
Runoff Coefficient	0.7	0.69	0.64	0.67
Total Imperviousness (%)	71	70	63	67
Pipe Length (m)	2028	2317	1098	1519
Pipe Dia (mm)	250	250	250	250
Perf. Pipe Length (m)	780	870	420	570
Pipe Vol. (m ³)	38.29	42.71	20.62	27.98
Trench Width (m)	1.25	1.25	1.25	1.25
Trench Height (m)	0.4	0.4	0.4	0.4
Trench Length (m)	30	30	30	30
Void Ratio	0.4	0.4	0.4	0.4
Trench Vol. (m ³)	140.68	156.92	75.75	102.81
Total Vol. (m ³)	179	200	96	131
Area of Trench (m ²)	975.00	1087.50	525.00	712.50
# of CB's	26	29	14	19
Soil Infiltration Rate (mm/hr)	9	9	9	9
Safety Factor	2.5	2.5	2.5	2.5
Reduced Rate (mm/hr)	3.6	3.6	3.6	3.6
Infiltration rate (m ³ /s)	0.0010	0.0011	0.0005	0.0007

Water Budget Scenario Summary

The models were run for 36 years using hourly rainfall data from the Ottawa Airport, and the annual evaporation, infiltration and runoff volumes calculated for each scenario. Tables 2-4 summarize the annual average water balance under existing conditions and post-development conditions for the proposed development lands with and without LID measures in place, as m³/year, mm/year and % of total annual rainfall.

Table 2:Pre-Development Water Balance

Drainage Area (ha)		34.15	Imperviousness:	7%
Annual Average Volume	Precipitation	Evapotranspiration	Runoff	Infiltration
m ³	203,451	116,566	25,635	61,251
mm	596	341	75	179
%	100%	57.3%	12.6%	30.1%

Table 3:Post Development Water Balance – Without LIDs

Drainage Area (ha)		34.15	Imperviousness:	68%
Annual Average Volume	Precipitation	Evapotranspiration	Runoff	Infiltration
m ³	203,451	71,209	104,433	27,810
mm	596	209	306	81
%	100.0%	35.0%	51.3%	13.7%

Table 4:Post Development Water Balance – With LIDs

Drainage Area (ha)		34.15	Imperviousness:	68%
Annual Average Volume	Precipitation	Evapotranspiration	Runoff	Infiltration
m ³	203,451	71,209	79,285	52,957
mm	596	209	232	155
%	100%	35.0%	39.0%	26.0%

Based on this analysis of pre-development conditions, this site will evaporate **57.3%**, runoff **12.6%** and infiltrate **30.1%** of all annual rainfall. Under post-development conditions without LIDs, this site will evaporate **35.0%**, runoff **51.3%** and infiltrate **13.7%** of all annual rainfall, resulting in a deficit of 98 mm/year infiltrated from pre-development conditions. Under post-development conditions with LIDs, this site will evaporate **35.0%**, runoff **39.0%** and infiltrate **26.0%** and of all annual rainfall, resulting in a deficit of 24 mm/year infiltrated from pre-development conditions. Full annual breakdowns of the three conditions have been provided in **Attachment B, Tables B1-B3**. An average annual summary of the infiltration volume for each of the proposed LID measures is outlined in **Table B4**, which shows that the LIDs alone provide a total average annual infiltration volume of **72 mm/year**.

Conclusion

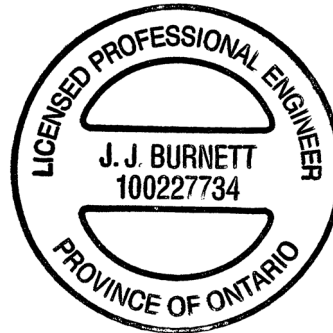
A preliminary water balance analysis of the existing site was completed to determine pre-development infiltration rates, based on continuous hydrologic model simulations. A post-development analysis for the site, where no LIDs were implemented, showed that the volume of annual rainfall infiltrated would decrease by **98 mm/yr. (-55% from existing)**. Implementing LIDs in the way of infiltration trenches connected to the catchbasins would reduce this deficit to **24 mm/year (-4.1% from existing)**. Based on the above it has been shown that the Barrhaven Conservancy West Developments will be able to meet pre-development infiltration rates within $\pm 5\%$ under post-development conditions through the use of LIDs.

Yours truly,
J.F Sabourin and Associates Inc.



Jonathon Burnett, P.Eng
Water Resources Engineer

cc: J.F Sabourin, M.Eng, P.Eng
Director of Water Resources Projects



Tables

- Table 1: Proposed LID Summary
- Table 2: Pre-Development Water Balance
- Table 3: Post Development Water Balance – Without LIDs
- Table 4: Post Development Water Balance – With LIDs

Attachments

- Attachment A: SWMHYMO Models & Parameters
- Attachment B: Water Budget Results

Modelling Files (Provided Electronically)

- SWMHYMO BCD_WEST-PRE_v02.dat
- BCD_WEST-POST_v02.dat



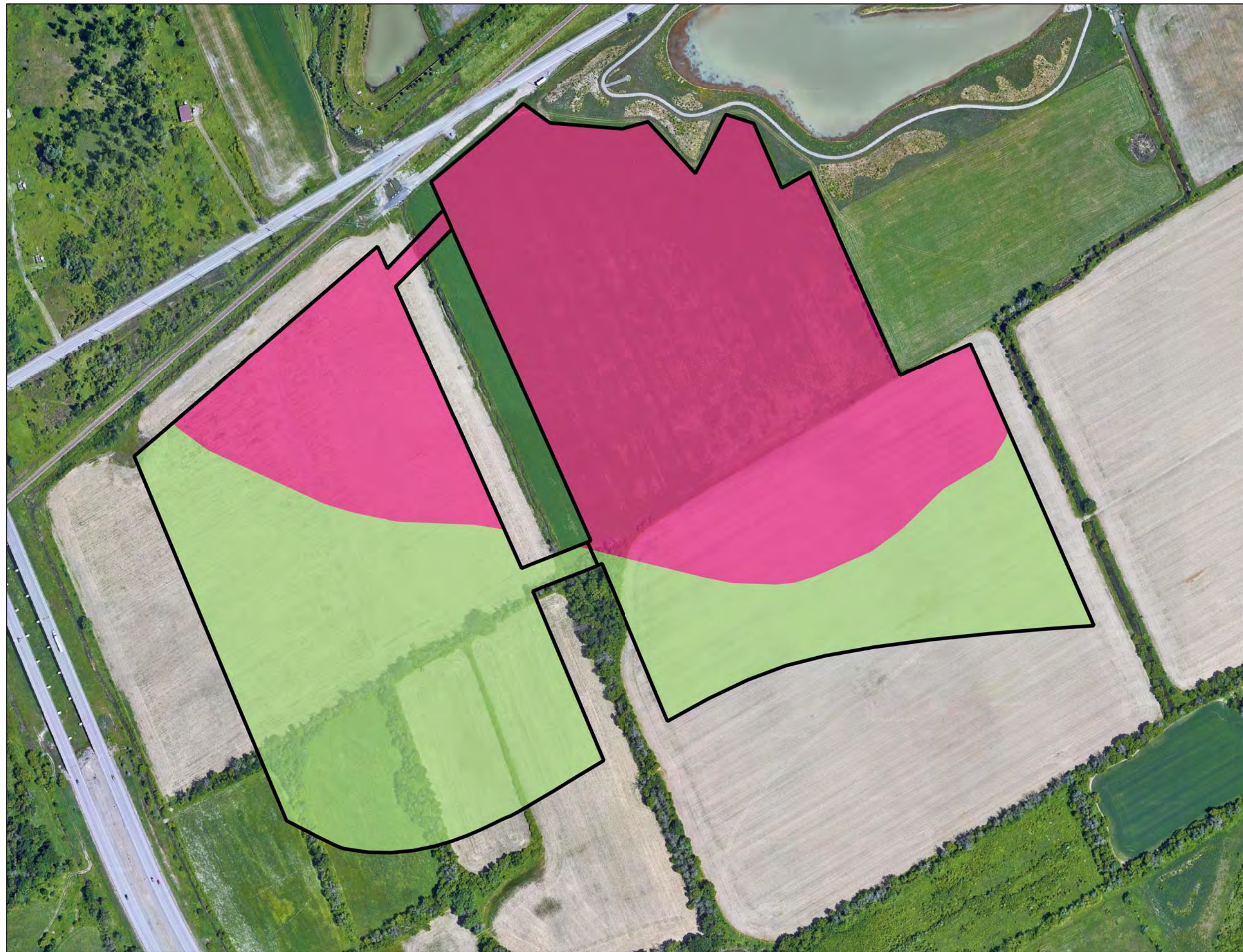
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Québec, QC

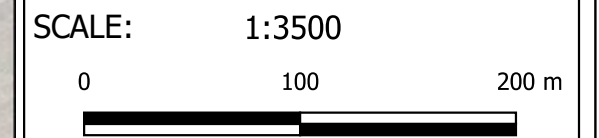
Attachment A

SWMHYMO Models & Parameters



Legend

- Development Area
- Soil Name (SCS Value)
- BRANDON (D)
- CARSONBY (C)



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Figure A1: Soil Types

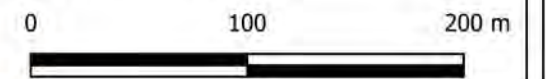
PROJECT	1474(03)
DRAWN	JB
DATE	Dec 2021




Legend

-  Development Area
- Land Use
-  Hedge Rows
-  Tilled

SCALE: 1:3500



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Figure A2: Land Use

PROJECT	1474(03)
---------	----------

DRAWN	JB
-------	----

DATE	Dec 2022
------	----------



Legend

- Flow Lengths
- Development Area
- Terrain (m)
- 90.5
- 91
- 91.5
- 92
- 92.5
- 93
- 93.5
- 94
- 94.5
- Contours (0.25m)

SCALE: 1:3500

0 100 200 m

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Figure A3: Flow Paths

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DRAWN	JB
DATE	Dec 2022



Legend

- Drainage Areas
 <Name>
 <Area (ha)>
 <Runoff Coefficient>
- Minor System

SCALE: 1:3500
 0 100 200 m

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DSEL
 david schaeffer engineering ltd

BCD Phase 3

Figure A4: Proposed Development

PROJECT	1474(03)
DRAWN	JB
DATE	Dec 2022

Table A1: Continuous Simulation Parameters

Parameter(s) & Value(s)	Description
APII=[50], APIK=[0.90]/day	Used to compute the Antecedent Precipitation Index during the continuous simulation. Without model calibration, these are the default values.
IAimp = [1.57](mm), IAper=[4.67](mm)	Default Initial Abstraction (IA) values per the City of Ottawa Design Guidelines
IaREC=[6](hrs);	The time that it takes for the Initial Abstraction over pervious areas to recover during a dry period in undeveloped areas.
SMIN=[-1], SMAX=[-1](mm)	The negative values indicate that the storage volume in the SCS procedure will vary between the "S" determined for AMC I and AMC III conditions of the entered CN value in undeveloped and urban areas.
SK=[0.03]/(mm);	A calibration coefficient that can typically vary from 0.01 to 0.3 for undeveloped and urban areas. The higher the value, the more runoff generated. To set the baseline for existing conditions, it was decided to take a value in the low range.
InitGWResVol=[10](mm), GWResK=[0.9](mm/day/mm), VhydCond=[1](mm/hr);	Parameters that are used to simulate both the groundwater storage and discharge to surface watercourses from undeveloped areas. Without adequate field measurements, these parameters were selected based on previous continuous modelling experience.
IaRECper=[6](hrs);	The time that it takes for the Initial Abstraction over pervious areas to recover during a dry period in urban areas.
IaRECimp=[1.5](hrs);	The time that it takes for the Initial Abstraction over impervious areas to recover during a dry period in urban areas.
InterEventTime=[12](hrs)	The continuous dry time is required to reset the parameters in the SCS procedure to their initial values.

Table A2: Calculation of SCS Curve Number (CN) and Modified Curve Number (CN*)

		West-A (19.67 ha)							
Name	Total Area (ha)	Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
West-A	19.67	14.842	Tilled	BRANDON	D	Fair	84	75.5%	63.4
West-A	19.67	0.068	Hedge Rows	CARSONBY	C	Fair	70	0.3%	0.2
West-A	19.67	0.034	Hedge Rows	BRANDON	D	Fair	77	0.2%	0.1
West-A	19.67	4.726	Tilled	CARSONBY	C	Fair	79	24.0%	19.0
								CN	82.7
								CN*	76

		West-B (14.48 ha)							
Name	Total Area (ha)	Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
West-B	14.48	1.154	Hedge Rows	CARSONBY	C	Fair	70	8.0%	5.6
West-B	14.48	9.06	Tilled	CARSONBY	C	Fair	79	62.6%	49.4
West-B	14.48	4.266	Tilled	BRANDON	D	Fair	84	29.5%	24.7
								CN	79.8
								CN*	72

Table A3: Time to Peak Calculations

Parameter	Units	West-A	West-B
Area	ha	19.67	14.48
CN*	-	76	72
Ptotal to calc C from CN, use 2 yr 12 hr SCS stom	P(mm)	43.2	43.2
	Ia(mm)	4.67	4.67
	RV(mm)	12.7	10.8
C	-	0.29	0.25
Length of Channel	m	619	541
	ft	2029	1776
Elevation of Head Water	m	92.07	91.52
	ft	302	300
Elevation of Outlet	m	90.96	90.31
	ft	298	296
Average Slope	m/m	0.18%	0.22%
	ft/ft	0.18%	0.22%
Kirpich			
Time of Concentration	mins	31	26
Time to Peak	min	21	17
Time to Peak	Hours	0.35	0.29
FAA			
Time of Concentration	mins	116	106
Time to Peak	mins	77	71
Time to Peak	Hours	1.29	1.18
Barnsby Williams			
Time of Concentration	mins	37	32
Time to Peak	mins	25	21
Time to Peak	Hours	0.41	0.36
SCS			
Time of Concentration	mins	148	134
Time to Peak	mins	98	90
Time to Peak	Hours	1.64	1.49
Selected Method			
FAA			
Time to Peak	min	77	71
Time to Peak	Hours	1.29	1.18

Note:

All methods calculated as per Appendix A of the SWMHYMO manual

Time to Peak calculated as 2/3 Time of concentration

```

00001> 20      Metric units / ID Numbers OFF
00002> *#*****
00003> *# SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00004> *#*****
00005> *# Project Name: Barrhaven Conservancy Development
00006> *# Project Number: 1474
00007> *# Date       : 2021/Oct/18
00008> *# Modeller  : J.Burnett, P.Eng.
00009> *# Updated   : 2022/Dec/07 [JB]
00010> *# Updated   : 2022/Dec/13 [LP]
00011> *# Company   : J.F. Sabourin and Associates
00012> *# License # : 2582634
00013> *#*****
00014> START      TZERO=[1967.0101], METOUT=[2], NSTORM=[0], NRUN=[67]
00015> *#         [""] <--storm filename, one per line for NSTORM time
00016> *#-----|-----
00017> *# Ottawa International Airport (1967 - 2003)
00018> READ AES DATA AES_FILENAME=["YOW_1967_2007.123"],
00019> IELEM=[123], START_DATE=[0], END_DATE=[-364]
00020> *#-----|-----
00021> COMPUTE API  APII=[50], APIK=[0.90]/day
00022> *#-----|-----
00023> *#*****
00024> *# Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00025> *#*****
00026> *#-----|-----
00027> CONTINUOUS NASHYD NHYD=["West-A"], DT=[5](min), AREA=[19.67](ha)
00028> DWF=[0](cms), CN/C=[76], IA=[4.67](mm), N=[3], TP=[1.29](hrs),
00029> Continuous simulation parameters:
00030> IaRECper=[6](hrs),SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.03]/(mm), InterEventTime=[12](hrs)
00031> Baseflow simulation parameters:
00032> BaseFlowOption=[1], InitGWResVol=[10](mm), GWResK=[0.9](mm/day/mm)
00033> VHydCond=[1.0](mm/hr), END=-1
00034> *#-----|-----
00035> CONTINUOUS NASHYD NHYD=["West-B"], DT=[5](min), AREA=[14.48](ha)
00036> DWF=[0](cms), CN/C=[72], IA=[4.67](mm), N=[3], TP=[1.18](hrs),
00037> Continuous simulation parameters:
00038> IaRECper=[6](hrs),SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.03]/(mm), InterEventTime=[12](hrs)
00039> Baseflow simulation parameters:
00040> BaseFlowOption=[1], InitGWResVol=[10](mm), GWResK=[0.9](mm/day/mm)
00041> VHydCond=[1.0](mm/hr), END=-1
00042> *#-----|-----
00043> ADD HYD      NHYDsum=["West-Total"], NHYDs to add=["West-A","West-B"]
00044> *#-----|-----
00045> *#*****
00046> *# Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITION
00047> *#*****
00048> *# Set infiltration to 0 (CN = 99.99) for water balance analysis
00049> *#*****
00050> CONTINUOUS NASHYD NHYD=["INF-West-A"], DT=[5](min), AREA=[19.67](ha)
00051> DWF=[0](cms), CN/C=[99.99], IA=[4.67](mm), N=[3], TP=[1.29](hrs),
00052> Continuous simulation parameters:
00053> IaRECper=[6](hrs),SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.03]/(mm), InterEventTime=[12](hrs)
00054> Baseflow simulation parameters:
00055> BaseFlowOption=[1], InitGWResVol=[10](mm), GWResK=[0.9](mm/day/mm)
00056> VHydCond=[1.0](mm/hr), END=-1
00057> *#-----|-----
00058> CONTINUOUS NASHYD NHYD=["INF-West-B"], DT=[5](min), AREA=[14.48](ha)
00059> DWF=[0](cms), CN/C=[99.99], IA=[4.67](mm), N=[3], TP=[1.18](hrs),
00060> Continuous simulation parameters:
00061> IaRECper=[6](hrs),SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.03]/(mm), InterEventTime=[12](hrs)
00062> Baseflow simulation parameters:
00063> BaseFlowOption=[1], InitGWResVol=[10](mm), GWResK=[0.9](mm/day/mm)
00064> VHydCond=[1.0](mm/hr), END=-1
00065> *#-----|-----
00066> ADD HYD      NHYDsum=["INF-West-Total"], NHYDs to add=["INF-West-A","INF-West-B"]
00067> *#-----|-----
00068> *#-----|-----
00069> *#*****
00070> *# CONTINUOUS RAINFALL DATA
00071> *#*****
00072> *#-----|-----
00073> *#-----|-----
00074> START      TZERO=[1968.0101], METOUT=[2], NSTORM=[0], NRUN=[68]
00075> *#-----|-----
00076> START      TZERO=[1969.0101], METOUT=[2], NSTORM=[0], NRUN=[69]
00077> *#-----|-----
00078> START      TZERO=[1970.0101], METOUT=[2], NSTORM=[0], NRUN=[70]
00079> *#-----|-----
00080> START      TZERO=[1971.0101], METOUT=[2], NSTORM=[0], NRUN=[71]
00081> *#-----|-----
00082> START      TZERO=[1972.0101], METOUT=[2], NSTORM=[0], NRUN=[72]
00083> *#-----|-----
00084> START      TZERO=[1973.0101], METOUT=[2], NSTORM=[0], NRUN=[73]
00085> *#-----|-----
00086> START      TZERO=[1974.0101], METOUT=[2], NSTORM=[0], NRUN=[74]
00087> *#-----|-----
00088> START      TZERO=[1975.0101], METOUT=[2], NSTORM=[0], NRUN=[75]
00089> *#-----|-----

```

```

00090> START                TZERO=[1976.0101], METOUT=[2], NSTORM=[0], NRUN=[76]
00091> *%-----|-----
00092> START                TZERO=[1977.0101], METOUT=[2], NSTORM=[0], NRUN=[77]
00093> *%-----|-----
00094> START                TZERO=[1978.0101], METOUT=[2], NSTORM=[0], NRUN=[78]
00095> *%-----|-----
00096> START                TZERO=[1979.0101], METOUT=[2], NSTORM=[0], NRUN=[79]
00097> *%-----|-----
00098> START                TZERO=[1980.0101], METOUT=[2], NSTORM=[0], NRUN=[80]
00099> *%-----|-----
00100> START                TZERO=[1981.0101], METOUT=[2], NSTORM=[0], NRUN=[81]
00101> *%-----|-----
00102> START                TZERO=[1982.0101], METOUT=[2], NSTORM=[0], NRUN=[82]
00103> *%-----|-----
00104> START                TZERO=[1983.0101], METOUT=[2], NSTORM=[0], NRUN=[83]
00105> *%-----|-----
00106> START                TZERO=[1984.0101], METOUT=[2], NSTORM=[0], NRUN=[84]
00107> *%-----|-----
00108> START                TZERO=[1985.0101], METOUT=[2], NSTORM=[0], NRUN=[85]
00109> *%-----|-----
00110> START                TZERO=[1986.0101], METOUT=[2], NSTORM=[0], NRUN=[86]
00111> *%-----|-----
00112> START                TZERO=[1987.0101], METOUT=[2], NSTORM=[0], NRUN=[87]
00113> *%-----|-----
00114> START                TZERO=[1988.0101], METOUT=[2], NSTORM=[0], NRUN=[88]
00115> *%-----|-----
00116> START                TZERO=[1989.0101], METOUT=[2], NSTORM=[0], NRUN=[89]
00117> *%-----|-----
00118> START                TZERO=[1990.0101], METOUT=[2], NSTORM=[0], NRUN=[90]
00119> *%-----|-----
00120> START                TZERO=[1991.0101], METOUT=[2], NSTORM=[0], NRUN=[91]
00121> *%-----|-----
00122> START                TZERO=[1992.0101], METOUT=[2], NSTORM=[0], NRUN=[92]
00123> *%-----|-----
00124> START                TZERO=[1993.0101], METOUT=[2], NSTORM=[0], NRUN=[93]
00125> *%-----|-----
00126> START                TZERO=[1994.0101], METOUT=[2], NSTORM=[0], NRUN=[94]
00127> *%-----|-----
00128> START                TZERO=[1995.0101], METOUT=[2], NSTORM=[0], NRUN=[95]
00129> *%-----|-----
00130> START                TZERO=[1996.0101], METOUT=[2], NSTORM=[0], NRUN=[96]
00131> *%-----|-----
00132> START                TZERO=[1997.0101], METOUT=[2], NSTORM=[0], NRUN=[97]
00133> *%-----|-----
00134> START                TZERO=[1998.0101], METOUT=[2], NSTORM=[0], NRUN=[98]
00135> *%-----|-----
00136> START                TZERO=[1999.0101], METOUT=[2], NSTORM=[0], NRUN=[99]
00137> *%-----|-----
00138> START                TZERO=[2000.0101], METOUT=[2], NSTORM=[0], NRUN=[100]
00139> *%-----|-----
00140> *% MISSING FROM AES RAINFALL DATA
00141> *%START                TZERO=[2001.0101], METOUT=[2], NSTORM=[0], NRUN=[101]
00142> *%-----|-----
00143> START                TZERO=[2002.0101], METOUT=[2], NSTORM=[0], NRUN=[102]
00144> *%-----|-----
00145> START                TZERO=[2003.0101], METOUT=[2], NSTORM=[0], NRUN=[103]
00146> *%-----|-----
00147> FINISH

```

```

00001> =====
00002>
00003> SSSSS W W M M H H Y Y M M OOO 222 000 11 5555 =====
00004> S W W W MM MM H H Y Y MM MM O O 2 0 0 11 5
00005> SSSSS W W W M M M HHHHH Y M M M O O 2 0 0 11 5 Ver 5.500
00006> S W W M M H H Y M M O O 222 0 0 11 555 FEB 2015
00007> SSSSS W W M M H H Y M M OOO 2 0 0 11 5 =====
00008> 2 0 0 11 5 # 2549237
00009> StormWater Management HYdrologic Model 222 000 11 555 =====
00010>
00011> *****
00012> ***** SWMHYMO Ver 5.500 *****
00013> ***** A single event and continuous hydrologic simulation model *****
00014> ***** based on the principles of HYMO and its successors *****
00015> ***** OTHYMO-83 and OTHYMO-89. *****
00016> *****
00017> ***** Distributed by: J.F. Sabourin and Associates Inc. *****
00018> ***** Ottawa, Ontario: (613) 836-3884 *****
00019> ***** Gatineau, Quebec: (819) 243-6858 *****
00020> ***** E-Mail: swmhymo@jfsa.Com *****
00021> *****
00022>
00023> ++++++
00024> ++++++ Licensed user: JFSAinc. ++++++
00025> ++++++ Ottawa SERIAL#:2549237 ++++++
00026> ++++++
00027>
00028> *****
00029> ***** ++++++ PROGRAM ARRAY DIMENSIONS ++++++ *****
00030> ***** Maximum value for ID numbers : 11 *****
00031> ***** Max. number of rainfall points: 105408 *****
00032> ***** Max. number of flow points : 105408 *****
00033> *****
00034>
00035>
00036> ***** S U M M A R Y O U T P U T *****
00037> *****
00038> * RUN DATE: 2022-12-13 TIME: 12:43:36 RUN COUNTER: 004324 *
00039> *****
00040> * Input file: C:\Users\lpipk\Desktop\20221213-Pre-Dev\BCD_WEST-PRE_v02.dat *
00041> * Output file: C:\Users\lpipk\Desktop\20221213-Pre-Dev\BCD_WEST-PRE_v02.out *
00042> * Summary file: C:\Users\lpipk\Desktop\20221213-Pre-Dev\BCD_WEST-PRE_v02.sum *
00043> * User comments: *
00044> * 1: _____ *
00045> * 2: _____ *
00046> * 3: _____ *
00047> *****
00048>
00049>
00050> #*****
00051> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00052> #*****
00053> # Project Name: Barrhaven Conservancy Development
00054> # Project Number: 1474
00055> # Date : 2021/Oct/18
00056> # Modeller : J.Burnett, P.Eng.
00057> # Updated : 2022/Dec/07 [JB]
00058> # Updated : 2022/Dec/13 [LP]
00059> # Company : J.F. Sabourin and Associates
00060> # License # : 2582634
00061> #*****
00062> ** END OF RUN : 66
00063>
00064> *****
00065>
00066>
00067>
00068>
00069>
00070> RUN#:COMMAND#
00071> R0067:C00001-----
00072> START
00073> [TZERO = .00 hrs on 19670101]
00074> [METOUT= 2 (1=imperial, 2=metric output)]
00075> [NSTORM= 0 ]
00076> [NRUN = 0067 ]
00077> #*****
00078> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00079> #*****
00080> # Project Name: Barrhaven Conservancy Development
00081> # Project Number: 1474
00082> # Date : 2021/Oct/18
00083> # Modeller : J.Burnett, P.Eng.
00084> # Updated : 2022/Dec/07 [JB]
00085> # Updated : 2022/Dec/13 [LP]
00086> # Company : J.F. Sabourin and Associates
00087> # License # : 2582634
00088> #*****
00089> # Ottawa International Airport (1967 - 2003)

```

```

00090> R0067:C00002-----
00091> * READ AES DATA
00092> [Filename = YOW_1967_2007.123 ]
00093> [Start_date= 1967.0101: End_date= 1967.1231]
00094> [DT= 60.min: Length= 3984.hrs: WetHrs= 257: DryHrs= 3727: PTOT= 386.90]
00095> Maximum average rainfall intensities over
00096> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00097> 24.60 17.65 13.20 7.25 3.83 2.36 1.73 1.32 .90 mm/hr
00098> 24.60 35.30 39.60 43.50 46.00 56.60 62.30 63.20 64.90 mm
00099> 19670921 19670921 19670921 19670921 19670921 19670922 19670922 19670923 19670924 date
00100> Number of rainfall events per following interevent time
00101> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00102> 80 65 56 40 32 29 24 20 18
00103> Number of events with at least the following durations
00104> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00105> 79 42 29 14 3 0 0 0 0
00106> R0067:C00003-----
00107> COMPUTE API
00108> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
00109> [APImax= 76.77: APIavg= 24.81: APImin= 3.06]
00110> #*****
00111> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00112> #*****
00113> R0067:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00114> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .214 1967.0921_19:10 70.91 .183 .000
00115> [CN= 76.0: N= 3.00: Tp= 1.29]
00116> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
00117> [InterEventTime= 12.00]
00118> R0067:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00119> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .143 1967.0921_18:55 63.09 .163 .000
00120> [CN= 72.0: N= 3.00: Tp= 1.18]
00121> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
00122> [InterEventTime= 12.00]
00123> R0067:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00124> ADD HYD 5.0 02:West-A 19.67 .214 1967.0921_19:10 70.91 n/a .000
00125> + 5.0 02:West-B 14.48 .143 1967.0921_18:55 63.09 n/a .000
00126> SUM= 5.0 01:West-Total 34.15 .356 1967.0921_19:05 67.59 n/a .000
00127> #*****
00128> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00129> #*****
00130> # Set infiltration to 0 (CN = 99.99) for water balance analysis
00131> #*****
00132> R0067:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00133> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .580 1967.0921_18:30 190.21 .492 .000
00134> [CN=100.0: N= 3.00: Tp= 1.29]
00135> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
00136> [InterEventTime= 12.00]
00137> R0067:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00138> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .450 1967.0921_18:25 190.21 .492 .000
00139> [CN=100.0: N= 3.00: Tp= 1.18]
00140> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
00141> [InterEventTime= 12.00]
00142> R0067:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00143> ADD HYD 5.0 02:INF-West-A 19.67 .580 1967.0921_18:30 190.21 n/a .000
00144> + 5.0 02:INF-West-B 14.48 .450 1967.0921_18:25 190.21 n/a .000
00145> SUM= 5.0 01:INF-West-T 34.15 1.028 1967.0921_18:30 190.21 n/a .000
00146> #####
00147> # CONTINUOUS RAINFALL DATA
00148> #####
00149> ** END OF RUN : 67
00150>
00151> *****
00152>
00153>
00154>
00155>
00156>
00157> RUN#:COMMAND#
00158> R0068:C00001-----
00159> START
00160> [TZERO = .00 hrs on 19680101]
00161> [METOUT= 2 (1=imperial, 2=metric output)]
00162> [NSTORM= 0 ]
00163> [NRUN = 0068 ]
00164> #*****
00165> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00166> #*****
00167> # Project Name: Barrhaven Conservancy Development
00168> # Project Number: 1474
00169> # Date : 2021/Oct/18
00170> # Modeller : J.Burnett, P.Eng.
00171> # Updated : 2022/Dec/07 [JB]
00172> # Updated : 2022/Dec/13 [LP]
00173> # Company : J.F. Sabourin and Associates
00174> # License # : 2582634
00175> #*****
00176> # Ottawa International Airport (1967 - 2003)
00177> R0068:C00002-----
00178> * READ AES DATA

```

```

00179> [Filename = YOW_1967_2007.123 ]
00180> [Start_date= 1968.0101: End_date= 1968.1230]
00181> [DT= 60.min: Length= 8760.hrs: WetHrs= 413: DryHrs= 8347: PTOT= 592.80]
00182> Maximum average rainfall intensities over
00183> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00184> 33.30 17.05 11.37 6.23 3.74 1.87 1.26 .95 .70 mm/hr
00185> 33.30 34.10 34.10 37.40 44.90 44.90 45.40 45.40 50.20 mm
00186> 19680817 19680817 19680817 19680808 19680817 19680818 19680817 19680808 19680820 date
00187> Number of rainfall events per following interevent time
00188> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00189> 137 105 93 84 72 63 48 43 36
00190> Number of events with at least the following durations
00191> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00192> 136 76 49 18 5 0 0 0 0
00193> R0068:C00003-----
00194> COMPUTE API
00195> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
00196> {APImax= 67.52: APIavg= 16.74: APImin= .27}
00197> #*****
00198> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00199> #*****
00200> R0068:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00201> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .213 1968.0817_ 6:05 77.11 .130 .000
00202> [CN= 76.0: N= 3.00: Tp= 1.29]
00203> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
00204> [InterEventTime= 12.00]
00205> R0068:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00206> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .149 1968.0817_ 6:00 67.82 .114 .000
00207> [CN= 72.0: N= 3.00: Tp= 1.18]
00208> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
00209> [InterEventTime= 12.00]
00210> R0068:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00211> ADD HYD 5.0 02:West-A 19.67 .213 1968.0817_ 6:05 77.11 n/a .000
00212> + 5.0 02:West-B 14.48 .149 1968.0817_ 6:00 67.82 n/a .000
00213> SUM= 5.0 01:West-Total 34.15 .361 1968.0817_ 6:00 73.17 n/a .000
00214> #*****
00215> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00216> #*****
00217> # Set infiltration to 0 (CN = 99.99) for water balance analysis
00218> #*****
00219> R0068:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00220> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .597 1968.0817_ 5:55 257.40 .434 .000
00221> [CN=100.0: N= 3.00: Tp= 1.29]
00222> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
00223> [InterEventTime= 12.00]
00224> R0068:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00225> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .477 1968.0817_ 5:50 257.40 .434 .000
00226> [CN=100.0: N= 3.00: Tp= 1.18]
00227> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
00228> [InterEventTime= 12.00]
00229> R0068:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00230> ADD HYD 5.0 02:INF-West-A 19.67 .597 1968.0817_ 5:55 257.40 n/a .000
00231> + 5.0 02:INF-West-B 14.48 .477 1968.0817_ 5:50 257.40 n/a .000
00232> SUM= 5.0 01:INF-West-T 34.15 1.072 1968.0817_ 5:50 257.40 n/a .000
00233> #####
00234> # CONTINUOUS RAINFALL DATA
00235> #####
00236> ** END OF RUN : 68
00237>
00238> *****
00239>
00240>
00241>
00242>
00243>
00244> RUN#:COMMAND#
00245> R0069:C00001-----
00246> START
00247> [TZERO = .00 hrs on 19690101]
00248> [METOUT= 2 (1=imperial, 2=metric output)]
00249> [NSTORM= 0 ]
00250> [NRUN = 0069 ]
00251> #*****
00252> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00253> #*****
00254> # Project Name: Barrhaven Conservancy Development
00255> # Project Number: 1474
00256> # Date : 2021/Oct/18
00257> # Modeller : J.Burnett, P.Eng.
00258> # Updated : 2022/Dec/07 [JB]
00259> # Updated : 2022/Dec/13 [LP]
00260> # Company : J.F. Sabourin and Associates
00261> # License # : 2582634
00262> #*****
00263> # Ottawa International Airport (1967 - 2003)
00264> R0069:C00002-----
00265> * READ AES DATA
00266> [Filename = YOW_1967_2007.123 ]
00267> [Start_date= 1969.0101: End_date= 1969.1231]

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00268> {DT= 60.min: Length= 8760.hrs: WetHrs= 470: DryHrs= 8290: PTOT= 570.30}
00269> Maximum average rainfall intensities over
00270> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00271> 21.10 16.25 10.83 7.78 3.93 2.10 1.40 1.09 .75 mm/hr
00272> 21.10 32.50 32.50 46.70 47.20 50.30 50.30 52.10 54.00 mm
00273> 19690818 19690818 19690818 19690819 19690819 19690819 19690819 19690819 19690819 date
00274> Number of rainfall events per following interevent time
00275> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00276> 157 119 107 92 72 58 49 43 32
00277> Number of events with at least the following durations
00278> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00279> 156 84 58 21 5 0 0 0 0
00280> R0069:C00003-----
00281> COMPUTE API
00282> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
00283> [APImax= 56.77: APIavg= 16.06: APImin= .16]
00284> #*****
00285> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00286> #*****
00287> R0069:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00288> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .189 1969.0819_ 3:00 63.40 .111 .000
00289> [CN= 76.0: N= 3.00: Tp= 1.29]
00290> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
00291> [InterEventTime= 12.00]
00292> R0069:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00293> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .134 1969.0819_ 2:55 55.35 .097 .000
00294> [CN= 72.0: N= 3.00: Tp= 1.18]
00295> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
00296> [InterEventTime= 12.00]
00297> R0069:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00298> ADD HYD 5.0 02:West-A 19.67 .189 1969.0819_ 3:00 63.40 n/a .000
00299> + 5.0 02:West-B 14.48 .134 1969.0819_ 2:55 55.35 n/a .000
00300> SUM= 5.0 01:West-Total 34.15 .322 1969.0819_ 2:55 59.99 n/a .000
00301> #*****
00302> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00303> #*****
00304> # Set infiltration to 0 (CN = 99.99) for water balance analysis
00305> #*****
00306> R0069:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00307> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .522 1969.0818_22:45 233.70 .410 .000
00308> [CN=100.0: N= 3.00: Tp= 1.29]
00309> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
00310> [InterEventTime= 12.00]
00311> R0069:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00312> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .415 1969.0818_22:40 233.70 .410 .000
00313> [CN=100.0: N= 3.00: Tp= 1.18]
00314> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
00315> [InterEventTime= 12.00]
00316> R0069:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00317> ADD HYD 5.0 02:INF-West-A 19.67 .522 1969.0818_22:45 233.70 n/a .000
00318> + 5.0 02:INF-West-B 14.48 .415 1969.0818_22:40 233.70 n/a .000
00319> SUM= 5.0 01:INF-West-T 34.15 .936 1969.0818_22:45 233.70 n/a .000
00320> #####
00321> # CONTINUOUS RAINFALL DATA
00322> #####
00323> ** END OF RUN : 69
00324>
00325> *****
00326>
00327>
00328>
00329>
00330>
00331> RUN#:COMMAND#
00332> R0070:C00001-----
00333> START
00334> [TZERO = .00 hrs on 19700101]
00335> [METOUT= 2 (1=imperial, 2=metric output)]
00336> [NSTORM= 0 ]
00337> [NRUN = 0070 ]
00338> #*****
00339> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00340> #*****
00341> # Project Name: Barrhaven Conservancy Development
00342> # Project Number: 1474
00343> # Date : 2021/Oct/18
00344> # Modeller : J.Burnett, P.Eng.
00345> # Updated : 2022/Dec/07 [JB]
00346> # Updated : 2022/Dec/13 [LP]
00347> # Company : J.F. Sabourin and Associates
00348> # License # : 2582634
00349> #*****
00350> # Ottawa International Airport (1967 - 2003)
00351> R0070:C00002-----
00352> * READ AES DATA
00353> [Filename = YOW_1967_2007.123 ]
00354> [Start_date= 1970.0101: End_date= 1970.1231]
00355> {DT= 60.min: Length= 8760.hrs: WetHrs= 373: DryHrs= 8387: PTOT= 558.90}
00356> Maximum average rainfall intensities over

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00357>      1 hr   2 hrs   3 hrs   6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00358>      35.30  18.30  12.20   6.10   3.63   1.81   1.21   1.46   .99   mm/hr
00359>      35.30  36.60  36.60  36.60  43.50  43.50  43.50  69.90  71.20   mm
00360>      19700926 19700926 19700926 19700927 19700817 19700817 19700818 19700926 19700927   date
00361>      Number of rainfall events per following interevent time
00362>      1 hr   2 hrs   3 hrs   6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00363>      148    127    109    84     72    60     54    41     30
00364>      Number of events with at least the following durations
00365>      1 hr   2 hrs   3 hrs   6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00366>      147    79     40     15     3      0      0      0      0
00367> R0070:C00003-----
00368>      COMPUTE API
00369>      [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
00370>      [APImax= 76.00: APIavg= 15.84: APImin= .07]
00371> #*****
00372> #      Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00373> #*****
00374> R0070:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
00375>      CONTINUOUS NASHYD   5.0 01:West-A   19.67   .270 1970.0926_22:05  60.26 .108   .000
00376>      [CN= 76.0: N= 3.00: Tp= 1.29]
00377>      [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
00378>      [InterEventTime= 12.00]
00379> R0070:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
00380>      CONTINUOUS NASHYD   5.0 01:West-B   14.48   .190 1970.0926_22:00  52.85 .095   .000
00381>      [CN= 72.0: N= 3.00: Tp= 1.18]
00382>      [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
00383>      [InterEventTime= 12.00]
00384> R0070:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
00385>      ADD HYD              5.0 02:West-A   19.67   .270 1970.0926_22:05  60.26 n/a   .000
00386>      +                    5.0 02:West-B   14.48   .190 1970.0926_22:00  52.85 n/a   .000
00387>      SUM=                 5.0 01:West-Total 34.15   .459 1970.0926_22:05  57.12 n/a   .000
00388> #*****
00389> #      Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00390> #*****
00391> #      Set infiltration to 0 (CN = 99.99) for water balance analysis
00392> #*****
00393> R0070:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
00394>      CONTINUOUS NASHYD   5.0 01:INF-West-A  19.67   .647 1970.0926_21:55  222.47 .398   .000
00395>      [CN=100.0: N= 3.00: Tp= 1.29]
00396>      [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
00397>      [InterEventTime= 12.00]
00398> R0070:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
00399>      CONTINUOUS NASHYD   5.0 01:INF-West-B  14.48   .516 1970.0926_21:50  222.47 .398   .000
00400>      [CN=100.0: N= 3.00: Tp= 1.18]
00401>      [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
00402>      [InterEventTime= 12.00]
00403> R0070:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
00404>      ADD HYD              5.0 02:INF-West-A  19.67   .647 1970.0926_21:55  222.47 n/a   .000
00405>      +                    5.0 02:INF-West-B  14.48   .516 1970.0926_21:50  222.47 n/a   .000
00406>      SUM=                 5.0 01:INF-West-T  34.15   1.161 1970.0926_21:55  222.47 n/a   .000
00407> #####
00408> # CONTINUOUS RAINFALL DATA
00409> #####
00410> ** END OF RUN : 70
00411>
00412> *****
00413>
00414>
00415>
00416>
00417>
00418> RUN#:COMMAND#
00419> R0071:C00001-----
00420>      START
00421>      [TZERO = .00 hrs on 19710101]
00422>      [METOUT= 2 (1=imperial, 2=metric output)]
00423>      [NSTORM= 0 ]
00424>      [NRUN = 0071 ]
00425> #*****
00426> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00427> #*****
00428> # Project Name: Barrhaven Conservancy Development
00429> # Project Number: 1474
00430> # Date : 2021/Oct/18
00431> # Modeller : J.Burnett, P.Eng.
00432> # Updated : 2022/Dec/07 [JB]
00433> # Updated : 2022/Dec/13 [LP]
00434> # Company : J.F. Sabourin and Associates
00435> # License # : 2582634
00436> #*****
00437> # Ottawa International Airport (1967 - 2003)
00438> R0071:C00002-----
00439> * READ AES DATA
00440> [Filename = YOW_1967_2007.123 ]
00441> [Start_date= 1971.0101: End_date= 1971.1231]
00442> {DT= 60.min: Length= 8760.hrs: WetHrs= 412: DryHrs= 8348: PTOT= 522.10}
00443> Maximum average rainfall intensities over
00444>      1 hr   2 hrs   3 hrs   6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00445>      24.60  16.60  11.67   6.13   3.09   1.56   1.06   .79   .54   mm/hr

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00446>      24.60  33.20  35.00  36.80  37.10  37.40  38.00  38.00  38.90  mm
00447>      19710810 19710810 19710810 19710810 19710810 19710810 19710811 19710812 19710830  date
00448>      Number of rainfall events per following interevent time
00449>      1 hr  2 hrs  3 hrs  6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00450>      156  123  113  93  72  61  52  42  33
00451>      Number of events with at least the following durations
00452>      1 hr  2 hrs  3 hrs  6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00453>      155  81  59  21  2  0  0  0  0
00454> R0071:C00003-----
00455>      COMPUTE API
00456>      [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
00457>      {APIimax= 62.22: APIavg= 14.84: APIimin= .36}
00458> #*****
00459> #      Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00460> #*****
00461> R0071:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00462>      CONTINUOUS NASHYD  5.0 01:West-A  19.67  .204 1971.0810_16:35  45.48 .087 .000
00463>      [CN= 76.0: N= 3.00: Tp= 1.29]
00464>      [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
00465>      [InterEventTime= 12.00]
00466> R0071:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00467>      CONTINUOUS NASHYD  5.0 01:West-B  14.48  .139 1971.0810_16:30  39.74 .076 .000
00468>      [CN= 72.0: N= 3.00: Tp= 1.18]
00469>      [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
00470>      [InterEventTime= 12.00]
00471> R0071:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00472>      ADD HYD
00473>      + 5.0 02:West-A  19.67  .204 1971.0810_16:35  45.48 n/a .000
00474>      + 5.0 02:West-B  14.48  .139 1971.0810_16:30  39.74 n/a .000
00475>      SUM= 5.0 01:West-Total  34.15  .342 1971.0810_16:35  43.04 n/a .000
00476> #*****
00477> #      Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00478> #      Set infiltration to 0 (CN = 99.99) for water balance analysis
00479> #*****
00480> R0071:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00481>      CONTINUOUS NASHYD  5.0 01:INF-West-A  19.67  .575 1971.0810_16:20  181.82 .348 .000
00482>      [CN=100.0: N= 3.00: Tp= 1.29]
00483>      [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
00484>      [InterEventTime= 12.00]
00485> R0071:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00486>      CONTINUOUS NASHYD  5.0 01:INF-West-B  14.48  .450 1971.0810_16:10  181.82 .348 .000
00487>      [CN=100.0: N= 3.00: Tp= 1.18]
00488>      [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
00489>      [InterEventTime= 12.00]
00490> R0071:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00491>      ADD HYD
00492>      + 5.0 02:INF-West-A  19.67  .575 1971.0810_16:20  181.82 n/a .000
00493>      + 5.0 02:INF-West-B  14.48  .450 1971.0810_16:10  181.82 n/a .000
00494>      SUM= 5.0 01:INF-West-T  34.15  1.024 1971.0810_16:15  181.82 n/a .000
00495> #####
00496> # CONTINUOUS RAINFALL DATA
00497> #####
00498> ** END OF RUN : 71
00499> *****
00500>
00501>
00502>
00503>
00504>
00505> RUN#:COMMAND#
00506> R0072:C00001-----
00507>      START
00508>      [TZERO = .00 hrs on 19720101]
00509>      [METOUT= 2 (1=imperial, 2=metric output)]
00510>      [NSTORM= 0 ]
00511>      [NRUN = 0072 ]
00512> #*****
00513> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00514> #*****
00515> # Project Name: Barrhaven Conservancy Development
00516> # Project Number: 1474
00517> # Date : 2021/Oct/18
00518> # Modeller : J.Burnett, P.Eng.
00519> # Updated : 2022/Dec/07 [JB]
00520> # Updated : 2022/Dec/13 [LP]
00521> # Company : J.F. Sabourin and Associates
00522> # License # : 2582634
00523> #*****
00524> # Ottawa International Airport (1967 - 2003)
00525> R0072:C00002-----
00526> * READ AES DATA
00527> [Filename = YOW_1967_2007.123 ]
00528> [Start_date= 1972.0101: End_date= 1972.1230]
00529> {DT= 60.min: Length= 8760.hrs: WetHrs= 489: DryHrs= 8271: PTOT= 784.30}
00530> Maximum average rainfall intensities over
00531> 1 hr  2 hrs  3 hrs  6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00532> 37.30  19.15  12.97  8.15  4.50  2.53  2.00  1.71  1.17 mm/hr
00533> 37.30  38.30  38.90  48.90  54.00  60.70  72.10  82.20  84.20 mm
00534> 19720712 19720712 19720807 19720808 19720808 19720808 19720713 19720714 19720715 date

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00535>      Number of rainfall events per following interevent time
00536>      1 hr  2 hrs  3 hrs  6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00537>      170  133  122   86   76   60   45   41   31
00538>      Number of events with at least the following durations
00539>      1 hr  2 hrs  3 hrs  6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00540>      169  96   58   21   5    0    0    0    0
00541> R0072:C00003-----
00542>      COMPUTE API
00543>      [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
00544>      {APImax=108.88: APIavg= 21.70: APImin= .00}
00545> #*****
00546> #      Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00547> #*****
00548> R0072:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00549>      CONTINUOUS NASHYD  5.0 01:West-A  19.67  .385 1972.0807_23:55 136.80 .174 .000
00550>      [CN= 76.0: N= 3.00: Tp= 1.29]
00551>      [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
00552>      [InterEventTime= 12.00]
00553> R0072:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00554>      CONTINUOUS NASHYD  5.0 01:West-B  14.48  .274 1972.0807_23:50 121.97 .156 .000
00555>      [CN= 72.0: N= 3.00: Tp= 1.18]
00556>      [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
00557>      [InterEventTime= 12.00]
00558> R0072:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00559>      ADD HYD  5.0 02:West-A  19.67  .385 1972.0807_23:55 136.80 n/a .000
00560>      + 5.0 02:West-B  14.48  .274 1972.0807_23:50 121.97 n/a .000
00561>      SUM= 5.0 01:West-Total 34.15  .659 1972.0807_23:50 130.51 n/a .000
00562> #*****
00563> #      Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00564> #*****
00565> #      Set infiltration to 0 (CN = 99.99) for water balance analysis
00566> #*****
00567> R0072:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00568>      CONTINUOUS NASHYD  5.0 01:INF-West-A  19.67  .729 1972.0807_23:40 375.41 .479 .000
00569>      [CN=100.0: N= 3.00: Tp= 1.29]
00570>      [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
00571>      [InterEventTime= 12.00]
00572> R0072:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00573>      CONTINUOUS NASHYD  5.0 01:INF-West-B  14.48  .573 1972.0807_23:35 375.41 .479 .000
00574>      [CN=100.0: N= 3.00: Tp= 1.18]
00575>      [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
00576>      [InterEventTime= 12.00]
00577> R0072:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00578>      ADD HYD  5.0 02:INF-West-A  19.67  .729 1972.0807_23:40 375.41 n/a .000
00579>      + 5.0 02:INF-West-B  14.48  .573 1972.0807_23:35 375.41 n/a .000
00580>      SUM= 5.0 01:INF-West-T 34.15  1.301 1972.0807_23:40 375.41 n/a .000
00581> #####
00582> # CONTINUOUS RAINFALL DATA
00583> #####
00584> ** END OF RUN : 72
00585>
00586> *****
00587>
00588>
00589>
00590>
00591>
00592>      RUN#:COMMAND#
00593> R0073:C00001-----
00594>      START
00595>      [TZERO = .00 hrs on 19730101]
00596>      [METOUT= 2 (1=imperial, 2=metric output)]
00597>      [NSTORM= 0 ]
00598>      [NRUN = 0073 ]
00599> #*****
00600> #      SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00601> #*****
00602> #      Project Name: Barrhaven Conservancy Development
00603> #      Project Number: 1474
00604> #      Date : 2021/Oct/18
00605> #      Modeller : J.Burnett, P.Eng.
00606> #      Updated : 2022/Dec/07 [JB]
00607> #      Updated : 2022/Dec/13 [LP]
00608> #      Company : J.F. Sabourin and Associates
00609> #      License # : 2582634
00610> #*****
00611> #      Ottawa International Airport (1967 - 2003)
00612> R0073:C00002-----
00613> *      READ AES DATA
00614>      [Filename = YOW_1967_2007.123 ]
00615>      [Start_date= 1973.0101: End_date= 1973.1231]
00616>      [DT= 60.min: Length= 8760.hrs: WetHrs= 549: DryHrs= 8211: PTOT= 744.90]
00617>      Maximum average rainfall intensities over
00618>      1 hr  2 hrs  3 hrs  6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00619>      30.00 17.25 12.33 7.10 3.63 1.89 1.28 .96 .96 mm/hr
00620>      30.00 34.50 37.00 42.60 43.60 45.40 46.00 46.00 69.20 mm
00621>      19730611 19730808 19730808 19730808 19730808 19730616 19730616 19730616 19731005 date
00622>      Number of rainfall events per following interevent time
00623>      1 hr  2 hrs  3 hrs  6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs

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00624>      200      164      143      108      79      61      54      43      37
00625>      Number of events with at least the following durations
00626>      1 hr  2 hrs  3 hrs  6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00627>      200    102    66     20     4     0     0     0     0
00628> R0073:C00003-----
00629>      COMPUTE API
00630>      [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
00631>      {APImax= 78.26: APIavg= 20.56: APImin= .06}
00632> #*****
00633> #      Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00634> #*****
00635> R0073:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
00636>      CONTINUOUS NASHYD      5.0 01:West-A      19.67      .322 1973.0808_21:00 101.49 .136      .000
00637>      [CN= 76.0: N= 3.00: Tp= 1.29]
00638>      [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
00639>      [InterEventTime= 12.00]
00640> R0073:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
00641>      CONTINUOUS NASHYD      5.0 01:West-B      14.48      .225 1973.0808_20:55 89.43 .120      .000
00642>      [CN= 72.0: N= 3.00: Tp= 1.18]
00643>      [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
00644>      [InterEventTime= 12.00]
00645> R0073:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
00646>      ADD HYD      5.0 02:West-A      19.67      .322 1973.0808_21:00 101.49 n/a      .000
00647>      +      5.0 02:West-B      14.48      .225 1973.0808_20:55 89.43 n/a      .000
00648>      SUM=      5.0 01:West-Total      34.15      .546 1973.0808_20:55 96.37 n/a      .000
00649> #*****
00650> #      Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00651> #*****
00652> #      Set infiltration to 0 (CN = 99.99) for water balance analysis
00653> #*****
00654> R0073:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
00655>      CONTINUOUS NASHYD      5.0 01:INF-West-A      19.67      .712 1973.0808_20:45 337.66 .453      .000
00656>      [CN=100.0: N= 3.00: Tp= 1.29]
00657>      [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
00658>      [InterEventTime= 12.00]
00659> R0073:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
00660>      CONTINUOUS NASHYD      5.0 01:INF-West-B      14.48      .560 1973.0808_20:40 337.66 .453      .000
00661>      [CN=100.0: N= 3.00: Tp= 1.18]
00662>      [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
00663>      [InterEventTime= 12.00]
00664> R0073:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
00665>      ADD HYD      5.0 02:INF-West-A      19.67      .712 1973.0808_20:45 337.66 n/a      .000
00666>      +      5.0 02:INF-West-B      14.48      .560 1973.0808_20:40 337.66 n/a      .000
00667>      SUM=      5.0 01:INF-West-T      34.15      1.270 1973.0808_20:40 337.66 n/a      .000
00668> #####
00669> # CONTINUOUS RAINFALL DATA
00670> #####
00671> ** END OF RUN : 73
00672>
00673> *****
00674>
00675>
00676>
00677>
00678>
00679> RUN#:COMMAND#
00680> R0074:C00001-----
00681>      START
00682>      [TZERO = .00 hrs on 19740101]
00683>      [METOUT= 2 (1=imperial, 2=metric output)]
00684>      [NSTORM= 0 ]
00685>      [NRUN = 0074 ]
00686> #*****
00687> #      SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00688> #*****
00689> #      Project Name: Barrhaven Conservancy Development
00690> #      Project Number: 1474
00691> #      Date : 2021/Oct/18
00692> #      Modeller : J.Burnett, P.Eng.
00693> #      Updated : 2022/Dec/07 [JB]
00694> #      Updated : 2022/Dec/13 [LP]
00695> #      Company : J.F. Sabourin and Associates
00696> #      License # : 2582634
00697> #*****
00698> #      Ottawa International Airport (1967 - 2003)
00699> R0074:C00002-----
00700> *      READ AES DATA
00701>      [Filename = YOW_1967_2007.123 ]
00702>      [Start_date= 1974.0101: End_date= 1974.1231]
00703>      [DT= 60.min: Length= 8760.hrs: WetHrs= 320: DryHrs= 8440: PTOT= 386.20]
00704>      Maximum average rainfall intensities over
00705>      1 hr  2 hrs  3 hrs  6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00706>      20.60 15.40 10.37 5.18 2.98 1.63 1.08 .81 .54 mm/hr
00707>      20.60 30.80 31.10 31.10 35.70 39.00 39.00 39.00 39.00 mm
00708>      19740718 19740719 19740719 19740719 19740305 19740305 19740306 19740306 19740307 date
00709>      Number of rainfall events per following interevent time
00710>      1 hr  2 hrs  3 hrs  6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00711>      129 105 93 77 63 50 38 33 23
00712>      Number of events with at least the following durations

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00713>      1 hr   2 hrs   3 hrs   6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00714>      128     66     32     10     3       0       0       0       0
00715> R0074:C00003-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00716>      COMPUTE API
00717>      [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
00718>      {APImax= 52.93: APIavg= 11.36: APImin= .00}
00719> #*****
00720> #      Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00721> #*****
00722> R0074:C00004-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00723>      CONTINUOUS NASHYD      5.0 01:West-A      19.67      .124 1974.0719_ 1:45 27.61 .072      .000
00724>      [CN= 76.0: N= 3.00: Tp= 1.29]
00725>      [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
00726>      [InterEventTime= 12.00]
00727> R0074:C00005-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00728>      CONTINUOUS NASHYD      5.0 01:West-B      14.48      .084 1974.0719_ 1:40 24.04 .062      .000
00729>      [CN= 72.0: N= 3.00: Tp= 1.18]
00730>      [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
00731>      [InterEventTime= 12.00]
00732> R0074:C00006-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00733>      ADD HYD      5.0 02:West-A      19.67      .124 1974.0719_ 1:45 27.61 n/a      .000
00734>      +      5.0 02:West-B      14.48      .084 1974.0719_ 1:40 24.04 n/a      .000
00735>      SUM=      5.0 01:West-Total      34.15      .208 1974.0719_ 1:45 26.10 n/a      .000
00736> #*****
00737> #      Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00738> #*****
00739> #      Set infiltration to 0 (CN = 99.99) for water balance analysis
00740> #*****
00741> R0074:C00007-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00742>      CONTINUOUS NASHYD      5.0 01:INF-West-A      19.67      .459 1974.0719_ 1:30 119.81 .310      .000
00743>      [CN=100.0: N= 3.00: Tp= 1.29]
00744>      [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
00745>      [InterEventTime= 12.00]
00746> R0074:C00008-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00747>      CONTINUOUS NASHYD      5.0 01:INF-West-B      14.48      .360 1974.0719_ 1:25 119.81 .310      .000
00748>      [CN=100.0: N= 3.00: Tp= 1.18]
00749>      [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
00750>      [InterEventTime= 12.00]
00751> R0074:C00009-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00752>      ADD HYD      5.0 02:INF-West-A      19.67      .459 1974.0719_ 1:30 119.81 n/a      .000
00753>      +      5.0 02:INF-West-B      14.48      .360 1974.0719_ 1:25 119.81 n/a      .000
00754>      SUM=      5.0 01:INF-West-T      34.15      .817 1974.0719_ 1:30 119.81 n/a      .000
00755> #####
00756> # CONTINUOUS RAINFALL DATA
00757> #####
00758> ** END OF RUN : 74
00759>
00760> *****
00761>
00762>
00763>
00764>
00765>
00766> RUN#:COMMAND#
00767> R0075:C00001-----D-----
00768>      START
00769>      [TZERO = .00 hrs on 19750101]
00770>      [METOUT= 2 (1=imperial, 2=metric output)]
00771>      [NSTORM= 0 ]
00772>      [NRUN = 0075 ]
00773> #*****
00774> #      SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00775> #*****
00776> #      Project Name: Barrhaven Conservancy Development
00777> #      Project Number: 1474
00778> #      Date : 2021/Oct/18
00779> #      Modeller : J.Burnett, P.Eng.
00780> #      Updated : 2022/Dec/07 [JB]
00781> #      Updated : 2022/Dec/13 [LP]
00782> #      Company : J.F. Sabourin and Associates
00783> #      License # : 2582634
00784> #*****
00785> #      Ottawa International Airport (1967 - 2003)
00786> R0075:C00002-----D-----
00787> *      READ AES DATA
00788>      [Filename = YOW_1967_2007.123 ]
00789>      [Start_date= 1975.0101: End_date= 1975.1231]
00790>      {DT= 60.min: Length= 8760.hrs: WetHrs= 344: DryHrs= 8416: PTOT= 535.50}
00791>      Maximum average rainfall intensities over
00792>      1 hr   2 hrs   3 hrs   6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00793>      34.80  18.40  12.53   6.32   3.33   1.73   1.15   .87   .62      mm/hr
00794>      34.80  36.80  37.60  37.90  40.00  41.50  41.50  41.80  44.40      mm
00795>      19750708 19750720 19750720 19750720 19750721 19750721 19750721 19750721 19750928      date
00796>      Number of rainfall events per following interevent time
00797>      1 hr   2 hrs   3 hrs   6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00798>      136   118    99    78    61    49    40    33    25
00799>      Number of events with at least the following durations
00800>      1 hr   2 hrs   3 hrs   6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00801>      135    70    40    17    1     0     0     0     0

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00802> R0075:C00003-----
00803> COMPUTE API
00804> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
00805> [APImax= 73.23: APIavg= 15.16: APImin= .00]
00806> #*****
00807> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00808> #*****
00809> R0075:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00810> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .213 1975.0720_17:45 61.11 .114 .000
00811> [CN= 76.0: N= 3.00: Tp= 1.29]
00812> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
00813> [InterEventTime= 12.00]
00814> R0075:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00815> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .146 1975.0720_17:40 53.72 .100 .000
00816> [CN= 72.0: N= 3.00: Tp= 1.18]
00817> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
00818> [InterEventTime= 12.00]
00819> R0075:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00820> ADD HYD 5.0 02:West-A 19.67 .213 1975.0720_17:45 61.11 n/a .000
00821> + 5.0 02:West-B 14.48 .146 1975.0720_17:40 53.72 n/a .000
00822> SUM= 5.0 01:West-Total 34.15 .359 1975.0720_17:45 57.98 n/a .000
00823> #*****
00824> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00825> #*****
00826> # Set infiltration to 0 (CN = 99.99) for water balance analysis
00827> #*****
00828> R0075:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00829> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .600 1975.0708_18:00 219.51 .410 .000
00830> [CN=100.0: N= 3.00: Tp= 1.29]
00831> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
00832> [InterEventTime= 12.00]
00833> R0075:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00834> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .480 1975.0708_17:50 219.51 .410 .000
00835> [CN=100.0: N= 3.00: Tp= 1.18]
00836> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
00837> [InterEventTime= 12.00]
00838> R0075:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00839> ADD HYD 5.0 02:INF-West-A 19.67 .600 1975.0708_18:00 219.51 n/a .000
00840> + 5.0 02:INF-West-B 14.48 .480 1975.0708_17:50 219.51 n/a .000
00841> SUM= 5.0 01:INF-West-T 34.15 1.078 1975.0708_17:55 219.51 n/a .000
00842> #####
00843> # CONTINUOUS RAINFALL DATA
00844> #####
00845> ** END OF RUN : 75
00846>
00847> *****
00848>
00849>
00850>
00851>
00852>
00853> RUN#:COMMAND#
00854> R0076:C00001-----
00855> START
00856> [TZERO = .00 hrs on 19760101]
00857> [METOUT= 2 (1=imperial, 2=metric output)]
00858> [NSTORM= 0 ]
00859> [NRUN = 0076 ]
00860> #*****
00861> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00862> #*****
00863> # Project Name: Barrhaven Conservancy Development
00864> # Project Number: 1474
00865> # Date : 2021/Oct/18
00866> # Modeller : J.Burnett, P.Eng.
00867> # Updated : 2022/Dec/07 [JB]
00868> # Updated : 2022/Dec/13 [LP]
00869> # Company : J.F. Sabourin and Associates
00870> # License # : 2582634
00871> #*****
00872> # Ottawa International Airport (1967 - 2003)
00873> R0076:C00002-----
00874> * READ AES DATA
00875> [Filename = YOW_1967_2007.123 ]
00876> [Start_date= 1976.0101: End_date= 1976.1230]
00877> {DT= 60.min: Length= 8064.hrs: WetHrs= 390: DryHrs= 7674: PTOT= 493.20}
00878> Maximum average rainfall intensities over
00879> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00880> 14.00 8.90 6.43 4.65 2.35 1.39 .97 .99 .80 mm/hr
00881> 14.00 17.80 19.30 27.90 28.20 33.30 35.10 47.60 57.50 mm
00882> 19760828 19760828 19760828 19760828 19760920 19760520 19760520 19760921 date
00883> Number of rainfall events per following interevent time
00884> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00885> 164 133 117 89 72 62 46 40 28
00886> Number of events with at least the following durations
00887> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00888> 163 80 47 15 2 0 0 0 0
00889> R0076:C00003-----
00890> COMPUTE API

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00891> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
00892> {APImax= 59.66: APIavg= 15.35: APImin= .02}
00893> #*****
00894> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00895> #*****
00896> R0076:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00897> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .098 1976.0519_23:20 42.34 .086 .000
00898> [CN= 76.0: N= 3.00: Tp= 1.29]
00899> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
00900> [InterEventTime= 12.00]
00901> R0076:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00902> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .065 1976.0519_23:20 36.78 .075 .000
00903> [CN= 72.0: N= 3.00: Tp= 1.18]
00904> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
00905> [InterEventTime= 12.00]
00906> R0076:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00907> ADD HYD 5.0 02:West-A 19.67 .098 1976.0519_23:20 42.34 n/a .000
00908> + 5.0 02:West-B 14.48 .065 1976.0519_23:20 36.78 n/a .000
00909> SUM= 5.0 01:West-Total 34.15 .163 1976.0519_23:20 39.98 n/a .000
00910> #*****
00911> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00912> #*****
00913> # Set infiltration to 0 (CN = 99.99) for water balance analysis
00914> #*****
00915> R0076:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00916> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .206 1976.0828_20:30 170.05 .345 .000
00917> [CN=100.0: N= 3.00: Tp= 1.29]
00918> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
00919> [InterEventTime= 12.00]
00920> R0076:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00921> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .161 1976.0828_20:25 170.05 .345 .000
00922> [CN=100.0: N= 3.00: Tp= 1.18]
00923> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
00924> [InterEventTime= 12.00]
00925> R0076:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00926> ADD HYD 5.0 02:INF-West-A 19.67 .206 1976.0828_20:30 170.05 n/a .000
00927> + 5.0 02:INF-West-B 14.48 .161 1976.0828_20:25 170.05 n/a .000
00928> SUM= 5.0 01:INF-West-T 34.15 .366 1976.0828_20:30 170.05 n/a .000
00929> #####
00930> # CONTINUOUS RAINFALL DATA
00931> #####
00932> ** END OF RUN : 76
00933>
00934> *****
00935>
00936>
00937>
00938>
00939>
00940> RUN#:COMMAND#
00941> R0077:C00001-----
00942> START
00943> [TZERO = .00 hrs on 19770101]
00944> [METOUT= 2 (1=imperial, 2=metric output)]
00945> [NSTORM= 0 ]
00946> [NRUN = 0077 ]
00947> #*****
00948> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00949> #*****
00950> # Project Name: Barrhaven Conservancy Development
00951> # Project Number: 1474
00952> # Date : 2021/Oct/18
00953> # Modeller : J.Burnett, P.Eng.
00954> # Updated : 2022/Dec/07 [JB]
00955> # Updated : 2022/Dec/13 [LP]
00956> # Company : J.F. Sabourin and Associates
00957> # License # : 2582634
00958> #*****
00959> # Ottawa International Airport (1967 - 2003)
00960> R0077:C00002-----
00961> * READ AES DATA
00962> [Filename = YOW_1967_2007.123 ]
00963> [Start_date= 1977.0101: End_date= 1977.1231]
00964> {DT= 60.min: Length= 8016.hrs: WetHrs= 512: DryHrs= 7504: PTOT= 677.80}
00965> Maximum average rainfall intensities over
00966> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00967> 21.30 15.20 10.40 6.53 3.30 1.66 1.40 1.06 .73 mm/hr
00968> 21.30 30.40 31.20 39.20 39.60 39.80 50.40 51.00 52.40 mm
00969> 19770717 19770717 19770717 19770901 19770902 19770314 19770314 19770314 19770718 date
00970> Number of rainfall events per following interevent time
00971> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00972> 172 142 126 99 78 63 53 42 30
00973> Number of events with at least the following durations
00974> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00975> 171 88 60 22 5 1 0 0 0
00976> R0077:C00003-----
00977> COMPUTE API
00978> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
00979> {APImax= 74.80: APIavg= 20.62: APImin= 1.63}

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00980> #*****
00981> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00982> #*****
00983> R0077:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
00984> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .208 1977.0901_23:55 80.37 .119 .000
00985> [CN= 76.0: N= 3.00: Tp= 1.29]
00986> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
00987> [InterEventTime= 12.00]
00988> R0077:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
00989> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .144 1977.0901_23:50 70.59 .104 .000
00990> [CN= 72.0: N= 3.00: Tp= 1.18]
00991> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
00992> [InterEventTime= 12.00]
00993> R0077:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
00994> ADD HYD 5.0 02:West-A 19.67 .208 1977.0901_23:55 80.37 n/a .000
00995> + 5.0 02:West-B 14.48 .144 1977.0901_23:50 70.59 n/a .000
00996> SUM= 5.0 01:West-Total 34.15 .351 1977.0901_23:55 76.23 n/a .000
00997> #*****
00998> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00999> #*****
01000> # Set infiltration to 0 (CN = 99.99) for water balance analysis
01001> #*****
01002> R0077:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
01003> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .522 1977.0901_23:40 283.86 .419 .000
01004> [CN=100.0: N= 3.00: Tp= 1.29]
01005> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01006> [InterEventTime= 12.00]
01007> R0077:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
01008> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .407 1977.0901_23:35 283.86 .419 .000
01009> [CN=100.0: N= 3.00: Tp= 1.18]
01010> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01011> [InterEventTime= 12.00]
01012> R0077:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
01013> ADD HYD 5.0 02:INF-West-A 19.67 .522 1977.0901_23:40 283.86 n/a .000
01014> + 5.0 02:INF-West-B 14.48 .407 1977.0901_23:35 283.86 n/a .000
01015> SUM= 5.0 01:INF-West-T 34.15 .928 1977.0901_23:40 283.86 n/a .000
01016> #####
01017> # CONTINUOUS RAINFALL DATA
01018> #####
01019> ** END OF RUN : 77
01020>
01021> *****
01022>
01023>
01024>
01025>
01026>
01027> RUN#:COMMAND#
01028> R0078:C00001-----
01029> START
01030> [TZERO = .00 hrs on 19780101]
01031> [METOUT= 2 (1=imperial, 2=metric output)]
01032> [NSTORM= 0 ]
01033> [NRUN = 0078 ]
01034> #*****
01035> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
01036> #*****
01037> # Project Name: Barrhaven Conservancy Development
01038> # Project Number: 1474
01039> # Date : 2021/Oct/18
01040> # Modeller : J.Burnett, P.Eng.
01041> # Updated : 2022/Dec/07 [JB]
01042> # Updated : 2022/Dec/13 [LP]
01043> # Company : J.F. Sabourin and Associates
01044> # License # : 2582634
01045> #*****
01046> # Ottawa International Airport (1967 - 2003)
01047> R0078:C00002-----
01048> * READ AES DATA
01049> [Filename = YOW_1967_2007.123 ]
01050> [Start_date= 1978.0101: End_date= 1978.1231]
01051> {DT= 60.min: Length= 8040.hrs: WetHrs= 409: DryHrs= 7631: PTOT= 641.40}
01052> Maximum average rainfall intensities over
01053> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01054> 36.00 18.15 12.10 6.05 3.04 1.64 1.13 .87 .58 mm/hr
01055> 36.00 36.30 36.30 36.30 36.50 39.40 40.60 41.60 41.60 mm
01056> 19780618 19780618 19780618 19780618 19780619 19780411 19780412 19780620 19780621 date
01057> Number of rainfall events per following interevent time
01058> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01059> 154 128 118 97 71 58 51 46 33
01060> Number of events with at least the following durations
01061> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01062> 154 75 44 18 5 0 0 0 0
01063> R0078:C00003-----
01064> COMPUTE API
01065> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
01066> {APIimax= 65.36: APIavg= 19.25: APIimin= .25}
01067> #*****
01068> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS

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01069> #*****
01070> R0078:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01071> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .252 1978.0618_18:05 61.75 .096 .000
01072> [CN= 76.0: N= 3.00: Tp= 1.29]
01073> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
01074> [InterEventTime= 12.00]
01075> R0078:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01076> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .177 1978.0618_18:00 53.70 .084 .000
01077> [CN= 72.0: N= 3.00: Tp= 1.18]
01078> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
01079> [InterEventTime= 12.00]
01080> R0078:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01081> ADD HYD 5.0 02:West-A 19.67 .252 1978.0618_18:05 61.75 n/a .000
01082> + 5.0 02:West-B 14.48 .177 1978.0618_18:00 53.70 n/a .000
01083> SUM= 5.0 01:West-Total 34.15 .428 1978.0618_18:00 58.33 n/a .000
01084> #*****
01085> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01086> #*****
01087> # Set infiltration to 0 (CN = 99.99) for water balance analysis
01088> #*****
01089> R0078:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01090> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .647 1978.0618_17:55 269.84 .421 .000
01091> [CN=100.0: N= 3.00: Tp= 1.29]
01092> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01093> [InterEventTime= 12.00]
01094> R0078:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01095> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .517 1978.0618_17:50 269.84 .421 .000
01096> [CN=100.0: N= 3.00: Tp= 1.18]
01097> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01098> [InterEventTime= 12.00]
01099> R0078:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01100> ADD HYD 5.0 02:INF-West-A 19.67 .647 1978.0618_17:55 269.84 n/a .000
01101> + 5.0 02:INF-West-B 14.48 .517 1978.0618_17:50 269.84 n/a .000
01102> SUM= 5.0 01:INF-West-T 34.15 1.161 1978.0618_17:55 269.84 n/a .000
01103> #####
01104> # CONTINUOUS RAINFALL DATA
01105> #####
01106> ** END OF RUN : 78
01107>
01108> *****
01109>
01110>
01111>
01112>
01113>
01114> RUN#:COMMAND#
01115> R0079:C00001-----
01116> START
01117> [TZERO = .00 hrs on 19790101]
01118> [METOUT= 2 (1=imperial, 2=metric output)]
01119> [NSTORM= 0 ]
01120> [NRUN = 0079 ]
01121> #*****
01122> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
01123> #*****
01124> # Project Name: Barrhaven Conservancy Development
01125> # Project Number: 1474
01126> # Date : 2021/Oct/18
01127> # Modeller : J.Burnett, P.Eng.
01128> # Updated : 2022/Dec/07 [JB]
01129> # Updated : 2022/Dec/13 [LP]
01130> # Company : J.F. Sabourin and Associates
01131> # License # : 2582634
01132> #*****
01133> # Ottawa International Airport (1967 - 2003)
01134> R0079:C00002-----
01135> * READ AES DATA
01136> [Filename = YOW_1967_2007.123 ]
01137> [Start_date= 1979.0101: End_date= 1979.1231]
01138> {DT= 60.min: Length= 8760.hrs: WetHrs= 546: DryHrs= 8214: PTOT= 866.50}
01139> Maximum average rainfall intensities over
01140> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01141> 34.90 22.00 14.67 7.33 5.14 2.63 1.75 1.31 .88 mm/hr
01142> 34.90 44.00 44.00 44.00 61.70 63.00 63.00 63.00 63.00 mm
01143> 19790616 19790616 19790616 19790914 19790915 19790915 19790917 date
01144> Number of rainfall events per following interevent time
01145> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01146> 188 147 129 103 86 60 53 43 36
01147> Number of events with at least the following durations
01148> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01149> 187 97 65 25 6 1 0 0 0
01150> R0079:C00003-----
01151> COMPUTE API
01152> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
01153> {APImax= 78.42: APIavg= 23.13: APImin= .13}
01154> #*****
01155> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01156> #*****
01157> R0079:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms

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01158> CONTINUOUS NASHYD      5.0 01:West-A      19.67      .350 1979.0616_15:00 159.06 .184      .000
01159> [CN= 76.0: N= 3.00: Tp= 1.29]
01160> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
01161> [InterEventTime= 12.00]
01162> R0079:C00005-----D Tmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01163> CONTINUOUS NASHYD      5.0 01:West-B      14.48      .248 1979.0616_14:55 141.55 .163      .000
01164> [CN= 72.0: N= 3.00: Tp= 1.18]
01165> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
01166> [InterEventTime= 12.00]
01167> R0079:C00006-----D Tmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01168> ADD HYD
+      5.0 02:West-A      19.67      .350 1979.0616_15:00 159.06 n/a      .000
01169> +      5.0 02:West-B      14.48      .248 1979.0616_14:55 141.55 n/a      .000
01170> SUM=      5.0 01:West-Total 34.15      .597 1979.0616_15:00 151.64 n/a      .000
01171> #*****
01172> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01173> #*****
01174> # Set infiltration to 0 (CN = 99.99) for water balance analysis
01175> #*****
01176> R0079:C00007-----D Tmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01177> CONTINUOUS NASHYD      5.0 01:INF-West-A      19.67      .798 1979.0616_14:50 449.28 .519      .000
01178> [CN=100.0: N= 3.00: Tp= 1.29]
01179> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01180> [InterEventTime= 12.00]
01181> R0079:C00008-----D Tmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01182> CONTINUOUS NASHYD      5.0 01:INF-West-B      14.48      .635 1979.0616_14:45 449.28 .519      .000
01183> [CN=100.0: N= 3.00: Tp= 1.18]
01184> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01185> [InterEventTime= 12.00]
01186> R0079:C00009-----D Tmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01187> ADD HYD
+      5.0 02:INF-West-A      19.67      .798 1979.0616_14:50 449.28 n/a      .000
01188> +      5.0 02:INF-West-B      14.48      .635 1979.0616_14:45 449.28 n/a      .000
01189> SUM=      5.0 01:INF-West-T 34.15      1.430 1979.0616_14:45 449.28 n/a      .000
01190> #####
01191> # CONTINUOUS RAINFALL DATA
01192> #####
01193> ** END OF RUN : 79
01194>
01195> *****
01196>
01197>
01198>
01199>
01200>
01201> RUN#:COMMAND#
01202> R0080:C00001-----
01203> START
01204> [TZERO = .00 hrs on 19800101]
01205> [METOUT= 2 (1=imperial, 2=metric output)]
01206> [NSTORM= 0 ]
01207> [NRUN = 0080 ]
01208> #*****
01209> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
01210> #*****
01211> # Project Name: Barrhaven Conservancy Development
01212> # Project Number: 1474
01213> # Date : 2021/Oct/18
01214> # Modeller : J.Burnett, P.Eng.
01215> # Updated : 2022/Dec/07 [JB]
01216> # Updated : 2022/Dec/13 [LP]
01217> # Company : J.F. Sabourin and Associates
01218> # License # : 2582634
01219> #*****
01220> # Ottawa International Airport (1967 - 2003)
01221> R0080:C00002-----
01222> * READ AES DATA
01223> [Filename = YOW_1967_2007.123 ]
01224> [Start_date= 1980.0101: End_date= 1980.1230]
01225> {DT= 60.min: Length= 8760.hrs: WetHrs= 427: DryHrs= 8333: PTOT= 622.00}
01226> Maximum average rainfall intensities over
01227> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01228> 15.00 9.20 6.50 4.72 3.57 1.97 1.35 1.01 .86 mm/hr
01229> 15.00 18.40 19.50 28.30 42.80 47.20 48.60 48.60 62.00 mm
01230> 19800830 19800830 19801025 19801025 19801026 19801026 19801027 19800902 date
01231> Number of rainfall events per following interevent time
01232> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01233> 151 125 112 93 79 62 49 44 28
01234> Number of events with at least the following durations
01235> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01236> 150 85 54 16 4 0 0 0 0
01237> R0080:C00003-----
01238> COMPUTE API
01239> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
01240> [APImax= 68.72: APIavg= 17.50: APImin= .06]
01241> #*****
01242> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01243> #*****
01244> R0080:C00004-----D Tmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01245> CONTINUOUS NASHYD      5.0 01:West-A      19.67      .118 1980.1026_ 0:35 66.79 .107      .000
01246> [CN= 76.0: N= 3.00: Tp= 1.29]

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01247> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
01248> [InterEventTime= 12.00]
01249> R0080:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01250> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .080 1980.1026_ 0:30 58.50 .094 .000
01251> [CN= 72.0: N= 3.00: Tp= 1.18]
01252> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
01253> [InterEventTime= 12.00]
01254> R0080:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01255> ADD HYD 5.0 02:West-A 19.67 .118 1980.1026_ 0:35 66.79 n/a .000
01256> + 5.0 02:West-B 14.48 .080 1980.1026_ 0:30 58.50 n/a .000
01257> SUM= 5.0 01:West-Total 34.15 .198 1980.1026_ 0:30 63.27 n/a .000
01258> #*****
01259> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01260> #*****
01261> # Set infiltration to 0 (CN = 99.99) for water balance analysis
01262> #*****
01263> R0080:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01264> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .253 1980.1025_17:45 254.15 .409 .000
01265> [CN=100.0: N= 3.00: Tp= 1.29]
01266> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01267> [InterEventTime= 12.00]
01268> R0080:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01269> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .194 1980.1025_17:35 254.15 .409 .000
01270> [CN=100.0: N= 3.00: Tp= 1.18]
01271> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01272> [InterEventTime= 12.00]
01273> R0080:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01274> ADD HYD 5.0 02:INF-West-A 19.67 .253 1980.1025_17:45 254.15 n/a .000
01275> + 5.0 02:INF-West-B 14.48 .194 1980.1025_17:35 254.15 n/a .000
01276> SUM= 5.0 01:INF-West-T 34.15 .446 1980.1025_17:40 254.15 n/a .000
01277> #####
01278> # CONTINUOUS RAINFALL DATA
01279> #####
01280> ** END OF RUN : 80
01281>
01282> *****
01283>
01284>
01285>
01286>
01287>
01288> RUN#:COMMAND#
01289> R0081:C00001-----
01290> START
01291> [TZERO = .00 hrs on 19810101]
01292> [METOUT= 2 (1=imperial, 2=metric output)]
01293> [NSTORM= 0 ]
01294> [NRUN = 0081 ]
01295> #*****
01296> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
01297> #*****
01298> # Project Name: Barrhaven Conservancy Development
01299> # Project Number: 1474
01300> # Date : 2021/Oct/18
01301> # Modeller : J.Burnett, P.Eng.
01302> # Updated : 2022/Dec/07 [JB]
01303> # Updated : 2022/Dec/13 [LP]
01304> # Company : J.F. Sabourin and Associates
01305> # License # : 2582634
01306> #*****
01307> # Ottawa International Airport (1967 - 2003)
01308> R0081:C00002-----
01309> * READ AES DATA
01310> [Filename = YOW_1967_2007.123 ]
01311> [Start_date= 1981.0101: End_date= 1981.1231]
01312> {DT= 60.min: Length= 8760.hrs: WetHrs= 641: DryHrs= 8119: PTOT= 936.40}
01313> Maximum average rainfall intensities over
01314> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01315> 35.30 31.85 26.20 18.15 9.27 4.83 3.22 2.41 1.62 mm/hr
01316> 35.30 63.70 78.60 108.90 111.30 115.90 115.90 115.90 116.70 mm
01317> 19810805 19810805 19810805 19810805 19810805 19810805 19810806 19810806 19810805 date
01318> Number of rainfall events per following interevent time
01319> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01320> 226 171 136 109 83 68 59 47 30
01321> Number of events with at least the following durations
01322> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01323> 225 128 79 28 7 0 0 0 0
01324> R0081:C00003-----
01325> COMPUTE API
01326> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
01327> {APIimax=123.49: APIavg= 25.69: APIimin= .26}
01328> #*****
01329> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01330> #*****
01331> R0081:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01332> CONTINUOUS NASHYD 5.0 01:West-A 19.67 1.076 1981.0805_ 3:05 196.98 .210 .000
01333> [CN= 76.0: N= 3.00: Tp= 1.29]
01334> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
01335> [InterEventTime= 12.00]

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01336> R0081:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01337> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .781 1981.0805_ 3:00 179.64 .192 .000
01338> [CN= 72.0: N= 3.00: Tp= 1.18]
01339> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
01340> [InterEventTime= 12.00]
01341> R0081:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01342> ADD HYD 5.0 02:West-A 19.67 1.076 1981.0805_ 3:05 196.98 n/a .000
01343> + 5.0 02:West-B 14.48 .781 1981.0805_ 3:00 179.64 n/a .000
01344> SUM= 5.0 01:West-Total 34.15 1.855 1981.0805_ 3:05 189.63 n/a .000
01345> #*****
01346> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01347> #*****
01348> # Set infiltration to 0 (CN = 99.99) for water balance analysis
01349> #*****
01350> R0081:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01351> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 1.402 1981.0805_ 2:40 459.70 .491 .000
01352> [CN=100.0: N= 3.00: Tp= 1.29]
01353> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01354> [InterEventTime= 12.00]
01355> R0081:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01356> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 1.079 1981.0805_ 2:35 459.70 .491 .000
01357> [CN=100.0: N= 3.00: Tp= 1.18]
01358> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01359> [InterEventTime= 12.00]
01360> R0081:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01361> ADD HYD 5.0 02:INF-West-A 19.67 1.402 1981.0805_ 2:40 459.70 n/a .000
01362> + 5.0 02:INF-West-B 14.48 1.079 1981.0805_ 2:35 459.70 n/a .000
01363> SUM= 5.0 01:INF-West-T 34.15 2.479 1981.0805_ 2:35 459.70 n/a .000
01364> #####
01365> # CONTINUOUS RAINFALL DATA
01366> #####
01367> ** END OF RUN : 81
01368>
01369> *****
01370>
01371>
01372>
01373>
01374>
01375> RUN#:COMMAND#
01376> R0082:C00001-----
01377> START
01378> [TZERO = .00 hrs on 19820101]
01379> [METOUT= 2 (1=imperial, 2=metric output)]
01380> [NSTORM= 0 ]
01381> [NRUN = 0082 ]
01382> #*****
01383> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
01384> #*****
01385> # Project Name: Barrhaven Conservancy Development
01386> # Project Number: 1474
01387> # Date : 2021/Oct/18
01388> # Modeller : J.Burnett, P.Eng.
01389> # Updated : 2022/Dec/07 [JB]
01390> # Updated : 2022/Dec/13 [LP]
01391> # Company : J.F. Sabourin and Associates
01392> # License # : 2582634
01393> #*****
01394> # Ottawa International Airport (1967 - 2003)
01395> R0082:C00002-----
01396> * READ AES DATA
01397> [Filename = YOW_1967_2007.123 ]
01398> [Start_date= 1982.0101: End_date= 1982.1231]
01399> {DT= 60.min: Length= 8760.hrs: WetHrs= 436: DryHrs= 8324: PTOT= 596.10}
01400> Maximum average rainfall intensities over
01401> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01402> 19.80 10.75 7.60 5.83 3.36 1.68 1.12 .96 .80 mm/hr
01403> 19.80 21.50 22.80 35.00 40.30 40.30 46.30 57.30 mm
01404> 19820801 19820901 19820825 19820825 19820825 19820826 19820826 19820825 19820825 date
01405> Number of rainfall events per following interevent time
01406> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01407> 134 110 98 78 66 57 48 41 33
01408> Number of events with at least the following durations
01409> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01410> 133 81 58 18 4 1 1 0 0
01411> R0082:C00003-----
01412> COMPUTE API
01413> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
01414> {APImax= 56.66: APIavg= 16.78: APImin= .03}
01415> #*****
01416> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01417> #*****
01418> R0082:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01419> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .154 1982.0825_12:25 54.10 .091 .000
01420> [CN= 76.0: N= 3.00: Tp= 1.29]
01421> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
01422> [InterEventTime= 12.00]
01423> R0082:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01424> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .102 1982.0825_12:20 47.17 .079 .000

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01425> [CN= 72.0: N= 3.00: Tp= 1.18]
01426> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
01427> [InterEventTime= 12.00]
01428> R0082:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
01429> ADD HYD 5.0 02:West-A 19.67 .154 1982.0825_12:25 54.10 n/a .000
01430> + 5.0 02:West-B 14.48 .102 1982.0825_12:20 47.17 n/a .000
01431> SUM= 5.0 01:West-Total 34.15 .255 1982.0825_12:25 51.16 n/a .000
01432> #*****
01433> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01434> #*****
01435> # Set infiltration to 0 (CN = 99.99) for water balance analysis
01436> #*****
01437> R0082:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
01438> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .402 1982.0825_11:40 228.69 .384 .000
01439> [CN=100.0: N= 3.00: Tp= 1.29]
01440> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01441> [InterEventTime= 12.00]
01442> R0082:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
01443> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .307 1982.0825_11:35 228.69 .384 .000
01444> [CN=100.0: N= 3.00: Tp= 1.18]
01445> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01446> [InterEventTime= 12.00]
01447> R0082:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
01448> ADD HYD 5.0 02:INF-West-A 19.67 .402 1982.0825_11:40 228.69 n/a .000
01449> + 5.0 02:INF-West-B 14.48 .307 1982.0825_11:35 228.69 n/a .000
01450> SUM= 5.0 01:INF-West-T 34.15 .709 1982.0825_11:40 228.69 n/a .000
01451> #####
01452> # CONTINUOUS RAINFALL DATA
01453> #####
01454> ** END OF RUN : 82
01455>
01456> *****
01457>
01458>
01459>
01460>
01461>
01462> RUN#:COMMAND#
01463> R0083:C00001-----
01464> START
01465> [TZERO = .00 hrs on 19830101]
01466> [METOUT= 2 (1=imperial, 2=metric output)]
01467> [NSTORM= 0 ]
01468> [NRUN = 0083 ]
01469> #*****
01470> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
01471> #*****
01472> # Project Name: Barrhaven Conservancy Development
01473> # Project Number: 1474
01474> # Date : 2021/Oct/18
01475> # Modeller : J.Burnett, P.Eng.
01476> # Updated : 2022/Dec/07 [JB]
01477> # Updated : 2022/Dec/13 [LP]
01478> # Company : J.F. Sabourin and Associates
01479> # License # : 2582634
01480> #*****
01481> # Ottawa International Airport (1967 - 2003)
01482> R0083:C00002-----
01483> * READ AES DATA
01484> [Filename = YOW_1967_2007.123 ]
01485> [Start_date= 1983.0101: End_date= 1983.1231]
01486> [DT= 60.min: Length= 8760.hrs: WetHrs= 462: DryHrs= 8298: PTOT= 587.50]
01487> Maximum average rainfall intensities over
01488> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01489> 10.40 9.70 7.53 5.43 3.18 2.36 1.68 1.32 .92 mm/hr
01490> 10.40 19.40 22.60 32.60 38.20 56.70 60.40 63.20 66.00 mm
01491> 19831004 19830921 19830921 19831005 19831005 19831005 19831006 19831008 date
01492> Number of rainfall events per following interevent time
01493> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01494> 143 115 103 85 70 55 50 45 35
01495> Number of events with at least the following durations
01496> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01497> 142 87 56 28 5 0 0 0 0
01498> R0083:C00003-----
01499> COMPUTE API
01500> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
01501> [APImax= 79.86: APIavg= 16.57: APImin= .05]
01502> #*****
01503> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01504> #*****
01505> R0083:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
01506> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .196 1983.1005_16:40 58.94 .100 .000
01507> [CN= 76.0: N= 3.00: Tp= 1.29]
01508> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
01509> [InterEventTime= 12.00]
01510> R0083:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
01511> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .133 1983.1005_16:30 51.78 .088 .000
01512> [CN= 72.0: N= 3.00: Tp= 1.18]
01513> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]

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01514> [InterEventTime= 12.00]
01515> R0083:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01516> ADD HYD 5.0 02:West-A 19.67 .196 1983.1005_16:40 58.94 n/a .000
01517> + 5.0 02:West-B 14.48 .133 1983.1005_16:30 51.78 n/a .000
01518> SUM= 5.0 01:West-Total 34.15 .328 1983.1005_16:35 55.90 n/a .000
01519> #*****
01520> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01521> #*****
01522> # Set infiltration to 0 (CN = 99.99) for water balance analysis
01523> #*****
01524> R0083:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01525> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .365 1983.1005_16:10 217.30 .370 .000
01526> [CN=100.0: N= 3.00: Tp= 1.29]
01527> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01528> [InterEventTime= 12.00]
01529> R0083:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01530> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .280 1983.1005_16:00 217.30 .370 .000
01531> [CN=100.0: N= 3.00: Tp= 1.18]
01532> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01533> [InterEventTime= 12.00]
01534> R0083:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01535> ADD HYD 5.0 02:INF-West-A 19.67 .365 1983.1005_16:10 217.30 n/a .000
01536> + 5.0 02:INF-West-B 14.48 .280 1983.1005_16:00 217.30 n/a .000
01537> SUM= 5.0 01:INF-West-T 34.15 .644 1983.1005_16:05 217.30 n/a .000
01538> #####
01539> # CONTINUOUS RAINFALL DATA
01540> #####
01541> ** END OF RUN : 83
01542>
01543> *****
01544>
01545>
01546>
01547>
01548>
01549> RUN#:COMMAND#
01550> R0084:C00001-----
01551> START
01552> [TZERO = .00 hrs on 19840101]
01553> [METOUT= 2 (1=imperial, 2=metric output)]
01554> [NSTORM= 0 ]
01555> [NRUN = 0084 ]
01556> #*****
01557> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
01558> #*****
01559> # Project Name: Barrhaven Conservancy Development
01560> # Project Number: 1474
01561> # Date : 2021/Oct/18
01562> # Modeller : J.Burnett, P.Eng.
01563> # Updated : 2022/Dec/07 [JB]
01564> # Updated : 2022/Dec/13 [LP]
01565> # Company : J.F. Sabourin and Associates
01566> # License # : 2582634
01567> #*****
01568> # Ottawa International Airport (1967 - 2003)
01569> R0084:C00002-----
01570> * READ AES DATA
01571> [Filename = YOW_1967_2007.123 ]
01572> [Start_date= 1984.0101: End_date= 1984.1230]
01573> {DT= 60.min: Length= 8760.hrs: WetHrs= 308: DryHrs= 8452: PTOT= 459.40}
01574> Maximum average rainfall intensities over
01575> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01576> 17.80 9.70 7.57 4.33 3.01 1.85 1.58 1.19 1.00 mm/hr
01577> 17.80 19.40 22.70 26.00 36.10 44.30 57.00 57.00 72.20 mm
01578> 19840812 19840812 19840812 19840806 19840812 19840813 19840813 19840814 19840813 date
01579> Number of rainfall events per following interevent time
01580> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01581> 98 80 75 63 55 48 40 34 26
01582> Number of events with at least the following durations
01583> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01584> 97 58 39 11 3 1 0 0 0
01585> R0084:C00003-----
01586> COMPUTE API
01587> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
01588> [APImax= 86.83: APIavg= 13.22: APImin= .00]
01589> #*****
01590> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01591> #*****
01592> R0084:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01593> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .156 1984.0813_ 7:20 56.90 .124 .000
01594> [CN= 76.0: N= 3.00: Tp= 1.29]
01595> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
01596> [InterEventTime= 12.00]
01597> R0084:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01598> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .111 1984.0813_ 7:10 49.92 .109 .000
01599> [CN= 72.0: N= 3.00: Tp= 1.18]
01600> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
01601> [InterEventTime= 12.00]
01602> R0084:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms

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01603> ADD HYD 5.0 02:West-A 19.67 .156 1984.0813_ 7:20 56.90 n/a .000
01604> + 5.0 02:West-B 14.48 .111 1984.0813_ 7:10 49.92 n/a .000
01605> SUM= 5.0 01:West-Total 34.15 .267 1984.0813_ 7:15 53.94 n/a .000
01606> #*****
01607> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01608> #*****
01609> # Set infiltration to 0 (CN = 99.99) for water balance analysis
01610> #*****
01611> R0084:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01612> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .357 1984.0812_ 7:55 207.21 .451 .000
01613> [CN=100.0: N= 3.00: Tp= 1.29]
01614> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01615> [InterEventTime= 12.00]
01616> R0084:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01617> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .285 1984.0812_ 7:45 207.21 .451 .000
01618> [CN=100.0: N= 3.00: Tp= 1.18]
01619> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01620> [InterEventTime= 12.00]
01621> R0084:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01622> ADD HYD 5.0 02:INF-West-A 19.67 .357 1984.0812_ 7:55 207.21 n/a .000
01623> + 5.0 02:INF-West-B 14.48 .285 1984.0812_ 7:45 207.21 n/a .000
01624> SUM= 5.0 01:INF-West-T 34.15 .641 1984.0812_ 7:50 207.21 n/a .000
01625> #####
01626> # CONTINUOUS RAINFALL DATA
01627> #####
01628> ** END OF RUN : 84
01629>
01630> *****
01631>
01632>
01633>
01634>
01635>
01636> RUN#:COMMAND#
01637> R0085:C00001-----
01638> START
01639> [TZERO = .00 hrs on 19850101]
01640> [METOUT= 2 (1=imperial, 2=metric output)]
01641> [NSTORM= 0 ]
01642> [NRUN = 0085 ]
01643> #*****
01644> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
01645> #*****
01646> # Project Name: Barrhaven Conservancy Development
01647> # Project Number: 1474
01648> # Date : 2021/Oct/18
01649> # Modeller : J.Burnett, P.Eng.
01650> # Updated : 2022/Dec/07 [JB]
01651> # Updated : 2022/Dec/13 [LP]
01652> # Company : J.F. Sabourin and Associates
01653> # License # : 2582634
01654> #*****
01655> # Ottawa International Airport (1967 - 2003)
01656> R0085:C00002-----
01657> * READ AES DATA
01658> [Filename = YOW_1967_2007.123 ]
01659> [Start_date= 1985.0101: End_date= 1985.1231]
01660> {DT= 60.min: Length= 8760.hrs: WetHrs= 354: DryHrs= 8406: PTOT= 559.90}
01661> Maximum average rainfall intensities over
01662> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01663> 19.00 13.60 11.73 6.60 3.30 1.65 1.11 .89 .60 mm/hr
01664> 19.00 27.20 35.20 39.60 39.60 39.60 40.10 42.80 43.40 mm
01665> 19850716 19850617 19850617 19850618 19850618 19850618 19850618 19850827 19850827 date
01666> Number of rainfall events per following interevent time
01667> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01668> 108 88 84 74 69 56 49 43 32
01669> Number of events with at least the following durations
01670> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01671> 107 70 43 13 4 1 0 0 0
01672> R0085:C00003-----
01673> COMPUTE API
01674> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
01675> [APImax= 57.29: APIavg= 15.86: APImin= .20]
01676> #*****
01677> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01678> #*****
01679> R0085:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01680> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .185 1985.0618_ 0:45 60.37 .108 .000
01681> [CN= 76.0: N= 3.00: Tp= 1.29]
01682> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
01683> [InterEventTime= 12.00]
01684> R0085:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01685> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .125 1985.0618_ 0:35 52.48 .094 .000
01686> [CN= 72.0: N= 3.00: Tp= 1.18]
01687> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
01688> [InterEventTime= 12.00]
01689> R0085:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01690> ADD HYD 5.0 02:West-A 19.67 .185 1985.0618_ 0:45 60.37 n/a .000
01691> + 5.0 02:West-B 14.48 .125 1985.0618_ 0:35 52.48 n/a .000

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01692> SUM= 5.0 01:West-Total 34.15 .310 1985.0618_ 0:40 57.02 n/a .000
01693> #*****
01694> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01695> #*****
01696> # Set infiltration to 0 (CN = 99.99) for water balance analysis
01697> #*****
01698> R0085:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01699> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .499 1985.0618_ 0:15 262.29 .468 .000
01700> [CN=100.0: N= 3.00: Tp= 1.29]
01701> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01702> [InterEventTime= 12.00]
01703> R0085:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01704> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .384 1985.0618_ 0:10 262.29 .468 .000
01705> [CN=100.0: N= 3.00: Tp= 1.18]
01706> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01707> [InterEventTime= 12.00]
01708> R0085:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01709> ADD HYD 5.0 02:INF-West-A 19.67 .499 1985.0618_ 0:15 262.29 n/a .000
01710> + 5.0 02:INF-West-B 14.48 .384 1985.0618_ 0:10 262.29 n/a .000
01711> SUM= 5.0 01:INF-West-T 34.15 .881 1985.0618_ 0:15 262.29 n/a .000
01712> #####
01713> # CONTINUOUS RAINFALL DATA
01714> #####
01715> ** END OF RUN : 85
01716>
01717> *****
01718>
01719>
01720>
01721>
01722>
01723> RUN#:COMMAND#
01724> R0086:C00001-----
01725> START
01726> [TZERO = .00 hrs on 19860101]
01727> [METOUT= 2 (1=imperial, 2=metric output)]
01728> [NSTORM= 0 ]
01729> [NRUN = 0086 ]
01730> #*****
01731> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
01732> #*****
01733> # Project Name: Barrhaven Conservancy Development
01734> # Project Number: 1474
01735> # Date : 2021/Oct/18
01736> # Modeller : J.Burnett, P.Eng.
01737> # Updated : 2022/Dec/07 [JB]
01738> # Updated : 2022/Dec/13 [LP]
01739> # Company : J.F. Sabourin and Associates
01740> # License # : 2582634
01741> #*****
01742> # Ottawa International Airport (1967 - 2003)
01743> R0086:C00002-----
01744> * READ AES DATA
01745> [Filename = YOW_1967_2007.123 ]
01746> [Start_date= 1986.0101: End_date= 1986.1231]
01747> {DT= 60.min: Length= 8040.hrs: WetHrs= 520: DryHrs= 7520: PTOT= 849.40}
01748> Maximum average rainfall intensities over
01749> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01750> 18.30 17.80 13.57 7.07 4.84 2.89 2.42 1.85 1.31 mm/hr
01751> 18.30 35.60 40.70 42.40 58.10 69.30 87.00 88.60 94.40 mm
01752> 19860729 19860729 19860729 19860729 19860912 19860912 19860912 19860912 19860913 date
01753> Number of rainfall events per following interevent time
01754> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01755> 178 144 131 104 80 63 53 48 33
01756> Number of events with at least the following durations
01757> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01758> 177 104 76 24 2 0 0 0 0
01759> R0086:C00003-----
01760> COMPUTE API
01761> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
01762> [APIimax=102.23: APIavg= 25.30: APIimin= .17]
01763> #*****
01764> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01765> #*****
01766> R0086:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01767> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .363 1986.0911_23:45 163.15 .192 .000
01768> [CN= 76.0: N= 3.00: Tp= 1.29]
01769> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
01770> [InterEventTime= 12.00]
01771> R0086:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01772> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .258 1986.0911_23:40 146.75 .173 .000
01773> [CN= 72.0: N= 3.00: Tp= 1.18]
01774> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
01775> [InterEventTime= 12.00]
01776> R0086:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01777> ADD HYD 5.0 02:West-A 19.67 .363 1986.0911_23:45 163.15 n/a .000
01778> + 5.0 02:West-B 14.48 .258 1986.0911_23:40 146.75 n/a .000
01779> SUM= 5.0 01:West-Total 34.15 .621 1986.0911_23:45 156.19 n/a .000
01780> #*****

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01781> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01782> #*****
01783> # Set infiltration to 0 (CN = 99.99) for water balance analysis
01784> #*****
01785> R0086:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01786> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .630 1986.0729_15:50 418.06 .492 .000
01787> [CN=100.0: N= 3.00: Tp= 1.29]
01788> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01789> [InterEventTime= 12.00]
01790> R0086:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01791> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .491 1986.0729_15:40 418.06 .492 .000
01792> [CN=100.0: N= 3.00: Tp= 1.18]
01793> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01794> [InterEventTime= 12.00]
01795> R0086:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01796> ADD HYD 5.0 02:INF-West-A 19.67 .630 1986.0729_15:50 418.05 n/a .000
01797> + 5.0 02:INF-West-B 14.48 .491 1986.0729_15:40 418.05 n/a .000
01798> SUM= 5.0 01:INF-West-T 34.15 1.119 1986.0729_15:45 418.06 n/a .000
01799> #####
01800> # CONTINUOUS RAINFALL DATA
01801> #####
01802> ** END OF RUN : 86
01803>
01804> *****
01805>
01806>
01807>
01808>
01809>
01810> RUN#:COMMAND#
01811> R0087:C00001-----
01812> START
01813> [TZERO = .00 hrs on 19870101]
01814> [METOUT= 2 (1=imperial, 2=metric output)]
01815> [NSTORM= 0 ]
01816> [NRUN = 0087 ]
01817> #*****
01818> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
01819> #*****
01820> # Project Name: Barrhaven Conservancy Development
01821> # Project Number: 1474
01822> # Date : 2021/Oct/18
01823> # Modeller : J.Burnett, P.Eng.
01824> # Updated : 2022/Dec/07 [JB]
01825> # Updated : 2022/Dec/13 [LP]
01826> # Company : J.F. Sabourin and Associates
01827> # License # : 2582634
01828> #*****
01829> # Ottawa International Airport (1967 - 2003)
01830> R0087:C00002-----
01831> * READ AES DATA
01832> [Filename = YOW_1967_2007.123 ]
01833> [Start_date= 1987.0101: End_date= 1987.1231]
01834> {DT= 60.min: Length= 7344.hrs: WetHrs= 492: DryHrs= 6852: PTOT= 640.10}
01835> Maximum average rainfall intensities over
01836> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01837> 20.00 13.90 14.03 7.05 4.87 2.46 1.84 1.40 .93 mm/hr
01838> 20.00 27.80 42.10 42.30 58.40 59.00 66.40 67.00 67.00 mm
01839> 19870724 19870724 19870724 19870724 19870724 19870725 19870725 19870726 19870726 date
01840> Number of rainfall events per following interevent time
01841> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01842> 180 147 128 93 74 55 49 41 28
01843> Number of events with at least the following durations
01844> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01845> 179 94 60 20 3 0 0 0 0
01846> R0087:C00003-----
01847> COMPUTE API
01848> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
01849> {APImax= 75.76: APIavg= 21.41: APImin= 1.18}
01850> #*****
01851> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01852> #*****
01853> R0087:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01854> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .264 1987.0724_15:45 77.04 .120 .000
01855> [CN= 76.0: N= 3.00: Tp= 1.29]
01856> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
01857> [InterEventTime= 12.00]
01858> R0087:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01859> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .182 1987.0724_15:40 68.56 .107 .000
01860> [CN= 72.0: N= 3.00: Tp= 1.18]
01861> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
01862> [InterEventTime= 12.00]
01863> R0087:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01864> ADD HYD 5.0 02:West-A 19.67 .264 1987.0724_15:45 77.04 n/a .000
01865> + 5.0 02:West-B 14.48 .182 1987.0724_15:40 68.56 n/a .000
01866> SUM= 5.0 01:West-Total 34.15 .446 1987.0724_15:45 73.44 n/a .000
01867> #*****
01868> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01869> #*****

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01870> # Set infiltration to 0 (CN = 99.99) for water balance analysis
01871> #*****
01872> R0087:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01873> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .567 1987.0724_15:25 240.27 .375 .000
01874> [CN=100.0: N= 3.00: Tp= 1.29]
01875> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01876> [InterEventTime= 12.00]
01877> R0087:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01878> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .433 1987.0724_15:20 240.27 .375 .000
01879> [CN=100.0: N= 3.00: Tp= 1.18]
01880> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01881> [InterEventTime= 12.00]
01882> R0087:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01883> ADD HYD 5.0 02:INF-West-A 19.67 .567 1987.0724_15:25 240.27 n/a .000
01884> + 5.0 02:INF-West-B 14.48 .433 1987.0724_15:20 240.27 n/a .000
01885> SUM= 5.0 01:INF-West-T 34.15 1.000 1987.0724_15:25 240.27 n/a .000
01886> #####
01887> # CONTINUOUS RAINFALL DATA
01888> #####
01889> ** END OF RUN : 87
01890>
01891> *****
01892>
01893>
01894>
01895>
01896>
01897> RUN#:COMMAND#
01898> R0088:C00001-----
01899> START
01900> [TZERO = .00 hrs on 19880101]
01901> [METOUT= 2 (1=imperial, 2=metric output)]
01902> [NSTORM= 0 ]
01903> [NRUN = 0088 ]
01904> #*****
01905> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
01906> #*****
01907> # Project Name: Barrhaven Conservancy Development
01908> # Project Number: 1474
01909> # Date : 2021/Oct/18
01910> # Modeller : J.Burnett, P.Eng.
01911> # Updated : 2022/Dec/07 [JB]
01912> # Updated : 2022/Dec/13 [LP]
01913> # Company : J.F. Sabourin and Associates
01914> # License # : 2582634
01915> #*****
01916> # Ottawa International Airport (1967 - 2003)
01917> R0088:C00002-----
01918> * READ AES DATA
01919> [Filename = YOW_1967_2007.123 ]
01920> [Start_date= 1988.0101: End_date= 1988.1230]
01921> {DT= 60.min: Length= 8760.hrs: WetHrs= 487: DryHrs= 8273: PTOT= 643.80}
01922> Maximum average rainfall intensities over
01923> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01924> 25.50 18.20 12.77 7.37 3.78 1.91 1.27 .95 .94 mm/hr
01925> 25.50 36.40 38.30 44.20 45.40 45.80 45.80 45.80 67.40 mm
01926> 19880917 19880726 19880625 19880625 19880625 19880625 19880625 19880626 19880625 date
01927> Number of rainfall events per following interevent time
01928> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01929> 165 130 109 80 66 56 49 42 26
01930> Number of events with at least the following durations
01931> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01932> 164 102 71 20 5 0 0 0 0
01933> R0088:C00003-----
01934> COMPUTE API
01935> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
01936> {APIimax= 66.04: APIavg= 18.06: APIimin= .03}
01937> #*****
01938> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01939> #*****
01940> R0088:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01941> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .323 1988.0625_13:50 75.66 .118 .000
01942> [CN= 76.0: N= 3.00: Tp= 1.29]
01943> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
01944> [InterEventTime= 12.00]
01945> R0088:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01946> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .226 1988.0625_13:45 66.49 .103 .000
01947> [CN= 72.0: N= 3.00: Tp= 1.18]
01948> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
01949> [InterEventTime= 12.00]
01950> R0088:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01951> ADD HYD 5.0 02:West-A 19.67 .323 1988.0625_13:50 75.66 n/a .000
01952> + 5.0 02:West-B 14.48 .226 1988.0625_13:45 66.49 n/a .000
01953> SUM= 5.0 01:West-Total 34.15 .548 1988.0625_13:45 71.77 n/a .000
01954> #*****
01955> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01956> #*****
01957> # Set infiltration to 0 (CN = 99.99) for water balance analysis
01958> #*****

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01959> R0088:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01960> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .676 1988.0625_13:35 255.71 .397 .000
01961> [CN=100.0: N= 3.00: Tp= 1.29]
01962> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01963> [InterEventTime= 12.00]
01964> R0088:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01965> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .526 1988.0625_13:30 255.71 .397 .000
01966> [CN=100.0: N= 3.00: Tp= 1.18]
01967> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
01968> [InterEventTime= 12.00]
01969> R0088:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01970> ADD HYD 5.0 02:INF-West-A 19.67 .676 1988.0625_13:35 255.71 n/a .000
01971> + 5.0 02:INF-West-B 14.48 .526 1988.0625_13:30 255.71 n/a .000
01972> SUM= 5.0 01:INF-West-T 34.15 1.202 1988.0625_13:30 255.71 n/a .000
01973> #####
01974> # CONTINUOUS RAINFALL DATA
01975> #####
01976> ** END OF RUN : 88
01977>
01978> *****
01979>
01980>
01981>
01982>
01983>
01984> RUN#:COMMAND#
01985> R0089:C00001-----
01986> START
01987> [TZERO = .00 hrs on 19890101]
01988> [METOUT= 2 (1=imperial, 2=metric output)]
01989> [NSTORM= 0]
01990> [NRUN = 0089]
01991> #####
01992> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
01993> #####
01994> # Project Name: Barrhaven Conservancy Development
01995> # Project Number: 1474
01996> # Date : 2021/Oct/18
01997> # Modeller : J.Burnett, P.Eng.
01998> # Updated : 2022/Dec/07 [JB]
01999> # Updated : 2022/Dec/13 [LP]
02000> # Company : J.F. Sabourin and Associates
02001> # License # : 2582634
02002> #####
02003> # Ottawa International Airport (1967 - 2003)
02004> R0089:C00002-----
02005> * READ AES DATA
02006> [Filename = YOW_1967_2007.123 ]
02007> [Start_date= 1989.0101: End_date= 1989.1231]
02008> {DT= 60.min: Length= 8040.hrs: WetHrs= 422: DryHrs= 7618: PTOT= 523.20}
02009> Maximum average rainfall intensities over
02010> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02011> 22.70 12.60 8.93 5.75 3.03 1.69 1.14 .86 .59 mm/hr
02012> 22.70 25.20 26.80 34.50 36.30 40.60 40.90 41.30 42.50 mm
02013> 19890727 19890727 19890727 19890727 19890727 19891021 19891021 19891021 19891022 date
02014> Number of rainfall events per following interevent time
02015> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02016> 151 125 108 89 67 53 42 37 29
02017> Number of events with at least the following durations
02018> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02019> 150 81 52 19 5 0 0 0 0
02020> R0089:C00003-----
02021> COMPUTE API
02022> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
02023> {APImax= 55.10: APIavg= 16.03: APImin= .02}
02024> #####
02025> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02026> #####
02027> R0089:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02028> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .141 1989.0727_16:15 47.58 .091 .000
02029> [CN= 76.0: N= 3.00: Tp= 1.29]
02030> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
02031> [InterEventTime= 12.00]
02032> R0089:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02033> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .095 1989.0727_16:10 41.43 .079 .000
02034> [CN= 72.0: N= 3.00: Tp= 1.18]
02035> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
02036> [InterEventTime= 12.00]
02037> R0089:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02038> ADD HYD 5.0 02:West-A 19.67 .141 1989.0727_16:15 47.58 n/a .000
02039> + 5.0 02:West-B 14.48 .095 1989.0727_16:10 41.43 n/a .000
02040> SUM= 5.0 01:West-Total 34.15 .236 1989.0727_16:15 44.97 n/a .000
02041> #####
02042> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02043> #####
02044> # Set infiltration to 0 (CN = 99.99) for water balance analysis
02045> #####
02046> R0089:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02047> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .477 1989.0727_16:00 197.69 .378 .000

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02048> [CN=100.0: N= 3.00: Tp= 1.29]
02049> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
02050> [InterEventTime= 12.00]
02051> R0089:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02052> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .377 1989.0727_15:55 197.69 .378 .000
02053> [CN=100.0: N= 3.00: Tp= 1.18]
02054> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
02055> [InterEventTime= 12.00]
02056> R0089:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02057> ADD HYD 5.0 02:INF-West-A 19.67 .477 1989.0727_16:00 197.69 n/a .000
02058> + 5.0 02:INF-West-B 14.48 .377 1989.0727_15:55 197.69 n/a .000
02059> SUM= 5.0 01:INF-West-T 34.15 .853 1989.0727_15:55 197.69 n/a .000
02060> #####
02061> # CONTINUOUS RAINFALL DATA
02062> #####
02063> ** END OF RUN : 89
02064>
02065> *****
02066>
02067>
02068>
02069>
02070>
02071> RUN#:COMMAND#
02072> R0090:C00001-----
02073> START
02074> [TZERO = .00 hrs on 19900101]
02075> [METOUT= 2 (1=imperial, 2=metric output)]
02076> [NSTORM= 0 ]
02077> [NRUN = 0090 ]
02078> #*****
02079> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
02080> #*****
02081> # Project Name: Barrhaven Conservancy Development
02082> # Project Number: 1474
02083> # Date : 2021/Oct/18
02084> # Modeller : J.Burnett, P.Eng.
02085> # Updated : 2022/Dec/07 [JB]
02086> # Updated : 2022/Dec/13 [LP]
02087> # Company : J.F. Sabourin and Associates
02088> # License # : 2582634
02089> #*****
02090> # Ottawa International Airport (1967 - 2003)
02091> R0090:C00002-----
02092> * READ AES DATA
02093> [Filename = YOW_1967_2007.123 ]
02094> [Start_date= 1990.0101: End_date= 1990.1231]
02095> [DT= 60.min: Length= 7344.hrs: WetHrs= 618: DryHrs= 6726: PTOT= 727.80]
02096> Maximum average rainfall intensities over
02097> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02098> 20.60 12.25 9.60 5.58 4.43 2.25 1.50 1.23 1.06 mm/hr
02099> 20.60 24.50 28.80 33.50 53.20 54.00 54.00 59.00 76.60 mm
02100> 19900720 19900720 19900828 19900828 19900720 19900720 19900720 19900722 19900723 date
02101> Number of rainfall events per following interevent time
02102> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02103> 204 156 141 107 84 66 56 47 33
02104> Number of events with at least the following durations
02105> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02106> 203 116 75 31 6 1 0 0 0
02107> R0090:C00003-----
02108> COMPUTE API
02109> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
02110> [APImax= 75.10: APIavg= 23.47: APImin= 3.10]
02111> #*****
02112> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02113> #*****
02114> R0090:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02115> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .265 1990.0720_14:15 96.52 .133 .000
02116> [CN= 76.0: N= 3.00: Tp= 1.29]
02117> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
02118> [InterEventTime= 12.00]
02119> R0090:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02120> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .185 1990.0720_14:10 85.06 .117 .000
02121> [CN= 72.0: N= 3.00: Tp= 1.18]
02122> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
02123> [InterEventTime= 12.00]
02124> R0090:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02125> ADD HYD 5.0 02:West-A 19.67 .265 1990.0720_14:15 96.52 n/a .000
02126> + 5.0 02:West-B 14.48 .185 1990.0720_14:10 85.06 n/a .000
02127> SUM= 5.0 01:West-Total 34.15 .450 1990.0720_14:10 91.66 n/a .000
02128> #*****
02129> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02130> #*****
02131> # Set infiltration to 0 (CN = 99.99) for water balance analysis
02132> #*****
02133> R0090:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02134> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .427 1990.0720_ 6:00 311.89 .429 .000
02135> [CN=100.0: N= 3.00: Tp= 1.29]
02136> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]

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02137> [InterEventTime= 12.00]
02138> R0090:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02139> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .337 1990.0720_ 5:55 311.89 .429 .000
02140> [CN=100.0: N= 3.00: Tp= 1.18]
02141> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
02142> [InterEventTime= 12.00]
02143> R0090:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02144> ADD HYD 5.0 02:INF-West-A 19.67 .427 1990.0720_ 6:00 311.89 n/a .000
02145> + 5.0 02:INF-West-B 14.48 .337 1990.0720_ 5:55 311.89 n/a .000
02146> SUM= 5.0 01:INF-West-T 34.15 .763 1990.0720_ 6:00 311.89 n/a .000
02147> #####
02148> # CONTINUOUS RAINFALL DATA
02149> #####
02150> ** END OF RUN : 90
02151>
02152> *****
02153>
02154>
02155>
02156>
02157>
02158> RUN#:COMMAND#
02159> R0091:C00001-----
02160> START
02161> [TZERO = .00 hrs on 19910101]
02162> [METOUT= 2 (1=imperial, 2=metric output)]
02163> [NSTORM= 0 ]
02164> [NRUN = 0091 ]
02165> #*****
02166> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
02167> #*****
02168> # Project Name: Barrhaven Conservancy Development
02169> # Project Number: 1474
02170> # Date : 2021/Oct/18
02171> # Modeller : J.Burnett, P.Eng.
02172> # Updated : 2022/Dec/07 [JB]
02173> # Updated : 2022/Dec/13 [LP]
02174> # Company : J.F. Sabourin and Associates
02175> # License # : 2582634
02176> #*****
02177> # Ottawa International Airport (1967 - 2003)
02178> R0091:C00002-----
02179> * READ AES DATA
02180> [Filename = YOW_1967_2007.123 ]
02181> [Start_date= 1991.0101: End_date= 1991.1231]
02182> [DT= 60.min: Length= 8040.hrs: WetHrs= 486: DryHrs= 7554: PTOT= 556.00]
02183> Maximum average rainfall intensities over
02184> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02185> 11.30 9.90 6.87 4.10 2.53 1.72 1.28 1.08 .79 mm/hr
02186> 11.30 19.80 20.60 24.60 30.40 41.20 46.00 51.60 57.00 mm
02187> 19910409 19910409 19910409 19910409 19911016 19910422 19910410 19910410 19910423 date
02188> Number of rainfall events per following interevent time
02189> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02190> 165 137 127 102 80 63 52 45 38
02191> Number of events with at least the following durations
02192> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02193> 164 89 56 21 6 1 0 0 0
02194> R0091:C00003-----
02195> COMPUTE API
02196> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
02197> [APImax= 72.80: APIavg= 16.88: APImin= .26]
02198> #*****
02199> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02200> #*****
02201> R0091:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02202> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .120 1991.0410_ 4:10 52.68 .095 .000
02203> [CN= 76.0: N= 3.00: Tp= 1.29]
02204> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
02205> [InterEventTime= 12.00]
02206> R0091:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02207> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .084 1991.0410_ 4:00 46.13 .083 .000
02208> [CN= 72.0: N= 3.00: Tp= 1.18]
02209> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
02210> [InterEventTime= 12.00]
02211> R0091:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02212> ADD HYD 5.0 02:West-A 19.67 .120 1991.0410_ 4:10 52.68 n/a .000
02213> + 5.0 02:West-B 14.48 .084 1991.0410_ 4:00 46.13 n/a .000
02214> SUM= 5.0 01:West-Total 34.15 .204 1991.0410_ 4:05 49.90 n/a .000
02215> #*****
02216> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02217> #*****
02218> # Set infiltration to 0 (CN = 99.99) for water balance analysis
02219> #*****
02220> R0091:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02221> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .267 1991.0409_ 1:50 197.89 .356 .000
02222> [CN=100.0: N= 3.00: Tp= 1.29]
02223> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
02224> [InterEventTime= 12.00]
02225> R0091:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms

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02226> CONTINUOUS NASHYD      5.0 01:INF-West-B   14.48   .211 1991.0409_ 1:45 197.89 .356   .000
02227> [CN=100.0: N= 3.00: Tp= 1.18]
02228> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
02229> [InterEventTime= 12.00]
02230> R0091:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02231> ADD HYD                5.0 02:INF-West-A   19.67   .267 1991.0409_ 1:50 197.89 n/a   .000
02232> +                      5.0 02:INF-West-B   14.48   .211 1991.0409_ 1:45 197.89 n/a   .000
02233> SUM=                   5.0 01:INF-West-T   34.15   .478 1991.0409_ 1:50 197.89 n/a   .000
02234> #####
02235> # CONTINUOUS RAINFALL DATA
02236> #####
02237> ** END OF RUN : 91
02238>
02239> *****
02240>
02241>
02242>
02243>
02244>
02245> RUN#:COMMAND#
02246> R0092:C00001-----
02247> START
02248> [TZERO = .00 hrs on 19920101]
02249> [METOUT= 2 (1=imperial, 2=metric output)]
02250> [NSTORM= 0 ]
02251> [NRUN = 0092 ]
02252> #*****
02253> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
02254> #*****
02255> # Project Name: Barrhaven Conservancy Development
02256> # Project Number: 1474
02257> # Date : 2021/Oct/18
02258> # Modeller : J.Burnett, P.Eng.
02259> # Updated : 2022/Dec/07 [JB]
02260> # Updated : 2022/Dec/13 [LP]
02261> # Company : J.F. Sabourin and Associates
02262> # License # : 2582634
02263> #*****
02264> # Ottawa International Airport (1967 - 2003)
02265> R0092:C00002-----
02266> * READ AES DATA
02267> [Filename = YOW_1967_2007.123 ]
02268> [Start_date= 1992.0101: End_date= 1992.1230]
02269> [DT= 60.min: Length= 8760.hrs: WetHrs= 551: DryHrs= 8209: PTOT= 732.80]
02270> Maximum average rainfall intensities over
02271> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02272> 31.50 18.00 13.30 7.22 4.14 2.26 1.51 1.51 1.02 mm/hr
02273> 31.50 36.00 39.90 43.30 49.70 54.20 54.20 72.60 73.60 mm
02274> 19920804 19920804 19920804 19920804 19920717 19920718 19920718 19920719 19920720 date
02275> Number of rainfall events per following interevent time
02276> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02277> 190 151 132 100 84 69 55 47 38
02278> Number of events with at least the following durations
02279> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02280> 189 109 70 22 5 1 0 0 0
02281> R0092:C00003-----
02282> COMPUTE API
02283> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
02284> [APImax= 97.62: APIavg= 20.33: APImin= 1.07]
02285> #*****
02286> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02287> #*****
02288> R0092:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02289> CONTINUOUS NASHYD      5.0 01:West-A   19.67   .416 1992.0717_19:25 106.69 .146   .000
02290> [CN= 76.0: N= 3.00: Tp= 1.29]
02291> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
02292> [InterEventTime= 12.00]
02293> R0092:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02294> CONTINUOUS NASHYD      5.0 01:West-B   14.48   .292 1992.0717_19:20 94.75 .129   .000
02295> [CN= 72.0: N= 3.00: Tp= 1.18]
02296> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
02297> [InterEventTime= 12.00]
02298> R0092:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02299> ADD HYD                5.0 02:West-A   19.67   .416 1992.0717_19:25 106.69 n/a   .000
02300> +                      5.0 02:West-B   14.48   .292 1992.0717_19:20 94.75 n/a   .000
02301> SUM=                   5.0 01:West-Total 34.15   .708 1992.0717_19:25 101.63 n/a   .000
02302> #*****
02303> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02304> #*****
02305> # Set infiltration to 0 (CN = 99.99) for water balance analysis
02306> #*****
02307> R0092:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02308> CONTINUOUS NASHYD      5.0 01:INF-West-A   19.67   .707 1992.0804_15:00 326.37 .445   .000
02309> [CN=100.0: N= 3.00: Tp= 1.29]
02310> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
02311> [InterEventTime= 12.00]
02312> R0092:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02313> CONTINUOUS NASHYD      5.0 01:INF-West-B   14.48   .559 1992.0804_14:50 326.37 .445   .000
02314> [CN=100.0: N= 3.00: Tp= 1.18]

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02315> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
02316> [InterEventTime= 12.00]
02317> R0092:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02318> ADD HYD 5.0 02:INF-West-A 19.67 .707 1992.0804_15:00 326.37 n/a .000
02319> + 5.0 02:INF-West-B 14.48 .559 1992.0804_14:50 326.37 n/a .000
02320> SUM= 5.0 01:INF-West-T 34.15 1.264 1992.0804_14:55 326.37 n/a .000
02321> #####
02322> # CONTINUOUS RAINFALL DATA
02323> #####
02324> ** END OF RUN : 92
02325>
02326> *****
02327>
02328>
02329>
02330>
02331>
02332> RUN#:COMMAND#
02333> R0093:C00001-----
02334> START
02335> [TZERO = .00 hrs on 19930101]
02336> [METOUT= 2 (1=imperial, 2=metric output)]
02337> [NSTORM= 0 ]
02338> [NRUN = 0093 ]
02339> #####
02340> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
02341> #####
02342> # Project Name: Barrhaven Conservancy Development
02343> # Project Number: 1474
02344> # Date : 2021/Oct/18
02345> # Modeller : J.Burnett, P.Eng.
02346> # Updated : 2022/Dec/07 [JB]
02347> # Updated : 2022/Dec/13 [LP]
02348> # Company : J.F. Sabourin and Associates
02349> # License # : 2582634
02350> #####
02351> # Ottawa International Airport (1967 - 2003)
02352> R0093:C00002-----
02353> * READ AES DATA
02354> [Filename = YOW_1967_2007.123 ]
02355> [Start_date= 1993.0101: End_date= 1993.1231]
02356> [DT= 60.min: Length= 8760.hrs: WetHrs= 585: DryHrs= 8175: PTOT= 721.30]
02357> Maximum average rainfall intensities over
02358> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02359> 12.60 6.60 4.83 3.72 3.58 2.31 1.61 1.21 .81 mm/hr
02360> 12.60 13.20 14.50 22.30 43.00 55.50 58.10 58.10 58.10 mm
02361> 19930703 19930703 19931127 19931128 19931128 19931128 19931128 19931128 19931129 date
02362> Number of rainfall events per following interevent time
02363> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02364> 191 154 137 111 91 73 57 48 34
02365> Number of events with at least the following durations
02366> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02367> 190 110 66 27 7 2 0 0 0
02368> R0093:C00003-----
02369> COMPUTE API
02370> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
02371> [APImax= 66.56: APIavg= 20.01: APImin= .11]
02372> #####
02373> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02374> #####
02375> R0093:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02376> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .153 1993.1128_ 7:40 71.45 .099 .000
02377> [CN= 76.0: N= 3.00: Tp= 1.29]
02378> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
02379> [InterEventTime= 12.00]
02380> R0093:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02381> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .105 1993.1128_ 7:35 62.59 .087 .000
02382> [CN= 72.0: N= 3.00: Tp= 1.18]
02383> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
02384> [InterEventTime= 12.00]
02385> R0093:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02386> ADD HYD 5.0 02:West-A 19.67 .153 1993.1128_ 7:40 71.45 n/a .000
02387> + 5.0 02:West-B 14.48 .105 1993.1128_ 7:35 62.59 n/a .000
02388> SUM= 5.0 01:West-Total 34.15 .258 1993.1128_ 7:40 67.69 n/a .000
02389> #####
02390> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02391> #####
02392> # Set infiltration to 0 (CN = 99.99) for water balance analysis
02393> #####
02394> R0093:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02395> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .236 1993.1128_ 7:25 264.26 .366 .000
02396> [CN=100.0: N= 3.00: Tp= 1.29]
02397> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
02398> [InterEventTime= 12.00]
02399> R0093:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02400> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .177 1993.1128_ 7:20 264.26 .366 .000
02401> [CN=100.0: N= 3.00: Tp= 1.18]
02402> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
02403> [InterEventTime= 12.00]

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02404> R0093:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02405>   ADD HYD                5.0 02:INF-West-A   19.67   .236 1993.1128_ 7:25  264.26  n/a   .000
02406>                +          5.0 02:INF-West-B   14.48   .177 1993.1128_ 7:20  264.26  n/a   .000
02407>                SUM=      5.0 01:INF-West-T   34.15   .413 1993.1128_ 7:25  264.26  n/a   .000
02408> #####
02409> # CONTINUOUS RAINFALL DATA
02410> #####
02411> ** END OF RUN : 93
02412>
02413> *****
02414>
02415>
02416>
02417>
02418>
02419> RUN#:COMMAND#
02420> R0094:C00001-----
02421>   START
02422>   [TZERO = .00 hrs on 19940101]
02423>   [METOUT= 2 (1=imperial, 2=metric output)]
02424>   [NSTORM= 0 ]
02425>   [NRUN = 0094 ]
02426> #*****
02427> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
02428> #*****
02429> # Project Name: Barrhaven Conservancy Development
02430> # Project Number: 1474
02431> # Date : 2021/Oct/18
02432> # Modeller : J.Burnett, P.Eng.
02433> # Updated : 2022/Dec/07 [JB]
02434> # Updated : 2022/Dec/13 [LP]
02435> # Company : J.F. Sabourin and Associates
02436> # License # : 2582634
02437> #*****
02438> # Ottawa International Airport (1967 - 2003)
02439> R0094:C00002-----
02440> * READ AES DATA
02441> [Filename = YOW_1967_2007.123 ]
02442> [Start_date= 1994.0101: End_date= 1994.1231]
02443> {DT= 60.min: Length= 8760.hrs: WetHrs= 342: DryHrs= 8418: PTOT= 540.20}
02444> Maximum average rainfall intensities over
02445> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02446> 22.60 11.90 8.43 5.42 2.92 1.79 1.19 .89 1.15 mm/hr
02447> 22.60 23.80 25.30 32.50 35.00 42.90 42.90 42.90 82.60 mm
02448> 19940629 19940629 19940627 19940625 19940625 19940625 19940626 19940626 19940627 date
02449> Number of rainfall events per following interevent time
02450> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02451> 138 115 101 79 62 48 39 34 26
02452> Number of events with at least the following durations
02453> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02454> 137 72 48 12 1 0 0 0 0
02455> R0094:C00003-----
02456> COMPUTE API
02457> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
02458> [APImax= 97.84: APIavg= 15.35: APImin= .02]
02459> #*****
02460> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02461> #*****
02462> R0094:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02463> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .153 1994.0627_11:40 67.89 .126 .000
02464> [CN= 76.0: N= 3.00: Tp= 1.29]
02465> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
02466> [InterEventTime= 12.00]
02467> R0094:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02468> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .103 1994.0627_11:35 59.78 .111 .000
02469> [CN= 72.0: N= 3.00: Tp= 1.18]
02470> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
02471> [InterEventTime= 12.00]
02472> R0094:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02473> ADD HYD                5.0 02:West-A   19.67   .153 1994.0627_11:40 67.89  n/a   .000
02474>                +          5.0 02:West-B   14.48   .103 1994.0627_11:35 59.78  n/a   .000
02475>                SUM=      5.0 01:West-Total 34.15   .256 1994.0627_11:35 64.45  n/a   .000
02476> #*****
02477> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02478> #*****
02479> # Set infiltration to 0 (CN = 99.99) for water balance analysis
02480> #*****
02481> R0094:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02482> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .383 1994.0627_11:05 227.40 .421 .000
02483> [CN=100.0: N= 3.00: Tp= 1.29]
02484> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
02485> [InterEventTime= 12.00]
02486> R0094:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02487> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .299 1994.0629_13:50 227.40 .421 .000
02488> [CN=100.0: N= 3.00: Tp= 1.18]
02489> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
02490> [InterEventTime= 12.00]
02491> R0094:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02492> ADD HYD                5.0 02:INF-West-A 19.67 .383 1994.0627_11:05 227.40 n/a .000

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02493>          +      5.0 02:INF-West-B   14.48   .299 1994.0629_13:50 227.40 n/a   .000
02494>          SUM=    5.0 01:INF-West-T   34.15   .675 1994.0627_11:00 227.40 n/a   .000
02495> #####
02496> # CONTINUOUS RAINFALL DATA
02497> #####
02498> ** END OF RUN :   94
02499>
02500> *****
02501>
02502>
02503>
02504>
02505>
02506> RUN#:COMMAND#
02507> R0095:C00001-----
02508> START
02509> [TZERO = .00 hrs on 19950101]
02510> [METOUT= 2 (1=imperial, 2=metric output)]
02511> [NSTORM= 0 ]
02512> [NRUN = 0095 ]
02513> #*****
02514> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
02515> #*****
02516> # Project Name: Barrhaven Conservancy Development
02517> # Project Number: 1474
02518> # Date : 2021/Oct/18
02519> # Modeller : J.Burnett, P.Eng.
02520> # Updated : 2022/Dec/07 [JB]
02521> # Updated : 2022/Dec/13 [LP]
02522> # Company : J.F. Sabourin and Associates
02523> # License # : 2582634
02524> #*****
02525> # Ottawa International Airport (1967 - 2003)
02526> R0095:C00002-----
02527> * READ AES DATA
02528> [Filename = YOW_1967_2007.123 ]
02529> [Start_date= 1995.0101: End_date= 1995.1231]
02530> {DT= 60.min: Length= 8040.hrs: WetHrs= 332: DryHrs= 7708: PTOT= 538.50}
02531> Maximum average rainfall intensities over
02532> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02533> 16.90 13.25 11.33 8.98 6.35 3.48 2.95 2.21 1.48 mm/hr
02534> 16.90 26.50 34.00 53.90 76.20 83.40 106.20 106.20 106.20 mm
02535> 19950603 19950603 19951006 19951006 19951006 19951006 19951007 19951007 19951008 date
02536> Number of rainfall events per following interevent time
02537> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02538> 91 73 65 55 47 41 34 31 25
02539> Number of events with at least the following durations
02540> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02541> 90 54 35 16 7 1 0 0 0
02542> R0095:C00003-----
02543> COMPUTE API
02544> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
02545> {APIimax= 99.57: APIavg= 16.58: APIimin= .00}
02546> #*****
02547> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02548> #*****
02549> R0095:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02550> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .427 1995.0603_ 9:35 172.16 .320 .000
02551> [CN= 76.0: N= 3.00: Tp= 1.29]
02552> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
02553> [InterEventTime= 12.00]
02554> R0095:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02555> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .310 1995.0603_ 9:30 159.14 .296 .000
02556> [CN= 72.0: N= 3.00: Tp= 1.18]
02557> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
02558> [InterEventTime= 12.00]
02559> R0095:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02560> ADD HYD 5.0 02:West-A 19.67 .427 1995.0603_ 9:35 172.16 n/a .000
02561> + 5.0 02:West-B 14.48 .310 1995.0603_ 9:30 159.14 n/a .000
02562> SUM= 5.0 01:West-Total 34.15 .737 1995.0603_ 9:35 166.64 n/a .000
02563> #*****
02564> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02565> #*****
02566> # Set infiltration to 0 (CN = 99.99) for water balance analysis
02567> #*****
02568> R0095:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02569> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .615 1995.1006_ 6:15 327.35 .608 .000
02570> [CN=100.0: N= 3.00: Tp= 1.29]
02571> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
02572> [InterEventTime= 12.00]
02573> R0095:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02574> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .462 1995.1006_ 6:05 327.35 .608 .000
02575> [CN=100.0: N= 3.00: Tp= 1.18]
02576> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
02577> [InterEventTime= 12.00]
02578> R0095:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02579> ADD HYD 5.0 02:INF-West-A 19.67 .615 1995.1006_ 6:15 327.35 n/a .000
02580> + 5.0 02:INF-West-B 14.48 .462 1995.1006_ 6:05 327.35 n/a .000
02581> SUM= 5.0 01:INF-West-T 34.15 1.076 1995.1006_ 6:10 327.35 n/a .000

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02582> #####
02583> # CONTINUOUS RAINFALL DATA
02584> #####
02585> ** END OF RUN : 95
02586>
02587> *****
02588>
02589>
02590>
02591>
02592>
02593> RUN#:COMMAND#
02594> R0096:C00001-----
02595> START
02596> [TZERO = .00 hrs on 19960101]
02597> [METOUT= 2 (1=imperial, 2=metric output)]
02598> [NSTORM= 0 ]
02599> [NRUN = 0096 ]
02600> #*****
02601> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
02602> #*****
02603> # Project Name: Barrhaven Conservancy Development
02604> # Project Number: 1474
02605> # Date : 2021/Oct/18
02606> # Modeller : J.Burnett, P.Eng.
02607> # Updated : 2022/Dec/07 [JB]
02608> # Updated : 2022/Dec/13 [LP]
02609> # Company : J.F. Sabourin and Associates
02610> # License # : 2582634
02611> #*****
02612> # Ottawa International Airport (1967 - 2003)
02613> R0096:C00002-----
02614> * READ AES DATA
02615> [Filename = YOW_1967_2007.123 ]
02616> [Start_date= 1996.0101: End_date= 1996.1230]
02617> [DT= 60.min: Length= 6552.hrs: WetHrs= 387: DryHrs= 6165: PTOT= 512.20]
02618> Maximum average rainfall intensities over
02619> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02620> 18.50 13.55 9.03 5.42 2.93 1.84 1.32 1.02 .70 mm/hr
02621> 18.50 27.10 27.10 32.50 35.10 44.10 47.50 49.00 50.30 mm
02622> 19960731 19960731 19960731 19960731 19960731 19961109 19961109 19961109 19961109 date
02623> Number of rainfall events per following interevent time
02624> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02625> 132 104 93 71 59 43 36 31 24
02626> Number of events with at least the following durations
02627> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02628> 131 72 50 19 2 1 0 0 0
02629> R0096:C00003-----
02630> COMPUTE API
02631> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
02632> [APIimax= 63.22: APIavg= 19.39: APIimin= .71]
02633> #*****
02634> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02635> #*****
02636> R0096:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02637> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .156 1996.0731_16:40 53.26 .104 .000
02638> [CN= 76.0: N= 3.00: Tp= 1.29]
02639> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
02640> [InterEventTime= 12.00]
02641> R0096:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02642> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .106 1996.0731_16:35 46.54 .091 .000
02643> [CN= 72.0: N= 3.00: Tp= 1.18]
02644> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
02645> [InterEventTime= 12.00]
02646> R0096:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02647> ADD HYD 5.0 02:West-A 19.67 .156 1996.0731_16:40 53.26 n/a .000
02648> + 5.0 02:West-B 14.48 .106 1996.0731_16:35 46.54 n/a .000
02649> SUM= 5.0 01:West-Total 34.15 .261 1996.0731_16:35 50.41 n/a .000
02650> #*****
02651> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02652> #*****
02653> # Set infiltration to 0 (CN = 99.99) for water balance analysis
02654> #*****
02655> R0096:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02656> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .438 1996.0731_16:25 195.06 .381 .000
02657> [CN=100.0: N= 3.00: Tp= 1.29]
02658> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
02659> [InterEventTime= 12.00]
02660> R0096:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02661> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .342 1996.0731_16:20 195.06 .381 .000
02662> [CN=100.0: N= 3.00: Tp= 1.18]
02663> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
02664> [InterEventTime= 12.00]
02665> R0096:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02666> ADD HYD 5.0 02:INF-West-A 19.67 .438 1996.0731_16:25 195.06 n/a .000
02667> + 5.0 02:INF-West-B 14.48 .342 1996.0731_16:20 195.06 n/a .000
02668> SUM= 5.0 01:INF-West-T 34.15 .778 1996.0731_16:25 195.06 n/a .000
02669> #####
02670> # CONTINUOUS RAINFALL DATA

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02671> #####
02672> ** END OF RUN : 96
02673>
02674> *****
02675>
02676>
02677>
02678>
02679>
02680> RUN#:COMMAND#
02681> R0097:C00001-----
02682> START
02683> [TZERO = .00 hrs on 19970101]
02684> [METOUT= 2 (1=imperial, 2=metric output)]
02685> [NSTORM= 0 ]
02686> [NRUN = 0097 ]
02687> #*****
02688> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
02689> #*****
02690> # Project Name: Barrhaven Conservancy Development
02691> # Project Number: 1474
02692> # Date : 2021/Oct/18
02693> # Modeller : J.Burnett, P.Eng.
02694> # Updated : 2022/Dec/07 [JB]
02695> # Updated : 2022/Dec/13 [LP]
02696> # Company : J.F. Sabourin and Associates
02697> # License # : 2582634
02698> #*****
02699> # Ottawa International Airport (1967 - 2003)
02700> R0097:C00002-----
02701> * READ AES DATA
02702> [Filename = YOW_1967_2007.123 ]
02703> [Start_date= 1997.0101: End_date= 1997.1231]
02704> [DT= 60.min: Length= 8040.hrs: WetHrs= 379: DryHrs= 7661: PTOT= 433.20]
02705> Maximum average rainfall intensities over
02706> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02707> 12.50 7.60 5.67 4.43 2.91 1.68 1.12 .84 .63 mm/hr
02708> 12.50 15.20 17.00 26.60 34.90 40.40 40.40 40.40 45.30 mm
02709> 19970622 19970622 19970622 19970221 19970222 19970222 19970222 19970222 19970222 date
02710> Number of rainfall events per following interevent time
02711> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02712> 113 92 83 67 61 55 48 43 30
02713> Number of events with at least the following durations
02714> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02715> 112 70 46 20 4 0 0 0 0
02716> R0097:C00003-----
02717> COMPUTE API
02718> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
02719> {APIimax= 50.00: APIavg= 13.66: APIimin= .27}
02720> #*****
02721> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02722> #*****
02723> R0097:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02724> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .093 1997.0221_21:45 32.31 .075 .000
02725> [CN= 76.0: N= 3.00: Tp= 1.29]
02726> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
02727> [InterEventTime= 12.00]
02728> R0097:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02729> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .062 1997.0221_21:40 27.92 .064 .000
02730> [CN= 72.0: N= 3.00: Tp= 1.18]
02731> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
02732> [InterEventTime= 12.00]
02733> R0097:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02734> ADD HYD 5.0 02:West-A 19.67 .093 1997.0221_21:45 32.31 n/a .000
02735> + 5.0 02:West-B 14.48 .062 1997.0221_21:40 27.92 n/a .000
02736> SUM= 5.0 01:West-Total 34.15 .155 1997.0221_21:40 30.45 n/a .000
02737> #*****
02738> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02739> #*****
02740> # Set infiltration to 0 (CN = 99.99) for water balance analysis
02741> #*****
02742> R0097:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02743> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .272 1997.0221_21:20 161.58 .373 .000
02744> [CN=100.0: N= 3.00: Tp= 1.29]
02745> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
02746> [InterEventTime= 12.00]
02747> R0097:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02748> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .204 1997.0221_21:20 161.58 .373 .000
02749> [CN=100.0: N= 3.00: Tp= 1.18]
02750> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
02751> [InterEventTime= 12.00]
02752> R0097:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02753> ADD HYD 5.0 02:INF-West-A 19.67 .272 1997.0221_21:20 161.58 n/a .000
02754> + 5.0 02:INF-West-B 14.48 .204 1997.0221_21:20 161.58 n/a .000
02755> SUM= 5.0 01:INF-West-T 34.15 .476 1997.0221_21:20 161.58 n/a .000
02756> #####
02757> # CONTINUOUS RAINFALL DATA
02758> #####
02759> ** END OF RUN : 97

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02760>
02761> *****
02762>
02763>
02764>
02765>
02766>
02767> RUN#:COMMAND#
02768> R0098:C00001-----
02769> START
02770> [TZERO = .00 hrs on 19980101]
02771> [METOUT= 2 (1=imperial, 2=metric output)]
02772> [NSTORM= 0 ]
02773> [NRRUN = 0098 ]
02774> #*****
02775> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
02776> #*****
02777> # Project Name: Barrhaven Conservancy Development
02778> # Project Number: 1474
02779> # Date : 2021/Oct/18
02780> # Modeller : J.Burnett, P.Eng.
02781> # Updated : 2022/Dec/07 [JB]
02782> # Updated : 2022/Dec/13 [LP]
02783> # Company : J.F. Sabourin and Associates
02784> # License # : 2582634
02785> #*****
02786> # Ottawa International Airport (1967 - 2003)
02787> R0098:C00002-----
02788> * READ AES DATA
02789> [Filename = YOW_1967_2007.123 ]
02790> [Start_date= 1998.0101: End_date= 1998.1231]
02791> [DT= 60.min: Length= 5088.hrs: WetHrs= 291: DryHrs= 4797: PTOT= 440.30]
02792> Maximum average rainfall intensities over
02793> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02794> 15.80 8.90 7.60 4.00 2.54 1.82 1.27 .95 .76 mm/hr
02795> 15.80 17.80 22.80 24.00 30.50 43.60 45.80 45.80 54.60 mm
02796> 19980716 19980627 19980927 19980927 19980927 19980927 19980928 19980928 19980615 date
02797> Number of rainfall events per following interevent time
02798> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02799> 126 104 95 78 63 42 37 32 21
02800> Number of events with at least the following durations
02801> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02802> 125 64 43 8 1 0 0 0 0
02803> R0098:C00003-----
02804> COMPUTE API
02805> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
02806> [APImax= 57.22: APIavg= 21.28: APImin= 1.69]
02807> #*****
02808> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02809> #*****
02810> R0098:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02811> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .099 1998.0927_15:15 37.63 .085 .000
02812> [CN= 76.0: N= 3.00: Tp= 1.29]
02813> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
02814> [InterEventTime= 12.00]
02815> R0098:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02816> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .069 1998.0927_15:10 32.64 .074 .000
02817> [CN= 72.0: N= 3.00: Tp= 1.18]
02818> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
02819> [InterEventTime= 12.00]
02820> R0098:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02821> ADD HYD 5.0 02:West-A 19.67 .099 1998.0927_15:15 37.63 n/a .000
02822> + 5.0 02:West-B 14.48 .069 1998.0927_15:10 32.64 n/a .000
02823> SUM= 5.0 01:West-Total 34.15 .167 1998.0927_15:10 35.52 n/a .000
02824> #*****
02825> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02826> #*****
02827> # Set infiltration to 0 (CN = 99.99) for water balance analysis
02828> #*****
02829> R0098:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02830> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .285 1998.0627_ 2:00 163.10 .370 .000
02831> [CN=100.0: N= 3.00: Tp= 1.29]
02832> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
02833> [InterEventTime= 12.00]
02834> R0098:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02835> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .226 1998.0627_ 1:55 163.10 .370 .000
02836> [CN=100.0: N= 3.00: Tp= 1.18]
02837> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
02838> [InterEventTime= 12.00]
02839> R0098:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02840> ADD HYD 5.0 02:INF-West-A 19.67 .285 1998.0627_ 2:00 163.11 n/a .000
02841> + 5.0 02:INF-West-B 14.48 .226 1998.0627_ 1:55 163.10 n/a .000
02842> SUM= 5.0 01:INF-West-T 34.15 .509 1998.0627_ 1:55 163.10 n/a .000
02843> #####
02844> # CONTINUOUS RAINFALL DATA
02845> #####
02846> ** END OF RUN : 98
02847>
02848> *****

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02849>
02850>
02851>
02852>
02853>
02854> RUN#:COMMAND#
02855> R0099:C00001-----
02856> START
02857> [TZERO = .00 hrs on 19990101]
02858> [METOUT= 2 (1=imperial, 2=metric output)]
02859> [NSTORM= 0 ]
02860> [NRUN = 0099 ]
02861> #*****
02862> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
02863> #*****
02864> # Project Name: Barrhaven Conservancy Development
02865> # Project Number: 1474
02866> # Date : 2021/Oct/18
02867> # Modeller : J.Burnett, P.Eng.
02868> # Updated : 2022/Dec/07 [JB]
02869> # Updated : 2022/Dec/13 [LP]
02870> # Company : J.F. Sabourin and Associates
02871> # License # : 2582634
02872> #*****
02873> # Ottawa International Airport (1967 - 2003)
02874> R0099:C00002-----
02875> * READ AES DATA
02876> [Filename = YOW_1967_2007.123 ]
02877> [Start_date= 1999.0101: End_date= 1999.1231]
02878> [DT= 60.min: Length= 4440.hrs: WetHrs= 247: DryHrs= 4193: PTOT= 424.40]
02879> Maximum average rainfall intensities over
02880> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02881> 17.50 10.10 9.03 6.57 3.31 1.65 1.45 1.22 .97 mm/hr
02882> 17.50 20.20 27.10 39.40 39.70 39.70 52.20 58.60 69.50 mm
02883> 19990717 19990717 19990906 19990906 19990906 19990906 19990907 19990908 19990908 date
02884> Number of rainfall events per following interevent time
02885> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02886> 102 80 70 63 56 39 31 28 18
02887> Number of events with at least the following durations
02888> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02889> 101 57 31 10 1 0 0 0 0
02890> R0099:C00003-----
02891> COMPUTE API
02892> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
02893> [APImax= 69.51: APIavg= 23.97: APImin= 1.93]
02894> #*****
02895> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02896> #*****
02897> R0099:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02898> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .141 1999.0906_10:20 38.58 .091 .000
02899> [CN= 76.0: N= 3.00: Tp= 1.29]
02900> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
02901> [InterEventTime= 12.00]
02902> R0099:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02903> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .093 1999.0906_10:15 33.50 .079 .000
02904> [CN= 72.0: N= 3.00: Tp= 1.18]
02905> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
02906> [InterEventTime= 12.00]
02907> R0099:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02908> ADD HYD 5.0 02:West-A 19.67 .141 1999.0906_10:20 38.58 n/a .000
02909> + 5.0 02:West-B 14.48 .093 1999.0906_10:15 33.50 n/a .000
02910> SUM= 5.0 01:West-Total 34.15 .234 1999.0906_10:20 36.42 n/a .000
02911> #*****
02912> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02913> #*****
02914> # Set infiltration to 0 (CN = 99.99) for water balance analysis
02915> #*****
02916> R0099:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02917> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .419 1999.0906_ 9:15 171.71 .405 .000
02918> [CN=100.0: N= 3.00: Tp= 1.29]
02919> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
02920> [InterEventTime= 12.00]
02921> R0099:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02922> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .319 1999.0906_ 9:10 171.71 .405 .000
02923> [CN=100.0: N= 3.00: Tp= 1.18]
02924> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
02925> [InterEventTime= 12.00]
02926> R0099:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02927> ADD HYD 5.0 02:INF-West-A 19.67 .419 1999.0906_ 9:15 171.71 n/a .000
02928> + 5.0 02:INF-West-B 14.48 .319 1999.0906_ 9:10 171.71 n/a .000
02929> SUM= 5.0 01:INF-West-T 34.15 .737 1999.0906_ 9:15 171.71 n/a .000
02930> #####
02931> # CONTINUOUS RAINFALL DATA
02932> #####
02933> ** END OF RUN : 99
02934>
02935> *****
02936>
02937>

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02938>
02939>
02940>
02941> RUN#:COMMAND#
02942> R0100:C00001-----
02943> START
02944> [TZERO = .00 hrs on 20000101]
02945> [METOUT= 2 (1=imperial, 2=metric output)]
02946> [NSTORM= 0 ]
02947> [NRUN = 0100 ]
02948> #*****
02949> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
02950> #*****
02951> # Project Name: Barrhaven Conservancy Development
02952> # Project Number: 1474
02953> # Date : 2021/Oct/18
02954> # Modeller : J.Burnett, P.Eng.
02955> # Updated : 2022/Dec/07 [JB]
02956> # Updated : 2022/Dec/13 [LP]
02957> # Company : J.F. Sabourin and Associates
02958> # License # : 2582634
02959> #*****
02960> # Ottawa International Airport (1967 - 2003)
02961> R0100:C00002-----
02962> * READ AES DATA
02963> [Filename = YOW_1967_2007.123 ]
02964> [Start_date= 2000.0101: End_date= 2000.1230]
02965> [DT= 60.min: Length= 5160.hrs: WetHrs= 401: DryHrs= 4759: PTOT= 535.90]
02966> Maximum average rainfall intensities over
02967> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02968> 14.70 9.60 8.03 6.43 3.89 1.95 1.30 1.03 .84 mm/hr
02969> 14.70 19.20 24.10 38.60 46.70 46.70 46.80 49.30 60.40 mm
02970> 20000625 20000625 20000625 20000625 20000625 20000625 20000626 20000510 20000511 date
02971> Number of rainfall events per following interevent time
02972> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02973> 156 125 110 86 67 46 34 30 23
02974> Number of events with at least the following durations
02975> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02976> 155 82 49 16 2 0 0 0 0
02977> R0100:C00003-----
02978> COMPUTE API
02979> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
02980> [APImax= 76.65: APIavg= 25.66: APImin= 5.70]
02981> #*****
02982> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02983> #*****
02984> R0100:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02985> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .291 2000.0625_10:50 63.91 .119 .000
02986> [CN= 76.0: N= 3.00: Tp= 1.29]
02987> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
02988> [InterEventTime= 12.00]
02989> R0100:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02990> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .205 2000.0625_10:45 56.28 .105 .000
02991> [CN= 72.0: N= 3.00: Tp= 1.18]
02992> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
02993> [InterEventTime= 12.00]
02994> R0100:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02995> ADD HYD 5.0 02:West-A 19.67 .291 2000.0625_10:50 63.91 n/a .000
02996> + 5.0 02:West-B 14.48 .205 2000.0625_10:45 56.28 n/a .000
02997> SUM= 5.0 01:West-Total 34.15 .496 2000.0625_10:45 60.67 n/a .000
02998> #*****
02999> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
03000> #*****
03001> # Set infiltration to 0 (CN = 99.99) for water balance analysis
03002> #*****
03003> R0100:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03004> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .460 2000.0625_10:35 214.65 .401 .000
03005> [CN=100.0: N= 3.00: Tp= 1.29]
03006> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
03007> [InterEventTime= 12.00]
03008> R0100:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03009> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .353 2000.0625_10:35 214.65 .401 .000
03010> [CN=100.0: N= 3.00: Tp= 1.18]
03011> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
03012> [InterEventTime= 12.00]
03013> R0100:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03014> ADD HYD 5.0 02:INF-West-A 19.67 .460 2000.0625_10:35 214.65 n/a .000
03015> + 5.0 02:INF-West-B 14.48 .353 2000.0625_10:35 214.65 n/a .000
03016> SUM= 5.0 01:INF-West-T 34.15 .813 2000.0625_10:35 214.65 n/a .000
03017> #####
03018> # CONTINUOUS RAINFALL DATA
03019> #####
03020> ** END OF RUN : 101
03021>
03022> *****
03023>
03024>
03025>
03026>

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03027>
03028> RUN#:COMMAND#
03029> R0102:C00001-----
03030> START
03031> [TZERO = .00 hrs on 20020101]
03032> [METOUT= 2 (1=imperial, 2=metric output)]
03033> [NSTORM= 0 ]
03034> [NRUN = 0102 ]
03035> #*****
03036> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
03037> #*****
03038> # Project Name: Barrhaven Conservancy Development
03039> # Project Number: 1474
03040> # Date : 2021/Oct/18
03041> # Modeller : J.Burnett, P.Eng.
03042> # Updated : 2022/Dec/07 [JB]
03043> # Updated : 2022/Dec/13 [LP]
03044> # Company : J.F. Sabourin and Associates
03045> # License # : 2582634
03046> #*****
03047> # Ottawa International Airport (1967 - 2003)
03048> R0102:C00002-----
03049> * READ AES DATA
03050> [Filename = YOW_1967_2007.123 ]
03051> [Start_date= 2002.0101: End_date= 2002.1231]
03052> [DT= 60.min: Length= 5088.hrs: WetHrs= 304: DryHrs= 4784: PTOT= 551.50]
03053> Maximum average rainfall intensities over
03054> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03055> 45.00 26.75 18.40 9.48 4.74 2.48 2.08 1.56 1.04 mm/hr
03056> 45.00 53.50 55.20 56.90 56.90 59.50 74.90 74.90 74.90 mm
03057> 20020627 20020627 20020627 20020627 20020627 20020627 20020627 20020628 20020629 date
03058> Number of rainfall events per following interevent time
03059> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03060> 100 83 78 56 47 41 36 34 25
03061> Number of events with at least the following durations
03062> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03063> 100 59 33 13 5 0 0 0 0
03064> R0102:C00003-----
03065> COMPUTE API
03066> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
03067> [APImax=114.06: APIavg= 26.37: APImin= 4.40]
03068> #*****
03069> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
03070> #*****
03071> R0102:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03072> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .618 2002.0627_15:00 114.49 .208 .000
03073> [CN= 76.0: N= 3.00: Tp= 1.29]
03074> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
03075> [InterEventTime= 12.00]
03076> R0102:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03077> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .449 2002.0627_14:55 103.15 .187 .000
03078> [CN= 72.0: N= 3.00: Tp= 1.18]
03079> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
03080> [InterEventTime= 12.00]
03081> R0102:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03082> ADD HYD 5.0 02:West-A 19.67 .618 2002.0627_15:00 114.49 n/a .000
03083> + 5.0 02:West-B 14.48 .449 2002.0627_14:55 103.15 n/a .000
03084> SUM= 5.0 01:West-Total 34.15 1.064 2002.0627_15:00 109.69 n/a .000
03085> #*****
03086> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
03087> #*****
03088> # Set infiltration to 0 (CN = 99.99) for water balance analysis
03089> #*****
03090> R0102:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03091> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 1.037 2002.0627_14:50 294.04 .533 .000
03092> [CN=100.0: N= 3.00: Tp= 1.29]
03093> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
03094> [InterEventTime= 12.00]
03095> R0102:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03096> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .824 2002.0627_14:45 294.04 .533 .000
03097> [CN=100.0: N= 3.00: Tp= 1.18]
03098> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
03099> [InterEventTime= 12.00]
03100> R0102:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03101> ADD HYD 5.0 02:INF-West-A 19.67 1.037 2002.0627_14:50 294.04 n/a .000
03102> + 5.0 02:INF-West-B 14.48 .824 2002.0627_14:45 294.04 n/a .000
03103> SUM= 5.0 01:INF-West-T 34.15 1.857 2002.0627_14:45 294.04 n/a .000
03104> #####
03105> # CONTINUOUS RAINFALL DATA
03106> #####
03107> ** END OF RUN : 102
03108>
03109> *****
03110>
03111>
03112>
03113>
03114>
03115> RUN#:COMMAND#

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03116> R0103:C00001-----
03117> START
03118> [TZERO = .00 hrs on 20030101]
03119> [METOUT= 2 (1=imperial, 2=metric output)]
03120> [NSTORM= 0 ]
03121> [NRUN = 0103 ]
03122> #*****
03123> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
03124> #*****
03125> # Project Name: Barrhaven Conservancy Development
03126> # Project Number: 1474
03127> # Date : 2021/Oct/18
03128> # Modeller : J.Burnett, P.Eng.
03129> # Updated : 2022/Dec/07 [JB]
03130> # Updated : 2022/Dec/13 [LP]
03131> # Company : J.F. Sabourin and Associates
03132> # License # : 2582634
03133> #*****
03134> # Ottawa International Airport (1967 - 2003)
03135> R0103:C00002-----
03136> * READ AES DATA
03137> [Filename = YOW_1967_2007.123 ]
03138> [Start_date= 2003.0101: End_date= 2003.1231]
03139> {DT= 60.min: Length= 4440.hrs: WetHrs= 406: DryHrs= 4034: PTOT= 554.60}
03140> Maximum average rainfall intensities over
03141> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03142> 15.10 10.00 7.13 4.28 3.18 1.86 1.25 .94 .81 mm/hr
03143> 15.10 20.00 21.40 25.70 38.20 44.60 44.90 45.10 58.30 mm
03144> 20030711 20030711 20030711 20030711 20031021 20031015 20030525 20030526 20030527 date
03145> Number of rainfall events per following interevent time
03146> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03147> 145 127 109 86 64 45 38 25 15
03148> Number of events with at least the following durations
03149> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03150> 144 80 43 13 5 1 0 0 0
03151> R0103:C00003-----
03152> COMPUTE API
03153> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
03154> [APImax= 72.10: APIavg= 28.54: APImin= 4.70]
03155> #*****
03156> # Barrhaven Conservancy West Developments (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
03157> #*****
03158> R0103:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
03159> CONTINUOUS NASHYD 5.0 01:West-A 19.67 .211 2003.0711_17:50 86.07 .155 .000
03160> [CN= 76.0: N= 3.00: Tp= 1.29]
03161> [IaREC= 6.00: SMIN= 32.46: SMAX=216.39: SK= .030]
03162> [InterEventTime= 12.00]
03163> R0103:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
03164> CONTINUOUS NASHYD 5.0 01:West-B 14.48 .147 2003.0711_17:45 76.16 .137 .000
03165> [CN= 72.0: N= 3.00: Tp= 1.18]
03166> [IaREC= 6.00: SMIN= 39.75: SMAX=264.99: SK= .030]
03167> [InterEventTime= 12.00]
03168> R0103:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
03169> ADD HYD 5.0 02:West-A 19.67 .211 2003.0711_17:50 86.07 n/a .000
03170> + 5.0 02:West-B 14.48 .147 2003.0711_17:45 76.16 n/a .000
03171> SUM= 5.0 01:West-Total 34.15 .358 2003.0711_17:50 81.87 n/a .000
03172> #*****
03173> # Barrhaven Conservancy West Developments (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
03174> #*****
03175> # Set infiltration to 0 (CN = 99.99) for water balance analysis
03176> #*****
03177> R0103:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
03178> CONTINUOUS NASHYD 5.0 01:INF-West-A 19.67 .430 2003.0711_17:40 251.88 .454 .000
03179> [CN=100.0: N= 3.00: Tp= 1.29]
03180> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
03181> [InterEventTime= 12.00]
03182> R0103:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
03183> CONTINUOUS NASHYD 5.0 01:INF-West-B 14.48 .337 2003.0711_17:35 251.88 .454 .000
03184> [CN=100.0: N= 3.00: Tp= 1.18]
03185> [IaREC= 6.00: SMIN= 1.39: SMAX= 9.24: SK= .030]
03186> [InterEventTime= 12.00]
03187> R0103:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
03188> ADD HYD 5.0 02:INF-West-A 19.67 .430 2003.0711_17:40 251.88 n/a .000
03189> + 5.0 02:INF-West-B 14.48 .337 2003.0711_17:35 251.88 n/a .000
03190> SUM= 5.0 01:INF-West-T 34.15 .766 2003.0711_17:40 251.88 n/a .000
03191> #####
03192> # CONTINUOUS RAINFALL DATA
03193> #####
03194> R0103:C00002-----
03195> FINISH
03196> -----
03197> *****
03198> WARNINGS / ERRORS / NOTES
03199> -----
03200> R0067:C00002 READ AES DATA
03201> *** WARNING: Requested start date is less than start date in file.
03202> *** WARNING: Missing rainfall increments were set to 0.
03203> *** WARNING: Missing rainfall increments were set to 0.
03204> *** WARNING: Missing rainfall increments were set to 0.

```

03205> *** WARNING: Missing rainfall increments were set to 0.
03206> *** WARNING: Missing rainfall increments were set to 0.
03207> *** WARNING: Missing rainfall increments were set to 0.
03208> *** WARNING: Missing rainfall increments were set to 0.
03209> *** WARNING: Missing rainfall increments were set to 0.
03210> *** WARNING: Missing rainfall increments were set to 0.
03211> *** WARNING: Missing rainfall increments were set to 0.
03212> *** WARNING: Requested start date is less than start date in file.
03213> *** WARNING: Missing rainfall increments were set to 0.
03214> *** WARNING: Missing rainfall increments were set to 0.
03215> *** WARNING: Missing rainfall increments were set to 0.
03216> *** WARNING: Missing rainfall increments were set to 0.
03217> *** WARNING: Missing rainfall increments were set to 0.
03218> *** WARNING: Missing rainfall increments were set to 0.
03219> *** WARNING: Missing rainfall increments were set to 0.
03220> *** WARNING: Missing rainfall increments were set to 0.
03221> *** WARNING: Missing rainfall increments were set to 0.
03222> *** WARNING: Missing rainfall increments were set to 0.
03223> *** WARNING: Requested start date is less than start date in file.
03224> *** WARNING: Missing rainfall increments were set to 0.
03225> *** WARNING: Missing rainfall increments were set to 0.
03226> *** WARNING: Missing rainfall increments were set to 0.
03227> *** WARNING: Requested start date is less than start date in file.
03228> *** WARNING: Missing rainfall increments were set to 0.
03229> *** WARNING: Missing rainfall increments were set to 0.
03230> *** WARNING: Missing rainfall increments were set to 0.
03231> *** WARNING: Missing rainfall increments were set to 0.
03232> *** WARNING: Missing rainfall increments were set to 0.
03233> *** WARNING: Missing rainfall increments were set to 0.
03234> *** WARNING: Requested start date is less than start date in file.
03235> *** WARNING: Missing rainfall increments were set to 0.
03236> *** WARNING: Missing rainfall increments were set to 0.
03237> *** WARNING: Requested start date is less than start date in file.
03238> *** WARNING: Missing rainfall increments were set to 0.
03239> *** WARNING: Requested start date is less than start date in file.
03240> *** WARNING: Missing rainfall increments were set to 0.
03241> *** WARNING: Requested start date is less than start date in file.
03242> *** WARNING: Missing rainfall increments were set to 0.
03243> *** WARNING: Requested start date is less than start date in file.
03244> *** WARNING: Missing rainfall increments were set to 0.
03245> *** WARNING: Requested start date is less than start date in file.
03246> *** WARNING: Missing rainfall increments were set to 0.
03247> Simulation ended on 2022-12-13 at 12:43:47
03248> =====
03249>
03250>


```

00001> 20      Metric units / ID Numbers OFF
00002> *#*****
00003> *# SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00004> *#*****
00005> *# Project Name: Barrhaven Conservancy Development
00006> *# Project Number: 1474
00007> *# Date       : 2021/Oct/18
00008> *# Modeller   : J.Burnett, P.Eng.
00009> *# Updated    : 2022/Dec/13 [LP]
00010> *# Company    : J.F. Sabourin and Associates
00011> *# License #  : 2582634
00012> *#*****
00013> START      TZERO=[1967.0101], METOUT=[2], NSTORM=[0], NRUN=[67]
00014> *%-----|-----
00015> *%-----|-----
00016> *# Ottawa International Airport (1967 - 2003)
00017> READ AES DATA  AES_FILENAME=["YOW_1967_2007.123"],
00018>                IELEM=[123], START_DATE=[0], END_DATE=[-364]
00019> *%-----|-----
00020> COMPUTE API    APII=[50], APIK=[0.90]/day
00021> *%-----|-----
00022> *#*****
00023> *# Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITIO
00024> *#*****
00025> *%-----|-----
00026> CONTINUOUS STANDHYD  NHYD=["W1"], DT=[5] (min), AREA=[8.92] (ha)
00027>                XIMP=[0.66], TIMP=[0.71], DWF=[0] (cms),
00028>                LOSS=[2]: SCS curve number CN=[71],
00029>                Pervious areas: IAper=[4.67] (mm), SLPP=[2.0] (%), LGP=[40] (m), MNP=[0.250], SCP=[0] (min),
00030>                Impervious areas: IAimp=[1.57] (mm), SLPI=[0.5] (%), LGI=[244] (m), MNI=[0.013], SCI=[0] (min)
00031>                Continuous simulation parameters:
00032>                IaRECper=[6] (hrs), IaRECimp=[1.5] (hrs),
00033>                SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.03]/(mm), InterEventTime=[12] (hrs), END=-1
00034> *%-----|-----
00035> *# LID for Outlet W1 (26 catchbasins, 30 m long trench each)
00036> *# Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
00037> *# Total Volume provided by LID - 179 m3
00038> *# Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00039> ROUTE RESERVOIR    NHYDout=["W1-LID"], NHYDin=["W1"], RDT=[5] (min),
00040>                TABLE of ( OUTFLOW-STORAGE ) values
00041>                (cms) - (ha-m)
00042>                [ 0.0000 , 0.0000 ]
00043>                [ 0.0009 , 0.0001 ]
00044>                [ 0.0010 , 0.0179 ]
00045>                [ -1 , -1 ]
00046>                NHYDovf=["W1-LID-Out"],
00047> *%-----|-----
00048> CONTINUOUS STANDHYD  NHYD=["W2"], DT=[5] (min), AREA=[10.75] (ha)
00049>                XIMP=[0.65], TIMP=[0.70], DWF=[0] (cms),
00050>                LOSS=[2]: SCS curve number CN=[71],
00051>                Pervious areas: IAper=[4.67] (mm), SLPP=[2.0] (%), LGP=[40] (m), MNP=[0.250], SCP=[0] (min),
00052>                Impervious areas: IAimp=[1.57] (mm), SLPI=[0.5] (%), LGI=[268] (m), MNI=[0.013], SCI=[0] (min)
00053>                Continuous simulation parameters:
00054>                IaRECper=[6] (hrs), IaRECimp=[1.5] (hrs),
00055>                SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.03]/(mm), InterEventTime=[12] (hrs), END=-1
00056> *%-----|-----
00057> *# LID for Outlet W2 (29 catchbasins, 30 m long trench each)
00058> *# Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pip
00059> *# Total Volume provided by LID - 200 m3
00060> *# Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00061> ROUTE RESERVOIR    NHYDout=["W2-LID"], NHYDin=["W2"], RDT=[5] (min),
00062>                TABLE of ( OUTFLOW-STORAGE ) values
00063>                (cms) - (ha-m)
00064>                [ 0.0000 , 0.0000 ]
00065>                [ 0.0010 , 0.0001 ]
00066>                [ 0.0011 , 0.0200 ]
00067>                [ -1 , -1 ]
00068>                NHYDovf=["W2-LID-Out"],
00069> *%-----|-----
00070> CONTINUOUS STANDHYD  NHYD=["W3"], DT=[5] (min), AREA=[6.30] (ha)
00071>                XIMP=[0.53], TIMP=[0.63], DWF=[0] (cms),
00072>                LOSS=[2]: SCS curve number CN=[71],
00073>                Pervious areas: IAper=[4.67] (mm), SLPP=[2.0] (%), LGP=[40] (m), MNP=[0.250], SCP=[0] (min),
00074>                Impervious areas: IAimp=[1.57] (mm), SLPI=[0.5] (%), LGI=[205] (m), MNI=[0.013], SCI=[0] (min)
00075>                Continuous simulation parameters:
00076>                IaRECper=[6] (hrs), IaRECimp=[1.5] (hrs),
00077>                SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.03]/(mm), InterEventTime=[12] (hrs), END=-1
00078> *%-----|-----
00079> *# LID for Outlet W3 (14 catchbasins, 30 m long trench each)
00080> *# Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pip
00081> *# Total Volume provided by LID - 96 m3
00082> *# Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00083> ROUTE RESERVOIR    NHYDout=["W3-LID"], NHYDin=["W3"], RDT=[5] (min),
00084>                TABLE of ( OUTFLOW-STORAGE ) values
00085>                (cms) - (ha-m)
00086>                [ 0.0000 , 0.0000 ]
00087>                [ 0.0004 , 0.0001 ]
00088>                [ 0.0005 , 0.0096 ]
00089>                [ -1 , -1 ]

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00090> NHYDovf=["W3-LID-Out"],
00091> *%-----|-----
00092> CONTINUOUS STANDHYD NHYD=["W4"], DT=[5] (min), AREA=[8.18] (ha)
00093> XIMP=[0.57], TIMP=[0.67], DWF=[0] (cms),
00094> LOSS=[2]: SCS curve number CN=[71],
00095> Pervious areas: IAper=[4.67] (mm), SLPP=[2.0] (%), LGP=[40] (m), MNP=[0.250], SCP=[0] (min),
00096> Impervious areas: IAimp=[1.57] (mm), SLPI=[0.5] (%), LGI=[234] (m), MNI=[0.013], SCI=[0] (min)
00097> Continuous simulation parameters:
00098> IaREcper=[6] (hrs), IaREcimp=[1.5] (hrs),
00099> SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.03]/(mm), InterEventTime=[12] (hrs), END=-1
00100> *%-----|-----
00101> *# LID for Outlet W4 (26 catchbasins, 30 m long trench each)
00102> *# Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pip
00103> *# Total Volume provided by LID - 131 m3
00104> *# Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00105> ROUTE RESERVOIR NHYD=["W4-LID"], NHYDin=["W4"], RDT=[5] (min),
00106> TABLE of ( OUTFLOW-STORAGE ) values
00107> (cms) - (ha-m)
00108> [ 0.0000 , 0.0000 ]
00109> [ 0.0006 , 0.0001 ]
00110> [ 0.0007 , 0.0131 ]
00111> [ -1 , -1 ]
00112> NHYDovf=["W4-LID-Out"],
00113> *%-----|-----
00114> *Development Without LIDs
00115> ADD HYD NHYDsum=["BCD-PH3"], NHYDs to add=["W1", "W2", "W3", "W4"]
00116> *%-----|-----
00117> *Development With LIDs
00118> ADD HYD NHYDsum=["BCD-PH3-LID"], NHYDs to add=["W1-LID-Out", "W2-LID-Out", "W3-LID-Out", "W4-LID-Out"]
00119> *%-----|-----
00120> *#*****
00121> *# Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDI
00122> *#*****
00123> *# Set infiltration to 0 (CN = 99.99) for water balance analysis
00124> *#*****
00125> CONTINUOUS STANDHYD NHYD=["INF-W1"], DT=[5] (min), AREA=[8.92] (ha)
00126> XIMP=[0.66], TIMP=[0.71], DWF=[0] (cms),
00127> LOSS=[2]: SCS curve number CN=[99.99],
00128> Pervious areas: IAper=[4.67] (mm), SLPP=[2.0] (%), LGP=[40] (m), MNP=[0.250], SCP=[0] (min),
00129> Impervious areas: IAimp=[1.57] (mm), SLPI=[0.5] (%), LGI=[244] (m), MNI=[0.013], SCI=[0] (min)
00130> Continuous simulation parameters:
00131> IaREcper=[6] (hrs), IaREcimp=[1.5] (hrs),
00132> SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.03]/(mm), InterEventTime=[12] (hrs), END=-1
00133> *%-----|-----
00134> CONTINUOUS STANDHYD NHYD=["INF-W2"], DT=[5] (min), AREA=[10.75] (ha)
00135> XIMP=[0.65], TIMP=[0.70], DWF=[0] (cms),
00136> LOSS=[2]: SCS curve number CN=[99.99],
00137> Pervious areas: IAper=[4.67] (mm), SLPP=[2.0] (%), LGP=[40] (m), MNP=[0.250], SCP=[0] (min),
00138> Impervious areas: IAimp=[1.57] (mm), SLPI=[0.5] (%), LGI=[268] (m), MNI=[0.013], SCI=[0] (min)
00139> Continuous simulation parameters:
00140> IaREcper=[6] (hrs), IaREcimp=[1.5] (hrs),
00141> SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.03]/(mm), InterEventTime=[12] (hrs), END=-1
00142> *%-----|-----
00143> CONTINUOUS STANDHYD NHYD=["INF-W3"], DT=[5] (min), AREA=[6.30] (ha)
00144> XIMP=[0.53], TIMP=[0.63], DWF=[0] (cms),
00145> LOSS=[2]: SCS curve number CN=[99.99],
00146> Pervious areas: IAper=[4.67] (mm), SLPP=[2.0] (%), LGP=[40] (m), MNP=[0.250], SCP=[0] (min),
00147> Impervious areas: IAimp=[1.57] (mm), SLPI=[0.5] (%), LGI=[205] (m), MNI=[0.013], SCI=[0] (min)
00148> Continuous simulation parameters:
00149> IaREcper=[6] (hrs), IaREcimp=[1.5] (hrs),
00150> SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.03]/(mm), InterEventTime=[12] (hrs), END=-1
00151> *%-----|-----
00152> CONTINUOUS STANDHYD NHYD=["INF-W4"], DT=[5] (min), AREA=[8.18] (ha)
00153> XIMP=[0.57], TIMP=[0.67], DWF=[0] (cms),
00154> LOSS=[2]: SCS curve number CN=[99.99],
00155> Pervious areas: IAper=[4.67] (mm), SLPP=[2.0] (%), LGP=[40] (m), MNP=[0.250], SCP=[0] (min),
00156> Impervious areas: IAimp=[1.57] (mm), SLPI=[0.5] (%), LGI=[234] (m), MNI=[0.013], SCI=[0] (min)
00157> Continuous simulation parameters:
00158> IaREcper=[6] (hrs), IaREcimp=[1.5] (hrs),
00159> SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.03]/(mm), InterEventTime=[12] (hrs), END=-1
00160> *%-----|-----
00161> *Development Without Infiltration for water budget
00162> ADD HYD NHYDsum=["INF-BCD-PH3"], NHYDs to add=["INF-W1", "INF-W2", "INF-W3", "INF-W4"]
00163> *%-----|-----
00164> *#*****
00165> *# CONTINUOUS RAINFALL DATA
00166> *#*****
00167> *%-----|-----
00168> *%-----|-----
00169> START TZERO=[1968.0101], METOUT=[2], NSTORM=[0], NRUN=[68]
00170> *%-----|-----
00171> START TZERO=[1969.0101], METOUT=[2], NSTORM=[0], NRUN=[69]
00172> *%-----|-----
00173> START TZERO=[1970.0101], METOUT=[2], NSTORM=[0], NRUN=[70]
00174> *%-----|-----
00175> START TZERO=[1971.0101], METOUT=[2], NSTORM=[0], NRUN=[71]
00176> *%-----|-----
00177> START TZERO=[1972.0101], METOUT=[2], NSTORM=[0], NRUN=[72]
00178> *%-----|-----

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00179> START          TZERO=[1973.0101], METOUT=[2], NSTORM=[0], NRUN=[73]
00180> *%-----|-----
00181> START          TZERO=[1974.0101], METOUT=[2], NSTORM=[0], NRUN=[74]
00182> *%-----|-----
00183> START          TZERO=[1975.0101], METOUT=[2], NSTORM=[0], NRUN=[75]
00184> *%-----|-----
00185> START          TZERO=[1976.0101], METOUT=[2], NSTORM=[0], NRUN=[76]
00186> *%-----|-----
00187> START          TZERO=[1977.0101], METOUT=[2], NSTORM=[0], NRUN=[77]
00188> *%-----|-----
00189> START          TZERO=[1978.0101], METOUT=[2], NSTORM=[0], NRUN=[78]
00190> *%-----|-----
00191> START          TZERO=[1979.0101], METOUT=[2], NSTORM=[0], NRUN=[79]
00192> *%-----|-----
00193> START          TZERO=[1980.0101], METOUT=[2], NSTORM=[0], NRUN=[80]
00194> *%-----|-----
00195> START          TZERO=[1981.0101], METOUT=[2], NSTORM=[0], NRUN=[81]
00196> *%-----|-----
00197> START          TZERO=[1982.0101], METOUT=[2], NSTORM=[0], NRUN=[82]
00198> *%-----|-----
00199> START          TZERO=[1983.0101], METOUT=[2], NSTORM=[0], NRUN=[83]
00200> *%-----|-----
00201> START          TZERO=[1984.0101], METOUT=[2], NSTORM=[0], NRUN=[84]
00202> *%-----|-----
00203> START          TZERO=[1985.0101], METOUT=[2], NSTORM=[0], NRUN=[85]
00204> *%-----|-----
00205> START          TZERO=[1986.0101], METOUT=[2], NSTORM=[0], NRUN=[86]
00206> *%-----|-----
00207> START          TZERO=[1987.0101], METOUT=[2], NSTORM=[0], NRUN=[87]
00208> *%-----|-----
00209> START          TZERO=[1988.0101], METOUT=[2], NSTORM=[0], NRUN=[88]
00210> *%-----|-----
00211> START          TZERO=[1989.0101], METOUT=[2], NSTORM=[0], NRUN=[89]
00212> *%-----|-----
00213> START          TZERO=[1990.0101], METOUT=[2], NSTORM=[0], NRUN=[90]
00214> *%-----|-----
00215> START          TZERO=[1991.0101], METOUT=[2], NSTORM=[0], NRUN=[91]
00216> *%-----|-----
00217> START          TZERO=[1992.0101], METOUT=[2], NSTORM=[0], NRUN=[92]
00218> *%-----|-----
00219> START          TZERO=[1993.0101], METOUT=[2], NSTORM=[0], NRUN=[93]
00220> *%-----|-----
00221> START          TZERO=[1994.0101], METOUT=[2], NSTORM=[0], NRUN=[94]
00222> *%-----|-----
00223> START          TZERO=[1995.0101], METOUT=[2], NSTORM=[0], NRUN=[95]
00224> *%-----|-----
00225> START          TZERO=[1996.0101], METOUT=[2], NSTORM=[0], NRUN=[96]
00226> *%-----|-----
00227> START          TZERO=[1997.0101], METOUT=[2], NSTORM=[0], NRUN=[97]
00228> *%-----|-----
00229> START          TZERO=[1998.0101], METOUT=[2], NSTORM=[0], NRUN=[98]
00230> *%-----|-----
00231> START          TZERO=[1999.0101], METOUT=[2], NSTORM=[0], NRUN=[99]
00232> *%-----|-----
00233> START          TZERO=[2000.0101], METOUT=[2], NSTORM=[0], NRUN=[100]
00234> *%-----|-----
00235> *% MISSING FROM AES RAINFALL DATA
00236> *%START          TZERO=[2001.0101], METOUT=[2], NSTORM=[0], NRUN=[101]
00237> *%-----|-----
00238> START          TZERO=[2002.0101], METOUT=[2], NSTORM=[0], NRUN=[102]
00239> *%-----|-----
00240> START          TZERO=[2003.0101], METOUT=[2], NSTORM=[0], NRUN=[103]
00241> *%-----|-----
00242> FINISH

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00001> =====
00002>
00003> SSSSS W W M M H H Y Y M M OOO 222 000 11 5555 =====
00004> S W W W MM MM H H Y Y MM MM O O 2 0 0 11 5
00005> SSSSS W W W M M M HHHHH Y M M M O O 2 0 0 11 5 Ver 5.500
00006> S W W M M H H Y M M O O 222 0 0 11 555 FEB 2015
00007> SSSSS W W M M H H Y M M OOO 2 0 0 11 5 =====
00008> 2 0 0 11 5 # 2549237
00009> StormWater Management HYdrologic Model 222 000 11 555 =====
00010>
00011> *****
00012> ***** SWMHYMO Ver 5.500 *****
00013> ***** A single event and continuous hydrologic simulation model *****
00014> ***** based on the principles of HYMO and its successors *****
00015> ***** OTHYMO-83 and OTHYMO-89. *****
00016> *****
00017> ***** Distributed by: J.F. Sabourin and Associates Inc. *****
00018> ***** Ottawa, Ontario: (613) 836-3884 *****
00019> ***** Gatineau, Quebec: (819) 243-6858 *****
00020> ***** E-Mail: swmhymo@jfsa.Com *****
00021> *****
00022>
00023> ++++++
00024> ++++++ Licensed user: JFSaInc. ++++++
00025> ++++++ Ottawa SERIAL#:2549237 ++++++
00026> ++++++
00027>
00028> *****
00029> ***** ++++++ PROGRAM ARRAY DIMENSIONS ++++++ *****
00030> ***** Maximum value for ID numbers : 11 *****
00031> ***** Max. number of rainfall points: 105408 *****
00032> ***** Max. number of flow points : 105408 *****
00033> *****
00034>
00035>
00036> ***** S U M M A R Y O U T P U T *****
00037> *****
00038> * RUN DATE: 2022-12-13 TIME: 12:43:53 RUN COUNTER: 004325 *
00039> *****
00040> * Input file: C:\Users\lpipk\Desktop\20221213-Post-Dev\BCD_PH3-POST_v02.dat *
00041> * Output file: C:\Users\lpipk\Desktop\20221213-Post-Dev\BCD_PH3-POST_v02.out *
00042> * Summary file: C:\Users\lpipk\Desktop\20221213-Post-Dev\BCD_PH3-POST_v02.sum *
00043> * User comments: *
00044> * 1: _____ *
00045> * 2: _____ *
00046> * 3: _____ *
00047> *****
00048>
00049>
00050> #*****
00051> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00052> #*****
00053> # Project Name: Barrhaven Conservancy Development
00054> # Project Number: 1474
00055> # Date : 2021/Oct/18
00056> # Modeller : J.Burnett, P.Eng.
00057> # Updated : 2022/Dec/13 [LP]
00058> # Company : J.F. Sabourin and Associates
00059> # License # : 2582634
00060> #*****
00061> ** END OF RUN : 66
00062>
00063> *****
00064>
00065>
00066>
00067>
00068>
00069> RUN#:COMMAND#
00070> R0067:C00001-----
00071> START
00072> [TZERO = .00 hrs on 19670101]
00073> [METOUT= 2 (1=imperial, 2=metric output)]
00074> [NSTORM= 0 ]
00075> [NRUN = 0067 ]
00076> #*****
00077> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00078> #*****
00079> # Project Name: Barrhaven Conservancy Development
00080> # Project Number: 1474
00081> # Date : 2021/Oct/18
00082> # Modeller : J.Burnett, P.Eng.
00083> # Updated : 2022/Dec/13 [LP]
00084> # Company : J.F. Sabourin and Associates
00085> # License # : 2582634
00086> #*****
00087> # Ottawa International Airport (1967 - 2003)
00088> R0067:C00002-----
00089> * READ AES DATA

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00090> [Filename = YOW_1967_2007.123 ]
00091> [Start_date= 1967.0101: End_date= 1967.1231]
00092> [DT= 60.min: Length= 3984.hrs: WetHrs= 257: DryHrs= 3727: PTOT= 386.90]
00093> Maximum average rainfall intensities over
00094> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00095> 24.60 17.65 13.20 7.25 3.83 2.36 1.73 1.32 .90 mm/hr
00096> 24.60 35.30 39.60 43.50 46.00 56.60 62.30 63.20 64.90 mm
00097> 19670921 19670921 19670921 19670921 19670921 19670922 19670923 19670924 date
00098> Number of rainfall events per following interevent time
00099> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00100> 80 65 56 40 32 29 24 20 18
00101> Number of events with at least the following durations
00102> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00103> 79 42 29 14 3 0 0 0 0
00104> R0067:C00003-----
00105> COMPUTE API
00106> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
00107> {APImax= 76.77: APIavg= 24.81: APImin= 3.06}
00108> #*****
00109> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
00110> #*****
00111> R0067:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00112> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .420 1967.0921_17:00 224.61 .581 .000
00113> [XIMP=.66:TIMP=.71]
00114> [LOSS= 2 :CN= 71.0]
00115> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00116> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
00117> [IaREcimp= 1.50: IaREcper= 6.00]
00118> [SMIN= 41.38: SMAX=275.84: SK= .030]
00119> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
00120> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
00121> # Total Volume provided by LID - 179 m³
00122> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00123> R0067:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00124> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .420 1967.0921_17:00 224.61 n/a .000
00125> out <= 5.0 01:W1-LID 1.87 .001 1967.0725_0:30 224.61 n/a .000
00126> overflow <= 5.0 03:W1-LID-Out 7.05 .416 1967.0921_17:00 224.61 n/a .000
00127> {MxStoUsed=.1789E-01 m3, TotOvfVol=.1585E+01 m3, N-Ovf= 66, TotDurOvf= 121.hrs}
00128> R0067:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00129> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .499 1967.0921_17:00 222.14 .574 .000
00130> [XIMP=.65:TIMP=.70]
00131> [LOSS= 2 :CN= 71.0]
00132> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00133> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
00134> [IaREcimp= 1.50: IaREcper= 6.00]
00135> [SMIN= 41.38: SMAX=275.84: SK= .030]
00136> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
00137> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
00138> # Total Volume provided by LID - 200 m³
00139> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00140> R0067:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00141> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .499 1967.0921_17:00 222.14 n/a .000
00142> out <= 5.0 01:W2-LID 2.12 .001 1967.0725_0:30 222.14 n/a .000
00143> overflow <= 5.0 03:W2-LID-Out 8.63 .493 1967.0921_17:00 222.14 n/a .000
00144> {MxStoUsed=.1999E-01 m3, TotOvfVol=.1918E+01 m3, N-Ovf= 72, TotDurOvf= 123.hrs}
00145> R0067:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00146> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .253 1967.0921_17:00 197.15 .510 .000
00147> [XIMP=.53:TIMP=.63]
00148> [LOSS= 2 :CN= 71.0]
00149> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00150> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
00151> [IaREcimp= 1.50: IaREcper= 6.00]
00152> [SMIN= 41.38: SMAX=275.84: SK= .030]
00153> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
00154> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
00155> # Total Volume provided by LID - 96 m³
00156> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00157> R0067:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00158> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .253 1967.0921_17:00 197.15 n/a .000
00159> out <= 5.0 01:W3-LID 1.12 .001 1967.0725_0:30 197.15 n/a .000
00160> overflow <= 5.0 03:W3-LID-Out 5.18 .248 1967.0921_17:00 197.15 n/a .000
00161> {MxStoUsed=.9598E-02 m3, TotOvfVol=.1022E+01 m3, N-Ovf= 77, TotDurOvf= 127.hrs}
00162> R0067:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00163> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .348 1967.0921_17:00 207.14 .535 .000
00164> [XIMP=.57:TIMP=.67]
00165> [LOSS= 2 :CN= 71.0]
00166> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00167> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
00168> [IaREcimp= 1.50: IaREcper= 6.00]
00169> [SMIN= 41.38: SMAX=275.84: SK= .030]
00170> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
00171> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
00172> # Total Volume provided by LID - 131 m³
00173> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00174> R0067:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00175> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .348 1967.0921_17:00 207.14 n/a .000
00176> out <= 5.0 01:W4-LID 1.47 .001 1967.0725_0:30 207.14 n/a .000
00177> overflow <= 5.0 03:W4-LID-Out 6.71 .343 1967.0921_17:00 207.14 n/a .000
00178> {MxStoUsed=.1309E-01 m3, TotOvfVol=.1390E+01 m3, N-Ovf= 66, TotDurOvf= 126.hrs}

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00179> R0067:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00180>   ADD HYD           5.0 02:W1           8.92   .420 1967.0921_17:00 224.61 n/a   .000
00181>           +           5.0 02:W2          10.75   .499 1967.0921_17:00 222.14 n/a   .000
00182>           +           5.0 02:W3           6.30    .253 1967.0921_17:00 197.15 n/a   .000
00183>           +           5.0 02:W4           8.18    .348 1967.0921_17:00 207.14 n/a   .000
00184>           SUM=       5.0 01:BCD-PH3       34.15   1.519 1967.0921_17:00 214.58 n/a   .000
00185> R0067:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00186>   ADD HYD           5.0 02:W1-LID-Out       7.05    .416 1967.0921_17:00 224.61 n/a   .000
00187>           +           5.0 02:W2-LID-Out       8.63    .493 1967.0921_17:00 222.14 n/a   .000
00188>           +           5.0 02:W3-LID-Out       5.18    .248 1967.0921_17:00 197.15 n/a   .000
00189>           +           5.0 02:W4-LID-Out       6.71    .343 1967.0921_17:00 207.14 n/a   .000
00190>           SUM=       5.0 01:BCD-PH3-LI     27.58   1.500 1967.0921_17:00 214.43 n/a   .000
00191> #*****
00192> #           Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
00193> #*****
00194> #           Set infiltration to 0 (CN = 99.99) for water balance analysis
00195> #*****
00196> R0067:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00197>   CONTINUOUS STANDHYD 5.0 01:INF-W1           8.92    .564 1967.0921_17:00 271.41 .702   .000
00198>   [XIMP=.66:TIMP=.71]
00199>   [LOSS= 2 :CN=100.0]
00200>   [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00201>   [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
00202>   [IaRECImp= 1.50: IaRECper= 6.00]
00203>   [SMIN= 1.39: SMAX= 9.24: SK= .030]
00204> R0067:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00205>   CONTINUOUS STANDHYD 5.0 01:INF-W2          10.75    .676 1967.0921_17:00 270.26 .699   .000
00206>   [XIMP=.65:TIMP=.70]
00207>   [LOSS= 2 :CN=100.0]
00208>   [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00209>   [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
00210>   [IaRECImp= 1.50: IaRECper= 6.00]
00211>   [SMIN= 1.39: SMAX= 9.24: SK= .030]
00212> R0067:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00213>   CONTINUOUS STANDHYD 5.0 01:INF-W3           6.30    .394 1967.0921_17:00 262.85 .679   .000
00214>   [XIMP=.53:TIMP=.63]
00215>   [LOSS= 2 :CN=100.0]
00216>   [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00217>   [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
00218>   [IaRECImp= 1.50: IaRECper= 6.00]
00219>   [SMIN= 1.39: SMAX= 9.24: SK= .030]
00220> R0067:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00221>   CONTINUOUS STANDHYD 5.0 01:INF-W4           8.18    .515 1967.0921_17:00 267.51 .691   .000
00222>   [XIMP=.57:TIMP=.67]
00223>   [LOSS= 2 :CN=100.0]
00224>   [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00225>   [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
00226>   [IaRECImp= 1.50: IaRECper= 6.00]
00227>   [SMIN= 1.39: SMAX= 9.24: SK= .030]
00228> R0067:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00229>   ADD HYD           5.0 02:INF-W1           8.92    .564 1967.0921_17:00 271.41 n/a   .000
00230>           +           5.0 02:INF-W2          10.75    .676 1967.0921_17:00 270.26 n/a   .000
00231>           +           5.0 02:INF-W3           6.30    .394 1967.0921_17:00 262.85 n/a   .000
00232>           +           5.0 02:INF-W4           8.18    .515 1967.0921_17:00 267.51 n/a   .000
00233>           SUM=       5.0 01:INF-BCD-PH     34.15   2.149 1967.0921_17:00 268.53 n/a   .000
00234> #####
00235> # CONTINUOUS RAINFALL DATA
00236> #####
00237> ** END OF RUN : 67
00238>
00239> *****
00240>
00241>
00242>
00243>
00244>
00245> RUN#:COMMAND#
00246> R0068:C00001-----
00247>   START
00248>   [TZERO = .00 hrs on 19680101]
00249>   [METOUT= 2 (1=imperial, 2=metric output)]
00250>   [NSTORM= 0 ]
00251>   [NRUN = 0068 ]
00252> #*****
00253> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00254> #*****
00255> # Project Name: Barrhaven Conservancy Development
00256> # Project Number: 1474
00257> # Date : 2021/Oct/18
00258> # Modeller : J.Burnett, P.Eng.
00259> # Updated : 2022/Dec/13 [LP]
00260> # Company : J.F. Sabourin and Associates
00261> # License # : 2582634
00262> #*****
00263> # Ottawa International Airport (1967 - 2003)
00264> R0068:C00002-----
00265> * READ AES DATA
00266> [Filename = YOW_1967_2007.123 ]
00267> [Start_date= 1968.0101: End_date= 1968.1230]

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00268> {DT= 60.min: Length= 8760.hrs: WetHrs= 413: DryHrs= 8347: PTOT= 592.80}
00269> Maximum average rainfall intensities over
00270> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00271> 33.30 17.05 11.37 6.23 3.74 1.87 1.26 .95 .70 mm/hr
00272> 33.30 34.10 34.10 37.40 44.90 44.90 45.40 45.40 50.20 mm
00273> 19680817 19680817 19680817 19680817 19680817 19680817 19680817 19680817 19680820 date
00274> Number of rainfall events per following interevent time
00275> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00276> 137 105 93 84 72 63 48 43 36
00277> Number of events with at least the following durations
00278> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00279> 136 76 49 18 5 0 0 0 0
00280> R0068:C00003-----
00281> COMPUTE API
00282> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
00283> [APImax= 67.52: APIavg= 16.74: APImin= .27]
00284> #*****
00285> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
00286> #*****
00287> R0068:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00288> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .612 1968.0817_ 5:00 321.18 .542 .000
00289> [XIMP=.66:TIMP=.71]
00290> [LOSS= 2 :CN= 71.0]
00291> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00292> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
00293> [IaRECimp= 1.50: IaRECper= 6.00]
00294> [SMIN= 41.38: SMAX=275.84: SK= .030]
00295> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
00296> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
00297> # Total Volume provided by LID - 179 m³
00298> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00299> R0068:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00300> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .612 1968.0817_ 5:00 321.18 n/a .000
00301> out <= 5.0 01:W1-LID 2.47 .001 1968.0130_ 4:25 321.19 n/a .000
00302> overflow <= 5.0 03:W1-LID-Out 6.45 .600 1968.0817_ 5:00 321.18 n/a .000
00303> {MxStoUsed=.1790E-01 m3, TotOvfVol=.2073E+01 m3, N-Ovf= 108, TotDurOvf= 164.hrs}
00304> R0068:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00305> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .728 1968.0817_ 5:00 317.28 .535 .000
00306> [XIMP=.65:TIMP=.70]
00307> [LOSS= 2 :CN= 71.0]
00308> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00309> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
00310> [IaRECimp= 1.50: IaRECper= 6.00]
00311> [SMIN= 41.38: SMAX=275.84: SK= .030]
00312> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
00313> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
00314> # Total Volume provided by LID - 200 m³
00315> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00316> R0068:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00317> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .728 1968.0817_ 5:00 317.28 n/a .000
00318> out <= 5.0 01:W2-LID 2.80 .001 1968.0130_ 3:55 317.27 n/a .000
00319> overflow <= 5.0 03:W2-LID-Out 7.95 .713 1968.0817_ 5:00 317.28 n/a .000
00320> {MxStoUsed=.2000E-01 m3, TotOvfVol=.2521E+01 m3, N-Ovf= 119, TotDurOvf= 170.hrs}
00321> R0068:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00322> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .382 1968.0817_ 5:00 275.30 .464 .000
00323> [XIMP=.53:TIMP=.63]
00324> [LOSS= 2 :CN= 71.0]
00325> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00326> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
00327> [IaRECimp= 1.50: IaRECper= 6.00]
00328> [SMIN= 41.38: SMAX=275.84: SK= .030]
00329> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
00330> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
00331> # Total Volume provided by LID - 96 m³
00332> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00333> R0068:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00334> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .382 1968.0817_ 5:00 275.30 n/a .000
00335> out <= 5.0 01:W3-LID 1.52 .001 1968.0130_ 3:55 275.31 n/a .000
00336> overflow <= 5.0 03:W3-LID-Out 4.78 .370 1968.0817_ 5:00 275.30 n/a .000
00337> {MxStoUsed=.9600E-02 m3, TotOvfVol=.1316E+01 m3, N-Ovf= 107, TotDurOvf= 173.hrs}
00338> R0068:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00339> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .520 1968.0817_ 5:00 291.04 .491 .000
00340> [XIMP=.57:TIMP=.67]
00341> [LOSS= 2 :CN= 71.0]
00342> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00343> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
00344> [IaRECimp= 1.50: IaRECper= 6.00]
00345> [SMIN= 41.38: SMAX=275.84: SK= .030]
00346> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
00347> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
00348> # Total Volume provided by LID - 131 m³
00349> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00350> R0068:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00351> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .520 1968.0817_ 5:00 291.04 n/a .000
00352> out <= 5.0 01:W4-LID 1.99 .001 1968.0130_ 3:50 291.04 n/a .000
00353> overflow <= 5.0 03:W4-LID-Out 6.19 .505 1968.0817_ 5:00 291.04 n/a .000
00354> {MxStoUsed=.1310E-01 m3, TotOvfVol=.1803E+01 m3, N-Ovf= 115, TotDurOvf= 174.hrs}
00355> R0068:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00356> ADD HYD 5.0 02:W1 8.92 .612 1968.0817_ 5:00 321.18 n/a .000

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00357>      +      5.0 02:W2      10.75      .728 1968.0817_ 5:00 317.28 n/a .000
00358>      +      5.0 02:W3      6.30      .382 1968.0817_ 5:00 275.30 n/a .000
00359>      +      5.0 02:W4      8.18      .520 1968.0817_ 5:00 291.04 n/a .000
00360>      SUM=      5.0 01:BCD-PH3      34.15      2.241 1968.0817_ 5:00 304.27 n/a .000
00361> R0068:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00362>      ADD HYD      5.0 02:W1-LID-Out      6.45      .600 1968.0817_ 5:00 321.18 n/a .000
00363>      +      5.0 02:W2-LID-Out      7.95      .713 1968.0817_ 5:00 317.28 n/a .000
00364>      +      5.0 02:W3-LID-Out      4.78      .370 1968.0817_ 5:00 275.30 n/a .000
00365>      +      5.0 02:W4-LID-Out      6.19      .505 1968.0817_ 5:00 291.04 n/a .000
00366>      SUM=      5.0 01:BCD-PH3-LI      25.37      2.188 1968.0817_ 5:00 303.96 n/a .000
00367> #*****
00368> #      Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
00369> #*****
00370> #      Set infiltration to 0 (CN = 99.99) for water balance analysis
00371> #*****
00372> R0068:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00373>      CONTINUOUS STANDHYD      5.0 01:INF-W1      8.92      .790 1968.0817_ 5:00 392.41 .662 .000
00374>      [XIMP=.66:TIMP=.71]
00375>      [LOSS= 2 :CN=100.0]
00376>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00377>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
00378>      [IaRECimp= 1.50: IaRECper= 6.00]
00379>      [SMIN= 1.39: SMAX= 9.24: SK= .030]
00380> R0068:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00381>      CONTINUOUS STANDHYD      5.0 01:INF-W2      10.75      .948 1968.0817_ 5:00 390.46 .659 .000
00382>      [XIMP=.65:TIMP=.70]
00383>      [LOSS= 2 :CN=100.0]
00384>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00385>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
00386>      [IaRECimp= 1.50: IaRECper= 6.00]
00387>      [SMIN= 1.39: SMAX= 9.24: SK= .030]
00388> R0068:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00389>      CONTINUOUS STANDHYD      5.0 01:INF-W3      6.30      .564 1968.0817_ 5:00 376.68 .635 .000
00390>      [XIMP=.53:TIMP=.63]
00391>      [LOSS= 2 :CN=100.0]
00392>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00393>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
00394>      [IaRECimp= 1.50: IaRECper= 6.00]
00395>      [SMIN= 1.39: SMAX= 9.24: SK= .030]
00396> R0068:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00397>      CONTINUOUS STANDHYD      5.0 01:INF-W4      8.18      .722 1968.0817_ 5:00 384.61 .649 .000
00398>      [XIMP=.57:TIMP=.67]
00399>      [LOSS= 2 :CN=100.0]
00400>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00401>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
00402>      [IaRECimp= 1.50: IaRECper= 6.00]
00403>      [SMIN= 1.39: SMAX= 9.24: SK= .030]
00404> R0068:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00405>      ADD HYD      5.0 02:INF-W1      8.92      .790 1968.0817_ 5:00 392.41 n/a .000
00406>      +      5.0 02:INF-W2      10.75      .948 1968.0817_ 5:00 390.46 n/a .000
00407>      +      5.0 02:INF-W3      6.30      .564 1968.0817_ 5:00 376.68 n/a .000
00408>      +      5.0 02:INF-W4      8.18      .722 1968.0817_ 5:00 384.61 n/a .000
00409>      SUM=      5.0 01:INF-BCD-PH      34.15      3.023 1968.0817_ 5:00 387.03 n/a .000
00410> #####
00411> # CONTINUOUS RAINFALL DATA
00412> #####
00413> ** END OF RUN : 68
00414>
00415> *****
00416>
00417>
00418>
00419>
00420>
00421> RUN#:COMMAND#
00422> R0069:C00001-----
00423>      START
00424>      [TZERO = .00 hrs on 19690101]
00425>      [METOUT= 2 (1=imperial, 2=metric output)]
00426>      [NSTORM= 0 ]
00427>      [NRUN = 0069 ]
00428> #*****
00429> #      SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00430> #*****
00431> #      Project Name: Barrhaven Conservancy Development
00432> #      Project Number: 1474
00433> #      Date : 2021/Oct/18
00434> #      Modeller : J.Burnett, P.Eng.
00435> #      Updated : 2022/Dec/13 [LP]
00436> #      Company : J.F. Sabourin and Associates
00437> #      License # : 2582634
00438> #*****
00439> #      Ottawa International Airport (1967 - 2003)
00440> R0069:C00002-----
00441> *      READ AES DATA
00442>      [Filename = YOW_1967_2007.123 ]
00443>      [Start_date= 1969.0101: End_date= 1969.1231]
00444>      {DT= 60.min: Length= 8760.hrs: DryHrs= 470: DryHrs= 8290: PTOT= 570.30}
00445>      Maximum average rainfall intensities over

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00446>      1 hr   2 hrs   3 hrs   6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00447>      21.10  16.25  10.83   7.78   3.93   2.10   1.40   1.09   .75   mm/hr
00448>      21.10  32.50  32.50  46.70  47.20  50.30  50.30  52.10  54.00   mm
00449>      19690818 19690818 19690818 19690819 19690819 19690819 19690819 19690819 19690819   date
00450>      Number of rainfall events per following interevent time
00451>      1 hr   2 hrs   3 hrs   6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00452>      157    119    107    92     72    58     49    43     32
00453>      Number of events with at least the following durations
00454>      1 hr   2 hrs   3 hrs   6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00455>      156    84     58    21     5     0     0     0     0
00456> R0069:C00003-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00457>      COMPUTE API
00458>      [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
00459>      [APImax= 56.77: APIavg= 16.06: APImin= .06]
00460> #*****
00461> #      Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
00462> #*****
00463> R0069:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00464>      CONTINUOUS STANDHYD 5.0 01:W1      8.92   .384 1969.0818_22:00 294.38 .516   .000
00465>      [XIMP=.66:TIMP=.71]
00466>      [LOSS= 2 :CN= 71.0]
00467>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00468>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
00469>      [IaRECimp= 1.50: IaRECper= 6.00]
00470>      [SMIN= 41.38: SMAX=275.84: SK= .030]
00471> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
00472> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
00473> # Total Volume provided by LID - 179 m³
00474> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00475> R0069:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00476>      ROUTE RESERVOIR -> 5.0 02:W1      8.92   .384 1969.0818_22:00 294.38 n/a   .000
00477>      out <= 5.0 01:W1-LID      2.45   .001 1969.0124_11:10 294.39 n/a   .000
00478>      overflow <= 5.0 03:W1-LID-Out 6.47   .379 1969.0818_22:00 294.38 n/a   .000
00479>      {MxStoUsed=.1790E-01 m3, TotOvfVol=.1904E+01 m3, N-Ovf= 90, TotDurOvf= 174.hrs}
00480> R0069:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00481>      CONTINUOUS STANDHYD 5.0 01:W2      10.75  .457 1969.0818_22:00 290.70 .510   .000
00482>      [XIMP=.65:TIMP=.70]
00483>      [LOSS= 2 :CN= 71.0]
00484>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00485>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
00486>      [IaRECimp= 1.50: IaRECper= 6.00]
00487>      [SMIN= 41.38: SMAX=275.84: SK= .030]
00488> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
00489> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
00490> # Total Volume provided by LID - 200 m³
00491> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00492> R0069:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00493>      ROUTE RESERVOIR -> 5.0 02:W2      10.75  .457 1969.0818_22:00 290.70 n/a   .000
00494>      out <= 5.0 01:W2-LID      2.81   .001 1969.0124_11:05 290.70 n/a   .000
00495>      overflow <= 5.0 03:W2-LID-Out 7.94   .450 1969.0818_22:00 290.70 n/a   .000
00496>      {MxStoUsed=.1999E-01 m3, TotOvfVol=.2308E+01 m3, N-Ovf= 96, TotDurOvf= 180.hrs}
00497> R0069:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00498>      CONTINUOUS STANDHYD 5.0 01:W3      6.30   .238 1969.0818_22:00 251.22 .441   .000
00499>      [XIMP=.53:TIMP=.63]
00500>      [LOSS= 2 :CN= 71.0]
00501>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00502>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
00503>      [IaRECimp= 1.50: IaRECper= 6.00]
00504>      [SMIN= 41.38: SMAX=275.84: SK= .030]
00505> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
00506> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
00507> # Total Volume provided by LID - 96 m³
00508> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00509> R0069:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00510>      ROUTE RESERVOIR -> 5.0 02:W3      6.30   .238 1969.0818_22:00 251.22 n/a   .000
00511>      out <= 5.0 01:W3-LID      1.54   .001 1969.0124_11:05 251.23 n/a   .000
00512>      overflow <= 5.0 03:W3-LID-Out 4.76   .233 1969.0818_22:00 251.22 n/a   .000
00513>      {MxStoUsed=.9599E-02 m3, TotOvfVol=.1197E+01 m3, N-Ovf= 94, TotDurOvf= 183.hrs}
00514> R0069:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00515>      CONTINUOUS STANDHYD 5.0 01:W4      8.18   .325 1969.0818_22:00 266.02 .466   .000
00516>      [XIMP=.57:TIMP=.67]
00517>      [LOSS= 2 :CN= 71.0]
00518>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00519>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
00520>      [IaRECimp= 1.50: IaRECper= 6.00]
00521>      [SMIN= 41.38: SMAX=275.84: SK= .030]
00522> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
00523> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
00524> # Total Volume provided by LID - 131 m³
00525> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00526> R0069:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00527>      ROUTE RESERVOIR -> 5.0 02:W4      8.18   .325 1969.0818_22:00 266.02 n/a   .000
00528>      out <= 5.0 01:W4-LID      2.01   .001 1969.0124_11:00 266.02 n/a   .000
00529>      overflow <= 5.0 03:W4-LID-Out 6.17   .318 1969.0818_22:00 266.02 n/a   .000
00530>      {MxStoUsed=.1309E-01 m3, TotOvfVol=.1642E+01 m3, N-Ovf= 90, TotDurOvf= 184.hrs}
00531> R0069:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00532>      ADD HYD      5.0 02:W1      8.92   .384 1969.0818_22:00 294.38 n/a   .000
00533>      +      5.0 02:W2      10.75  .457 1969.0818_22:00 290.70 n/a   .000
00534>      +      5.0 02:W3      6.30   .238 1969.0818_22:00 251.22 n/a   .000

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00535>          +      5.0 02:W4          8.18      .325 1969.0818_22:00 266.02 n/a      .000
00536>          SUM=    5.0 01:BCD-PH3      34.15      1.404 1969.0818_22:00 278.47 n/a      .000
00537> R0069:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00538>      ADD HYD          5.0 02:W1-LID-Out 6.47      .379 1969.0818_22:00 294.38 n/a      .000
00539>          +      5.0 02:W2-LID-Out 7.94      .450 1969.0818_22:00 290.70 n/a      .000
00540>          +      5.0 02:W3-LID-Out 4.76      .233 1969.0818_22:00 251.22 n/a      .000
00541>          +      5.0 02:W4-LID-Out 6.17      .318 1969.0818_22:00 266.02 n/a      .000
00542>          SUM=    5.0 01:BCD-PH3-LI 25.34      1.381 1969.0818_22:00 278.21 n/a      .000
00543> #*****
00544> #      Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
00545> #*****
00546> #      Set infiltration to 0 (CN = 99.99) for water balance analysis
00547> #*****
00548> R0069:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00549>      CONTINUOUS STANDHYD 5.0 01:INF-W1      8.92      .509 1969.0818_22:00 361.76 .634      .000
00550>      [XIMP=.66:TIMP=.71]
00551>      [LOSS= 2 :CN=100.0]
00552>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00553>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
00554>      [IaRECimp= 1.50: IaRECper= 6.00]
00555>      [SMIN= 1.39: SMAX= 9.24: SK= .030]
00556> R0069:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00557>      CONTINUOUS STANDHYD 5.0 01:INF-W2      10.75     .612 1969.0818_22:00 359.93 .631      .000
00558>      [XIMP=.65:TIMP=.70]
00559>      [LOSS= 2 :CN=100.0]
00560>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00561>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
00562>      [IaRECimp= 1.50: IaRECper= 6.00]
00563>      [SMIN= 1.39: SMAX= 9.24: SK= .030]
00564> R0069:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00565>      CONTINUOUS STANDHYD 5.0 01:INF-W3      6.30      .359 1969.0818_22:00 347.21 .609      .000
00566>      [XIMP=.53:TIMP=.63]
00567>      [LOSS= 2 :CN=100.0]
00568>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00569>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
00570>      [IaRECimp= 1.50: IaRECper= 6.00]
00571>      [SMIN= 1.39: SMAX= 9.24: SK= .030]
00572> R0069:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00573>      CONTINUOUS STANDHYD 5.0 01:INF-W4      8.18      .467 1969.0818_22:00 354.61 .622      .000
00574>      [XIMP=.57:TIMP=.67]
00575>      [LOSS= 2 :CN=100.0]
00576>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00577>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
00578>      [IaRECimp= 1.50: IaRECper= 6.00]
00579>      [SMIN= 1.39: SMAX= 9.24: SK= .030]
00580> R0069:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00581>      ADD HYD          5.0 02:INF-W1      8.92      .509 1969.0818_22:00 361.76 n/a      .000
00582>          +      5.0 02:INF-W2      10.75     .612 1969.0818_22:00 359.93 n/a      .000
00583>          +      5.0 02:INF-W3      6.30      .359 1969.0818_22:00 347.21 n/a      .000
00584>          +      5.0 02:INF-W4      8.18      .467 1969.0818_22:00 354.61 n/a      .000
00585>          SUM=    5.0 01:INF-BCD-PH 34.15      1.948 1969.0818_22:00 356.79 n/a      .000
00586> #####
00587> # CONTINUOUS RAINFALL DATA
00588> #####
00589> ** END OF RUN : 69
00590>
00591> *****
00592>
00593>
00594>
00595>
00596>
00597>      RUN#:COMMAND#
00598> R0070:C00001-----
00599>      START
00600>      [TZERO = .00 hrs on 19700101]
00601>      [METOUT= 2 (1=imperial, 2=metric output)]
00602>      [NSTORM= 0 ]
00603>      [NRUN = 0070 ]
00604> #*****
00605> #      SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00606> #*****
00607> #      Project Name: Barrhaven Conservancy Development
00608> #      Project Number: 1474
00609> #      Date : 2021/Oct/18
00610> #      Modeller : J.Burnett, P.Eng.
00611> #      Updated : 2022/Dec/13 [LP]
00612> #      Company : J.F. Sabourin and Associates
00613> #      License # : 2582634
00614> #*****
00615> #      Ottawa International Airport (1967 - 2003)
00616> R0070:C00002-----
00617> *      READ AES DATA
00618>      [Filename = YOW_1967_2007.123 ]
00619>      [Start_date= 1970.0101: End_date= 1970.1231]
00620>      {DT= 60.min: Length= 8760.hrs: WetHrs= 373: DryHrs= 8387: PTOT= 558.90}
00621>      Maximum average rainfall intensities over
00622>      1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00623>      35.30 18.30 12.20 6.10 3.63 1.81 1.21 1.46 .99 mm/hr

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00624>      35.30  36.60  36.60  36.60  43.50  43.50  43.50  69.90  71.20  mm
00625>      19700926 19700926 19700926 19700927 19700817 19700817 19700818 19700926 19700927  date
00626>      Number of rainfall events per following interevent time
00627>      1 hr   2 hrs   3 hrs   6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00628>      148   127   109    84    72    60    54    41    30
00629>      Number of events with at least the following durations
00630>      1 hr   2 hrs   3 hrs   6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00631>      147    79    40    15    3    0    0    0    0
00632> R0070:C00003-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00633>      COMPUTE API
00634>      [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
00635>      {APIimax= 76.00: APIavg= 15.84: APIimin= .07}
00636> #*****
00637> #      Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
00638> #*****
00639> R0070:C00004-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00640>      CONTINUOUS STANDHYD  5.0 01:W1      8.92      .665 1970.0926_21:00 288.79 .517 .000
00641>      [XIMP=.66:TIMP=.71]
00642>      [LOSS= 2 :CN= 71.0]
00643>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00644>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
00645>      [IaRECImp= 1.50: IaRECper= 6.00]
00646>      [SMIN= 41.38: SMAX=275.84: SK= .030]
00647> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
00648> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
00649> # Total Volume provided by LID - 179 m³
00650> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00651> R0070:C00005-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00652>      ROUTE RESERVOIR ->  5.0 02:W1      8.92      .665 1970.0926_21:00 288.79 n/a .000
00653>      out <= 5.0 01:W1-LID      2.45      .001 1970.0202_11:50 288.79 n/a .000
00654>      overflow <= 5.0 03:W1-LID-Out  6.47      .651 1970.0926_21:00 288.79 n/a .000
00655>      {MxStoUsed=.1789E-01 m3, TotOvfVol=.1870E+01 m3, N-Ovf= 84, TotDurOvf= 133.hrs}
00656> R0070:C00006-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00657>      CONTINUOUS STANDHYD  5.0 01:W2     10.75     .792 1970.0926_21:00 285.15 .510 .000
00658>      [XIMP=.65:TIMP=.70]
00659>      [LOSS= 2 :CN= 71.0]
00660>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00661>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
00662>      [IaRECImp= 1.50: IaRECper= 6.00]
00663>      [SMIN= 41.38: SMAX=275.84: SK= .030]
00664> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
00665> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
00666> # Total Volume provided by LID - 200 m³
00667> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00668> R0070:C00007-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00669>      ROUTE RESERVOIR ->  5.0 02:W2     10.75     .792 1970.0926_21:00 285.15 n/a .000
00670>      out <= 5.0 01:W2-LID      2.79      .001 1970.0202_11:45 285.14 n/a .000
00671>      overflow <= 5.0 03:W2-LID-Out  7.96      .775 1970.0926_21:00 285.15 n/a .000
00672>      {MxStoUsed=.1998E-01 m3, TotOvfVol=.2270E+01 m3, N-Ovf= 102, TotDurOvf= 138.hrs}
00673> R0070:C00008-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00674>      CONTINUOUS STANDHYD  5.0 01:W3      6.30      .423 1970.0926_21:00 245.92 .440 .000
00675>      [XIMP=.53:TIMP=.63]
00676>      [LOSS= 2 :CN= 71.0]
00677>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00678>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
00679>      [IaRECImp= 1.50: IaRECper= 6.00]
00680>      [SMIN= 41.38: SMAX=275.84: SK= .030]
00681> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
00682> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
00683> # Total Volume provided by LID - 96 m³
00684> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00685> R0070:C00009-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00686>      ROUTE RESERVOIR ->  5.0 02:W3      6.30      .423 1970.0926_21:00 245.92 n/a .000
00687>      out <= 5.0 01:W3-LID      1.52      .001 1970.0202_11:40 245.93 n/a .000
00688>      overflow <= 5.0 03:W3-LID-Out  4.78      .409 1970.0926_21:00 245.92 n/a .000
00689>      {MxStoUsed=.9597E-02 m3, TotOvfVol=.1175E+01 m3, N-Ovf= 91, TotDurOvf= 141.hrs}
00690> R0070:C00010-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00691>      CONTINUOUS STANDHYD  5.0 01:W4      8.18      .572 1970.0926_21:00 260.57 .466 .000
00692>      [XIMP=.57:TIMP=.67]
00693>      [LOSS= 2 :CN= 71.0]
00694>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00695>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
00696>      [IaRECImp= 1.50: IaRECper= 6.00]
00697>      [SMIN= 41.38: SMAX=275.84: SK= .030]
00698> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
00699> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
00700> # Total Volume provided by LID - 131 m³
00701> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00702> R0070:C00011-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00703>      ROUTE RESERVOIR ->  5.0 02:W4      8.18      .572 1970.0926_21:00 260.57 n/a .000
00704>      out <= 5.0 01:W4-LID      1.99      .001 1970.0202_11:45 260.57 n/a .000
00705>      overflow <= 5.0 03:W4-LID-Out  6.19      .555 1970.0926_21:00 260.57 n/a .000
00706>      {MxStoUsed=.1310E-01 m3, TotOvfVol=.1614E+01 m3, N-Ovf= 93, TotDurOvf= 141.hrs}
00707> R0070:C00012-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00708>      ADD HYD
00709>      + 5.0 02:W1      8.92      .665 1970.0926_21:00 288.79 n/a .000
00710>      + 5.0 02:W2     10.75     .792 1970.0926_21:00 285.15 n/a .000
00711>      + 5.0 02:W3      6.30      .423 1970.0926_21:00 245.92 n/a .000
00712>      + 5.0 02:W4      8.18      .572 1970.0926_21:00 260.57 n/a .000
00712>      SUM= 5.0 01:BCD-PH3  34.15     2.451 1970.0926_21:00 272.98 n/a .000

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00713> R0070:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00714>   ADD HYD                5.0 02:W1-LID-Out      6.47      .651 1970.0926_21:00 288.79  n/a   .000
00715>   +                5.0 02:W2-LID-Out      7.96      .775 1970.0926_21:00 285.15  n/a   .000
00716>   +                5.0 02:W3-LID-Out      4.78      .409 1970.0926_21:00 245.92  n/a   .000
00717>   +                5.0 02:W4-LID-Out      6.19      .555 1970.0926_21:00 260.57  n/a   .000
00718>   SUM=                5.0 01:BCD-PH3-LI    25.41     2.391 1970.0926_21:00 272.71  n/a   .000
00719> #*****
00720> #           Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
00721> #*****
00722> #           Set infiltration to 0 (CN = 99.99) for water balance analysis
00723> #*****
00724> R0070:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00725>   CONTINUOUS STANDHYD  5.0 01:INF-W1      8.92      .840 1970.0926_21:00 353.78  .633   .000
00726>   [XIMP=.66:TIMP=.71]
00727>   [LOSS= 2 :CN=100.0]
00728>   [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00729>   [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
00730>   [IaRECimp= 1.50: IaRECper= 6.00]
00731>   [SMIN= 1.39: SMAX= 9.24: SK= .030]
00732> R0070:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00733>   CONTINUOUS STANDHYD  5.0 01:INF-W2     10.75     1.008 1970.0926_21:00 351.90  .630   .000
00734>   [XIMP=.65:TIMP=.70]
00735>   [LOSS= 2 :CN=100.0]
00736>   [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00737>   [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
00738>   [IaRECimp= 1.50: IaRECper= 6.00]
00739>   [SMIN= 1.39: SMAX= 9.24: SK= .030]
00740> R0070:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00741>   CONTINUOUS STANDHYD  5.0 01:INF-W3      6.30      .598 1970.0926_21:00 339.10  .607   .000
00742>   [XIMP=.53:TIMP=.63]
00743>   [LOSS= 2 :CN=100.0]
00744>   [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00745>   [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
00746>   [IaRECimp= 1.50: IaRECper= 6.00]
00747>   [SMIN= 1.39: SMAX= 9.24: SK= .030]
00748> R0070:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00749>   CONTINUOUS STANDHYD  5.0 01:INF-W4      8.18      .777 1970.0926_21:00 346.75  .620   .000
00750>   [XIMP=.57:TIMP=.67]
00751>   [LOSS= 2 :CN=100.0]
00752>   [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00753>   [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
00754>   [IaRECimp= 1.50: IaRECper= 6.00]
00755>   [SMIN= 1.39: SMAX= 9.24: SK= .030]
00756> R0070:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00757>   ADD HYD                5.0 02:INF-W1      8.92      .840 1970.0926_21:00 353.78  n/a   .000
00758>   +                5.0 02:INF-W2     10.75     1.008 1970.0926_21:00 351.90  n/a   .000
00759>   +                5.0 02:INF-W3      6.30      .598 1970.0926_21:00 339.10  n/a   .000
00760>   +                5.0 02:INF-W4      8.18      .777 1970.0926_21:00 346.75  n/a   .000
00761>   SUM=                5.0 01:INF-BCD-PH    34.15     3.224 1970.0926_21:00 348.80  n/a   .000
00762> #####
00763> # CONTINUOUS RAINFALL DATA
00764> #####
00765> ** END OF RUN : 70
00766>
00767> *****
00768>
00769>
00770>
00771>
00772>
00773> RUN#:COMMAND#
00774> R0071:C00001-----
00775>   START
00776>   [TZERO = .00 hrs on 19710101]
00777>   [METOUT= 2 (1=imperial, 2=metric output)]
00778>   [NSTORM= 0 ]
00779>   [NRUN = 0071 ]
00780> #*****
00781> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00782> #*****
00783> # Project Name: Barrhaven Conservancy Development
00784> # Project Number: 1474
00785> # Date : 2021/Oct/18
00786> # Modeller : J.Burnett, P.Eng.
00787> # Updated : 2022/Dec/13 [LP]
00788> # Company : J.F. Sabourin and Associates
00789> # License # : 2582634
00790> #*****
00791> # Ottawa International Airport (1967 - 2003)
00792> R0071:C00002-----
00793> * READ AES DATA
00794> [Filename = YOW_1967_2007.123 ]
00795> [Start_date= 1971.0101: End_date= 1971.1231]
00796> {DT= 60.min: Length= 8760.hrs: WetHrs= 412: DryHrs= 8348: PTOT= 522.10}
00797> Maximum average rainfall intensities over
00798> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00799> 24.60 16.60 11.67 6.13 3.09 1.56 1.06 .79 .54 mm/hr
00800> 24.60 33.20 35.00 36.80 37.10 37.40 38.00 38.00 38.90 mm
00801> 19710810 19710810 19710810 19710810 19710810 19710810 19710811 19710812 19710830 date

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00802>      Number of rainfall events per following interevent time
00803>      1 hr   2 hrs   3 hrs   6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00804>      156   123    113    93     72     61     52     42     33
00805>      Number of events with at least the following durations
00806>      1 hr   2 hrs   3 hrs   6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00807>      155   81     59     21     2       0       0       0       0
00808> R0071:C00003-----D-----
00809>      COMPUTE API
00810>      [APIni= 50.00: APIKdy= .9000: APIKdt= .9956]
00811>      {APImax= 62.22: APIavg= 14.84: APImin= .36}
00812> #*****
00813> #      Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
00814> #*****
00815> R0071:C00004-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00816>      CONTINUOUS STANDHYD 5.0 01:W1      8.92      .432 1971.0810_15:00 258.23 .495      .000
00817>      [XIMP=.66:TIMP=.71]
00818>      [LOSS= 2 :CN= 71.0]
00819>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00820>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
00821>      [IaRECimp= 1.50: IaRECper= 6.00]
00822>      [SMIN= 41.38: SMAX=275.84: SK= .030]
00823> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
00824> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
00825> # Total Volume provided by LID - 179 m³
00826> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00827> R0071:C00005-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00828>      ROUTE RESERVOIR -> 5.0 02:W1      8.92      .432 1971.0810_15:00 258.23 n/a      .000
00829>      out <= 5.0 01:W1-LID      2.81      .001 1971.0402_ 3:00 258.23 n/a      .000
00830>      overflow <= 5.0 03:W1-LID-Out 6.11      .426 1971.0810_15:00 258.23 n/a      .000
00831>      {MxStoUsed=.1789E-01 m3, TotOvfVol=.1577E+01 m3, N-Ovf= 97, TotDurOvf= 116.hrs}
00832> R0071:C00006-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00833>      CONTINUOUS STANDHYD 5.0 01:W2      10.75     .513 1971.0810_15:00 254.87 .488      .000
00834>      [XIMP=.65:TIMP=.70]
00835>      [LOSS= 2 :CN= 71.0]
00836>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00837>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
00838>      [IaRECimp= 1.50: IaRECper= 6.00]
00839>      [SMIN= 41.38: SMAX=275.84: SK= .030]
00840> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
00841> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
00842> # Total Volume provided by LID - 200 m³
00843> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00844> R0071:C00007-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00845>      ROUTE RESERVOIR -> 5.0 02:W2      10.75     .513 1971.0810_15:00 254.87 n/a      .000
00846>      out <= 5.0 01:W2-LID      3.21      .001 1971.0402_ 2:45 254.86 n/a      .000
00847>      overflow <= 5.0 03:W2-LID-Out 7.54      .506 1971.0810_15:00 254.87 n/a      .000
00848>      {MxStoUsed=.1999E-01 m3, TotOvfVol=.1922E+01 m3, N-Ovf= 94, TotDurOvf= 122.hrs}
00849> R0071:C00008-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00850>      CONTINUOUS STANDHYD 5.0 01:W3      6.30      .262 1971.0810_15:00 218.03 .418      .000
00851>      [XIMP=.53:TIMP=.63]
00852>      [LOSS= 2 :CN= 71.0]
00853>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00854>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
00855>      [IaRECimp= 1.50: IaRECper= 6.00]
00856>      [SMIN= 41.38: SMAX=275.84: SK= .030]
00857> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
00858> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
00859> # Total Volume provided by LID - 96 m³
00860> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00861> R0071:C00009-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00862>      ROUTE RESERVOIR -> 5.0 02:W3      6.30      .262 1971.0810_15:00 218.03 n/a      .000
00863>      out <= 5.0 01:W3-LID      1.77      .001 1971.0402_ 2:40 218.03 n/a      .000
00864>      overflow <= 5.0 03:W3-LID-Out 4.53      .257 1971.0810_15:00 218.03 n/a      .000
00865>      {MxStoUsed=.9597E-02 m3, TotOvfVol=.9883E+00 m3, N-Ovf= 100, TotDurOvf= 126.hrs}
00866> R0071:C00010-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00867>      CONTINUOUS STANDHYD 5.0 01:W4      8.18      .359 1971.0810_15:00 231.57 .444      .000
00868>      [XIMP=.57:TIMP=.67]
00869>      [LOSS= 2 :CN= 71.0]
00870>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00871>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
00872>      [IaRECimp= 1.50: IaRECper= 6.00]
00873>      [SMIN= 41.38: SMAX=275.84: SK= .030]
00874> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
00875> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
00876> # Total Volume provided by LID - 131 m³
00877> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00878> R0071:C00011-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00879>      ROUTE RESERVOIR -> 5.0 02:W4      8.18      .359 1971.0810_15:00 231.57 n/a      .000
00880>      out <= 5.0 01:W4-LID      2.30      .001 1971.0402_ 2:35 231.57 n/a      .000
00881>      overflow <= 5.0 03:W4-LID-Out 5.88      .353 1971.0810_15:00 231.57 n/a      .000
00882>      {MxStoUsed=.1309E-01 m3, TotOvfVol=.1362E+01 m3, N-Ovf= 97, TotDurOvf= 127.hrs}
00883> R0071:C00012-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00884>      ADD HYD      5.0 02:W1      8.92      .432 1971.0810_15:00 258.23 n/a      .000
00885>      +      5.0 02:W2      10.75     .513 1971.0810_15:00 254.87 n/a      .000
00886>      +      5.0 02:W3      6.30      .262 1971.0810_15:00 218.03 n/a      .000
00887>      +      5.0 02:W4      8.18      .359 1971.0810_15:00 231.57 n/a      .000
00888>      SUM=      5.0 01:BCD-PH3 34.15     1.566 1971.0810_15:00 243.37 n/a      .000
00889> R0071:C00013-----D-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00890>      ADD HYD      5.0 02:W1-LID-Out 6.11      .426 1971.0810_15:00 258.23 n/a      .000

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00891>          +      5.0 02:W2-LID-Out      7.54      .506 1971.0810_15:00 254.87 n/a      .000
00892>          +      5.0 02:W3-LID-Out      4.53      .257 1971.0810_15:00 218.03 n/a      .000
00893>          +      5.0 02:W4-LID-Out      5.88      .353 1971.0810_15:00 231.57 n/a      .000
00894>          SUM=      5.0 01:BCD-PH3-LI      24.06      1.542 1971.0810_15:00 243.09 n/a      .000
00895> #*****
00896> #          Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
00897> #*****
00898> #          Set infiltration to 0 (CN = 99.99) for water balance analysis
00899> #*****
00900> R0071:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00901> CONTINUOUS STANDHYD 5.0 01:INF-W1      8.92      .577 1971.0810_15:00 313.64 .601      .000
00902> [XIMP=.66:TIMP=.71]
00903> [LOSS= 2 :CN=100.0]
00904> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00905> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
00906> [IaREcimp= 1.50: IaRECper= 6.00]
00907> [SMIN= 1.39: SMAX= 9.24: SK= .030]
00908> R0071:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00909> CONTINUOUS STANDHYD 5.0 01:INF-W2      10.75     .692 1971.0810_15:00 311.74 .597      .000
00910> [XIMP=.65:TIMP=.70]
00911> [LOSS= 2 :CN=100.0]
00912> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00913> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
00914> [IaREcimp= 1.50: IaRECper= 6.00]
00915> [SMIN= 1.39: SMAX= 9.24: SK= .030]
00916> R0071:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00917> CONTINUOUS STANDHYD 5.0 01:INF-W3      6.30      .405 1971.0810_15:00 298.09 .571      .000
00918> [XIMP=.53:TIMP=.63]
00919> [LOSS= 2 :CN=100.0]
00920> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00921> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
00922> [IaREcimp= 1.50: IaRECper= 6.00]
00923> [SMIN= 1.39: SMAX= 9.24: SK= .030]
00924> R0071:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00925> CONTINUOUS STANDHYD 5.0 01:INF-W4      8.18      .527 1971.0810_15:00 305.79 .586      .000
00926> [XIMP=.57:TIMP=.67]
00927> [LOSS= 2 :CN=100.0]
00928> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00929> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
00930> [IaREcimp= 1.50: IaRECper= 6.00]
00931> [SMIN= 1.39: SMAX= 9.24: SK= .030]
00932> R0071:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00933> ADD HYD          5.0 02:INF-W1      8.92      .577 1971.0810_15:00 313.64 n/a      .000
00934> +          5.0 02:INF-W2      10.75     .692 1971.0810_15:00 311.74 n/a      .000
00935> +          5.0 02:INF-W3      6.30      .405 1971.0810_15:00 298.09 n/a      .000
00936> +          5.0 02:INF-W4      8.18      .527 1971.0810_15:00 305.79 n/a      .000
00937>          SUM=      5.0 01:INF-BCD-PH      34.15     2.201 1971.0810_15:00 308.29 n/a      .000
00938> #####
00939> # CONTINUOUS RAINFALL DATA
00940> #####
00941> ** END OF RUN : 71
00942>
00943> *****
00944>
00945>
00946>
00947>
00948>
00949> RUN#:COMMAND#
00950> R0072:C00001-----
00951> START
00952> [TZERO = .00 hrs on 19720101]
00953> [METOUT= 2 (1=imperial, 2=metric output)]
00954> [NSTORM= 0 ]
00955> [NRUN = 0072 ]
00956> #*****
00957> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00958> #*****
00959> # Project Name: Barrhaven Conservancy Development
00960> # Project Number: 1474
00961> # Date : 2021/Oct/18
00962> # Modeller : J.Burnett, P.Eng.
00963> # Updated : 2022/Dec/13 [LP]
00964> # Company : J.F. Sabourin and Associates
00965> # License # : 2582634
00966> #*****
00967> # Ottawa International Airport (1967 - 2003)
00968> R0072:C00002-----
00969> * READ AES DATA
00970> [Filename = YOW_1967_2007.123 ]
00971> [Start_date= 1972.0101: End_date= 1972.1230]
00972> [DT= 60.min: Length= 8760.hrs: WetHrs= 489: DryHrs= 8271: PTOT= 784.30]
00973> Maximum average rainfall intensities over
00974> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00975> 37.30 19.15 12.97 8.15 4.50 2.53 2.00 1.71 1.17 mm/hr
00976> 37.30 38.30 38.90 48.90 54.00 60.70 72.10 82.20 84.20 mm
00977> 19720712 19720713 19720807 19720808 19720808 19720808 19720713 19720714 19720715 date
00978> Number of rainfall events per following interevent time
00979> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs

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00980>      170      133      122      86      76      60      45      41      31
00981>      Number of events with at least the following durations
00982>      1 hr   2 hrs   3 hrs   6 hrs   12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
00983>      169     96     58     21     5     0     0     0     0
00984> R0072:C00003-----
00985>      COMPUTE API
00986>      [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
00987>      {APImax=108.88: APIavg= 21.70: APImin= .00}
00988> #*****Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION*****
00989> #
00990> #*****
00991> R0072:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
00992>      CONTINUOUS STANDHYD 5.0 01:W1 8.92 .698 1972.0712_ 4:00 447.90 .571 .000
00993>      [XIMP=.66:TIMP=.71]
00994>      [LOSS= 2 :CN= 71.0]
00995>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
00996>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
00997>      [IaRECimp= 1.50: IaRECper= 6.00]
00998>      [SMIN= 41.38: SMAX=275.84: SK= .030]
00999> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
01000> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01001> # Total Volume provided by LID - 179 m³
01002> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01003> R0072:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01004>      ROUTE RESERVOIR -> 5.0 02:W1 8.92 .698 1972.0712_ 4:00 447.90 n/a .000
01005>      out <= 5.0 01:W1-LID 1.94 .001 1972.0413_10:00 447.91 n/a .000
01006>      overflow <= 5.0 03:W1-LID-Out 6.98 .683 1972.0712_ 4:00 447.90 n/a .000
01007>      {MxStoUsed=.1789E-01 m3, TotOvfVol=.3126E+01 m3, N-Ovf= 138, TotDurOvf= 198.hrs}
01008> R0072:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01009>      CONTINUOUS STANDHYD 5.0 01:W2 10.75 .831 1972.0712_ 4:00 442.89 .565 .000
01010>      [XIMP=.65:TIMP=.70]
01011>      [LOSS= 2 :CN= 71.0]
01012>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01013>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
01014>      [IaRECimp= 1.50: IaRECper= 6.00]
01015>      [SMIN= 41.38: SMAX=275.84: SK= .030]
01016> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
01017> # Assumed 870 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01018> # Total Volume provided by LID - 200 m³
01019> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01020> R0072:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01021>      ROUTE RESERVOIR -> 5.0 02:W2 10.75 .831 1972.0712_ 4:00 442.89 n/a .000
01022>      out <= 5.0 01:W2-LID 2.20 .001 1972.0413_ 9:55 442.88 n/a .000
01023>      overflow <= 5.0 03:W2-LID-Out 8.55 .812 1972.0712_ 4:00 442.89 n/a .000
01024>      {MxStoUsed=.2000E-01 m3, TotOvfVol=.3786E+01 m3, N-Ovf= 143, TotDurOvf= 204.hrs}
01025> R0072:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01026>      CONTINUOUS STANDHYD 5.0 01:W3 6.30 .442 1972.0712_ 4:00 391.20 .499 .000
01027>      [XIMP=.53:TIMP=.63]
01028>      [LOSS= 2 :CN= 71.0]
01029>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01030>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
01031>      [IaRECimp= 1.50: IaRECper= 6.00]
01032>      [SMIN= 41.38: SMAX=275.84: SK= .030]
01033> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
01034> # Assumed 420 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01035> # Total Volume provided by LID - 96 m³
01036> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01037> R0072:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01038>      ROUTE RESERVOIR -> 5.0 02:W3 6.30 .442 1972.0712_ 4:00 391.20 n/a .000
01039>      out <= 5.0 01:W3-LID 1.17 .001 1972.0413_ 9:50 391.21 n/a .000
01040>      overflow <= 5.0 03:W3-LID-Out 5.13 .426 1972.0712_ 4:00 391.20 n/a .000
01041>      {MxStoUsed=.9599E-02 m3, TotOvfVol=.2008E+01 m3, N-Ovf= 141, TotDurOvf= 210.hrs}
01042> R0072:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01043>      CONTINUOUS STANDHYD 5.0 01:W4 8.18 .598 1972.0712_ 4:00 411.36 .525 .000
01044>      [XIMP=.57:TIMP=.67]
01045>      [LOSS= 2 :CN= 71.0]
01046>      [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01047>      [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
01048>      [IaRECimp= 1.50: IaRECper= 6.00]
01049>      [SMIN= 41.38: SMAX=275.84: SK= .030]
01050> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
01051> # Assumed 570 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01052> # Total Volume provided by LID - 131 m³
01053> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01054> R0072:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01055>      ROUTE RESERVOIR -> 5.0 02:W4 8.18 .598 1972.0712_ 4:00 411.36 n/a .000
01056>      out <= 5.0 01:W4-LID 1.54 .001 1972.0413_ 9:55 411.37 n/a .000
01057>      overflow <= 5.0 03:W4-LID-Out 6.64 .579 1972.0712_ 4:00 411.36 n/a .000
01058>      {MxStoUsed=.1310E-01 m3, TotOvfVol=.2733E+01 m3, N-Ovf= 151, TotDurOvf= 209.hrs}
01059> R0072:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01060>      ADD HYD 5.0 02:W1 8.92 .698 1972.0712_ 4:00 447.90 n/a .000
01061>      + 5.0 02:W2 10.75 .831 1972.0712_ 4:00 442.89 n/a .000
01062>      + 5.0 02:W3 6.30 .442 1972.0712_ 4:00 391.20 n/a .000
01063>      + 5.0 02:W4 8.18 .598 1972.0712_ 4:00 411.36 n/a .000
01064>      SUM= 5.0 01:BCD-PH3 34.15 2.569 1972.0712_ 4:00 427.11 n/a .000
01065> R0072:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01066>      ADD HYD 5.0 02:W1-LID-Out 6.98 .683 1972.0712_ 4:00 447.90 n/a .000
01067>      + 5.0 02:W2-LID-Out 8.55 .812 1972.0712_ 4:00 442.89 n/a .000
01068>      + 5.0 02:W3-LID-Out 5.13 .426 1972.0712_ 4:00 391.20 n/a .000

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01069>          +      5.0 02:W4-LID-Out      6.64      .579 1972.0712_ 4:00 411.36 n/a      .000
01070>          SUM=      5.0 01:BCD-PH3-LI      27.30      2.501 1972.0712_ 4:00 426.78 n/a      .000
01071> #*****
01072> #          Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
01073> #*****
01074> #          Set infiltration to 0 (CN = 99.99) for water balance analysis
01075> #*****
01076> R0072:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
01077> CONTINUOUS STANDHYD 5.0 01:INF-W1      8.92      .900 1972.0712_ 4:00 542.44 .692      .000
01078> [XIMP=.66:TIMP=.71]
01079> [LOSS= 2 :CN=100.0]
01080> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01081> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
01082> [IaRECimp= 1.50: IaRECper= 6.00]
01083> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01084> R0072:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
01085> CONTINUOUS STANDHYD 5.0 01:INF-W2      10.75      1.068 1972.0712_ 4:00 540.07 .689      .000
01086> [XIMP=.65:TIMP=.70]
01087> [LOSS= 2 :CN=100.0]
01088> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01089> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
01090> [IaRECimp= 1.50: IaRECper= 6.00]
01091> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01092> R0072:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
01093> CONTINUOUS STANDHYD 5.0 01:INF-W3      6.30      .635 1972.0712_ 4:00 524.93 .669      .000
01094> [XIMP=.53:TIMP=.63]
01095> [LOSS= 2 :CN=100.0]
01096> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01097> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
01098> [IaRECimp= 1.50: IaRECper= 6.00]
01099> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01100> R0072:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
01101> CONTINUOUS STANDHYD 5.0 01:INF-W4      8.18      .824 1972.0712_ 4:00 534.52 .682      .000
01102> [XIMP=.57:TIMP=.67]
01103> [LOSS= 2 :CN=100.0]
01104> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01105> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
01106> [IaRECimp= 1.50: IaRECper= 6.00]
01107> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01108> R0072:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
01109> ADD HYD          5.0 02:INF-W1      8.92      .900 1972.0712_ 4:00 542.44 n/a      .000
01110>          +      5.0 02:INF-W2      10.75      1.068 1972.0712_ 4:00 540.07 n/a      .000
01111>          +      5.0 02:INF-W3      6.30      .635 1972.0712_ 4:00 524.93 n/a      .000
01112>          +      5.0 02:INF-W4      8.18      .824 1972.0712_ 4:00 534.51 n/a      .000
01113>          SUM=      5.0 01:INF-BCD-PH      34.15      3.427 1972.0712_ 4:00 536.57 n/a      .000
01114> #####
01115> # CONTINUOUS RAINFALL DATA
01116> #####
01117> ** END OF RUN : 72
01118>
01119> *****
01120>
01121>
01122>
01123>
01124>
01125> RUN#:COMMAND#
01126> R0073:C00001-----
01127> START
01128> [TZERO = .00 hrs on 19730101]
01129> [METOUT= 2 (1=imperial, 2=metric output)]
01130> [NSTORM= 0 ]
01131> [NRUN = 0073 ]
01132> #*****
01133> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
01134> #*****
01135> # Project Name: Barrhaven Conservancy Development
01136> # Project Number: 1474
01137> # Date : 2021/Oct/18
01138> # Modeller : J.Burnett, P.Eng.
01139> # Updated : 2022/Dec/13 [LP]
01140> # Company : J.F. Sabourin and Associates
01141> # License # : 2582634
01142> #*****
01143> # Ottawa International Airport (1967 - 2003)
01144> R0073:C00002-----
01145> * READ AES DATA
01146> [Filename = YOW_1967_2007.123 ]
01147> [Start_date= 1973.0101: End_date= 1973.1231]
01148> [DT= 60.min: Length= 8760.hrs: WetHrs= 549: DryHrs= 8211: PTOT= 744.90]
01149> Maximum average rainfall intensities over
01150> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01151> 30.00 17.25 12.33 7.10 3.63 1.89 1.28 .96 .96 mm/hr
01152> 30.00 34.50 37.00 42.60 43.60 45.40 46.00 46.00 69.20 mm
01153> 19730611 19730808 19730808 19730808 19730808 19730616 19730616 19730616 19731005 date
01154> Number of rainfall events per following interevent time
01155> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01156> 200 164 143 108 79 61 54 43 37
01157> Number of events with at least the following durations

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01158>      1 hr   2 hrs   3 hrs   6 hrs  12 hrs  24 hrs  36 hrs  48 hrs  72 hrs
01159>      200    102     66     20     4      0      0      0      0
01160> R0073:C00003-----
01161>      COMPUTE API
01162>      [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
01163>      [APImax= 78.26: APIavg= 20.56: APImin= .06]
01164> #*****
01165> #      Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
01166> #*****
01167> R0073:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01168> CONTINUOUS STANDHYD 5.0 01:W1      8.92      .542 1973.0611_17:00 400.85 .538      .000
01169> [XIMP=.66:TIMP=.71]
01170> [LOSS= 2 :CN= 71.0]
01171> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01172> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
01173> [IaRECImp= 1.50: IaRECper= 6.00]
01174> [SMIN= 41.38: SMAX=275.84: SK= .030]
01175> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
01176> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01177> # Total Volume provided by LID - 179 m³
01178> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01179> R0073:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01180> ROUTE RESERVOIR -> 5.0 02:W1      8.92      .542 1973.0611_17:00 400.85 n/a      .000
01181> out <= 5.0 01:W1-LID      2.08      .001 1973.0317_ 7:55 400.86 n/a      .000
01182> overflow <= 5.0 03:W1-LID-Out      6.84      .532 1973.0611_17:00 400.85 n/a      .000
01183> {MxStoUsed=.1790E-01 m3, TotOvfVol=.2742E+01 m3, N-Ovf= 111, TotDurOvf= 188.hrs}
01184> R0073:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01185> CONTINUOUS STANDHYD 5.0 01:W2      10.75     .644 1973.0611_17:00 396.04 .532      .000
01186> [XIMP=.65:TIMP=.70]
01187> [LOSS= 2 :CN= 71.0]
01188> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01189> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
01190> [IaRECImp= 1.50: IaRECper= 6.00]
01191> [SMIN= 41.38: SMAX=275.84: SK= .030]
01192> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
01193> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01194> # Total Volume provided by LID - 200 m³
01195> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01196> R0073:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01197> ROUTE RESERVOIR -> 5.0 02:W2      10.75     .644 1973.0611_17:00 396.04 n/a      .000
01198> out <= 5.0 01:W2-LID      2.37      .001 1973.0317_ 7:50 396.03 n/a      .000
01199> overflow <= 5.0 03:W2-LID-Out      8.38      .632 1973.0611_17:00 396.04 n/a      .000
01200> {MxStoUsed=.1997E-01 m3, TotOvfVol=.3320E+01 m3, N-Ovf= 109, TotDurOvf= 194.hrs}
01201> R0073:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01202> CONTINUOUS STANDHYD 5.0 01:W3      6.30      .338 1973.0808_20:00 344.92 .463      .000
01203> [XIMP=.53:TIMP=.63]
01204> [LOSS= 2 :CN= 71.0]
01205> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01206> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
01207> [IaRECImp= 1.50: IaRECper= 6.00]
01208> [SMIN= 41.38: SMAX=275.84: SK= .030]
01209> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
01210> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01211> # Total Volume provided by LID - 96 m³
01212> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01213> R0073:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01214> ROUTE RESERVOIR -> 5.0 02:W3      6.30      .338 1973.0808_20:00 344.92 n/a      .000
01215> out <= 5.0 01:W3-LID      1.27      .001 1973.0317_ 7:50 344.93 n/a      .000
01216> overflow <= 5.0 03:W3-LID-Out      5.03      .327 1973.0808_20:00 344.92 n/a      .000
01217> {MxStoUsed=.9591E-02 m3, TotOvfVol=.1734E+01 m3, N-Ovf= 115, TotDurOvf= 196.hrs}
01218> R0073:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01219> CONTINUOUS STANDHYD 5.0 01:W4      8.18      .457 1973.0611_17:00 364.28 .489      .000
01220> [XIMP=.57:TIMP=.67]
01221> [LOSS= 2 :CN= 71.0]
01222> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01223> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
01224> [IaRECImp= 1.50: IaRECper= 6.00]
01225> [SMIN= 41.38: SMAX=275.84: SK= .030]
01226> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
01227> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01228> # Total Volume provided by LID - 131 m³
01229> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01230> R0073:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01231> ROUTE RESERVOIR -> 5.0 02:W4      8.18      .457 1973.0611_17:00 364.28 n/a      .000
01232> out <= 5.0 01:W4-LID      1.67      .001 1973.0317_ 7:50 364.28 n/a      .000
01233> overflow <= 5.0 03:W4-LID-Out      6.51      .445 1973.0611_17:00 364.28 n/a      .000
01234> {MxStoUsed=.1310E-01 m3, TotOvfVol=.2372E+01 m3, N-Ovf= 115, TotDurOvf= 197.hrs}
01235> R0073:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01236> ADD HYD      5.0 02:W1      8.92      .542 1973.0611_17:00 400.85 n/a      .000
01237> +      5.0 02:W2      10.75     .644 1973.0611_17:00 396.04 n/a      .000
01238> +      5.0 02:W3      6.30      .338 1973.0808_20:00 344.92 n/a      .000
01239> +      5.0 02:W4      8.18      .457 1973.0611_17:00 364.28 n/a      .000
01240> SUM=      5.0 01:BCD-PH3      34.15     1.977 1973.0611_17:00 380.26 n/a      .000
01241> R0073:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01242> ADD HYD      5.0 02:W1-LID-Out      6.84      .532 1973.0611_17:00 400.85 n/a      .000
01243> +      5.0 02:W2-LID-Out      8.38      .632 1973.0611_17:00 396.04 n/a      .000
01244> +      5.0 02:W3-LID-Out      5.03      .327 1973.0808_20:00 344.92 n/a      .000
01245> +      5.0 02:W4-LID-Out      6.51      .445 1973.0611_17:00 364.28 n/a      .000
01246> SUM=      5.0 01:BCD-PH3-LI      26.76     1.935 1973.0611_17:00 379.94 n/a      .000

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01247> #*****
01248> #           Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
01249> #*****
01250> #           Set infiltration to 0 (CN = 99.99) for water balance analysis
01251> #*****
01252> R0073:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01253> CONTINUOUS STANDHYD 5.0 01:INF-W1      8.92      .702 1973.0611_17:00 493.83 .663      .000
01254> [XIMP=.66:TIMP=.71]
01255> [LOSS= 2 :CN=100.0]
01256> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01257> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
01258> [IaREcimp= 1.50: IaREcper= 6.00]
01259> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01260> R0073:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01261> CONTINUOUS STANDHYD 5.0 01:INF-W2      10.75     .842 1973.0611_17:00 491.61 .660      .000
01262> [XIMP=.65:TIMP=.70]
01263> [LOSS= 2 :CN=100.0]
01264> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01265> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
01266> [IaREcimp= 1.50: IaREcper= 6.00]
01267> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01268> R0073:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01269> CONTINUOUS STANDHYD 5.0 01:INF-W3      6.30      .492 1973.0611_17:00 476.58 .640      .000
01270> [XIMP=.53:TIMP=.63]
01271> [LOSS= 2 :CN=100.0]
01272> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01273> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
01274> [IaREcimp= 1.50: IaREcper= 6.00]
01275> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01276> R0073:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01277> CONTINUOUS STANDHYD 5.0 01:INF-W4      8.18      .641 1973.0611_17:00 485.56 .652      .000
01278> [XIMP=.57:TIMP=.67]
01279> [LOSS= 2 :CN=100.0]
01280> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01281> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
01282> [IaREcimp= 1.50: IaREcper= 6.00]
01283> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01284> R0073:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01285> ADD HYD              5.0 02:INF-W1      8.92      .702 1973.0611_17:00 493.83 n/a      .000
01286> +                    5.0 02:INF-W2     10.75     .842 1973.0611_17:00 491.61 n/a      .000
01287> +                    5.0 02:INF-W3      6.30      .492 1973.0611_17:00 476.58 n/a      .000
01288> +                    5.0 02:INF-W4      8.18      .641 1973.0611_17:00 485.56 n/a      .000
01289> SUM=                 5.0 01:INF-BCD-PH 34.15    2.677 1973.0611_17:00 487.97 n/a      .000
01290> #####
01291> # CONTINUOUS RAINFALL DATA
01292> #####
01293> ** END OF RUN : 73
01294>
01295> *****
01296>
01297>
01298>
01299>
01300>
01301> RUN#:COMMAND#
01302> R0074:C00001-----
01303> START
01304> [TZERO = .00 hrs on 19740101]
01305> [METOUT= 2 (1=imperial, 2=metric output)]
01306> [NSTORM= 0 ]
01307> [NRUN = 0074 ]
01308> #*****
01309> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
01310> #*****
01311> # Project Name: Barrhaven Conservancy Development
01312> # Project Number: 1474
01313> # Date : 2021/Oct/18
01314> # Modeller : J.Burnett, P.Eng.
01315> # Updated : 2022/Dec/13 [LP]
01316> # Company : J.F. Sabourin and Associates
01317> # License # : 2582634
01318> #*****
01319> # Ottawa International Airport (1967 - 2003)
01320> R0074:C00002-----
01321> * READ AES DATA
01322> [Filename = YOW_1967_2007.123 ]
01323> [Start_date= 1974.0101: End_date= 1974.1231]
01324> [DT= 60.min: Length= 8760.hrs: WetHrs= 320: DryHrs= 8440: PTOT= 386.20]
01325> Maximum average rainfall intensities over
01326> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01327> 20.60 15.40 10.37 5.18 2.98 1.63 1.08 .81 .54 mm/hr
01328> 20.60 30.80 31.10 31.10 35.70 39.00 39.00 39.00 39.00 mm
01329> 19740718 19740719 19740719 19740719 19740305 19740305 19740306 19740306 19740307 date
01330> Number of rainfall events per following interevent time
01331> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01332> 129 105 93 77 63 50 38 33 23
01333> Number of events with at least the following durations
01334> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01335> 128 66 32 10 3 0 0 0 0

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01336> R0074:C00003-----
01337> COMPUTE API
01338> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
01339> [APImax= 52.93: APIavg= 11.36: APImin= .00]
01340> #*****
01341> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
01342> #*****
01343> R0074:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01344> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .343 1974.0719_ 0:00 183.65 .476 .000
01345> [XIMP=.66:TIMP=.71]
01346> [LOSS= 2 :CN= 71.0]
01347> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01348> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
01349> [IaRECimp= 1.50: IaRECper= 6.00]
01350> [SMIN= 41.38: SMAX=275.84: SK= .030]
01351> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
01352> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01353> # Total Volume provided by LID - 179 m³
01354> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01355> R0074:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01356> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .343 1974.0719_ 0:00 183.65 n/a .000
01357> out <= 5.0 01:W1-LID 3.10 .001 1974.0222_14:45 183.65 n/a .000
01358> overflow <= 5.0 03:W1-LID-Out 5.82 .340 1974.0719_ 0:00 183.65 n/a .000
01359> {MxStoUsed=.1789E-01 m3, TotOvfVol=.1069E+01 m3, N-Ovf= 77, TotDurOvf= 95.hrs}
01360> R0074:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01361> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .407 1974.0719_ 0:00 181.19 .469 .000
01362> [XIMP=.65:TIMP=.70]
01363> [LOSS= 2 :CN= 71.0]
01364> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01365> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
01366> [IaRECimp= 1.50: IaRECper= 6.00]
01367> [SMIN= 41.38: SMAX=275.84: SK= .030]
01368> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
01369> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01370> # Total Volume provided by LID - 200 m³
01371> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01372> R0074:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01373> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .407 1974.0719_ 0:00 181.19 n/a .000
01374> out <= 5.0 01:W2-LID 3.53 .001 1974.0222_14:30 181.19 n/a .000
01375> overflow <= 5.0 03:W2-LID-Out 7.22 .403 1974.0719_ 0:00 181.19 n/a .000
01376> {MxStoUsed=.2000E-01 m3, TotOvfVol=.1309E+01 m3, N-Ovf= 88, TotDurOvf= 101.hrs}
01377> R0074:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01378> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .201 1974.0719_ 0:00 153.93 .399 .000
01379> [XIMP=.53:TIMP=.63]
01380> [LOSS= 2 :CN= 71.0]
01381> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01382> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
01383> [IaRECimp= 1.50: IaRECper= 6.00]
01384> [SMIN= 41.38: SMAX=275.84: SK= .030]
01385> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
01386> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01387> # Total Volume provided by LID - 96 m³
01388> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01389> R0074:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01390> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .201 1974.0719_ 0:00 153.93 n/a .000
01391> out <= 5.0 01:W3-LID 1.95 .001 1974.0222_14:30 153.93 n/a .000
01392> overflow <= 5.0 03:W3-LID-Out 4.35 .199 1974.0719_ 0:00 153.93 n/a .000
01393> {MxStoUsed=.9595E-02 m3, TotOvfVol=.6700E+00 m3, N-Ovf= 85, TotDurOvf= 103.hrs}
01394> R0074:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01395> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .278 1974.0719_ 0:00 163.80 .424 .000
01396> [XIMP=.57:TIMP=.67]
01397> [LOSS= 2 :CN= 71.0]
01398> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01399> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
01400> [IaRECimp= 1.50: IaRECper= 6.00]
01401> [SMIN= 41.38: SMAX=275.84: SK= .030]
01402> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
01403> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01404> # Total Volume provided by LID - 131 m³
01405> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01406> R0074:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01407> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .278 1974.0719_ 0:00 163.80 n/a .000
01408> out <= 5.0 01:W4-LID 2.53 .001 1974.0222_14:25 163.80 n/a .000
01409> overflow <= 5.0 03:W4-LID-Out 5.65 .275 1974.0719_ 0:00 163.80 n/a .000
01410> {MxStoUsed=.1310E-01 m3, TotOvfVol=.9248E+00 m3, N-Ovf= 91, TotDurOvf= 103.hrs}
01411> R0074:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01412> ADD HYD 5.0 02:W1 8.92 .343 1974.0719_ 0:00 183.65 n/a .000
01413> + 5.0 02:W2 10.75 .407 1974.0719_ 0:00 181.19 n/a .000
01414> + 5.0 02:W3 6.30 .201 1974.0719_ 0:00 153.93 n/a .000
01415> + 5.0 02:W4 8.18 .278 1974.0719_ 0:00 163.80 n/a .000
01416> SUM= 5.0 01:BCD-PH3 34.15 1.229 1974.0719_ 0:00 172.64 n/a .000
01417> R0074:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01418> ADD HYD 5.0 02:W1-LID-Out 5.82 .340 1974.0719_ 0:00 183.65 n/a .000
01419> + 5.0 02:W2-LID-Out 7.22 .403 1974.0719_ 0:00 181.19 n/a .000
01420> + 5.0 02:W3-LID-Out 4.35 .199 1974.0719_ 0:00 153.93 n/a .000
01421> + 5.0 02:W4-LID-Out 5.65 .275 1974.0719_ 0:00 163.80 n/a .000
01422> SUM= 5.0 01:BCD-PH3-LI 23.05 1.217 1974.0719_ 0:00 172.40 n/a .000
01423> #*****
01424> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT

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01425> #*****
01426> #          Set infiltration to 0 (CN = 99.99) for water balance analysis
01427> #*****
01428> R0074:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
01429> CONTINUOUS STANDHYD 5.0 01:INF-W1          8.92      .453 1974.0719_ 0:00 221.72 .574      .000
01430> [XIMP=.66:TIMP=.71]
01431> [LOSS= 2 :CN=100.0]
01432> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01433> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
01434> [IaRECimp= 1.50: IaRECper= 6.00]
01435> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01436> R0074:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
01437> CONTINUOUS STANDHYD 5.0 01:INF-W2          10.75     .530 1974.0719_ 0:00 220.25 .570      .000
01438> [XIMP=.65:TIMP=.70]
01439> [LOSS= 2 :CN=100.0]
01440> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01441> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
01442> [IaRECimp= 1.50: IaRECper= 6.00]
01443> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01444> R0074:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
01445> CONTINUOUS STANDHYD 5.0 01:INF-W3          6.30      .312 1974.0719_ 0:00 209.53 .543      .000
01446> [XIMP=.53:TIMP=.63]
01447> [LOSS= 2 :CN=100.0]
01448> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01449> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
01450> [IaRECimp= 1.50: IaRECper= 6.00]
01451> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01452> R0074:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
01453> CONTINUOUS STANDHYD 5.0 01:INF-W4          8.18      .410 1974.0719_ 0:00 215.51 .558      .000
01454> [XIMP=.57:TIMP=.67]
01455> [LOSS= 2 :CN=100.0]
01456> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01457> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
01458> [IaRECimp= 1.50: IaRECper= 6.00]
01459> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01460> R0074:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
01461> ADD HYD          5.0 02:INF-W1          8.92      .453 1974.0719_ 0:00 221.72 n/a      .000
01462> +          5.0 02:INF-W2          10.75     .530 1974.0719_ 0:00 220.25 n/a      .000
01463> +          5.0 02:INF-W3          6.30      .312 1974.0719_ 0:00 209.53 n/a      .000
01464> +          5.0 02:INF-W4          8.18      .410 1974.0719_ 0:00 215.51 n/a      .000
01465> SUM=          5.0 01:INF-BCD-PH          34.15     1.705 1974.0719_ 0:00 217.52 n/a      .000
01466> #####
01467> # CONTINUOUS RAINFALL DATA
01468> #####
01469> ** END OF RUN : 74
01470>
01471> *****
01472>
01473>
01474>
01475>
01476>
01477> RUN#:COMMAND#
01478> R0075:C00001-----
01479> START
01480> [TZERO = .00 hrs on 19750101]
01481> [METOUT= 2 (1=imperial, 2=metric output)]
01482> [NSTORM= 0 ]
01483> [NRUN = 0075 ]
01484> #*****
01485> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
01486> #*****
01487> # Project Name: Barrhaven Conservancy Development
01488> # Project Number: 1474
01489> # Date : 2021/Oct/18
01490> # Modeller : J.Burnett, P.Eng.
01491> # Updated : 2022/Dec/13 [LP]
01492> # Company : J.F. Sabourin and Associates
01493> # License # : 2582634
01494> #*****
01495> # Ottawa International Airport (1967 - 2003)
01496> R0075:C00002-----
01497> * READ AES DATA
01498> [Filename = YOW_1967_2007.123 ]
01499> [Start_date= 1975.0101: End_date= 1975.1231]
01500> {DT= 60.min: Length= 8760.hrs: WetHrs= 344: DryHrs= 8416: PTOT= 535.50}
01501> Maximum average rainfall intensities over
01502> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01503> 34.80 18.40 12.53 6.32 3.33 1.73 1.15 .87 .62 mm/hr
01504> 34.80 36.80 37.60 37.90 40.00 41.50 41.50 41.80 44.40 mm
01505> 19750708 19750720 19750720 19750720 19750721 19750721 19750721 19750721 19750928 date
01506> Number of rainfall events per following interevent time
01507> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01508> 136 118 99 78 61 49 40 33 25
01509> Number of events with at least the following durations
01510> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01511> 135 70 40 17 1 0 0 0 0
01512> R0075:C00003-----
01513> COMPUTE API

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01514> [APIni= 50.00: APIkdy= .9000: APIkdt= .9956]
01515> {APImax= 73.23: APIavg= 15.16: APImin= .00}
01516> #*****
01517> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
01518> #*****
01519> R0075:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01520> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .621 1975.0708_17:00 284.52 .531 .000
01521> [XIMP=.66:TIMP=.71]
01522> [LOSS= 2 :CN= 71.0]
01523> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01524> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
01525> [IaREcimp= 1.50: IaRECper= 6.00]
01526> [SMIN= 41.38: SMAX=275.84: SK= .030]
01527> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
01528> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01529> # Total Volume provided by LID - 179 m³
01530> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01531> R0075:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01532> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .621 1975.0708_17:00 284.52 n/a .000
01533> out <= 5.0 01:W1-LID 2.36 .001 1975.0109_8:40 284.53 n/a .000
01534> overflow <= 5.0 03:W1-LID-Out 6.56 .609 1975.0708_17:00 284.52 n/a .000
01535> {MxStoUsed=.1789E-01 m3, TotOvfVol=.1866E+01 m3, N-Ovf= 92, TotDurOvf= 117.hrs}
01536> R0075:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01537> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .738 1975.0708_17:00 280.95 .525 .000
01538> [XIMP=.65:TIMP=.70]
01539> [LOSS= 2 :CN= 71.0]
01540> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01541> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
01542> [IaREcimp= 1.50: IaRECper= 6.00]
01543> [SMIN= 41.38: SMAX=275.84: SK= .030]
01544> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
01545> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01546> # Total Volume provided by LID - 200 m³
01547> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01548> R0075:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01549> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .738 1975.0708_17:00 280.95 n/a .000
01550> out <= 5.0 01:W2-LID 2.68 .001 1975.0109_8:35 280.95 n/a .000
01551> overflow <= 5.0 03:W2-LID-Out 8.07 .724 1975.0708_17:00 280.95 n/a .000
01552> {MxStoUsed=.1999E-01 m3, TotOvfVol=.2268E+01 m3, N-Ovf= 100, TotDurOvf= 122.hrs}
01553> R0075:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01554> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .380 1975.0708_17:00 242.53 .453 .000
01555> [XIMP=.53:TIMP=.63]
01556> [LOSS= 2 :CN= 71.0]
01557> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01558> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
01559> [IaREcimp= 1.50: IaRECper= 6.00]
01560> [SMIN= 41.38: SMAX=275.84: SK= .030]
01561> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
01562> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01563> # Total Volume provided by LID - 96 m³
01564> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01565> R0075:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01566> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .380 1975.0708_17:00 242.53 n/a .000
01567> out <= 5.0 01:W3-LID 1.45 .001 1975.0109_8:35 242.53 n/a .000
01568> overflow <= 5.0 03:W3-LID-Out 4.85 .369 1975.0708_17:00 242.53 n/a .000
01569> {MxStoUsed=.9598E-02 m3, TotOvfVol=.1177E+01 m3, N-Ovf= 101, TotDurOvf= 126.hrs}
01570> R0075:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01571> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .520 1975.0708_17:00 256.91 .480 .000
01572> [XIMP=.57:TIMP=.67]
01573> [LOSS= 2 :CN= 71.0]
01574> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01575> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
01576> [IaREcimp= 1.50: IaRECper= 6.00]
01577> [SMIN= 41.38: SMAX=275.84: SK= .030]
01578> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
01579> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01580> # Total Volume provided by LID - 131 m³
01581> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01582> R0075:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01583> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .520 1975.0708_17:00 256.91 n/a .000
01584> out <= 5.0 01:W4-LID 1.89 .001 1975.0109_8:35 256.91 n/a .000
01585> overflow <= 5.0 03:W4-LID-Out 6.29 .506 1975.0708_17:00 256.91 n/a .000
01586> {MxStoUsed=.1308E-01 m3, TotOvfVol=.1615E+01 m3, N-Ovf= 106, TotDurOvf= 126.hrs}
01587> R0075:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01588> ADD HYD 5.0 02:W1 8.92 .621 1975.0708_17:00 284.52 n/a .000
01589> + 5.0 02:W2 10.75 .738 1975.0708_17:00 280.95 n/a .000
01590> + 5.0 02:W3 6.30 .380 1975.0708_17:00 242.53 n/a .000
01591> + 5.0 02:W4 8.18 .520 1975.0708_17:00 256.91 n/a .000
01592> SUM= 5.0 01:BCD-PH3 34.15 2.258 1975.0708_17:00 269.04 n/a .000
01593> R0075:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01594> ADD HYD 5.0 02:W1-LID-Out 6.56 .609 1975.0708_17:00 284.52 n/a .000
01595> + 5.0 02:W2-LID-Out 8.07 .724 1975.0708_17:00 280.95 n/a .000
01596> + 5.0 02:W3-LID-Out 4.85 .369 1975.0708_17:00 242.53 n/a .000
01597> + 5.0 02:W4-LID-Out 6.29 .506 1975.0708_17:00 256.91 n/a .000
01598> SUM= 5.0 01:BCD-PH3-LI 25.77 2.208 1975.0708_17:00 268.76 n/a .000
01599> #*****
01600> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
01601> #*****
01602> # Set infiltration to 0 (CN = 99.99) for water balance analysis

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01603> #*****
01604> R0075:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01605> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .819 1975.0708_17:00 348.61 .651 .000
01606> [XIMP=.66:TIMP=.71]
01607> [LOSS= 2 :CN=100.0]
01608> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01609> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
01610> [IaREcimp= 1.50: IaRECper= 6.00]
01611> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01612> R0075:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01613> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .982 1975.0708_17:00 346.77 .648 .000
01614> [XIMP=.65:TIMP=.70]
01615> [LOSS= 2 :CN=100.0]
01616> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01617> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
01618> [IaREcimp= 1.50: IaRECper= 6.00]
01619> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01620> R0075:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01621> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .587 1975.0708_17:00 334.63 .625 .000
01622> [XIMP=.53:TIMP=.63]
01623> [LOSS= 2 :CN=100.0]
01624> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01625> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
01626> [IaREcimp= 1.50: IaRECper= 6.00]
01627> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01628> R0075:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01629> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .763 1975.0708_17:00 342.11 .639 .000
01630> [XIMP=.57:TIMP=.67]
01631> [LOSS= 2 :CN=100.0]
01632> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01633> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
01634> [IaREcimp= 1.50: IaRECper= 6.00]
01635> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01636> R0075:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01637> ADD HYD 5.0 02:INF-W1 8.92 .819 1975.0708_17:00 348.61 n/a .000
01638> + 5.0 02:INF-W2 10.75 .982 1975.0708_17:00 346.77 n/a .000
01639> + 5.0 02:INF-W3 6.30 .587 1975.0708_17:00 334.63 n/a .000
01640> + 5.0 02:INF-W4 8.18 .763 1975.0708_17:00 342.11 n/a .000
01641> SUM= 5.0 01:INF-BCD-PH 34.15 3.151 1975.0708_17:00 343.90 n/a .000
01642> #####
01643> # CONTINUOUS RAINFALL DATA
01644> #####
01645> ** END OF RUN : 75
01646>
01647> *****
01648>
01649>
01650>
01651>
01652>
01653> RUN#:COMMAND#
01654> R0076:C00001-----
01655> START
01656> [TZERO = .00 hrs on 19760101]
01657> [METOUT= 2 (1=imperial, 2=metric output)]
01658> [NSTORM= 0 ]
01659> [NRUN = 0076 ]
01660> #*****
01661> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
01662> #*****
01663> # Project Name: Barrhaven Conservancy Development
01664> # Project Number: 1474
01665> # Date : 2021/Oct/18
01666> # Modeller : J.Burnett, P.Eng.
01667> # Updated : 2022/Dec/13 [LP]
01668> # Company : J.F. Sabourin and Associates
01669> # License # : 2582634
01670> #*****
01671> # Ottawa International Airport (1967 - 2003)
01672> R0076:C00002-----
01673> * READ AES DATA
01674> [Filename = YOW_1967_2007.123 ]
01675> [Start_date= 1976.0101: End_date= 1976.1230]
01676> {DT= 60.min: Length= 8064.hrs: WetHrs= 390: DryHrs= 7674: PTOT= 493.20}
01677> Maximum average rainfall intensities over
01678> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01679> 14.00 8.90 6.43 4.65 2.35 1.39 .97 .99 .80 mm/hr
01680> 14.00 17.80 19.30 27.90 28.20 33.30 35.10 47.60 57.50 mm
01681> 19760828 19760828 19760828 19760828 19760828 19760920 19760520 19760520 19760921 date
01682> Number of rainfall events per following interevent time
01683> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01684> 164 133 117 89 72 62 46 40 28
01685> Number of events with at least the following durations
01686> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01687> 163 80 47 15 2 0 0 0 0
01688> R0076:C00003-----
01689> COMPUTE API
01690> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
01691> [APIimax= 59.66: APIavg= 15.35: APIimin= .02]

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01692> #*****
01693> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
01694> #*****
01695> R0076:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01696> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .228 1976.0828_19:00 239.90 .486 .000
01697> [XIMP=.66:TIMP=.71]
01698> [LOSS= 2 :CN= 71.0]
01699> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01700> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
01701> [IaRECImp= 1.50: IaRECper= 6.00]
01702> [SMIN= 41.38: SMAX=275.84: SK= .030]
01703> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
01704> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01705> # Total Volume provided by LID - 179 m3
01706> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01707> R0076:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01708> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .228 1976.0828_19:00 239.90 n/a .000
01709> out <= 5.0 01:W1-LID 2.77 .001 1976.0331_15:15 239.90 n/a .000
01710> overflow <= 5.0 03:W1-LID-Out 6.15 .226 1976.0828_19:00 239.90 n/a .000
01711> {MxStoUsed=.1790E+01 m3, TotOvfVol=.1476E+01 m3, N-Ovf= 119, TotDurOvf= 137.hrs}
01712> R0076:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01713> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .270 1976.0828_19:00 236.79 .480 .000
01714> [XIMP=.65:TIMP=.70]
01715> [LOSS= 2 :CN= 71.0]
01716> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01717> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
01718> [IaRECImp= 1.50: IaRECper= 6.00]
01719> [SMIN= 41.38: SMAX=275.84: SK= .030]
01720> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
01721> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01722> # Total Volume provided by LID - 200 m3
01723> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01724> R0076:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01725> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .270 1976.0828_19:00 236.79 n/a .000
01726> out <= 5.0 01:W2-LID 3.15 .001 1976.0331_15:10 236.79 n/a .000
01727> overflow <= 5.0 03:W2-LID-Out 7.60 .267 1976.0828_19:00 236.79 n/a .000
01728> {MxStoUsed=.2000E+01 m3, TotOvfVol=.1799E+01 m3, N-Ovf= 122, TotDurOvf= 144.hrs}
01729> R0076:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01730> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .132 1976.0828_19:00 202.95 .411 .000
01731> [XIMP=.53:TIMP=.63]
01732> [LOSS= 2 :CN= 71.0]
01733> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01734> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
01735> [IaRECImp= 1.50: IaRECper= 6.00]
01736> [SMIN= 41.38: SMAX=275.84: SK= .030]
01737> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
01738> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01739> # Total Volume provided by LID - 96 m3
01740> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01741> R0076:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01742> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .132 1976.0828_19:00 202.95 n/a .000
01743> out <= 5.0 01:W3-LID 1.73 .001 1976.0331_15:10 202.95 n/a .000
01744> overflow <= 5.0 03:W3-LID-Out 4.57 .130 1976.0828_19:00 202.95 n/a .000
01745> {MxStoUsed=.9600E+02 m3, TotOvfVol=.9275E+00 m3, N-Ovf= 117, TotDurOvf= 151.hrs}
01746> R0076:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01747> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .183 1976.0828_19:00 215.45 .437 .000
01748> [XIMP=.57:TIMP=.67]
01749> [LOSS= 2 :CN= 71.0]
01750> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01751> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
01752> [IaRECImp= 1.50: IaRECper= 6.00]
01753> [SMIN= 41.38: SMAX=275.84: SK= .030]
01754> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
01755> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01756> # Total Volume provided by LID - 131 m3
01757> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01758> R0076:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01759> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .183 1976.0828_19:00 215.45 n/a .000
01760> out <= 5.0 01:W4-LID 2.25 .001 1976.0331_15:10 215.45 n/a .000
01761> overflow <= 5.0 03:W4-LID-Out 5.93 .181 1976.0828_19:00 215.45 n/a .000
01762> {MxStoUsed=.1310E+01 m3, TotOvfVol=.1277E+01 m3, N-Ovf= 121, TotDurOvf= 150.hrs}
01763> R0076:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01764> ADD HYD 5.0 02:W1 8.92 .228 1976.0828_19:00 239.90 n/a .000
01765> + 5.0 02:W2 10.75 .270 1976.0828_19:00 236.79 n/a .000
01766> + 5.0 02:W3 6.30 .132 1976.0828_19:00 202.95 n/a .000
01767> + 5.0 02:W4 8.18 .183 1976.0828_19:00 215.45 n/a .000
01768> SUM= 5.0 01:BCD-PH3 34.15 .813 1976.0828_19:00 226.25 n/a .000
01769> R0076:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01770> ADD HYD 5.0 02:W1-LID-Out 6.15 .226 1976.0828_19:00 239.90 n/a .000
01771> + 5.0 02:W2-LID-Out 7.60 .267 1976.0828_19:00 236.79 n/a .000
01772> + 5.0 02:W3-LID-Out 4.57 .130 1976.0828_19:00 202.95 n/a .000
01773> + 5.0 02:W4-LID-Out 5.93 .181 1976.0828_19:00 215.45 n/a .000
01774> SUM= 5.0 01:BCD-PH3-LI 24.25 .805 1976.0828_19:00 225.99 n/a .000
01775> #*****
01776> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
01777> #*****
01778> # Set infiltration to 0 (CN = 99.99) for water balance analysis
01779> #*****
01780> R0076:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms

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01781> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .280 1976.0828_19:00 291.65 .591 .000
01782> [XIMP=.66:TIMP=.71]
01783> [LOSS= 2 :CN=100.0]
01784> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01785> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
01786> [IaRECimp= 1.50: IaRECper= 6.00]
01787> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01788> R0076:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01789> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .326 1976.0828_19:00 289.91 .588 .000
01790> [XIMP=.65:TIMP=.70]
01791> [LOSS= 2 :CN=100.0]
01792> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01793> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
01794> [IaRECimp= 1.50: IaRECper= 6.00]
01795> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01796> R0076:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01797> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .187 1976.0828_19:00 277.98 .564 .000
01798> [XIMP=.53:TIMP=.63]
01799> [LOSS= 2 :CN=100.0]
01800> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01801> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
01802> [IaRECimp= 1.50: IaRECper= 6.00]
01803> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01804> R0076:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01805> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .249 1976.0828_19:00 285.07 .578 .000
01806> [XIMP=.57:TIMP=.67]
01807> [LOSS= 2 :CN=100.0]
01808> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01809> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
01810> [IaRECimp= 1.50: IaRECper= 6.00]
01811> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01812> R0076:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01813> ADD HYD 5.0 02:INF-W1 8.92 .280 1976.0828_19:00 291.65 n/a .000
01814> + 5.0 02:INF-W2 10.75 .326 1976.0828_19:00 289.91 n/a .000
01815> + 5.0 02:INF-W3 6.30 .187 1976.0828_19:00 277.98 n/a .000
01816> + 5.0 02:INF-W4 8.18 .249 1976.0828_19:00 285.07 n/a .000
01817> SUM= 5.0 01:INF-BCD-PH 34.15 1.042 1976.0828_19:00 287.00 n/a .000
01818> #####
01819> # CONTINUOUS RAINFALL DATA
01820> #####
01821> ** END OF RUN : 76
01822>
01823> *****
01824>
01825>
01826>
01827>
01828>
01829> RUN#:COMMAND#
01830> R0077:C00001-----
01831> START
01832> [TZERO = .00 hrs on 19770101]
01833> [METOUT= 2 (1=imperial, 2=metric output)]
01834> [NSTORM= 0]
01835> [NRUN = 0077 ]
01836> #*****
01837> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
01838> #*****
01839> # Project Name: Barrhaven Conservancy Development
01840> # Project Number: 1474
01841> # Date : 2021/Oct/18
01842> # Modeller : J.Burnett, P.Eng.
01843> # Updated : 2022/Dec/13 [LP]
01844> # Company : J.F. Sabourin and Associates
01845> # License # : 2582634
01846> #*****
01847> # Ottawa International Airport (1967 - 2003)
01848> R0077:C00002-----
01849> * READ AES DATA
01850> [Filename = YOW_1967_2007.123 ]
01851> [Start_date= 1977.0101: End_date= 1977.1231]
01852> {DT= 60.min: Length= 8016.hrs: WetHrs= 512: DryHrs= 7504: PTOT= 677.80}
01853> Maximum average rainfall intensities over
01854> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01855> 21.30 15.20 10.40 6.53 3.30 1.66 1.40 1.06 .73 mm/hr
01856> 21.30 30.40 31.20 39.20 39.60 39.80 50.40 51.00 52.40 mm
01857> 19770717 19770717 19770717 19770901 19770902 19770314 19770314 19770314 19770718 date
01858> Number of rainfall events per following interevent time
01859> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01860> 172 142 126 99 78 63 53 42 30
01861> Number of events with at least the following durations
01862> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01863> 171 88 60 22 5 1 0 0 0
01864> R0077:C00003-----
01865> COMPUTE API
01866> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
01867> [APImax= 74.80: APIavg= 20.62: APImin= 1.63]
01868> #*****
01869> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION

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01870> #*****
01871> R0077:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01872> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .368 1977.0717_16:00 365.11 .539 .000
01873> [XIMP=.66:TIMP=.71]
01874> [LOSS= 2 :CN= 71.0]
01875> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01876> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
01877> [IaRECimp= 1.50: IaRECper= 6.00]
01878> [SMIN= 41.38: SMAX=275.84: SK= .030]
01879> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
01880> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01881> # Total Volume provided by LID - 179 m³
01882> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01883> R0077:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01884> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .368 1977.0717_16:00 365.11 n/a .000
01885> out <= 5.0 01:W1-LID 2.42 .001 1977.0304_20:50 365.12 n/a .000
01886> overflow <= 5.0 03:W1-LID-Out 6.50 .364 1977.0717_16:00 365.11 n/a .000
01887> {MxStoUsed=.1790E-01 m3, TotOvfVol=.2374E+01 m3, N-Ovf= 124, TotDurOvf= 211.hrs}
01888> R0077:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01889> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .437 1977.0717_16:00 360.57 .532 .000
01890> [XIMP=.65:TIMP=.70]
01891> [LOSS= 2 :CN= 71.0]
01892> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01893> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
01894> [IaRECimp= 1.50: IaRECper= 6.00]
01895> [SMIN= 41.38: SMAX=275.84: SK= .030]
01896> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
01897> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01898> # Total Volume provided by LID - 200 m³
01899> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01900> R0077:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01901> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .437 1977.0717_16:00 360.57 n/a .000
01902> out <= 5.0 01:W2-LID 2.74 .001 1977.0304_20:50 360.56 n/a .000
01903> overflow <= 5.0 03:W2-LID-Out 8.01 .432 1977.0717_16:00 360.57 n/a .000
01904> {MxStoUsed=.2000E-01 m3, TotOvfVol=.2888E+01 m3, N-Ovf= 130, TotDurOvf= 217.hrs}
01905> R0077:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01906> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .229 1977.0901_23:00 311.46 .460 .000
01907> [XIMP=.53:TIMP=.63]
01908> [LOSS= 2 :CN= 71.0]
01909> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01910> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
01911> [IaRECimp= 1.50: IaRECper= 6.00]
01912> [SMIN= 41.38: SMAX=275.84: SK= .030]
01913> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
01914> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01915> # Total Volume provided by LID - 96 m³
01916> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01917> R0077:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01918> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .229 1977.0901_23:00 311.46 n/a .000
01919> out <= 5.0 01:W3-LID 1.48 .001 1977.0304_20:45 311.47 n/a .000
01920> overflow <= 5.0 03:W3-LID-Out 4.82 .224 1977.0901_23:00 311.46 n/a .000
01921> {MxStoUsed=.9598E-02 m3, TotOvfVol=.1501E+01 m3, N-Ovf= 127, TotDurOvf= 222.hrs}
01922> R0077:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01923> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .309 1977.0901_23:00 329.71 .486 .000
01924> [XIMP=.57:TIMP=.67]
01925> [LOSS= 2 :CN= 71.0]
01926> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01927> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
01928> [IaRECimp= 1.50: IaRECper= 6.00]
01929> [SMIN= 41.38: SMAX=275.84: SK= .030]
01930> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
01931> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
01932> # Total Volume provided by LID - 131 m³
01933> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01934> R0077:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01935> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .309 1977.0901_23:00 329.71 n/a .000
01936> out <= 5.0 01:W4-LID 1.94 .001 1977.0304_20:45 329.72 n/a .000
01937> overflow <= 5.0 03:W4-LID-Out 6.24 .302 1977.0901_23:00 329.71 n/a .000
01938> {MxStoUsed=.1309E-01 m3, TotOvfVol=.2058E+01 m3, N-Ovf= 133, TotDurOvf= 222.hrs}
01939> R0077:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01940> ADD HYD 5.0 02:W1 8.92 .368 1977.0717_16:00 365.11 n/a .000
01941> + 5.0 02:W2 10.75 .437 1977.0717_16:00 360.57 n/a .000
01942> + 5.0 02:W3 6.30 .229 1977.0901_23:00 311.46 n/a .000
01943> + 5.0 02:W4 8.18 .309 1977.0901_23:00 329.71 n/a .000
01944> SUM= 5.0 01:BCD-PH3 34.15 1.330 1977.0717_16:00 345.30 n/a .000
01945> R0077:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01946> ADD HYD 5.0 02:W1-LID-Out 6.50 .364 1977.0717_16:00 365.11 n/a .000
01947> + 5.0 02:W2-LID-Out 8.01 .432 1977.0717_16:00 360.57 n/a .000
01948> + 5.0 02:W3-LID-Out 4.82 .224 1977.0901_23:00 311.46 n/a .000
01949> + 5.0 02:W4-LID-Out 6.24 .302 1977.0901_23:00 329.71 n/a .000
01950> SUM= 5.0 01:BCD-PH3-LI 25.57 1.312 1977.0717_16:00 344.94 n/a .000
01951> #*****
01952> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIR
01953> #*****
01954> # Set infiltration to 0 (CN = 99.99) for water balance analysis
01955> #*****
01956> R0077:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01957> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .484 1977.0717_16:00 446.64 .659 .000
01958> [XIMP=.66:TIMP=.71]

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01959> [LOSS= 2 :CN=100.0]
01960> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01961> [Impervious area: IAimp= 1.57:SLPI=.50:LGI= 244.:MNI=.013:SCI= .0]
01962> [IaRECImp= 1.50: IaRECper= 6.00]
01963> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01964> R0077:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01965> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .569 1977.0717_16:00 444.31 .656 .000
01966> [XIMP=.65:TIMP=.70]
01967> [LOSS= 2 :CN=100.0]
01968> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01969> [Impervious area: IAimp= 1.57:SLPI=.50:LGI= 268.:MNI=.013:SCI= .0]
01970> [IaRECImp= 1.50: IaRECper= 6.00]
01971> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01972> R0077:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01973> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .337 1977.0717_16:00 428.34 .632 .000
01974> [XIMP=.53:TIMP=.63]
01975> [LOSS= 2 :CN=100.0]
01976> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01977> [Impervious area: IAimp= 1.57:SLPI=.50:LGI= 205.:MNI=.013:SCI= .0]
01978> [IaRECImp= 1.50: IaRECper= 6.00]
01979> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01980> R0077:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01981> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .440 1977.0717_16:00 437.81 .646 .000
01982> [XIMP=.57:TIMP=.67]
01983> [LOSS= 2 :CN=100.0]
01984> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
01985> [Impervious area: IAimp= 1.57:SLPI=.50:LGI= 234.:MNI=.013:SCI= .0]
01986> [IaRECImp= 1.50: IaRECper= 6.00]
01987> [SMIN= 1.39: SMAX= 9.24: SK= .030]
01988> R0077:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
01989> ADD HYD 5.0 02:INF-W1 8.92 .484 1977.0717_16:00 446.64 n/a .000
01990> + 5.0 02:INF-W2 10.75 .569 1977.0717_16:00 444.31 n/a .000
01991> + 5.0 02:INF-W3 6.30 .337 1977.0717_16:00 428.34 n/a .000
01992> + 5.0 02:INF-W4 8.18 .440 1977.0717_16:00 437.81 n/a .000
01993> SUM= 5.0 01:INF-BCD-PH 34.15 1.830 1977.0717_16:00 440.41 n/a .000
01994> #####
01995> # CONTINUOUS RAINFALL DATA
01996> #####
01997> ** END OF RUN : 77
01998>
01999> *****
02000>
02001>
02002>
02003>
02004>
02005> RUN#:COMMAND#
02006> R0078:C00001-----
02007> START
02008> [TZERO = .00 hrs on 19780101]
02009> [METOUT= 2 (1=imperial, 2=metric output)]
02010> [NSTORM= 0 ]
02011> [NRUN = 0078 ]
02012> #*****
02013> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
02014> #*****
02015> # Project Name: Barrhaven Conservancy Development
02016> # Project Number: 1474
02017> # Date : 2021/Oct/18
02018> # Modeller : J.Burnett, P.Eng.
02019> # Updated : 2022/Dec/13 [LP]
02020> # Company : J.F. Sabourin and Associates
02021> # License # : 2582634
02022> #*****
02023> # Ottawa International Airport (1967 - 2003)
02024> R0078:C00002-----
02025> * READ AES DATA
02026> [Filename = YOW_1967_2007.123 ]
02027> [Start_date= 1978.0101: End_date= 1978.1231]
02028> {DT= 60.min: Length= 8040.hrs: WetHrs= 409: DryHrs= 7631: PTOT= 641.40}
02029> Maximum average rainfall intensities over
02030> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02031> 36.00 18.15 12.10 6.05 3.04 1.64 1.13 .87 .58 mm/hr
02032> 36.00 36.30 36.30 36.30 36.50 39.40 40.60 41.60 41.60 mm
02033> 19780618 19780618 19780618 19780618 19780619 19780411 19780412 19780620 19780621 date
02034> Number of rainfall events per following interevent time
02035> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02036> 154 128 118 97 71 58 51 46 33
02037> Number of events with at least the following durations
02038> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02039> 154 75 44 18 5 0 0 0 0
02040> R0078:C00003-----
02041> COMPUTE API
02042> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
02043> [APImax= 65.36: APIavg= 19.25: APImin= .25]
02044> #*****
02045> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
02046> #*****
02047> R0078:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms

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02048> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .670 1978.0618_17:00 347.07 .541 .000
02049> [XIMP=.66:TIMP=.71]
02050> [LOSS= 2 :CN= 71.0]
02051> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02052> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
02053> [IaRECImp= 1.50: IaRECper= 6.00]
02054> [SMIN= 41.38: SMAX=275.84: SK= .030]
02055> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
02056> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02057> # Total Volume provided by LID - 179 m³
02058> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02059> R0078:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02060> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .670 1978.0618_17:00 347.07 n/a .000
02061> out <= 5.0 01:W1-LID 2.39 .001 1978.0108_ 3:30 347.08 n/a .000
02062> overflow <= 5.0 03:W1-LID-Out 6.53 .656 1978.0618_17:00 347.07 n/a .000
02063> {MxStoUsed=.1790E-01 m3, TotOvfVol=.2267E+01 m3, N-Ovf= 106, TotDurOvf= 160.hrs}
02064> R0078:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02065> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .797 1978.0618_17:00 342.55 .534 .000
02066> [XIMP=.65:TIMP=.70]
02067> [LOSS= 2 :CN= 71.0]
02068> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02069> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
02070> [IaRECImp= 1.50: IaRECper= 6.00]
02071> [SMIN= 41.38: SMAX=275.84: SK= .030]
02072> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
02073> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02074> # Total Volume provided by LID - 200 m³
02075> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02076> R0078:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02077> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .797 1978.0618_17:00 342.55 n/a .000
02078> out <= 5.0 01:W2-LID 2.73 .001 1978.0108_ 3:25 342.54 n/a .000
02079> overflow <= 5.0 03:W2-LID-Out 8.02 .780 1978.0618_17:00 342.55 n/a .000
02080> {MxStoUsed=.2000E-01 m3, TotOvfVol=.2749E+01 m3, N-Ovf= 106, TotDurOvf= 164.hrs}
02081> R0078:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02082> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .423 1978.0618_17:00 292.83 .457 .000
02083> [XIMP=.53:TIMP=.63]
02084> [LOSS= 2 :CN= 71.0]
02085> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02086> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
02087> [IaRECImp= 1.50: IaRECper= 6.00]
02088> [SMIN= 41.38: SMAX=275.84: SK= .030]
02089> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
02090> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02091> # Total Volume provided by LID - 96 m³
02092> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02093> R0078:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02094> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .423 1978.0618_17:00 292.83 n/a .000
02095> out <= 5.0 01:W3-LID 1.51 .001 1978.0108_ 3:25 292.83 n/a .000
02096> overflow <= 5.0 03:W3-LID-Out 4.79 .408 1978.0618_17:00 292.83 n/a .000
02097> {MxStoUsed=.9597E-02 m3, TotOvfVol=.1404E+01 m3, N-Ovf= 113, TotDurOvf= 167.hrs}
02098> R0078:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02099> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .573 1978.0618_17:00 311.01 .485 .000
02100> [XIMP=.57:TIMP=.67]
02101> [LOSS= 2 :CN= 71.0]
02102> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02103> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
02104> [IaRECImp= 1.50: IaRECper= 6.00]
02105> [SMIN= 41.38: SMAX=275.84: SK= .030]
02106> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
02107> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02108> # Total Volume provided by LID - 131 m³
02109> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02110> R0078:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02111> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .573 1978.0618_17:00 311.01 n/a .000
02112> out <= 5.0 01:W4-LID 1.96 .001 1978.0108_ 3:25 311.01 n/a .000
02113> overflow <= 5.0 03:W4-LID-Out 6.22 .555 1978.0618_17:00 311.01 n/a .000
02114> {MxStoUsed=.1310E-01 m3, TotOvfVol=.1935E+01 m3, N-Ovf= 103, TotDurOvf= 167.hrs}
02115> R0078:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02116> ADD HYD 5.0 02:W1 8.92 .670 1978.0618_17:00 347.07 n/a .000
02117> + 5.0 02:W2 10.75 .797 1978.0618_17:00 342.55 n/a .000
02118> + 5.0 02:W3 6.30 .423 1978.0618_17:00 292.83 n/a .000
02119> + 5.0 02:W4 8.18 .573 1978.0618_17:00 311.01 n/a .000
02120> SUM= 5.0 01:BCD-PH3 34.15 2.462 1978.0618_17:00 327.00 n/a .000
02121> R0078:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02122> ADD HYD 5.0 02:W1-LID-Out 6.53 .656 1978.0618_17:00 347.07 n/a .000
02123> + 5.0 02:W2-LID-Out 8.02 .780 1978.0618_17:00 342.55 n/a .000
02124> + 5.0 02:W3-LID-Out 4.79 .408 1978.0618_17:00 292.83 n/a .000
02125> + 5.0 02:W4-LID-Out 6.22 .555 1978.0618_17:00 311.01 n/a .000
02126> SUM= 5.0 01:BCD-PH3-LI 25.57 2.400 1978.0618_17:00 326.71 n/a .000
02127> #*****
02128> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
02129> #*****
02130> # Set infiltration to 0 (CN = 99.99) for water balance analysis
02131> #*****
02132> R0078:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02133> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .856 1978.0618_17:00 429.43 .670 .000
02134> [XIMP=.66:TIMP=.71]
02135> [LOSS= 2 :CN=100.0]
02136> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]

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02137> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
02138> [IaRECimp= 1.50: IaRECper= 6.00]
02139> [SMIN= 1.39: SMAX= 9.24: SK= .030]
02140> R0078:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02141> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 1.028 1978.0618_17:00 427.15 .666 .000
02142> [XIMP=.65:TIMP=.70]
02143> [LOSS= 2 :CN=100.0]
02144> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02145> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
02146> [IaRECimp= 1.50: IaRECper= 6.00]
02147> [SMIN= 1.39: SMAX= 9.24: SK= .030]
02148> R0078:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02149> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .611 1978.0618_17:00 410.75 .640 .000
02150> [XIMP=.53:TIMP=.63]
02151> [LOSS= 2 :CN=100.0]
02152> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02153> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
02154> [IaRECimp= 1.50: IaRECper= 6.00]
02155> [SMIN= 1.39: SMAX= 9.24: SK= .030]
02156> R0078:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02157> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .794 1978.0618_17:00 420.01 .655 .000
02158> [XIMP=.57:TIMP=.67]
02159> [LOSS= 2 :CN=100.0]
02160> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02161> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
02162> [IaRECimp= 1.50: IaRECper= 6.00]
02163> [SMIN= 1.39: SMAX= 9.24: SK= .030]
02164> R0078:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02165> ADD HYD 5.0 02:INF-W1 8.92 .856 1978.0618_17:00 429.43 n/a .000
02166> + 5.0 02:INF-W2 10.75 1.028 1978.0618_17:00 427.15 n/a .000
02167> + 5.0 02:INF-W3 6.30 .611 1978.0618_17:00 410.75 n/a .000
02168> + 5.0 02:INF-W4 8.18 .794 1978.0618_17:00 420.01 n/a .000
02169> SUM= 5.0 01:INF-BCD-PH 34.15 3.289 1978.0618_17:00 423.01 n/a .000
02170> #####
02171> # CONTINUOUS RAINFALL DATA
02172> #####
02173> ** END OF RUN : 78
02174>
02175> *****
02176>
02177>
02178>
02179>
02180>
02181> RUN#:COMMAND#
02182> R0079:C00001-----
02183> START
02184> [TZERO = .00 hrs on 19790101]
02185> [METOUT= 2 (1=imperial, 2=metric output)]
02186> [NSTORM= 0 ]
02187> [NRUN = 0079 ]
02188> #*****
02189> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
02190> #*****
02191> # Project Name: Barrhaven Conservancy Development
02192> # Project Number: 1474
02193> # Date : 2021/Oct/18
02194> # Modeller : J.Burnett, P.Eng.
02195> # Updated : 2022/Dec/13 [LP]
02196> # Company : J.F. Sabourin and Associates
02197> # License # : 2582634
02198> #*****
02199> # Ottawa International Airport (1967 - 2003)
02200> R0079:C00002-----
02201> * READ AES DATA
02202> [Filename = YOW_1967_2007.123 ]
02203> [Start_date= 1979.0101: End_date= 1979.1231]
02204> {DT= 60.min: Length= 8760.hrs: WetHrs= 546: DryHrs= 8214: PTOT= 866.50}
02205> Maximum average rainfall intensities over
02206> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02207> 34.90 22.00 14.67 7.33 5.14 2.63 1.75 1.31 .88 mm/hr
02208> 34.90 44.00 44.00 44.00 61.70 63.00 63.00 63.00 63.00 mm
02209> 19790616 19790616 19790616 19790616 19790914 19790915 19790915 19790915 19790917 date
02210> Number of rainfall events per following interevent time
02211> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02212> 188 147 129 103 86 60 53 43 36
02213> Number of events with at least the following durations
02214> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02215> 187 97 65 25 6 1 0 0 0
02216> R0079:C00003-----
02217> COMPUTE API
02218> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
02219> [APImax= 78.42: APIavg= 23.13: APImin= .13]
02220> #*****
02221> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
02222> #*****
02223> R0079:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02224> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .682 1979.0616_14:00 506.86 .585 .000
02225> [XIMP=.66:TIMP=.71]

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02226> [LOSS= 2 :CN= 71.0]
02227> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02228> [Impervious area: IAimp= 1.57:SLPI=.50:LGI= 244.:MNI=.013:SCI= .0]
02229> [IaREcimp= 1.50: IaRCper= 6.00]
02230> [SMIN= 41.38: SMAX=275.84: SK= .030]
02231> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
02232> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02233> # Total Volume provided by LID - 179 m³
02234> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02235> R0079:C00005-----D Tmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02236> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .682 1979.0616_14:00 506.86 n/a .000
02237> out <= 5.0 01:W1-LID 1.79 .001 1979.0101_19:55 506.87 n/a .000
02238> overflow <= 5.0 03:W1-LID-Out 7.13 .665 1979.0616_14:00 506.86 n/a .000
02239> {MxStoUsed=.1790E-01 m3, TotOvfVol=.3613E+01 m3, N-Ovf= 122, TotDurOvf= 209.hrs}
02240> R0079:C00006-----D Tmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02241> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .813 1979.0616_14:00 501.22 .578 .000
02242> [XIMP=.65:TIMP=.70]
02243> [LOSS= 2 :CN= 71.0]
02244> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02245> [Impervious area: IAimp= 1.57:SLPI=.50:LGI= 268.:MNI=.013:SCI= .0]
02246> [IaREcimp= 1.50: IaRCper= 6.00]
02247> [SMIN= 41.38: SMAX=275.84: SK= .030]
02248> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
02249> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02250> # Total Volume provided by LID - 200 m³
02251> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02252> R0079:C00007-----D Tmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02253> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .813 1979.0616_14:00 501.22 n/a .000
02254> out <= 5.0 01:W2-LID 2.03 .001 1979.0101_19:40 501.21 n/a .000
02255> overflow <= 5.0 03:W2-LID-Out 8.72 .793 1979.0616_14:00 501.22 n/a .000
02256> {MxStoUsed=.2000E-01 m3, TotOvfVol=.4370E+01 m3, N-Ovf= 128, TotDurOvf= 213.hrs}
02257> R0079:C00008-----D Tmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02258> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .460 1979.0616_14:00 442.52 .511 .000
02259> [XIMP=.53:TIMP=.63]
02260> [LOSS= 2 :CN= 71.0]
02261> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02262> [Impervious area: IAimp= 1.57:SLPI=.50:LGI= 205.:MNI=.013:SCI= .0]
02263> [IaREcimp= 1.50: IaRCper= 6.00]
02264> [SMIN= 41.38: SMAX=275.84: SK= .030]
02265> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
02266> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02267> # Total Volume provided by LID - 96 m³
02268> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02269> R0079:C00009-----D Tmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02270> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .460 1979.0616_14:00 442.52 n/a .000
02271> out <= 5.0 01:W3-LID 1.08 .001 1979.0101_19:30 442.52 n/a .000
02272> overflow <= 5.0 03:W3-LID-Out 5.22 .438 1979.0616_14:00 442.52 n/a .000
02273> {MxStoUsed=.9598E-02 m3, TotOvfVol=.2310E+01 m3, N-Ovf= 126, TotDurOvf= 216.hrs}
02274> R0079:C00010-----D Tmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02275> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .594 1979.0616_14:00 465.26 .537 .000
02276> [XIMP=.57:TIMP=.67]
02277> [LOSS= 2 :CN= 71.0]
02278> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02279> [Impervious area: IAimp= 1.57:SLPI=.50:LGI= 234.:MNI=.013:SCI= .0]
02280> [IaREcimp= 1.50: IaRCper= 6.00]
02281> [SMIN= 41.38: SMAX=275.84: SK= .030]
02282> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
02283> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02284> # Total Volume provided by LID - 131 m³
02285> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02286> R0079:C00011-----D Tmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02287> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .594 1979.0616_14:00 465.26 n/a .000
02288> out <= 5.0 01:W4-LID 1.42 .001 1979.0101_19:35 465.27 n/a .000
02289> overflow <= 5.0 03:W4-LID-Out 6.76 .574 1979.0616_14:00 465.26 n/a .000
02290> {MxStoUsed=.1310E-01 m3, TotOvfVol=.3145E+01 m3, N-Ovf= 124, TotDurOvf= 218.hrs}
02291> R0079:C00012-----D Tmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02292> ADD HYD 5.0 02:W1 8.92 .682 1979.0616_14:00 506.86 n/a .000
02293> + 5.0 02:W2 10.75 .813 1979.0616_14:00 501.22 n/a .000
02294> + 5.0 02:W3 6.30 .460 1979.0616_14:00 442.52 n/a .000
02295> + 5.0 02:W4 8.18 .594 1979.0616_14:00 465.26 n/a .000
02296> SUM= 5.0 01:BCD-PH3 34.15 2.549 1979.0616_14:00 483.25 n/a .000
02297> R0079:C00013-----D Tmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02298> ADD HYD 5.0 02:W1-LID-Out 7.13 .665 1979.0616_14:00 506.86 n/a .000
02299> + 5.0 02:W2-LID-Out 8.72 .793 1979.0616_14:00 501.22 n/a .000
02300> + 5.0 02:W3-LID-Out 5.22 .438 1979.0616_14:00 442.52 n/a .000
02301> + 5.0 02:W4-LID-Out 6.76 .574 1979.0616_14:00 465.26 n/a .000
02302> SUM= 5.0 01:BCD-PH3-LI 27.83 2.470 1979.0616_14:00 482.92 n/a .000
02303> #*****
02304> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDI
02305> #*****
02306> # Set infiltration to 0 (CN = 99.99) for water balance analysis
02307> #*****
02308> R0079:C00014-----D Tmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02309> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .850 1979.0616_14:00 620.26 .716 .000
02310> [XIMP=.66:TIMP=.71]
02311> [LOSS= 2 :CN=100.0]
02312> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02313> [Impervious area: IAimp= 1.57:SLPI=.50:LGI= 244.:MNI=.013:SCI= .0]
02314> [IaREcimp= 1.50: IaRCper= 6.00]

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02315> [SMIN= 1.39: SMAX= 9.24: SK= .030]
02316> R0079:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02317> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 1.022 1979.0616_14:00 617.83 .713 .000
02318> [XIMP=.65:TIMP=.70]
02319> [LOSS= 2 :CN=100.0]
02320> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02321> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
02322> [IaRECimp= 1.50: IaRECper= 6.00]
02323> [SMIN= 1.39: SMAX= 9.24: SK= .030]
02324> R0079:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02325> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .607 1979.0616_14:00 601.90 .695 .000
02326> [XIMP=.53:TIMP=.63]
02327> [LOSS= 2 :CN=100.0]
02328> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02329> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
02330> [IaRECimp= 1.50: IaRECper= 6.00]
02331> [SMIN= 1.39: SMAX= 9.24: SK= .030]
02332> R0079:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02333> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .786 1979.0616_14:00 611.76 .706 .000
02334> [XIMP=.57:TIMP=.67]
02335> [LOSS= 2 :CN=100.0]
02336> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02337> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
02338> [IaRECimp= 1.50: IaRECper= 6.00]
02339> [SMIN= 1.39: SMAX= 9.24: SK= .030]
02340> R0079:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02341> ADD HYD 5.0 02:INF-W1 8.92 .850 1979.0616_14:00 620.26 n/a .000
02342> + 5.0 02:INF-W2 10.75 1.022 1979.0616_14:00 617.83 n/a .000
02343> + 5.0 02:INF-W3 6.30 .607 1979.0616_14:00 601.90 n/a .000
02344> + 5.0 02:INF-W4 8.18 .786 1979.0616_14:00 611.76 n/a .000
02345> SUM= 5.0 01:INF-BCD-PH 34.15 3.266 1979.0616_14:00 614.07 n/a .000
02346> #####
02347> # CONTINUOUS RAINFALL DATA
02348> #####
02349> ** END OF RUN : 79
02350>
02351> *****
02352>
02353>
02354>
02355>
02356>
02357> RUN#:COMMAND#
02358> R0080:C00001-----
02359> START
02360> [TZERO = .00 hrs on 19800101]
02361> [METOUT= 2 (1=imperial, 2=metric output)]
02362> [NSTORM= 0 ]
02363> [NRUN = 0080 ]
02364> #*****
02365> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
02366> #*****
02367> # Project Name: Barrhaven Conservancy Development
02368> # Project Number: 1474
02369> # Date : 2021/Oct/18
02370> # Modeller : J.Burnett, P.Eng.
02371> # Updated : 2022/Dec/13 [LP]
02372> # Company : J.F. Sabourin and Associates
02373> # License # : 2582634
02374> #*****
02375> # Ottawa International Airport (1967 - 2003)
02376> R0080:C00002-----
02377> * READ AES DATA
02378> [Filename = YOW_1967_2007.123 ]
02379> [Start_date= 1980.0101: End_date= 1980.1230]
02380> {DT= 60.min: Length= 8760.hrs: WetHrs= 427: DryHrs= 8333: PTOT= 622.00}
02381> Maximum average rainfall intensities over
02382> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02383> 15.00 9.20 6.50 4.72 3.57 1.97 1.35 1.01 .86 mm/hr
02384> 15.00 18.40 19.50 28.30 42.80 47.20 48.60 48.60 62.00 mm
02385> 19800830 19800830 19801025 19801025 19801026 19801026 19801026 19801027 19800902 date
02386> Number of rainfall events per following interevent time
02387> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02388> 151 125 112 93 79 62 49 44 28
02389> Number of events with at least the following durations
02390> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02391> 150 85 54 16 4 0 0 0 0
02392> R0080:C00003-----
02393> COMPUTE API
02394> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
02395> {APIimax= 68.72: APIavg= 17.50: APIimin= .06}
02396> #*****
02397> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
02398> #*****
02399> R0080:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02400> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .246 1980.0830_14:00 333.35 .536 .000
02401> [XIMP=.66:TIMP=.71]
02402> [LOSS= 2 :CN= 71.0]
02403> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]

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02404> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
02405> [IaREcimp= 1.50: IaREcper= 6.00]
02406> [SMIN= 41.38: SMAX=275.84: SK= .030]
02407> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
02408> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02409> # Total Volume provided by LID - 179 m³
02410> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02411> R0080:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02412> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .246 1980.0830_14:00 333.35 n/a .000
02413> out <= 5.0 01:W1-LID 2.37 .001 1980.0111_21:10 333.36 n/a .000
02414> overflow <= 5.0 03:W1-LID-Out 6.55 .244 1980.0830_14:00 333.35 n/a .000
02415> {MxStoUsed=.1789E-01 m3, TotOvfVol=.2183E+01 m3, N-Ovf= 117, TotDurOvf= 162.hrs}
02416> R0080:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02417> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .291 1980.0830_14:00 329.13 .529 .000
02418> [XIMP=.65:TIMP=.70]
02419> [LOSS= 2 :CN= 71.0]
02420> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02421> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
02422> [IaREcimp= 1.50: IaREcper= 6.00]
02423> [SMIN= 41.38: SMAX=275.84: SK= .030]
02424> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
02425> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02426> # Total Volume provided by LID - 200 m³
02427> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02428> R0080:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02429> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .291 1980.0830_14:00 329.13 n/a .000
02430> out <= 5.0 01:W2-LID 2.71 .001 1980.0111_21:05 329.12 n/a .000
02431> overflow <= 5.0 03:W2-LID-Out 8.04 .288 1980.0830_14:00 329.13 n/a .000
02432> {MxStoUsed=.2000E-01 m3, TotOvfVol=.2647E+01 m3, N-Ovf= 128, TotDurOvf= 168.hrs}
02433> R0080:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02434> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .143 1980.0830_14:00 283.32 .456 .000
02435> [XIMP=.53:TIMP=.63]
02436> [LOSS= 2 :CN= 71.0]
02437> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02438> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
02439> [IaREcimp= 1.50: IaREcper= 6.00]
02440> [SMIN= 41.38: SMAX=275.84: SK= .030]
02441> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
02442> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02443> # Total Volume provided by LID - 96 m³
02444> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02445> R0080:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02446> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .143 1980.0830_14:00 283.32 n/a .000
02447> out <= 5.0 01:W3-LID 1.48 .001 1980.0111_21:05 283.33 n/a .000
02448> overflow <= 5.0 03:W3-LID-Out 4.82 .142 1980.0830_14:00 283.32 n/a .000
02449> {MxStoUsed=.9601E-02 m3, TotOvfVol=.1366E+01 m3, N-Ovf= 128, TotDurOvf= 173.hrs}
02450> R0080:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02451> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .198 1980.0830_14:00 300.36 .483 .000
02452> [XIMP=.57:TIMP=.67]
02453> [LOSS= 2 :CN= 71.0]
02454> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02455> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
02456> [IaREcimp= 1.50: IaREcper= 6.00]
02457> [SMIN= 41.38: SMAX=275.84: SK= .030]
02458> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
02459> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02460> # Total Volume provided by LID - 131 m³
02461> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02462> R0080:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02463> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .198 1980.0830_14:00 300.36 n/a .000
02464> out <= 5.0 01:W4-LID 1.93 .001 1980.0111_21:05 300.36 n/a .000
02465> overflow <= 5.0 03:W4-LID-Out 6.25 .196 1980.0830_14:00 300.36 n/a .000
02466> {MxStoUsed=.1310E-01 m3, TotOvfVol=.1877E+01 m3, N-Ovf= 128, TotDurOvf= 172.hrs}
02467> R0080:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02468> ADD HYD 5.0 02:W1 8.92 .246 1980.0830_14:00 333.35 n/a .000
02469> + 5.0 02:W2 10.75 .291 1980.0830_14:00 329.13 n/a .000
02470> + 5.0 02:W3 6.30 .143 1980.0830_14:00 283.32 n/a .000
02471> + 5.0 02:W4 8.18 .198 1980.0830_14:00 300.36 n/a .000
02472> SUM= 5.0 01:BCD-PH3 34.15 .879 1980.0830_14:00 314.89 n/a .000
02473> R0080:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02474> ADD HYD 5.0 02:W1-LID-Out 6.55 .244 1980.0830_14:00 333.35 n/a .000
02475> + 5.0 02:W2-LID-Out 8.04 .288 1980.0830_14:00 329.13 n/a .000
02476> + 5.0 02:W3-LID-Out 4.82 .142 1980.0830_14:00 283.32 n/a .000
02477> + 5.0 02:W4-LID-Out 6.25 .196 1980.0830_14:00 300.36 n/a .000
02478> SUM= 5.0 01:BCD-PH3-LI 25.66 .869 1980.0830_14:00 314.59 n/a .000
02479> #*****
02480> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
02481> #*****
02482> # Set infiltration to 0 (CN = 99.99) for water balance analysis
02483> #*****
02484> R0080:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02485> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .304 1980.0830_14:00 408.33 .656 .000
02486> [XIMP=.66:TIMP=.71]
02487> [LOSS= 2 :CN=100.0]
02488> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02489> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
02490> [IaREcimp= 1.50: IaREcper= 6.00]
02491> [SMIN= 1.39: SMAX= 9.24: SK= .030]
02492> R0080:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms

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02493> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .362 1980.0830_14:00 406.13 .653 .000
02494> [XIMP=.65:TIMP=.70]
02495> [LOSS= 2 :CN=100.0]
02496> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02497> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
02498> [IaRECImp= 1.50: IaRECper= 6.00]
02499> [SMIN= 1.39: SMAX= 9.24: SK= .030]
02500> R0080:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02501> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .204 1980.0830_14:00 390.89 .628 .000
02502> [XIMP=.53:TIMP=.63]
02503> [LOSS= 2 :CN=100.0]
02504> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02505> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
02506> [IaRECImp= 1.50: IaRECper= 6.00]
02507> [SMIN= 1.39: SMAX= 9.24: SK= .030]
02508> R0080:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02509> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .271 1980.0830_14:00 399.88 .643 .000
02510> [XIMP=.57:TIMP=.67]
02511> [LOSS= 2 :CN=100.0]
02512> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02513> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
02514> [IaRECImp= 1.50: IaRECper= 6.00]
02515> [SMIN= 1.39: SMAX= 9.24: SK= .030]
02516> R0080:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02517> ADD HYD 5.0 02:INF-W1 8.92 .304 1980.0830_14:00 408.33 n/a .000
02518> + 5.0 02:INF-W2 10.75 .362 1980.0830_14:00 406.13 n/a .000
02519> + 5.0 02:INF-W3 6.30 .204 1980.0830_14:00 390.89 n/a .000
02520> + 5.0 02:INF-W4 8.18 .271 1980.0830_14:00 399.88 n/a .000
02521> SUM= 5.0 01:INF-BCD-PH 34.15 1.141 1980.0830_14:00 402.39 n/a .000
02522> #####
02523> # CONTINUOUS RAINFALL DATA
02524> #####
02525> ** END OF RUN : 80
02526>
02527> *****
02528>
02529>
02530>
02531>
02532>
02533> RUN#:COMMAND#
02534> R0081:C00001-----
02535> START
02536> [TZERO = .00 hrs on 19810101]
02537> [METOUT= 2 (1=imperial, 2=metric output)]
02538> [NSTORM= 0 ]
02539> [NRUN = 0081 ]
02540> #*****
02541> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
02542> #*****
02543> # Project Name: Barrhaven Conservancy Development
02544> # Project Number: 1474
02545> # Date : 2021/Oct/18
02546> # Modeller : J.Burnett, P.Eng.
02547> # Updated : 2022/Dec/13 [LP]
02548> # Company : J.F. Sabourin and Associates
02549> # License # : 2582634
02550> #*****
02551> # Ottawa International Airport (1967 - 2003)
02552> R0081:C00002-----
02553> * READ AES DATA
02554> [Filename = YOW_1967_2007.123 ]
02555> [Start_date= 1981.0101: End_date= 1981.1231]
02556> {DT= 60.min: Length= 8760.hrs: WetHrs= 641: DryHrs= 8119: PTOT= 936.40}
02557> Maximum average rainfall intensities over
02558> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02559> 35.30 31.85 26.20 18.15 9.27 4.83 3.22 2.41 1.62 mm/hr
02560> 35.30 63.70 78.60 108.90 111.30 115.90 115.90 115.90 116.70 mm
02561> 19810805 19810805 19810805 19810805 19810805 19810805 19810806 19810806 19810805 date
02562> Number of rainfall events per following interevent time
02563> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02564> 226 171 136 109 83 68 59 47 30
02565> Number of events with at least the following durations
02566> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02567> 225 128 79 28 7 0 0 0 0
02568> R0081:C00003-----
02569> COMPUTE API
02570> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
02571> {APImax=123.49: APIavg= 25.69: APImin= .26}
02572> #*****
02573> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
02574> #*****
02575> R0081:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02576> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .847 1981.0805_ 2:00 545.48 .583 .000
02577> [XIMP=.66:TIMP=.71]
02578> [LOSS= 2 :CN= 71.0]
02579> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02580> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
02581> [IaRECImp= 1.50: IaRECper= 6.00]

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02582> [SMIN= 41.38: SMAX=275.84: SK= .030]
02583> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
02584> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02585> # Total Volume provided by LID - 179 m³
02586> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02587> R0081:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02588> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .847 1981.0805_ 2:00 545.48 n/a .000
02589> out <= 5.0 01:W1-LID 1.94 .001 1981.0202_12:35 545.48 n/a .000
02590> overflow <= 5.0 03:W1-LID-Out 6.98 .832 1981.0805_ 2:05 545.48 n/a .000
02591> {MxStoUsed=.1788E-01 m3, TotOvfVol=.3806E+01 m3, N-Ovf= 145, TotDurOvf= 218.hrs}
02592> R0081:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02593> CONTINUOUS STANDHYD 5.0 01:W2 10.75 1.017 1981.0805_ 2:00 539.83 .577 .000
02594> [XIMP=.65:TIMP=.70]
02595> [LOSS= 2 :CN= 71.0]
02596> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02597> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
02598> [IaRECimp= 1.50: IaRECper= 6.00]
02599> [SMIN= 41.38: SMAX=275.84: SK= .030]
02600> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
02601> # Assumed 870 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02602> # Total Volume provided by LID - 200 m³
02603> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02604> R0081:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02605> ROUTE RESERVOIR -> 5.0 02:W2 10.75 1.017 1981.0805_ 2:00 539.83 n/a .000
02606> out <= 5.0 01:W2-LID 2.20 .001 1981.0202_12:25 539.82 n/a .000
02607> overflow <= 5.0 03:W2-LID-Out 8.55 1.002 1981.0805_ 2:05 539.83 n/a .000
02608> {MxStoUsed=.1999E-01 m3, TotOvfVol=.4616E+01 m3, N-Ovf= 149, TotDurOvf= 224.hrs}
02609> R0081:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02610> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .600 1981.0805_ 2:00 481.48 .514 .000
02611> [XIMP=.53:TIMP=.63]
02612> [LOSS= 2 :CN= 71.0]
02613> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02614> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
02615> [IaRECimp= 1.50: IaRECper= 6.00]
02616> [SMIN= 41.38: SMAX=275.84: SK= .030]
02617> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
02618> # Assumed 420 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02619> # Total Volume provided by LID - 96 m³
02620> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02621> R0081:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02622> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .600 1981.0805_ 2:00 481.48 n/a .000
02623> out <= 5.0 01:W3-LID 1.15 .001 1981.0202_12:15 481.49 n/a .000
02624> overflow <= 5.0 03:W3-LID-Out 5.15 .572 1981.0805_ 2:00 481.48 n/a .000
02625> {MxStoUsed=.9601E-02 m3, TotOvfVol=.2479E+01 m3, N-Ovf= 151, TotDurOvf= 228.hrs}
02626> R0081:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02627> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .781 1981.0805_ 2:00 504.22 .538 .000
02628> [XIMP=.57:TIMP=.67]
02629> [LOSS= 2 :CN= 71.0]
02630> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02631> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
02632> [IaRECimp= 1.50: IaRECper= 6.00]
02633> [SMIN= 41.38: SMAX=275.84: SK= .030]
02634> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
02635> # Assumed 570 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02636> # Total Volume provided by LID - 131 m³
02637> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02638> R0081:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02639> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .781 1981.0805_ 2:00 504.22 n/a .000
02640> out <= 5.0 01:W4-LID 1.53 .001 1981.0202_12:15 504.22 n/a .000
02641> overflow <= 5.0 03:W4-LID-Out 6.65 .777 1981.0805_ 2:05 504.22 n/a .000
02642> {MxStoUsed=.1308E-01 m3, TotOvfVol=.3355E+01 m3, N-Ovf= 153, TotDurOvf= 227.hrs}
02643> R0081:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02644> ADD HYD 5.0 02:W1 8.92 .847 1981.0805_ 2:00 545.48 n/a .000
02645> + 5.0 02:W2 10.75 1.017 1981.0805_ 2:00 539.83 n/a .000
02646> + 5.0 02:W3 6.30 .600 1981.0805_ 2:00 481.48 n/a .000
02647> + 5.0 02:W4 8.18 .781 1981.0805_ 2:00 504.22 n/a .000
02648> SUM= 5.0 01:BCD-PH3 34.15 3.245 1981.0805_ 2:00 522.01 n/a .000
02649> R0081:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02650> ADD HYD 5.0 02:W1-LID-Out 6.98 .832 1981.0805_ 2:05 545.48 n/a .000
02651> + 5.0 02:W2-LID-Out 8.55 1.002 1981.0805_ 2:05 539.83 n/a .000
02652> + 5.0 02:W3-LID-Out 5.15 .572 1981.0805_ 2:00 481.48 n/a .000
02653> + 5.0 02:W4-LID-Out 6.65 .777 1981.0805_ 2:05 504.22 n/a .000
02654> SUM= 5.0 01:BCD-PH3-LI 27.33 3.178 1981.0805_ 2:05 521.61 n/a .000
02655> #*****
02656> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDI
02657> #*****
02658> # Set infiltration to 0 (CN = 99.99) for water balance analysis
02659> #*****
02660> R0081:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02661> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .875 1981.0805_ 2:00 650.22 .694 .000
02662> [XIMP=.66:TIMP=.71]
02663> [LOSS= 2 :CN=100.0]
02664> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02665> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
02666> [IaRECimp= 1.50: IaRECper= 6.00]
02667> [SMIN= 1.39: SMAX= 9.24: SK= .030]
02668> R0081:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02669> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 1.055 1981.0805_ 2:00 647.50 .691 .000
02670> [XIMP=.65:TIMP=.70]

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02671> [LOSS= 2 :CN=100.0]
02672> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02673> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
02674> [IaRECImp= 1.50: IaRECper= 6.00]
02675> [SMIN= 1.39: SMAX= 9.24: SK= .030]
02676> R0081:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02677> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .621 1981.0805_ 2:00 629.67 .672 .000
02678> [XIMP=.53:TIMP=.63]
02679> [LOSS= 2 :CN=100.0]
02680> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02681> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
02682> [IaRECImp= 1.50: IaRECper= 6.00]
02683> [SMIN= 1.39: SMAX= 9.24: SK= .030]
02684> R0081:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02685> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .805 1981.0805_ 2:00 640.67 .684 .000
02686> [XIMP=.57:TIMP=.67]
02687> [LOSS= 2 :CN=100.0]
02688> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02689> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
02690> [IaRECImp= 1.50: IaRECper= 6.00]
02691> [SMIN= 1.39: SMAX= 9.24: SK= .030]
02692> R0081:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02693> ADD HYD 5.0 02:INF-W1 8.92 .875 1981.0805_ 2:00 650.22 n/a .000
02694> + 5.0 02:INF-W2 10.75 1.055 1981.0805_ 2:00 647.50 n/a .000
02695> + 5.0 02:INF-W3 6.30 .621 1981.0805_ 2:00 629.67 n/a .000
02696> + 5.0 02:INF-W4 8.18 .805 1981.0805_ 2:00 640.67 n/a .000
02697> SUM= 5.0 01:INF-BCD-PH 34.15 3.356 1981.0805_ 2:00 643.29 n/a .000
02698> #####
02699> # CONTINUOUS RAINFALL DATA
02700> #####
02701> ** END OF RUN : 81
02702>
02703> *****
02704>
02705>
02706>
02707>
02708>
02709> RUN#:COMMAND#
02710> R0082:C00001-----
02711> START
02712> [TZERO = .00 hrs on 19820101]
02713> [METOUT= 2 (1=imperial, 2=metric output)]
02714> [NSTORM= 0 ]
02715> [NRUN = 0082 ]
02716> #*****
02717> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
02718> #*****
02719> # Project Name: Barrhaven Conservancy Development
02720> # Project Number: 1474
02721> # Date : 2021/Oct/18
02722> # Modeller : J.Burnett, P.Eng.
02723> # Updated : 2022/Dec/13 [LP]
02724> # Company : J.F. Sabourin and Associates
02725> # License # : 2582634
02726> #*****
02727> # Ottawa International Airport (1967 - 2003)
02728> R0082:C00002-----
02729> * READ AES DATA
02730> [Filename = YOW_1967_2007.123 ]
02731> [Start_date= 1982.0101: End_date= 1982.1231]
02732> {DT= 60.min: Length= 8760.hrs: WetHrs= 436: DryHrs= 8324: PTOT= 596.10}
02733> Maximum average rainfall intensities over
02734> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02735> 19.80 10.75 7.60 5.83 3.36 1.68 1.12 .96 .80 mm/hr
02736> 19.80 21.50 22.80 35.00 40.30 40.30 40.30 46.30 57.30 mm
02737> 19820801 19820901 19820825 19820825 19820825 19820826 19820825 19820825 date
02738> Number of rainfall events per following interevent time
02739> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02740> 134 110 98 78 66 57 48 41 33
02741> Number of events with at least the following durations
02742> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02743> 133 81 58 18 4 1 1 0 0
02744> R0082:C00003-----
02745> COMPUTE API
02746> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
02747> [APIimax= 56.66: APIavg= 16.78: APIimin= .03]
02748> #*****
02749> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
02750> #*****
02751> R0082:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02752> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .332 1982.0801_19:00 318.54 .534 .000
02753> [XIMP=.66:TIMP=.71]
02754> [LOSS= 2 :CN= 71.0]
02755> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02756> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
02757> [IaRECImp= 1.50: IaRECper= 6.00]
02758> [SMIN= 41.38: SMAX=275.84: SK= .030]
02759> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)

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02760> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02761> # Total Volume provided by LID - 179 m³
02762> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02763> R0082:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02764> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .332 1982.0801_19:00 318.54 n/a .000
02765> out <= 5.0 01:W1-LID 2.61 .001 1982.0313_11:20 318.55 n/a .000
02766> overflow <= 5.0 03:W1-LID-Out 6.31 .329 1982.0801_19:00 318.54 n/a .000
02767> {MxStoUsed=.1790E-01 m3, TotOvfVol=.2011E+01 m3, N-Ovf= 122, TotDurOvf= 176.hrs}
02768> R0082:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02769> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .392 1982.0801_19:00 314.38 .527 .000
02770> [XIMP=.65:TIMP=.70]
02771> [LOSS= 2 :CN= 71.0]
02772> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02773> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
02774> [IaREcimp= 1.50: IaREcper= 6.00]
02775> [SMIN= 41.38: SMAX=275.84: SK= .030]
02776> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
02777> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02778> # Total Volume provided by LID - 200 m³
02779> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02780> R0082:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02781> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .392 1982.0801_19:00 314.38 n/a .000
02782> out <= 5.0 01:W2-LID 2.96 .001 1982.0313_11:15 314.37 n/a .000
02783> overflow <= 5.0 03:W2-LID-Out 7.79 .388 1982.0801_19:00 314.38 n/a .000
02784> {MxStoUsed=.2000E-01 m3, TotOvfVol=.2449E+01 m3, N-Ovf= 123, TotDurOvf= 184.hrs}
02785> R0082:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02786> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .195 1982.0801_19:00 268.25 .450 .000
02787> [XIMP=.53:TIMP=.63]
02788> [LOSS= 2 :CN= 71.0]
02789> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02790> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
02791> [IaREcimp= 1.50: IaREcper= 6.00]
02792> [SMIN= 41.38: SMAX=275.84: SK= .030]
02793> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
02794> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02795> # Total Volume provided by LID - 96 m³
02796> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02797> R0082:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02798> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .195 1982.0801_19:00 268.25 n/a .000
02799> out <= 5.0 01:W3-LID 1.64 .001 1982.0313_11:15 268.25 n/a .000
02800> overflow <= 5.0 03:W3-LID-Out 4.66 .193 1982.0801_19:00 268.25 n/a .000
02801> {MxStoUsed=.9596E-02 m3, TotOvfVol=.1251E+01 m3, N-Ovf= 138, TotDurOvf= 187.hrs}
02802> R0082:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02803> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .270 1982.0801_19:00 285.01 .478 .000
02804> [XIMP=.57:TIMP=.67]
02805> [LOSS= 2 :CN= 71.0]
02806> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02807> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
02808> [IaREcimp= 1.50: IaREcper= 6.00]
02809> [SMIN= 41.38: SMAX=275.84: SK= .030]
02810> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
02811> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02812> # Total Volume provided by LID - 131 m³
02813> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02814> R0082:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02815> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .270 1982.0801_19:00 285.01 n/a .000
02816> out <= 5.0 01:W4-LID 2.13 .001 1982.0313_11:15 285.01 n/a .000
02817> overflow <= 5.0 03:W4-LID-Out 6.05 .266 1982.0801_19:00 285.01 n/a .000
02818> {MxStoUsed=.1310E-01 m3, TotOvfVol=.1726E+01 m3, N-Ovf= 135, TotDurOvf= 188.hrs}
02819> R0082:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02820> ADD HYD 5.0 02:W1 8.92 .332 1982.0801_19:00 318.54 n/a .000
02821> + 5.0 02:W2 10.75 .392 1982.0801_19:00 314.38 n/a .000
02822> + 5.0 02:W3 6.30 .195 1982.0801_19:00 268.25 n/a .000
02823> + 5.0 02:W4 8.18 .270 1982.0801_19:00 285.01 n/a .000
02824> SUM= 5.0 01:BCD-PH3 34.15 1.189 1982.0801_19:00 299.92 n/a .000
02825> R0082:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02826> ADD HYD 5.0 02:W1-LID-Out 6.31 .329 1982.0801_19:00 318.54 n/a .000
02827> + 5.0 02:W2-LID-Out 7.79 .388 1982.0801_19:00 314.38 n/a .000
02828> + 5.0 02:W3-LID-Out 4.66 .193 1982.0801_19:00 268.25 n/a .000
02829> + 5.0 02:W4-LID-Out 6.05 .266 1982.0801_19:00 285.01 n/a .000
02830> SUM= 5.0 01:BCD-PH3-LI 24.82 1.176 1982.0801_19:00 299.61 n/a .000
02831> #*****
02832> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
02833> #*****
02834> # Set infiltration to 0 (CN = 99.99) for water balance analysis
02835> #*****
02836> R0082:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02837> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .429 1982.0801_19:00 388.92 .652 .000
02838> [XIMP=.66:TIMP=.71]
02839> [LOSS= 2 :CN=100.0]
02840> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02841> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
02842> [IaREcimp= 1.50: IaREcper= 6.00]
02843> [SMIN= 1.39: SMAX= 9.24: SK= .030]
02844> R0082:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02845> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .512 1982.0801_19:00 386.61 .649 .000
02846> [XIMP=.65:TIMP=.70]
02847> [LOSS= 2 :CN=100.0]
02848> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]

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02849> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
02850> [IaREcimp= 1.50: IaREcper= 6.00]
02851> [SMIN= 1.39: SMAX= 9.24: SK= .030]
02852> R0082:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02853> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .302 1982.0801_19:00 370.01 .621 .000
02854> [XIMP=.53:TIMP=.63]
02855> [LOSS= 2 :CN=100.0]
02856> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02857> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
02858> [IaREcimp= 1.50: IaREcper= 6.00]
02859> [SMIN= 1.39: SMAX= 9.24: SK= .030]
02860> R0082:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02861> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .396 1982.0801_19:00 379.41 .637 .000
02862> [XIMP=.57:TIMP=.67]
02863> [LOSS= 2 :CN=100.0]
02864> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02865> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
02866> [IaREcimp= 1.50: IaREcper= 6.00]
02867> [SMIN= 1.39: SMAX= 9.24: SK= .030]
02868> R0082:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02869> ADD HYD 5.0 02:INF-W1 8.92 .429 1982.0801_19:00 388.92 n/a .000
02870> + 5.0 02:INF-W2 10.75 .512 1982.0801_19:00 386.61 n/a .000
02871> + 5.0 02:INF-W3 6.30 .302 1982.0801_19:00 370.01 n/a .000
02872> + 5.0 02:INF-W4 8.18 .396 1982.0801_19:00 379.41 n/a .000
02873> SUM= 5.0 01:INF-BCD-PH 34.15 1.639 1982.0801_19:00 382.43 n/a .000
02874> #####
02875> # CONTINUOUS RAINFALL DATA
02876> #####
02877> ** END OF RUN : 82
02878>
02879> *****
02880>
02881>
02882>
02883>
02884>
02885> RUN#:COMMAND#
02886> R0083:C00001-----
02887> START
02888> [TZERO = .00 hrs on 19830101]
02889> [METOUT= 2 (1=imperial, 2=metric output)]
02890> [NSTORM= 0 ]
02891> [NRUN = 0083 ]
02892> #*****
02893> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
02894> #*****
02895> # Project Name: Barrhaven Conservancy Development
02896> # Project Number: 1474
02897> # Date : 2021/Oct/18
02898> # Modeller : J.Burnett, P.Eng.
02899> # Updated : 2022/Dec/13 [LP]
02900> # Company : J.F. Sabourin and Associates
02901> # License # : 2582634
02902> #*****
02903> # Ottawa International Airport (1967 - 2003)
02904> R0083:C00002-----
02905> * READ AES DATA
02906> [Filename = YOW_1967_2007.123 ]
02907> [Start_date= 1983.0101: End_date= 1983.1231]
02908> {DT= 60.min: Length= 8760.hrs: WetHrs= 462: DryHrs= 8298: PTOT= 587.50}
02909> Maximum average rainfall intensities over
02910> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02911> 10.40 9.70 7.53 5.43 3.18 2.36 1.68 1.32 .92 mm/hr
02912> 10.40 19.40 22.60 32.60 38.20 56.70 60.40 63.20 66.00 mm
02913> 19831004 19830921 19830921 19831005 19831005 19831005 19831006 19831008 date
02914> Number of rainfall events per following interevent time
02915> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02916> 143 115 103 85 70 55 50 45 35
02917> Number of events with at least the following durations
02918> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02919> 142 87 56 28 5 0 0 0 0
02920> R0083:C00003-----
02921> COMPUTE API
02922> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
02923> [APImax= 79.86: APIavg= 16.57: APImin= .05]
02924> #*****
02925> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
02926> #*****
02927> R0083:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
02928> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .196 1983.1005_15:00 305.95 .521 .000
02929> [XIMP=.66:TIMP=.71]
02930> [LOSS= 2 :CN= 71.0]
02931> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02932> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
02933> [IaREcimp= 1.50: IaREcper= 6.00]
02934> [SMIN= 41.38: SMAX=275.84: SK= .030]
02935> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
02936> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02937> # Total Volume provided by LID - 179 m³

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02938> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02939> R0083:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02940> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .196 1983.1005_15:00 305.95 n/a .000
02941> out <= 5.0 01:W1-LID 2.68 .001 1983.0318_23:35 305.96 n/a .000
02942> overflow <= 5.0 03:W1-LID-Out 6.24 .194 1983.1005_15:00 305.95 n/a .000
02943> {MxStoUsed=.1790E-01 m3, TotOvfVol=.1910E+01 m3, N-Ovf= 128, TotDurOvf= 184.hrs}
02944> R0083:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02945> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .234 1983.1005_15:00 302.07 .514 .000
02946> [XIMP=.65:TIMP=.70]
02947> [LOSS= 2 :CN= 71.0]
02948> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02949> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
02950> [IaREcimp= 1.50: IaREcper= 6.00]
02951> [SMIN= 41.38: SMAX=275.84: SK= .030]
02952> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
02953> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02954> # Total Volume provided by LID - 200 m³
02955> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02956> R0083:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02957> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .234 1983.1005_15:00 302.07 n/a .000
02958> out <= 5.0 01:W2-LID 3.04 .001 1983.0318_23:35 302.06 n/a .000
02959> overflow <= 5.0 03:W2-LID-Out 7.71 .231 1983.1005_15:00 302.07 n/a .000
02960> {MxStoUsed=.1999E-01 m3, TotOvfVol=.2328E+01 m3, N-Ovf= 116, TotDurOvf= 191.hrs}
02961> R0083:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02962> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .129 1983.1005_15:00 259.77 .442 .000
02963> [XIMP=.53:TIMP=.63]
02964> [LOSS= 2 :CN= 71.0]
02965> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02966> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
02967> [IaREcimp= 1.50: IaREcper= 6.00]
02968> [SMIN= 41.38: SMAX=275.84: SK= .030]
02969> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
02970> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02971> # Total Volume provided by LID - 96 m³
02972> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02973> R0083:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02974> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .129 1983.1005_15:00 259.77 n/a .000
02975> out <= 5.0 01:W3-LID 1.67 .001 1983.0318_23:30 259.78 n/a .000
02976> overflow <= 5.0 03:W3-LID-Out 4.63 .127 1983.1005_15:00 259.77 n/a .000
02977> {MxStoUsed=.9592E-02 m3, TotOvfVol=.1203E+01 m3, N-Ovf= 125, TotDurOvf= 195.hrs}
02978> R0083:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02979> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .173 1983.1005_15:00 275.42 .469 .000
02980> [XIMP=.57:TIMP=.67]
02981> [LOSS= 2 :CN= 71.0]
02982> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
02983> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
02984> [IaREcimp= 1.50: IaREcper= 6.00]
02985> [SMIN= 41.38: SMAX=275.84: SK= .030]
02986> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
02987> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
02988> # Total Volume provided by LID - 131 m³
02989> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02990> R0083:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02991> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .173 1983.1005_15:00 275.42 n/a .000
02992> out <= 5.0 01:W4-LID 2.17 .001 1983.0318_23:35 275.42 n/a .000
02993> overflow <= 5.0 03:W4-LID-Out 6.01 .171 1983.1005_15:05 275.42 n/a .000
02994> {MxStoUsed=.1310E-01 m3, TotOvfVol=.1654E+01 m3, N-Ovf= 124, TotDurOvf= 195.hrs}
02995> R0083:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
02996> ADD HYD 5.0 02:W1 8.92 .196 1983.1005_15:00 305.95 n/a .000
02997> + 5.0 02:W2 10.75 .234 1983.1005_15:00 302.07 n/a .000
02998> + 5.0 02:W3 6.30 .129 1983.1005_15:00 259.77 n/a .000
02999> + 5.0 02:W4 8.18 .173 1983.1005_15:00 275.42 n/a .000
03000> SUM= 5.0 01:BCD-PH3 34.15 .732 1983.1005_15:00 288.90 n/a .000
03001> R0083:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03002> ADD HYD 5.0 02:W1-LID-Out 6.24 .194 1983.1005_15:00 305.95 n/a .000
03003> + 5.0 02:W2-LID-Out 7.71 .231 1983.1005_15:00 302.07 n/a .000
03004> + 5.0 02:W3-LID-Out 4.63 .127 1983.1005_15:00 259.77 n/a .000
03005> + 5.0 02:W4-LID-Out 6.01 .171 1983.1005_15:05 275.42 n/a .000
03006> SUM= 5.0 01:BCD-PH3-LI 24.58 .722 1983.1005_15:05 288.58 n/a .000
03007> #*****
03008> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
03009> #*****
03010> # Set infiltration to 0 (CN = 99.99) for water balance analysis
03011> #*****
03012> R0083:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03013> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .242 1983.1005_15:00 370.31 .630 .000
03014> [XIMP=.66:TIMP=.71]
03015> [LOSS= 2 :CN=100.0]
03016> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03017> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
03018> [IaREcimp= 1.50: IaREcper= 6.00]
03019> [SMIN= 1.39: SMAX= 9.24: SK= .030]
03020> R0083:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03021> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .291 1983.1005_15:00 368.12 .627 .000
03022> [XIMP=.65:TIMP=.70]
03023> [LOSS= 2 :CN=100.0]
03024> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03025> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
03026> [IaREcimp= 1.50: IaREcper= 6.00]

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03027> [SMIN= 1.39: SMAX= 9.24: SK=.030]
03028> R0083:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03029> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .171 1983.1005_15:00 353.08 .601 .000
03030> [XIMP=.53:TIMP=.63]
03031> [LOSS= 2 :CN=100.0]
03032> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03033> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
03034> [IaRECimp= 1.50: IaRECper= 6.00]
03035> [SMIN= 1.39: SMAX= 9.24: SK=.030]
03036> R0083:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03037> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .221 1983.1005_15:00 362.01 .616 .000
03038> [XIMP=.57:TIMP=.67]
03039> [LOSS= 2 :CN=100.0]
03040> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03041> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
03042> [IaRECimp= 1.50: IaRECper= 6.00]
03043> [SMIN= 1.39: SMAX= 9.24: SK=.030]
03044> R0083:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03045> ADD HYD 5.0 02:INF-W1 8.92 .242 1983.1005_15:00 370.31 n/a .000
03046> + 5.0 02:INF-W2 10.75 .291 1983.1005_15:00 368.12 n/a .000
03047> + 5.0 02:INF-W3 6.30 .171 1983.1005_15:00 353.08 n/a .000
03048> + 5.0 02:INF-W4 8.18 .221 1983.1005_15:00 362.01 n/a .000
03049> SUM= 5.0 01:INF-BCD-PH 34.15 .925 1983.1005_15:00 364.45 n/a .000
03050> #####
03051> # CONTINUOUS RAINFALL DATA
03052> #####
03053> ** END OF RUN : 83
03054>
03055> *****
03056>
03057>
03058>
03059>
03060>
03061> RUN#:COMMAND#
03062> R0084:C00001-----
03063> START
03064> [TZERO = .00 hrs on 19840101]
03065> [METOUT= 2 (1=imperial, 2=metric output)]
03066> [NSTORM= 0 ]
03067> [NRUN = 0084 ]
03068> #*****
03069> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
03070> #*****
03071> # Project Name: Barrhaven Conservancy Development
03072> # Project Number: 1474
03073> # Date : 2021/Oct/18
03074> # Modeller : J.Burnett, P.Eng.
03075> # Updated : 2022/Dec/13 [LP]
03076> # Company : J.F. Sabourin and Associates
03077> # License # : 2582634
03078> #*****
03079> # Ottawa International Airport (1967 - 2003)
03080> R0084:C00002-----
03081> * READ AES DATA
03082> [Filename = YOW_1967_2007.123 ]
03083> [Start_date= 1984.0101: End_date= 1984.1230]
03084> {DT= 60.min: Length= 8760.hrs: WetHrs= 308: DryHrs= 8452: PTOT= 459.40}
03085> Maximum average rainfall intensities over
03086> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03087> 17.80 9.70 7.57 4.33 3.01 1.85 1.58 1.19 1.00 mm/hr
03088> 17.80 19.40 22.70 26.00 36.10 44.30 57.00 57.00 72.20 mm
03089> 19840812 19840812 19840812 19840806 19840812 19840813 19840813 19840814 19840813 date
03090> Number of rainfall events per following interevent time
03091> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03092> 98 80 75 63 55 48 40 34 26
03093> Number of events with at least the following durations
03094> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03095> 97 58 39 11 3 1 0 0 0
03096> R0084:C00003-----
03097> COMPUTE API
03098> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
03099> {APImax= 86.83: APIavg= 13.22: APImin= .00}
03100> #*****
03101> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
03102> #*****
03103> R0084:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03104> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .314 1984.0812_ 7:00 254.10 .553 .000
03105> [XIMP=.66:TIMP=.71]
03106> [LOSS= 2 :CN= 71.0]
03107> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03108> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
03109> [IaRECimp= 1.50: IaRECper= 6.00]
03110> [SMIN= 41.38: SMAX=275.84: SK=.030]
03111> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
03112> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
03113> # Total Volume provided by LID - 179 m3
03114> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
03115> R0084:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms

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03116> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .314 1984.0812_ 7:00 254.10 n/a .000
03117> out <= 5.0 01:W1-LID 2.14 .001 1984.0214_ 9:10 254.10 n/a .000
03118> overflow <= 5.0 03:W1-LID-Out 6.78 .310 1984.0812_ 7:00 254.10 n/a .000
03119> {MxStoUsed=.1788E-01 m3, TotOvfVol=.1723E+01 m3, N-Ovf= 89, TotDurOvf= 140.hrs}
03120> R0084:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03121> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .373 1984.0812_ 7:00 250.97 .546 .000
03122> [XIMP=.65:TIMP=.70]
03123> [LOSS= 2 :CN= 71.0]
03124> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03125> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
03126> [IaREcimp= 1.50: IaRECper= 6.00]
03127> [SMIN= 41.38: SMAX=275.84: SK= .030]
03128> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
03129> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
03130> # Total Volume provided by LID - 200 m³
03131> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
03132> R0084:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03133> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .373 1984.0812_ 7:00 250.97 n/a .000
03134> out <= 5.0 01:W2-LID 2.44 .001 1984.0214_ 9:00 250.97 n/a .000
03135> overflow <= 5.0 03:W2-LID-Out 8.31 .369 1984.0812_ 7:00 250.97 n/a .000
03136> {MxStoUsed=.2000E-01 m3, TotOvfVol=.2086E+01 m3, N-Ovf= 97, TotDurOvf= 143.hrs}
03137> R0084:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03138> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .194 1984.0812_ 7:00 217.61 .474 .000
03139> [XIMP=.53:TIMP=.63]
03140> [LOSS= 2 :CN= 71.0]
03141> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03142> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
03143> [IaREcimp= 1.50: IaRECper= 6.00]
03144> [SMIN= 41.38: SMAX=275.84: SK= .030]
03145> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
03146> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
03147> # Total Volume provided by LID - 96 m³
03148> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
03149> R0084:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03150> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .194 1984.0812_ 7:00 217.61 n/a .000
03151> out <= 5.0 01:W3-LID 1.33 .001 1984.0214_ 8:55 217.61 n/a .000
03152> overflow <= 5.0 03:W3-LID-Out 4.97 .191 1984.0812_ 7:00 217.61 n/a .000
03153> {MxStoUsed=.9592E-02 m3, TotOvfVol=.1082E+01 m3, N-Ovf= 97, TotDurOvf= 147.hrs}
03154> R0084:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03155> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .265 1984.0812_ 7:00 230.17 .501 .000
03156> [XIMP=.57:TIMP=.67]
03157> [LOSS= 2 :CN= 71.0]
03158> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03159> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
03160> [IaREcimp= 1.50: IaRECper= 6.00]
03161> [SMIN= 41.38: SMAX=275.84: SK= .030]
03162> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
03163> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
03164> # Total Volume provided by LID - 131 m³
03165> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
03166> R0084:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03167> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .265 1984.0812_ 7:00 230.18 n/a .000
03168> out <= 5.0 01:W4-LID 1.73 .001 1984.0214_ 8:55 230.17 n/a .000
03169> overflow <= 5.0 03:W4-LID-Out 6.45 .261 1984.0812_ 7:00 230.18 n/a .000
03170> {MxStoUsed=.1309E-01 m3, TotOvfVol=.1484E+01 m3, N-Ovf= 88, TotDurOvf= 146.hrs}
03171> R0084:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03172> ADD HYD 5.0 02:W1 8.92 .314 1984.0812_ 7:00 254.10 n/a .000
03173> + 5.0 02:W2 10.75 .373 1984.0812_ 7:00 250.97 n/a .000
03174> + 5.0 02:W3 6.30 .194 1984.0812_ 7:00 217.61 n/a .000
03175> + 5.0 02:W4 8.18 .265 1984.0812_ 7:00 230.18 n/a .000
03176> SUM= 5.0 01:BCD-PH3 34.15 1.147 1984.0812_ 7:00 240.65 n/a .000
03177> R0084:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03178> ADD HYD 5.0 02:W1-LID-Out 6.78 .310 1984.0812_ 7:00 254.10 n/a .000
03179> + 5.0 02:W2-LID-Out 8.31 .369 1984.0812_ 7:00 250.97 n/a .000
03180> + 5.0 02:W3-LID-Out 4.97 .191 1984.0812_ 7:00 217.61 n/a .000
03181> + 5.0 02:W4-LID-Out 6.45 .261 1984.0812_ 7:00 230.18 n/a .000
03182> SUM= 5.0 01:BCD-PH3-LI 26.51 1.131 1984.0812_ 7:00 240.45 n/a .000
03183> #*****
03184> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
03185> #*****
03186> # Set infiltration to 0 (CN = 99.99) for water balance analysis
03187> #*****
03188> R0084:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03189> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .413 1984.0812_ 7:00 313.27 .682 .000
03190> [XIMP=.66:TIMP=.71]
03191> [LOSS= 2 :CN=100.0]
03192> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03193> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
03194> [IaREcimp= 1.50: IaRECper= 6.00]
03195> [SMIN= 1.39: SMAX= 9.24: SK= .030]
03196> R0084:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03197> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .495 1984.0812_ 7:00 311.76 .679 .000
03198> [XIMP=.65:TIMP=.70]
03199> [LOSS= 2 :CN=100.0]
03200> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03201> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
03202> [IaREcimp= 1.50: IaRECper= 6.00]
03203> [SMIN= 1.39: SMAX= 9.24: SK= .030]
03204> R0084:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms

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03205> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .292 1984.0812_ 7:00 301.85 .657 .000
03206> [XIMP=.53:TIMP=.63]
03207> [LOSS= 2 :CN=100.0]
03208> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03209> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
03210> [IaREcimp= 1.50: IaRECper= 6.00]
03211> [SMIN= 1.39: SMAX= 9.24: SK= .030]
03212> R0084:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03213> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .376 1984.0812_ 7:00 307.93 .670 .000
03214> [XIMP=.57:TIMP=.67]
03215> [LOSS= 2 :CN=100.0]
03216> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03217> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
03218> [IaREcimp= 1.50: IaRECper= 6.00]
03219> [SMIN= 1.39: SMAX= 9.24: SK= .030]
03220> R0084:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03221> ADD HYD 5.0 02:INF-W1 8.92 .413 1984.0812_ 7:00 313.27 n/a .000
03222> + 5.0 02:INF-W2 10.75 .495 1984.0812_ 7:00 311.76 n/a .000
03223> + 5.0 02:INF-W3 6.30 .292 1984.0812_ 7:00 301.85 n/a .000
03224> + 5.0 02:INF-W4 8.18 .376 1984.0812_ 7:00 307.93 n/a .000
03225> SUM= 5.0 01:INF-BCD-PH 34.15 1.577 1984.0812_ 7:00 309.41 n/a .000
03226> #####
03227> # CONTINUOUS RAINFALL DATA
03228> #####
03229> ** END OF RUN : 84
03230>
03231> *****
03232>
03233>
03234>
03235>
03236>
03237> RUN#:COMMAND#
03238> R0085:C00001-----
03239> START
03240> [TZERO = .00 hrs on 19850101]
03241> [METOUT= 2 (1=imperial, 2=metric output)]
03242> [NSTORM= 0 ]
03243> [NRUN = 0085 ]
03244> #*****
03245> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
03246> #*****
03247> # Project Name: Barrhaven Conservancy Development
03248> # Project Number: 1474
03249> # Date : 2021/Oct/18
03250> # Modeller : J.Burnett, P.Eng.
03251> # Updated : 2022/Dec/13 [LP]
03252> # Company : J.F. Sabourin and Associates
03253> # License # : 2582634
03254> #*****
03255> # Ottawa International Airport (1967 - 2003)
03256> R0085:C00002-----
03257> * READ AES DATA
03258> [Filename = YOW_1967_2007.123 ]
03259> [Start_date= 1985.0101: End_date= 1985.1231]
03260> {DT= 60.min: Length= 8760.hrs: WetHrs= 354: DryHrs= 8406: PTOT= 559.90}
03261> Maximum average rainfall intensities over
03262> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03263> 19.00 13.60 11.73 6.60 3.30 1.65 1.11 .89 .60 mm/hr
03264> 19.00 27.20 35.20 39.60 39.60 40.10 42.80 43.40
03265> 19850716 19850617 19850617 19850618 19850618 19850618 19850618 19850827 19850827 date
03266> Number of rainfall events per following interevent time
03267> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03268> 108 88 84 74 69 56 49 43 32
03269> Number of events with at least the following durations
03270> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03271> 107 70 43 13 4 1 0 0 0
03272> R0085:C00003-----
03273> COMPUTE API
03274> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
03275> [APIimax= 57.29: APIavg= 15.86: APIimin= .20]
03276> #*****
03277> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
03278> #*****
03279> R0085:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03280> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .320 1985.0716_14:00 313.70 .560 .000
03281> [XIMP=.66:TIMP=.71]
03282> [LOSS= 2 :CN= 71.0]
03283> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03284> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
03285> [IaREcimp= 1.50: IaRECper= 6.00]
03286> [SMIN= 41.38: SMAX=275.84: SK= .030]
03287> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
03288> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
03289> # Total Volume provided by LID - 179 m³
03290> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
03291> R0085:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03292> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .320 1985.0716_14:00 313.70 n/a .000
03293> out <= 5.0 01:W1-LID 2.11 .001 1985.0223_12:30 313.71 n/a .000

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03294> overflow <= 5.0 03:W1-LID-Out 6.81 .317 1985.0716_14:00 313.70 n/a .000
03295> {MxStoUsed=.1789E-01 m3, TotOvfVol=.2136E+01 m3, N-Ovf= 76, TotDurOvf= 145.hrs}
03296> R0085:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RVmm-R.C.---DWFcms
03297> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .379 1985.0716_14:00 309.67 .553 .000
03298> [XIMP=.65:TIMP=.70]
03299> [LOSS= 2 :CN= 71.0]
03300> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03301> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
03302> [IaRECimp= 1.50: IaRECper= 6.00]
03303> [SMIN= 41.38: SMAX=275.84: SK= .030]
03304> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
03305> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
03306> # Total Volume provided by LID - 200 m³
03307> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
03308> R0085:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RVmm-R.C.---DWFcms
03309> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .379 1985.0716_14:00 309.67 n/a .000
03310> out <= 5.0 01:W2-LID 2.41 .001 1985.0222_ 9:10 309.67 n/a .000
03311> overflow <= 5.0 03:W2-LID-Out 8.34 .375 1985.0716_14:00 309.67 n/a .000
03312> {MxStoUsed=.1999E-01 m3, TotOvfVol=.2581E+01 m3, N-Ovf= 86, TotDurOvf= 150.hrs}
03313> R0085:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RVmm-R.C.---DWFcms
03314> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .188 1985.0716_14:00 265.42 .474 .000
03315> [XIMP=.53:TIMP=.63]
03316> [LOSS= 2 :CN= 71.0]
03317> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03318> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
03319> [IaRECimp= 1.50: IaRECper= 6.00]
03320> [SMIN= 41.38: SMAX=275.84: SK= .030]
03321> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
03322> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
03323> # Total Volume provided by LID - 96 m³
03324> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
03325> R0085:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RVmm-R.C.---DWFcms
03326> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .188 1985.0716_14:00 265.42 n/a .000
03327> out <= 5.0 01:W3-LID 1.33 .001 1985.0222_ 9:05 265.43 n/a .000
03328> overflow <= 5.0 03:W3-LID-Out 4.97 .186 1985.0716_14:00 265.42 n/a .000
03329> {MxStoUsed=.9599E-02 m3, TotOvfVol=.1319E+01 m3, N-Ovf= 87, TotDurOvf= 153.hrs}
03330> R0085:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RVmm-R.C.---DWFcms
03331> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .260 1985.0716_14:00 281.65 .503 .000
03332> [XIMP=.57:TIMP=.67]
03333> [LOSS= 2 :CN= 71.0]
03334> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03335> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
03336> [IaRECimp= 1.50: IaRECper= 6.00]
03337> [SMIN= 41.38: SMAX=275.84: SK= .030]
03338> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
03339> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
03340> # Total Volume provided by LID - 131 m³
03341> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
03342> R0085:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RVmm-R.C.---DWFcms
03343> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .260 1985.0716_14:00 281.65 n/a .000
03344> out <= 5.0 01:W4-LID 1.73 .001 1985.0222_ 9:05 281.65 n/a .000
03345> overflow <= 5.0 03:W4-LID-Out 6.45 .257 1985.0716_14:00 281.65 n/a .000
03346> {MxStoUsed=.1310E-01 m3, TotOvfVol=.1816E+01 m3, N-Ovf= 81, TotDurOvf= 153.hrs}
03347> R0085:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RVmm-R.C.---DWFcms
03348> ADD HYD 5.0 02:W1 8.92 .320 1985.0716_14:00 313.70 n/a .000
03349> + 5.0 02:W2 10.75 .379 1985.0716_14:00 309.67 n/a .000
03350> + 5.0 02:W3 6.30 .188 1985.0716_14:00 265.42 n/a .000
03351> + 5.0 02:W4 8.18 .260 1985.0716_14:00 281.65 n/a .000
03352> SUM= 5.0 01:BCD-PH3 34.15 1.147 1985.0716_14:00 295.85 n/a .000
03353> R0085:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RVmm-R.C.---DWFcms
03354> ADD HYD 5.0 02:W1-LID-Out 6.81 .317 1985.0716_14:00 313.70 n/a .000
03355> + 5.0 02:W2-LID-Out 8.34 .375 1985.0716_14:00 309.67 n/a .000
03356> + 5.0 02:W3-LID-Out 4.97 .186 1985.0716_14:00 265.42 n/a .000
03357> + 5.0 02:W4-LID-Out 6.45 .257 1985.0716_14:00 281.65 n/a .000
03358> SUM= 5.0 01:BCD-PH3-LI 26.56 1.134 1985.0716_14:00 295.62 n/a .000
03359> #*****
03360> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
03361> #*****
03362> # Set infiltration to 0 (CN = 99.99) for water balance analysis
03363> #*****
03364> R0085:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RVmm-R.C.---DWFcms
03365> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .413 1985.0716_14:00 392.45 .701 .000
03366> [XIMP=.66:TIMP=.71]
03367> [LOSS= 2 :CN=100.0]
03368> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03369> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
03370> [IaRECimp= 1.50: IaRECper= 6.00]
03371> [SMIN= 1.39: SMAX= 9.24: SK= .030]
03372> R0085:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RVmm-R.C.---DWFcms
03373> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .494 1985.0716_14:00 390.59 .698 .000
03374> [XIMP=.65:TIMP=.70]
03375> [LOSS= 2 :CN=100.0]
03376> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03377> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
03378> [IaRECimp= 1.50: IaRECper= 6.00]
03379> [SMIN= 1.39: SMAX= 9.24: SK= .030]
03380> R0085:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm----RVmm-R.C.---DWFcms
03381> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .291 1985.0716_14:00 377.36 .674 .000
03382> [XIMP=.53:TIMP=.63]

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03383> [LOSS= 2 :CN=100.0]
03384> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03385> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
03386> [IaREcimp= 1.50: IaRECper= 6.00]
03387> [SMIN= 1.39: SMAX= 9.24: SK= .030]
03388> R0085:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03389> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .381 1985.0716_14:00 384.89 .687 .000
03390> [XIMP=.57:TIMP=.67]
03391> [LOSS= 2 :CN=100.0]
03392> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03393> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
03394> [IaREcimp= 1.50: IaRECper= 6.00]
03395> [SMIN= 1.39: SMAX= 9.24: SK= .030]
03396> R0085:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03397> ADD HYD 5.0 02:INF-W1 8.92 .413 1985.0716_14:00 392.45 n/a .000
03398> + 5.0 02:INF-W2 10.75 .494 1985.0716_14:00 390.59 n/a .000
03399> + 5.0 02:INF-W3 6.30 .291 1985.0716_14:00 377.36 n/a .000
03400> + 5.0 02:INF-W4 8.18 .381 1985.0716_14:00 384.89 n/a .000
03401> SUM= 5.0 01:INF-BCD-PH 34.15 1.579 1985.0716_14:00 387.27 n/a .000
03402> #####
03403> # CONTINUOUS RAINFALL DATA
03404> #####
03405> ** END OF RUN : 85
03406>
03407> *****
03408>
03409>
03410>
03411>
03412>
03413> RUN#:COMMAND#
03414> R0086:C00001-----
03415> START
03416> [TZERO = .00 hrs on 19860101]
03417> [METOUT= 2 (1=imperial, 2=metric output)]
03418> [NSTORM= 0 ]
03419> [NRUN = 0086 ]
03420> #*****
03421> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
03422> #*****
03423> # Project Name: Barrhaven Conservancy Development
03424> # Project Number: 1474
03425> # Date : 2021/Oct/18
03426> # Modeller : J.Burnett, P.Eng.
03427> # Updated : 2022/Dec/13 [LP]
03428> # Company : J.F. Sabourin and Associates
03429> # License # : 2582634
03430> #*****
03431> # Ottawa International Airport (1967 - 2003)
03432> R0086:C00002-----
03433> * READ AES DATA
03434> [Filename = YOW_1967_2007.123 ]
03435> [Start_date= 1986.0101: End_date= 1986.1231]
03436> {DT= 60.min: Length= 8040.hrs: WetHrs= 520: DryHrs= 7520: PTOT= 849.40}
03437> Maximum average rainfall intensities over
03438> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03439> 18.30 17.80 13.57 7.07 4.84 2.89 2.42 1.85 1.31 mm/hr
03440> 18.30 35.60 40.70 42.40 58.10 69.30 87.00 88.60 94.40 mm
03441> 19860729 19860729 19860729 19860729 19860912 19860912 19860912 19860912 19860913 date
03442> Number of rainfall events per following interevent time
03443> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03444> 178 144 131 104 80 63 53 48 33
03445> Number of events with at least the following durations
03446> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03447> 177 104 76 24 2 0 0 0 0
03448> R0086:C00003-----
03449> COMPUTE API
03450> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
03451> {APImax=102.23: APIavg= 25.30: APImin= .17}
03452> #*****
03453> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
03454> #*****
03455> R0086:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03456> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .363 1986.0729_15:00 495.15 .583 .000
03457> [XIMP=.66:TIMP=.71]
03458> [LOSS= 2 :CN= 71.0]
03459> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03460> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
03461> [IaREcimp= 1.50: IaRECper= 6.00]
03462> [SMIN= 41.38: SMAX=275.84: SK= .030]
03463> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
03464> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
03465> # Total Volume provided by LID - 179 m³
03466> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
03467> R0086:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03468> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .363 1986.0729_15:00 495.15 n/a .000
03469> out <= 5.0 01:W1-LID 1.92 .001 1986.0119_19:30 495.17 n/a .000
03470> overflow <= 5.0 03:W1-LID-Out 7.00 .358 1986.0729_15:00 495.15 n/a .000
03471> {MxStoUsed=.1790E-01 m3, TotOvfVol=.3464E+01 m3, N-Ovf= 162, TotDurOvf= 203.hrs}

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03472> R0086:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03473> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .433 1986.0729_15:00 489.83 .577 .000
03474> [XIMP=.65:TIMP=.70]
03475> [LOSS= 2 :CN= 71.0]
03476> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03477> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
03478> [IaRECimp= 1.50: IaRECper= 6.00]
03479> [SMIN= 41.38: SMAX=275.84: SK= .030]
03480> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
03481> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
03482> # Total Volume provided by LID - 200 m³
03483> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
03484> R0086:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03485> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .433 1986.0729_15:00 489.83 n/a .000
03486> out <= 5.0 01:W2-LID 2.19 .001 1986.0119_19:20 489.82 n/a .000
03487> overflow <= 5.0 03:W2-LID-Out 8.56 .427 1986.0729_15:00 489.83 n/a .000
03488> {MxStoUsed=.2000E-01 m3, TotOvfVol=.4195E+01 m3, N-Ovf= 171, TotDurOvf= 209.hrs}
03489> R0086:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03490> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .237 1986.0729_15:00 435.04 .512 .000
03491> [XIMP=.53:TIMP=.63]
03492> [LOSS= 2 :CN= 71.0]
03493> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03494> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
03495> [IaRECimp= 1.50: IaRECper= 6.00]
03496> [SMIN= 41.38: SMAX=275.84: SK= .030]
03497> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
03498> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
03499> # Total Volume provided by LID - 96 m³
03500> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
03501> R0086:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03502> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .237 1986.0729_15:00 435.04 n/a .000
03503> out <= 5.0 01:W3-LID 1.15 .001 1986.0119_19:20 435.05 n/a .000
03504> overflow <= 5.0 03:W3-LID-Out 5.15 .232 1986.0729_15:00 435.04 n/a .000
03505> {MxStoUsed=.9598E-02 m3, TotOvfVol=.2240E+01 m3, N-Ovf= 170, TotDurOvf= 215.hrs}
03506> R0086:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03507> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .318 1986.0729_15:00 456.50 .537 .000
03508> [XIMP=.57:TIMP=.67]
03509> [LOSS= 2 :CN= 71.0]
03510> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03511> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
03512> [IaRECimp= 1.50: IaRECper= 6.00]
03513> [SMIN= 41.38: SMAX=275.84: SK= .030]
03514> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
03515> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
03516> # Total Volume provided by LID - 131 m³
03517> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
03518> R0086:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03519> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .318 1986.0729_15:00 456.50 n/a .000
03520> out <= 5.0 01:W4-LID 1.52 .001 1986.0119_19:15 456.51 n/a .000
03521> overflow <= 5.0 03:W4-LID-Out 6.66 .312 1986.0729_15:00 456.50 n/a .000
03522> {MxStoUsed=.1310E-01 m3, TotOvfVol=.3040E+01 m3, N-Ovf= 163, TotDurOvf= 215.hrs}
03523> R0086:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03524> ADD HYD 5.0 02:W1 8.92 .363 1986.0729_15:00 495.15 n/a .000
03525> + 5.0 02:W2 10.75 .433 1986.0729_15:00 489.83 n/a .000
03526> + 5.0 02:W3 6.30 .237 1986.0729_15:00 435.04 n/a .000
03527> + 5.0 02:W4 8.18 .318 1986.0729_15:00 456.50 n/a .000
03528> SUM= 5.0 01:BCD-PH3 34.15 1.350 1986.0729_15:00 473.13 n/a .000
03529> R0086:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03530> ADD HYD 5.0 02:W1-LID-Out 7.00 .358 1986.0729_15:00 495.15 n/a .000
03531> + 5.0 02:W2-LID-Out 8.56 .427 1986.0729_15:00 489.83 n/a .000
03532> + 5.0 02:W3-LID-Out 5.15 .232 1986.0729_15:00 435.04 n/a .000
03533> + 5.0 02:W4-LID-Out 6.66 .312 1986.0729_15:00 456.50 n/a .000
03534> SUM= 5.0 01:BCD-PH3-LI 27.37 1.330 1986.0729_15:00 472.78 n/a .000
03535> #*****
03536> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
03537> #*****
03538> # Set infiltration to 0 (CN = 99.99) for water balance analysis
03539> #*****
03540> R0086:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03541> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .450 1986.0729_15:00 595.87 .702 .000
03542> [XIMP=.66:TIMP=.71]
03543> [LOSS= 2 :CN=100.0]
03544> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03545> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
03546> [IaRECimp= 1.50: IaRECper= 6.00]
03547> [SMIN= 1.39: SMAX= 9.24: SK= .030]
03548> R0086:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03549> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .541 1986.0729_15:00 593.35 .699 .000
03550> [XIMP=.65:TIMP=.70]
03551> [LOSS= 2 :CN=100.0]
03552> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03553> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
03554> [IaRECimp= 1.50: IaRECper= 6.00]
03555> [SMIN= 1.39: SMAX= 9.24: SK= .030]
03556> R0086:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03557> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .319 1986.0729_15:00 577.26 .680 .000
03558> [XIMP=.53:TIMP=.63]
03559> [LOSS= 2 :CN=100.0]
03560> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]

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03561> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
03562> [IaREcimp= 1.50: IaREcper= 6.00]
03563> [SMIN= 1.39: SMAX= 9.24: SK= .030]
03564> R0086:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
03565> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .413 1986.0729_15:00 587.46 .692 .000
03566> [XIMP=.57:TIMP=.67]
03567> [LOSS= 2 :CN=100.0]
03568> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03569> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
03570> [IaREcimp= 1.50: IaREcper= 6.00]
03571> [SMIN= 1.39: SMAX= 9.24: SK= .030]
03572> R0086:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
03573> ADD HYD 5.0 02:INF-W1 8.92 .450 1986.0729_15:00 595.87 n/a .000
03574> + 5.0 02:INF-W2 10.75 .541 1986.0729_15:00 593.35 n/a .000
03575> + 5.0 02:INF-W3 6.30 .319 1986.0729_15:00 577.26 n/a .000
03576> + 5.0 02:INF-W4 8.18 .413 1986.0729_15:00 587.46 n/a .000
03577> SUM= 5.0 01:INF-BCD-PH 34.15 1.722 1986.0729_15:00 589.63 n/a .000
03578> #####
03579> # CONTINUOUS RAINFALL DATA
03580> #####
03581> ** END OF RUN : 86
03582>
03583> *****
03584>
03585>
03586>
03587>
03588>
03589> RUN#:COMMAND#
03590> R0087:C00001-----
03591> START
03592> [TZERO = .00 hrs on 19870101]
03593> [METOUT= 2 (1=imperial, 2=metric output)]
03594> [NSTORM= 0 ]
03595> [NRUN = 0087 ]
03596> #*****
03597> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
03598> #*****
03599> # Project Name: Barrhaven Conservancy Development
03600> # Project Number: 1474
03601> # Date : 2021/Oct/18
03602> # Modeller : J.Burnett, P.Eng.
03603> # Updated : 2022/Dec/13 [LP]
03604> # Company : J.F. Sabourin and Associates
03605> # License # : 2582634
03606> #*****
03607> # Ottawa International Airport (1967 - 2003)
03608> R0087:C00002-----
03609> * READ AES DATA
03610> [Filename = YOW_1967_2007.123 ]
03611> [Start_date= 1987.0101: End_date= 1987.1231]
03612> {DT= 60.min: Length= 7344.hrs: WetHrs= 492: DryHrs= 6852: PTOT= 640.10}
03613> Maximum average rainfall intensities over
03614> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03615> 20.00 13.90 14.03 7.05 4.87 2.46 1.84 1.40 .93 mm/hr
03616> 20.00 27.80 42.10 42.30 58.40 59.00 66.40 67.00 67.00 mm
03617> 19870724 19870724 19870724 19870724 19870724 19870725 19870726 19870726 date
03618> Number of rainfall events per following interevent time
03619> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03620> 180 147 128 93 74 55 49 41 28
03621> Number of events with at least the following durations
03622> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03623> 179 94 60 20 3 0 0 0 0
03624> R0087:C00003-----
03625> COMPUTE API
03626> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
03627> {APImax= 75.76: APIavg= 21.41: APImin= 1.18}
03628> #*****
03629> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
03630> #*****
03631> R0087:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
03632> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .339 1987.0724_13:00 332.97 .520 .000
03633> [XIMP=.66:TIMP=.71]
03634> [LOSS= 2 :CN= 71.0]
03635> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03636> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
03637> [IaREcimp= 1.50: IaREcper= 6.00]
03638> [SMIN= 41.38: SMAX=275.84: SK= .030]
03639> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
03640> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
03641> # Total Volume provided by LID - 179 m³
03642> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
03643> R0087:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
03644> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .339 1987.0724_13:00 332.97 n/a .000
03645> out <= 5.0 01:W1-LID 2.53 .001 1987.0326_15:50 332.97 n/a .000
03646> overflow <= 5.0 03:W1-LID-Out 6.39 .335 1987.0724_13:00 332.97 n/a .000
03647> {MxStoUsed=.1790E-01 m3, TotOvfVol=.2126E+01 m3, N-Ovf= 124, TotDurOvf= 159.hrs}
03648> R0087:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
03649> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .402 1987.0724_13:00 328.89 .514 .000

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03650> [XIMP=.65:TIMP=.70]
03651> [LOSS= 2 :CN= 71.0]
03652> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03653> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
03654> [IaREcimp= 1.50: IaRECper= 6.00]
03655> [SMIN= 41.38: SMAX=275.84: SK= .030]
03656> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
03657> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
03658> # Total Volume provided by LID - 200 m³
03659> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
03660> R0087:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03661> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .402 1987.0724_13:00 328.89 n/a .000
03662> out <= 5.0 01:W2-LID 2.88 .001 1987.0326_15:10 328.89 n/a .000
03663> overflow <= 5.0 03:W2-LID-Out 7.87 .397 1987.0724_13:00 328.89 n/a .000
03664> {MxStoUsed=.2000E-01 m3, TotOvfVol=.2588E+01 m3, N-Ovf= 127, TotDurOvf= 165.hrs}
03665> R0087:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03666> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .201 1987.0724_13:00 285.09 .445 .000
03667> [XIMP=.53:TIMP=.63]
03668> [LOSS= 2 :CN= 71.0]
03669> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03670> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
03671> [IaREcimp= 1.50: IaRECper= 6.00]
03672> [SMIN= 41.38: SMAX=275.84: SK= .030]
03673> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
03674> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
03675> # Total Volume provided by LID - 96 m³
03676> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
03677> R0087:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03678> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .201 1987.0724_13:00 285.09 n/a .000
03679> out <= 5.0 01:W3-LID 1.56 .001 1987.0326_15:05 285.10 n/a .000
03680> overflow <= 5.0 03:W3-LID-Out 4.74 .198 1987.0724_13:00 285.09 n/a .000
03681> {MxStoUsed=.9598E-02 m3, TotOvfVol=.1352E+01 m3, N-Ovf= 141, TotDurOvf= 169.hrs}
03682> R0087:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03683> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .277 1987.0724_13:00 301.51 .471 .000
03684> [XIMP=.57:TIMP=.67]
03685> [LOSS= 2 :CN= 71.0]
03686> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03687> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
03688> [IaREcimp= 1.50: IaRECper= 6.00]
03689> [SMIN= 41.38: SMAX=275.84: SK= .030]
03690> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
03691> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
03692> # Total Volume provided by LID - 131 m³
03693> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
03694> R0087:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03695> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .277 1987.0724_13:00 301.51 n/a .000
03696> out <= 5.0 01:W4-LID 2.04 .001 1987.0326_15:00 301.51 n/a .000
03697> overflow <= 5.0 03:W4-LID-Out 6.14 .273 1987.0724_13:00 301.51 n/a .000
03698> {MxStoUsed=.1309E-01 m3, TotOvfVol=.1852E+01 m3, N-Ovf= 134, TotDurOvf= 170.hrs}
03699> R0087:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03700> ADD HYD 5.0 02:W1 8.92 .339 1987.0724_13:00 332.97 n/a .000
03701> + 5.0 02:W2 10.75 .402 1987.0724_13:00 328.89 n/a .000
03702> + 5.0 02:W3 6.30 .201 1987.0724_13:00 285.09 n/a .000
03703> + 5.0 02:W4 8.18 .277 1987.0724_13:00 301.51 n/a .000
03704> SUM= 5.0 01:BCD-PH3 34.15 1.219 1987.0724_13:00 315.32 n/a .000
03705> R0087:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03706> ADD HYD 5.0 02:W1-LID-Out 6.39 .335 1987.0724_13:00 332.97 n/a .000
03707> + 5.0 02:W2-LID-Out 7.87 .397 1987.0724_13:00 328.89 n/a .000
03708> + 5.0 02:W3-LID-Out 4.74 .198 1987.0724_13:00 285.09 n/a .000
03709> + 5.0 02:W4-LID-Out 6.14 .273 1987.0724_13:00 301.51 n/a .000
03710> SUM= 5.0 01:BCD-PH3-LI 25.14 1.203 1987.0724_13:00 314.98 n/a .000
03711> #*****
03712> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
03713> #*****
03714> # Set infiltration to 0 (CN = 99.99) for water balance analysis
03715> #*****
03716> R0087:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03717> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .434 1987.0724_13:00 399.53 .624 .000
03718> [XIMP=.66:TIMP=.71]
03719> [LOSS= 2 :CN=100.0]
03720> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03721> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
03722> [IaREcimp= 1.50: IaRECper= 6.00]
03723> [SMIN= 1.39: SMAX= 9.24: SK= .030]
03724> R0087:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03725> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .518 1987.0724_13:00 397.23 .621 .000
03726> [XIMP=.65:TIMP=.70]
03727> [LOSS= 2 :CN=100.0]
03728> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03729> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
03730> [IaREcimp= 1.50: IaRECper= 6.00]
03731> [SMIN= 1.39: SMAX= 9.24: SK= .030]
03732> R0087:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03733> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .305 1987.0724_13:00 381.20 .596 .000
03734> [XIMP=.53:TIMP=.63]
03735> [LOSS= 2 :CN=100.0]
03736> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03737> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
03738> [IaREcimp= 1.50: IaRECper= 6.00]

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03739> [SMIN= 1.39: SMAX= 9.24: SK= .030]
03740> R0087:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03741> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .400 1987.0724_13:00 390.61 .610 .000
03742> [XIMP=.57:TIMP=.67]
03743> [LOSS= 2 :CN=100.0]
03744> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03745> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
03746> [IaRECimp= 1.50: IaRECper= 6.00]
03747> [SMIN= 1.39: SMAX= 9.24: SK= .030]
03748> R0087:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03749> ADD HYD 5.0 02:INF-W1 8.92 .434 1987.0724_13:00 399.53 n/a .000
03750> + 5.0 02:INF-W2 10.75 .518 1987.0724_13:00 397.23 n/a .000
03751> + 5.0 02:INF-W3 6.30 .305 1987.0724_13:00 381.20 n/a .000
03752> + 5.0 02:INF-W4 8.18 .400 1987.0724_13:00 390.61 n/a .000
03753> SUM= 5.0 01:INF-BCD-PH 34.15 1.657 1987.0724_13:00 393.29 n/a .000
03754> #####
03755> # CONTINUOUS RAINFALL DATA
03756> #####
03757> ** END OF RUN : 87
03758>
03759> *****
03760>
03761>
03762>
03763>
03764>
03765> RUN#:COMMAND#
03766> R0088:C00001-----
03767> START
03768> [TZERO = .00 hrs on 19880101]
03769> [METOUT= 2 (1=imperial, 2=metric output)]
03770> [NSTORM= 0 ]
03771> [NRUN = 0088 ]
03772> #*****
03773> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
03774> #*****
03775> # Project Name: Barrhaven Conservancy Development
03776> # Project Number: 1474
03777> # Date : 2021/Oct/18
03778> # Modeller : J.Burnett, P.Eng.
03779> # Updated : 2022/Dec/13 [LP]
03780> # Company : J.F. Sabourin and Associates
03781> # License # : 2582634
03782> #*****
03783> # Ottawa International Airport (1967 - 2003)
03784> R0088:C00002-----
03785> * READ AES DATA
03786> [Filename = YOW_1967_2007.123 ]
03787> [Start_date= 1988.0101: End_date= 1988.1230]
03788> [DT= 60.min: Length= 8760.hrs: WetHrs= 487: DryHrs= 8273: PTOT= 643.80]
03789> Maximum average rainfall intensities over
03790> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03791> 25.50 18.20 12.77 7.37 3.78 1.91 1.27 .95 .94 mm/hr
03792> 25.50 36.40 38.30 44.20 45.40 45.80 45.80 45.80 67.40 mm
03793> 19880917 19880726 19880625 19880625 19880625 19880625 19880625 19880626 19880625 date
03794> Number of rainfall events per following interevent time
03795> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03796> 165 130 109 80 66 56 49 42 26
03797> Number of events with at least the following durations
03798> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03799> 164 102 71 20 5 0 0 0 0
03800> R0088:C00003-----
03801> COMPUTE API
03802> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
03803> [APImax= 66.04: APIavg= 18.06: APImin= .03]
03804> #*****
03805> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
03806> #*****
03807> R0088:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03808> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .444 1988.0726_13:00 334.51 .520 .000
03809> [XIMP=.66:TIMP=.71]
03810> [LOSS= 2 :CN= 71.0]
03811> [Pervious out area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03812> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
03813> [IaRECimp= 1.50: IaRECper= 6.00]
03814> [SMIN= 41.38: SMAX=275.84: SK= .030]
03815> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
03816> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
03817> # Total Volume provided by LID - 179 m3
03818> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
03819> R0088:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03820> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .444 1988.0726_13:00 334.51 n/a .000
03821> out <= 5.0 01:W1-LID 2.53 .001 1988.0117_22:50 334.52 n/a .000
03822> overflow <= 5.0 03:W1-LID-Out 6.39 .438 1988.0726_13:00 334.51 n/a .000
03823> {MxStoUsed=.1789E-01 m3, TotOvfVol=.2136E+01 m3, N-Ovf= 121, TotDurOvf= 161.hrs}
03824> R0088:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03825> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .527 1988.0726_13:00 330.37 .513 .000
03826> [XIMP=.65:TIMP=.70]
03827> [LOSS= 2 :CN= 71.0]

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03828> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03829> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
03830> [IaRECImp= 1.50: IaRECper= 6.00]
03831> [SMIN= 41.38: SMAX=275.84: SK= .030]
03832> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
03833> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
03834> # Total Volume provided by LID - 200 m³
03835> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
03836> R0088:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
03837> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .527 1988.0726_13:00 330.37 n/a .000
03838> out <= 5.0 01:W2-LID 2.88 .001 1988.0117_22:35 330.37 n/a .000
03839> overflow <= 5.0 03:W2-LID-Out 7.87 .519 1988.0726_13:00 330.37 n/a .000
03840> {MxStoUsed=.2000E-01 m3, TotOvfVol=.2599E+01 m3, N-Ovf= 130, TotDurOvf= 168.hrs}
03841> R0088:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
03842> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .274 1988.0726_13:00 285.65 .444 .000
03843> [XIMP=.53:TIMP=.63]
03844> [LOSS= 2 :CN= 71.0]
03845> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03846> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
03847> [IaRECImp= 1.50: IaRECper= 6.00]
03848> [SMIN= 41.38: SMAX=275.84: SK= .030]
03849> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
03850> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
03851> # Total Volume provided by LID - 96 m³
03852> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
03853> R0088:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
03854> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .274 1988.0726_13:00 285.65 n/a .000
03855> out <= 5.0 01:W3-LID 1.56 .001 1988.0117_22:30 285.66 n/a .000
03856> overflow <= 5.0 03:W3-LID-Out 4.74 .268 1988.0726_13:00 285.65 n/a .000
03857> {MxStoUsed=.9595E-02 m3, TotOvfVol=.1353E+01 m3, N-Ovf= 127, TotDurOvf= 170.hrs}
03858> R0088:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
03859> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .375 1988.0726_13:00 302.40 .470 .000
03860> [XIMP=.57:TIMP=.67]
03861> [LOSS= 2 :CN= 71.0]
03862> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03863> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
03864> [IaRECImp= 1.50: IaRECper= 6.00]
03865> [SMIN= 41.38: SMAX=275.84: SK= .030]
03866> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
03867> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
03868> # Total Volume provided by LID - 131 m³
03869> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
03870> R0088:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
03871> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .375 1988.0726_13:00 302.40 n/a .000
03872> out <= 5.0 01:W4-LID 2.04 .001 1988.0117_22:30 302.40 n/a .000
03873> overflow <= 5.0 03:W4-LID-Out 6.14 .367 1988.0726_13:00 302.40 n/a .000
03874> {MxStoUsed=.1308E-01 m3, TotOvfVol=.1855E+01 m3, N-Ovf= 122, TotDurOvf= 170.hrs}
03875> R0088:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
03876> ADD HYD 5.0 02:W1 8.92 .444 1988.0726_13:00 334.51 n/a .000
03877> + 5.0 02:W2 10.75 .527 1988.0726_13:00 330.37 n/a .000
03878> + 5.0 02:W3 6.30 .274 1988.0726_13:00 285.65 n/a .000
03879> + 5.0 02:W4 8.18 .375 1988.0726_13:00 302.40 n/a .000
03880> SUM= 5.0 01:BCD-PH3 34.15 1.619 1988.0726_13:00 316.50 n/a .000
03881> R0088:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
03882> ADD HYD 5.0 02:W1-LID-Out 6.39 .438 1988.0726_13:00 334.51 n/a .000
03883> + 5.0 02:W2-LID-Out 7.87 .519 1988.0726_13:00 330.37 n/a .000
03884> + 5.0 02:W3-LID-Out 4.74 .268 1988.0726_13:00 285.65 n/a .000
03885> + 5.0 02:W4-LID-Out 6.14 .367 1988.0726_13:00 302.40 n/a .000
03886> SUM= 5.0 01:BCD-PH3-LI 25.13 1.591 1988.0726_13:00 316.16 n/a .000
03887> #*****
03888> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
03889> #*****
03890> # Set infiltration to 0 (CN = 99.99) for water balance analysis
03891> #*****
03892> R0088:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
03893> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .583 1988.0726_13:00 406.13 .631 .000
03894> [XIMP=.66:TIMP=.71]
03895> [LOSS= 2 :CN=100.0]
03896> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03897> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
03898> [IaRECImp= 1.50: IaRECper= 6.00]
03899> [SMIN= 1.39: SMAX= 9.24: SK= .030]
03900> R0088:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
03901> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .698 1988.0726_13:00 403.95 .627 .000
03902> [XIMP=.65:TIMP=.70]
03903> [LOSS= 2 :CN=100.0]
03904> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03905> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
03906> [IaRECImp= 1.50: IaRECper= 6.00]
03907> [SMIN= 1.39: SMAX= 9.24: SK= .030]
03908> R0088:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
03909> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .407 1988.0726_13:00 388.00 .603 .000
03910> [XIMP=.53:TIMP=.63]
03911> [LOSS= 2 :CN=100.0]
03912> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03913> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
03914> [IaRECImp= 1.50: IaRECper= 6.00]
03915> [SMIN= 1.39: SMAX= 9.24: SK= .030]
03916> R0088:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms

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03917> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .531 1988.0726_13:00 396.98 .617 .000
03918> [XIMP=.57:TIMP=.67]
03919> [LOSS= 2 :CN=100.0]
03920> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03921> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
03922> [IaRECImp= 1.50: IaRECper= 6.00]
03923> [SMIN= 1.39: SMAX= 9.24: SK= .030]
03924> R0088:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03925> ADD HYD 5.0 02:INF-W1 8.92 .583 1988.0726_13:00 406.13 n/a .000
03926> + 5.0 02:INF-W2 10.75 .698 1988.0726_13:00 403.95 n/a .000
03927> + 5.0 02:INF-W3 6.30 .407 1988.0726_13:00 388.00 n/a .000
03928> + 5.0 02:INF-W4 8.18 .531 1988.0726_13:00 396.98 n/a .000
03929> SUM= 5.0 01:INF-BCD-PH 34.15 2.219 1988.0726_13:00 399.91 n/a .000
03930> #####
03931> # CONTINUOUS RAINFALL DATA
03932> #####
03933> ** END OF RUN : 88
03934>
03935> *****
03936>
03937>
03938>
03939>
03940>
03941> RUN#:COMMAND#
03942> R0089:C00001-----
03943> START
03944> [TZERO = .00 hrs on 19890101]
03945> [METOUT= 2 (1=imperial, 2=metric output)]
03946> [NSTORM= 0 ]
03947> [NRUN = 0089 ]
03948> #*****
03949> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
03950> #*****
03951> # Project Name: Barrhaven Conservancy Development
03952> # Project Number: 1474
03953> # Date : 2021/Oct/18
03954> # Modeller : J.Burnett, P.Eng.
03955> # Updated : 2022/Dec/13 [LP]
03956> # Company : J.F. Sabourin and Associates
03957> # License # : 2582634
03958> #*****
03959> # Ottawa International Airport (1967 - 2003)
03960> R0089:C00002-----
03961> * READ AES DATA
03962> [Filename = YOW_1967_2007.123 ]
03963> [Start_date= 1989.0101: End_date= 1989.1231]
03964> [DT= 60.min: Length= 8040.hrs: WetHrs= 422: DryHrs= 7618: PTOT= 523.20]
03965> Maximum average rainfall intensities over
03966> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03967> 22.70 12.60 8.93 5.75 3.03 1.69 1.14 .86 .59 mm/hr
03968> 22.70 25.20 26.80 34.50 36.30 40.60 40.90 41.30 42.50 mm
03969> 19890727 19890727 19890727 19890727 19890727 19891020 19891021 19891021 19891022 date
03970> Number of rainfall events per following interevent time
03971> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03972> 151 125 108 89 67 53 42 37 29
03973> Number of events with at least the following durations
03974> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
03975> 150 81 52 19 5 0 0 0 0
03976> R0089:C00003-----
03977> COMPUTE API
03978> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
03979> [APImax= 55.10: APIavg= 16.03: APImin= .02]
03980> #*****
03981> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
03982> #*****
03983> R0089:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03984> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .401 1989.0727_15:00 267.84 .512 .000
03985> [XIMP=.66:TIMP=.71]
03986> [LOSS= 2 :CN= 71.0]
03987> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
03988> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
03989> [IaRECImp= 1.50: IaRECper= 6.00]
03990> [SMIN= 41.38: SMAX=275.84: SK= .030]
03991> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
03992> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
03993> # Total Volume provided by LID - 179 m3
03994> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
03995> R0089:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
03996> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .401 1989.0727_15:00 267.84 n/a .000
03997> out <= 5.0 01:W1-LID 2.58 .001 1989.0325_13:35 267.84 n/a .000
03998> overflow <= 5.0 03:W1-LID-Out 6.34 .395 1989.0727_15:00 267.84 n/a .000
03999> [MxStoUsed=.1790E-01 m3, TotOvfVol=.1699E+01 m3, N-Ovf= 95, TotDurOvf= 152.hrs]
04000> R0089:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04001> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .472 1989.0727_15:00 264.35 .505 .000
04002> [XIMP=.65:TIMP=.70]
04003> [LOSS= 2 :CN= 71.0]
04004> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04005> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]

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04006> [IaREcImp= 1.50: IaRECper= 6.00]
04007> [SMIN= 41.38: SMAX=275.84: SK= .030]
04008> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
04009> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04010> # Total Volume provided by LID - 200 m³
04011> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04012> R0089:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04013> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .472 1989.0727_15:00 264.35 n/a .000
04014> out <= 5.0 01:W2-LID 2.95 .001 1989.0325_13:25 264.35 n/a .000
04015> overflow <= 5.0 03:W2-LID-Out 7.80 .466 1989.0727_15:00 264.35 n/a .000
04016> {MxStoUsed=.1999E-01 m3, TotOvfVol=.2063E+01 m3, N-Ovf= 94, TotDurOvf= 157.hrs}
04017> R0089:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04018> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .245 1989.0727_15:00 226.07 .432 .000
04019> [XIMP=.53:TIMP=.63]
04020> [LOSS= 2 :CN= 71.0]
04021> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04022> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
04023> [IaREcImp= 1.50: IaRECper= 6.00]
04024> [SMIN= 41.38: SMAX=275.84: SK= .030]
04025> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
04026> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04027> # Total Volume provided by LID - 96 m³
04028> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04029> R0089:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04030> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .245 1989.0727_15:00 226.07 n/a .000
04031> out <= 5.0 01:W3-LID 1.62 .001 1989.0325_13:25 226.07 n/a .000
04032> overflow <= 5.0 03:W3-LID-Out 4.68 .240 1989.0727_15:00 226.07 n/a .000
04033> {MxStoUsed=.9599E-02 m3, TotOvfVol=.1059E+01 m3, N-Ovf= 97, TotDurOvf= 158.hrs}
04034> R0089:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04035> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .335 1989.0727_15:00 240.09 .459 .000
04036> [XIMP=.57:TIMP=.67]
04037> [LOSS= 2 :CN= 71.0]
04038> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04039> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
04040> [IaREcImp= 1.50: IaRECper= 6.00]
04041> [SMIN= 41.38: SMAX=275.84: SK= .030]
04042> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
04043> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04044> # Total Volume provided by LID - 131 m³
04045> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04046> R0089:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04047> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .335 1989.0727_15:00 240.09 n/a .000
04048> out <= 5.0 01:W4-LID 2.11 .001 1989.0325_13:25 240.09 n/a .000
04049> overflow <= 5.0 03:W4-LID-Out 6.07 .328 1989.0727_15:00 240.09 n/a .000
04050> {MxStoUsed=.1310E-01 m3, TotOvfVol=.1458E+01 m3, N-Ovf= 108, TotDurOvf= 159.hrs}
04051> R0089:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04052> ADD HYD 5.0 02:W1 8.92 .401 1989.0727_15:00 267.84 n/a .000
04053> + 5.0 02:W2 10.75 .472 1989.0727_15:00 264.35 n/a .000
04054> + 5.0 02:W3 6.30 .245 1989.0727_15:00 226.07 n/a .000
04055> + 5.0 02:W4 8.18 .335 1989.0727_15:00 240.09 n/a .000
04056> SUM= 5.0 01:BCD-PH3 34.15 1.452 1989.0727_15:00 252.39 n/a .000
04057> R0089:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04058> ADD HYD 5.0 02:W1-LID-Out 6.34 .395 1989.0727_15:00 267.84 n/a .000
04059> + 5.0 02:W2-LID-Out 7.80 .466 1989.0727_15:00 264.35 n/a .000
04060> + 5.0 02:W3-LID-Out 4.68 .240 1989.0727_15:00 226.07 n/a .000
04061> + 5.0 02:W4-LID-Out 6.07 .328 1989.0727_15:00 240.09 n/a .000
04062> SUM= 5.0 01:BCD-PH3-LI 24.90 1.429 1989.0727_15:00 252.12 n/a .000
04063> #*****
04064> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
04065> #*****
04066> # Set infiltration to 0 (CN = 99.99) for water balance analysis
04067> #*****
04068> R0089:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04069> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .535 1989.0727_15:00 328.10 .627 .000
04070> [XIMP=.66:TIMP=.71]
04071> [LOSS= 2 :CN=100.0]
04072> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04073> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
04074> [IaREcImp= 1.50: IaRECper= 6.00]
04075> [SMIN= 1.39: SMAX= 9.24: SK= .030]
04076> R0089:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04077> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .642 1989.0727_15:00 326.22 .624 .000
04078> [XIMP=.65:TIMP=.70]
04079> [LOSS= 2 :CN=100.0]
04080> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04081> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
04082> [IaREcImp= 1.50: IaRECper= 6.00]
04083> [SMIN= 1.39: SMAX= 9.24: SK= .030]
04084> R0089:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04085> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .376 1989.0727_15:00 312.77 .598 .000
04086> [XIMP=.53:TIMP=.63]
04087> [LOSS= 2 :CN=100.0]
04088> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04089> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
04090> [IaREcImp= 1.50: IaRECper= 6.00]
04091> [SMIN= 1.39: SMAX= 9.24: SK= .030]
04092> R0089:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04093> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .489 1989.0727_15:00 320.35 .612 .000
04094> [XIMP=.57:TIMP=.67]

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04095> [LOSS= 2 :CN=100.0]
04096> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04097> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
04098> [IaRECImp= 1.50: IaRECper= 6.00]
04099> [SMIN= 1.39: SMAX= 9.24: SK= .030]
04100> R0089:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04101> ADD HYD 5.0 02:INF-W1 8.92 .535 1989.0727_15:00 328.10 n/a .000
04102> + 5.0 02:INF-W2 10.75 .642 1989.0727_15:00 326.22 n/a .000
04103> + 5.0 02:INF-W3 6.30 .376 1989.0727_15:00 312.76 n/a .000
04104> + 5.0 02:INF-W4 8.18 .489 1989.0727_15:00 320.35 n/a .000
04105> SUM= 5.0 01:INF-BCD-PH 34.15 2.043 1989.0727_15:00 322.82 n/a .000
04106> #####
04107> # CONTINUOUS RAINFALL DATA
04108> #####
04109> ** END OF RUN : 89
04110>
04111> *****
04112>
04113>
04114>
04115>
04116>
04117> RUN#:COMMAND#
04118> R0090:C00001-----
04119> START
04120> [TZERO = .00 hrs on 19900101]
04121> [METOUT= 2 (1=imperial, 2=metric output)]
04122> [NSTORM= 0 ]
04123> [NRUN = 0090 ]
04124> #*****
04125> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
04126> #*****
04127> # Project Name: Barrhaven Conservancy Development
04128> # Project Number: 1474
04129> # Date : 2021/Oct/18
04130> # Modeller : J.Burnett, P.Eng.
04131> # Updated : 2022/Dec/13 [LP]
04132> # Company : J.F. Sabourin and Associates
04133> # License # : 2582634
04134> #*****
04135> # Ottawa International Airport (1967 - 2003)
04136> R0090:C00002-----
04137> * READ AES DATA
04138> [Filename = YOW_1967_2007.123 ]
04139> [Start_date= 1990.0101: End_date= 1990.1231]
04140> [DT= 60.min: Length= 7344.hrs: WetHrs= 618: DryHrs= 6726: PTOT= 727.80]
04141> Maximum average rainfall intensities over
04142> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
04143> 20.60 12.25 9.60 5.58 4.43 2.25 1.50 1.23 1.06 mm/hr
04144> 20.60 24.50 28.80 33.50 53.20 54.00 54.00 59.00 76.60 mm
04145> 19900720 19900720 19900828 19900828 19900720 19900720 19900720 19900722 19900723 date
04146> Number of rainfall events per following interevent time
04147> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
04148> 204 156 141 107 84 66 56 47 33
04149> Number of events with at least the following durations
04150> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
04151> 203 116 75 31 6 1 0 0 0
04152> R0090:C00003-----
04153> COMPUTE API
04154> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
04155> [APImax= 75.10: APIavg= 23.47: APImin= 3.10]
04156> #*****
04157> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
04158> #*****
04159> R0090:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04160> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .359 1990.0720_ 5:00 387.16 .532 .000
04161> [XIMP=.66:TIMP=.71]
04162> [LOSS= 2 :CN= 71.0]
04163> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04164> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
04165> [IaRECImp= 1.50: IaRECper= 6.00]
04166> [SMIN= 41.38: SMAX=275.84: SK= .030]
04167> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
04168> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04169> # Total Volume provided by LID - 179 m³
04170> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04171> R0090:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04172> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .359 1990.0720_ 5:00 387.16 n/a .000
04173> out <= 5.0 01:W1-LID 2.33 .001 1990.0312_17:15 387.18 n/a .000
04174> overflow <= 5.0 03:W1-LID-Out 6.59 .355 1990.0720_ 5:00 387.16 n/a .000
04175> [MxStoUsed=.1789E-01 m3, TotOvfVol=.2550E+01 m3, N-Ovf= 130, TotDurOvf= 225.hrs]
04176> R0090:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04177> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .427 1990.0720_ 5:00 382.52 .526 .000
04178> [XIMP=.65:TIMP=.70]
04179> [LOSS= 2 :CN= 71.0]
04180> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04181> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
04182> [IaRECImp= 1.50: IaRECper= 6.00]
04183> [SMIN= 41.38: SMAX=275.84: SK= .030]

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04184> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
04185> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04186> # Total Volume provided by LID - 200 m³
04187> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04188> R0090:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04189> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .427 1990.0720_ 5:00 382.52 n/a .000
04190> out <= 5.0 01:W2-LID 2.65 .001 1990.0312_17:10 382.51 n/a .000
04191> overflow <= 5.0 03:W2-LID-Out 8.10 .422 1990.0720_ 5:00 382.52 n/a .000
04192> {MxStoUsed=.1999E-01 m3, TotOvfVol=.3097E+01 m3, N-Ovf= 122, TotDurOvf= 231.hrs}
04193> R0090:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04194> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .217 1990.0720_ 5:00 332.93 .457 .000
04195> [XIMP=.53:TIMP=.63]
04196> [LOSS= 2 :CN= 71.0]
04197> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04198> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
04199> [IaRECimp= 1.50: IaRECper= 6.00]
04200> [SMIN= 41.38: SMAX=275.84: SK= .030]
04201> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
04202> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04203> # Total Volume provided by LID - 96 m³
04204> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04205> R0090:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04206> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .217 1990.0720_ 5:00 332.93 n/a .000
04207> out <= 5.0 01:W3-LID 1.43 .001 1990.0312_17:10 332.94 n/a .000
04208> overflow <= 5.0 03:W3-LID-Out 4.87 .213 1990.0720_ 5:00 332.93 n/a .000
04209> {MxStoUsed=.9597E-02 m3, TotOvfVol=.1621E+01 m3, N-Ovf= 121, TotDurOvf= 234.hrs}
04210> R0090:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04211> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .298 1990.0720_ 5:00 351.63 .483 .000
04212> [XIMP=.57:TIMP=.67]
04213> [LOSS= 2 :CN= 71.0]
04214> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04215> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
04216> [IaRECimp= 1.50: IaRECper= 6.00]
04217> [SMIN= 41.38: SMAX=275.84: SK= .030]
04218> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
04219> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04220> # Total Volume provided by LID - 131 m³
04221> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04222> R0090:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04223> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .298 1990.0720_ 5:00 351.63 n/a .000
04224> out <= 5.0 01:W4-LID 1.88 .001 1990.0312_17:10 351.64 n/a .000
04225> overflow <= 5.0 03:W4-LID-Out 6.30 .293 1990.0720_ 5:00 351.63 n/a .000
04226> {MxStoUsed=.1309E-01 m3, TotOvfVol=.2217E+01 m3, N-Ovf= 124, TotDurOvf= 234.hrs}
04227> R0090:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04228> ADD HYD 5.0 02:W1 3.59 1990.0720_ 5:00 387.16 n/a .000
04229> + 5.0 02:W2 10.75 .427 1990.0720_ 5:00 382.52 n/a .000
04230> + 5.0 02:W3 6.30 .217 1990.0720_ 5:00 332.93 n/a .000
04231> + 5.0 02:W4 8.18 .298 1990.0720_ 5:00 351.63 n/a .000
04232> SUM= 5.0 01:BCD-PH3 34.15 1.300 1990.0720_ 5:00 367.19 n/a .000
04233> R0090:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04234> ADD HYD 5.0 02:W1-LID-Out 6.59 .355 1990.0720_ 5:00 387.16 n/a .000
04235> + 5.0 02:W2-LID-Out 8.10 .422 1990.0720_ 5:00 382.52 n/a .000
04236> + 5.0 02:W3-LID-Out 4.87 .213 1990.0720_ 5:00 332.93 n/a .000
04237> + 5.0 02:W4-LID-Out 6.30 .293 1990.0720_ 5:00 351.63 n/a .000
04238> SUM= 5.0 01:BCD-PH3-LI 25.85 1.283 1990.0720_ 5:00 366.83 n/a .000
04239> #*****
04240> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIR
04241> #*****
04242> # Set infiltration to 0 (CN = 99.99) for water balance analysis
04243> #*****
04244> R0090:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04245> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .482 1990.0720_ 5:00 472.43 .649 .000
04246> [XIMP=.66:TIMP=.71]
04247> [LOSS= 2 :CN=100.0]
04248> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04249> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
04250> [IaRECimp= 1.50: IaRECper= 6.00]
04251> [SMIN= 1.39: SMAX= 9.24: SK= .030]
04252> R0090:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04253> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .571 1990.0720_ 5:00 470.12 .646 .000
04254> [XIMP=.65:TIMP=.70]
04255> [LOSS= 2 :CN=100.0]
04256> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04257> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
04258> [IaRECimp= 1.50: IaRECper= 6.00]
04259> [SMIN= 1.39: SMAX= 9.24: SK= .030]
04260> R0090:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04261> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .338 1990.0720_ 5:00 454.32 .624 .000
04262> [XIMP=.53:TIMP=.63]
04263> [LOSS= 2 :CN=100.0]
04264> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04265> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
04266> [IaRECimp= 1.50: IaRECper= 6.00]
04267> [SMIN= 1.39: SMAX= 9.24: SK= .030]
04268> R0090:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04269> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .440 1990.0720_ 5:00 463.65 .637 .000
04270> [XIMP=.57:TIMP=.67]
04271> [LOSS= 2 :CN=100.0]
04272> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]

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04273> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
04274> [IaRECImp= 1.50: IaRECper= 6.00]
04275> [SMIN= 1.39: SMAX= 9.24: SK= .030]
04276> R0090:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04277> ADD HYD 5.0 02:INF-W1 8.92 .482 1990.0720_ 5:00 472.43 n/a .000
04278> + 5.0 02:INF-W2 10.75 .571 1990.0720_ 5:00 470.12 n/a .000
04279> + 5.0 02:INF-W3 6.30 .338 1990.0720_ 5:00 454.32 n/a .000
04280> + 5.0 02:INF-W4 8.18 .440 1990.0720_ 5:00 463.65 n/a .000
04281> SUM= 5.0 01:INF-BCD-PH 34.15 1.831 1990.0720_ 5:00 466.26 n/a .000
04282> #####
04283> # CONTINUOUS RAINFALL DATA
04284> #####
04285> ** END OF RUN : 90
04286>
04287> *****
04288>
04289>
04290>
04291>
04292>
04293> RUN#:COMMAND#
04294> R0091:C00001-----
04295> START
04296> [TZERO = .00 hrs on 19910101]
04297> [METOUT= 2 (1=imperial, 2=metric output)]
04298> [NSTORM= 0 ]
04299> [NRUN = 0091 ]
04300> #####
04301> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
04302> #####
04303> # Project Name: Barrhaven Conservancy Development
04304> # Project Number: 1474
04305> # Date : 2021/Oct/18
04306> # Modeller : J.Burnett, P.Eng.
04307> # Updated : 2022/Dec/13 [LP]
04308> # Company : J.F. Sabourin and Associates
04309> # License # : 2582634
04310> #####
04311> # Ottawa International Airport (1967 - 2003)
04312> R0091:C00002-----
04313> * READ AES DATA
04314> [Filename = YOW_1967_2007.123 ]
04315> [Start_date= 1991.0101: End_date= 1991.1231]
04316> [DT= 60.min: Length= 8040.hrs: WetHrs= 486: DryHrs= 7554: PTOT= 556.00]
04317> Maximum average rainfall intensities over
04318> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
04319> 11.30 9.90 6.87 4.10 2.53 1.72 1.28 1.08 .79 mm/hr
04320> 11.30 19.80 20.60 24.60 30.40 41.20 46.00 51.60 57.00 mm
04321> 19910409 19910409 19910409 19910409 19911016 19910422 19910410 19910410 19910423 date
04322> Number of rainfall events per following interevent time
04323> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
04324> 165 137 127 102 80 63 52 45 38
04325> Number of events with at least the following durations
04326> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
04327> 164 89 56 21 6 1 0 0 0
04328> R0091:C00003-----
04329> COMPUTE API
04330> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
04331> {APImax= 72.80: APIavg= 16.88: APImin= .26}
04332> #####
04333> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
04334> #####
04335> R0091:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04336> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .200 1991.0410_ 3:00 288.10 .518 .000
04337> [XIMP=.66:TIMP=.71]
04338> [LOSS= 2 :CN= 71.0]
04339> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04340> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
04341> [IaRECImp= 1.50: IaRECper= 6.00]
04342> [SMIN= 41.38: SMAX=275.84: SK= .030]
04343> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
04344> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04345> # Total Volume provided by LID - 179 m3
04346> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04347> R0091:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04348> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .200 1991.0410_ 3:00 288.10 n/a .000
04349> out <= 5.0 01:W1-LID 2.89 .001 1991.0302_ 6:50 288.11 n/a .000
04350> overflow <= 5.0 03:W1-LID-Out 6.03 .195 1991.0410_ 3:05 288.10 n/a .000
04351> {MxStoUsed=.1790E+01 m3, TotOvfVol=.1737E+01 m3, N-Ovf= 106, TotDurOvf= 185.hrs}
04352> R0091:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04353> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .234 1991.0410_ 3:00 284.38 .511 .000
04354> [XIMP=.65:TIMP=.70]
04355> [LOSS= 2 :CN= 71.0]
04356> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04357> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
04358> [IaRECImp= 1.50: IaRECper= 6.00]
04359> [SMIN= 41.38: SMAX=275.84: SK= .030]
04360> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
04361> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe

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04362> # Total Volume provided by LID - 200 m³
04363> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04364> R0091:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04365>   ROUTE RESERVOIR -> 5.0 02:W2 10.75 .234 1991.0410_ 3:00 284.38 n/a .000
04366>   out <= 5.0 01:W2-LID 3.28 .001 1991.0302_ 6:45 284.37 n/a .000
04367>   overflow <= 5.0 03:W2-LID-Out 7.47 .229 1991.0410_ 3:05 284.38 n/a .000
04368>   {MxStoUsed=.1999E-01 m3, TotOvfVol=.2124E+01 m3, N-Ovf= 106, TotDurOvf= 191.hrs}
04369> R0091:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04370>   CONTINUOUS STANDHYD 5.0 01:W3 6.30 .130 1991.0410_ 3:00 243.73 .438 .000
04371>   [XIMP=.53:TIMP=.63]
04372>   [LOSS= 2 :CN= 71.0]
04373>   [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04374>   [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
04375>   [IaRECImp= 1.50: IaRECper= 6.00]
04376>   [SMIN= 41.38: SMAX=275.84: SK= .030]
04377> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
04378> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04379> # Total Volume provided by LID - 96 m³
04380> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04381> R0091:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04382>   ROUTE RESERVOIR -> 5.0 02:W3 6.30 .130 1991.0410_ 3:00 243.73 n/a .000
04383>   out <= 5.0 01:W3-LID 1.79 .001 1991.0302_ 6:45 243.74 n/a .000
04384>   overflow <= 5.0 03:W3-LID-Out 4.51 .126 1991.0410_ 3:00 243.73 n/a .000
04385>   {MxStoUsed=.9596E-02 m3, TotOvfVol=.1099E+01 m3, N-Ovf= 123, TotDurOvf= 194.hrs}
04386> R0091:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04387>   CONTINUOUS STANDHYD 5.0 01:W4 8.18 .174 1991.0410_ 3:00 258.64 .465 .000
04388>   [XIMP=.57:TIMP=.67]
04389>   [LOSS= 2 :CN= 71.0]
04390>   [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04391>   [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
04392>   [IaRECImp= 1.50: IaRECper= 6.00]
04393>   [SMIN= 41.38: SMAX=275.84: SK= .030]
04394> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
04395> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04396> # Total Volume provided by LID - 131 m³
04397> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04398> R0091:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04399>   ROUTE RESERVOIR -> 5.0 02:W4 8.18 .174 1991.0410_ 3:00 258.64 n/a .000
04400>   out <= 5.0 01:W4-LID 2.34 .001 1991.0302_ 6:45 258.64 n/a .000
04401>   overflow <= 5.0 03:W4-LID-Out 5.84 .171 1991.0410_ 3:05 258.64 n/a .000
04402>   {MxStoUsed=.1310E-01 m3, TotOvfVol=.1511E+01 m3, N-Ovf= 111, TotDurOvf= 194.hrs}
04403> R0091:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04404>   ADD HYD 5.0 02:W1 8.92 .200 1991.0410_ 3:00 288.10 n/a .000
04405>   + 5.0 02:W2 10.75 .234 1991.0410_ 3:00 284.38 n/a .000
04406>   + 5.0 02:W3 6.30 .130 1991.0410_ 3:00 243.73 n/a .000
04407>   + 5.0 02:W4 8.18 .174 1991.0410_ 3:00 258.64 n/a .000
04408>   SUM= 5.0 01:BCD-PH3 34.15 .738 1991.0410_ 3:00 271.69 n/a .000
04409> R0091:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04410>   ADD HYD 5.0 02:W1-LID-Out 6.03 .195 1991.0410_ 3:05 288.10 n/a .000
04411>   + 5.0 02:W2-LID-Out 7.47 .229 1991.0410_ 3:05 284.38 n/a .000
04412>   + 5.0 02:W3-LID-Out 4.51 .126 1991.0410_ 3:00 243.73 n/a .000
04413>   + 5.0 02:W4-LID-Out 5.84 .171 1991.0410_ 3:05 258.64 n/a .000
04414>   SUM= 5.0 01:BCD-PH3-LI 23.85 .721 1991.0410_ 3:05 271.33 n/a .000
04415> #*****
04416> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
04417> #*****
04418> # Set infiltration to 0 (CN = 99.99) for water balance analysis
04419> #*****
04420> R0091:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04421>   CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .261 1991.0409_ 1:00 346.97 .624 .000
04422>   [XIMP=.66:TIMP=.71]
04423>   [LOSS= 2 :CN=100.0]
04424>   [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04425>   [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
04426>   [IaRECImp= 1.50: IaRECper= 6.00]
04427>   [SMIN= 1.39: SMAX= 9.24: SK= .030]
04428> R0091:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04429>   CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .313 1991.0409_ 1:00 344.79 .620 .000
04430>   [XIMP=.65:TIMP=.70]
04431>   [LOSS= 2 :CN=100.0]
04432>   [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04433>   [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
04434>   [IaRECImp= 1.50: IaRECper= 6.00]
04435>   [SMIN= 1.39: SMAX= 9.24: SK= .030]
04436> R0091:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04437>   CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .185 1991.0409_ 1:00 329.01 .592 .000
04438>   [XIMP=.53:TIMP=.63]
04439>   [LOSS= 2 :CN=100.0]
04440>   [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04441>   [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
04442>   [IaRECImp= 1.50: IaRECper= 6.00]
04443>   [SMIN= 1.39: SMAX= 9.24: SK= .030]
04444> R0091:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04445>   CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .241 1991.0409_ 1:00 337.77 .608 .000
04446>   [XIMP=.57:TIMP=.67]
04447>   [LOSS= 2 :CN=100.0]
04448>   [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04449>   [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
04450>   [IaRECImp= 1.50: IaRECper= 6.00]

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04451> [SMIN= 1.39: SMAX= 9.24: SK= .030]
04452> R0091:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04453> ADD HYD 5.0 02:INF-W1 8.92 .261 1991.0409_ 1:00 346.97 n/a .000
04454> + 5.0 02:INF-W2 10.75 .313 1991.0409_ 1:00 344.79 n/a .000
04455> + 5.0 02:INF-W3 6.30 .185 1991.0409_ 1:00 329.01 n/a .000
04456> + 5.0 02:INF-W4 8.18 .241 1991.0409_ 1:00 337.77 n/a .000
04457> SUM= 5.0 01:INF-BCD-PH 34.15 .999 1991.0409_ 1:00 340.77 n/a .000
04458> #####
04459> # CONTINUOUS RAINFALL DATA
04460> #####
04461> ** END OF RUN : 91
04462>
04463> *****
04464>
04465>
04466>
04467>
04468>
04469> RUN#:COMMAND#
04470> R0092:C00001-----
04471> START
04472> [TZERO = .00 hrs on 19920101]
04473> [METOUT= 2 (1=imperial, 2=metric output)]
04474> [NSTORM= 0 ]
04475> [NRUN = 0092 ]
04476> #*****
04477> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
04478> #*****
04479> # Project Name: Barrhaven Conservancy Development
04480> # Project Number: 1474
04481> # Date : 2021/Oct/18
04482> # Modeller : J.Burnett, P.Eng.
04483> # Updated : 2022/Dec/13 [LP]
04484> # Company : J.F. Sabourin and Associates
04485> # License # : 2582634
04486> #*****
04487> # Ottawa International Airport (1967 - 2003)
04488> R0092:C00002-----
04489> * READ AES DATA
04490> [Filename = YOW_1967_2007.123 ]
04491> [Start_date= 1992.0101: End_date= 1992.1230]
04492> [DT= 60.min: Length= 8760.hrs: WetHrs= 551: DryHrs= 8209: PTOT= 732.80]
04493> Maximum average rainfall intensities over
04494> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
04495> 31.50 18.00 13.30 7.22 4.14 2.26 1.51 1.51 1.02 mm/hr
04496> 31.50 36.00 39.90 43.30 49.70 54.20 54.20 72.60 73.60 mm
04497> 19920804 19920804 19920804 19920804 19920717 19920718 19920718 19920719 19920720 date
04498> Number of rainfall events per following interevent time
04499> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
04500> 190 151 132 100 84 69 55 47 38
04501> Number of events with at least the following durations
04502> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
04503> 189 109 70 22 5 1 0 0 0
04504> R0092:C00003-----
04505> COMPUTE API
04506> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
04507> [APImax= 97.62: APIavg= 20.33: APImin= 1.07]
04508> #*****
04509> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
04510> #*****
04511> R0092:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04512> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .613 1992.0804_14:00 400.30 .546 .000
04513> [XIMP=.66:TIMP=.71]
04514> [LOSS= 2 :CN= 71.0]
04515> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04516> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
04517> [IaRECimp= 1.50: IaRECper= 6.00]
04518> [SMIN= 41.38: SMAX=275.84: SK= .030]
04519> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
04520> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04521> # Total Volume provided by LID - 179 m³
04522> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04523> R0092:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04524> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .613 1992.0804_14:00 400.30 n/a .000
04525> out <= 5.0 01:W1-LID 2.29 .001 1992.0104_21:55 400.31 n/a .000
04526> overflow <= 5.0 03:W1-LID-Out 6.63 .601 1992.0804_14:00 400.30 n/a .000
04527> {MxStoUsed=.1788E-01 m3, TotOvfVol=.2653E+01 m3, N-Ovf= 118, TotDurOvf= 186.hrs}
04528> R0092:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04529> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .731 1992.0804_14:00 395.59 .540 .000
04530> [XIMP=.65:TIMP=.70]
04531> [LOSS= 2 :CN= 71.0]
04532> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04533> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
04534> [IaRECimp= 1.50: IaRECper= 6.00]
04535> [SMIN= 41.38: SMAX=275.84: SK= .030]
04536> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
04537> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04538> # Total Volume provided by LID - 200 m³
04539> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5

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04540> R0092:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04541> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .731 1992.0804_14:00 395.59 n/a .000
04542> out <= 5.0 01:W2-LID 2.60 .001 1992.0104_21:45 395.58 n/a .000
04543> overflow <= 5.0 03:W2-LID-Out 8.15 .717 1992.0804_14:00 395.59 n/a .000
04544> {MxStoUsed=.2000E-01 m3, TotOvfVol=.3223E+01 m3, N-Ovf= 117, TotDurOvf= 194.hrs}
04545> R0092:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04546> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .398 1992.0804_14:00 345.26 .471 .000
04547> [XIMP=.53:TIMP=.63]
04548> [LOSS= 2 :CN= 71.0]
04549> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04550> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
04551> [IaRECImp= 1.50: IaRECper= 6.00]
04552> [SMIN= 41.38: SMAX=275.84: SK= .030]
04553> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
04554> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04555> # Total Volume provided by LID - 96 m³
04556> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04557> R0092:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04558> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .398 1992.0804_14:00 345.26 n/a .000
04559> out <= 5.0 01:W3-LID 1.40 .001 1992.0104_21:45 345.27 n/a .000
04560> overflow <= 5.0 03:W3-LID-Out 4.90 .386 1992.0804_14:00 345.26 n/a .000
04561> {MxStoUsed=.9598E-02 m3, TotOvfVol=.1692E+01 m3, N-Ovf= 136, TotDurOvf= 196.hrs}
04562> R0092:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04563> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .534 1992.0804_14:00 364.21 .497 .000
04564> [XIMP=.57:TIMP=.67]
04565> [LOSS= 2 :CN= 71.0]
04566> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04567> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
04568> [IaRECImp= 1.50: IaRECper= 6.00]
04569> [SMIN= 41.38: SMAX=275.84: SK= .030]
04570> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
04571> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04572> # Total Volume provided by LID - 131 m³
04573> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04574> R0092:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04575> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .534 1992.0804_14:00 364.21 n/a .000
04576> out <= 5.0 01:W4-LID 1.83 .001 1992.0104_21:45 364.21 n/a .000
04577> overflow <= 5.0 03:W4-LID-Out 6.35 .520 1992.0804_14:00 364.21 n/a .000
04578> {MxStoUsed=.1308E-01 m3, TotOvfVol=.2311E+01 m3, N-Ovf= 133, TotDurOvf= 197.hrs}
04579> R0092:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04580> ADD HYD 5.0 02:W1 8.92 .613 1992.0804_14:00 400.30 n/a .000
04581> + 5.0 02:W2 10.75 .731 1992.0804_14:00 395.59 n/a .000
04582> + 5.0 02:W3 6.30 .398 1992.0804_14:00 345.26 n/a .000
04583> + 5.0 02:W4 8.18 .534 1992.0804_14:00 364.21 n/a .000
04584> SUM= 5.0 01:BCD-PH3 34.15 2.277 1992.0804_14:00 380.02 n/a .000
04585> R0092:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04586> ADD HYD 5.0 02:W1-LID-Out 6.63 .601 1992.0804_14:00 400.30 n/a .000
04587> + 5.0 02:W2-LID-Out 8.15 .717 1992.0804_14:00 395.59 n/a .000
04588> + 5.0 02:W3-LID-Out 4.90 .386 1992.0804_14:00 345.26 n/a .000
04589> + 5.0 02:W4-LID-Out 6.35 .520 1992.0804_14:00 364.21 n/a .000
04590> SUM= 5.0 01:BCD-PH3-LI 26.02 2.224 1992.0804_14:00 379.65 n/a .000
04591> #*****
04592> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
04593> #*****
04594> # Set infiltration to 0 (CN = 99.99) for water balance analysis
04595> #*****
04596> R0092:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04597> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .761 1992.0804_14:00 487.30 .665 .000
04598> [XIMP=.66:TIMP=.71]
04599> [LOSS= 2 :CN=100.0]
04600> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04601> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
04602> [IaRECImp= 1.50: IaRECper= 6.00]
04603> [SMIN= 1.39: SMAX= 9.24: SK= .030]
04604> R0092:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04605> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .914 1992.0804_14:00 484.99 .662 .000
04606> [XIMP=.65:TIMP=.70]
04607> [LOSS= 2 :CN=100.0]
04608> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04609> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
04610> [IaRECImp= 1.50: IaRECper= 6.00]
04611> [SMIN= 1.39: SMAX= 9.24: SK= .030]
04612> R0092:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04613> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .536 1992.0804_14:00 468.97 .640 .000
04614> [XIMP=.53:TIMP=.63]
04615> [LOSS= 2 :CN=100.0]
04616> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04617> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
04618> [IaRECImp= 1.50: IaRECper= 6.00]
04619> [SMIN= 1.39: SMAX= 9.24: SK= .030]
04620> R0092:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04621> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .696 1992.0804_14:00 478.36 .653 .000
04622> [XIMP=.57:TIMP=.67]
04623> [LOSS= 2 :CN=100.0]
04624> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04625> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
04626> [IaRECImp= 1.50: IaRECper= 6.00]
04627> [SMIN= 1.39: SMAX= 9.24: SK= .030]
04628> R0092:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms

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04629> ADD HYD 5.0 02:INF-W1 8.92 .761 1992.0804_14:00 487.30 n/a .000
04630> + 5.0 02:INF-W2 10.75 .914 1992.0804_14:00 484.99 n/a .000
04631> + 5.0 02:INF-W3 6.30 .536 1992.0804_14:00 468.97 n/a .000
04632> + 5.0 02:INF-W4 8.18 .696 1992.0804_14:00 478.36 n/a .000
04633> SUM= 5.0 01:INF-BCD-PH 34.15 2.907 1992.0804_14:00 481.05 n/a .000
04634> #####
04635> # CONTINUOUS RAINFALL DATA
04636> #####
04637> ** END OF RUN : 92
04638>
04639> *****
04640>
04641>
04642>
04643>
04644>
04645> RUN#:COMMAND#
04646> R0093:C00001-----
04647> START
04648> [TZERO = .00 hrs on 19930101]
04649> [METOUT= 2 (1=imperial, 2=metric output)]
04650> [NSTORM= 0 ]
04651> [NRUN = 0093 ]
04652> #*****
04653> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
04654> #*****
04655> # Project Name: Barrhaven Conservancy Development
04656> # Project Number: 1474
04657> # Date : 2021/Oct/18
04658> # Modeller : J.Burnett, P.Eng.
04659> # Updated : 2022/Dec/13 [LP]
04660> # Company : J.F. Sabourin and Associates
04661> # License # : 2582634
04662> #*****
04663> # Ottawa International Airport (1967 - 2003)
04664> R0093:C00002-----
04665> * READ AES DATA
04666> [Filename = YOW_1967_2007.123 ]
04667> [Start_date= 1993.0101: End_date= 1993.1231]
04668> {DT= 60.min: Length= 8760.hrs: WetHrs= 585: DryHrs= 8175: PTOT= 721.30}
04669> Maximum average rainfall intensities over
04670> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
04671> 12.60 6.60 4.83 3.72 3.58 2.31 1.61 1.21 .81 mm/hr
04672> 12.60 13.20 14.50 22.30 43.00 55.50 58.10 58.10 58.10 mm
04673> 19930703 19930703 19931127 19931128 19931128 19931128 19931128 19931128 19931129 date
04674> Number of rainfall events per following interevent time
04675> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
04676> 191 154 137 111 91 73 57 48 34
04677> Number of events with at least the following durations
04678> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
04679> 190 110 66 27 7 2 0 0 0
04680> R0093:C00003-----
04681> COMPUTE API
04682> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
04683> [APImax= 66.56: APIavg= 20.01: APImin= .11]
04684> #*****
04685> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
04686> #*****
04687> R0093:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04688> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .205 1993.0703_ 9:00 376.19 .522 .000
04689> [XIMP=.66:TIMP=.71]
04690> [LOSS= 2 :CN= 71.0]
04691> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04692> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
04693> [IaREcimp= 1.50: IaRECper= 6.00]
04694> [SMIN= 41.38: SMAX=275.84: SK= .030]
04695> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
04696> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04697> # Total Volume provided by LID - 179 m3
04698> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04699> R0093:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04700> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .205 1993.0703_ 9:00 376.19 n/a .000
04701> out <= 5.0 01:W1-LID 2.75 .001 1993.0104_ 1:05 376.20 n/a .000
04702> overflow <= 5.0 03:W1-LID-Out 6.17 .202 1993.0703_ 9:00 376.19 n/a .000
04703> {MxStoUsed=.1790E-01 m3, TotOvfVol=.2321E+01 m3, N-Ovf= 145, TotDurOvf= 223.hrs}
04704> R0093:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04705> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .240 1993.0703_ 9:00 371.40 .515 .000
04706> [XIMP=.65:TIMP=.70]
04707> [LOSS= 2 :CN= 71.0]
04708> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04709> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
04710> [IaREcimp= 1.50: IaRECper= 6.00]
04711> [SMIN= 41.38: SMAX=275.84: SK= .030]
04712> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
04713> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04714> # Total Volume provided by LID - 200 m3
04715> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04716> R0093:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04717> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .240 1993.0703_ 9:00 371.40 n/a .000

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04718>          out <=      5.0 01:W2-LID          3.14      .001 1993.0104_ 0:55 371.39 n/a      .000
04719>          overflow <= 5.0 03:W2-LID-Out       7.61      .237 1993.0703_ 9:00 371.40 n/a      .000
04720> {MxStoUsed=.1999E-01 m3, TotOvfVol=.2827E+01 m3, N-Ovf= 156, TotDurOvf= 232.hrs}
04721> R0093:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
04722> CONTINUOUS STANDHYD 5.0 01:W3              6.30      .118 1993.0703_ 9:00 319.25 .443      .000
04723> [XIMP=.53:TIMP=.63]
04724> [LOSS= 2 :CN= 71.0]
04725> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04726> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
04727> [IaRECImp= 1.50: IaRECper= 6.00]
04728> [SMIN= 41.38: SMAX=275.84: SK= .030]
04729> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
04730> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04731> # Total Volume provided by LID - 96 m³
04732> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04733> R0093:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
04734> ROUTE RESERVOIR -> 5.0 02:W3              6.30      .118 1993.0703_ 9:00 319.25 n/a      .000
04735>          out <=      5.0 01:W3-LID          1.72      .001 1993.0104_ 0:50 319.25 n/a      .000
04736>          overflow <= 5.0 03:W3-LID-Out       4.58      .117 1993.0703_ 9:00 319.25 n/a      .000
04737> {MxStoUsed=.9599E-02 m3, TotOvfVol=.1463E+01 m3, N-Ovf= 160, TotDurOvf= 239.hrs}
04738> R0093:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
04739> CONTINUOUS STANDHYD 5.0 01:W4              8.18      .164 1993.0703_ 9:00 338.57 .469      .000
04740> [XIMP=.57:TIMP=.67]
04741> [LOSS= 2 :CN= 71.0]
04742> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04743> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
04744> [IaRECImp= 1.50: IaRECper= 6.00]
04745> [SMIN= 41.38: SMAX=275.84: SK= .030]
04746> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
04747> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04748> # Total Volume provided by LID - 131 m³
04749> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04750> R0093:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
04751> ROUTE RESERVOIR -> 5.0 02:W4              8.18      .164 1993.0703_ 9:00 338.57 n/a      .000
04752>          out <=      5.0 01:W4-LID          2.24      .001 1993.0104_ 0:50 338.57 n/a      .000
04753>          overflow <= 5.0 03:W4-LID-Out       5.94      .162 1993.0703_ 9:00 338.57 n/a      .000
04754> {MxStoUsed=.1309E-01 m3, TotOvfVol=.2011E+01 m3, N-Ovf= 158, TotDurOvf= 240.hrs}
04755> R0093:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
04756> ADD HYD          5.0 02:W1              8.92      .205 1993.0703_ 9:00 376.19 n/a      .000
04757> +              5.0 02:W2              10.75     .240 1993.0703_ 9:00 371.40 n/a      .000
04758> +              5.0 02:W3              6.30      .118 1993.0703_ 9:00 319.25 n/a      .000
04759> +              5.0 02:W4              8.18      .164 1993.0703_ 9:00 338.57 n/a      .000
04760> SUM=           5.0 01:BCD-PH3          34.15     .727 1993.0703_ 9:00 355.16 n/a      .000
04761> R0093:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
04762> ADD HYD          5.0 02:W1-LID-Out         6.17      .202 1993.0703_ 9:00 376.19 n/a      .000
04763> +              5.0 02:W2-LID-Out         7.61      .237 1993.0703_ 9:00 371.40 n/a      .000
04764> +              5.0 02:W3-LID-Out         4.58      .117 1993.0703_ 9:00 319.25 n/a      .000
04765> +              5.0 02:W4-LID-Out         5.94      .162 1993.0703_ 9:00 338.57 n/a      .000
04766> SUM=           5.0 01:BCD-PH3-LI       24.31     .718 1993.0703_ 9:00 354.76 n/a      .000
04767> #*****
04768> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
04769> #*****
04770> # Set infiltration to 0 (CN = 99.99) for water balance analysis
04771> #*****
04772> R0093:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
04773> CONTINUOUS STANDHYD 5.0 01:INF-W1          8.92      .241 1993.0703_ 9:00 454.07 .630      .000
04774> [XIMP=.66:TIMP=.71]
04775> [LOSS= 2 :CN=100.0]
04776> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04777> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
04778> [IaRECImp= 1.50: IaRECper= 6.00]
04779> [SMIN= 1.39: SMAX= 9.24: SK= .030]
04780> R0093:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
04781> CONTINUOUS STANDHYD 5.0 01:INF-W2          10.75     .285 1993.0703_ 9:00 451.33 .626      .000
04782> [XIMP=.65:TIMP=.70]
04783> [LOSS= 2 :CN=100.0]
04784> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04785> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
04786> [IaRECImp= 1.50: IaRECper= 6.00]
04787> [SMIN= 1.39: SMAX= 9.24: SK= .030]
04788> R0093:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
04789> CONTINUOUS STANDHYD 5.0 01:INF-W3          6.30      .164 1993.0703_ 9:00 431.74 .599      .000
04790> [XIMP=.53:TIMP=.63]
04791> [LOSS= 2 :CN=100.0]
04792> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04793> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
04794> [IaRECImp= 1.50: IaRECper= 6.00]
04795> [SMIN= 1.39: SMAX= 9.24: SK= .030]
04796> R0093:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
04797> CONTINUOUS STANDHYD 5.0 01:INF-W4          8.18      .219 1993.0703_ 9:00 442.84 .614      .000
04798> [XIMP=.57:TIMP=.67]
04799> [LOSS= 2 :CN=100.0]
04800> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04801> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
04802> [IaRECImp= 1.50: IaRECper= 6.00]
04803> [SMIN= 1.39: SMAX= 9.24: SK= .030]
04804> R0093:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
04805> ADD HYD          5.0 02:INF-W1              8.92      .241 1993.0703_ 9:00 454.07 n/a      .000
04806> +              5.0 02:INF-W2          10.75     .285 1993.0703_ 9:00 451.33 n/a      .000

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04807>          +      5.0 02:INF-W3          6.30      .164 1993.0703_ 9:00 431.74 n/a      .000
04808>          +      5.0 02:INF-W4          8.18      .219 1993.0703_ 9:00 442.84 n/a      .000
04809>          SUM=    5.0 01:INF-BCD-PH      34.15      .909 1993.0703_ 9:00 446.40 n/a      .000
04810> #####
04811> # CONTINUOUS RAINFALL DATA
04812> #####
04813> ** END OF RUN : 93
04814>
04815> *****
04816>
04817>
04818>
04819>
04820>
04821> RUN#:COMMAND#
04822> R0094:C00001-----
04823> START
04824> [TZERO = .00 hrs on 19940101]
04825> [METOUT= 2 (1=imperial, 2=metric output)]
04826> [NSTORM= 0 ]
04827> [NRUN = 0094 ]
04828> #*****
04829> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
04830> #*****
04831> # Project Name: Barrhaven Conservancy Development
04832> # Project Number: 1474
04833> # Date : 2021/Oct/18
04834> # Modeller : J.Burnett, P.Eng.
04835> # Updated : 2022/Dec/13 [LP]
04836> # Company : J.F. Sabourin and Associates
04837> # License # : 2582634
04838> #*****
04839> # Ottawa International Airport (1967 - 2003)
04840> R0094:C00002-----
04841> * READ AES DATA
04842> [Filename = YOW_1967_2007.123 ]
04843> [Start_date= 1994.0101: End_date= 1994.1231]
04844> {DT= 60.min: Length= 8760.hrs: WetHrs= 342: DryHrs= 8418: PTOT= 540.20}
04845> Maximum average rainfall intensities over
04846> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
04847> 22.60 11.90 8.43 5.42 2.92 1.79 1.19 .89 1.15 mm/hr
04848> 22.60 23.80 25.30 32.50 35.00 42.90 42.90 42.90 82.60 mm
04849> 19940629 19940629 19940627 19940625 19940625 19940625 19940626 19940626 19940627 date
04850> Number of rainfall events per following interevent time
04851> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
04852> 138 115 101 79 62 48 39 34 26
04853> Number of events with at least the following durations
04854> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
04855> 137 72 48 12 1 0 0 0 0
04856> R0094:C00003-----
04857> COMPUTE API
04858> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
04859> {APIimax= 97.84: APIavg= 15.35: APIimin= .02}
04860> #*****
04861> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
04862> #*****
04863> R0094:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04864> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .404 1994.0629_13:00 289.36 .536 .000
04865> [XIMP=.66:TIMP=.71]
04866> [LOSS= 2 :CN= 71.0]
04867> [Pervious area: IAPER= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04868> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
04869> [IaRECimp= 1.50: IaRECper= 6.00]
04870> [SMIN= 41.38: SMAX=275.84: SK= .030]
04871> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
04872> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04873> # Total Volume provided by LID - 179 m3
04874> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04875> R0094:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04876> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .404 1994.0629_13:00 289.36 n/a .000
04877> out <= 5.0 01:W1-LID 2.30 .001 1994.0322_ 1:35 289.37 n/a .000
04878> overflow <= 5.0 03:W1-LID-Out 6.62 .399 1994.0629_13:00 289.36 n/a .000
04879> {MxStoUsed=.1790E-01 m3, TotOvfVol=.1916E+01 m3, N-Ovf= 105, TotDurOvf= 117.hrs}
04880> R0094:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04881> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .475 1994.0629_13:00 285.81 .529 .000
04882> [XIMP=.65:TIMP=.70]
04883> [LOSS= 2 :CN= 71.0]
04884> [Pervious area: IAPER= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04885> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
04886> [IaRECimp= 1.50: IaRECper= 6.00]
04887> [SMIN= 41.38: SMAX=275.84: SK= .030]
04888> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
04889> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04890> # Total Volume provided by LID - 200 m3
04891> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04892> R0094:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04893> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .475 1994.0629_13:00 285.81 n/a .000
04894> out <= 5.0 01:W2-LID 2.61 .001 1994.0322_ 1:25 285.81 n/a .000
04895> overflow <= 5.0 03:W2-LID-Out 8.14 .468 1994.0629_13:00 285.81 n/a .000

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04896> {MxStoUsed=.1999E-01 m3, TotOvfVol=.2327E+01 m3, N-Ovf= 112, TotDurOvf= 124.hrs}
04897> R0094:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04898> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .249 1994.0629_13:00 247.94 .459 .000
04899> [XIMP=.53:TIMP=.63]
04900> [LOSS= 2 :CN= 71.0]
04901> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04902> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
04903> [IaRECimp= 1.50: IaRECper= 6.00]
04904> [SMIN= 41.38: SMAX=275.84: SK= .030]
04905> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
04906> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04907> # Total Volume provided by LID - 96 m³
04908> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04909> R0094:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04910> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .249 1994.0629_13:00 247.94 n/a .000
04911> out <= 5.0 01:W3-LID 1.40 .001 1994.0322_1:20 247.94 n/a .000
04912> overflow <= 5.0 03:W3-LID-Out 4.90 .244 1994.0629_13:00 247.94 n/a .000
04913> {MxStoUsed=.9588E-02 m3, TotOvfVol=.1214E+01 m3, N-Ovf= 109, TotDurOvf= 127.hrs}
04914> R0094:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04915> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .340 1994.0629_13:00 262.21 .485 .000
04916> [XIMP=.57:TIMP=.67]
04917> [LOSS= 2 :CN= 71.0]
04918> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04919> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
04920> [IaRECimp= 1.50: IaRECper= 6.00]
04921> [SMIN= 41.38: SMAX=275.84: SK= .030]
04922> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
04923> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
04924> # Total Volume provided by LID - 131 m³
04925> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
04926> R0094:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04927> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .340 1994.0629_13:00 262.21 n/a .000
04928> out <= 5.0 01:W4-LID 1.84 .001 1994.0322_1:20 262.22 n/a .000
04929> overflow <= 5.0 03:W4-LID-Out 6.34 .334 1994.0629_13:00 262.21 n/a .000
04930> {MxStoUsed=.1310E-01 m3, TotOvfVol=.1662E+01 m3, N-Ovf= 111, TotDurOvf= 128.hrs}
04931> R0094:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04932> ADD HYD 5.0 02:W1 8.92 .404 1994.0629_13:00 289.36 n/a .000
04933> + 5.0 02:W2 10.75 .475 1994.0629_13:00 285.81 n/a .000
04934> + 5.0 02:W3 6.30 .249 1994.0629_13:00 247.94 n/a .000
04935> + 5.0 02:W4 8.18 .340 1994.0629_13:00 262.21 n/a .000
04936> SUM= 5.0 01:BCD-PH3 34.15 1.469 1994.0629_13:00 274.10 n/a .000
04937> R0094:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04938> ADD HYD 5.0 02:W1-LID-Out 6.62 .399 1994.0629_13:00 289.36 n/a .000
04939> + 5.0 02:W2-LID-Out 8.14 .468 1994.0629_13:00 285.81 n/a .000
04940> + 5.0 02:W3-LID-Out 4.90 .244 1994.0629_13:00 247.94 n/a .000
04941> + 5.0 02:W4-LID-Out 6.34 .334 1994.0629_13:00 262.21 n/a .000
04942> SUM= 5.0 01:BCD-PH3-LI 26.00 1.445 1994.0629_13:00 273.83 n/a .000
04943> #*****
04944> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
04945> #*****
04946> # Set infiltration to 0 (CN = 99.99) for water balance analysis
04947> #*****
04948> R0094:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04949> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .520 1994.0629_13:00 353.48 .654 .000
04950> [XIMP=.66:TIMP=.71]
04951> [LOSS= 2 :CN=100.0]
04952> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04953> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
04954> [IaRECimp= 1.50: IaRECper= 6.00]
04955> [SMIN= 1.39: SMAX= 9.24: SK= .030]
04956> R0094:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04957> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .623 1994.0629_13:00 351.67 .651 .000
04958> [XIMP=.65:TIMP=.70]
04959> [LOSS= 2 :CN=100.0]
04960> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04961> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
04962> [IaRECimp= 1.50: IaRECper= 6.00]
04963> [SMIN= 1.39: SMAX= 9.24: SK= .030]
04964> R0094:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04965> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .363 1994.0629_13:00 339.63 .629 .000
04966> [XIMP=.53:TIMP=.63]
04967> [LOSS= 2 :CN=100.0]
04968> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04969> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
04970> [IaRECimp= 1.50: IaRECper= 6.00]
04971> [SMIN= 1.39: SMAX= 9.24: SK= .030]
04972> R0094:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04973> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .473 1994.0629_13:00 346.97 .642 .000
04974> [XIMP=.57:TIMP=.67]
04975> [LOSS= 2 :CN=100.0]
04976> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
04977> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
04978> [IaRECimp= 1.50: IaRECper= 6.00]
04979> [SMIN= 1.39: SMAX= 9.24: SK= .030]
04980> R0094:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
04981> ADD HYD 5.0 02:INF-W1 8.92 .520 1994.0629_13:00 353.48 n/a .000
04982> + 5.0 02:INF-W2 10.75 .623 1994.0629_13:00 351.67 n/a .000
04983> + 5.0 02:INF-W3 6.30 .363 1994.0629_13:00 339.63 n/a .000
04984> + 5.0 02:INF-W4 8.18 .473 1994.0629_13:00 346.97 n/a .000

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04985>          SUM=      5.0 01:INF-BCD-PH    34.15    1.979 1994.0629_13:00 348.80 n/a    .000
04986> #####
04987> # CONTINUOUS RAINFALL DATA
04988> #####
04989> ** END OF RUN :    94
04990>
04991> *****
04992>
04993>
04994>
04995>
04996>
04997> RUN#:COMMAND#
04998> R0095:C00001-----
04999> START
05000> [TZERO =      .00 hrs on 19950101]
05001> [METOUT= 2      (1=imperial, 2=metric output)]
05002> [NSTORM= 0 ]
05003> [NRUN = 0095 ]
05004> #*****
05005> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
05006> #*****
05007> # Project Name: Barrhaven Conservancy Development
05008> # Project Number: 1474
05009> # Date : 2021/Oct/18
05010> # Modeller : J.Burnett, P.Eng.
05011> # Updated : 2022/Dec/13 [LP]
05012> # Company : J.F. Sabourin and Associates
05013> # License # : 2582634
05014> #*****
05015> # Ottawa International Airport (1967 - 2003)
05016> R0095:C00002-----
05017> * READ AES DATA
05018> [Filename = YOW_1967_2007.123 ]
05019> [Start_date= 1995.0101: End_date= 1995.1231]
05020> [DT= 60.min: Length= 8040.hrs: WetHrs= 332: DryHrs= 7708: PTOT= 538.50]
05021> Maximum average rainfall intensities over
05022> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
05023> 16.90 13.25 11.33 8.98 6.35 3.48 2.95 2.21 1.48 mm/hr
05024> 16.90 26.50 34.00 53.90 76.20 83.40 106.20 106.20 106.20 mm
05025> 19950603 19950603 19951006 19951006 19951006 19951006 19951007 19951007 19951008 date
05026> Number of rainfall events per following interevent time
05027> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
05028> 91 73 65 55 47 41 34 31 25
05029> Number of events with at least the following durations
05030> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
05031> 90 54 35 16 7 1 0 0 0
05032> R0095:C00003-----
05033> COMPUTE API
05034> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
05035> [APImax= 99.57: APIavg= 16.58: APImin= .00]
05036> #*****
05037> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
05038> #*****
05039> R0095:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05040> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .312 1995.0603_ 2:00 352.28 .654 .000
05041> [XIMP=.66:TIMP=.71]
05042> [LOSS= 2 :CN= 71.0]
05043> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05044> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
05045> [IaRECImp= 1.50: IaRECper= 6.00]
05046> [SMIN= 41.38: SMAX=275.84: SK= .030]
05047> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
05048> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05049> # Total Volume provided by LID - 179 m3
05050> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05051> R0095:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05052> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .312 1995.0603_ 2:00 352.28 n/a .000
05053> out <= 5.0 01:W1-LID 1.46 .001 1995.0113_15:35 352.28 n/a .000
05054> overflow <= 5.0 03:W1-LID-Out 7.46 .308 1995.0603_ 2:00 352.28 n/a .000
05055> {MxStoUsed=.1790E-01 m3, TotOvfVol=.2629E+01 m3, N-Ovf= 63, TotDurOvf= 154.hrs}
05056> R0095:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05057> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .372 1995.0603_ 2:00 349.29 .649 .000
05058> [XIMP=.65:TIMP=.70]
05059> [LOSS= 2 :CN= 71.0]
05060> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05061> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
05062> [IaRECImp= 1.50: IaRECper= 6.00]
05063> [SMIN= 41.38: SMAX=275.84: SK= .030]
05064> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
05065> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05066> # Total Volume provided by LID - 200 m3
05067> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05068> R0095:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05069> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .372 1995.0603_ 2:00 349.29 n/a .000
05070> out <= 5.0 01:W2-LID 1.66 .001 1995.0113_15:35 349.29 n/a .000
05071> overflow <= 5.0 03:W2-LID-Out 9.09 .366 1995.0603_ 2:00 349.29 n/a .000
05072> {MxStoUsed=.1999E-01 m3, TotOvfVol=.3175E+01 m3, N-Ovf= 70, TotDurOvf= 157.hrs}
05073> R0095:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms

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05074> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .203 1995.0603_ 8:05 319.42 .593 .000
05075> [XIMP=.53:TIMP=.63]
05076> [LOSS= 2 :CN= 71.0]
05077> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05078> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
05079> [IaRECImp= 1.50: IaRECper= 6.00]
05080> [SMIN= 41.38: SMAX=275.84: SK= .030]
05081> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
05082> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05083> # Total Volume provided by LID - 96 m³
05084> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05085> R0095:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05086> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .203 1995.0603_ 8:05 319.42 n/a .000
05087> out <= 5.0 01:W3-LID .86 .001 1995.0113_15:35 319.42 n/a .000
05088> overflow <= 5.0 03:W3-LID-Out 5.44 .202 1995.0603_ 8:05 319.42 n/a .000
05089> {MxStoUsed=.9595E-02 m3, TotOvfVol=.1738E+01 m3, N-Ovf= 65, TotDurOvf= 159.hrs}
05090> R0095:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05091> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .267 1995.0603_ 8:05 331.54 .616 .000
05092> [XIMP=.57:TIMP=.67]
05093> [LOSS= 2 :CN= 71.0]
05094> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05095> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
05096> [IaRECImp= 1.50: IaRECper= 6.00]
05097> [SMIN= 41.38: SMAX=275.84: SK= .030]
05098> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
05099> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05100> # Total Volume provided by LID - 131 m³
05101> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05102> R0095:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05103> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .267 1995.0603_ 8:05 331.54 n/a .000
05104> out <= 5.0 01:W4-LID 1.14 .001 1995.0113_15:35 331.54 n/a .000
05105> overflow <= 5.0 03:W4-LID-Out 7.04 .265 1995.0603_ 8:05 331.54 n/a .000
05106> {MxStoUsed=.1310E-01 m3, TotOvfVol=.2333E+01 m3, N-Ovf= 70, TotDurOvf= 160.hrs}
05107> R0095:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05108> ADD HYD 5.0 02:W1 8.92 .312 1995.0603_ 2:00 352.28 n/a .000
05109> + 5.0 02:W2 10.75 .372 1995.0603_ 2:00 349.29 n/a .000
05110> + 5.0 02:W3 6.30 .203 1995.0603_ 8:05 319.42 n/a .000
05111> + 5.0 02:W4 8.18 .267 1995.0603_ 8:05 331.54 n/a .000
05112> SUM= 5.0 01:BCD-PH3 34.15 1.145 1995.0603_ 2:00 340.31 n/a .000
05113> R0095:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05114> ADD HYD 5.0 02:W1-LID-Out 7.46 .308 1995.0603_ 2:00 352.28 n/a .000
05115> + 5.0 02:W2-LID-Out 9.09 .366 1995.0603_ 2:00 349.29 n/a .000
05116> + 5.0 02:W3-LID-Out 5.44 .202 1995.0603_ 8:05 319.42 n/a .000
05117> + 5.0 02:W4-LID-Out 7.04 .265 1995.0603_ 8:05 331.54 n/a .000
05118> SUM= 5.0 01:BCD-PH3-LI 29.03 1.128 1995.0603_ 2:00 340.16 n/a .000
05119> #*****
05120> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDI
05121> #*****
05122> # Set infiltration to 0 (CN = 99.99) for water balance analysis
05123> #*****
05124> R0095:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05125> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .405 1995.0603_ 2:00 413.01 .767 .000
05126> [XIMP=.66:TIMP=.71]
05127> [LOSS= 2 :CN=100.0]
05128> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05129> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
05130> [IaRECImp= 1.50: IaRECper= 6.00]
05131> [SMIN= 1.39: SMAX= 9.24: SK= .030]
05132> R0095:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05133> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .487 1995.0603_ 2:00 411.79 .765 .000
05134> [XIMP=.65:TIMP=.70]
05135> [LOSS= 2 :CN=100.0]
05136> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05137> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
05138> [IaRECImp= 1.50: IaRECper= 6.00]
05139> [SMIN= 1.39: SMAX= 9.24: SK= .030]
05140> R0095:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05141> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .288 1995.0603_ 2:00 403.66 .750 .000
05142> [XIMP=.53:TIMP=.63]
05143> [LOSS= 2 :CN=100.0]
05144> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05145> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
05146> [IaRECImp= 1.50: IaRECper= 6.00]
05147> [SMIN= 1.39: SMAX= 9.24: SK= .030]
05148> R0095:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05149> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .371 1995.0603_ 2:00 408.61 .759 .000
05150> [XIMP=.57:TIMP=.67]
05151> [LOSS= 2 :CN=100.0]
05152> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05153> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
05154> [IaRECImp= 1.50: IaRECper= 6.00]
05155> [SMIN= 1.39: SMAX= 9.24: SK= .030]
05156> R0095:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05157> ADD HYD 5.0 02:INF-W1 8.92 .405 1995.0603_ 2:00 413.01 n/a .000
05158> + 5.0 02:INF-W2 10.75 .487 1995.0603_ 2:00 411.79 n/a .000
05159> + 5.0 02:INF-W3 6.30 .288 1995.0603_ 2:00 403.66 n/a .000
05160> + 5.0 02:INF-W4 8.18 .371 1995.0603_ 2:00 408.61 n/a .000
05161> SUM= 5.0 01:INF-BCD-PH 34.15 1.551 1995.0603_ 2:00 409.85 n/a .000
05162> #####

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05163> # CONTINUOUS RAINFALL DATA
05164> #####
05165> ** END OF RUN : 95
05166>
05167> *****
05168>
05169>
05170>
05171>
05172>
05173> RUN#:COMMAND#
05174> R0096:C00001-----
05175> START
05176> [TZERO = .00 hrs on 19960101]
05177> [METOUT= 2 (1=imperial, 2=metric output)]
05178> [NSTORM= 0 ]
05179> [NRUN = 0096 ]
05180> #*****
05181> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
05182> #*****
05183> # Project Name: Barrhaven Conservancy Development
05184> # Project Number: 1474
05185> # Date : 2021/Oct/18
05186> # Modeller : J.Burnett, P.Eng.
05187> # Updated : 2022/Dec/13 [LP]
05188> # Company : J.F. Sabourin and Associates
05189> # License # : 2582634
05190> #*****
05191> # Ottawa International Airport (1967 - 2003)
05192> R0096:C00002-----
05193> * READ AES DATA
05194> [Filename = YOW_1967_2007.123 ]
05195> [Start_date= 1996.0101: End_date= 1996.1230]
05196> [DT= 60.min: Length= 6552.hrs: WetHrs= 387: DryHrs= 6165: PTOT= 512.20]
05197> Maximum average rainfall intensities over
05198> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
05199> 18.50 13.55 9.03 5.42 2.93 1.84 1.32 1.02 .70 mm/hr
05200> 18.50 27.10 27.10 32.50 35.10 44.10 47.50 49.00 50.30 mm
05201> 19960731 19960731 19960731 19960731 19960731 19961109 19961109 19961109 date
05202> Number of rainfall events per following interevent time
05203> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
05204> 132 104 93 71 59 43 36 31 24
05205> Number of events with at least the following durations
05206> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
05207> 131 72 50 19 2 1 0 0 0
05208> R0096:C00003-----
05209> COMPUTE API
05210> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
05211> {APIimax= 63.22: APIavg= 19.39: APIimin= .71}
05212> #*****
05213> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
05214> #*****
05215> R0096:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
05216> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .319 1996.0731_15:00 268.38 .524 .000
05217> [XIMP=.66:TIMP=.71]
05218> [LOSS= 2 :CN= 71.0]
05219> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05220> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
05221> [IaRECimp= 1.50: IaRECper= 6.00]
05222> [SMIN= 41.38: SMAX=275.84: SK= .030]
05223> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
05224> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05225> # Total Volume provided by LID - 179 m³
05226> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05227> R0096:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
05228> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .319 1996.0731_15:00 268.38 n/a .000
05229> out <= 5.0 01:W1-LID 2.54 .001 1996.0416_16:20 268.38 n/a .000
05230> overflow <= 5.0 03:W1-LID-Out 6.38 .315 1996.0731_15:00 268.38 n/a .000
05231> {MxStoUsed=.1790E-01 m3, TotOvfVol=.1712E+01 m3, N-Ovf= 112, TotDurOvf= 144.hrs}
05232> R0096:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
05233> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .378 1996.0731_15:00 264.99 .517 .000
05234> [XIMP=.65:TIMP=.70]
05235> [LOSS= 2 :CN= 71.0]
05236> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05237> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
05238> [IaRECimp= 1.50: IaRECper= 6.00]
05239> [SMIN= 41.38: SMAX=275.84: SK= .030]
05240> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
05241> # Assumed 870 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05242> # Total Volume provided by LID - 200 m³
05243> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05244> R0096:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
05245> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .378 1996.0731_15:00 264.99 n/a .000
05246> out <= 5.0 01:W2-LID 2.89 .001 1996.0416_16:15 264.98 n/a .000
05247> overflow <= 5.0 03:W2-LID-Out 7.86 .374 1996.0731_15:00 264.99 n/a .000
05248> {MxStoUsed=.1999E-01 m3, TotOvfVol=.2083E+01 m3, N-Ovf= 110, TotDurOvf= 151.hrs}
05249> R0096:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
05250> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .193 1996.0731_15:00 228.30 .446 .000
05251> [XIMP=.53:TIMP=.63]

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05252> [LOSS= 2 :CN= 71.0]
05253> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05254> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
05255> [IaRECImp= 1.50: IaRECper= 6.00]
05256> [SMIN= 41.38: SMAX=275.84: SK= .030]
05257> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
05258> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05259> # Total Volume provided by LID - 96 m³
05260> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05261> R0096:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05262> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .193 1996.0731_15:00 228.30 n/a .000
05263> out <= 5.0 01:W3-LID 1.58 .001 1996.0416_16:10 228.31 n/a .000
05264> overflow <= 5.0 03:W3-LID-Out 4.72 .189 1996.0731_15:00 228.30 n/a .000
05265> {MxStoUsed=.9599E-02 m3, TotOvfVol=.1079E+01 m3, N-Ovf= 111, TotDurOvf= 154.hrs}
05266> R0096:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05267> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .265 1996.0731_15:00 241.96 .472 .000
05268> [XIMP=.57:TIMP=.67]
05269> [LOSS= 2 :CN= 71.0]
05270> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05271> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
05272> [IaRECImp= 1.50: IaRECper= 6.00]
05273> [SMIN= 41.38: SMAX=275.84: SK= .030]
05274> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
05275> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05276> # Total Volume provided by LID - 131 m³
05277> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05278> R0096:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05279> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .265 1996.0731_15:00 241.96 n/a .000
05280> out <= 5.0 01:W4-LID 2.06 .001 1996.0416_16:10 241.96 n/a .000
05281> overflow <= 5.0 03:W4-LID-Out 6.12 .260 1996.0731_15:00 241.96 n/a .000
05282> {MxStoUsed=.1309E-01 m3, TotOvfVol=.1482E+01 m3, N-Ovf= 116, TotDurOvf= 155.hrs}
05283> R0096:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05284> ADD HYD 5.0 02:W1 8.92 .319 1996.0731_15:00 268.38 n/a .000
05285> + 5.0 02:W2 10.75 .378 1996.0731_15:00 264.99 n/a .000
05286> + 5.0 02:W3 6.30 .193 1996.0731_15:00 228.30 n/a .000
05287> + 5.0 02:W4 8.18 .265 1996.0731_15:00 241.96 n/a .000
05288> SUM= 5.0 01:BCD-PH3 34.15 1.155 1996.0731_15:00 253.59 n/a .000
05289> R0096:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05290> ADD HYD 5.0 02:W1-LID-Out 6.38 .315 1996.0731_15:00 268.38 n/a .000
05291> + 5.0 02:W2-LID-Out 7.86 .374 1996.0731_15:00 264.99 n/a .000
05292> + 5.0 02:W3-LID-Out 4.72 .189 1996.0731_15:00 228.30 n/a .000
05293> + 5.0 02:W4-LID-Out 6.12 .260 1996.0731_15:00 241.96 n/a .000
05294> SUM= 5.0 01:BCD-PH3-LI 25.09 1.138 1996.0731_15:00 253.32 n/a .000
05295> #*****
05296> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
05297> #*****
05298> # Set infiltration to 0 (CN = 99.99) for water balance analysis
05299> #*****
05300> R0096:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05301> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .415 1996.0731_15:00 325.58 .636 .000
05302> [XIMP=.66:TIMP=.71]
05303> [LOSS= 2 :CN=100.0]
05304> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05305> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
05306> [IaRECImp= 1.50: IaRECper= 6.00]
05307> [SMIN= 1.39: SMAX= 9.24: SK= .030]
05308> R0096:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05309> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .496 1996.0731_15:00 323.72 .632 .000
05310> [XIMP=.65:TIMP=.70]
05311> [LOSS= 2 :CN=100.0]
05312> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05313> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
05314> [IaRECImp= 1.50: IaRECper= 6.00]
05315> [SMIN= 1.39: SMAX= 9.24: SK= .030]
05316> R0096:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05317> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .294 1996.0731_15:00 310.77 .607 .000
05318> [XIMP=.53:TIMP=.63]
05319> [LOSS= 2 :CN=100.0]
05320> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05321> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
05322> [IaRECImp= 1.50: IaRECper= 6.00]
05323> [SMIN= 1.39: SMAX= 9.24: SK= .030]
05324> R0096:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05325> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .384 1996.0731_15:00 318.36 .622 .000
05326> [XIMP=.57:TIMP=.67]
05327> [LOSS= 2 :CN=100.0]
05328> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05329> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
05330> [IaRECImp= 1.50: IaRECper= 6.00]
05331> [SMIN= 1.39: SMAX= 9.24: SK= .030]
05332> R0096:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05333> ADD HYD 5.0 02:INF-W1 8.92 .415 1996.0731_15:00 325.58 n/a .000
05334> + 5.0 02:INF-W2 10.75 .496 1996.0731_15:00 323.72 n/a .000
05335> + 5.0 02:INF-W3 6.30 .294 1996.0731_15:00 310.77 n/a .000
05336> + 5.0 02:INF-W4 8.18 .384 1996.0731_15:00 318.36 n/a .000
05337> SUM= 5.0 01:INF-BCD-PH 34.15 1.590 1996.0731_15:00 320.53 n/a .000
05338> #*****
05339> # CONTINUOUS RAINFALL DATA
05340> #*****

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05341> ** END OF RUN : 96
05342>
05343> *****
05344>
05345>
05346>
05347>
05348>
05349> RUN#:COMMAND#
05350> R0097:C00001-----
05351> START
05352> [TZERO = .00 hrs on 19970101]
05353> [METOUT= 2 (1=imperial, 2=metric output)]
05354> [NSTORM= 0 ]
05355> [NRUN = 0097 ]
05356> #*****
05357> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
05358> #*****
05359> # Project Name: Barrhaven Conservancy Development
05360> # Project Number: 1474
05361> # Date : 2021/Oct/18
05362> # Modeller : J.Burnett, P.Eng.
05363> # Updated : 2022/Dec/13 [LP]
05364> # Company : J.F. Sabourin and Associates
05365> # License # : 2582634
05366> #*****
05367> # Ottawa International Airport (1967 - 2003)
05368> R0097:C00002-----
05369> * READ AES DATA
05370> [Filename = YOW_1967_2007.123 ]
05371> [Start_date= 1997.0101: End_date= 1997.1231]
05372> [DT= 60.min: Length= 8040.hrs: WetHrs= 379: DryHrs= 7661: PTOT= 433.20]
05373> Maximum average rainfall intensities over
05374> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
05375> 12.50 7.60 5.67 4.43 2.91 1.68 1.12 .84 .63 mm/hr
05376> 12.50 15.20 17.00 26.60 34.90 40.40 40.40 40.40 45.30 mm
05377> 19970622 19970622 19970622 19970221 19970222 19970222 19970222 19970222 19970222 date
05378> Number of rainfall events per following interevent time
05379> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
05380> 113 92 83 67 61 55 48 43 30
05381> Number of events with at least the following durations
05382> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
05383> 112 70 46 20 4 0 0 0 0
05384> R0097:C00003-----
05385> COMPUTE API
05386> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
05387> [APImax= 50.00: APIavg= 13.66: APImin= .27]
05388> #*****
05389> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
05390> #*****
05391> R0097:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05392> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .212 1997.0622_ 4:00 226.27 .522 .000
05393> [XIMP=.66:TIMP=.71]
05394> [LOSS= 2 :CN= 71.0]
05395> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05396> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
05397> [IaRECimp= 1.50: IaRECper= 6.00]
05398> [SMIN= 41.38: SMAX=275.84: SK= .030]
05399> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
05400> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05401> # Total Volume provided by LID - 179 m3
05402> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05403> R0097:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05404> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .212 1997.0622_ 4:00 226.27 n/a .000
05405> out <= 5.0 01:W1-LID 2.71 .001 1997.0219_19:20 226.27 n/a .000
05406> overflow <= 5.0 03:W1-LID-Out 6.21 .209 1997.0622_ 4:00 226.27 n/a .000
05407> {MxStoUsed=.1790E+01 m3, TotOvfVol=.1405E+01 m3, N-Ovf= 81, TotDurOvf= 158.hrs}
05408> R0097:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05409> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .249 1997.0622_ 4:00 223.23 .515 .000
05410> [XIMP=.65:TIMP=.70]
05411> [LOSS= 2 :CN= 71.0]
05412> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05413> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
05414> [IaRECimp= 1.50: IaRECper= 6.00]
05415> [SMIN= 41.38: SMAX=275.84: SK= .030]
05416> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
05417> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05418> # Total Volume provided by LID - 200 m3
05419> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05420> R0097:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05421> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .249 1997.0622_ 4:00 223.23 n/a .000
05422> out <= 5.0 01:W2-LID 3.09 .001 1997.0219_19:00 223.23 n/a .000
05423> overflow <= 5.0 03:W2-LID-Out 7.66 .246 1997.0622_ 4:00 223.23 n/a .000
05424> {MxStoUsed=.2000E+01 m3, TotOvfVol=.1710E+01 m3, N-Ovf= 85, TotDurOvf= 163.hrs}
05425> R0097:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05426> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .126 1997.0622_ 4:00 189.53 .438 .000
05427> [XIMP=.53:TIMP=.63]
05428> [LOSS= 2 :CN= 71.0]
05429> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]

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05430> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
05431> [IaRECimp= 1.50: IaRECper= 6.00]
05432> [SMIN= 41.38: SMAX=275.84: SK= .030]
05433> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
05434> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05435> # Total Volume provided by LID - 96 m³
05436> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05437> R0097:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05438> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .126 1997.0622_ 4:00 189.53 n/a .000
05439> out <= 5.0 01:W3-LID 1.71 .001 1997.0219_18:50 189.53 n/a .000
05440> overflow <= 5.0 03:W3-LID-Out 4.59 .124 1997.0622_ 4:00 189.53 n/a .000
05441> {MxStoUsed=.9597E-02 m3, TotOvfVol=.8705E+00 m3, N-Ovf= 88, TotDurOvf= 167.hrs}
05442> R0097:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05443> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .174 1997.0622_ 4:00 201.76 .466 .000
05444> [XIMP=.57:TIMP=.67]
05445> [LOSS= 2 :CN= 71.0]
05446> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05447> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
05448> [IaRECimp= 1.50: IaRECper= 6.00]
05449> [SMIN= 41.38: SMAX=275.84: SK= .030]
05450> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
05451> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05452> # Total Volume provided by LID - 131 m³
05453> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05454> R0097:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05455> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .174 1997.0622_ 4:00 201.76 n/a .000
05456> out <= 5.0 01:W4-LID 2.22 .001 1997.0219_18:50 201.76 n/a .000
05457> overflow <= 5.0 03:W4-LID-Out 5.96 .171 1997.0622_ 4:00 201.76 n/a .000
05458> {MxStoUsed=.1310E-01 m3, TotOvfVol=.1202E+01 m3, N-Ovf= 93, TotDurOvf= 167.hrs}
05459> R0097:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05460> ADD HYD 5.0 02:W1 8.92 .212 1997.0622_ 4:00 226.27 n/a .000
05461> + 5.0 02:W2 10.75 .249 1997.0622_ 4:00 223.23 n/a .000
05462> + 5.0 02:W3 6.30 .126 1997.0622_ 4:00 189.53 n/a .000
05463> + 5.0 02:W4 8.18 .174 1997.0622_ 4:00 201.76 n/a .000
05464> SUM= 5.0 01:BCD-PH3 34.15 .760 1997.0622_ 4:00 212.66 n/a .000
05465> R0097:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05466> ADD HYD 5.0 02:W1-LID-Out 6.21 .209 1997.0622_ 4:00 226.27 n/a .000
05467> + 5.0 02:W2-LID-Out 7.66 .246 1997.0622_ 4:00 223.23 n/a .000
05468> + 5.0 02:W3-LID-Out 4.59 .124 1997.0622_ 4:00 189.53 n/a .000
05469> + 5.0 02:W4-LID-Out 5.96 .171 1997.0622_ 4:00 201.76 n/a .000
05470> SUM= 5.0 01:BCD-PH3-LI 24.42 .751 1997.0622_ 4:00 212.43 n/a .000
05471> #*****
05472> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
05473> #*****
05474> # Set infiltration to 0 (CN = 99.99) for water balance analysis
05475> #*****
05476> R0097:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05477> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .282 1997.0622_ 4:00 278.62 .643 .000
05478> [XIMP=.66:TIMP=.71]
05479> [LOSS= 2 :CN=100.0]
05480> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05481> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
05482> [IaRECimp= 1.50: IaRECper= 6.00]
05483> [SMIN= 1.39: SMAX= 9.24: SK= .030]
05484> R0097:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05485> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .333 1997.0622_ 4:00 276.95 .639 .000
05486> [XIMP=.65:TIMP=.70]
05487> [LOSS= 2 :CN=100.0]
05488> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05489> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
05490> [IaRECimp= 1.50: IaRECper= 6.00]
05491> [SMIN= 1.39: SMAX= 9.24: SK= .030]
05492> R0097:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05493> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .197 1997.0622_ 4:00 265.55 .613 .000
05494> [XIMP=.53:TIMP=.63]
05495> [LOSS= 2 :CN=100.0]
05496> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05497> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
05498> [IaRECimp= 1.50: IaRECper= 6.00]
05499> [SMIN= 1.39: SMAX= 9.24: SK= .030]
05500> R0097:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05501> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .257 1997.0622_ 4:00 272.33 .629 .000
05502> [XIMP=.57:TIMP=.67]
05503> [LOSS= 2 :CN=100.0]
05504> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05505> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
05506> [IaRECimp= 1.50: IaRECper= 6.00]
05507> [SMIN= 1.39: SMAX= 9.24: SK= .030]
05508> R0097:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05509> ADD HYD 5.0 02:INF-W1 8.92 .282 1997.0622_ 4:00 278.62 n/a .000
05510> + 5.0 02:INF-W2 10.75 .333 1997.0622_ 4:00 276.95 n/a .000
05511> + 5.0 02:INF-W3 6.30 .197 1997.0622_ 4:00 265.55 n/a .000
05512> + 5.0 02:INF-W4 8.18 .257 1997.0622_ 4:00 272.33 n/a .000
05513> SUM= 5.0 01:INF-BCD-PH 34.15 1.069 1997.0622_ 4:00 274.18 n/a .000
05514> #*****
05515> # CONTINUOUS RAINFALL DATA
05516> #*****
05517> ** END OF RUN : 97
05518>

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05519> *****
05520>
05521>
05522>
05523>
05524>
05525> RUN#:COMMAND#
05526> R0098:C00001-----
05527> START
05528> [TZERO = .00 hrs on 19980101]
05529> [METOUT= 2 (1=imperial, 2=metric output)]
05530> [NSTORM= 0 ]
05531> [NRUN = 0098 ]
05532> #*****
05533> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
05534> #*****
05535> # Project Name: Barrhaven Conservancy Development
05536> # Project Number: 1474
05537> # Date : 2021/Oct/18
05538> # Modeller : J.Burnett, P.Eng.
05539> # Updated : 2022/Dec/13 [LP]
05540> # Company : J.F. Sabourin and Associates
05541> # License # : 2582634
05542> #*****
05543> # Ottawa International Airport (1967 - 2003)
05544> R0098:C00002-----
05545> * READ AES DATA
05546> [Filename = YOW_1967_2007.123 ]
05547> [Start_date= 1998.0101: End_date= 1998.1231]
05548> [DT= 60.min: Length= 5088.hrs: WetHrs= 291: DryHrs= 4797: PTOT= 440.30]
05549> Maximum average rainfall intensities over
05550> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
05551> 15.80 8.90 7.60 4.00 2.54 1.82 1.27 .95 .76 mm/hr
05552> 15.80 17.80 22.80 24.00 30.50 43.60 45.80 45.80 54.60 mm
05553> 19980716 19980627 19980927 19980927 19980927 19980927 19980928 19980928 19980615 date
05554> Number of rainfall events per following interevent time
05555> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
05556> 126 104 95 78 63 42 37 32 21
05557> Number of events with at least the following durations
05558> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
05559> 125 64 43 8 1 0 0 0 0
05560> R0098:C00003-----
05561> COMPUTE API
05562> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
05563> [APImax= 57.22: APIavg= 21.28: APImin= 1.69]
05564> #*****
05565> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
05566> #*****
05567> R0098:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05568> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .270 1998.0627_ 1:00 220.99 .502 .000
05569> [XIMP=.66:TIMP=.71]
05570> [LOSS= 2 :CN= 71.0]
05571> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05572> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
05573> [IaREcimp= 1.50: IaRCper= 6.00]
05574> [SMIN= 41.38: SMAX=275.84: SK= .030]
05575> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
05576> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05577> # Total Volume provided by LID - 179 m3
05578> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05579> R0098:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05580> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .270 1998.0627_ 1:00 220.99 n/a .000
05581> out <= 5.0 01:W1-LID 2.57 .001 1998.0424_17:35 220.99 n/a .000
05582> overflow <= 5.0 03:W1-LID-Out 6.35 .267 1998.0627_ 1:00 220.99 n/a .000
05583> {MxStoUsed=.1789E-01 m3, TotOvfVol=.1404E+01 m3, N-Ovf= 97, TotDurOvf= 104.hrs}
05584> R0098:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05585> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .321 1998.0627_ 1:00 218.10 .495 .000
05586> [XIMP=.65:TIMP=.70]
05587> [LOSS= 2 :CN= 71.0]
05588> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05589> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
05590> [IaREcimp= 1.50: IaRCper= 6.00]
05591> [SMIN= 41.38: SMAX=275.84: SK= .030]
05592> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
05593> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05594> # Total Volume provided by LID - 200 m3
05595> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05596> R0098:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05597> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .321 1998.0627_ 1:00 218.10 n/a .000
05598> out <= 5.0 01:W2-LID 2.93 .001 1998.0424_17:30 218.10 n/a .000
05599> overflow <= 5.0 03:W2-LID-Out 7.82 .317 1998.0627_ 1:00 218.10 n/a .000
05600> {MxStoUsed=.2000E-01 m3, TotOvfVol=.1705E+01 m3, N-Ovf= 102, TotDurOvf= 109.hrs}
05601> R0098:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05602> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .161 1998.0627_ 1:00 186.61 .424 .000
05603> [XIMP=.53:TIMP=.63]
05604> [LOSS= 2 :CN= 71.0]
05605> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05606> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
05607> [IaREcimp= 1.50: IaRCper= 6.00]

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05608> [SMIN= 41.38: SMAX=275.84: SK= .030]
05609> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
05610> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05611> # Total Volume provided by LID - 96 m³
05612> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05613> R0098:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05614> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .161 1998.0627_ 1:00 186.61 n/a .000
05615> out <= 5.0 01:W3-LID 1.61 .001 1998.0424_17:30 186.61 n/a .000
05616> overflow <= 5.0 03:W3-LID-Out 4.69 .159 1998.0627_ 1:00 186.61 n/a .000
05617> {MxStoUsed=.9600E-02 m3, TotOvfVol=.8746E+00 m3, N-Ovf= 105, TotDurOvf= 113.hrs}
05618> R0098:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05619> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .222 1998.0627_ 1:00 198.22 .450 .000
05620> [XIMP=.57:TIMP=.67]
05621> [LOSS= 2 :CN= 71.0]
05622> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05623> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
05624> [IaRECimp= 1.50: IaRECper= 6.00]
05625> [SMIN= 41.38: SMAX=275.84: SK= .030]
05626> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
05627> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05628> # Total Volume provided by LID - 131 m³
05629> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05630> R0098:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05631> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .222 1998.0627_ 1:00 198.22 n/a .000
05632> out <= 5.0 01:W4-LID 2.10 .001 1998.0424_17:30 198.22 n/a .000
05633> overflow <= 5.0 03:W4-LID-Out 6.08 .219 1998.0627_ 1:00 198.22 n/a .000
05634> {MxStoUsed=.1310E-01 m3, TotOvfVol=.1204E+01 m3, N-Ovf= 101, TotDurOvf= 113.hrs}
05635> R0098:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05636> ADD HYD 5.0 02:W1 8.92 .270 1998.0627_ 1:00 220.99 n/a .000
05637> + 5.0 02:W2 10.75 .321 1998.0627_ 1:00 218.10 n/a .000
05638> + 5.0 02:W3 6.30 .161 1998.0627_ 1:00 186.61 n/a .000
05639> + 5.0 02:W4 8.18 .222 1998.0627_ 1:00 198.22 n/a .000
05640> SUM= 5.0 01:BCD-PH3 34.15 .974 1998.0627_ 1:00 208.28 n/a .000
05641> R0098:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05642> ADD HYD 5.0 02:W1-LID-Out 6.35 .267 1998.0627_ 1:00 220.99 n/a .000
05643> + 5.0 02:W2-LID-Out 7.82 .317 1998.0627_ 1:00 218.10 n/a .000
05644> + 5.0 02:W3-LID-Out 4.69 .159 1998.0627_ 1:00 186.61 n/a .000
05645> + 5.0 02:W4-LID-Out 6.08 .219 1998.0627_ 1:00 198.22 n/a .000
05646> SUM= 5.0 01:BCD-PH3-LI 24.93 .962 1998.0627_ 1:00 208.07 n/a .000
05647> #*****
05648> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
05649> #*****
05650> # Set infiltration to 0 (CN = 99.99) for water balance analysis
05651> #*****
05652> R0098:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05653> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .355 1998.0627_ 1:00 271.31 .616 .000
05654> [XIMP=.66:TIMP=.71]
05655> [LOSS= 2 :CN=100.0]
05656> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05657> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
05658> [IaRECimp= 1.50: IaRECper= 6.00]
05659> [SMIN= 1.39: SMAX= 9.24: SK= .030]
05660> R0098:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05661> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .425 1998.0627_ 1:00 269.77 .613 .000
05662> [XIMP=.65:TIMP=.70]
05663> [LOSS= 2 :CN=100.0]
05664> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05665> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
05666> [IaRECimp= 1.50: IaRECper= 6.00]
05667> [SMIN= 1.39: SMAX= 9.24: SK= .030]
05668> R0098:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05669> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .247 1998.0627_ 1:00 259.04 .588 .000
05670> [XIMP=.53:TIMP=.63]
05671> [LOSS= 2 :CN=100.0]
05672> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05673> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
05674> [IaRECimp= 1.50: IaRECper= 6.00]
05675> [SMIN= 1.39: SMAX= 9.24: SK= .030]
05676> R0098:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05677> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .323 1998.0627_ 1:00 265.31 .603 .000
05678> [XIMP=.57:TIMP=.67]
05679> [LOSS= 2 :CN=100.0]
05680> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05681> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
05682> [IaRECimp= 1.50: IaRECper= 6.00]
05683> [SMIN= 1.39: SMAX= 9.24: SK= .030]
05684> R0098:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05685> ADD HYD 5.0 02:INF-W1 8.92 .355 1998.0627_ 1:00 271.31 n/a .000
05686> + 5.0 02:INF-W2 10.75 .425 1998.0627_ 1:00 269.77 n/a .000
05687> + 5.0 02:INF-W3 6.30 .247 1998.0627_ 1:00 259.04 n/a .000
05688> + 5.0 02:INF-W4 8.18 .323 1998.0627_ 1:00 265.32 n/a .000
05689> SUM= 5.0 01:INF-BCD-PH 34.15 1.351 1998.0627_ 1:00 267.12 n/a .000
05690> #####
05691> # CONTINUOUS RAINFALL DATA
05692> #####
05693> ** END OF RUN : 98
05694>
05695> *****
05696>

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05697>
05698>
05699>
05700>
05701> RUN#:COMMAND#
05702> R0099:C00001-----
05703> START
05704> [TZERO = .00 hrs on 19990101]
05705> [METOUT= 2 (1=imperial, 2=metric output)]
05706> [NSTORM= 0 ]
05707> [NRUN = 0099 ]
05708> #*****
05709> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
05710> #*****
05711> # Project Name: Barrhaven Conservancy Development
05712> # Project Number: 1474
05713> # Date : 2021/Oct/18
05714> # Modeller : J.Burnett, P.Eng.
05715> # Updated : 2022/Dec/13 [LP]
05716> # Company : J.F. Sabourin and Associates
05717> # License # : 2582634
05718> #*****
05719> # Ottawa International Airport (1967 - 2003)
05720> R0099:C00002-----
05721> * READ AES DATA
05722> [Filename = YOW_1967_2007.123 ]
05723> [Start_date= 1999.0101: End_date= 1999.1231]
05724> [DT= 60.min: Length= 4440.hrs: WetHrs= 247: DryHrs= 4193: PTOT= 424.40]
05725> Maximum average rainfall intensities over
05726> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
05727> 17.50 10.10 9.03 6.57 3.31 1.65 1.45 1.22 .97 mm/hr
05728> 17.50 20.20 27.10 39.40 39.70 39.70 52.20 58.60 69.50 mm
05729> 19990717 19990717 19990906 19990906 19990906 19990906 19990907 19990908 19990908 date
05730> Number of rainfall events per following interevent time
05731> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
05732> 102 80 70 63 56 39 31 28 18
05733> Number of events with at least the following durations
05734> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
05735> 101 57 31 10 1 0 0 0 0
05736> R0099:C00003-----
05737> COMPUTE API
05738> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
05739> [APImax= 69.51: APIavg= 23.97: APImin= 1.93]
05740> #*****
05741> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
05742> #*****
05743> R0099:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05744> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .296 1999.0717_15:00 224.02 .528 .000
05745> [XIMP=.66:TIMP=.71]
05746> [LOSS= 2 :CN= 71.0]
05747> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05748> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
05749> [IaRECimp= 1.50: IaRECper= 6.00]
05750> [SMIN= 41.38: SMAX=275.84: SK= .030]
05751> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
05752> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05753> # Total Volume provided by LID - 179 m³
05754> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05755> R0099:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05756> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .296 1999.0717_15:00 224.02 n/a .000
05757> out <= 5.0 01:W1-LID 2.24 .001 1999.0508_17:50 224.02 n/a .000
05758> overflow <= 5.0 03:W1-LID-Out 6.68 .293 1999.0717_15:00 224.02 n/a .000
05759> {MxStoUsed=.1789E-01 m3, TotOvfVol=.1497E+01 m3, N-Ovf= 96, TotDurOvf= 96.hrs}
05760> R0099:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05761> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .351 1999.0717_15:00 221.08 .521 .000
05762> [XIMP=.65:TIMP=.70]
05763> [LOSS= 2 :CN= 71.0]
05764> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05765> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
05766> [IaRECimp= 1.50: IaRECper= 6.00]
05767> [SMIN= 41.38: SMAX=275.84: SK= .030]
05768> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
05769> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05770> # Total Volume provided by LID - 200 m³
05771> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05772> R0099:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05773> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .351 1999.0717_15:00 221.08 n/a .000
05774> out <= 5.0 01:W2-LID 2.53 .001 1999.0508_17:40 221.08 n/a .000
05775> overflow <= 5.0 03:W2-LID-Out 8.22 .348 1999.0717_15:00 221.08 n/a .000
05776> {MxStoUsed=.2000E-01 m3, TotOvfVol=.1817E+01 m3, N-Ovf= 95, TotDurOvf= 101.hrs}
05777> R0099:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05778> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .176 1999.0717_15:00 189.03 .445 .000
05779> [XIMP=.53:TIMP=.63]
05780> [LOSS= 2 :CN= 71.0]
05781> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05782> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
05783> [IaRECimp= 1.50: IaRECper= 6.00]
05784> [SMIN= 41.38: SMAX=275.84: SK= .030]
05785> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)

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05786> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05787> # Total Volume provided by LID - 96 m³
05788> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05789> R0099:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05790> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .176 1999.0717_15:00 189.03 n/a .000
05791> out <= 5.0 01:W3-LID 1.38 .001 1999.0508_17:35 189.02 n/a .000
05792> overflow <= 5.0 03:W3-LID-Out 4.92 .174 1999.0717_15:00 189.03 n/a .000
05793> {MxStoUsed=.9598E-02 m3, TotOvfVol=.9294E+00 m3, N-Ovf= 105, TotDurOvf= 103.hrs}
05794> R0099:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05795> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .243 1999.0717_15:00 200.84 .473 .000
05796> [XIMP=.57:TIMP=.67]
05797> [LOSS= 2 :CN= 71.0]
05798> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05799> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
05800> [IaREcimp= 1.50: IaREcper= 6.00]
05801> [SMIN= 41.38: SMAX=275.84: SK= .030]
05802> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
05803> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05804> # Total Volume provided by LID - 131 m³
05805> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05806> R0099:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05807> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .243 1999.0717_15:00 200.84 n/a .000
05808> out <= 5.0 01:W4-LID 1.80 .001 1999.0508_17:35 200.84 n/a .000
05809> overflow <= 5.0 03:W4-LID-Out 6.38 .240 1999.0717_15:00 200.84 n/a .000
05810> {MxStoUsed=.1310E-01 m3, TotOvfVol=.1281E+01 m3, N-Ovf= 94, TotDurOvf= 104.hrs}
05811> R0099:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05812> ADD HYD 5.0 02:W1 8.92 .296 1999.0717_15:00 224.02 n/a .000
05813> + 5.0 02:W2 10.75 .351 1999.0717_15:00 221.08 n/a .000
05814> + 5.0 02:W3 6.30 .176 1999.0717_15:00 189.03 n/a .000
05815> + 5.0 02:W4 8.18 .243 1999.0717_15:00 200.84 n/a .000
05816> SUM= 5.0 01:BCD-PH3 34.15 1.066 1999.0717_15:00 211.09 n/a .000
05817> R0099:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05818> ADD HYD 5.0 02:W1-LID-Out 6.68 .293 1999.0717_15:00 224.02 n/a .000
05819> + 5.0 02:W2-LID-Out 8.22 .348 1999.0717_15:00 221.08 n/a .000
05820> + 5.0 02:W3-LID-Out 4.92 .174 1999.0717_15:00 189.03 n/a .000
05821> + 5.0 02:W4-LID-Out 6.38 .240 1999.0717_15:00 200.84 n/a .000
05822> SUM= 5.0 01:BCD-PH3-LI 26.20 1.055 1999.0717_15:00 210.89 n/a .000
05823> #*****
05824> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
05825> #*****
05826> # Set infiltration to 0 (CN = 99.99) for water balance analysis
05827> #*****
05828> R0099:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05829> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .391 1999.0717_15:00 277.73 .654 .000
05830> [XIMP=.66:TIMP=.71]
05831> [LOSS= 2 :CN=100.0]
05832> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05833> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
05834> [IaREcimp= 1.50: IaREcper= 6.00]
05835> [SMIN= 1.39: SMAX= 9.24: SK= .030]
05836> R0099:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05837> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .467 1999.0717_15:00 276.22 .651 .000
05838> [XIMP=.65:TIMP=.70]
05839> [LOSS= 2 :CN=100.0]
05840> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05841> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
05842> [IaREcimp= 1.50: IaREcper= 6.00]
05843> [SMIN= 1.39: SMAX= 9.24: SK= .030]
05844> R0099:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05845> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .276 1999.0717_15:00 266.49 .628 .000
05846> [XIMP=.53:TIMP=.63]
05847> [LOSS= 2 :CN=100.0]
05848> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05849> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
05850> [IaREcimp= 1.50: IaREcper= 6.00]
05851> [SMIN= 1.39: SMAX= 9.24: SK= .030]
05852> R0099:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05853> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .355 1999.0717_15:00 272.58 .642 .000
05854> [XIMP=.57:TIMP=.67]
05855> [LOSS= 2 :CN=100.0]
05856> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05857> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
05858> [IaREcimp= 1.50: IaREcper= 6.00]
05859> [SMIN= 1.39: SMAX= 9.24: SK= .030]
05860> R0099:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05861> ADD HYD 5.0 02:INF-W1 8.92 .391 1999.0717_15:00 277.73 n/a .000
05862> + 5.0 02:INF-W2 10.75 .467 1999.0717_15:00 276.22 n/a .000
05863> + 5.0 02:INF-W3 6.30 .276 1999.0717_15:00 266.49 n/a .000
05864> + 5.0 02:INF-W4 8.18 .355 1999.0717_15:00 272.58 n/a .000
05865> SUM= 5.0 01:INF-BCD-PH 34.15 1.489 1999.0717_15:00 273.94 n/a .000
05866> #####
05867> # CONTINUOUS RAINFALL DATA
05868> #####
05869> ** END OF RUN : 99
05870>
05871> *****
05872>
05873>
05874>

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05875>
05876>
05877> RUN#:COMMAND#
05878> R0100:C00001-----
05879> START
05880> [TZERO = .00 hrs on 20000101]
05881> [METOUT= 2 (1=imperial, 2=metric output)]
05882> [NSTORM= 0 ]
05883> [NRUN = 0100 ]
05884> #*****
05885> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
05886> #*****
05887> # Project Name: Barrhaven Conservancy Development
05888> # Project Number: 1474
05889> # Date : 2021/Oct/18
05890> # Modeller : J.Burnett, P.Eng.
05891> # Updated : 2022/Dec/13 [LP]
05892> # Company : J.F. Sabourin and Associates
05893> # License # : 2582634
05894> #*****
05895> # Ottawa International Airport (1967 - 2003)
05896> R0100:C00002-----
05897> * READ AES DATA
05898> [Filename = YOW_1967_2007.123 ]
05899> [Start_date= 2000.0101: End_date= 2000.1230]
05900> [DT= 60.min: Length= 5160.hrs: WetHrs= 401: DryHrs= 4759: PTOT= 535.90]
05901> Maximum average rainfall intensities over
05902> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
05903> 14.70 9.60 8.03 6.43 3.89 1.95 1.30 1.03 .84 mm/hr
05904> 14.70 19.20 24.10 38.60 46.70 46.70 46.80 49.30 60.40 mm
05905> 20000625 20000625 20000625 20000625 20000625 20000625 20000626 20000510 20000511 date
05906> Number of rainfall events per following interevent time
05907> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
05908> 156 125 110 86 67 46 34 30 23
05909> Number of events with at least the following durations
05910> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
05911> 155 82 49 16 2 0 0 0 0
05912> R0100:C00003-----
05913> COMPUTE API
05914> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
05915> [APImax= 76.65: APIavg= 25.66: APImin= 5.70]
05916> #*****
05917> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
05918> #*****
05919> R0100:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05920> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .307 2000.0625_10:00 278.30 .519 .000
05921> [XIMP=.66:TIMP=.71]
05922> [LOSS= 2 :CN= 71.0]
05923> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05924> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
05925> [IaRECimp= 1.50: IaRECper= 6.00]
05926> [SMIN= 41.38: SMAX=275.84: SK= .030]
05927> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
05928> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05929> # Total Volume provided by LID - 179 m3
05930> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05931> R0100:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05932> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .307 2000.0625_10:00 278.30 n/a .000
05933> out <= 5.0 01:W1-LID 2.33 .001 2000.0421_ 4:30 278.30 n/a .000
05934> overflow <= 5.0 03:W1-LID-Out 6.59 .302 2000.0625_10:00 278.30 n/a .000
05935> {MxStoUsed=.1789E+01 m3, TotOvfVol=.1835E+01 m3, N-Ovf= 92, TotDurOvf= 134.hrs}
05936> R0100:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05937> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .366 2000.0625_10:00 274.90 .513 .000
05938> [XIMP=.65:TIMP=.70]
05939> [LOSS= 2 :CN= 71.0]
05940> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05941> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
05942> [IaRECimp= 1.50: IaRECper= 6.00]
05943> [SMIN= 41.38: SMAX=275.84: SK= .030]
05944> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
05945> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05946> # Total Volume provided by LID - 200 m3
05947> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05948> R0100:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05949> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .366 2000.0625_10:00 274.90 n/a .000
05950> out <= 5.0 01:W2-LID 2.66 .001 2000.0421_ 4:25 274.90 n/a .000
05951> overflow <= 5.0 03:W2-LID-Out 8.09 .360 2000.0625_10:00 274.90 n/a .000
05952> {MxStoUsed=.2000E+01 m3, TotOvfVol=.2225E+01 m3, N-Ovf= 96, TotDurOvf= 139.hrs}
05953> R0100:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05954> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .206 2000.0625_10:00 238.49 .445 .000
05955> [XIMP=.53:TIMP=.63]
05956> [LOSS= 2 :CN= 71.0]
05957> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05958> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
05959> [IaRECimp= 1.50: IaRECper= 6.00]
05960> [SMIN= 41.38: SMAX=275.84: SK= .030]
05961> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
05962> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05963> # Total Volume provided by LID - 96 m3

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05964> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05965> R0100:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05966> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .206 2000.0625_10:00 238.49 n/a .000
05967> out <= 5.0 01:W3-LID 1.44 .001 2000.0421_ 4:20 238.49 n/a .000
05968> overflow <= 5.0 03:W3-LID-Out 4.86 .202 2000.0625_10:00 238.49 n/a .000
05969> {MxStoUsed=.9599E-02 m3, TotOvfVol=.1159E+01 m3, N-Ovf= 105, TotDurOvf= 140.hrs}
05970> R0100:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05971> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .273 2000.0625_10:00 252.42 .471 .000
05972> [XIMP=.57:TIMP=.67]
05973> [LOSS= 2 :CN= 71.0]
05974> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
05975> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
05976> [IaREcimp= 1.50: IaRECper= 6.00]
05977> [SMIN= 41.38: SMAX=275.84: SK= .030]
05978> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
05979> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
05980> # Total Volume provided by LID - 131 m³
05981> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05982> R0100:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05983> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .273 2000.0625_10:00 252.42 n/a .000
05984> out <= 5.0 01:W4-LID 1.89 .001 2000.0421_ 4:20 252.42 n/a .000
05985> overflow <= 5.0 03:W4-LID-Out 6.29 .268 2000.0625_10:00 252.42 n/a .000
05986> {MxStoUsed=.1310E-01 m3, TotOvfVol=.1589E+01 m3, N-Ovf= 104, TotDurOvf= 141.hrs}
05987> R0100:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05988> ADD HYD 5.0 02:W1 8.92 .307 2000.0625_10:00 278.30 n/a .000
05989> + 5.0 02:W2 10.75 .366 2000.0625_10:00 274.90 n/a .000
05990> + 5.0 02:W3 6.30 .206 2000.0625_10:00 238.49 n/a .000
05991> + 5.0 02:W4 8.18 .273 2000.0625_10:00 252.42 n/a .000
05992> SUM= 5.0 01:BCD-PH3 34.15 1.153 2000.0625_10:00 263.68 n/a .000
05993> R0100:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
05994> ADD HYD 5.0 02:W1-LID-Out 6.59 .302 2000.0625_10:00 278.30 n/a .000
05995> + 5.0 02:W2-LID-Out 8.09 .360 2000.0625_10:00 274.90 n/a .000
05996> + 5.0 02:W3-LID-Out 4.86 .202 2000.0625_10:00 238.49 n/a .000
05997> + 5.0 02:W4-LID-Out 6.29 .268 2000.0625_10:00 252.42 n/a .000
05998> SUM= 5.0 01:BCD-PH3-LI 25.84 1.132 2000.0625_10:00 263.44 n/a .000
05999> #*****
06000> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
06001> #*****
06002> # Set infiltration to 0 (CN = 99.99) for water balance analysis
06003> #*****
06004> R0100:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
06005> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .351 2000.0625_10:00 338.07 .631 .000
06006> [XIMP=.66:TIMP=.71]
06007> [LOSS= 2 :CN=100.0]
06008> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
06009> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
06010> [IaREcimp= 1.50: IaRECper= 6.00]
06011> [SMIN= 1.39: SMAX= 9.24: SK= .030]
06012> R0100:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
06013> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .421 2000.0625_10:00 336.31 .628 .000
06014> [XIMP=.65:TIMP=.70]
06015> [LOSS= 2 :CN=100.0]
06016> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
06017> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
06018> [IaREcimp= 1.50: IaRECper= 6.00]
06019> [SMIN= 1.39: SMAX= 9.24: SK= .030]
06020> R0100:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
06021> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .246 2000.0625_10:00 323.88 .604 .000
06022> [XIMP=.53:TIMP=.63]
06023> [LOSS= 2 :CN=100.0]
06024> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
06025> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
06026> [IaREcimp= 1.50: IaRECper= 6.00]
06027> [SMIN= 1.39: SMAX= 9.24: SK= .030]
06028> R0100:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
06029> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .320 2000.0625_10:00 331.13 .618 .000
06030> [XIMP=.57:TIMP=.67]
06031> [LOSS= 2 :CN=100.0]
06032> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
06033> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
06034> [IaREcimp= 1.50: IaRECper= 6.00]
06035> [SMIN= 1.39: SMAX= 9.24: SK= .030]
06036> R0100:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
06037> ADD HYD 5.0 02:INF-W1 8.92 .351 2000.0625_10:00 338.07 n/a .000
06038> + 5.0 02:INF-W2 10.75 .421 2000.0625_10:00 336.31 n/a .000
06039> + 5.0 02:INF-W3 6.30 .246 2000.0625_10:00 323.88 n/a .000
06040> + 5.0 02:INF-W4 8.18 .320 2000.0625_10:00 331.13 n/a .000
06041> SUM= 5.0 01:INF-BCD-PH 34.15 1.338 2000.0625_10:00 333.24 n/a .000
06042> #####
06043> # CONTINUOUS RAINFALL DATA
06044> #####
06045> ** END OF RUN : 101
06046>
06047> *****
06048>
06049>
06050>
06051>
06052>

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06053> RUN#:COMMAND#
06054> R0102:C00001-----
06055> START
06056> [TZERO = .00 hrs on 20020101]
06057> [METOUT= 2 (1=imperial, 2=metric output)]
06058> [NSTORM= 0 ]
06059> [NRUN = 0102 ]
06060> #*****
06061> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
06062> #*****
06063> # Project Name: Barrhaven Conservancy Development
06064> # Project Number: 1474
06065> # Date : 2021/Oct/18
06066> # Modeller : J.Burnett, P.Eng.
06067> # Updated : 2022/Dec/13 [LP]
06068> # Company : J.F. Sabourin and Associates
06069> # License # : 2582634
06070> #*****
06071> # Ottawa International Airport (1967 - 2003)
06072> R0102:C00002-----
06073> * READ AES DATA
06074> [Filename = YOW_1967_2007.123 ]
06075> [Start_date= 2002.0101: End_date= 2002.1231]
06076> {DT= 60.min: Length= 5088.hrs: WetHrs= 304: DryHrs= 4784: PTOT= 551.50}
06077> Maximum average rainfall intensities over
06078> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
06079> 45.00 26.75 18.40 9.48 4.74 2.48 2.08 1.56 1.04 mm/hr
06080> 45.00 53.50 55.20 56.90 56.90 59.50 74.90 74.90 74.90 mm
06081> 20020627 20020627 20020627 20020627 20020627 20020627 20020628 20020629 date
06082> Number of rainfall events per following interevent time
06083> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
06084> 100 83 78 56 47 41 36 34 25
06085> Number of events with at least the following durations
06086> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
06087> 100 59 33 13 5 0 0 0 0
06088> R0102:C00003-----
06089> COMPUTE API
06090> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
06091> [APImax=114.06: APIavg= 26.37: APImin= 4.40]
06092> #*****
06093> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
06094> #*****
06095> R0102:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
06096> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .978 2002.0627_14:00 331.06 .600 .000
06097> [XIMP=.66:TIMP=.71]
06098> [LOSS= 2 :CN= 71.0]
06099> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
06100> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
06101> [IaRECimp= 1.50: IaRECper= 6.00]
06102> [SMIN= 41.38: SMAX=275.84: SK= .030]
06103> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
06104> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
06105> # Total Volume provided by LID - 179 m³
06106> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
06107> R0102:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
06108> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .978 2002.0627_14:00 331.06 n/a .000
06109> out <= 5.0 01:W1-LID 1.68 .001 2002.0412_23:20 331.07 n/a .000
06110> overflow <= 5.0 03:W1-LID-Out 7.24 .954 2002.0627_14:00 331.06 n/a .000
06111> {MxStoUsed=.1790E-01 m3, TotOvfVol=.2397E+01 m3, N-Ovf= 79, TotDurOvf= 141.hrs}
06112> R0102:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
06113> CONTINUOUS STANDHYD 5.0 01:W2 10.75 1.171 2002.0627_14:00 327.38 .594 .000
06114> [XIMP=.65:TIMP=.70]
06115> [LOSS= 2 :CN= 71.0]
06116> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
06117> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
06118> [IaRECimp= 1.50: IaRECper= 6.00]
06119> [SMIN= 41.38: SMAX=275.84: SK= .030]
06120> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
06121> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
06122> # Total Volume provided by LID - 200 m³
06123> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
06124> R0102:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
06125> ROUTE RESERVOIR -> 5.0 02:W2 10.75 1.171 2002.0627_14:00 327.38 n/a .000
06126> out <= 5.0 01:W2-LID 1.89 .001 2002.0412_23:20 327.38 n/a .000
06127> overflow <= 5.0 03:W2-LID-Out 8.86 1.140 2002.0627_14:00 327.38 n/a .000
06128> {MxStoUsed=.2000E-01 m3, TotOvfVol=.2899E+01 m3, N-Ovf= 85, TotDurOvf= 143.hrs}
06129> R0102:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
06130> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .669 2002.0627_14:00 290.95 .528 .000
06131> [XIMP=.53:TIMP=.63]
06132> [LOSS= 2 :CN= 71.0]
06133> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
06134> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
06135> [IaRECimp= 1.50: IaRECper= 6.00]
06136> [SMIN= 41.38: SMAX=275.84: SK= .030]
06137> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
06138> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
06139> # Total Volume provided by LID - 96 m³
06140> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
06141> R0102:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms

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06142> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .669 2002.0627_14:00 290.95 n/a .000
06143> out <= 5.0 01:W3-LID 1.00 .001 2002.0412_23:15 290.96 n/a .000
06144> overflow <= 5.0 03:W3-LID-Out 5.30 .644 2002.0627_14:00 290.95 n/a .000
06145> {MxStoUsed=.9599E-02 m3, TotOvfVol=.1541E+01 m3, N-Ovf= 87, TotDurOvf= 146.hrs}
06146> R0102:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
06147> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .882 2002.0627_14:00 305.09 .553 .000
06148> [XIMP=.57:TIMP=.67]
06149> [LOSS= 2 :CN= 71.0]
06150> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
06151> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
06152> [IaRECImp= 1.50: IaRECper= 6.00]
06153> [SMIN= 41.38: SMAX=275.84: SK= .030]
06154> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
06155> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
06156> # Total Volume provided by LID - 131 m³
06157> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
06158> R0102:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
06159> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .882 2002.0627_14:00 305.09 n/a .000
06160> out <= 5.0 01:W4-LID 1.32 .001 2002.0412_23:15 305.09 n/a .000
06161> overflow <= 5.0 03:W4-LID-Out 6.86 .853 2002.0627_14:00 305.09 n/a .000
06162> {MxStoUsed=.1310E-01 m3, TotOvfVol=.2094E+01 m3, N-Ovf= 82, TotDurOvf= 147.hrs}
06163> R0102:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
06164> ADD HYD 5.0 02:W1 8.92 .978 2002.0627_14:00 331.06 n/a .000
06165> + 5.0 02:W2 10.75 1.171 2002.0627_14:00 327.38 n/a .000
06166> + 5.0 02:W3 6.30 .669 2002.0627_14:00 290.95 n/a .000
06167> + 5.0 02:W4 8.18 .882 2002.0627_14:00 305.09 n/a .000
06168> SUM= 5.0 01:BCD-PH3 34.15 3.700 2002.0627_14:00 316.28 n/a .000
06169> R0102:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
06170> ADD HYD 5.0 02:W1-LID-Out 7.24 .954 2002.0627_14:00 331.06 n/a .000
06171> + 5.0 02:W2-LID-Out 8.86 1.140 2002.0627_14:00 327.38 n/a .000
06172> + 5.0 02:W3-LID-Out 5.30 .644 2002.0627_14:00 290.95 n/a .000
06173> + 5.0 02:W4-LID-Out 6.86 .853 2002.0627_14:00 305.09 n/a .000
06174> SUM= 5.0 01:BCD-PH3-LI 28.26 3.592 2002.0627_14:00 316.08 n/a .000
06175> #*****
06176> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
06177> #*****
06178> # Set infiltration to 0 (CN = 99.99) for water balance analysis
06179> #*****
06180> R0102:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
06181> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 1.105 2002.0627_14:00 401.51 .728 .000
06182> [XIMP=.66:TIMP=.71]
06183> [LOSS= 2 :CN=100.0]
06184> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
06185> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
06186> [IaRECImp= 1.50: IaRECper= 6.00]
06187> [SMIN= 1.39: SMAX= 9.24: SK= .030]
06188> R0102:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
06189> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 1.330 2002.0627_14:00 399.97 .725 .000
06190> [XIMP=.65:TIMP=.70]
06191> [LOSS= 2 :CN=100.0]
06192> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
06193> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
06194> [IaRECImp= 1.50: IaRECper= 6.00]
06195> [SMIN= 1.39: SMAX= 9.24: SK= .030]
06196> R0102:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
06197> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .781 2002.0627_14:00 390.15 .707 .000
06198> [XIMP=.53:TIMP=.63]
06199> [LOSS= 2 :CN=100.0]
06200> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
06201> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
06202> [IaRECImp= 1.50: IaRECper= 6.00]
06203> [SMIN= 1.39: SMAX= 9.24: SK= .030]
06204> R0102:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
06205> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 1.013 2002.0627_14:00 396.36 .719 .000
06206> [XIMP=.57:TIMP=.67]
06207> [LOSS= 2 :CN=100.0]
06208> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
06209> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
06210> [IaRECImp= 1.50: IaRECper= 6.00]
06211> [SMIN= 1.39: SMAX= 9.24: SK= .030]
06212> R0102:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
06213> ADD HYD 5.0 02:INF-W1 8.92 1.105 2002.0627_14:00 401.51 n/a .000
06214> + 5.0 02:INF-W2 10.75 1.330 2002.0627_14:00 399.97 n/a .000
06215> + 5.0 02:INF-W3 6.30 .781 2002.0627_14:00 390.15 n/a .000
06216> + 5.0 02:INF-W4 8.18 1.013 2002.0627_14:00 396.36 n/a .000
06217> SUM= 5.0 01:INF-BCD-PH 34.15 4.228 2002.0627_14:00 397.70 n/a .000
06218> #*****
06219> # CONTINUOUS RAINFALL DATA
06220> #*****
06221> ** END OF RUN : 102
06222>
06223> *****
06224>
06225>
06226>
06227>
06228>
06229> RUN#:COMMAND#
06230> R0103:C00001-----

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06231> START
06232> [TZERO = .00 hrs on 20030101]
06233> [METOUT= 2 (1=imperial, 2=metric output)]
06234> [NSTORM= 0 ]
06235> [NRUN = 0103 ]
06236> #*****
06237> # SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
06238> #*****
06239> # Project Name: Barrhaven Conservancy Development
06240> # Project Number: 1474
06241> # Date : 2021/Oct/18
06242> # Modeller : J.Burnett, P.Eng.
06243> # Updated : 2022/Dec/13 [LP]
06244> # Company : J.F. Sabourin and Associates
06245> # License # : 2582634
06246> #*****
06247> # Ottawa International Airport (1967 - 2003)
06248> R0103:C00002-----
06249> * READ AES DATA
06250> [Filename = YOW_1967_2007.123 ]
06251> [Start_date= 2003.0101: End_date= 2003.1231]
06252> {DT= 60.min: Length= 4440.hrs: WetHrs= 406: DryHrs= 4034: PTOT= 554.60}
06253> Maximum average rainfall intensities over
06254> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
06255> 15.10 10.00 7.13 4.28 3.18 1.86 1.25 .94 .81 mm/hr
06256> 15.10 20.00 21.40 25.70 38.20 44.60 44.90 45.10 58.30 mm
06257> 20030711 20030711 20030711 20030711 20031021 20031015 20030525 20030526 20030527 date
06258> Number of rainfall events per following interevent time
06259> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
06260> 145 127 109 86 64 45 38 25 15
06261> Number of events with at least the following durations
06262> 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
06263> 144 80 43 13 5 1 0 0 0
06264> R0103:C00003-----
06265> COMPUTE API
06266> [APIini= 50.00: APIkdy= .9000: APIkdt= .9956]
06267> [APImax= 72.10: APIavg= 28.54: APImin= 4.70]
06268> #*****
06269> # Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITION
06270> #*****
06271> R0103:C00004-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
06272> CONTINUOUS STANDHYD 5.0 01:W1 8.92 .297 2003.0711_17:00 305.89 .552 .000
06273> [XIMP=.66:TIMP=.71]
06274> [LOSS= 2 :CN= 71.0]
06275> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
06276> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
06277> [IaREcimp= 1.50: IaRECper= 6.00]
06278> [SMIN= 41.38: SMAX=275.84: SK= .030]
06279> # LID for Outlet W1 (26 catchbasins, 30 m long trench each)
06280> # Assumed 780 m long trench 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
06281> # Total Volume provided by LID - 179 m³
06282> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
06283> R0103:C00005-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
06284> ROUTE RESERVOIR -> 5.0 02:W1 8.92 .297 2003.0711_17:00 305.89 n/a .000
06285> out <= 5.0 01:W1-LID 2.30 .001 2003.0501_10:25 305.90 n/a .000
06286> overflow <= 5.0 03:W1-LID-Out 6.62 .292 2003.0711_17:00 305.89 n/a .000
06287> {MxStoUsed=.1790E-01 m3, TotOvfVol=.2026E+01 m3, N-Ovf= 97, TotDurOvf= 161.hrs}
06288> R0103:C00006-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
06289> CONTINUOUS STANDHYD 5.0 01:W2 10.75 .350 2003.0711_17:00 302.35 .545 .000
06290> [XIMP=.65:TIMP=.70]
06291> [LOSS= 2 :CN= 71.0]
06292> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
06293> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
06294> [IaREcimp= 1.50: IaRECper= 6.00]
06295> [SMIN= 41.38: SMAX=275.84: SK= .030]
06296> # LID for Outlet W2 (29 catchbasins, 30 m long trench each)
06297> # Assumed 870 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
06298> # Total Volume provided by LID - 200 m³
06299> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
06300> R0103:C00007-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
06301> ROUTE RESERVOIR -> 5.0 02:W2 10.75 .350 2003.0711_17:00 302.35 n/a .000
06302> out <= 5.0 01:W2-LID 2.62 .001 2003.0501_10:15 302.34 n/a .000
06303> overflow <= 5.0 03:W2-LID-Out 8.13 .345 2003.0711_17:00 302.35 n/a .000
06304> {MxStoUsed=.2000E-01 m3, TotOvfVol=.2457E+01 m3, N-Ovf= 103, TotDurOvf= 166.hrs}
06305> R0103:C00008-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
06306> CONTINUOUS STANDHYD 5.0 01:W3 6.30 .194 2003.0711_17:00 265.05 .478 .000
06307> [XIMP=.53:TIMP=.63]
06308> [LOSS= 2 :CN= 71.0]
06309> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
06310> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
06311> [IaREcimp= 1.50: IaRECper= 6.00]
06312> [SMIN= 41.38: SMAX=275.84: SK= .030]
06313> # LID for Outlet W3 (14 catchbasins, 30 m long trench each)
06314> # Assumed 420 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
06315> # Total Volume provided by LID - 96 m³
06316> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
06317> R0103:C00009-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C---DWFcms
06318> ROUTE RESERVOIR -> 5.0 02:W3 6.30 .194 2003.0711_17:00 265.05 n/a .000
06319> out <= 5.0 01:W3-LID 1.40 .001 2003.0501_ 5:30 265.06 n/a .000

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06320>          overflow <= 5.0 03:W3-LID-Out 4.90 .189 2003.0711_17:00 265.05 n/a .000
06321> {MxStoUsed=.9599E-02 m3, TotOvfVol=.1298E+01 m3, N-Ovf= 101, TotDurOvf= 167.hrs}
06322> R0103:C00010-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
06323> CONTINUOUS STANDHYD 5.0 01:W4 8.18 .260 2003.0711_17:00 279.28 .504 .000
06324> [XIMP=.57:TIMP=.67]
06325> [LOSS= 2 :CN= 71.0]
06326> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
06327> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
06328> [IaRECimp= 1.50: IaRECper= 6.00]
06329> [SMIN= 41.38: SMAX=275.84: SK= .030]
06330> # LID for Outlet W4 (26 catchbasins, 30 m long trench each)
06331> # Assumed 570 m long trench, 1.25 m wide by 0.40 m deep, porosity of 0.40 with 250 mm diameter perforated pipe
06332> # Total Volume provided by LID - 131 m³
06333> # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
06334> R0103:C00011-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
06335> ROUTE RESERVOIR -> 5.0 02:W4 8.18 .260 2003.0711_17:00 279.28 n/a .000
06336> out <= 5.0 01:W4-LID 1.85 .001 2003.0501_ 5:10 279.28 n/a .000
06337> overflow <= 5.0 03:W4-LID-Out 6.33 .254 2003.0711_17:00 279.28 n/a .000
06338> {MxStoUsed=.1309E-01 m3, TotOvfVol=.1769E+01 m3, N-Ovf= 103, TotDurOvf= 169.hrs}
06339> R0103:C00012-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
06340> ADD HYD 5.0 02:W1 8.92 .297 2003.0711_17:00 305.89 n/a .000
06341> + 5.0 02:W2 10.75 .350 2003.0711_17:00 302.35 n/a .000
06342> + 5.0 02:W3 6.30 .194 2003.0711_17:00 265.05 n/a .000
06343> + 5.0 02:W4 8.18 .260 2003.0711_17:00 279.28 n/a .000
06344> SUM= 5.0 01:BCD-PH3 34.15 1.100 2003.0711_17:00 290.87 n/a .000
06345> R0103:C00013-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
06346> ADD HYD 5.0 02:W1-LID-Out 6.62 .292 2003.0711_17:00 305.89 n/a .000
06347> + 5.0 02:W2-LID-Out 8.13 .345 2003.0711_17:00 302.35 n/a .000
06348> + 5.0 02:W3-LID-Out 4.90 .189 2003.0711_17:00 265.05 n/a .000
06349> + 5.0 02:W4-LID-Out 6.33 .254 2003.0711_17:00 279.28 n/a .000
06350> SUM= 5.0 01:BCD-PH3-LI 25.98 1.080 2003.0711_17:00 290.60 n/a .000
06351> #*****
06352> # Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDIT
06353> #*****
06354> # Set infiltration to 0 (CN = 99.99) for water balance analysis
06355> #*****
06356> R0103:C00014-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
06357> CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .361 2003.0711_17:00 370.85 .669 .000
06358> [XIMP=.66:TIMP=.71]
06359> [LOSS= 2 :CN=100.0]
06360> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
06361> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 244.:MNI=.013:SCI= .0]
06362> [IaRECimp= 1.50: IaRECper= 6.00]
06363> [SMIN= 1.39: SMAX= 9.24: SK= .030]
06364> R0103:C00015-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
06365> CONTINUOUS STANDHYD 5.0 01:INF-W2 10.75 .433 2003.0711_17:00 369.11 .666 .000
06366> [XIMP=.65:TIMP=.70]
06367> [LOSS= 2 :CN=100.0]
06368> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
06369> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 268.:MNI=.013:SCI= .0]
06370> [IaRECimp= 1.50: IaRECper= 6.00]
06371> [SMIN= 1.39: SMAX= 9.24: SK= .030]
06372> R0103:C00016-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
06373> CONTINUOUS STANDHYD 5.0 01:INF-W3 6.30 .254 2003.0711_17:00 356.89 .644 .000
06374> [XIMP=.53:TIMP=.63]
06375> [LOSS= 2 :CN=100.0]
06376> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
06377> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 205.:MNI=.013:SCI= .0]
06378> [IaRECimp= 1.50: IaRECper= 6.00]
06379> [SMIN= 1.39: SMAX= 9.24: SK= .030]
06380> R0103:C00017-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
06381> CONTINUOUS STANDHYD 5.0 01:INF-W4 8.18 .330 2003.0711_17:00 363.86 .656 .000
06382> [XIMP=.57:TIMP=.67]
06383> [LOSS= 2 :CN=100.0]
06384> [Pervious area: IAper= 4.67:SLPP=2.00:LGP= 40.:MNP=.250:SCP= .0]
06385> [Impervious area: IAimp= 1.57:SLPI= .50:LGI= 234.:MNI=.013:SCI= .0]
06386> [IaRECimp= 1.50: IaRECper= 6.00]
06387> [SMIN= 1.39: SMAX= 9.24: SK= .030]
06388> R0103:C00018-----DTmin-ID:NHYD-----AREAha-QPEAKcms-TpeakDate_hh:mm---RVmm-R.C.---DWFcms
06389> ADD HYD 5.0 02:INF-W1 8.92 .361 2003.0711_17:00 370.85 n/a .000
06390> + 5.0 02:INF-W2 10.75 .433 2003.0711_17:00 369.11 n/a .000
06391> + 5.0 02:INF-W3 6.30 .254 2003.0711_17:00 356.89 n/a .000
06392> + 5.0 02:INF-W4 8.18 .330 2003.0711_17:00 363.86 n/a .000
06393> SUM= 5.0 01:INF-BCD-PH 34.15 1.378 2003.0711_17:00 366.05 n/a .000
06394> #####
06395> # CONTINUOUS RAINFALL DATA
06396> #####
06397> R0103:C00002-----
06398> FINISH
06399> -----
06400> *****
06401> WARNINGS / ERRORS / NOTES
06402> -----
06403> R0067:C00002 READ AES DATA
06404> *** WARNING: Requested start date is less than start date in file.
06405> *** WARNING: Missing rainfall increments were set to 0.
06406> *** WARNING: Missing rainfall increments were set to 0.
06407> *** WARNING: Missing rainfall increments were set to 0.
06408> *** WARNING: Missing rainfall increments were set to 0.

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06409> *** WARNING: Missing rainfall increments were set to 0.
06410> *** WARNING: Missing rainfall increments were set to 0.
06411> *** WARNING: Missing rainfall increments were set to 0.
06412> *** WARNING: Missing rainfall increments were set to 0.
06413> *** WARNING: Missing rainfall increments were set to 0.
06414> *** WARNING: Missing rainfall increments were set to 0.
06415> *** WARNING: Requested start date is less than start date in file.
06416> *** WARNING: Missing rainfall increments were set to 0.
06417> *** WARNING: Missing rainfall increments were set to 0.
06418> *** WARNING: Missing rainfall increments were set to 0.
06419> *** WARNING: Missing rainfall increments were set to 0.
06420> *** WARNING: Missing rainfall increments were set to 0.
06421> *** WARNING: Missing rainfall increments were set to 0.
06422> *** WARNING: Missing rainfall increments were set to 0.
06423> *** WARNING: Missing rainfall increments were set to 0.
06424> *** WARNING: Missing rainfall increments were set to 0.
06425> *** WARNING: Missing rainfall increments were set to 0.
06426> *** WARNING: Requested start date is less than start date in file.
06427> *** WARNING: Missing rainfall increments were set to 0.
06428> *** WARNING: Missing rainfall increments were set to 0.
06429> *** WARNING: Missing rainfall increments were set to 0.
06430> *** WARNING: Requested start date is less than start date in file.
06431> *** WARNING: Missing rainfall increments were set to 0.
06432> *** WARNING: Missing rainfall increments were set to 0.
06433> *** WARNING: Missing rainfall increments were set to 0.
06434> *** WARNING: Missing rainfall increments were set to 0.
06435> *** WARNING: Missing rainfall increments were set to 0.
06436> *** WARNING: Missing rainfall increments were set to 0.
06437> *** WARNING: Requested start date is less than start date in file.
06438> *** WARNING: Missing rainfall increments were set to 0.
06439> *** WARNING: Missing rainfall increments were set to 0.
06440> *** WARNING: Requested start date is less than start date in file.
06441> *** WARNING: Missing rainfall increments were set to 0.
06442> *** WARNING: Requested start date is less than start date in file.
06443> *** WARNING: Missing rainfall increments were set to 0.
06444> *** WARNING: Requested start date is less than start date in file.
06445> *** WARNING: Missing rainfall increments were set to 0.
06446> *** WARNING: Requested start date is less than start date in file.
06447> *** WARNING: Missing rainfall increments were set to 0.
06448> *** WARNING: Requested start date is less than start date in file.
06449> *** WARNING: Missing rainfall increments were set to 0.
06450> Simulation ended on 2022-12-13 at 12:44:35
06451> =====
06452>
06453>

Attachment B

Water Budget Results

Table B1: BCD West - Pre Development Water Budget

Year	Total Rainfall		Evaporation		Runoff		Infiltration	
	(mm)	(m ³)	(mm)	(m ³)	(mm)	(m ³)	(mm)	(m ³)
1967	386.9	132,126	196.7	67,170	67.6	23,082	122.6	41,875
1968	592.8	202,441	335.4	114,539	73.2	24,988	184.2	62,915
1969	570.3	194,757	336.6	114,949	60.0	20,487	173.7	59,322
1970	558.9	190,864	336.4	114,891	57.1	19,506	165.4	56,467
1971	522.1	178,297	340.3	116,206	43.0	14,698	138.8	47,393
1972	784.3	267,838	408.9	139,636	130.5	44,569	244.9	83,633
1973	744.9	254,383	407.2	139,072	96.4	32,910	241.3	82,401
1974	386.2	131,887	266.4	90,972	26.1	8,913	93.7	32,002
1975	535.5	182,873	316.0	107,911	58.0	19,800	161.5	55,162
1976	493.2	168,428	323.2	110,356	40.0	13,653	130.1	44,419
1977	677.8	231,469	393.9	134,531	76.2	26,033	207.6	70,906
1978	641.4	219,038	371.6	126,888	58.3	19,920	211.5	72,231
1979	866.5	295,910	417.2	142,481	151.6	51,785	297.6	101,644
1980	622	212,413	367.9	125,621	63.3	21,607	190.9	65,186
1981	936.4	319,781	476.7	162,793	189.6	64,759	270.1	92,229
1982	596.1	203,568	367.4	125,471	51.2	17,471	177.5	60,626
1983	587.5	200,631	370.2	126,423	55.9	19,090	161.4	55,118
1984	459.4	156,885	252.2	86,123	53.9	18,421	153.3	52,342
1985	559.9	191,206	297.6	101,634	57.0	19,472	205.3	70,100
1986	849.4	290,070	431.3	147,303	156.2	53,339	261.9	89,429
1987	640.1	218,594	399.8	136,542	73.4	25,080	166.8	56,972
1988	643.8	219,858	388.1	132,533	71.8	24,509	183.9	62,816
1989	523.2	178,673	325.5	111,162	45.0	15,357	152.7	52,154
1990	727.8	248,544	415.9	142,033	91.7	31,302	220.2	75,209
1991	556	189,874	358.1	122,295	49.9	17,041	148.0	50,539
1992	732.8	250,251	406.4	138,796	101.6	34,707	224.7	76,749
1993	721.3	246,324	457.0	156,079	67.7	23,116	196.6	67,129
1994	540.2	184,478	312.8	106,821	64.5	22,010	163.0	55,647
1995	538.5	183,898	211.2	72,108	166.6	56,908	160.7	54,882
1996	512.2	174,916	317.1	108,303	50.4	17,215	144.7	49,398
1997	433.2	147,938	271.6	92,758	30.5	10,399	131.1	44,781
1998	440.3	150,362	277.2	94,664	35.5	12,130	127.6	43,569
1999	424.4	144,933	252.7	86,294	36.4	12,437	135.3	46,202
2000	535.9	183,010	321.3	109,707	60.7	20,719	154.0	52,584
2002	551.5	188,337	257.5	87,923	109.7	37,459	184.4	62,956
2003	554.6	189,396	302.7	103,379	81.9	27,959	170.0	58,058
Minimum	386.2	131,887	196.7	67,170	26.1	8,913	93.7	32,002
Maximum	936.4	319,781	476.7	162,793	189.6	64,759	297.6	101,644
Average	595.8	203,451	341.3	116,566	75.1	25,635	179.4	61,251
Percentage	100.0%	100.0%	57.3%	57.3%	12.6%	12.6%	30.1%	30.1%

Table B2: BCD Phase 3 - Post Development Water Budget - Without LIDs

Year	Total Rainfall		Runoff (No Infiltration)		Evaporation		Runoff		Infiltration	
	(mm)	(m ³)	(mm)	(m ³)	(mm)	(m ³)	(mm)	(m ³)	(mm)	(m ³)
1967	386.9	132,126	268.53	91,703	118.4	40,423	214.6	73,279	54.0	18,424
1968	592.8	202,441	387.03	132,171	205.8	70,270	304.3	103,908	82.8	28,263
1969	570.3	194,757	356.79	121,844	213.5	72,914	278.5	95,098	78.3	26,746
1970	558.9	190,864	348.80	119,115	210.1	71,749	273.0	93,223	75.8	25,893
1971	522.1	178,297	308.29	105,281	213.8	73,016	243.4	83,111	64.9	22,170
1972	784.3	267,838	536.57	183,239	247.7	84,600	427.1	145,858	109.5	37,381
1973	744.9	254,383	487.97	166,642	256.9	87,742	380.3	129,859	107.7	36,783
1974	386.2	131,887	217.52	74,283	168.7	57,604	172.6	58,957	44.9	15,327
1975	535.5	182,873	343.90	117,442	191.6	65,431	269.0	91,877	74.9	25,565
1976	493.2	168,428	287.00	98,011	206.2	70,417	226.3	77,264	60.8	20,746
1977	677.8	231,469	440.41	150,400	237.4	81,069	345.3	117,920	95.1	32,480
1978	641.4	219,038	423.01	144,458	218.4	74,580	327.0	111,671	96.0	32,787
1979	866.5	295,910	614.07	209,705	252.4	86,205	483.3	165,030	130.8	44,675
1980	622	212,413	402.39	137,416	219.6	74,997	314.9	107,535	87.5	29,881
1981	936.4	319,781	643.29	219,684	293.1	100,097	522.0	178,266	121.3	41,417
1982	596.1	203,568	382.43	130,600	213.7	72,968	299.9	102,423	82.5	28,177
1983	587.5	200,631	364.45	124,460	223.1	76,172	288.9	98,659	75.6	25,800
1984	459.4	156,885	309.41	105,664	150.0	51,222	240.7	82,182	68.8	23,482
1985	559.9	191,206	387.27	132,253	172.6	58,953	295.9	101,033	91.4	31,220
1986	849.4	290,070	589.63	201,359	259.8	88,711	473.1	161,574	116.5	39,785
1987	640.1	218,594	393.29	134,309	246.8	84,286	315.3	107,682	78.0	26,627
1988	643.8	219,858	399.91	136,569	243.9	83,288	316.5	108,085	83.4	28,485
1989	523.2	178,673	322.82	110,243	200.4	68,430	252.4	86,191	70.4	24,052
1990	727.8	248,544	466.26	159,228	261.5	89,316	367.2	125,395	99.1	33,832
1991	556	189,874	340.77	116,373	215.2	73,501	271.7	92,782	69.1	23,591
1992	732.8	250,251	481.05	164,279	251.8	85,973	380.0	129,777	101.0	34,502
1993	721.3	246,324	446.40	152,446	274.9	93,878	355.2	121,287	91.2	31,158
1994	540.2	184,478	348.80	119,115	191.4	65,363	274.1	93,605	74.7	25,510
1995	538.5	183,898	409.85	139,964	128.7	43,934	340.3	116,216	69.5	23,748
1996	512.2	174,916	320.53	109,461	191.7	65,455	253.6	86,601	66.9	22,860
1997	433.2	147,938	274.18	93,632	159.0	54,305	212.7	72,623	61.5	21,009
1998	440.3	150,362	267.12	91,221	173.2	59,141	208.3	71,128	58.8	20,094
1999	424.4	144,933	273.94	93,551	150.5	51,382	211.1	72,087	62.9	21,463
2000	535.9	183,010	333.24	113,801	202.7	69,208	263.7	90,047	69.6	23,755
2002	551.5	188,337	397.70	135,815	153.8	52,523	316.3	108,010	81.4	27,805
2003	554.6	189,396	366.05	125,006	188.6	64,390	290.9	99,332	75.2	25,674
Minimum	386.2	131,887	218	74283	118.4	40,423	172.6	58,957	44.9	15,327
Maximum	936.4	319,781	643	219684	293.1	100,097	522.0	178,266	130.8	44,675
Average	595.8	203,451	387	132243	208.5	71,209	305.8	104,433	81.4	27,810
Percentage	100.0%	100.0%	65.0%	65.0%	35.0%	35.0%	51.3%	51.3%	13.7%	13.7%

Table B3: BCD Phase 3- Post Development Water Budget - With LIDs

Year	Total Rainfall		Runoff (No Infiltration)		Evaporation		Runoff		Infiltration	
	(mm)	(m ³)	(mm)	(m ³)	(mm)	(m ³)	(mm)	(m ³)	(mm)	(m ³)
1967	386.9	132,126	268.53	91,703	118.4	40,423	173.2	59,140	95.4	32,563
1968	592.8	202,441	387.03	132,171	205.8	70,270	225.8	77,115	161.2	55,056
1969	570.3	194,757	356.79	121,844	213.5	72,914	206.4	70,498	150.4	51,345
1970	558.9	190,864	348.80	119,115	210.1	71,749	202.9	69,296	145.9	49,820
1971	522.1	178,297	308.29	105,281	213.8	73,016	171.3	58,487	137.0	46,794
1972	784.3	267,838	536.57	183,239	247.7	84,600	341.2	116,511	195.4	66,728
1973	744.9	254,383	487.97	166,642	256.9	87,742	297.7	101,672	190.2	64,970
1974	386.2	131,887	217.52	74,283	168.7	57,604	116.4	39,738	101.2	34,545
1975	535.5	182,873	343.90	117,442	191.6	65,431	202.8	69,259	141.1	48,182
1976	493.2	168,428	287.00	98,011	206.2	70,417	160.5	54,803	126.5	43,208
1977	677.8	231,469	440.41	150,400	237.4	81,069	258.3	88,201	182.1	62,199
1978	641.4	219,038	423.01	144,458	218.4	74,580	244.6	83,540	178.4	60,918
1979	866.5	295,910	614.07	209,705	252.4	86,205	393.5	134,397	220.5	75,308
1980	622	212,413	402.39	137,416	219.6	74,997	236.4	80,724	166.0	56,692
1981	936.4	319,781	643.29	219,684	293.1	100,097	417.4	142,556	225.8	77,128
1982	596.1	203,568	382.43	130,600	213.7	72,968	217.8	74,363	164.7	56,237
1983	587.5	200,631	364.45	124,460	223.1	76,172	207.7	70,933	156.7	53,527
1984	459.4	156,885	309.41	105,664	150.0	51,222	186.7	63,743	122.8	41,920
1985	559.9	191,206	387.27	132,253	172.6	58,953	229.9	78,517	157.4	53,736
1986	849.4	290,070	589.63	201,359	259.8	88,711	378.9	129,400	210.7	71,959
1987	640.1	218,594	393.29	134,309	246.8	84,286	231.9	79,186	161.4	55,123
1988	643.8	219,858	399.91	136,569	243.9	83,288	232.7	79,451	167.3	57,118
1989	523.2	178,673	322.82	110,243	200.4	68,430	183.8	62,778	139.0	47,465
1990	727.8	248,544	466.26	159,228	261.5	89,316	277.7	94,826	188.6	64,402
1991	556	189,874	340.77	116,373	215.2	73,501	189.5	64,712	151.3	51,661
1992	732.8	250,251	481.05	164,279	251.8	85,973	289.3	98,785	191.8	65,494
1993	721.3	246,324	446.40	152,446	274.9	93,878	252.5	86,242	193.9	66,203
1994	540.2	184,478	348.80	119,115	191.4	65,363	208.5	71,196	140.3	47,919
1995	538.5	183,898	409.85	139,964	128.7	43,934	289.2	98,748	120.7	41,215
1996	512.2	174,916	320.53	109,461	191.7	65,455	186.1	63,558	134.4	45,903
1997	433.2	147,938	274.18	93,632	159.0	54,305	151.9	51,875	122.3	41,757
1998	440.3	150,362	267.12	91,221	173.2	59,141	151.9	51,872	115.2	39,350
1999	424.4	144,933	273.94	93,551	150.5	51,382	161.8	55,253	112.1	38,297
2000	535.9	183,010	333.24	113,801	202.7	69,208	199.3	68,073	133.9	45,729
2002	551.5	188,337	397.70	135,815	153.8	52,523	261.6	89,324	136.1	46,490
2003	554.6	189,396	366.05	125,006	188.6	64,390	221.1	75,498	145.0	49,508
Minimum	386.2	131,887	218	74283	118.4	40,423	116.4	39,738	95.4	32,563
Maximum	936.4	319,781	643	219684	293.1	100,097	417.4	142,556	225.8	77,128
Average	595.8	203,451	387	132243	208.5	71,209	232.2	79,285	155.1	52,957
Percentage	100.0%	100.0%	65.0%	65.0%	35.0%	35.0%	39.0%	39.0%	26.0%	26.0%

Table B4- LID Infiltration Summary

LID	Area (ha)	Average Annual Infiltration Volume (m³/Yr)	Average Annual Infiltration Volume (mm/Yr)
W1	8.92	7,436	83
W2	10.75	8,356	78
W3	6.3	3,925	62
W4	8.18	5,431	66
Total/Average	34.15	25,149	72

March 08, 2021

Project Number: 1474

David Schaeffer Engineering Ltd
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Attention: Steve Pichette, P.Eng.

Subject: Review of Quantity Control Requirement for Jock River-Reach One

Introduction

Phase 2 of the Barrhaven Conservancy Development (aka Conservancy East) is located in Barrhaven, Ontario, north of the Jock River, south of the Fraser Clarke Creek and east of the Foster Creek. The proposed development is approximately 59.26 ha that will primarily comprise of single and townhouse residential lots. As a part of the City of Ottawa's review of the proposed development draft plan of Phase 2 of the Barrhaven Conservancy Development, submitted in December 2020, it is proposed that flood quantity control measures will not need to be implemented as a part of this development. This assumption is based on the work completed by Stantec in June 2007 in the "Jock River Reach One Subwatershed Study" which concluded that for future developments within Reach 1 of the Jock River: "No quantity control storage is required for flood control purposes as the hydrograph from the subwatershed will peak before the upstream peak in the Jock River" and that "No erosion control storage is required to maintain the predevelopment in-stream erosion condition". Although this study did not consider the future development of the Barrhaven Conservancy Lands, and as such the modelling completed by Stantec has been updated by JFSA to reflect these changes. The following memo outlines data sources, assessed scenarios, assumptions, and conclusions of this independent Jock River Reach One study.

It is noted that RVCA is currently engaging in a formal update/review of the Jock River Reach One Subwatershed Study, with the findings of this study having the potential to affect the above-noted design criteria. While that study is underway J.F. Sabourin and Associates Inc. (JFSA) has completed an independent Jock River - Reach One study to re-assess/confirm that the assumptions presented in the original 2007 study by Stantec are still valid, as any changes to this conclusion could greatly impact the current BCDC Phase 2 development plan.

Background Data

The following outlines all the model and data sources used in this analysis:

- "Jock River Floodplain Mapping Report", (2005 - PSR Group Ltd. & JFSA)
- "Jock River Reach One Subwatershed Study Final Report", (2007 – Stantec)
- "Corrigan Stormwater Management Facility Stormwater Management Report and Design Brief", (2010 - IBI Group)
- "Citi Gate, Highway 416 Employment Lands, Servicing Study and Stormwater Management Report (O'Keefe SWM)", (2012 – Novatech)
- "Foster Stormwater Management Facility, Environmental Study Report", (2013 - CH2MHill)
- "Todd Pond Model Keeper Analysis (Re-Assessment of Existing System Capacity)", (2015 – JFSA)

- “CitiGate 416 Corporate Campus Detailed Servicing and Stormwater Management Report (Phase 1)”, (2015 – Novatech)
- “Kennedy-Burnett Stormwater Management Facility Retrofit, Detailed Design Report”, (2020 – Novatech)
- “Half Moon Bay South / Addendum to April 2015 Todd Pond Model Keeper Analysis, Re-Assessment of Existing System Capacity Report” (2020 - JFSA).

Model Development/Scenarios

The following section outlines the various hydrologic model scenarios developed as a part of this work, with a brief description of the data sources used for each scenario and how they have been incorporated into the existing Jock River subwatershed hydrologic model.

Model 1 - Jock River Floodplain Model – JFSA, 2005

This hydrologic model was developed as a part of the floodplain mapping study of the Jock River completed in 2005. The hydrologic model of the Jock River was developed by JFSA using SWMHYMO, with independent models developed to simulate both summer and spring events. Both models were calibrated to field measured flows, recorded at the Water Survey Canada Flow Gauge at Moodie Drive. These models function as the basis for which all future models (both by JFSA and others) have been built on. Refer to Figure 1 (JFSA, 2005) for an overview of the subcatchments for reach one in this model, with full SWMHYMO input and summary files provided in Attachment A.

Model 2 – Jock River Reach One Model – Stantec, 2007

The hydrologic analysis completed by Stantec in 2007 built upon the JFSA 2005 floodplain mapping modelling. As a part of the Stantec work, the lower reach of the Jock River (3,176 ha) which was represented as a single subcatchment in the 2005 study was subdivided into thirteen (13) subcatchments to better delineate the drainage areas to the various tributaries (O’Keefe, Fraser, Foster, Todd, Corrigan and Clarke) and to also provide a better representation of the existing development areas (Kennedy Burnett, Chapman Mills, Jockvale and Hearts Desire). The remaining natural/undeveloped areas within the Jock River corridor were subdivided into three smaller (3) sub-catchments. Refer to Figure 2 (Stantec, 2007) for an overview of the subcatchments for reach one in this model, with full SWMHYMO input and summary files provided in Attachment B.

As mentioned above from this study, it was concluded that developments located in the lower reaches of the Jock River do not require any quantity control storage for flood control purposes as the hydrograph from the subwatershed will peak before the upstream peak in the Jock River and that no erosion control storage is required to maintain the pre-development in-stream erosion conditions.

Model 3 – Jock River Reach One Model Update – JFSA, 2021

As a part of the study outlined in this report, the 2007 Stantec SWMHYMO model of the Jock River was updated to reflect (as best as possible with the available information) proposed, approved and potential future developments, since the 2007 study.

At the time of the 2007 study, it was assumed that the floodplain of reach one of the Jock River (from Highway 416 to Greenbank Road) would not be filled and developed. Furthermore, the assumptions that were made in 2007 for the total imperviousness of future developments are not reflective of the actual constructed conditions observed in 2021; for example, the total impervious area for the Todd drainage area was assumed to be 43% in the 2007 study, while based on latest aerial photography it appears that the imperviousness for this area is closer to 58.5%). Additionally, SWM quantity controls were implemented in some tributaries within Reach One (e.g., O'Keefe, Foster and Kennedy-Burnett) to respect the hydraulic capacity of the local watercourses or other existing hydraulic constraints.

As outlined in the Background Data section of this memo, data from various reports and studies were collected and used to update Stantec's 2007 model, to best reflect existing conditions and known approved and planned development projects. As such, the thirteen (13) subcatchments of the 2007 Stantec model have been further discretized into one hundred ten (110) subcatchments, with numerous additional major system storage, SWM Ponds, and channel routing commands added. This updated existing condition model is reflective of current 2021 conditions, which assumes that the lower Jock River floodplain is undeveloped. It should also be noted that only subcatchments downstream of Highway 416 have been updated as a part of this analysis. Updates to other catchments of the Jock River further upstream, such as the Monahan Drain, Hobbs Creek, King Creek, and development areas in Richmond, where additional new information may be available, have not been included in the model updates at this time. Refer to Figure 3 for an overview of the subcatchments for reach one in this model, with full SWMHYMO input and summary files been provided in Attachment C, detailed schematics of the subcatchments updated as a part of this study have been provided in Attachment F.

Note that Novatech's PCSWMM model of the Kennedy-Burnett area was used to create a detailed SWMHYMO model of the same area. In creating this SWMHYMO model it was found that the 100-year peak outflows from the Kennedy Burnett facility were 1.4 times higher than that reported in the Novatech PCSWMM model. While it is expected that different modelling software will produce slightly different results, this difference is significant and should be investigated further; although it is unlikely that this difference is expected to change the fundamental conclusions of this analysis.

Model 4A & 4B – Jock River Reach One Future Conditions (without and with quantity SWM controls) – JFSA, 2021

Two additional models (4A and 4B) were created (which built on model 3) to evaluate the impacts of developing portions of the lower Jock River floodplain (from Highway 416 to Greenbank Road). These lands make up approximately 156 ha and would include BCDC and other properties on the south side of the Jock River. Model 4A assumes that these lands would be developed without any SWM quantity controls and Model 4B assumes that the lands would be developed with SWM Post to Pre-development quantity controls. Refer to Figure 4 for an overview of the subcatchments for reach one in these models, with full SWMHYMO input and summary files for scenarios 4A and 4B provided in Attachment D & E, respectively.

Results

All hydrologic models were run using a 24 hours SCS storm for the 2-to-100-year events. Note that this analysis focuses on this particular rainfall event as for developed areas the summer rainfall events are more critical than the spring rainfall plus snowmelt conditions. Hence, only the summer peak flows have been summarized and compared for the various scenarios below, as the flow contributions from the developments in the lower Jock River under the spring rainfall + snowmelt event are negligible compared to the flows upstream from the greater Jock River. It is further noted that the same design storms were used in all models.

Peak flows at key locations along Reach One of the Jock River have been extracted from the various hydrologic models and provided in the following section. As a part of this analysis, 5 key locations on the Jock River have been selected to compare the simulated peak flows and are as follows: Highway 416, Borrisokane Road, Greenbank Road, Jockvale Road and the Jock River's confluence with the Rideau River. Note that for the older models (JFSA 2005 & Stantec 2007) results have only been provided at some locations, as these original models were not discretized to this higher level of detail. Additionally, the Stantec 2007 model did not assess flows on the Jock River for the 10- and 50-year events at any locations.

Table 1: Comparison of Summer Peak Flows (m³/s) at Highway 416 (52483.00 ha)

Scenario	Return Period					
	2-Year	5-Year	10-Year	25-Year	50-Year	100-Year
Model 1: 2005 Floodplain Study	45.676	66.292	82.076	104.643	122.469	141.415
Model 2: Stantec 2007 Reach One Analysis	45.789	66.413	n/a	104.834	n/a	141.853
Model 3: Updated Model 2 to current/ approved conditions	46.294	67.222	83.235	106.109	124.249	143.580
Model 4A: Model 3 with BCDC & others w/o SWM	46.294	67.222	83.235	106.109	124.249	143.580
Model 4B: Model 3 with BCDC & others with SWM	46.294	67.222	83.235	106.109	124.249	143.580

From Table 1 above it is seen that the peak flows on the Jock River at Highway 416 for Models 3, 4A and 4B are higher than in Models 1 and 2. This is because the computational time step in the updated models was reduced from 5 - 10 minutes to 1 minute. This change was necessary to provide stable results in the various models, especially with the additional ROUTE CHANNEL commands that have been added to the updated models. There were no other changes made to the models upstream of Highway 416.

Table 2: Comparison of Summer Peak Flows (m³/s) at Borrisokane Road (53577.82 ha)

Scenario	Return Period					
	2-Year	5- Year	10-Year	25-Year	50-Year	100-Year
Model 1: 2005 Floodplain Study	n/a	n/a	n/a	n/a	n/a	n/a
Model 2: Stantec 2007 Reach One Analysis	46.817	68.124	n/a	107.402	n/a	144.892
Model 3: Updated Model 2 to current/ approved conditions	47.379	69.117	85.613	108.988	127.740	147.849
Model 4A: Model 3 with BCDC & others w/o SWM	47.426	68.998	85.561	109.064	127.650	147.535
Model 4B: Model 3 with BCDC & others with SWM	47.599	69.319	85.870	109.449	128.055	147.939

From Table 2 it is seen that the peak flows on the Jock River at Borrisokane are generally lower in model 4A (developed without SWM controls) than under existing conditions (Model 3). The inclusion of SWM controls for these future developments results in the peak flows increasing from existing conditions for all return periods at this location. Note that the increase in flows at this location between the Stantec model (model 2) and the JFSA existing conditions model (model 3) again is due to the greater discretization of subcatchments at Borrisokane Road in the JFSA model. For example, in the Stantec model, the subcatchment that represents the currently undeveloped lands along the Jock River is represented as a single subcatchment (S-1). Where the JFSA updated model represents these lands as 14 individual subcatchments, all discharging to their respective locations within the Jock River (e.g. O’Keefe Creek, Foster Creek & Borrisokane Road).

Table 3: Comparison of Summer Peak Flows (m³/s) at Greenbank Road (54717.80 ha)

Scenario	Return Period					
	2-Year	5- Year	10-Year	25-Year	50-Year	100-Year
Model 1: 2005 Floodplain Study	n/a	n/a	n/a	n/a	n/a	n/a
Model 2: Stantec 2007 Reach One Analysis	49.195	71.220	n/a	111.172	n/a	149.236
Model 3: Updated Model 2 to current/ approved conditions	49.055	70.826	86.895	110.282	128.564	147.488
Model 4A: Model 3 with BCDC & others w/o SWM	48.599	69.773	85.389	103.842	126.050	144.531
Model 4B: Model 3 with BCDC & others with SWM	48.982	70.171	85.928	103.651	126.537	144.894

From Table 3 it is seen that peak flows on the Jock River at Greenbank Road are the lowest without SWM controls in place (Model 4A). With SWM controls in place, the peak flows are lower than the existing conditions, but not as low as when SWM controls are not implemented. Note that the JFSA existing conditions model (model 3) is presenting peak flows lower than the Stantec model (model 2) at this location, again this is due to the greater discretization in the JFSA model as discussed above.

Table 4: Comparison of Summer Peak Flows (m³/s) at Jockvale Road (55476.26 ha)

Scenario	Return Period					
	2-Year	5- Year	10-Year	25-Year	50-Year	100-Year
Model 1: 2005 Floodplain Study	n/a	n/a	n/a	n/a	n/a	n/a
Model 2: Stantec 2007 Reach One Analysis	49.870	72.143	n/a	112.074	n/a	150.033
Model 3: Updated Model 2 to current/ approved conditions	49.619	72.224	88.294	111.989	130.865	149.819
Model 4A: Model 3 with BCDC & others w/o SWM	49.482	71.017	86.165	105.082	128.174	146.840
Model 4B: Model 3 with BCDC & others with SWM	49.606	71.408	86.690	104.765	128.229	147.027

From Table 4 is seen that the peak flows at Jockvale Road are generally at their lowest without SWM controls in place, and that either implementing or not implementing SWM controls for future developments results in peak flows at this location being less than existing conditions.

Table 5: Comparison of Summer Peak Flows (m³/s) at Outlet of Jock River (55579.20 ha)

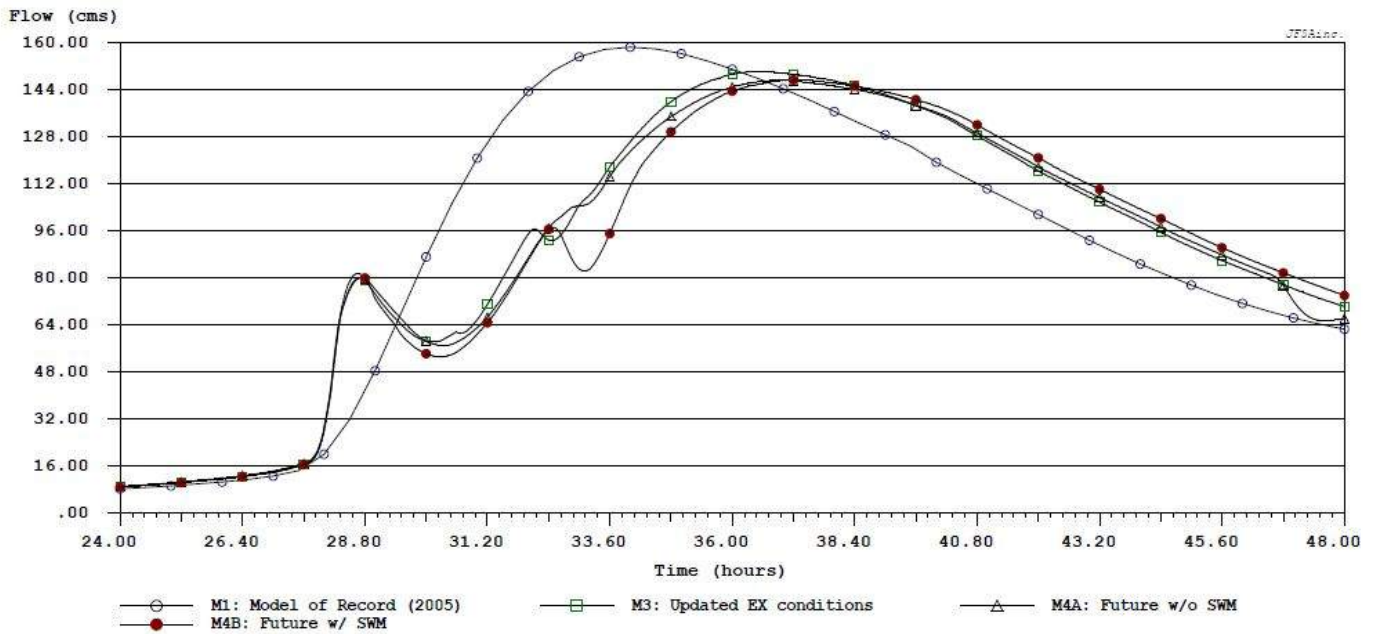
Scenario	Return Period					
	2-Year	5- Year	10-Year	25-Year	50-Year	100-Year
Model 1: 2005 Floodplain Study	49.16	72.08	89.96	115.84	136.46	158.42
Model 2: Stantec 2007 Reach One Analysis	50.78	73.65	n/a	113.97	n/a	157.69
Model 3: Updated Model 2 to current/ approved conditions	49.72	72.36	88.45	112.2	131.12	150.12
Model 4A: Model 3 with BCDC & others w/o SWM	49.58	71.17	86.35	105.27	128.42	147.10
Model 4B: Model 3 with BCDC & others with SWM	49.70	71.54	86.85	104.96	128.45	147.28

From Table 5 it is seen that the peak flows on the Jock River at the confluence with the Rideau River are generally at their lowest without SWM controls in place, and that either implementing or not implementing SWM controls for future developments results in peak flows at this location to be less than existing conditions.

Discussion

Although not initially obvious, the reason that future urban developments within Reach One of the Jock River are decreasing peak flows on the Jock River is because developing land not only affects the peak of the hydrograph but also the overall shape. Figure A below provides a comparison of the simulated hydrographs at the Jock River's confluence with the Rideau River from the various model scenarios. During any rainfall event, the runoff from the existing and future developments within Reach One will have already peaked and decayed before the peak flows arrive at this location from the upstream drainage area. For the 100-Year SCS storm, the peak from the development in Reach One can be seen in the figure below at around 28 hours, while the peak flow on the Jock River from the upstream drainage areas occurs at around 36-37 hours, this is approximately a 9-hour difference in timing. As such, implementing SWM measures for developments in the lower portions of the Jock River will decrease peak flows from the development, but would also prolong the period of time during which they discharge into the Jock River, thus coinciding with flows from the greater Jock River, ultimately resulting in potential increases in peak flows on the Jock River. This is seen in the figure below with the future condition with SWM controls (Model 4B - Red Circles) having a higher flow in the tail than future conditions without SWM controls (Model 4A – Black Triangles). Note that the difference between Model 1 and all other scenarios is simply due to further discretization of subcatchments within Reach One.

Figure A: Comparison of simulated 100 yr Jock River hydrographs at the confluence with the Rideau River



Hydrograph Statistics:

Legend	Filename & Comment	Time Step (min)	Drainage Area (ha)	Peak Flow (cms)	Time to Peak (hrs)	Runoff Volume (mm)	Runoff Volume (cu.m)	Duration of flow (hrs)	Average flow (cms)
○	N1_0100 : M1: Model of Record (2005)	30.00	55659.00	158.420	34.000	14.52	8.082E+06	24.000	93.538
□	SN_N1_0100 : M3: Updated EX conditions	1.00	55579.20	150.120	36.533	14.24	7.914E+06	24.000	91.603
△	SN_N1_0100 : M4A: Future w/o SWM	1.00	55579.20	147.102	36.917	14.12	7.848E+06	24.000	90.831
●	SN_N1_0100 : M4B: Future w/ SWM	1.00	55579.19	147.276	37.250	14.03	7.798E+06	24.000	90.252

Conclusion

The hydrologic model developed as a part of the Jock River Reach One Subwatershed Study (Stantec 2007) has been updated to provide additional refinements in the lower reaches of the Jock River (downstream of Highway 416) and assumes the development of lands that were previously not considered in the 2007 analysis (e.g. Barrhaven Conservancy). Future development condition models were created with and without SWM controls assumed, and the peak flows extracted from these models at key locations along the lower Jock River. From this analysis, it was found that with these additional developments in the lower Jock River peak flows are generally less than existing conditions without SWM controls in place. Implementing SWM controls for these developments has also been found to generally decrease peak flows on the Jock River, but not at all locations and not to the same degree as without SWM controls. Ultimately these findings are consistent with the fundamental conclusions drawn in Stantec's 2007 Jock River Reach One study, which initially determined that for future developments within Reach One of the Jock River "No quantity control storage is required for flood control purposes as the hydrograph from the subwatershed will peak before the upstream peak in the Jock River" and that "No erosion control storage is required to maintain the pre-development in-stream erosion condition". Based on the results of the updated analysis outlined in this memo, it can confirm that the fundamental conclusions drawn in Stantec's 2007 for developments in reach one of the Jock River remain valid.

Yours truly,
J.F Sabourin and Associates Inc.



Jonathon Burnett, P.Eng
Water Resources Engineer

cc: J.F Sabourin, M.Eng, P.Eng
Director of Water Resources Projects



Figures

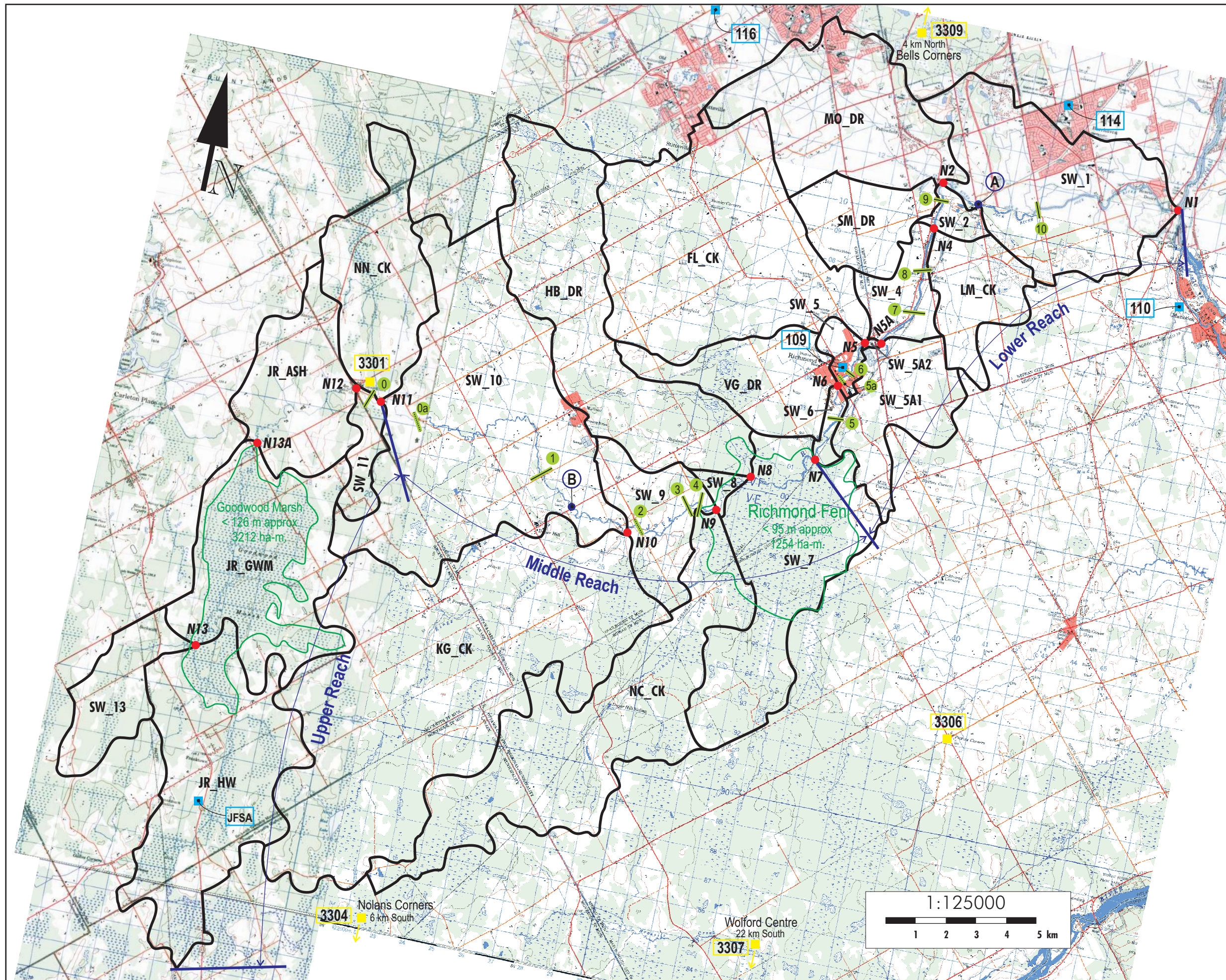
- Figure 1: Model 1 – Jock River Floodplain Model – JFSA, 2005
- Figure 2: Model 2 – Jock River Reach One Model – Stantec, 2007
- Figure 3: Model 3 – Jock River Reach One Model Update - JFSA, 2021
- Figure 4: Model 4A & 4B – Jock River Reach One Future Conditions - JFSA, 2021

Tables

- Table 1: Summer Peak Flows at Highway 416
- Table 2: Summer Peak Flows at Borrisokane Road.
- Table 3: Summer Peak Flows at Greenbank Road
- Table 4: Summer Peak Flows at Jockvale Road
- Table 5: Summer Peak Flows at Outlet of Jock River

Attachments

- Attachment A: Model 1 - SWMHYMO Input & Summary files
- Attachment B: Model 2 - SWMHYMO Input & Summary files
- Attachment C: Model 3 - SWMHYMO Input & Summary files
- Attachment D: Model 4A - SWMHYMO Input & Summary files
- Attachment E: Model 4B - SWMHYMO Input & Summary files
- Attachment F: Updated Subcatchment Schematics & Tables



- Legend:**
- Watershed
 - Bogs (Reservoir)
 - Nodes
 - Flow gauges
 - Rain gauges
 - Snow course stations
 - River Cross-Sections (based on topo. maps)
 - River Cross-Sections adjusted with field data
 - Reaches limits
- Flow gauges ID**
- 02LA007- Jock River near Richmond
 - Jock River at Franktown Rd
- Rain gauges ID**
- Richmond
 - Manotick
 - Barrhaven
 - Maple Grove
 - JFSA Inc, Temporary Rain Gauge 2003
- Snow course stations ID**
- Ashton
 - Nolans Corners
 - Pierces Corners
 - Bells Corners
 - Wolford Centre

Client:

Project:
Jock River Flood Plain Mapping Study

Title:
Watershed Delineation

J.F. Sabourin & Associates Inc.
WATER RESOURCES AND ENVIRONMENTAL CONSULTANTS
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GATINEAU (819) 243-6858

Figure 1 Ref. File: Base Map Jock River B.cdr



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Legend

- Existing SWM Facility
- Proposed Stormwater Facility
- Proposed Pond Outlet
- Jock River Tributary (Municipal Drain)
- Jock River Tributary (Non-Municipal Drain)
- Watershed Boundary
- 91.7 Regulatory Flood Level
- W/L 89.50 Normal Water Level
- Woodlot Limits
- Sub-drainage Area Limit
- Desire 24 ha
77 50% hrs
SCS Curve Number
- Application Plans Under Review
- 10 Year Flood Line
- 25 Year Flood Line
- 100 Year Flood Line

1	FINAL REPORT	BCB	N.C.	JUNE 2007
Revision		By	Appd.	YY.MM.DD
File Name:		Own.	Chgd.	Dgn.
Seal				YY.MM.DD

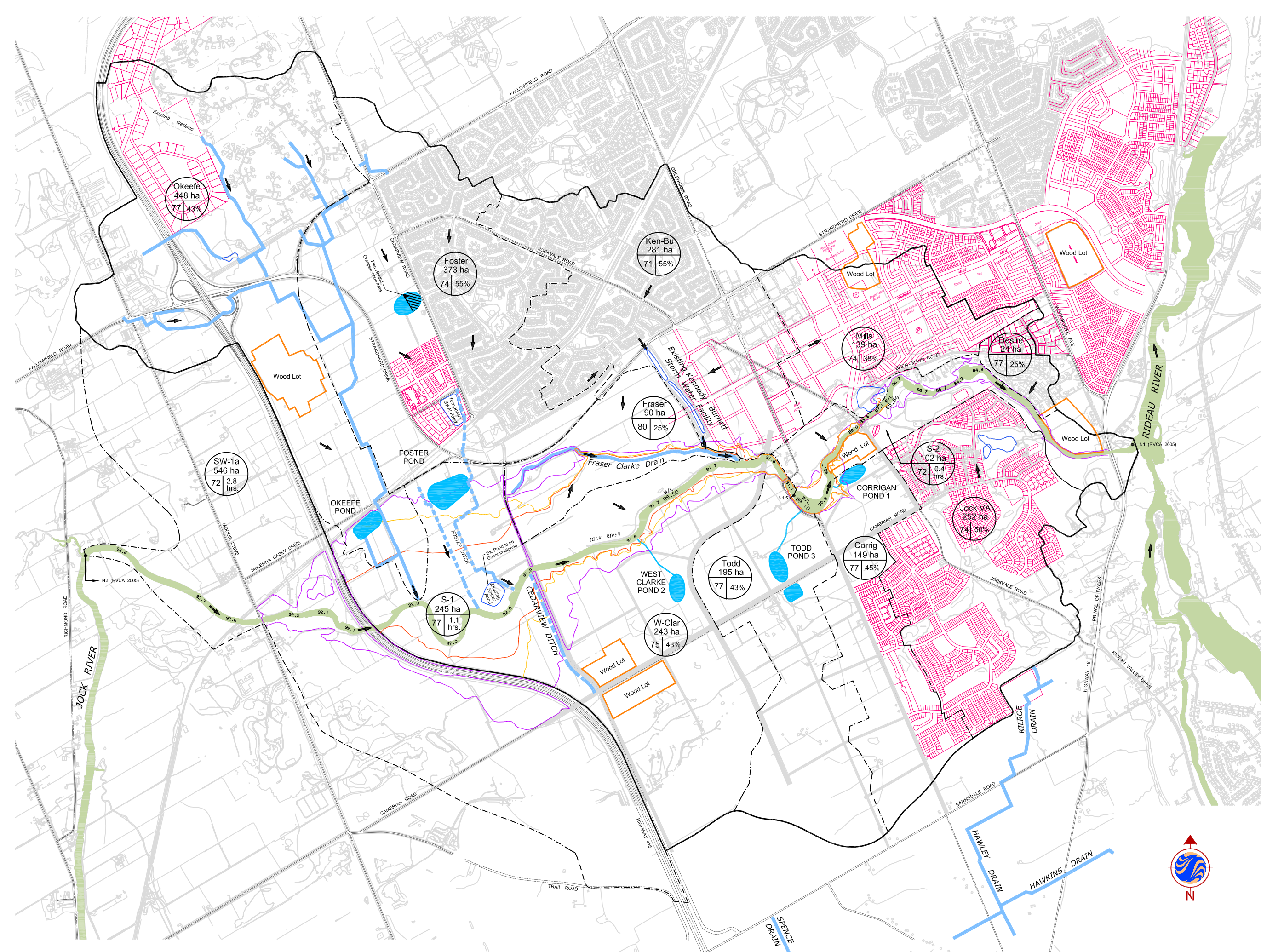
Client/Project

JOCK RIVER REACH ONE
SUB-WATERSHED STUDY
Ottawa ON Canada

Title
PROPOSED CONDITIONS
HYDROLOGIC MODEL
DRAINAGE BOUNDARIES

Project No. 60400414 Scale 1:10,000
Drawing No. _____ Sheet _____ Revision _____

Figure 2 1 of 1 1





- ### Legend
- Channel Cross Sections
 - S-1 Sub-catchments and Fraser Sub-catchments
 - S-1-A
 - S-1-B
 - S-1-D1
 - S-1-D2
 - S-1-D3
 - S-1-D4
 - S-1-D5
 - S-1-D6
 - S-1-D7
 - S-1-D8
 - S-1-FO-D1
 - S-1-FO-D2
 - S-1-FO-F-D
 - S-1-Okeefe
 - FRASER-DRN
 - FRASER-D
- Google Hybrid

File name: 20210304_S-1_Fraser_Schematic-Model4A.pdf

XS 3633 Cross Section at station 3633

S-1-A: Area ID
 90.84 ha: Area (ha)
 Ref. 1: Reference Number

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DSEI
 david schaeffer engineering ltd

PROJECT: BCDC - Quantity Control Study

TITLE: S-1 Sub-catchment and Fraser Clarke Sub-catchment Schematic

PROJECT NO.	1474-16
DRAWN:	MM
DATE:	Mar. 2021

Station	Channel Name	Area (ha)	Ref.	Flow (m³/s)	Velocity (m/s)	Depth (m)	Width (m)	Material	Notes
3633	Fraser	90.84	1	1500	1.5	10	100	Gravel	Channel cross section at station 3633

SCALE:





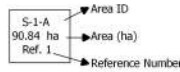
Legend

- Channel Cross Sections
- S-1 Sub-catchments and Fraser Sub-catchments
- S-1-A
- S-1-B
- S-1-D1
- S-1-D2
- S-1-D3
- S-1-D4
- S-1-D5
- S-1-D6
- S-1-D7
- S-1-D8
- S-1-FO-D1
- S-1-FO-D2
- S-1-FO-F-D
- S-1-Okeefe
- FRASER-DRN
- FRASER-D

Google Hybrid

File name: 20210304_S-1_Fraser_Schematic-Model4B.pdf

XS 3633 Cross Section at station 3633



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DSEL
 david schaeffer engineering ltd

PROJECT : BCDC - Quantity Control Study

TITLE : S-1 Sub-catchment and Fraser Clarke Sub-catchment Schematic

PROJECT NO. 1474-16

DRAWN: MM

DATE: Mar. 2021

Station	Channel	Area (ha)	Ref.	Sub-catchment	Area (ha)	Ref.	Channel	Area (ha)	Ref.	Sub-catchment	Area (ha)	Ref.	Channel	Area (ha)	Ref.	Sub-catchment	Area (ha)	Ref.
3633	FRASER-D	21.61	16	FRASER-D	21.61	16	FRASER-D	21.61	16	FRASER-D	21.61	16	FRASER-D	21.61	16	FRASER-D	21.61	16
3633	FRASER-DRN	13.65	15	FRASER-DRN	13.65	15	FRASER-DRN	13.65	15	FRASER-DRN	13.65	15	FRASER-DRN	13.65	15	FRASER-DRN	13.65	15
3633	S-1-A	75.88	1	S-1-A	75.88	1	S-1-A	75.88	1	S-1-A	75.88	1	S-1-A	75.88	1	S-1-A	75.88	1
3633	S-1-B	55.36	2	S-1-B	55.36	2	S-1-B	55.36	2	S-1-B	55.36	2	S-1-B	55.36	2	S-1-B	55.36	2
3633	S-1-D1	21.67	3	S-1-D1	21.67	3	S-1-D1	21.67	3	S-1-D1	21.67	3	S-1-D1	21.67	3	S-1-D1	21.67	3
3633	S-1-D2	18.67	4	S-1-D2	18.67	4	S-1-D2	18.67	4	S-1-D2	18.67	4	S-1-D2	18.67	4	S-1-D2	18.67	4
3633	S-1-D3	6.79	5	S-1-D3	6.79	5	S-1-D3	6.79	5	S-1-D3	6.79	5	S-1-D3	6.79	5	S-1-D3	6.79	5
3633	S-1-D4	3.28	6	S-1-D4	3.28	6	S-1-D4	3.28	6	S-1-D4	3.28	6	S-1-D4	3.28	6	S-1-D4	3.28	6
3633	S-1-D5	12.84	7	S-1-D5	12.84	7	S-1-D5	12.84	7	S-1-D5	12.84	7	S-1-D5	12.84	7	S-1-D5	12.84	7
3633	S-1-D6	1.75	8	S-1-D6	1.75	8	S-1-D6	1.75	8	S-1-D6	1.75	8	S-1-D6	1.75	8	S-1-D6	1.75	8
3633	S-1-D7	2.03	9	S-1-D7	2.03	9	S-1-D7	2.03	9	S-1-D7	2.03	9	S-1-D7	2.03	9	S-1-D7	2.03	9
3633	S-1-D8	5.27	10	S-1-D8	5.27	10	S-1-D8	5.27	10	S-1-D8	5.27	10	S-1-D8	5.27	10	S-1-D8	5.27	10
3633	S-1-FO-D1	5.11	11	S-1-FO-D1	5.11	11	S-1-FO-D1	5.11	11	S-1-FO-D1	5.11	11	S-1-FO-D1	5.11	11	S-1-FO-D1	5.11	11
3633	S-1-FO-D2	4.94	12	S-1-FO-D2	4.94	12	S-1-FO-D2	4.94	12	S-1-FO-D2	4.94	12	S-1-FO-D2	4.94	12	S-1-FO-D2	4.94	12
3633	S-1-FO-F-D	14.96	13	S-1-FO-F-D	14.96	13	S-1-FO-F-D	14.96	13	S-1-FO-F-D	14.96	13	S-1-FO-F-D	14.96	13	S-1-FO-F-D	14.96	13
3633	S-1-Okeefe	44.93	14	S-1-Okeefe	44.93	14	S-1-Okeefe	44.93	14	S-1-Okeefe	44.93	14	S-1-Okeefe	44.93	14	S-1-Okeefe	44.93	14





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Gatineau, QC
Montréal, QC
Québec, QC

Attachment A

Model 1 – Jock River Floodplain Model

JFSA, 2005

SWMHYMO Input & Summary files


```

1  20    Metric units / ID numbers OFF
2  *#*****
3  *# SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
4  *#*****
5  *# Project Name: [Jock River]    Project Number: [411-02]
6  *# Date       : 06-06-2003
7  *# Modeller   : [JoF]
8  *# Company    : JFSAinc.
9  *# License #  : 2549237
10 *#*****
11 *# CALIBRATION OF SUMMER MODEL PARAMETERS
12 *# USING CONTINUOUS SIMULATIONS
13 *# Rainfall data from JFSA raingauge installed at site + other gauges by the City
14 *# Use data collected from May 1st to July 14, 2003
15 *
16 * Calibrated parameters for Summer 2003 data:  APII=50, APIK=0.85, CN=varies,
17 *                                                SK=0.01, InterEventTime=12,
18 *                                                GWResk=0.96, VHydCond=0.055
19 *
20 *# -----
21 *
22 *START          TZERO=[2003.0501], METOUT=[2], NSTORM=[1], NRUN=[001]
23 *              ["XAVG0315.STM"] average storm data a 15 minute time step
24 *              The above rainf file is an average of the JFSA gauge data
25 *              with the City of Ottawa rainfall data collected during
26 *              the same period.
27 *% 2 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
28 START        TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[2]
29 *%             ["C24SC002.stm"] <--storm filename, one per line for NSTORM time
30 *%-----|-----
31 *%-----|-----
32 READ STORM   STORM_FILENAME=["storm.001"]
33 *%-----|-----
34 MODIFY STORM ICASEms=[1], NSHIFT=[96],
35 *           RedFACT=[1],
36 *%-----|-----
37 COMPUTE API  APII=[50], APIK=[.85]/day
38 *%-----|-----
39 *%-----|-----
40 *#
41 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
42 *# of 1.32
43 *%-----|-----
44 CONTINUOUS NASHYD NHYD=["JR_HW"], DT=[30]min, AREA=[3680] (ha),
45 *           DWF=[0] (cms), CN/C=[64], IA=[2.5] (mm),
46 *           N=[3.0], TP=[7.13]hrs,
47 *           Continuous simulation parameters:
48 *           IaRECper=[4] (hrs),
49 *           SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
50 *           InterEventTime=[12] (hrs)
51 *           Baseflow simulation parameters:
52 *           BaseFlowOption=[1] ,
53 *           InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
54 *           VHydCond=[0.055] (mm/hr), END=-1
55 *%-----|-----
56 *#
57 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
58 *# of 1.32
59 *%-----|-----
60 CONTINUOUS NASHYD NHYD=["SW_13"], DT=[30]min, AREA=[971] (ha),
61 *           DWF=[0] (cms), CN/C=[61], IA=[2.5] (mm),
62 *           N=[3.0], TP=[3.76]hrs,
63 *           Continuous simulation parameters:
64 *           IaRECper=[4] (hrs),
65 *           SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
66 *           InterEventTime=[12] (hrs)

```

```

67         Baseflow simulation parameters:
68         BaseFlowOption=[1] ,
69         InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
70         VHydCond=[0.055] (mm/hr),   END=-1
71     *%-----|-----
72     *#
73     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
74     *# of 1.80
75     *%-----|-----
76     CONTINUOUS NASHYD  NHYD=["JR_GWM"], DT=[30]min, AREA=[3074] (ha),
77                         DWF=[0] (cms),  CN/C=[55], IA=[2.5] (mm),
78                         N=[3], TP=[11.33]hrs,
79                         Continuous simulation parameters:
80                         IaRECper=[4] (hrs),
81                         SMIN=[-1] (mm),  SMAX=[-1] (mm), SK=[0.010]/(mm),
82                         InterEventTime=[12] (hrs)
83                         Baseflow simulation parameters:
84                         BaseFlowOption=[1] ,
85                         InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
86                         VHydCond=[0.055] (mm/hr),   END=-1
87     *%-----|-----
88     CONTINUOUS NASHYD  NHYD=["JR_ASH"], DT=[30]min, AREA=[1781] (ha),
89                         DWF=[0] (cms),  CN/C=[72], IA=[2.5] (mm),
90                         N=[3.0], TP=[3.91]hrs,
91                         Continuous simulation parameters:
92                         IaRECper=[4] (hrs),
93                         SMIN=[-1] (mm),  SMAX=[-1] (mm), SK=[0.010]/(mm),
94                         InterEventTime=[12] (hrs)
95                         Baseflow simulation parameters:
96                         BaseFlowOption=[1] ,
97                         InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
98                         VHydCond=[0.055] (mm/hr),   END=-1
99     *%-----|-----
100    CONTINUOUS NASHYD  NHYD=["SW_11"], DT=[30]min, AREA=[500] (ha),
101                        DWF=[0] (cms),  CN/C=[66], IA=[2.5] (mm),
102                        N=[3.0], TP=[1.24]hrs,
103                        Continuous simulation parameters:
104                        IaRECper=[4] (hrs),
105                        SMIN=[-1] (mm),  SMAX=[-1] (mm), SK=[0.010]/(mm),
106                        InterEventTime=[12] (hrs)
107                        Baseflow simulation parameters:
108                        BaseFlowOption=[1] ,
109                        InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
110                        VHydCond=[0.055] (mm/hr),   END=-1
111    *%-----|-----
112    *#
113    *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
114    *# of 1.80
115    *%-----|-----
116    CONTINUOUS NASHYD  NHYD=["NN_CK"], DT=[30]min, AREA=[1917] (ha),
117                        DWF=[0] (cms),  CN/C=[66], IA=[2.5] (mm),
118                        N=[3.0], TP=[5.29]hrs,
119                        Continuous simulation parameters:
120                        IaRECper=[4] (hrs),
121                        SMIN=[-1] (mm),  SMAX=[-1] (mm), SK=[0.010]/(mm),
122                        InterEventTime=[12] (hrs)
123                        Baseflow simulation parameters:
124                        BaseFlowOption=[1] ,
125                        InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
126                        VHydCond=[0.055] (mm/hr),   END=-1
127    *%-----|-----
128    *#
129    *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
130    *# of 1.52
131    *%-----|-----
132    CONTINUOUS NASHYD  NHYD=["SW_10"], DT=[30]min, AREA=[5666] (ha),

```

```

133 DWF=[0] (cms), CN/C=[72], IA=[2.5] (mm),
134 N=[3.0], TP=[8.00]hrs,
135 Continuous simulation parameters:
136 IaREcper=[4] (hrs),
137 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
138 InterEventTime=[12] (hrs)
139 Baseflow simulation parameters:
140 BaseFlowOption=[1] ,
141 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
142 VHydCond=[0.055] (mm/hr), END=-1
143 *%-----|-----
144 *#
145 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
146 *# of 1.75
147 *%-----|-----
148 CONTINUOUS NASHYD NHYD=["KG_CK"], DT=[30]min, AREA=[8376] (ha),
149 DWF=[0] (cms), CN/C=[66], IA=[2.5] (mm),
150 N=[3.0], TP=[11.66]hrs,
151 Continuous simulation parameters:
152 IaREcper=[4] (hrs),
153 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
154 InterEventTime=[12] (hrs)
155 Baseflow simulation parameters:
156 BaseFlowOption=[1] ,
157 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
158 VHydCond=[0.055] (mm/hr), END=-1
159 *%-----|-----
160 *#
161 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
162 *# of 1.68
163 *%-----|-----
164 CONTINUOUS NASHYD NHYD=["SW_9"], DT=[30]min, AREA=[1132] (ha),
165 DWF=[0] (cms), CN/C=[70], IA=[2.5] (mm),
166 N=[3.0], TP=[2.51]hrs,
167 Continuous simulation parameters:
168 IaREcper=[4] (hrs),
169 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
170 InterEventTime=[12] (hrs)
171 Baseflow simulation parameters:
172 BaseFlowOption=[1] ,
173 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
174 VHydCond=[0.055] (mm/hr), END=-1
175 *%-----|-----
176 *#
177 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
178 *# of 1.82
179 *%-----|-----
180 CONTINUOUS NASHYD NHYD=["NC_CK"], DT=[30]min, AREA=[4464] (ha),
181 DWF=[0] (cms), CN/C=[62], IA=[2.5] (mm),
182 N=[3.0], TP=[11.32]hrs,
183 Continuous simulation parameters:
184 IaREcper=[4] (hrs),
185 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
186 InterEventTime=[12] (hrs)
187 Baseflow simulation parameters:
188 BaseFlowOption=[1] ,
189 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
190 VHydCond=[0.055] (mm/hr), END=-1
191 *%-----|-----
192 *#
193 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
194 *# of 1.80
195 *%-----|-----
196 CONTINUOUS NASHYD NHYD=["SW_8"], DT=[30]min, AREA=[131] (ha),
197 DWF=[0] (cms), CN/C=[63], IA=[2.5] (mm),
198 N=[3.0], TP=[0.90]hrs,

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199         Continuous simulation parameters:
200         IaREcper=[4] (hrs),
201         SMIN=[-1] (mm),  SMAX=[-1] (mm), SK=[0.010]/(mm),
202         InterEventTime=[12] (hrs)
203         Baseflow simulation parameters:
204         BaseFlowOption=[1] ,
205         InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
206         VHydCond=[0.055] (mm/hr),  END=-1
207     *%-----|-----
208     *#
209     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
210     *# of 1.65
211     *%-----|-----
212     CONTINUOUS NASHYD  NHYD=["HB_DR"], DT=[30]min, AREA=[3854] (ha),
213                       DWF=[0] (cms),  CN/C=[66], IA=[2.5] (mm),
214                       N=[3.0], TP=[8.42]hrs,
215                       Continuous simulation parameters:
216                       IaREcper=[4] (hrs),
217                       SMIN=[-1] (mm),  SMAX=[-1] (mm), SK=[0.010]/(mm),
218                       InterEventTime=[12] (hrs)
219                       Baseflow simulation parameters:
220                       BaseFlowOption=[1] ,
221                       InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
222                       VHydCond=[0.055] (mm/hr),  END=-1
223     *%-----|-----
224     *#
225     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
226     *# of 1.82
227     *%-----|-----
228     CONTINUOUS NASHYD  NHYD=["SW_7"], DT=[30]min, AREA=[3197] (ha),
229                       DWF=[0] (cms),  CN/C=[57], IA=[2.5] (mm),
230                       N=[3.0], TP=[6.65]hrs,
231                       Continuous simulation parameters:
232                       IaREcper=[4] (hrs),
233                       SMIN=[-1] (mm),  SMAX=[-1] (mm), SK=[0.010]/(mm),
234                       InterEventTime=[12] (hrs)
235                       Baseflow simulation parameters:
236                       BaseFlowOption=[1] ,
237                       InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
238                       VHydCond=[0.055] (mm/hr),  END=-1
239     *%-----|-----
240     *#
241     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
242     *# of 1.75
243     *%-----|-----
244     CONTINUOUS NASHYD  NHYD=["SW_6"], DT=[30]min, AREA=[165] (ha),
245                       DWF=[0] (cms),  CN/C=[67], IA=[2.5] (mm),
246                       N=[3.0], TP=[4.18]hrs,
247                       Continuous simulation parameters:
248                       IaREcper=[4] (hrs),
249                       SMIN=[-1] (mm),  SMAX=[-1] (mm), SK=[0.010]/(mm),
250                       InterEventTime=[12] (hrs)
251                       Baseflow simulation parameters:
252                       BaseFlowOption=[1] ,
253                       InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
254                       VHydCond=[0.055] (mm/hr),  END=-1
255     *%-----|-----
256     *#
257     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
258     *# of 1.67
259     *%-----|-----
260     CONTINUOUS NASHYD  NHYD=["VG_DR"], DT=[30]min, AREA=[1332] (ha),
261                       DWF=[0] (cms),  CN/C=[72], IA=[2.5] (mm),
262                       N=[3.0], TP=[5.95]hrs,
263                       Continuous simulation parameters:
264                       IaREcper=[4] (hrs),

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265 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
266 InterEventTime=[12] (hrs)
267 Baseflow simulation parameters:
268 BaseFlowOption=[1] ,
269 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
270 VHydCond=[0.055] (mm/hr), END=-1
271 *%-----|
272 CONTINUOUS NASHYD NHYD=["SW_5"], DT=[30]min, AREA=[224] (ha),
273 DWF=[0] (cms), CN/C=[77], IA=[2.5] (mm),
274 N=[3.0], TP=[0.75]hrs,
275 Continuous simulation parameters:
276 IaRECper=[4] (hrs),
277 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
278 InterEventTime=[12] (hrs)
279 Baseflow simulation parameters:
280 BaseFlowOption=[1] ,
281 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
282 VHydCond=[0.055] (mm/hr), END=-1
283 *%-----|
284 *#
285 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
286 *# of 1.20
287 *%-----|
288 CONTINUOUS NASHYD NHYD=["FL_CK"], DT=[30]min, AREA=[4945] (ha),
289 DWF=[0] (cms), CN/C=[74], IA=[2.5] (mm),
290 N=[3.0], TP=[4.45]hrs,
291 Continuous simulation parameters:
292 IaRECper=[4] (hrs),
293 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
294 InterEventTime=[12] (hrs)
295 Baseflow simulation parameters:
296 BaseFlowOption=[1] ,
297 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
298 VHydCond=[0.055] (mm/hr), END=-1
299 *%-----|
300 CONTINUOUS NASHYD NHYD=["SW_5A2"], DT=[30]min, AREA=[20] (ha),
301 DWF=[0] (cms), CN/C=[81], IA=[2.5] (mm),
302 N=[3.0], TP=[0.62]hrs,
303 Continuous simulation parameters:
304 IaRECper=[4] (hrs),
305 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
306 InterEventTime=[12] (hrs)
307 Baseflow simulation parameters:
308 BaseFlowOption=[1] ,
309 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
310 VHydCond=[0.055] (mm/hr), END=-1
311 *%-----|
312 *#
313 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
314 *# of 1.61
315 *%-----|
316 CONTINUOUS NASHYD NHYD=["SW_5A1"], DT=[30]min, AREA=[1412] (ha),
317 DWF=[0] (cms), CN/C=[75], IA=[2.5] (mm),
318 N=[3.0], TP=[8.00]hrs,
319 Continuous simulation parameters:
320 IaRECper=[4] (hrs),
321 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
322 InterEventTime=[12] (hrs)
323 Baseflow simulation parameters:
324 BaseFlowOption=[1] ,
325 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
326 VHydCond=[0.055] (mm/hr), END=-1
327 *%-----|
328 CONTINUOUS NASHYD NHYD=["SW_4"], DT=[30]min, AREA=[585] (ha),
329 DWF=[0] (cms), CN/C=[81], IA=[2.5] (mm),
330 N=[3.0], TP=[1.75]hrs,

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331 Continuous simulation parameters:
332 IaREcper=[4] (hrs),
333 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
334 InterEventTime=[12] (hrs)
335 Baseflow simulation parameters:
336 BaseFlowOption=[1] ,
337 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
338 VHydCond=[0.055] (mm/hr), END=-1
339 *%-----|
340 CONTINUOUS NASHYD NHYD=["LM_CK"], DT=[30]min, AREA=[1021] (ha),
341 DWF=[0] (cms), CN/C=[80], IA=[2.5] (mm),
342 N=[3.0], TP=[2.46]hrs,
343 Continuous simulation parameters:
344 IaREcper=[4] (hrs),
345 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
346 InterEventTime=[12] (hrs)
347 Baseflow simulation parameters:
348 BaseFlowOption=[1] ,
349 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
350 VHydCond=[0.055] (mm/hr), END=-1
351 *%-----|
352 CONTINUOUS NASHYD NHYD=["SW_2"], DT=[30]min, AREA=[177] (ha),
353 DWF=[0] (cms), CN/C=[77], IA=[2.5] (mm),
354 N=[3.0], TP=[0.75]hrs,
355 Continuous simulation parameters:
356 IaREcper=[4] (hrs),
357 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
358 InterEventTime=[12] (hrs)
359 Baseflow simulation parameters:
360 BaseFlowOption=[1] ,
361 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
362 VHydCond=[0.055] (mm/hr), END=-1
363 *%-----|
364 CONTINUOUS NASHYD NHYD=["SM_DR"], DT=[30]min, AREA=[1122] (ha),
365 DWF=[0] (cms), CN/C=[81], IA=[2.5] (mm),
366 N=[3.0], TP=[3.25]hrs,
367 Continuous simulation parameters:
368 IaREcper=[4] (hrs),
369 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
370 InterEventTime=[12] (hrs)
371 Baseflow simulation parameters:
372 BaseFlowOption=[1] ,
373 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
374 VHydCond=[0.055] (mm/hr), END=-1
375 *%-----|
376 CONTINUOUS NASHYD NHYD=["MO_DR"], DT=[30]min, AREA=[2737] (ha),
377 DWF=[0] (cms), CN/C=[76], IA=[2.5] (mm),
378 N=[3.0], TP=[3.03]hrs,
379 Continuous simulation parameters:
380 IaREcper=[4] (hrs),
381 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
382 InterEventTime=[12] (hrs)
383 Baseflow simulation parameters:
384 BaseFlowOption=[1] ,
385 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
386 VHydCond=[0.055] (mm/hr), END=-1
387 *%-----|
388 CONTINUOUS NASHYD NHYD=["SW_1"], DT=[30]min, AREA=[3176] (ha),
389 DWF=[0] (cms), CN/C=[78], IA=[2.5] (mm),
390 N=[3.0], TP=[3.56]hrs,
391 Continuous simulation parameters:
392 IaREcper=[4] (hrs),
393 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
394 InterEventTime=[12] (hrs)
395 Baseflow simulation parameters:
396 BaseFlowOption=[1] ,

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397          InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
398          VHydCond=[0.055] (mm/hr),   END=-1
399  *%-----|-----
400  *#
401  *# Routing hydrographs
402  *#
403  *# Starting with the addition of Jock River Headwater and Subwatershed 13
404  *#
405  ADD HYD          NHYDsum=["S_N13"], NHYDs to add=["JR_HW"+"SW_13"]
406  *%-----|-----
407  *#
408  *# Sum of hydrographs from Node 13 routed to Node 13A
409  *# (Approximated cross-section - see cross-section 258)
410  *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
411  *#
412  ROUTE CHANNEL    NHYDout=["N13A"] ,NHYDin=["S_N13"],
413                      RDT=[30] (min),
414                      CHLGTH=[9074] (m),   CHSLOPE=[0.0220] (%),
415                      FPSLOPE=[0.0220] (%),
416                      SECNUM=[1.0],       NSEG=[1]
417                      ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
418                      ( DISTANCE (m), ELEVATION (m))=
419                      [-40, 132.5]
420                      [-30, 132]
421                      [-25, 131.5]
422                      [-13, 130]
423                      [-8, 127.00]
424                      [-7, 126.50]
425                      [-6, 126]
426                      [-5.5, 125.50]
427                      [0, 123.75]
428                      [4.5, 125.50]
429                      [6, 126]
430                      [7.5, 126.5]
431                      [9, 127]
432                      [10, 127.5]
433                      [11.5, 128.0]
434                      [15.5, 129.5]
435  *%-----|-----
436  *#
437  *# Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
438  *#
439  ADD HYD          NHYDsum=["SN13A"], NHYDs to add=["N13A"+"JR_GWM"]
440  *%-----|-----
441  *#
442  *# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
443  *#
444  ROUTE RESERVOIR NHYDout=["RES_GM"] ,NHYDin=["SN13A"],
445                      RDT=[30] (min),
446                      TABLE of ( OUTFLOW-STORAGE ) values
447                      (cms) - (ha-m)
448                      [ 0.0 , 0.0 ]
449                      [1.991, 2.144 ]
450                      [2.693, 39.826 ]
451                      [3.509, 81.697 ]
452                      [4.578, 318.774 ]
453                      [5.647, 594.947 ]
454                      [7.109, 910.219 ]
455                      [8.616, 1264.589 ]
456                      [10.371, 1658.057 ]
457                      [12.402, 2090.622 ]
458                      [22.056, 3462.487 ]
459                      [ -1 , -1 ] (max twenty pts)
460                      NHYDovf=[" " ] ,
461  *%-----|-----
462  *#

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463 SAVE HYD          NHYD=["RES_GM"], # OF PCYCLES=[-1], ICASEsh=[-1]
464                      HYD_FILENAME=["H_RESGM"]
465                      HYD_COMMENT=["Outflow from Res GM"]
466 *%-----|-----
467 *# Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
468 *# (Approximated cross-section - see cross-section 258)
469 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
470 ROUTE CHANNEL    NHYDout=["N12"] ,NHYDin=["RES_GM"] ,
471                      RDT=[30] (min),
472                      CHLGTH=[5926] (m),  CHSLOPE=[0.0759] (%),
473                      FPSLOPE=[0.0759] (%),
474                      SECNUM=[1.0],        NSEG=[1]
475                      ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
476                      ( DISTANCE (m), ELEVATION (m))=
477                      [-40, 132.5]
478                      [-30, 132]
479                      [-25, 131.5]
480                      [-13, 130]
481                      [-8, 127.00]
482                      [-7, 126.50]
483                      [-6, 126]
484                      [-5.5, 125.50]
485                      [0, 123.75]
486                      [4.5, 125.50]
487                      [6, 126]
488                      [7.5, 126.5]
489                      [9, 127]
490                      [10, 127.5]
491                      [11.5, 128.00]
492                      [15.5, 129.5]
493 *%-----|-----
494 *#
495 *# Addition of Subwatershed Jock River at Ashton to Node 12
496 *#
497 ADD HYD          NHYDsum=["S_N12"], NHYDs to add=["N12"+"JR_ASH"]
498 SAVE HYD          NHYD=["S_N12"], # OF PCYCLES=[-1], ICASEsh=[-1]
499                      HYD_FILENAME=["H_SN12"]
500                      HYD_COMMENT=["flow at S_N12 near Ashton"]
501 *%-----|-----
502 *#
503 *# Sum of hydrographs from Node 12 routed to Node 11
504 *# (Approximated cross-section - see cross-section 258)
505 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
506 ROUTE CHANNEL    NHYDout=["N11"] ,NHYDin=["S_N12"] ,
507                      RDT=[30] (min),
508                      CHLGTH=[972] (m),  CHSLOPE=[0.0514] (%),
509                      FPSLOPE=[0.0514] (%),
510                      SECNUM=[1.0],        NSEG=[1]
511                      ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
512                      ( DISTANCE (m), ELEVATION (m))=
513                      [-40, 132.5]
514                      [-30, 132]
515                      [-25, 131.5]
516                      [-13, 130]
517                      [-8, 127.00]
518                      [-7, 126.50]
519                      [-6, 126]
520                      [-5.5, 125.50]
521                      [0, 123.75]
522                      [4.5, 125.50]
523                      [6, 126]
524                      [7.5, 126.5]
525                      [9, 127]
526                      [10, 127.5]
527                      [11.5, 128.00]
528                      [15.5, 129.5]

```



```

595 *#
596 *# Addition of Subwatershed 10 to Node 10
597 *#
598 ADD HYD          NHYDsum=["S_N10"], NHYDs to add=["N10"+"SW_10"]
599 *%-----|-----
600 SAVE HYD        NHYD=["S_N10"], # OF PCYCLES=[-1], ICASEsh=[-1]
601                HYD_FILENAME=["H_SN10"]
602                HYD_COMMENT=["flow at S_N10: N10 + SW_10"]
603 *%-----|-----
604 *# Addition of Kings Creek to S_N10
605 *#
606 ADD HYD          NHYDsum=["S_N10A"], NHYDs to add=["S_N10"+"KG_CK"]
607 *%-----|-----
608 *#
609 *# Sum of hydrographs from Node 10 routed to Node 9
610 *# Section 2
611 *#
612 ROUTE CHANNEL   NHYDout=["N9"] ,NHYDin=["S_N10A"] ,
613                RDT=[30] (min),
614                CHLGTH=[3982] (m),  CHSLOPE=[0.0753] (%),
615                FPSLOPE=[0.0753] (%),
616                SECNUM=[1.0],      NSEG=[4]
617                ( SEGROUGH, SEGDIST (m))=
618                [0.04,-30.27
619                0.05,-18.42
620                -0.05,18.42
621                0.04,131.58] NSEG times
622                ( DISTANCE (m), ELEVATION (m))=
623                [-446.74, 106.00]
624                [-415.68, 105.50]
625                [-285.40, 105.00]
626                [-173.77, 104.50]
627                [-144.95, 104.00]
628                [-111.18, 103.50]
629                [-94.06, 103.00]
630                [-71.02, 102.50]
631                [-30.27, 102.00]
632                [-19.33, 100.00]
633                [-18.42, 99.50]
634                [18.42, 99.50]
635                [20.77, 100.00]
636                [27.93, 101.00]
637                [52.29, 101.00]
638                [68.80, 101.50]
639                [79.66, 103.00]
640                [91.50, 103.50]
641                [131.58, 104.00]
642 *%-----|-----
643 *#
644 *# Addition of Subwatershed 9 and Nichols Creek to Node 9
645 *#
646 ADD HYD          NHYDsum=["S_N9"], NHYDs to add=["N9"+"SW_9"+"NC_CK"]
647 *%-----|-----
648 *#
649 *# Sum of hydrographs from Node 9 routed to Node 8
650 *# Section 3
651 *#
652 ROUTE CHANNEL   NHYDout=["N8"] ,NHYDin=["S_N9"] ,
653                RDT=[30] (min),
654                CHLGTH=[2269] (m),  CHSLOPE=[0.0882] (%),
655                FPSLOPE=[0.0882] (%),
656                SECNUM=[1.0],      NSEG=[3]
657                ( SEGROUGH, SEGDIST (m))=
658                [0.1,-17.99
659                -0.045,17.31
660                0.1,456.58] NSEG times

```

```

661      ( DISTANCE (m), ELEVATION (m))=
662          [-201.19,100.50]
663          [-135.21, 100.00]
664          [-94.83, 99.50]
665          [-67.05, 99.00]
666          [-17.99, 98.50]
667          [-16.02, 98.00]
668          [-13.95, 97.50]
669          [13.95, 97.50]
670          [15.64, 98.00]
671          [17.31, 98.50]
672          [162.02, 98.50]
673          [172.89 ,99.00]
674          [314.38, 99.00]
675          [343.78, 99.50]
676          [365.67, 100.00]
677          [376.68, 100.00 ]
678          [393.11, 99.50]
679          [404.97, 99.50]
680          [431.70, 100.00]
681          [456.58, 100.50 ]
682  *%-----|-----
683  *#
684  *# Addition of Subwatershed 8 and Hobb's Drain to Node 8
685  *#
686  ADD HYD          NHYDsum=["S_N8"], NHYDs to add=["N8"+"SW_8"+"HB_DR"]
687  *%-----|-----
688  *#
689  *# Sum of hydrographs from Node 8 routed to Node 7
690  *# Section 4
691  *#
692  ROUTE CHANNEL   NHYDout=["N7"] ,NHYDin=["S_N8"],
693                    RDT=[30] (min) ,
694                    CHLGTH=[3750] (m),   CHSLOPE=[0.0533] (%),
695                                          FPSLOPE=[0.0533] (%),
696                    SECNUM=[1.0],       NSEG=[3]
697                    ( SEGROUGH, SEGDIST (m))=
698                      [0.12,-18.11
699                      -0.07,17.22
700                      0.12,590.05] NSEG times
701      ( DISTANCE (m), ELEVATION (m))=
702          [-433.21, 102.00]
703          [-425.34, 101.50]
704          [-377.56, 101.50]
705          [-366.23, 101.00]
706          [-202.60, 100.50]
707          [-96.25, 99.50]
708          [-68.36 99.00]
709          [-18.11, 98.50]
710          [-13.81, 97.50]
711          [13.81, 97.50]
712          [17.22, 98.50]
713          [161.95, 98.50]
714          [173.11, 99.00]
715          [314.05, 99.00]
716          [365.52, 100.00]
717          [404.70, 99.50]
718          [476.74, 100.50]
719          [502.31, 101.00]
720          [584.69, 101.00]
721          [585.79, 101.00]
722          [590.05, 102.00]
723  *%-----|-----
724  *#
725  *# Addition of Subwatershed 7 to Node 7
726  *#

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```

727 ADD HYD          NHYDsum=["S_N7"], NHYDs to add=["N7"+"SW_7"]
728 *%-----|-----|
729 SAVE HYD        NHYD=["S_N7"], # OF PCYCLES=[-1], ICASEsh=[-1]
730                HYD_FILENAME=["H_SN7"]
731                HYD_COMMENT=["flow at S_N7: N7 + SW_7"]
732 *%-----|-----|
733 *# Insertion of a reservoir to simulate the effects of the Richmond Fen.
734 *# Storage area and volumes were estimated from available topo maps.
735 *# Release rate from fen was assumed to be controlled by the downstream
736 *# river cross-section for summer conditions. It is was assumed that for up to
737 *# 0.75 m of water, the main channel of the river provided the storage. Above
738 *# this depth, the wetland starts to signigicantly store water.
739 *#
740 ROUTE RESERVOIR NHYDout=["RES_RF"] ,NHYDin=["S_N7"] ,
741                RDT=[30] (min),
742                TABLE of ( OUTFLOW-STORAGE ) values
743                (cms) - (ha-m)
744                TABLE of ( OUTFLOW-STORAGE ) values
745                (cms) - (ha-m)
746                [ 0.0 , 0.0 ]
747                [0.9051, 2.40]
748                [2.907, 4.13]
749                [9.744, 9.18]
750                [20.304, 14.96]
751                [34.167, 310.21]
752                [74.993, 605.46]
753                [104.876, 900.71]
754                [140.56, 2892.00]
755                [225.00, 3615.63]
756                [ -1 , -1 ] (max twenty pts)
757                NHYDovf=[" " ] ,
758 *%-----|-----|
759 SAVE HYD        NHYD=["RES_RF"], # OF PCYCLES=[-1], ICASEsh=[-1]
760                HYD_FILENAME=["H_ResRF"]
761                HYD_COMMENT=["outflow of Richmond Fen"]
762 *%-----|-----|
763 *#
764 *# Sum of hydrographs from Node 7 routed to Node 6
765 *# Section 5
766 *#
767 ROUTE CHANNEL   NHYDout=["N6"] ,NHYDin=["RES_RF"] ,
768                RDT=[30] (min),
769                CHLGTH=[3056] (m), CHSLOPE=[0.0818] (%),
770                FPSLOPE=[0.0818] (%),
771                SECNUM=[1.0], NSEG=[5]
772                ( SEGROUGH, SEGDIST (m))=
773                [0.025,-70.8
774                0.1,-23.9
775                -0.05,23.9
776                0.06,39.8
777                0.05,96.3] NSEG times
778                ( DISTANCE (m), ELEVATION (m))=
779                [-100.8, 97.00]
780                [-70.8, 96.50]
781                [-52.0, 96.00]
782                [-35.1, 95.50]
783                [-30.6, 95.00]
784                [-23.9, 94.54]
785                [23.9, 94.54]
786                [39.8, 95.00]
787                [50.4, 95.50]
788                [93.5, 96.00]
789                [94.9, 96.50]
790                [96.3, 97.00]
791 *%-----|-----|
792 *#

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793  *# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
794  *#
795  ADD HYD          NHYDsum=["S_N6"], NHYDs to add=["N6"+"SW_6"+"VG_DR"]
796  *%-----|-----
797  *#
798  *# Sum of hydrographs from Node 6 routed to Node 5
799  *# Section 6
800  *#
801  ROUTE CHANNEL    NHYDout=["N5"] ,NHYDin=["S_N6"] ,
802                  RDT=[30] (min),
803                  CHLGTH=[1852] (m),  CHSLOPE=[0.0540] (%),
804                                          FPSLOPE=[0.0540] (%),
805                  SECNUM=[1.0],      NSEG=[3]
806                  ( SEGROUGH, SEGDIST (m))=
807                    [0.035,-131.59
808                     -0.045,48.96
809                     0.1,239.04] NSEG times
810                  ( DISTANCE (m), ELEVATION (m))=
811                    [-686.30, 94.50]
812                    [-675.70, 94.00]
813                    [-492.52, 93.00]
814                    [-467.28, 94.00]
815                    [-131.59, 94.00]
816                    [-92.79, 92.50]
817                    [-18.06, 91.00]
818                    [18.06, 91.00]
819                    [43.47, 92.50]
820                    [48.96, 94.00]
821                    [177.43, 94.00]
822                    [239.04,94.50]
823  *%-----|-----
824  *#
825  *# Addition of Subwatershed 5 and Flowing Creek to Node 5
826  *#
827  ADD HYD          NHYDsum=["S_N5"], NHYDs to add=["N5"+"SW_5"+"FL_CK"]
828  *%-----|-----
829  *#
830  *# Sum of hydrographs from Node 5 routed to Node 5A
831  *# Section 7
832  *#
833  ROUTE CHANNEL    NHYDout=["N5A"] ,NHYDin=["S_N5"] ,
834                  RDT=[30] (min),
835                  CHLGTH=[556] (m),  CHSLOPE=[0.0900] (%),
836                                          FPSLOPE=[0.0900] (%),
837                  SECNUM=[1.0],      NSEG=[4]
838                  ( SEGROUGH, SEGDIST (m))=
839                    [0.04,-41.5
840                     0.1,-14.0
841                     -0.045,14.0
842                     0.1,41.1] NSEG times
843                  ( DISTANCE (m), ELEVATION (m))=
844                    [-275.8, 93.00]
845                    [-248.6, 92.50]
846                    [-237.0, 92.00]
847                    [-219.3, 91.50]
848                    [-202.1, 91.50]
849                    [-186.0, 92.00]
850                    [-129.2, 92.00]
851                    [-117.6, 91.50]
852                    [-100.6, 91.00]
853                    [-41.5, 91.00]
854                    [-20.0, 91.00]
855                    [-14.0, 90.54]
856                    [14.0, 90.54]
857                    [15.3, 91.00]
858                    [17.3, 91.50]

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859                                     [38.4, 92.00]
860                                     [39.8, 92.50]
861                                     [41.1, 93.00]
862 *%-----|-----
863 *#
864 *# Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
865 *#
866 ADD HYD                NHYDsum=["S_N5A"], NHYDs to add=["N5A"+"SW_5A2"+"SW_5A1"]
867 *%-----|-----
868 *#
869 *# Sum of hydrographs from Node 5A routed to Node 4
870 *# Section 8
871 *#
872 ROUTE CHANNEL        NHYDout=["N4"] ,NHYDin=["S_N5A"] ,
873                          RDT=[30] (min),
874                          CHLGTH=[4630] (m),  CHSLOPE=[0.0432] (%),
875                          FPSLOPE=[0.0432] (%),
876                          SECNUM=[1.0],      NSEG=[3]
877                          ( SEGROUGH, SEGDIST (m))=
878                          [0.05,-28.2
879                          -0.035,28.2
880                          0.05,173.1] NSEG times
881                          ( DISTANCE (m), ELEVATION (m))=
882                                     [-38.9, 92.00]
883                                     [-35.8, 91.50]
884                                     [-33.3, 91.00]
885                                     [-28.2, 90.50]
886                                     [-15.0, 87.48]
887                                     [-5.0, 88.34]
888                                     [5.0, 86.20]
889                                     [15.0, 88.55]
890                                     [28.2, 90.50]
891                                     [29.7, 91.00]
892                                     [46.5, 91.00]
893                                     [127.8, 91.00]
894                                     [148.7, 91.50]
895                                     [173.1, 92.00]
896 *%-----|-----
897 *#
898 *# Addition of Subwatershed 4 and Leamy Creek to Node 4
899 *#
900 ADD HYD                NHYDsum=["S_N4"], NHYDs to add=["N4"+"SW_4"+"LM_CK"]
901 SAVE HYD              NHYD=["S_N4"], # OF PCYCLES=[-1], ICASEsh=[1]
902                          HYD_COMMENT=["flow at S_N4"]
903 *%-----|-----
904 *#
905 *# Sum of hydrographs from Node 4 routed to Node 2
906 *# Section 9
907 *#
908 ROUTE CHANNEL        NHYDout=["N2"] ,NHYDin=["S_N4"] ,
909                          RDT=[30] (min),
910                          CHLGTH=[1667] (m),  CHSLOPE=[0.0600] (%),
911                          FPSLOPE=[0.0600] (%),
912                          SECNUM=[1.0],      NSEG=[4]
913                          ( SEGROUGH, SEGDIST (m))=
914                          [0.1,-28.0
915                          -0.04,28.4
916                          0.06,31.7
917                          0.04,80.2] NSEG times
918                          ( DISTANCE (m), ELEVATION (m))=
919                                     [-36.3, 92.00]
920                                     [-32.6, 91.50]
921                                     [-30.2, 91.00]
922                                     [-28.0, 90.45]
923                                     [-15.0, 87.48]
924                                     [-5.0, 88.34]

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925             [5.0, 86.20]
926             [15.0, 88.55]
927             [28.0, 90.45]
928             [28.4, 90.50]
929             [30.4, 91.00]
930             [31.7, 91.50]
931             [80.2, 92.00]
932 *%-----|-----
933 *#
934 *# Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2
935 *#
936 ADD HYD           NHYDsum=["S_N2"], NHYDs to add=["N2"+"SW_2"+"SM_DR"+"MO_DR"]
937 *%-----|-----
938 SAVE HYD        NHYD=["S_N2"], # OF PCYCLES=[-1], ICASEsh=[-1]
939                   HYD_FILENAME=["H_SN2"]
940                   HYD_COMMENT=["flow at S_N2 Jock River Gauge at Moodie Dr."]
941 *%-----|-----
942 *#
943 *# Sum of hydrographs from Node 2 routed to Node 1
944 *# Section 10
945 *#
946 ROUTE CHANNEL   NHYDout=["N1"] ,NHYDin=["S_N2"] ,
947                   RDТ=[30] (min),
948                   CHLGTH=[10046] (m),  CHSLOPE=[0.0498] (%),
949                                           FPSLOPE=[0.0498] (%),
950                   SECNUM=[1.0],        NSEG=[5]
951                   ( SEGRROUGH, SEGDIST (m))=
952                     [0.04,-27.6
953                     0.06,-15.0
954                     -0.045,15.0
955                     0.06,25.4
956                     0.04,122.6] NSEG times
957                   ( DISTANCE (m), ELEVATION (m))=
958                     [-87.0, 91.50]
959                     [-32.4, 91.00]
960                     [-27.6, 90.50]
961                     [-25.0, 90.00]
962                     [-22.9, 89.57]
963                     [-15.0, 86.20]
964                     [-5.0, 84.83]
965                     [5.0, 84.83]
966                     [15.0, 88.11]
967                     [22.9, 89.57]
968                     [25.4, 90.00]
969                     [27.9, 90.50]
970                     [38.0, 91.00]
971                     [112.5, 91.00]
972                     [114.3, 90.50]
973                     [115.1, 90.26]
974                     [116.3, 90.50]
975                     [119.0, 91.00]
976                     [121.0, 91.50]
977                     [122.6, 92.00]
978 *%-----|-----
979 *#
980 *# Addition of Subwatershed 1 to Node 1
981 *#
982 ADD HYD           NHYDsum=["N1"], NHYDs to add=["N1"+"SW_1"]
983 SAVE HYD        NHYD=["N1"], # OF PCYCLES=[-1], ICASEsh=[1]
984                   HYD_COMMENT=["total outflow of Jock River"]
985 *%-----|-----
986 *#####
987 *% 5 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
988 START           TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[5]
989 *%               ["C24SC005.stm"] <--storm filename, one per line for NSTORM time
990 *%-----|-----

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```
991  *% 10 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
992  START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[10]
993  *%              ["C24SC010.stm"] <--storm filename, one per line for NSTORM time
994  *%-----|-----|
995  *% 25 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
996  START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[25]
997  *%              ["C24SC025.stm"] <--storm filename, one per line for NSTORM time
998  *%-----|-----|
999  *% 50 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
1000 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[50]
1001 *%              ["C24SC050.stm"] <--storm filename, one per line for NSTORM time
1002 *%-----|-----|
1003 *% 100 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
1004 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
1005 *%              ["C24SC100.stm"] <--storm filename, one per line for NSTORM time
1006 FINISH
1007
```


00749# CONTINUOUS NASIDD 30 01:SW.SAI 1412.00 4.515 N_date 37:30 21.96 384 .000
00750# [C# 75.00 No. 3.00: Tm= 1.75]
00751# [I#RE 4.00 SM_N 15.31: SMNW=225.43: SK# 010]

00936# 00936# R0005:CO05050.....Dfm-I-D NND.....AREAb-QPEAKm-TpeakDte-hh:mm- Rvmr R C- -Dfwm
00938# ADD HYD 30 02: N7 35546.00 46.889 N_date 45:00 17.17 n/a .000
00939# [R#D=30.00] out c. 30 01: N7 3197.00 6.873 N_date 58:00 13.87 n/a .000

JFSainc.
Page 2

Table with columns for ID, description, and numerical values. The table contains detailed project information for various nodes (e.g., 02619 to 02995), including comments, coordinates, and specific parameters like flow rates and dates. The data is organized in a grid format with multiple columns for each entry.


```

02993 #
02984 # Sum of hydrographs from Node 6 routed to Node 5
02985 # Section 6
02986 #
02997 R0100: C00056..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
02998 ROUTE CHANNEL > 30.0 02: S_N 40240.01 60.383 No.date 59:30 36.31 n/a .000
02999 [RDF=30.00] out< 30.0 01: NSA 40240.01 60.383 No.date 60:30 36.31 n/a .000
03000 [L/S/n= 1852. / 054/ 035]
03001 [Vmax= .490; Dmax= 1.346]
03002 #
03003 # Addition of Subwatershed 5 and Flowing Creek to Node 5
03004 #
03005 R0100: C00057..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03006 ADD HYD + 30.0 02: S_N 45409.01 79.891 No.date 34:00 37.22 n/a .000
03007 + 30.0 02: SW_S 224.00 9.294 No.date 28:30 47.59 n/a .000
03008 + 30.0 02: FL_CK 4845.00 51.121 No.date 33:00 44.15 n/a .000
03009 SUM 30.0 01: S_N 45409.01 79.891 No.date 34:00 37.22 n/a .000
03010 #
03011 # Sum of hydrographs from Node 5 routed to Node 5A
03012 # Section 7
03013 #
03014 R0100: C00058..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03015 ROUTE CHANNEL > 30.0 02: S_N 45409.01 79.891 No.date 34:00 37.22 n/a .000
03016 [RDF=30.00] out< 30.0 01: NSA 45409.01 79.815 No.date 34:00 37.22 n/a .000
03017 [L/S/n= 556. 090/ 040]
03018 [Vmax= .544; Dmax= 1.346]
03019 #
03020 # Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
03021 #
03022 R0100: C00059..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03023 ADD HYD + 30.0 02: NSA 45409.01 79.815 No.date 34:00 37.22 n/a .000
03024 + 30.0 02: SW_S 20.00 1.014 No.date 28:30 52.03 n/a .000
03025 + 30.0 02: SW_S 1412.00 9.804 No.date 37:30 48.85 n/a .000
03026 SUM 30.0 01: S_N 46841.01 88.619 No.date 34:30 37.48 n/a .000
03027 #
03028 # Sum of hydrographs from Node 5A routed to Node 4
03029 # Section 8
03030 #
03031 R0100: C00060..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03032 ROUTE CHANNEL > 30.0 02: S_N 46841.01 88.619 No.date 34:30 37.48 n/a .000
03033 [RDF=30.00] out< 30.0 01: NI 46841.01 84.955 No.date 36:00 37.48 n/a .000
03034 [L/S/n= 4630. / 043/ 051]
03035 [Vmax= .901; Dmax= 3.849]
03036 #
03037 # Addition of Subwatershed 4 and Leamy Creek to Node 4
03038 #
03039 R0100: C00061..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03040 ADD HYD + 30.0 02: NI 46841.01 84.955 No.date 36:00 37.48 n/a .000
03041 + 30.0 02: SW_C 585.00 14.684 No.date 29:30 52.03 n/a .000
03042 + 30.0 02: FL_CK 1021.00 19.515 No.date 30:30 51.13 n/a .000
03043 SUM 30.0 01: S_N 48447.00 95.694 No.date 34:30 37.95 n/a .000
03044 R0100: C00062..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03045 SAVE HYD + 30.0 01: S_N 48447.00 95.694 No.date 34:30 37.95 n/a .000
03046 fname= S_N1.0100
03047 remark: flow at S_N1
03048 #
03049 # Sum of hydrographs from Node 4 routed to Node 2
03050 # Section 9
03051 #
03052 R0100: C00063..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03053 ROUTE CHANNEL > 30.0 02: S_N 48447.00 95.694 No.date 34:30 37.95 n/a .000
03054 [RDF=30.00] out< 30.0 01: NI 48447.00 95.342 No.date 35:00 37.95 n/a .000
03055 [L/S/n= 1667. / 060/ 040]
03056 [Vmax= .942; Dmax= 3.915]
03057 #
03058 # Addition of Subwatershed 2 with Mnohan Drain and Smith Drain to Node 2
03059 #
03060 R0100: C00064..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03061 ADD HYD + 30.0 02: NI 48447.00 95.342 No.date 35:00 37.95 n/a .000
03062 + 30.0 02: SW_C 177.00 7.344 No.date 28:30 47.59 n/a .000
03063 + 30.0 02: MD_DR 1122.00 17.710 No.date 31:30 52.03 n/a .000
03064 + 30.0 02: MD_DR 2737.00 40.026 No.date 31:00 46.72 n/a .000
03065 SUM 30.0 01: S_N 52483.00 141.415 No.date 32:30 38.74 n/a .000
03066 R0100: C00065..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03067 SAVE HYD + 30.0 01: S_N 52483.00 141.415 No.date 32:30 38.74 n/a .000
03068 fname= S_N2.0100
03069 remark: flow at S_N2 Jock River Gauge at Moudie Dr.
03070 #
03071 # Sum of hydrographs from Node 2 routed to Node 1
03072 # Section 10
03073 #
03074 R0100: C00066..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03075 ROUTE CHANNEL > 30.0 02: S_N 52483.00 141.415 No.date 32:30 38.74 n/a .000
03076 [RDF=30.00] out< 30.0 01: NI 52483.00 124.304 No.date 35:00 38.74 n/a .000
03077 [L/S/n=1046. / 050/ 040]
03078 [Vmax= 1.091; Dmax= 4.553]
03079 #
03080 # Addition of Subwatershed 1 to Node 1
03081 #
03082 R0100: C00067..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03083 ADD HYD + 30.0 02: NI 52483.00 124.304 No.date 35:00 38.74 n/a .000
03084 + 30.0 02: SW_C 3176.00 43.079 No.date 32:00 48.46 n/a .000
03085 SUM 30.0 01: NI 55659.00 158.420 No.date 34:00 39.29 n/a .000
03086 R0100: C00068..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03087 SAVE HYD + 30.0 01: NI 55659.00 158.420 No.date 34:00 39.29 n/a .000
03088 fname= NI.0100
03089 remark: initial outflow of Jock River
03090 *****
03091 R0100: C0002.....
03092 FLSN1
03093 *****
03094 *****
03095 *****
03096 *****
03097 R0002: C00015 CONTINUES NASHID
03098 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03099 R0002: C00020 CONTINUES NASHID
03100 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03101 R0002: C00022 CONTINUES NASHID
03102 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03103 R0002: C00026 CONTINUES NASHID
03104 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03105 R0005: C00015 CONTINUES NASHID
03106 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03107 R0005: C00020 CONTINUES NASHID
03108 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03109 R0005: C00022 CONTINUES NASHID
03110 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03111 R0005: C00026 CONTINUES NASHID
03112 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03113 R0010: C00015 CONTINUES NASHID
03114 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03115 R0010: C00020 CONTINUES NASHID
03116 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03117 R0010: C00022 CONTINUES NASHID
03118 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03119 R0010: C00026 CONTINUES NASHID
03120 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03121 R0025: C00015 CONTINUES NASHID
03122 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03123 R0025: C00020 CONTINUES NASHID
03124 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03125 R0025: C00022 CONTINUES NASHID
03126 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03127 R0025: C00026 CONTINUES NASHID
03128 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03129 R0050: C00015 CONTINUES NASHID
03130 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03131 R0050: C00020 CONTINUES NASHID
03132 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03133 R0050: C00022 CONTINUES NASHID
03134 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03135 R0050: C00026 CONTINUES NASHID
03136 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03137 R0100: C00015 CONTINUES NASHID
03138 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03139 R0100: C00020 CONTINUES NASHID
03140 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03141 R0100: C00022 CONTINUES NASHID
03142 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03143 R0100: C00026 CONTINUES NASHID
03144 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03145 Simulation ended on 2021-02-22 at 15:43:22
03146 *****
03147 *****
03148 *****

```

Attachment B

Model 2 – Jock River Reach One Model

Stantec, 2007

SWMHYMO Input & Summary files

```

1 2 Metric units
2 *****
3 *# Project Name: [Jock River Reach 1 SubWatershed Study]Project #: [160400414]
4 *# Date : October 2006
5 *# Mdeller : [Navin Gautam/ Original by Ana M Paerez]
6 *# Company : Stantec.
7 *# License # : 3824306
8 *****
9 START TZERO=[ 0.0], METOUT=[ 2], NSTORM=[ 1], NRUN=[ 002]
10 *% ["C24SC002.stm"] <--storm filename, one per line for NSTORMtime
11 *#-----|-----|
12 READ STORM STORM_FILENAME=[ "st or m 001"]
13 *%-----|-----|
14 MODIFY STORM I CASEms=[ 1], NSHIFT=[ 96],
15 RedFACT=[ 1],
16 *%-----|-----|
17 DEFAULT VALUES I CASEdv=[ 1], read and print values
18 DEFVAL_FILENAME=[ "MODIFIED.VAL"]
19 COMPUTE API API I=[ 50], API K=[. 85]/day
20 *****
21 *#
22 *# JOCK RIVER REACH 1 SUBWATERSHED STUDY DISCRETIZED MODEL
23 *# PROPOSED CONDITIONS DESIGN STORM MODEL (SUMMER)
24 *#
25 *# Version: Draft Final Report, October 2006
26 *# Revision History
27 *# -Draft Interim Condition Report, Nov. 2005
28 *****
29 *# Assumptions
30 *# - All catchments are assumed to be developed except S-1, S-2, and SW1a
31 *# - SWM facilities are modeled
32 *# - Rating curves were estimated based on existing reports and modeling for the
33 *# proposed SWM facilities
34 *# - The rating curve for the existing Kennedy Burnett SWM Facility was obtained from
35 *# the Urban Runoff Treatment in the Kennedy Burnett Settling Pond (URTKBP)- Regional
36 *# Municipality of Ottawa Carleton, March 1983
37 *# - River routing modeled
38 *# - River cross sections obtained from RVCA's HEC-RAS hydraulic model
39 *#-----|-----|
40 *# Parameters
41 *# - Design Storms: 2, 5, 10, 25, 50 & 100yr events: 24hr SCS (DT=10min)-model comparison
42 *# - Impervious area weighted based on: rural subdivision @0% urban @5%
43 *# - NRCS(SCS) CN based on landuse (airphoto) and soil type (base mapping)
44 *# - Time to peak using Uplands Method
45 *#-----|-----|
46 *****
47 *#Read hydrograph upstream of N2 from RVCA Jock R. floodrisk watershed modeling
48 *****
49 READ HYD ID=[ 1 ], NHYD=[ "S_N2" ],
50 HYD_FILENAME=[ "H-S_N2" ]
51 *%-----|-----|
52 *#
53 *# Hydrograph from Node 2 routed to Node 416
54 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 9025
55 *#
56 ROUTE CHANNEL IDout=[ 4], NHYD=[ "N_416" ], IDin=[ 1 ],
57 RDT=[ 10] (min),
58 CHLGTH=[ 2327] (m), CHSLOPE=[ 0.0498] (%),
59 FPSLOPE=[ 0.0498] (%),
60 SECNUM=[ 1.0], NSEG=[ 3]
61 ( SEGROUGH, SEGDIST (m) )=
62 [ 0.075, -23.96
63 -0.055, 23.96
64 0.075, 157.38] NSEG times
65 ( DISTANCE (m), ELEVATION (m) )=
66 [-336.97, 93.5]

```

```

67 [- 318. 85, 93]
68 [- 259, 92. 5]
69 [- 133. 18, 92]
70 [- 33. 17, 92]
71 [- 27. 21, 92]
72 [- 26. 14, 91. 5]
73 [- 24. 99, 91]
74 [- 23. 96, 90. 5]
75 [- 14. 33, 88. 26]
76 [- 0. 68, 88. 12]
77 [14. 33, 88. 26]
78 [23. 96, 90. 5]
79 [32. 12, 91]
80 [43. 74, 91. 5]
81 [57. 09, 92]
82 [73. 53, 92. 5]
83 [108. 27, 93]
84 [125. 88, 93. 5]
85 [144. 81, 94]
86 [157. 38, 94. 5]
87 *%-----|-----|
88 *#*****|
89 *# Catchment SW1a
90 *# - Portion of RVCA catchment SW1 outside of Reach 1 subwatershed
91 *# - Undeveloped agricultural land
92 *#*****|
93 CONTINUOUS NASHYD ID=[ 2], NHYD=[ "SW_1a"], DT=[ 5] mi n, AREA=[ 546] ( ha),
94 DWF=[ 0] ( cms), CN C=[ 72], IA=[ 4. 67] ( mm),
95 N=[ 3], TP=[ 2. 79] hr s,
96 Continuous simulation parameters:
97 IaRECper=[ 4] ( hr s),
98 SM N=[ - 1] ( mm), SMAX=[ - 1] ( mm), SK=[ 0. 010] / ( mm),
99 InterEvent Time=[ 12] ( hr s)
100 Baseflow simulation parameters:
101 BaseFlowOption=[ 1],
102 In it GWRes Vol=[ 50] ( mm), GWRes K=[ 0. 96] ( mm/ day/ mm)
103 VHydCond=[ 0. 055] ( mm/ hr), END=- 1
104 *%-----|-----|
105 ADD HYD IDsum=[ 3 ], NHYD=[ "SN_416"], IDsto add=[ 4, 2]
106 *%-----|-----|
107 SAVE HYD ID=[ 3 ], # OF PCYCLES=[ - 1], ICASEsh=[ 1]
108 HYD_COMMENT=[ "Total Flows at Highway 416"]
109 *%-----|-----|
110 *#
111 *# Hydrograph from Node 416 routed to Node at Okeefe drain
112 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 7245
113 *#
114 ROUTE CHANNEL IDout=[ 1], NHYD=[ "N_OK"], IDin=[ 3],
115 RDT=[ 5] ( mi n),
116 CHLGTH=[ 497] ( m), CHSLOPE=[ 0. 3018] ( %),
117 FPSLOPE=[ 0. 3018] ( %),
118 SECNUM=[ 1. 0], NSEG=[ 3]
119 ( SEGROUGH, SEGDI ST ( m)) =
120 [ 0. 075, - 19. 40
121 - 0. 055, 19. 40
122 0. 075, 377. 02] NSEG times
123 ( DI STANCE ( m), ELEVATI ON ( m)) =
124 [- 1062. 81, 93. 00]
125 [- 1061. 41, 92. 50]
126 [- 945. 91, 92. 00]
127 [- 783. 64, 91. 50]
128 [- 136. 74, 91. 00]
129 [- 134. 06, 91. 00]
130 [- 128. 97, 91. 00]
131 [- 86. 04, 91. 00]
132 [- 20. 86, 91. 00]

```

```

133      [- 20.18, 90.50]
134      [- 19.40, 90.00]
135      [- 11.68, 86.89]
136      [ 0.00, 86.10]
137      [ 12.09, 86.81]
138      [ 19.40, 90.00]
139      [ 34.68, 90.50]
140      [ 60.56, 91.00]
141      [ 170.14, 91.00]
142      [ 175.05, 90.50]
143      [ 180.29, 90.00]
144      [ 193.41, 90.00]
145      [ 195.98, 90.50]
146      [ 377.02, 92.50]
147  *%-----|-----|
148  *#*****|
149  *#      Catchment OKEEFE
150  *#      - To O Keefe drain (north of the Jock)
151  *#      - Developed with assumed 43% imp.
152  *#*****|
153  CONTINUOUS STANDHYD ID=[ 2], NHYD=["OKEEFE"], DT=[ 5](mi n), AREA=[ 448](ha),
154  XI MP=[ 0.43], TI MP=[ 0.43], DWF=[ 0](cms), LOSS=[ 2],
155  SCS curve number CN=[ 77],
156  Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 0.5](%),
157  LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n),
158  Impervious surfaces: I A i mp=[ 1.57](mm), SLPI=[ 0.5](%),
159  LGI=[ 1728](m), MNI=[ 0.013], SCI=[ 0](mi n),
160  Continuous simulation parameters:
161  I a RE C per=[ 4](hrs), I a RE C i mp=[ 4](hrs),
162  SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
163  Inter Event Ti me=[ 18](hrs), END=- 1
164
165  *#*****|
166  *#      Okeefe Pond
167  *#      - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
168  *#      and a ratio of the catchment area to the West Clarke pond rating curve
169  *#      from the MS for the next coordinates
170  *#*****|
171  ROUTE RESERVOIR I D out=[ 4], NHYD=["P_OKE"], I D i n=[ 2],
172  RDT=[ 5](mi n),
173  TABLE of ( OUTFLOW STORAGE ) values
174  ( cms ) - ( ha - m)
175  [ 0.0 , 0.0 ]
176  [ 0.20 , 1.72]
177  [ -1 , -1 ] (max twenty pts)
178  I D o v f=[ 9], NHYD o v f=["ok-OVF"]
179
180  *%-----|-----|
181  ADD HYD I D s um=[ 3 ], NHYD=["SN_OK"], I D s t o a dd=[ 1,4,9]
182  *%-----|-----|
183  SAVE HYD I D=[ 3 ], # OF PCYCLES=[ -1], I C A S E s h=[ 1]
184  HYD_COMMENT=["Total Flows at Okeefe Drain"]
185  *%-----|-----|
186  *#
187  *# Hydrograph from Node Okeefe routed to Node at Foster Drain
188  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
189  *#
190  ROUTE CHANNEL I D out=[ 1], NHYD=["N_FO"], I D i n=[ 3 ],
191  RDT=[ 5](mi n),
192  CHLGTH=[ 1183](m), CHSLOPE=[ 0.0761](%),
193  FPSLOPE=[ 0.0761](%),
194  SECNUM=[ 1.0], NSEG=[ 3]
195  ( SEGROUGH, SEGDI ST (m))=
196  [ 0.050, -33.89
197  -0.035, 31.59
198  0.050, 854.54] NSEG times

```

```

199      ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
200      [ - 1075. 50 , 93. 00 ]
201      [ - 1070. 59 , 92. 50 ]
202      [ - 1003. 21 , 92. 00 ]
203      [ - 1001. 67 , 92. 00 ]
204      [ - 986. 64 , 92. 00 ]
205      [ - 816. 61 , 91. 50 ]
206      [ - 797. 29 , 91. 00 ]
207      [ - 794. 18 , 91. 00 ]
208      [ - 775. 41 , 91. 50 ]
209      [ - 702. 63 , 91. 50 ]
210      [ - 546. 19 , 91. 50 ]
211      [ - 529. 54 , 91. 50 ]
212      [ - 323. 44 , 91. 00 ]
213      [ - 320. 71 , 91. 00 ]
214      [ - 183. 59 , 91. 00 ]
215      [ - 182. 54 , 90. 50 ]
216      [ - 181. 36 , 90. 00 ]
217      [ - 177. 37 , 90. 00 ]
218      [ - 87. 70 , 90. 00 ]
219      [ - 33. 89 , 90. 00 ]
220      [ - 18. 52 , 86. 88 ]
221      [ 0. 00 , 85. 20 ]
222      [ 16. 20 , 86. 83 ]
223      [ 31. 59 , 90. 00 ]
224      [ 33. 03 , 90. 50 ]
225      [ 34. 41 , 91. 00 ]
226      [ 34. 99 , 91. 00 ]
227      [ 72. 19 , 91. 00 ]
228      [ 208. 76 , 91. 50 ]
229      [ 846. 25 , 92. 00 ]
230      [ 854. 54 , 94. 00 ]
231      *%-----|-----|
232      *#*****|
233      *#      Catchment FOSTER
234      *#      - To Foster ditch (north of the Jock)
235      *#      - Partially developed (medium density); remaining agricultural
236      *#*****|
237      CONTINUOUS STANDHYD ID=[ 2 ] , NHYD=[ "FOSTER" ] , DT=[ 5 ] mi n , AREA=[ 373 ] ( ha ) ,
238      XI MP=[ 0. 55 ] , TI MP=[ 0. 55 ] , DWF=[ 0 ] ( cms ) , LOSS=[ 2 ] ,
239      SCS curve number CN=[ 74 ] ,
240      Per vi ous surfaces: I A per=[ 4. 67 ] ( mm ) , SLPP=[ 0. 5 ] ( % ) ,
241      LGP=[ 40 ] ( m ) , MNP=[ 0. 25 ] , SCP=[ 0 ] ( mi n ) ,
242      Imper vi ous surfaces: I A i mp=[ 1. 57 ] ( mm ) , SLPI=[ 0. 5 ] ( % ) ,
243      LGI=[ 1577 ] ( m ) , MNI=[ 0. 013 ] , SCI=[ 0 ] ( mi n ) ,
244      Conti nuous simulation parameters:
245      I a REC per=[ 4 ] ( hr s ) , I a REC i mp=[ 4 ] ( hr s ) ,
246      SM N=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
247      Inter Event Ti me=[ 18 ] ( hr s ) , END=- 1
248
249      *#*****|
250      *#      Foster Pond
251      *#      - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
252      *#      and a ratio of the catchment area to the West Clarke pond rating curve
253      *#      from the MS for the next coordinates
254      *#*****|
255      ROUTE RESERVOIR I D out =[ 4 ] , NHYD=[ "P_FOS" ] , I D i n =[ 2 ] ,
256      RDT=[ 5 ] ( mi n ) ,
257      TABLE of ( OUTFLOW STORAGE ) values
258      ( cms ) - ( ha - m )
259      [ 0. 0 , 0. 0 ]
260      [ 0. 20 , 1. 72 ]
261      [ - 1 , - 1 ] ( max twenty pts )
262      I D ovf =[ 9 ] , NHYD ovf =[ "FO- OVF" ]
263      *%-----|-----|
264      ADD HYD I D s um =[ 3 ] , NHYD=[ "SN_FO" ] , I D s to add =[ 1 , 4 , 9 ]

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265  *%-----|-----|
266  SAVE HYD          ID=[ 3 ], # OF PCYCLES=[ - 1], I CASEs h=[ 1]
267                  HYD_COMMENT=["Total Flows at Foster Drain"]
268  *%-----|-----|
269  *#
270  *# Hydrograph from Node Foster routed to Node at Cedarview Road
271  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6016
272  *#
273  ROUTE CHANNEL     IDout=[ 1], NHYD=["N_CE"], IDin=[ 3],
274                  RDT=[ 5](min),
275                  CHLGTH=[ 159](m), CHSLOPE=[ 0.0818](%),
276                  FPSLOPE=[ 0.0818](%),
277                  SECNUM=[ 1.0], NSEG=[ 3]
278                  ( SEGROUGH, SEGDI ST (m))=
279                    [ 0.050, -15.46
280                    -0.035, 26.55
281                    0.050, 1299.52] NSEG times
282                  ( DI STANCE (m), ELEVATI ON (m))=
283                    [- 891.38, 93.00]
284                    [- 882.49, 93.00]
285                    [- 880.92, 92.50]
286                    [- 879.37, 92.00]
287                    [- 877.72, 91.50]
288                    [- 876.10, 91.00]
289                    [- 873.23, 91.00]
290                    [- 871.82, 91.50]
291                    [- 870.40, 92.00]
292                    [- 803.44, 92.00]
293                    [- 645.23, 91.50]
294                    [- 391.20, 91.50]
295                    [- 91.00, 91.50]
296                    [- 85.52, 91.50]
297                    [- 15.46, 89.40]
298                    [- 9.79, 89.31]
299                    [- 3.22, 86.24]
300                    [ 3.22, 85.07]
301                    [ 10.96, 85.79]
302                    [ 16.44, 86.49]
303                    [ 26.55, 89.45]
304                    [ 29.03, 90.27]
305                    [ 35.76, 90.67]
306                    [ 36.67, 91.00]
307                    [ 108.08, 91.00]
308                    [ 109.82, 90.50]
309                    [ 112.04, 90.50]
310                    [ 114.62, 91.00]
311                    [ 116.76, 91.50]
312                    [ 118.42, 92.00]
313                    [ 449.53, 92.50]
314                    [ 571.98, 92.50]
315                    [ 1093.81, 93.50]
316                    [ 1150.48, 94.00]
317                    [ 1299.52, 95.00]
318  *%-----|-----|
319  *#*****|*****|
320  *# Catchment S-1
321  *# - To Jock River (north and south of Jock)
322  *# - Primarily agricultural fields; portion of sand quarry
323  *#*****|*****|
324  CONTINUOUS NASHYD ID=[ 2], NHYD=["S-1"], DT=[ 5]min, AREA=[ 245](ha),
325                  DWF=[ 0](cms), CNVC=[ 77], IA=[ 4.67](mm),
326                  N=[ 3], TP=[ 1.10]hrs,
327                  Continuous simulation parameters:
328                  IaRECper=[ 4](hrs),
329                  SMN=[ - 1](mm), SMAX=[ - 1](mm), SK=[ 0.010]/(mm),
330                  InterEventTime=[ 12](hrs)

```

```

331 Baseflow simulation parameters:
332 BaseFlowOption=[ 1] ,
333 InitGWResVol=[ 50] ( mm) , GWResK=[ 0.96] ( mm/ day/ mm)
334 VHydCond=[ 0.055] ( mm/ hr) , END=- 1
335
336 *%-----|-----|
337 ADD HYD IDsum=[ 3 ] , NHYD=[ "SN_CE" ] , IDs to add=[ 1,2]
338 *%-----|-----|
339 SAVE HYD ID=[ 3 ] , # OF PCYCLES=[ -1] , ICASEsh=[ 1]
340 HYD_COMMENT=[ "Total Flows at Cedarview Road" ]
341 *%-----|-----|
342 *#
343 *# Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain
344 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5002
345 *#
346 ROUTE CHANNEL IDout=[ 1] , NHYD=[ "N_WC" ] , IDin=[ 3] ,
347 RDT=[ 5] ( min) ,
348 CHLGTH=[ 825] ( m) , CHSLOPE=[ 0.01] ( % ) ,
349 FPSLOPE=[ 0.01] ( % ) ,
350 SECNUM=[ 1.0] , NSEG=[ 3]
351 ( SEGROUGH, SEGDI ST ( m) ) =
352 [ 0.050, -37.5
353 -0.035, 37.50
354 0.050, 1367.08] NSEG times
355 ( DI STANCE ( m) , ELEVATI ON ( m) ) =
356 [- 1095.18, 94.00]
357 [- 1091.79, 93.50]
358 [- 1088.95, 93.00]
359 [- 1086.77, 93.00]
360 [- 1069.38, 93.00]
361 [- 1063.14, 93.00]
362 [- 1017.52, 93.00]
363 [- 899.70, 93.00]
364 [- 877.78, 93.00]
365 [- 859.62, 92.50]
366 [- 803.18, 93.00]
367 [- 789.92, 92.00]
368 [- 37.50, 90.00]
369 [- 19.61, 87.04]
370 [ 0.00, 85.70]
371 [ 14.87, 86.93]
372 [ 37.50, 90.00]
373 [ 38.54, 90.50]
374 [ 42.23, 91]
375 [ 157.05, 91.50]
376 [ 161.44, 91.50]
377 [ 236.48, 93.00]
378 [ 385.47, 92.50]
379 [ 390.78, 92.50]
380 [ 863.80, 93.00]
381 [ 866.13, 93.00]
382 [ 990.85, 92.50]
383 [ 991.82, 92.50]
384 [ 993.04, 93.00]
385 [ 994.81, 93.50]
386 [ 1005.36, 93.00]
387 [ 1190.52, 93.00]
388 [ 1267.97, 93.50]
389 [ 1318.99, 94.00]
390 [ 1367.08, 94.50]
391 *%-----|-----|
392 *#*****
393 *# Catchment W_CLAR
394 *# - To West Clarke Drain (south of the Jock)
395 *# - Subdivision with 43% imp. as per Barrhaven South MSS
396 *#*****

```



```

397 CONTINUOUS STANDHYD ID=[ 2], NHYD=["W_CLAR"], DT=[ 5] mi n, AREA=[ 243] (ha),
398 XI MP=[ 0.43], TI MP=[ 0.43], DWF=[ 0] (cms), LOSS=[ 2],
399 SCS curve number CN=[ 75],
400 Pervious surfaces: I A per=[ 4.67] (mm), SLPP=[ 1] (%),
401 LGP=[ 40] (m), MNP=[ 0.25], SCP=[ 0] (mi n),
402 Impervious surfaces: I A i mp=[ 1.57] (mm), SLPI=[ 1] (%),
403 LGI=[ 1273] (m), MNI=[ 0.013], SCI=[ 0] (mi n),
404 Continuous simulation parameters:
405 I a REC per=[ 4] (hr s), I a REC i mp=[ 4] (hr s),
406 SM N=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
407 Inter Event Ti me=[ 18] (hr s), END=- 1
408
409 *%-----|-----|
410 *#*****|
411 *# West Clarke Pond 2
412 *# - Rating curve obtained from Barrhaven South M&S modeling
413 *# - Tributary Drainage Area to M&S Pond 2 = 241 ha
414 *#*****|
415 ROUTE RESERVOIR I D out=[ 8], NHYD=["M&S_P2"], I D i n=[ 2],
416 RDT=[ 5] (mi n),
417 TABLE of ( OUTFLOW STORAGE ) values
418 ( cms ) - ( ha - m)
419 [ 0.0 , 0.0 ]
420 [ 0.11 , 0.96]
421 [ -1 , -1 ] (max twenty pts)
422 I D o v f=[ 9], NHYD o v f=["P2- OVF"]
423 *%-----|-----|
424 ADD HYD I D s um=[ 4 ], NHYD=["SN_WC"], I D s t o a d d=[ 8,9,1]
425 *%-----|-----|
426 SAVE HYD I D=[ 4], # OF PCYCLES=[ -1], I C A S E s h=[ 1]
427 HYD_COMMENT=["Total Flows at West Clarke Pond Outlet"]
428 *%-----|-----|
429 *# Hydrograph from Node West Clarke routed to Node at Kennedy - Burnett Drain
430 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4534
431 *#
432 ROUTE CHANNEL I D out=[ 1], NHYD=["N_KB"], I D i n=[ 4],
433 RDT=[ 5] (mi n),
434 CHLGTH=[ 1020] (m), CHSLOPE=[ 0.0498] (%),
435 FPSLOPE=[ 0.0498] (%),
436 SECNUM=[ 1.0], NSEG=[ 3]
437 ( SEGROUGH, SEGDI ST (m))=
438 [ 0.050, -23.63
439 -0.035, 23.63
440 0.050, 728.3] NSEG times
441 ( DI STANCE (m), ELEVATI ON (m))=
442 [-1082.01, 94]
443 [-1028.17, 92.5]
444 [-992.3, 93.5]
445 [-279.34, 90]
446 [-23.63, 90]
447 [-13.45, 87.13]
448 [-0.07, 86.24]
449 [10.54, 87.15]
450 [23.63, 90]
451 [24.86, 90.5]
452 [26.72, 91]
453 [45.07, 91.5]
454 [128.17, 91.5]
455 [270.7, 92.5]
456 [728.3, 95]
457
458 *%-----|-----|
459 *#*****|
460 *# Catchment KEN_BU
461 *# - To Kennedy-Burnett SWM Facility
462 *# - Outlets to Fraser-Clarke drain (north of the Jock)

```

```

463  *# - Medium density residential subdivision
464  *#*****
465  CONTINUOUS STANDHYD ID=[ 2], NHYD=["KEN_BU"], DT=[ 5] mi n, AREA=[ 281] (ha),
466  XI MP=[ 0.55], TI MP=[ 0.55], DWF=[ 0] (cms), LOSS=[ 2],
467  SCS curve number CN=[ 71],
468  Pervious surfaces: IAper=[ 4.67] (mm), SLPP=[ 1] (%),
469  LGP=[ 40] (m), MNP=[ 0.25], SCP=[ 0] (mi n),
470  Impervious surfaces: IAi mp=[ 1.57] (mm), SLPI =[ 1] (%),
471  LGI =[ 1369] (m), MNI =[ 0.013], SCI =[ 0] (mi n),
472  Continuous simulation parameters:
473  IaRECper=[ 4] (hrs), IaRECI mp=[ 4] (hrs),
474  SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
475  InterEvent Time=[ 18] (hrs), END=- 1
476  *%-----|-----|
477  *#*****
478  *# Existing Kennedy-Burnett SWM Facility
479  *# - Rating curve obtained from URTKBP
480  *# - Tributary Drainage Area to Pond = 160 ha
481  *#*****
482  ROUTE RESERVOIR IDout=[ 5], NHYD=["KEN_P"], IDi n=[ 2],
483  RDT=[ 5] (mi n),
484  TABLE of ( OUTFLOW STORAGE ) values
485  ( cms ) - ( ha-m)
486  [ 0.0 , 0.0 ]
487  [ 0.13 , 0.26]
488  [ 0.43 , 0.56]
489  [ 0.67 , 0.90]
490  [ 0.86 , 1.32]
491  [ 1.01 , 1.79]
492  [ 1.15 , 2.33]
493  [ -1 , -1 ] (max twenty pts)
494  IDovf=[ 6], NHYDovf=["KEN_OV"]
495  *%-----|-----|
496  *#*****
497  *# Catchment FRASER
498  *# - To Fraser-Clarke drain (north of the Jock)
499  *# - Developed land with assumed 43% imp.
500  *#*****
501  CONTINUOUS STANDHYD ID=[ 7], NHYD=["FRASER"], DT=[ 5] mi n, AREA=[ 90] (ha),
502  XI MP=[ 0.25], TI MP=[ 0.25], DWF=[ 0] (cms), LOSS=[ 2],
503  SCS curve number CN=[ 80],
504  Pervious surfaces: IAper=[ 4.67] (mm), SLPP=[ 1] (%),
505  LGP=[ 40] (m), MNP=[ 0.25], SCP=[ 0] (mi n),
506  Impervious surfaces: IAi mp=[ 1.57] (mm), SLPI =[ 1] (%),
507  LGI =[ 775] (m), MNI =[ 0.013], SCI =[ 0] (mi n),
508  Continuous simulation parameters:
509  IaRECper=[ 4] (hrs), IaRECI mp=[ 4] (hrs),
510  SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
511  InterEvent Time=[ 18] (hrs), END=- 1
512
513  *%-----|-----|
514  ROUTE RESERVOIR IDout=[ 8], NHYD=["MS_P2"], IDi n=[ 7],
515  RDT=[ 5] (mi n),
516  TABLE of ( OUTFLOW STORAGE ) values
517  ( cms ) - ( ha-m)
518  [ 0.0 , 0.0 ]
519  [ 0.04 , 0.36]
520  [ -1 , -1 ] (max twenty pts)
521  IDovf=[ 9], NHYDovf=["P2-OVF"]
522  *%-----|-----|
523  ADD HYD IDsum=[ 4 ], NHYD=["SN_KB"], IDst o add=[ 5, 6, 8, 9, 1]
524  *%-----|-----|
525  SAVE HYD ID=[ 4], # OF PCYCLES=[ -1], ICASEsh=[ 1]
526  HYD_COMMENT=["Total Flows at Ken-Burnett Outlet"]
527  *%-----|-----|
528  *# Hydrograph from Node Kennedy - Burnett Drain to Node Todd Drain

```

```

529  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 3633
530  *#
531  ROUTE CHANNEL      I Dout =[ 1], NHYD=[ "N_TO" ] , I Di n=[ 4] ,
532                    RDT=[ 5] ( mi n),
533                    CHLGTH=[ 650] ( m),   CHSLOPE=[ 0. 0498] ( %),
534                    FPSLOPE=[ 0. 0498] ( %),
535                    SECNUM=[ 1. 0],      NSEG=[ 3]
536                    ( SEGROUGH, SEGDI ST ( m) )=
537                    [ 0. 050, - 23. 74
538                    - 0. 035, 23. 74
539                    0. 050, 74. 7] NSEG ti mes
540                    ( DI STANCE ( m), ELEVATI ON ( m) )=
541                    [- 74. 18, 92. 5]
542                    [- 65. 96, 92]
543                    [- 54. 17, 91. 5]
544                    [- 29. 24, 91]
545                    [- 27. 41, 90. 5]
546                    [- 25. 64, 90]
547                    [- 23. 74, 89. 5]
548                    [- 22, 89. 26]
549                    [- 20, 88. 51]
550                    [- 19, 88. 32]
551                    [- 15, 88. 1]
552                    [- 10, 88. 11]
553                    [- 5, 88. 17]
554                    [ 0, 88. 27]
555                    [ 5, 88. 19]
556                    [ 10, 88. 06]
557                    [ 15, 88. 48]
558                    [ 16, 88. 7]
559                    [ 23. 74, 89. 5]
560                    [ 24. 68, 90]
561                    [ 25. 57, 90. 5]
562                    [ 26. 5, 91]
563                    [ 47. 55, 91]
564                    [ 74. 7, 92. 5]
565  *%-----|-----|
566
567  *#*****
568  *#      Catchment TODD
569  *#      - To Todd Drain (south of the Jock)
570  *#      - Subdivision with 43% imp. as per Barrhaven South M&S
571  *#*****
572  CONTINUOUS STANDHYD I D=[ 3], NHYD=[ "TODD" ], DT=[ 5] mi n, AREA=[ 195] ( ha),
573                    XI MP=[ 0. 43], TI MP=[ 0. 43], DWF=[ 0] ( cms), LOSS=[ 2],
574                    SCS curve number CN=[ 77],
575                    Pervious surfaces: I Aper=[ 4. 67] ( mm), SLPP=[ 1] ( %),
576                    LGP=[ 40] ( m), MNP=[ 0. 25], SCP=[ 0] ( mi n),
577                    Impervious surfaces: I Ai mp=[ 1. 57] ( mm), SLPI=[ 1] ( %),
578                    LGI=[ 1140] ( m), MNI=[ 0. 013], SCI=[ 0] ( mi n),
579                    Continuous simulation parameters:
580                    I aREcper=[ 4] ( hr s), I aRECi mp=[ 4] ( hr s),
581                    SM N=[ - 1] ( mm), SMAX=[ - 1] ( mm), SK=[ 0. 010] / ( mm),
582                    Inter Event Ti me=[ 18] ( hr s), END=- 1
583
584  *#*****
585  *#      Todd Pond 3
586  *#      - Rating curve obtained from Barrhaven South M&S modeling
587  *#      - Tributary Drainage Area to M&S Pond 3 = 193 ha
588  *#*****
589  ROUTE RESERVOIR    I Dout =[ 2], NHYD=[ "M&S_P3" ], I Di n=[ 3],
590                    RDT=[ 5] ( mi n),
591                    TABLE of ( OUTFLOW STORAGE ) values
592                    ( cms) - ( ha- m)
593                    [ 0. 0 , 0. 0 ]
594                    [ 0. 08 , 0. 78]

```

```

595                                     [ -1 , -1 ] (max twenty pts)
596                               IDovf=[9], NHYDovf=["P3-OVF"]
597 *%-----|-----|
598 ADD HYD                               IDsum=[10], NHYD=["SN_TO"], IDstoadd=[1,2,9]
599 *%-----|-----|
600 SAVE HYD                               ID=[10], # OF PCYCLES=[-1], ICASEsh=[1]
601                               HYD_COMMENT=["Total Flows at Todd Drain"]
602 *%-----|-----|
603 *#
604 *# Hydrograph from Todd Drain routed to Corrigan Drain
605 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
606 *#
607 ROUTE CHANNEL                          IDout=[1], NHYD=["N_TO"], IDin=[10],
608                               RDT=[5] (min),
609                               CHLGTH=[280] (m), CHSLOPE=[0.033] (%),
610                               FPSLOPE=[0.033] (%),
611                               SECNUM=[1.0], NSEG=[3]
612                               ( SEGROUGH, SEGDI ST (m) ) =
613                               [0.075, -17.72
614                               -0.045, 17.72
615                               0.075, 80.62] NSEG times
616                               ( DI STANCE (m), ELEVATI ON (m) ) =
617                               [-83.32, 90.00]
618                               [-81.36, 89.50]
619                               [-79.12, 89.00]
620                               [-76.13, 88.50]
621                               [-20.46, 88.00]
622                               [-19.36, 87.50]
623                               [-18.51, 87.00]
624                               [-17.72, 86.50]
625                               [-11.95, 85.24]
626                               [-0.11, 85.12]
627                               [11.49, 85.20]
628                               [17.72, 86.50]
629                               [19.74, 87.00]
630                               [21.22, 87.50]
631                               [22.68, 88.00]
632                               [24.28, 88.50]
633                               [26.79, 89.00]
634                               [71.98, 90.00]
635                               [80.62, 90.50]
636 *%-----|-----|
637 *#*****
638 *# Catchment CORRIG
639 *# - To Corrigan Drain (south of the Jock)
640 *# - Primarily Developed (medium density)
641 *#*****
642 CONTINUOUS STANDHYD ID=[2], NHYD=["CORRIG"], DT=[5] min, AREA=[149] (ha),
643                               XI MP=[0.45], TI MP=[0.45], DWF=[0] (cms), LOSS=[2],
644                               SCS curve number CN=[77],
645                               Pervious surfaces: IAper=[4.67] (mm), SLPP=[1] (%),
646                               LGP=[40] (m), MNP=[0.25], SCP=[0] (min),
647                               Impervious surfaces: IAimp=[1.57] (mm), SLPI=[1] (%),
648                               LGI=[997] (m), MNI=[0.013], SCI=[0] (min),
649                               Continuous simulation parameters:
650                               IaRECper=[4] (hrs), IaRECI mp=[4] (hrs),
651                               SMN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010] / (mm),
652                               InterEvent Time=[18] (hrs), END=-1
653
654 *%-----|-----|
655 *#*****
656 *# Corrigan Pond 1
657 *# - Rating curve obtained from Barrhaven South MSS modeling
658 *# - Tributary Drainage Area to MSS Pond 1 = 145 ha
659 *#*****
660 ROUTE RESERVOIR IDout=[5], NHYD=["MS_P1"], IDin=[2],

```

```

661 RDT=[ 5] ( mi n),
662 TABLE of ( OUTFLOW STORAGE ) values
663 ( cms ) - ( ha- m)
664 [ 0. 0 , 0. 0 ]
665 [ 0. 06 , 0. 58]
666 [ -1 , -1 ] (max twenty pts)
667 I Dovf=[ 4], NHYDovf=[" P1- OVF" ]
668 *%-----|-----|
669 ADD HYD I Dsum=[ 3 ], NHYD=[" SN_CO" ], I Ds to add=[ 1, 4, 5]
670 *%-----|-----|
671 SAVE HYD I D=[ 3 ], # OF PCYCLES=[ -1], I CASEsh=[ 1]
672 HYD_COMMENT=[" Total Flows at Corrigan Drain" ]
673 *%-----|-----|
674 *#
675 *# Hydrograph from Corrigan Drain routed to Jockvale Road
676 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
677 *#
678 ROUTE CHANNEL I Dout =[ 1], NHYD=[" N_M" ], I Din =[ 3] ,
679 RDT=[ 5] ( mi n),
680 CHLGTH=[ 580] ( m), CHSLOPE=[ 0. 4448] ( %),
681 FPSLOPE=[ 0. 4448] ( %),
682 SECNUM=[ 1. 0], NSEG=[ 3]
683 ( SEGROUGH, SEGDI ST ( m) ) =
684 [ 0. 075, -17. 72
685 -0. 045, 17. 72
686 0. 075, 80. 62] NSEG times
687 ( DI STANCE ( m), ELEVATI ON ( m) ) =
688 [- 83. 32, 90. 00]
689 [- 81. 36, 89. 50]
690 [- 79. 12, 89. 00]
691 [- 76. 13, 88. 50]
692 [- 20. 46, 88. 00]
693 [- 19. 36, 87. 50]
694 [- 18. 51, 87. 00]
695 [- 17. 72, 86. 50]
696 [- 11. 95, 85. 24]
697 [- 0. 11, 85. 12]
698 [ 11. 49, 85. 20]
699 [ 17. 72, 86. 50]
700 [ 19. 74, 87. 00]
701 [ 21. 22, 87. 50]
702 [ 22. 68, 88. 00]
703 [ 24. 28, 88. 50]
704 [ 26. 79, 89. 00]
705 [ 71. 98, 90. 00]
706 [ 80. 62, 90. 50]
707 *%-----|-----|
708 *#*****|
709 *# Catchment MLLS
710 *# - To SWM Facility north of the Jock
711 *# - Primarily residential development
712 *#*****|
713 CONTINUOUS STANDHYD I D=[ 2], NHYD=[" MLLS" ], DT=[ 5] mi n, AREA=[ 139] ( ha),
714 XI MP=[ 0. 38], TI MP=[ 0. 38], DWF=[ 0] ( cms), LOSS=[ 2],
715 SCS curve number CN=[ 74],
716 Pervious surfaces: I Aper=[ 4. 67] ( mm), SLPP=[ 1] ( %),
717 LGP=[ 40] ( m), MNP=[ 0. 25], SCP=[ 0] ( mi n),
718 Impervious surfaces: I Ai mp=[ 1. 57] ( mm), SLPI=[ 1] ( %),
719 LGI=[ 963] ( m), MNI=[ 0. 013], SCI=[ 0] ( mi n),
720 Continuous simulation parameters:
721 I aRECper=[ 4] ( hrs), I aRECI mp=[ 4] ( hrs),
722 SM N=[ -1] ( mm), SMAX=[ -1] ( mm), SK=[ 0. 010] / ( mm),
723 I nter Event Ti me=[ 18] ( hrs), END=- 1
724
725 *%-----|-----|
726 *#*****|

```

```

727  *#      Chapman Mills SWM Pond
728  *#      - Rating curve obtained from CCL hydraulic modeling
729  *#*****
730  ROUTE RESERVOIR      I Dout =[ 5],      NHYD=[ "M LL_P" ],      I Di n=[ 2],
731                      RDT=[ 5] (mi n),
732                      TABLE of ( OUTFLOW STORAGE ) values
733                      ( cms ) - ( ha- m)
734                      [ 0. 0 , 0. 0 ]
735                      [ 0. 01 , 0. 01]
736                      [ 0. 05 , 0. 06]
737                      [ 0. 09 , 0. 11]
738                      [ 0. 13 , 0. 15]
739                      [ 0. 18 , 0. 19]
740                      [ 0. 28 , 0. 28]
741                      [ 0. 37 , 0. 34]
742                      [ 0. 45 , 0. 40]
743                      [ 0. 51 , 0. 44]
744                      [ 0. 56 , 0. 47]
745                      [ 0. 64 , 0. 52]
746                      [ 0. 76 , 0. 59]
747                      [ 0. 86 , 0. 65]
748                      [ 1. 09 , 0. 78]
749                      [ 1. 44 , 0. 96]
750                      [ 3. 18 , 1. 84]
751                      [ 4. 05 , 2. 31]
752                      [ -1 , -1 ] (max twenty pts)
753                      I Dovf =[ 4],      NHYDovf=[ "M L- OV" ]
754  *%-----|-----|
755  ADD HYD              I Dsum=[ 3 ],      NHYD=[ "SN_M" ],      I Ds to add=[ 1, 4, 5]
756  *%-----|-----|
757  SAVE HYD            I D=[ 3 ],      # OF PCYCLES=[ -1],      I CASEsh=[ 1]
758                      HYD_COMMENT=[ "Tot al Fl ows at Jockvale Road" ]
759  *%-----|-----|
760  *#
761  *# Hydrograph from Jockvale Road routed to Heart's Desire
762  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 689
763  *#
764  ROUTE CHANNEL      I Dout =[ 1],      NHYD=[ "N_DE" ] , I Di n=[ 3] ,
765                      RDT=[ 5] (mi n),
766                      CHLGTH=[ 1962] ( m),      CHSLOPE=[ 0. 2227] ( %),
767                      FPSLOPE=[ 0. 2227] ( %),
768                      SECNUM=[ 1. 0],      NSEG=[ 3]
769                      ( SEGROUGH, SEGDI ST ( m) ) =
770                      [ 0. 075, -17. 56
771                      -0. 045, 18. 27
772                      0. 075, 67. 59] NSEG times
773                      ( DI STANCE ( m), ELEVATI ON ( m) ) =
774                      [ -111. 59, 88. 00]
775                      [ -102. 58, 87. 50]
776                      [ -96. 20, 87. 00]
777                      [ -90. 04, 86. 50]
778                      [ -84. 02, 86. 00]
779                      [ -77. 54, 85. 50]
780                      [ -54. 07, 85. 00]
781                      [ -39. 43, 84. 50]
782                      [ -28. 30, 84. 00]
783                      [ -24. 12, 83. 50]
784                      [ -22. 30, 83. 00]
785                      [ -20. 55, 82. 50]
786                      [ -17. 56, 82. 00]
787                      [ -12. 63, 81. 22]
788                      [ -0. 11, 80. 75]
789                      [ 11. 55, 81. 22]
790                      [ 18. 27, 82. 00]
791                      [ 19. 82, 82. 50]
792                      [ 22. 48, 83. 00]

```

793 [27. 90, 83. 50]
794 [29. 31, 84. 00]
795 [30. 81, 84. 50]
796 [32. 51, 85. 00]
797 [34. 24, 85. 50]
798 [36. 34, 86. 00]
799 [41. 65, 86. 50]
800 [62. 64, 87. 00]
801 [65. 14, 87. 50]
802 [67. 59, 88. 00]

803 *%-----|-----|
804 *#*****|

805 *# Catchment DESIRE
806 *# - To Jock River (north of the Jock)
807 *# - Rural-estate subdivision (Heart's Desire Community)
808 *#*****|

809 CONTINUOUS STANDHYD ID=[2], NHYD=["DESIRE"], DT=[5] min, AREA=[24] (ha),
810 XI MP=[0. 25], TI MP=[0. 25], DWF=[0] (cms), LOSS=[2],
811 SCS curve number CN=[77],
812 Pervious surfaces: IAper=[4. 67] (mm), SLPP=[1] (%),
813 LGP=[40] (m), MNP=[0. 25], SCP=[0] (min),
814 Impervious surfaces: IAimp=[1. 57] (mm), SLPI=[1] (%),
815 LGI=[400] (m), MNI=[0. 013], SCI=[0] (min),
816 Continuous simulation parameters:
817 IaRECper=[4] (hrs), IaRECImp=[4] (hrs),
818 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
819 InterEventTime=[18] (hrs), END=- 1

821 *%-----|-----|
822 *#*****|

823 *# Catchment JOCKVA
824 *# - To Jockvale SWM Facility
825 *# - Residential development & golf course
826 *#*****|

827 CONTINUOUS STANDHYD ID=[3], NHYD=["JOCKVA"], DT=[5] min, AREA=[252] (ha),
828 XI MP=[0. 50], TI MP=[0. 50], DWF=[0] (cms), LOSS=[2],
829 SCS curve number CN=[74],
830 Pervious surfaces: IAper=[4. 67] (mm), SLPP=[1] (%),
831 LGP=[40] (m), MNP=[0. 25], SCP=[0] (min),
832 Impervious surfaces: IAimp=[1. 57] (mm), SLPI=[1] (%),
833 LGI=[1296] (m), MNI=[0. 013], SCI=[0] (min),
834 Continuous simulation parameters:
835 IaRECper=[4] (hrs), IaRECImp=[4] (hrs),
836 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
837 InterEventTime=[18] (hrs), END=- 1

839 *%-----|-----|
840 *#*****|

841 *# Jockvale SWM Facility
842 *# - Rating curve obtained from Jockvale Servicing Study (CCL 1999)
843 *#*****|

844 ROUTE RESERVOIR IDout=[5], NHYD=["JOCK_P"], IDin=[3],
845 RDT=[5] (min),
846 TABLE of (OUTFLOW STORAGE) values

847 (cms) - (ha- m)
848 [0. 0 , 0. 0]
849 [0. 27 , 0. 03]
850 [0. 28 , 0. 55]
851 [0. 29 , 1. 14]
852 [0. 30 , 1. 80]
853 [0. 31 , 2. 32]
854 [1. 12 , 2. 87]
855 [2. 92 , 3. 45]
856 [4. 64 , 4. 07]
857 [6. 69 , 4. 72]
858 [9. 02 , 5. 39]

```

859             [ 11.62 , 6.10]
860             [ 14.42 , 6.85]
861             [ 17.45 , 7.62]
862             [ 20.69 , 8.44]
863             [ 24.08 , 9.28]
864             [ 27.68 , 10.17]
865             [ -1 , -1 ] (max twenty pts)
866             IDovf=[4], NHYDovf=["JO-OVF"]
867 *%-----|-----|
868 ADD HYD           IDsum=[ 3 ], NHYD=["SN_DE"], IDs to add=[1,2,4,5]
869 *%-----|-----|
870 SAVE HYD         ID=[ 3 ], # OF PCYCLES=[-1], ICASEsh=[1]
871                 HYD_COMMENT=["Total Flows at Heart's Desire"]
872 *%-----|-----|
873 *#
874 *# Hydrograph from Heart's Desire routed to Rideau River
875 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 0
876 *#
877 ROUTE CHANNEL    IDout=[1], NHYD=["NI"], IDin=[3],
878                 RDT=[5](min),
879                 CHLGTH=[563](m), CHSLOPE=[0.9668](%),
880                                     FPSLOPE=[0.9668](%),
881                 SECNUM=[1.0], NSEG=[3]
882                 ( SEGROUGH, SEGDI ST (m))=
883                   [0.075, -30.20
884                     -0.045, 30.20
885                     0.075, 168.81] NSEG times
886                 ( DISTANCE (m), ELEVATION (m))=
887                   [-170.17, 86.00]
888                   [-164.75, 85.50]
889                   [-158.08, 85.00]
890                   [-113.12, 82.00]
891                   [-98.46, 81.50]
892                   [-92.24, 81.00]
893                   [-86.88, 80.50]
894                   [-81.54, 80.00]
895                   [-74.36, 79.50]
896                   [-63.54, 79.00]
897                   [-39.23, 78.50]
898                   [-34.51, 78.00]
899                   [-33.01, 77.50]
900                   [-30.20, 77.00]
901                   [-13.42, 76.18]
902                   [-1.14, 76.09]
903                   [17.06, 76.18]
904                   [30.20, 77.00]
905                   [32.95, 77.50]
906                   [34.06, 78.00]
907                   [35.11, 78.50]
908                   [36.32, 79.00]
909                   [37.74, 79.50]
910                   [48.48, 81.50]
911                   [49.25, 82.00]
912                   [55.61, 84.50]
913                   [57.09, 85.00]
914                   [59.51, 85.50]
915                   [64.34, 86.00]
916                   [66.30, 86.00]
917                   [76.71, 86.50]
918                   [101.83, 86.50]
919                   [119.73, 87.00]
920                   [142.04, 87.50]
921                   [168.81, 88.00]
922 *%-----|-----|
923 *#*****
924 *# Cat chment S-2

```



```

925 *# - To Jock River (north and south)
926 *# - Undeveloped floodplain and river
927 *#*****
928 CONTINUOUS NASHYD ID=[ 2], NHYD=["S-2"], DT=[ 5] min, AREA=[ 102] (ha),
929 DWF=[ 0] (cms), CNVC=[ 72], IA=[ 4.67] (mm),
930 N=[ 3], TP=[ 0.40] hrs,
931 Continuous simulation parameters:
932 IaRECper=[ 4] (hrs),
933 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010]/(mm),
934 InterEventTime=[ 12] (hrs)
935 Baseflow simulation parameters:
936 BaseFlowOption=[ 1],
937 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/day/mm)
938 VHydCond=[ 0.055] (mm/hr), END=- 1
939
940 *%-----|-----
941 ADD HYD IDsum=[ 3 ], NHYD=["SN_NI"], IDsto add=[ 1,2]
942 *%-----|-----
943 SAVE HYD ID=[ 3 ], # OF PCYCLES=[ -1], ICASEsh=[ 1]
944 HYD_COMMENT=["Total Flows at Rideau River"]
945 *%-----|-----
946 *% 5 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
947 START TZERO=[ 0.0], METOUT=[ 2], NSTORM=[ 1], NRUN=[ 005]
948 *% ["C24SC005.stm"] <--storm filename, one per line for NSTORMtime
949 *%-----|-----
950 *% 10 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
951 *%START TZERO=[ 0.0], METOUT=[ 2], NSTORM=[ 1], NRUN=[ 010]
952 *% ["C24SC010.stm"] <--storm filename, one per line for NSTORMtime
953 *%-----|-----
954 *% 25 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
955 START TZERO=[ 0.0], METOUT=[ 2], NSTORM=[ 1], NRUN=[ 025]
956 *% ["C24SC025.stm"] <--storm filename, one per line for NSTORMtime
957 *%-----|-----
958 *% 50 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
959 *%START TZERO=[ 0.0], METOUT=[ 2], NSTORM=[ 1], NRUN=[ 050]
960 *% ["C24SC050.stm"] <--storm filename, one per line for NSTORMtime
961 *%-----|-----
962 *% 100 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
963 START TZERO=[ 0.0], METOUT=[ 2], NSTORM=[ 1], NRUN=[ 100]
964 *% ["C24SC100.stm"] <--storm filename, one per line for NSTORMtime
965 *%-----|-----
966
967 *#####
968 FINISH
969
970
971
972
973
974
975
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990

```


007499 # 09:04:04P 359.57 18.663 N6_date 28:20 34.02 a/a

Attachment C

Model 3 – Jock River Reach One Update

JFSA, 2021

SWMHYMO Input & Summary files


```

1  20      Metric units / ID numbers OFF
2  *****
3  *# SWHYMO Ver: 5.02/Jan 2001 <BETA> / INPUT DATA FILE
4  *****
5  *# Project Name: [Jock River]      Project Number: [1474-16]
6  *# Date       : 04-03-2021
7  *# Modeller   : [MM]
8  *# Company    : JFSA Inc.
9  *# License #  : 2549237
10 *****
11 *# CALIBRATION OF SUMMER MODEL PARAMETERS
12 *# USING CONTINUOUS SIMULATIONS
13 *# Rainfall data from JFSA raingauge installed at site + other gauges by the City
14 *# Use data collected from May 1st to July 14, 2003
15 *# 2020-11-30 change TMSSTO in COMPUTE DUALHYD (TMSSTO = 0.1 instead of 0.0001)
16 *# 2020-12-01 correct pond curve values
17 *# 2020-12-01 change WCLAR_BRAZ_XIMP to 0.55, SLPI=[0.5](%) (impervious slope), and
    LGI up to 700m
18 *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 2462 (NHYDout=["N_TO"]
    ,NHYDin=["SN_TO"]) from 0.033 % (as per Stantec Report 2007) to 0.05 % so the model
    will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELS
    aren't well suited to really flat slopes.
19 *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHYDout=["N_WC"]
    ,NHYDin=["SN_CE"]) from 0.01 % (as per Stantec Report 2007) to 0.0255 % so the model
    will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELS
    aren't well suited to really flat slopes.
20 *
21 * Calibrated parameters for Summer 2003 data: APII=50, APIK=0.85, CN=varies,
22 *                                             SK=0.01, InterEventTime=12,
23 *                                             GWResk=0.96, VHydCond=0.055
24 *
25 *# -----
26 *
27 *START          TZERO=[2003.0501], METOUT=[2], NSTORM=[1], NRUN=[001]
28 *              ["XAVG0315.STM"] average storm data a 15 minute time step
29 *              The above rainf file is an average of the JFSA gauge data
30 *              with the City of Ottawa rainfall data collected during
31 *              the same period.
32 *% 2 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
33 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[2]
34              ["C24SC002.stm"] <-- storm filename, one per line for NSTORM time
35 *%-----|-----|
36 *%-----|-----|
37 READ STORM     STORM_FILENAME=["storm 001"]
38 *%-----|-----|
39 MODIFY STORM   ICASEms=[1], NSHIFT=[96],
40              RedFACT=[1],
41 *%-----|-----|
42 DEFAULT VALUES ICASEdef=[1], read and print values
43              DEFVAL_FILENAME=["CitiGate.DEF"]
44 *%-----|-----|
45 COMPUTE API    APII=[50], APIK=[.85]/day
46 *%-----|-----|
47 *%-----|-----|
48 *#
49 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
50 *# of 1.32
51 *%-----|-----|
52 CONTINUOUS NASHYD NHYD=["JR_HW"], DT=[1]min, AREA=[3680](ha),
53              DWF=[0](cms), CNVC=[64], IA=[2.5](mm),
54              N=[3.0], TP=[7.13]hrs,
55              Continuous simulation parameters:
56              IARECper=[4](hrs),
57              SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
58              InterEventTime=[12](hrs)
59              Baseflow simulation parameters:

```

```

60 BaseFlowOption=[ 1] ,
61 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
62 VHydCond=[ 0.055](mm/hr), END=- 1
63 *%-----|-----
64 *#
65 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
66 *# of 1.32
67 *%-----|-----
68 CONTINUOUS NASHYD NHYD=[ "SW_13"], DT=[ 1]min, AREA=[ 971](ha),
69 DWF=[ 0](cms), CNVC=[ 61], IA=[ 2.5](mm),
70 N=[ 3.0], TP=[ 3.76]hrs,
71 Continuous simulation parameters:
72 IaRECper=[ 4](hrs),
73 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
74 InterEventTime=[ 12](hrs)
75 Baseflow simulation parameters:
76 BaseFlowOption=[ 1] ,
77 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
78 VHydCond=[ 0.055](mm/hr), END=- 1
79 *%-----|-----
80 *#
81 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
82 *# of 1.80
83 *%-----|-----
84 CONTINUOUS NASHYD NHYD=[ "JR_GWM"], DT=[ 1]min, AREA=[ 3074](ha),
85 DWF=[ 0](cms), CNVC=[ 55], IA=[ 2.5](mm),
86 N=[ 3], TP=[ 11.33]hrs,
87 Continuous simulation parameters:
88 IaRECper=[ 4](hrs),
89 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
90 InterEventTime=[ 12](hrs)
91 Baseflow simulation parameters:
92 BaseFlowOption=[ 1] ,
93 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
94 VHydCond=[ 0.055](mm/hr), END=- 1
95 *%-----|-----
96 CONTINUOUS NASHYD NHYD=[ "JR_ASH"], DT=[ 1]min, AREA=[ 1781](ha),
97 DWF=[ 0](cms), CNVC=[ 72], IA=[ 2.5](mm),
98 N=[ 3.0], TP=[ 3.91]hrs,
99 Continuous simulation parameters:
100 IaRECper=[ 4](hrs),
101 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
102 InterEventTime=[ 12](hrs)
103 Baseflow simulation parameters:
104 BaseFlowOption=[ 1] ,
105 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
106 VHydCond=[ 0.055](mm/hr), END=- 1
107 *%-----|-----
108 CONTINUOUS NASHYD NHYD=[ "SW_11"], DT=[ 1]min, AREA=[ 500](ha),
109 DWF=[ 0](cms), CNVC=[ 66], IA=[ 2.5](mm),
110 N=[ 3.0], TP=[ 1.24]hrs,
111 Continuous simulation parameters:
112 IaRECper=[ 4](hrs),
113 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
114 InterEventTime=[ 12](hrs)
115 Baseflow simulation parameters:
116 BaseFlowOption=[ 1] ,
117 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
118 VHydCond=[ 0.055](mm/hr), END=- 1
119 *%-----|-----
120 *#
121 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
122 *# of 1.80
123 *%-----|-----
124 CONTINUOUS NASHYD NHYD=[ "NN_CK"], DT=[ 1]min, AREA=[ 1917](ha),
125 DWF=[ 0](cms), CNVC=[ 66], IA=[ 2.5](mm),

```

```

126 N=[ 3. 0], TP=[ 5. 29] hrs,
127 Continuous simulation parameters:
128 IaRECPper=[ 4] (hrs),
129 SMN=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010]/ (mm),
130 InterEventTime=[ 12] (hrs)
131 Baseflow simulation parameters:
132 BaseFlowOption=[ 1] ,
133 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
134 VHydCond=[ 0. 055] (mm/ hr), END=- 1
135 *%-----|-----
136 *#
137 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
138 *# of 1.52
139 *%-----|-----
140 CONTINUOUS NASHYD NHYD=[ "SW_10"], DT=[ 1] min, AREA=[ 5666] (ha),
141 DWF=[ 0] (cms), CNVC=[ 72], IA=[ 2. 5] (mm),
142 N=[ 3. 0], TP=[ 8. 00] hrs,
143 Continuous simulation parameters:
144 IaRECPper=[ 4] (hrs),
145 SMN=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010]/ (mm),
146 InterEventTime=[ 12] (hrs)
147 Baseflow simulation parameters:
148 BaseFlowOption=[ 1] ,
149 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
150 VHydCond=[ 0. 055] (mm/ hr), END=- 1
151 *%-----|-----
152 *#
153 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
154 *# of 1.75
155 *%-----|-----
156 CONTINUOUS NASHYD NHYD=[ "KG_CK"], DT=[ 1] min, AREA=[ 8376] (ha),
157 DWF=[ 0] (cms), CNVC=[ 66], IA=[ 2. 5] (mm),
158 N=[ 3. 0], TP=[ 11. 66] hrs,
159 Continuous simulation parameters:
160 IaRECPper=[ 4] (hrs),
161 SMN=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010]/ (mm),
162 InterEventTime=[ 12] (hrs)
163 Baseflow simulation parameters:
164 BaseFlowOption=[ 1] ,
165 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
166 VHydCond=[ 0. 055] (mm/ hr), END=- 1
167 *%-----|-----
168 *#
169 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
170 *# of 1.68
171 *%-----|-----
172 CONTINUOUS NASHYD NHYD=[ "SW_9"], DT=[ 1] min, AREA=[ 1132] (ha),
173 DWF=[ 0] (cms), CNVC=[ 70], IA=[ 2. 5] (mm),
174 N=[ 3. 0], TP=[ 2. 51] hrs,
175 Continuous simulation parameters:
176 IaRECPper=[ 4] (hrs),
177 SMN=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010]/ (mm),
178 InterEventTime=[ 12] (hrs)
179 Baseflow simulation parameters:
180 BaseFlowOption=[ 1] ,
181 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
182 VHydCond=[ 0. 055] (mm/ hr), END=- 1
183 *%-----|-----
184 *#
185 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
186 *# of 1.82
187 *%-----|-----
188 CONTINUOUS NASHYD NHYD=[ "NC_CK"], DT=[ 1] min, AREA=[ 4464] (ha),
189 DWF=[ 0] (cms), CNVC=[ 62], IA=[ 2. 5] (mm),
190 N=[ 3. 0], TP=[ 11. 32] hrs,
191 Continuous simulation parameters:

```

```

192 IaREcper=[ 4] (hr s),
193 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
194 InterEventTime=[ 12] (hr s)
195 Baseflow simulation parameters:
196 BaseFlowOption=[ 1] ,
197 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
198 VHydCond=[ 0. 055] (mm/ hr), END=- 1
199 *%-----|-----
200 *#
201 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
202 *# of 1.80
203 *%-----|-----
204 CONTINUOUS NASHYD NHYD=[ "SW_8" ], DT=[ 1] mi n, AREA=[ 131] (ha),
205 DWF=[ 0] (cms), CN C=[ 63], IA=[ 2. 5] (mm),
206 N=[ 3. 0], TP=[ 0. 90] hr s,
207 Continuous simulation parameters:
208 IaREcper=[ 4] (hr s),
209 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
210 InterEventTime=[ 12] (hr s)
211 Baseflow simulation parameters:
212 BaseFlowOption=[ 1] ,
213 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
214 VHydCond=[ 0. 055] (mm/ hr), END=- 1
215 *%-----|-----
216 *#
217 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
218 *# of 1.65
219 *%-----|-----
220 CONTINUOUS NASHYD NHYD=[ "HB_DR" ], DT=[ 1] mi n, AREA=[ 3854] (ha),
221 DWF=[ 0] (cms), CN C=[ 66], IA=[ 2. 5] (mm),
222 N=[ 3. 0], TP=[ 8. 42] hr s,
223 Continuous simulation parameters:
224 IaREcper=[ 4] (hr s),
225 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
226 InterEventTime=[ 12] (hr s)
227 Baseflow simulation parameters:
228 BaseFlowOption=[ 1] ,
229 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
230 VHydCond=[ 0. 055] (mm/ hr), END=- 1
231 *%-----|-----
232 *#
233 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
234 *# of 1.82
235 *%-----|-----
236 CONTINUOUS NASHYD NHYD=[ "SW_7" ], DT=[ 1] mi n, AREA=[ 3197] (ha),
237 DWF=[ 0] (cms), CN C=[ 57], IA=[ 2. 5] (mm),
238 N=[ 3. 0], TP=[ 6. 65] hr s,
239 Continuous simulation parameters:
240 IaREcper=[ 4] (hr s),
241 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
242 InterEventTime=[ 12] (hr s)
243 Baseflow simulation parameters:
244 BaseFlowOption=[ 1] ,
245 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
246 VHydCond=[ 0. 055] (mm/ hr), END=- 1
247 *%-----|-----
248 *#
249 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
250 *# of 1.75
251 *%-----|-----
252 CONTINUOUS NASHYD NHYD=[ "SW_6" ], DT=[ 1] mi n, AREA=[ 165] (ha),
253 DWF=[ 0] (cms), CN C=[ 67], IA=[ 2. 5] (mm),
254 N=[ 3. 0], TP=[ 4. 18] hr s,
255 Continuous simulation parameters:
256 IaREcper=[ 4] (hr s),
257 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),

```

```

258 InterEventTime=[ 12]( hrs)
259 Baseflow simulation parameters:
260 BaseFlowOption=[ 1] ,
261 InitGWResVol =[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
262 VHydCond=[ 0.055]( mm/ hr) , END=- 1
263 *%-----|-----
264 *#
265 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
266 *# of 1.67
267 *%-----|-----
268 CONTINUOUS NASHYD NHYD=[ "VG_DR" ], DT=[ 1] mi n, AREA=[ 1332]( ha) ,
269 DWF=[ 0]( cms) , CNVC=[ 72] , IA=[ 2.5]( mm) ,
270 N=[ 3.0] , TP=[ 5.95] hr s,
271 Continuous simulation parameters:
272 IaRECper=[ 4]( hr s) ,
273 SMN=[ -1]( mm) , SMAX=[ -1]( mm) , SK=[ 0.010]/ ( mm) ,
274 InterEventTime=[ 12]( hr s)
275 Baseflow simulation parameters:
276 BaseFlowOption=[ 1] ,
277 InitGWResVol =[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
278 VHydCond=[ 0.055]( mm/ hr) , END=- 1
279 *%-----|-----
280 CONTINUOUS NASHYD NHYD=[ "SW_5" ], DT=[ 1] mi n, AREA=[ 224]( ha) ,
281 DWF=[ 0]( cms) , CNVC=[ 77] , IA=[ 2.5]( mm) ,
282 N=[ 3.0] , TP=[ 0.75] hr s,
283 Continuous simulation parameters:
284 IaRECper=[ 4]( hr s) ,
285 SMN=[ -1]( mm) , SMAX=[ -1]( mm) , SK=[ 0.010]/ ( mm) ,
286 InterEventTime=[ 12]( hr s)
287 Baseflow simulation parameters:
288 BaseFlowOption=[ 1] ,
289 InitGWResVol =[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
290 VHydCond=[ 0.055]( mm/ hr) , END=- 1
291 *%-----|-----
292 *#
293 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
294 *# of 1.20
295 *%-----|-----
296 CONTINUOUS NASHYD NHYD=[ "FL_CK" ], DT=[ 1] mi n, AREA=[ 4945]( ha) ,
297 DWF=[ 0]( cms) , CNVC=[ 74] , IA=[ 2.5]( mm) ,
298 N=[ 3.0] , TP=[ 4.45] hr s,
299 Continuous simulation parameters:
300 IaRECper=[ 4]( hr s) ,
301 SMN=[ -1]( mm) , SMAX=[ -1]( mm) , SK=[ 0.010]/ ( mm) ,
302 InterEventTime=[ 12]( hr s)
303 Baseflow simulation parameters:
304 BaseFlowOption=[ 1] ,
305 InitGWResVol =[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
306 VHydCond=[ 0.055]( mm/ hr) , END=- 1
307 *%-----|-----
308 CONTINUOUS NASHYD NHYD=[ "SW_5A2" ], DT=[ 1] mi n, AREA=[ 20]( ha) ,
309 DWF=[ 0]( cms) , CNVC=[ 81] , IA=[ 2.5]( mm) ,
310 N=[ 3.0] , TP=[ 0.62] hr s,
311 Continuous simulation parameters:
312 IaRECper=[ 4]( hr s) ,
313 SMN=[ -1]( mm) , SMAX=[ -1]( mm) , SK=[ 0.010]/ ( mm) ,
314 InterEventTime=[ 12]( hr s)
315 Baseflow simulation parameters:
316 BaseFlowOption=[ 1] ,
317 InitGWResVol =[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
318 VHydCond=[ 0.055]( mm/ hr) , END=- 1
319 *%-----|-----
320 *#
321 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
322 *# of 1.61
323 *%-----|-----

```

324 CONTI NUOUS NASHYD NYHD=[" SW_5A1"], DT=[1] mi n, AREA=[1412] (ha),
325 DWF=[0] (cms), CNV C=[75], IA=[2. 5] (mm),
326 N=[3. 0], TP=[8. 00] hr s,
327 Continuous simulation parameters:
328 IaRECper=[4] (hr s),
329 SM N=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
330 Inter Event Time=[12] (hr s)
331 Baseflow simulation parameters:
332 BaseFlowOpt ion=[1] ,
333 In it GWRes Vol =[50] (mm), GWRes K=[0. 96] (mm/ day/ mm)
334 VHydCond=[0. 055] (mm/ hr), END=- 1

*%-----|

336 CONTI NUOUS NASHYD NYHD=[" SW_4"], DT=[1] mi n, AREA=[585] (ha),
337 DWF=[0] (cms), CNV C=[81], IA=[2. 5] (mm),
338 N=[3. 0], TP=[1. 75] hr s,
339 Continuous simulation parameters:
340 IaRECper=[4] (hr s),
341 SM N=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
342 Inter Event Time=[12] (hr s)
343 Baseflow simulation parameters:
344 BaseFlowOpt ion=[1] ,
345 In it GWRes Vol =[50] (mm), GWRes K=[0. 96] (mm/ day/ mm)
346 VHydCond=[0. 055] (mm/ hr), END=- 1

*%-----|

348 CONTI NUOUS NASHYD NYHD=[" LM_CK"], DT=[1] mi n, AREA=[1021] (ha),
349 DWF=[0] (cms), CNV C=[80], IA=[2. 5] (mm),
350 N=[3. 0], TP=[2. 46] hr s,
351 Continuous simulation parameters:
352 IaRECper=[4] (hr s),
353 SM N=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
354 Inter Event Time=[12] (hr s)
355 Baseflow simulation parameters:
356 BaseFlowOpt ion=[1] ,
357 In it GWRes Vol =[50] (mm), GWRes K=[0. 96] (mm/ day/ mm)
358 VHydCond=[0. 055] (mm/ hr), END=- 1

*%-----|

360 CONTI NUOUS NASHYD NYHD=[" SW_2"], DT=[1] mi n, AREA=[177] (ha),
361 DWF=[0] (cms), CNV C=[77], IA=[2. 5] (mm),
362 N=[3. 0], TP=[0. 75] hr s,
363 Continuous simulation parameters:
364 IaRECper=[4] (hr s),
365 SM N=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
366 Inter Event Time=[12] (hr s)
367 Baseflow simulation parameters:
368 BaseFlowOpt ion=[1] ,
369 In it GWRes Vol =[50] (mm), GWRes K=[0. 96] (mm/ day/ mm)
370 VHydCond=[0. 055] (mm/ hr), END=- 1

*%-----|

372 CONTI NUOUS NASHYD NYHD=[" SM_DR"], DT=[1] mi n, AREA=[1122] (ha),
373 DWF=[0] (cms), CNV C=[81], IA=[2. 5] (mm),
374 N=[3. 0], TP=[3. 25] hr s,
375 Continuous simulation parameters:
376 IaRECper=[4] (hr s),
377 SM N=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
378 Inter Event Time=[12] (hr s)
379 Baseflow simulation parameters:
380 BaseFlowOpt ion=[1] ,
381 In it GWRes Vol =[50] (mm), GWRes K=[0. 96] (mm/ day/ mm)
382 VHydCond=[0. 055] (mm/ hr), END=- 1

*%-----|

384 CONTI NUOUS NASHYD NYHD=[" MO_DR"], DT=[1] mi n, AREA=[2737] (ha),
385 DWF=[0] (cms), CNV C=[76], IA=[2. 5] (mm),
386 N=[3. 0], TP=[3. 03] hr s,
387 Continuous simulation parameters:
388 IaRECper=[4] (hr s),
389 SM N=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),

```

390 InterEventTime=[ 12]( hrs)
391 Baseflow simulation parameters:
392 BaseFlowOption=[ 1] ,
393 InitGWResVol=[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
394 VHydCond=[ 0.055]( mm/ hr) , END=- 1
395 *%-----|-----|
396 * -JFSA 2020 replaced SW_1 with a detailed model from Stantec Report 2007
397 *CONTINUOUS NASHYD NHYD=["SW_1"], DT=[ 1]mi n, AREA=[ 3176]( ha),
398 * DWF=[ 0]( cms) , CN/C=[ 78] , IA=[ 2.5]( mm),
399 * N=[ 3.0] , TP=[ 3.56]hrs,
400 * Continuous simulation parameters:
401 * IaRECper=[ 4]( hrs),
402 * SMN=[ -1]( mm) , SMAX=[ -1]( mm) , SK=[ 0.010]/( mm),
403 * InterEventTime=[ 12]( hrs)
404 * Baseflow simulation parameters:
405 * BaseFlowOption=[ 1] ,
406 * InitGWResVol=[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
407 * VHydCond=[ 0.055]( mm/ hr) , END=- 1
408 *%-----|-----|
409 *#
410 *# Routing hydrographs
411 *#
412 *# Starting with the addition of Jock River Headwater and Subwatershed 13
413 *#
414 ADD HYD NHYDsum=["S_N13"], NHYDs to add=["JR_HW"+"SW_13"]
415 *%-----|-----|
416 *#
417 *# Sum of hydrographs from Node 13 routed to Node 13A
418 *# (Approximated cross-section - see cross-section 258)
419 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
420 *#
421 ROUTE CHANNEL NHYDout=["N13A"] , NHYDin=["S_N13"],
422 RDT=[ 1]( mi n),
423 CHLGTH=[ 9074]( m) , CHSLOPE=[ 0.0220]( %),
424 FPSLOPE=[ 0.0220]( %),
425 SECNUM=[ 1.0] , NSEG=[ 1]
426 ( SEGROUGH, SEGDI ST ( m))=[ 0.04, 15.5] NSEG times
427 ( DI STANCE ( m) , ELEVATI ON ( m))=
428 [- 40, 132.5]
429 [- 30, 132]
430 [- 25, 131.5]
431 [- 13, 130]
432 [- 8, 127.00]
433 [- 7, 126.50]
434 [- 6, 126]
435 [- 5.5, 125.50]
436 [0, 123.75]
437 [4.5, 125.50]
438 [6, 126]
439 [7.5, 126.5]
440 [9, 127]
441 [10, 127.5]
442 [11.5, 128.0]
443 [15.5, 129.5]
444 *%-----|-----|
445 *#
446 *# Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
447 *#
448 ADD HYD NHYDsum=["SN13A"], NHYDs to add=["N13A"+"JR_GWM"]
449 *%-----|-----|
450 *#
451 *# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
452 *#
453 ROUTE RESERVOIR NHYDout=["RES_GM"] , NHYDin=["SN13A"],
454 RDT=[ 1]( mi n),
455 TABLE of ( OUTFLOW STORAGE ) values

```

```

456 (cms) - (ha-m)
457 [ 0.0 , 0.0 ]
458 [ 1.991, 2.144 ]
459 [ 2.693, 39.826 ]
460 [ 3.509, 81.697 ]
461 [ 4.578, 318.774 ]
462 [ 5.647, 594.947 ]
463 [ 7.109, 910.219 ]
464 [ 8.616, 1264.589 ]
465 [ 10.371, 1658.057 ]
466 [ 12.402, 2090.622 ]
467 [ 22.056, 3462.487 ]
468 [ -1 , -1 ] (max twenty pts)
469
470 NHYDovf=[ " " ] ,
471 *%-----|-----|
472 *#
473 SAVE HYD NHYD=[ "RES_GM" ], # OF PCYCLES=[ -1 ], I CASEs h=[ -1 ]
474 HYD_FILE NAME=[ "H_RES GM" ]
475 HYD_COMMENT=[ "Out flow from Res GM" ]
476 *%-----|-----|
477 *# Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
478 *# (Approximated cross-section - see cross-section 258)
479 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
480 ROUTE CHANNEL NHYDout=[ "N12" ] , NHYDin=[ "RES_GM" ] ,
481 RDT=[ 1 ] (min) ,
482 CHLGTH=[ 5926 ] (m) , CHSLOPE=[ 0.0759 ] ( % ) ,
483 FPSLOPE=[ 0.0759 ] ( % ) ,
484 SECNUM=[ 1.0 ] , NSEG=[ 1 ]
485 ( SEGROUGH, SEGDIST (m) )=[ 0.04, 15.5 ] NSEG times
486 ( DISTANCE (m) , ELEVATION (m) )=
487 [- 40, 132.5]
488 [- 30, 132]
489 [- 25, 131.5]
490 [- 13, 130]
491 [- 8, 127.00]
492 [- 7, 126.50]
493 [- 6, 126]
494 [- 5.5, 125.50]
495 [ 0, 123.75]
496 [ 4.5, 125.50]
497 [ 6, 126]
498 [ 7.5, 126.5]
499 [ 9, 127]
500 [ 10, 127.5]
501 [ 11.5, 128.00]
502 [ 15.5, 129.5]
503 *%-----|-----|
504 *#
505 *# Addition of Subwatershed Jock River at Ashton to Node 12
506 *#
507 ADD HYD NHYDsum=[ "S_N12" ] , NHYDsto add=[ "N12"+"JR_ASH" ]
508 SAVE HYD NHYD=[ "S_N12" ] , # OF PCYCLES=[ -1 ], I CASEs h=[ -1 ]
509 HYD_FILE NAME=[ "H_SN12" ]
510 HYD_COMMENT=[ "flow at S_N12 near Ashton" ]
511 *%-----|-----|
512 *#
513 *# Sum of hydrographs from Node 12 routed to Node 11
514 *# (Approximated cross-section - see cross-section 258)
515 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
516 *ROUTE CHANNEL NHYDout=[ "N11" ] , NHYDin=[ "S_N12" ] ,
517 * RDT=[ 1 ] (min) ,
518 * CHLGTH=[ 972 ] (m) , CHSLOPE=[ 0.0514 ] ( % ) ,
519 * FPSLOPE=[ 0.0514 ] ( % ) ,
520 * SECNUM=[ 1.0 ] , NSEG=[ 1 ]
521 * ( SEGROUGH, SEGDIST (m) )=[ 0.04, 15.5 ] NSEG times
522 * ( DISTANCE (m) , ELEVATION (m) )=

```



```

522 * [- 40, 132.5]
523 * [- 30, 132]
524 * [- 25, 131.5]
525 * [- 13, 130]
526 * [- 8, 127.00]
527 * [- 7, 126.50]
528 * [- 6, 126]
529 * [- 5.5, 125.50]
530 * [0, 123.75]
531 * [4.5, 125.50]
532 * [6, 126]
533 * [7.5, 126.5]
534 * [9, 127]
535 * [10, 127.5]
536 * [11.5, 128.00]
537 * [15.5, 129.5]
538 *%-----|-----
539 *#
540 *# Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
541 *#
542 ROUTE CHANNEL NHYDout=["Duml1"], NHYDin=["S_N12"],
543 RDT=[1](min),
544 CHLGTH=[972](m), CHSLOPE=[0.054](%),
545 FPSLOPE=[0.054](%),
546 SECNUM=[1.0], NSEG=[1]
547 ( SEGROUGH, SEGDIST (m))=[0.04, 15.5] NSEG times
548 ( DISTANCE (m), ELEVATION (m))=
549 [- 40, 132.5]
550 [- 30, 132]
551 [- 25, 131.5]
552 [- 13, 130]
553 [- 8, 127.00]
554 [- 7, 126.50]
555 [- 6, 126]
556 [- 5.5, 125.50]
557 [0, 123.75]
558 [4.5, 125.50]
559 [6, 126]
560 [7.5, 126.5]
561 [9, 127]
562 [10, 127.5]
563 [11.5, 128.00]
564 [15.5, 129.5]
565 *%-----|-----
566 *#
567 *# Addition of Subwatershed 11 and No Name Creek to Node 11
568 *#
569 ADD HYD NHYDsum=["S_N11"], NHYDstoadd=["Duml1"+"SW_11"+"NN_CK"]
570 *%-----|-----
571 *#
572 *# Sum of hydrographs from Node 11 routed to Node 10
573 *# Section 1
574 *#
575 ROUTE CHANNEL NHYDout=["N10"], NHYDin=["S_N11"],
576 RDT=[1](min),
577 CHLGTH=[14028](m), CHSLOPE=[0.1568](%),
578 FPSLOPE=[0.1568](%),
579 SECNUM=[1.0], NSEG=[5]
580 ( SEGROUGH, SEGDIST (m))=
581 [0.04, -52.82
582 0.1, -6.47
583 -0.05, 6.47
584 0.1, 45.36
585 0.04, 423.88] NSEG times
586 ( DISTANCE (m), ELEVATION (m))=
587 [- 226.24 , 112.50]

```

```

588             [- 167. 50 , 111. 50]
589             [- 106. 81 , 111. 00]
590             [- 92. 37 , 110. 00]
591             [- 52. 82 , 109. 00]
592             [- 24. 90, 109. 00]
593             [- 17. 02, 108. 50]
594             [- 6. 47, 108. 00]
595             [ 6. 47, 108. 00]
596             [ 15. 67, 108. 50]
597             [ 18. 95, 109. 00]
598             [ 45. 36, 109. 50]
599             [ 120. 79, 110. 00]
600             [ 145. 72, 111. 00]
601             [ 181. 56, 111. 50]
602             [ 423. 88, 112. 50]
603 *%-----|-----
604 *#
605 *# Addition of Subwatershed 10 to Node 10
606 *#
607 ADD HYD          NHYDs um=["S_N10"], NHYDs to add=["N10"+"SW_10"]
608 *%-----|-----
609 SAVE HYD        NHYD=["S_N10"], # OF PCYCLES=[- 1], I CASEs h=[- 1]
610                 HYD_FILE NAME=["H_SN10"]
611                 HYD_COMMENT=["flow at S_N10: N10 + SW_10"]
612 *%-----|-----
613 *# Addition of Kings Creek to S_N10
614 *#
615 ADD HYD          NHYDs um=["S_N10A"], NHYDs to add=["S_N10"+"KG_CK"]
616 *%-----|-----
617 *#
618 *# Sum of hydrographs from Node 10 routed to Node 9
619 *# Section 2
620 *#
621 ROUTE CHANNEL    NHYDout=["N9"] , NHYDin=["S_N10A"] ,
622                 RDT=[ 1] ( mi n) ,
623                 CHLGTH=[ 3982] ( m) ,   CHSLOPE=[ 0. 0753] ( % ) ,
624                                     FPSLOPE=[ 0. 0753] ( % ) ,
625                 SECNUM=[ 1. 0] ,       NSEG=[ 4]
626                 ( SEGROUGH, SEGDI ST ( m) ) =
627                 [ 0. 04, - 30. 27
628                 0. 05, - 18. 42
629                 - 0. 05, 18. 42
630                 0. 04, 131. 58] NSEG times
631                 ( DI STANCE ( m) , ELEVATI ON ( m) ) =
632                 [- 446. 74, 106. 00]
633                 [- 415. 68, 105. 50]
634                 [- 285. 40, 105. 00]
635                 [- 173. 77, 104. 50]
636                 [- 144. 95, 104. 00]
637                 [- 111. 18, 103. 50]
638                 [- 94. 06, 103. 00]
639                 [- 71. 02, 102. 50]
640                 [- 30. 27, 102. 00]
641                 [- 19. 33, 100. 00]
642                 [- 18. 42, 99. 50]
643                 [ 18. 42, 99. 50]
644                 [ 20. 77, 100. 00]
645                 [ 27. 93, 101. 00]
646                 [ 52. 29, 101. 00]
647                 [ 68. 80, 101. 50]
648                 [ 79. 66, 103. 00]
649                 [ 91. 50, 103. 50]
650                 [ 131. 58, 104. 00]
651 *%-----|-----
652 *#
653 *# Addition of Subwatershed 9 and Nichols Creek to Node 9

```

```

654  *#
655  ADD HYD          NHYDs um=[ "S_N9" ], NHYDs to add=[ "N9"+"SW_9"+"NC_CK" ]
656  *%-----|-----|
657  *#
658  *# Sum of hydrographs from Node 9 routed to Node 8
659  *# Section 3
660  *#
661  ROUTE CHANNEL    NHYDout =[ "N8" ] , NHYDin =[ "S_N9" ] ,
662                  RDT=[ 1 ] ( mi n ) ,
663                  CHLGTH=[ 2269 ] ( m ) ,   CHSLOPE=[ 0.0882 ] ( % ) ,
664                                          FPSLOPE=[ 0.0882 ] ( % ) ,
665                  SECNUM=[ 1.0 ] ,          NSEG=[ 3 ]
666                  ( SEGROUGH, SEGDI ST ( m ) ) =
667                    [ 0.1, -17.99
668                    -0.045, 17.31
669                    0.1, 456.58 ] NSEG t i m e s
670                  ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
671                    [ -201.19, 100.50 ]
672                    [ -135.21, 100.00 ]
673                    [ -94.83, 99.50 ]
674                    [ -67.05, 99.00 ]
675                    [ -17.99, 98.50 ]
676                    [ -16.02, 98.00 ]
677                    [ -13.95, 97.50 ]
678                    [ 13.95, 97.50 ]
679                    [ 15.64, 98.00 ]
680                    [ 17.31, 98.50 ]
681                    [ 162.02, 98.50 ]
682                    [ 172.89 , 99.00 ]
683                    [ 314.38, 99.00 ]
684                    [ 343.78, 99.50 ]
685                    [ 365.67, 100.00 ]
686                    [ 376.68, 100.00 ]
687                    [ 393.11, 99.50 ]
688                    [ 404.97, 99.50 ]
689                    [ 431.70, 100.00 ]
690                    [ 456.58, 100.50 ]
691  *%-----|-----|
692  *#
693  *# Addition of Subwatershed 8 and Hobb's Drain to Node 8
694  *#
695  ADD HYD          NHYDs um=[ "S_N8" ], NHYDs to add=[ "N8"+"SW_8"+"HB_DR" ]
696  *%-----|-----|
697  *#
698  *# Sum of hydrographs from Node 8 routed to Node 7
699  *# Section 4
700  *#
701  ROUTE CHANNEL    NHYDout =[ "N7" ] , NHYDin =[ "S_N8" ] ,
702                  RDT=[ 1 ] ( mi n ) ,
703                  CHLGTH=[ 3750 ] ( m ) ,   CHSLOPE=[ 0.0533 ] ( % ) ,
704                                          FPSLOPE=[ 0.0533 ] ( % ) ,
705                  SECNUM=[ 1.0 ] ,          NSEG=[ 3 ]
706                  ( SEGROUGH, SEGDI ST ( m ) ) =
707                    [ 0.12, -18.11
708                    -0.07, 17.22
709                    0.12, 590.05 ] NSEG t i m e s
710                  ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
711                    [ -433.21, 102.00 ]
712                    [ -425.34, 101.50 ]
713                    [ -377.56, 101.50 ]
714                    [ -366.23, 101.00 ]
715                    [ -202.60, 100.50 ]
716                    [ -96.25, 99.50 ]
717                    [ -68.36 99.00 ]
718                    [ -18.11, 98.50 ]
719                    [ -13.81, 97.50 ]

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```

720 [ 13. 81, 97. 50]
721 [ 17. 22, 98. 50]
722 [ 161. 95, 98. 50]
723 [ 173. 11, 99. 00]
724 [ 314. 05, 99. 00]
725 [ 365. 52, 100. 00]
726 [ 404. 70, 99. 50]
727 [ 476. 74, 100. 50]
728 [ 502. 31, 101. 00]
729 [ 584. 69, 101. 00]
730 [ 585. 79, 101. 00]
731 [ 590. 05, 102. 00]
732 *%-----|-----|
733 *#
734 *# Addition of Subwatershed 7 to Node 7
735 *#
736 ADD HYD          NHYDs um=[ "S_N7" ], NHYDs to add=[ "N7"+"SW_7" ]
737 *%-----|-----|
738 SAVE HYD         NHYD=[ "S_N7" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ - 1 ]
739                 HYD_FI LENAME=[ "H_SN7" ]
740                 HYD_COMMENT=[ "flow at S_N7: N7 + SW_7" ]
741 *%-----|-----|
742 *# Insertion of a reservoir to simulate the effects of the Richmond Fen.
743 *# Storage area and volumes were estimated from available topo maps.
744 *# Release rate from fen was assumed to be controlled by the downstream
745 *# river cross-section for summer conditions. It is was assumed that for up to
746 *# 0.75 m of water, the main channel of the river provided the storage. Above
747 *# this depth, the wetland starts to signigicantly store water.
748 *#
749 ROUTE RESERVOIR NHYDout =[ "RES_RF" ] , NHYDi n=[ "S_N7" ] ,
750                 RDT=[ 1 ] ( mi n ) ,
751                 TABLE of ( OUTFLOW STORAGE ) values
752                         ( cms ) - ( ha- m )
753                 TABLE of ( OUTFLOW STORAGE ) values
754                         ( cms ) - ( ha- m )
755                         [ 0. 0 , 0. 0 ]
756                         [ 0. 9051, 2. 40]
757                         [ 2. 907, 4. 13]
758                         [ 9. 744, 9. 18]
759                         [ 20. 304, 14. 96]
760                         [ 34. 167, 310. 21]
761                         [ 74. 993, 605. 46]
762                         [ 104. 876, 900. 71]
763                         [ 140. 56, 2892. 00]
764                         [ 225. 00, 3615. 63]
765                         [ - 1 , - 1 ] (max t wenty pts)
766                 NHYDovf=[ " " ] ,
767 *%-----|-----|
768 SAVE HYD         NHYD=[ "RES_RF" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ - 1 ]
769                 HYD_FI LENAME=[ "H_Res RF" ]
770                 HYD_COMMENT=[ "out flow of Ri chmond Fen" ]
771 *%-----|-----|
772 *#
773 *# Sum of hydrographs from Node 7 routed to Node 6
774 *# Section 5
775 *#
776 ROUTE CHANNEL   NHYDout =[ "N6" ] , NHYDi n=[ "RES_RF" ] ,
777                 RDT=[ 1 ] ( mi n ) ,
778                 CHLGTH=[ 3056 ] ( m ) , CHSLOPE=[ 0. 0818 ] ( % ) ,
779                 FPSLOPE=[ 0. 0818 ] ( % ) ,
780                 SECNUM=[ 1. 0 ] , NSEG=[ 5 ]
781                 ( SEGROUGH, SEGDI ST ( m ) ) =
782                 [ 0. 025, - 70. 8
783                 0. 1, - 23. 9
784                 - 0. 05, 23. 9
785                 0. 06, 39. 8

```

```

786           0. 05, 96. 3] NSEG times
787           ( DI STANCE ( m), ELEVATI ON ( m))=
788             [- 100. 8, 97. 00]
789             [- 70. 8, 96. 50]
790             [- 52. 0, 96. 00]
791             [- 35. 1, 95. 50]
792             [- 30. 6, 95. 00]
793             [- 23. 9, 94. 54]
794             [ 23. 9, 94. 54]
795             [ 39. 8, 95. 00]
796             [ 50. 4, 95. 50]
797             [ 93. 5, 96. 00]
798             [ 94. 9, 96. 50]
799             [ 96. 3, 97. 00]
800 *%-----|-----
801 *#
802 *# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
803 *#
804 ADD HYD           NHYDs um=[ "S_N6" ], NHYDs to add=[ "N6"+"SW_6"+"VG_DR" ]
805 *%-----|-----
806 *#
807 *# Sum of hydrographs from Node 6 routed to Node 5
808 *# Section 6
809 *#
810 ROUTE CHANNEL     NHYDout =[ "N5" ] , NHYDin =[ "S_N6" ] ,
811                   RDT=[ 1 ] ( mi n),
812                   CHLGTH=[ 1852 ] ( m),   CHSLOPE=[ 0. 0540 ] ( %),
813                                           FPSLOPE=[ 0. 0540 ] ( %),
814                   SECNUM=[ 1. 0 ],       NSEG=[ 3]
815                   ( SEGROUGH, SEGDI ST ( m))=
816                     [ 0. 035, - 131. 59
817                     - 0. 045, 48. 96
818                     0. 1, 239. 04] NSEG times
819                   ( DI STANCE ( m), ELEVATI ON ( m))=
820                     [- 686. 30, 94. 50]
821                     [- 675. 70, 94. 00]
822                     [- 492. 52, 93. 00]
823                     [- 467. 28, 94. 00]
824                     [- 131. 59, 94. 00]
825                     [- 92. 79, 92. 50]
826                     [- 18. 06, 91. 00]
827                     [ 18. 06, 91. 00]
828                     [ 43. 47, 92. 50]
829                     [ 48. 96, 94. 00]
830                     [ 177. 43, 94. 00]
831                     [ 239. 04, 94. 50]
832 *%-----|-----
833 *#
834 *# Addition of Subwatershed 5 and Flowing Creek to Node 5
835 *#
836 ADD HYD           NHYDs um=[ "S_N5" ], NHYDs to add=[ "N5"+"SW_5"+"FL_CK" ]
837 *%-----|-----
838 *#
839 *# Sum of hydrographs from Node 5 routed to Node 5A
840 *# Section 7
841 *#
842 ROUTE CHANNEL     NHYDout =[ "N5A" ] , NHYDin =[ "S_N5" ] ,
843                   RDT=[ 1 ] ( mi n),
844                   CHLGTH=[ 556 ] ( m),   CHSLOPE=[ 0. 0900 ] ( %),
845                                           FPSLOPE=[ 0. 0900 ] ( %),
846                   SECNUM=[ 1. 0 ],       NSEG=[ 4]
847                   ( SEGROUGH, SEGDI ST ( m))=
848                     [ 0. 04, - 41. 5
849                     0. 1, - 14. 0
850                     - 0. 045, 14. 0
851                     0. 1, 41. 1] NSEG times

```

```

852 ( DI STANCE ( m) , ELEVATI ON ( m) ) =
853 [- 275. 8, 93. 00]
854 [- 248. 6, 92. 50]
855 [- 237. 0, 92. 00]
856 [- 219. 3, 91. 50]
857 [- 202. 1, 91. 50]
858 [- 186. 0, 92. 00]
859 [- 129. 2, 92. 00]
860 [- 117. 6, 91. 50]
861 [- 100. 6, 91. 00]
862 [- 41. 5, 91. 00]
863 [- 20. 0, 91. 00]
864 [- 14. 0, 90. 54]
865 [ 14. 0, 90. 54]
866 [ 15. 3, 91. 00]
867 [ 17. 3, 91. 50]
868 [ 38. 4, 92. 00]
869 [ 39. 8, 92. 50]
870 [ 41. 1, 93. 00]
871 *%-----|-----|
872 *#
873 *# Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
874 *#
875 ADD HYD NHYDs um=[ "S_N5A" ] , NHYDs t o add=[ "N5A"+"SW_5A2"+"SW_5A1" ]
876 *%-----|-----|
877 *#
878 *# Sum of hydrographs from Node 5A routed to Node 4
879 *# Section 8
880 *#
881 ROUTE CHANNEL NHYDout =[ "N4" ] , NHYDi n=[ "S_N5A" ] ,
882 RDT=[ 1 ] ( mi n) ,
883 CHLGTH=[ 4630 ] ( m) , CHSLOPE=[ 0. 0432 ] ( % ) ,
884 FPSLOPE=[ 0. 0432 ] ( % ) ,
885 SECNUM=[ 1. 0 ] , NSEG=[ 3 ]
886 ( SEGROUGH, SEGDI ST ( m) ) =
887 [ 0. 05, -28. 2
888 -0. 035, 28. 2
889 0. 05, 173. 1 ] NSEG t i mes
890 ( DI STANCE ( m) , ELEVATI ON ( m) ) =
891 [- 38. 9, 92. 00]
892 [- 35. 8, 91. 50]
893 [- 33. 3, 91. 00]
894 [- 28. 2, 90. 50]
895 [- 15. 0, 87. 48]
896 [- 5. 0, 88. 34]
897 [ 5. 0, 86. 20]
898 [ 15. 0, 88. 55]
899 [ 28. 2, 90. 50]
900 [ 29. 7, 91. 00]
901 [ 46. 5, 91. 00]
902 [ 127. 8, 91. 00]
903 [ 148. 7, 91. 50]
904 [ 173. 1, 92. 00]
905 *%-----|-----|
906 *#
907 *# Addition of Subwatershed 4 and Leamy Creek to Node 4
908 *#
909 ADD HYD NHYDs um=[ "S_N4" ] , NHYDs t o add=[ "N4"+"SW_4"+"LM_CK" ]
910 SAVE HYD NHYD=[ "S_N4" ] , # OF PCYCLES=[ - 1 ] , I CASEs h=[ 1 ]
911 HYD_COMMENT=[ "f l ow at S_N4" ]
912 *%-----|-----|
913 *#
914 *# Sum of hydrographs from Node 4 routed to Node 2
915 *# Section 9
916 *#
917 ROUTE CHANNEL NHYDout =[ "N2" ] , NHYDi n=[ "S_N4" ] ,

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```

918 RDT=[ 1] ( mi n),
919 CHLGTH=[ 1667] ( m), CHSLOPE=[ 0. 0600] ( %),
920 FPSLOPE=[ 0. 0600] ( %),
921 SECNUM=[ 1. 0], NSEG=[ 4]
922 ( SEGROUGH, SEGDI ST ( m))=
923 [ 0. 1, - 28. 0
924 - 0. 04, 28. 4
925 0. 06, 31. 7
926 0. 04, 80. 2] NSEG t i m e s
927 ( DI STANCE ( m), ELEVATI ON ( m))=
928 [- 36. 3, 92. 00]
929 [- 32. 6, 91. 50]
930 [- 30. 2, 91. 00]
931 [- 28. 0, 90. 45]
932 [- 15. 0, 87. 48]
933 [- 5. 0, 88. 34]
934 [ 5. 0, 86. 20]
935 [ 15. 0, 88. 55]
936 [ 28. 0, 90. 45]
937 [ 28. 4, 90. 50]
938 [ 30. 4, 91. 00]
939 [ 31. 7, 91. 50]
940 [ 80. 2, 92. 00]
941 *%-----|-----|
942 *#
943 *# Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2
944 *#
945 ADD HYD NHYDs um=[ "S_N2"], NHYDs t o add=[ "N2"+"SW_2"+"SM_DR"+"MO_DR"]
946 *%-----|-----|
947 SAVE HYD NHYD=[ "S_N2"], # OF PCYCLES=[ - 1], I CAS E s h=[ - 1]
948 HYD_FI L E N A M E=[ "H_S_N2"]
949 HYD_C O M M E N T=[ "f l o w a t S_N2 J o c k R i v e r G a u g e a t M o d i e D r. "]
950 *%-----|-----|
951 *#
952 *# Sum of hydrographs from Node 2 routed to Node 1
953 *# Section 10
954 *#
955 *#*****
956 *%READ HYD NHYD=[ "S_N2"],
957 *% HYD_FI L E N A M E=[ "H_S_N2"]
958 *%-----|-----|
959 *#
960 *# Hydrograph from Node 2 routed to Node 416
961 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 9025
962 *#
963 ROUTE CHANNEL NHYDout =["N_416"] , NHYDin=["S_N2"] ,
964 RDT=[ 1] ( mi n),
965 CHLGTH=[ 2327] ( m), CHSLOPE=[ 0. 0498] ( %),
966 FPSLOPE=[ 0. 0498] ( %),
967 SECNUM=[ 1. 0], NSEG=[ 3]
968 ( SEGROUGH, SEGDI ST ( m))=
969 [ 0. 075, - 23. 96
970 - 0. 055, 23. 96
971 0. 075, 157. 38] NSEG t i m e s
972 ( DI STANCE ( m), ELEVATI ON ( m))=
973 [- 336. 97, 93. 5]
974 [- 318. 85, 93]
975 [- 259, 92. 5]
976 [- 133. 18, 92]
977 [- 33. 17, 92]
978 [- 27. 21, 92]
979 [- 26. 14, 91. 5]
980 [- 24. 99, 91]
981 [- 23. 96, 90. 5]
982 [- 14. 33, 88. 26]
983 [- 0. 68, 88. 12]

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```

984 [ 14. 33, 88. 26]
985 [ 23. 96, 90. 5]
986 [ 32. 12, 91]
987 [ 43. 74, 91. 5]
988 [ 57. 09, 92]
989 [ 73. 53, 92. 5]
990 [ 108. 27, 93]
991 [ 125. 88, 93. 5]
992 [ 144. 81, 94]
993 [ 157. 38, 94. 5]
994 *%-----|-----|
995 *#*****|
996 *# Catchment SW1a
997 *# - Portion of RVCA catchment SW1 outside of Reach 1 subwatershed
998 *# - Undeveloped agricultural land
999 *#*****|
1000 CONTINUOUS NASHYD NHYD=[ "SW1a" ], DT=[ 1] mi n, AREA=[ 536. 42] ( ha ),
1001 DWF=[ 0] ( cms ), CN C=[ 72], IA=[ 4. 67] ( mm ),
1002 N=[ 3], TP=[ 2. 79] hr s,
1003 Continuous simulation parameters:
1004 IaRECper=[ 4] ( hr s ),
1005 SMN=[ - 1] ( mm ), SMAX=[ - 1] ( mm ), SK=[ 0. 010] / ( mm ),
1006 InterEventTime=[ 12] ( hr s)
1007 Baseflow simulation parameters:
1008 BaseFlowOption=[ 1] ,
1009 InitGWResVol=[ 50] ( mm ), GWResK=[ 0. 96] ( mm/ day/ mm)
1010 VHydCond=[ 0. 055] ( mm/ hr ), END=- 1
1011 *%-----|-----|
1012 * -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
before station 7245 on Jock River
1013 *CONTINUOUS STANDHYD NHYD=[ "S-1-Okeefe" ], DT=[ 1] ( mi n), AREA=[ 44. 93] ( ha ), XI MP=[ 0. 65],
TI MP=[ 0. 65], DWF=[ 0] ( cms ),
1014 * LOSS=[ 2], SCS curve number CN=[ 75], Pervious surfaces:
I Aper=[ 4. 67] ( mm ), SLPP=[ 2. 0] ( % ),
1015 * LGP=[ 40] ( m ), MNP=[ 0. 25], SCP=[ 0] ( mi n), Impervious surfaces:
I Ai mp=[ 1. 57] ( mm ), SLPI=[ 0. 75] ( % ),
1016 * LGI=[ 547. 296] ( m ), MNI=[ 0. 013], SCI=[ 0] ( mi n),
1017 * Continuous simulation parameters:
1018 * IaRECper=[ 4] ( hr s), IaRECI mp=[ 4] ( hr s),
1019 * SMN=[ - 1] ( mm), SMAX=[ - 1] ( mm), SK=[ 0. 010] / ( mm),
1020 * InterEventTime=[ 12] ( hr s), END=- 1
1021 *%-----|-----|
1022 CONTINUOUS NASHYD NHYD=[ "S-1-Okeefe" ], DT=[ 1] mi n, AREA=[ 44. 93] ( ha ),
1023 DWF=[ 0] ( cms ), CN C=[ 77], IA=[ 4. 67] ( mm ),
1024 N=[ 3], TP=[ 1. 049] hr s,
1025 Continuous simulation parameters:
1026 IaRECper=[ 4] ( hr s),
1027 SMN=[ - 1] ( mm ), SMAX=[ - 1] ( mm ), SK=[ 0. 010] / ( mm ),
1028 InterEventTime=[ 12] ( hr s)
1029 Baseflow simulation parameters:
1030 BaseFlowOption=[ 1] ,
1031 InitGWResVol=[ 50] ( mm ), GWResK=[ 0. 96] ( mm/ day/ mm)
1032 VHydCond=[ 0. 055] ( mm/ hr ), END=- 1
1033 *%-----|-----|
1034 *COMPUTE DUALHYD NHYDin=[ "S-1-Okeefe" ], CINLET=[ 4. 796] ( cms ), NINLET=[ 1],
1035 * MajNHYD=[ "S-1-OkM" ]
1036 * MinNHYD=[ "S-1-OkMN" ]
1037 * TMI STO=[ 9999999] ( cu- m)
1038 *%-----|-----|
1039 *ADD HYD NHYDsum=[ "S-1-OkS" ], NHYDs to add=[ "S-1-OkM" +"S-1-OkMN" ]
1040 *%-----|-----|
1041 *ROUTE RESERVOIR NHYDout=[ "S-1-OkSR" ], NHYDin=[ "S-1-OkS" ],
1042 * RDT=[ 1] ( mi n),
1043 * TABLE of ( OUTFLOW STORAGE ) values
1044 * ( cms ) - ( ha- m)
1045 * [ 0. 0 , 0. 0 ]

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```

1046 * [ 0.5370, 1.7917 ]
1047 * [ -1 , -1 ] (max twenty pts)
1048 * NHYDovf=["S-1-OkSovf"]
1049 *%-----|-----|
1050 ADD HYD NHYDsum=["SN_416"], NHYDs to add=["N_416"+"SW_1a"+"S-1-Okeefe"]
1051 *%-----|-----|
1052 SAVE HYD NHYD=["SN_416"], # OF PCYCLES=[-1], I CASEs h=[1]
1053 HYD_COMMENT=["Total Flows at Highway 416"]
1054 *%-----|-----|
1055 *#
1056 *# Hydrograph from Node 416 routed to Node at Okeefe drain
1057 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 7245
1058 *#
1059 ROUTE CHANNEL NHYDout=["N_OK"], NHYDin=["SN_416"],
1060 RDT=[1](min),
1061 CHLGTH=[497](m), CHSLOPE=[0.3018](%),
1062 FPSLOPE=[0.3018](%),
1063 SECNUM=[1.0], NSEG=[3]
1064 ( SEGROUGH, SEGDI ST (m))=
1065 [0.075, -19.40
1066 -0.055, 19.40
1067 0.075, 377.02] NSEG times
1068 ( DI STANCE (m), ELEVATI ON (m))=
1069 [-1061.41, 92.50]
1070 [-945.91, 92.00]
1071 [-783.64, 91.50]
1072 [-136.74, 91.00]
1073 [-86.04, 91.00]
1074 [-20.86, 91.00]
1075 [-20.18, 90.50]
1076 [-19.40, 90.00]
1077 [-11.68, 86.89]
1078 [0.00, 86.10]
1079 [12.09, 86.81]
1080 [19.40, 90.00]
1081 [34.68, 90.50]
1082 [60.56, 91.00]
1083 [170.14, 91.00]
1084 [175.05, 90.50]
1085 [180.29, 90.00]
1086 [193.41, 90.00]
1087 [195.98, 90.50]
1088 [377.02, 92.50]
1089 *%-----|-----|
1090 *#*****|*****|
1091 *# Catchment OKEEFE
1092 *# - To O'Keefe drain (north of the Jock)
1093 *# - Developed with assumed 43% imp.
1094 *# - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area
1095 513.02 HA)
1096 *# - 2020-11-20 Okeefe detailed model was added as per the NOVATECH SWWHYMD model
1097 (Citi-Gate 2014).
1098 *%-----|-----|
1099 *#*****|*****|
1100 CONTINUOUS NASHYD NHYD=["O-1"], DT=[1]min, AREA=[63.72](ha),
1101 DWF=[0](cms), CNVC=[61], IA=[6.2](mm), N=[3], TP=[.9]hrs,
1102 Continuous simulation parameters:
1103 I aRECper=[4](hrs),
1104 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1105 InterEventTime=[12](hrs)
1106 Baseflow simulation parameters:
1107 BaseFlowOption=[1],
1108 In itGWRes Vol=[50](mm), GWRes K=[0.96](mm/day/mm)
1109 VHydCond=[0.055](mm/hr), END=-1

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```

1110  *%-----|-----
1111  *ROUTE FLOW THROUGH AREA 0-2
1112  ROUTE CHANNEL  NHYDout=["O-1R"], NHYDin=["O-1"], RDT=[1](min),
1113                CHLGTH=[960](m), CHSLOPE=[0.63](%), FPSLOPE=[0.63](%),
1114                SECNUM=[1], NSEG=[3]
1115                ( SEGROUGH, SEGDIST (m))=[0.06, 4 - .043, 6 0.06, 10] NSEG times
1116                ( DISTANCE (m), ELEVATION (m))=[0.00, 2.0]
1117                [0.0, 2.0]
1118                [4.0, 0.0]
1119                [6.0, 0.0]
1120                [10.0, 2.0]
1121  *%-----|-----
1122  CONTINUOUS NASHYD  NHYD=["O-2"], DT=[1]min, AREA=[28.61](ha),
1123                DWF=[0](cms), CNVC=[57], IA=[5.2](mm), N=[3], TP=[1.1]hrs,
1124                Continuous simulation parameters:
1125                IaRECper=[4](hrs),
1126                SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1127                InterEventTime=[12](hrs)
1128                Baseflow simulation parameters:
1129                BaseFlowOption=[1],
1130                InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1131                VHydCond=[0.055](mm/hr), END=-1
1132  *%-----|-----
1133  CONTINUOUS NASHYD  NHYD=["O-4"], DT=[1]min, AREA=[46.94](ha),
1134                DWF=[0](cms), CNVC=[49], IA=[9.2](mm), N=[3], TP=[0.9]hrs,
1135                Continuous simulation parameters:
1136                IaRECper=[4](hrs),
1137                SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1138                InterEventTime=[12](hrs)
1139                Baseflow simulation parameters:
1140                BaseFlowOption=[1],
1141                InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1142                VHydCond=[0.055](mm/hr), END=-1
1143  *%-----|-----
1144  *TOTAL EXTERNAL FLOW NORTH OF O'KEEFE CT. CROSSING
1145  ADD HYD  NHYDsum=["OKF-N"], NHYDstoadd=["O-1R"+"O-2"+"O-4"]
1146  *%-----|-----
1147  *ROUTE FLOW THROUGH AREA 0-6
1148  ROUTE CHANNEL  ROUTE CHANNEL NHYDout=["OKF-NR"], NHYDin=["OKF-N"], RDT=[1](min),
1149                CHLGTH=[210](m), CHSLOPE=[.81](%), FPSLOPE=[.81](%),
1150                SECNUM=[1], NSEG=[3]
1151                ( SEGROUGH, SEGDIST (m))=[0.043, 22.43 - 0.043, 25.07
1152                0.043, 45.54] NSEG times
1153                ( DISTANCE (m), ELEVATION (m))=[0.00, 3.73]
1154                (14.62, 1.56)
1155                (18.41, 1.44)
1156                (22.43, 0.00)
1157                (25.07, 0.70)
1158                (29.10, 1.79)
1159                (33.73, 2.71)
1160                (45.54, 3.58)
1161  *%-----|-----
1162  CONTINUOUS NASHYD  NHYD=["O-6"], DT=[1]min, AREA=[16.46](ha),
1163                DWF=[0](cms), CNVC=[43], IA=[9.2](mm), N=[3], TP=[0.7]hrs,
1164                Continuous simulation parameters:
1165                IaRECper=[4](hrs),
1166                SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1167                InterEventTime=[12](hrs)
1168                Baseflow simulation parameters:
1169                BaseFlowOption=[1],
1170                InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1171                VHydCond=[0.055](mm/hr), END=-1
1172  *%-----|-----
1173  CONTINUOUS STANDHYD  NHYD=["O-3"], DT=[1](min), AREA=[39.67](ha), XI MP=[0.15],
                TIMP=[0.30], DWF=[0](cms),

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1174      LOSS=[ 2], SCS curve number CN=[ 50], Pervious surfaces:
1175      IAper=[ 4.67](mm), SLPP=[ 0.32](%),
1176      LGP=[ 440](m), MNP=[ 0.035], SCP=[ 0](min), Impervious surfaces:
1177      IAimp=[ 1.57](mm), SLPI=[ 0.32](%),
1178      LGI=[ 1880](m), MNI=[ 0.013], SCI=[ 0](min),
1179      Continuous simulation parameters:
1180      IARECper=[ 4](hrs), IARECimp=[ 4](hrs),
1181      SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1182      InterEventTime=[ 12](hrs), END=- 1
1183 *%-----|-----|
1184 CONTINUOUS STANDHYD NHYD=["O-5"], DT=[ 1](min), AREA=[ 60.63](ha), XI MP=[ 0.13],
1185 TIMP=[ 0.26], DWF=[ 0](cms),
1186      LOSS=[ 2], SCS curve number CN=[ 61],
1187      Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1.38](%),
1188      LGP=[ 550](m), MNP=[ 0.035], SCP=[ 0](min), Impervious surfaces:
1189      IAimp=[ 1.57](mm), SLPI=[ 1.38](%),
1190      LGI=[ 1450](m), MNI=[ 0.013], SCI=[ 0](min),
1191      Continuous simulation parameters:
1192      IARECper=[ 4](hrs), IARECimp=[ 4](hrs),
1193      SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1194      InterEventTime=[ 12](hrs), END=- 1
1195 *%-----|-----|
1196 *TOTAL EXTERNAL FLOWS WEST OF THE SITE AND NORTH OF O'KEEFE CRT
1197 *%-----|-----|
1198 ADD HYD NHYDsum=["PT1"], NHYDs to add=["OKF-NR"+"O-3"+"O-5"+"O-6"]
1199 *%-----|-----|
1200 CONTINUOUS NASHYD NHYD=["O-7"], DT=[ 1]min, AREA=[ 5.28](ha),
1201 DWF=[ 0](cms), CN C=[ 54], IA=[ 7.5](mm), N=[ 3], TP=[ 0.6]hrs,
1202      Continuous simulation parameters:
1203      IARECper=[ 4](hrs),
1204      SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1205      InterEventTime=[ 12](hrs)
1206      Baseflow simulation parameters:
1207      BaseFlowOption=[ 1],
1208      InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
1209      VHydCond=[ 0.055](mm/hr), END=- 1
1210 *%-----|-----|
1211 *ANALYSIS POINT 1 - TOTAL FLOW NORTH OF FALLOWFIELD DR. AND O'KEEFE CRT.
1212 ADD HYD NHYDsum=["FF"], NHYDs to add=["PT1"+"O-7"]
1213 *%-----|-----|
1214 *ROUTE FLOW through O'Keefe Drain 1
1215 ROUTE CHANNEL NHYDout=["DRAIN1"], NHYDin=["FF"], RDT=[ 1](min),
1216      CHLGTH=[ 302](m), CHSLOPE=[ 1.00](%), FPSLOPE=[ 1.00](%),
1217      SECNUM=[ 1], NSEG=[ 3]
1218      ( SEGROUGH, SEGDIST (m))=[ 0.07, 13.45 -0.043, 16.55 0.07, 30.00] NSEG
1219      times
1220      ( DISTANCE (m), ELEVATION (m))=[ 0.00, 1.70]
1221      ( 3.45, 0.60)
1222      ( 13.45, 0.50)
1223      ( 14.45, 0.00)
1224      ( 15.55, 0.00)
1225      ( 16.55, 0.50)
1226      ( 26.55, 0.60)
1227      ( 30.00, 1.70)
1228 *%-----|-----|
1229 CONTINUOUS NASHYD NHYD=["DI"], DT=[ 1]min, AREA=[ 1.17](ha),
1230 DWF=[ 0](cms), CN C=[ 84], IA=[ 9.0](mm), N=[ 3], TP=[ 0.28]hrs,
1231      Continuous simulation parameters:
1232      IARECper=[ 4](hrs),
1233      SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1234      InterEventTime=[ 12](hrs)
1235      Baseflow simulation parameters:
1236      BaseFlowOption=[ 1],
1237      InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
1238      VHydCond=[ 0.055](mm/hr), END=- 1
1239 *%-----|-----|

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1235 CONTINUOUS STANDHYD NHYD=["A1"], DT=[1] min, AREA=[2.50](ha), XI MP=[0.68], TI MP=[0.85],
DWF=[0](cms), LOSS=[1]:

1236 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),

1237 Pervious areas: I A per=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),

1238 Impervious areas: I A i mp=[1.57](mm), SLPI=[0.5](%),
LGI=[223.607](m), MNI=[0.013], SCI=[0](min),

1239 Continuous simulation parameters:
1240 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=- 1

1241 *%-----|-----|
1242 ROUTE RESERVOIR NHYDout=["A1-STR"], NHYDin=["A1"], RDT=[1](min),
1243 TABLE of (OUTFLOW STORAGE) values
1244 (cms) - (ha-m)
1245 [0.000 , 0.000]
1246 [0.035 , 0.038]
1247 [0.072 , 0.051]
1248 [0.100 , 0.059]
1249 [0.125 , 0.070]
1250 [0.160 , 0.074]
1251 [0.185 , 0.081]
1252 [-1 , -1] (max twenty pts)
1253 NHYDovf=["A1-OVF"]

1254 *%-----|-----|
1255 CONTINUOUS STANDHYD NHYD=["ST-2"], DT=[1] min, AREA=[0.59](ha), XI MP=[0.46],
TI MP=[0.57], DWF=[0](cms), LOSS=[1]:

1256 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),

1257 Pervious areas: I A per=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),

1258 Impervious areas: I A i mp=[1.57](mm), SLPI=[0.5](%),
LGI=[108.628](m), MNI=[0.013], SCI=[0](min),

1259 Continuous simulation parameters:
1260 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=- 1

1261 *%-----|-----|
1262 ROUTE RESERVOIR NHYDout=["ST2STR"], NHYDin=["ST-2"], RDT=[1](min),
1263 TABLE of (OUTFLOW STORAGE) values
1264 (cms) - (ha-m)
1265 [0.000 , 0.0000]
1266 [0.052 , 0.0010]
1267 [0.053 , 0.0080]
1268 [-1 , -1] (max twenty pts)
1269 NHYDovf=["ST2OVF"]

1270 *%-----|-----|
1271 *%-----|-----|
1272 *TOTAL FLOW NORTH OF STRANDHERD DR. (EAST BRANCH) CROSSING
1273 *%-----|-----|
1274 CONTINUOUS NASHYD NHYD=["O-8"], DT=[1] min, AREA=[60.55](ha),
1275 DWF=[0](cms), CNV C=[69], I A=[4.0](mm), N=[3], TP=[1.0]hrs,
1276 Continuous simulation parameters:
1277 I a REC per=[4](hrs),
1278 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1279 I n t e r E v e n t T i m e=[12](hrs)
1280 Baseflow simulation parameters:
1281 BaseFlowOption=[1],
1282 I n i t G W R e s V o l=[50](mm), G W R e s K=[0.96](mm/day/mm)
1283 VHydCond=[0.055](mm/hr), END=- 1

1284 *%-----|-----|
1285 ROUTE PIPE PTYPE=[2]rect, NHYDout=["O8PIPE"], RNUMBER=[1], PW DTH=[1800](mm),
PHEI GHT=[1200](mm), PLNGTH=[335.1](m),
1286 PROUGH=[0.013], PSLOPE=[0.001](m/m), NHYDin=["O-8"], RDT=[1](min)
1287 *%-----|-----|
1288 *%-----|-----|
1289 ADD HYD NHYDs um=["ST2-IN"], NHYDs to

```

add=[ " DRAI N1 " + " D1 " + " A1 - STR" + " A1 - OVF" + " ST2STR" + " ST2OVF" + " O8PI PE" ]
1290 *%-----|-----|
1291 CONTI NUOUS STANDHYD NHYD=[ " A7" ], DT=[ 1 ] mi n, AREA=[ 3. 51 ] ( ha ), XI MP=[ 0. 68 ], TI MP=[ 0. 85 ],
DWF=[ 0 ] ( c ms ), LOSS=[ 1 ] :
1292 Hort on: Fo=[ 76. 20 ] ( mm/ hr ), Fc=[ 13. 20 ] ( mm/ hr ), DCAY=[ 4. 14 ] ( / hr ),
F=[ 0. 00 ] ( mm ),
1293 Per vious areas: I Aper =[ 4. 67 ] ( mm ), SLPP=[ 0. 5 ] ( % ), LGP=[ 50 ] ( m ),
MNP=[ 0. 250 ], SCP=[ 0 ] ( mi n ),
1294 Impervious areas: I Ai mp=[ 1. 57 ] ( mm ), SLPI =[ 0. 5 ] ( % ),
LGI=[ 264. 953 ] ( m ), MNI =[ 0. 013 ], SCI =[ 0 ] ( mi n ),
1295 Continuous simulation parameters:
1296 IaRECper=[ 4 ] ( hr s ), IaRECI mp=[ 4 ] ( hr s ), Int er Event Ti me=[ 12 ] ( hr s ),
END=- 1
1297 *%-----|-----|
1298 ROUTE RESERVOI R NHYDout =[ " A7 - STR" ], NHYDi n=[ " A7" ], RDT=[ 1 ] ( mi n ),
1299 TABLE of ( OUTFLOW STORAGE ) values
1300 ( c ms ) - ( ha - m )
1301 [ 0. 000 , 0. 000 ]
1302 [ 0. 049 , 0. 054 ]
1303 [ 0. 102 , 0. 072 ]
1304 [ 0. 140 , 0. 082 ]
1305 [ 0. 175 , 0. 099 ]
1306 [ 0. 225 , 0. 105 ]
1307 [ 0. 260 , 0. 114 ]
1308 [ - 1 , - 1 ] ( max t went y pt s )
1309 NHYDovf=[ " A7 - OVF" ]
1310 *%-----|-----|
1311 CONTI NUOUS STANDHYD NHYD=[ " ST - 3" ], DT=[ 1 ] mi n, AREA=[ 0. 71 ] ( ha ), XI MP=[ 0. 46 ],
TI MP=[ 0. 57 ], DWF=[ 0 ] ( c ms ), LOSS=[ 1 ] :
1312 Hort on: Fo=[ 76. 20 ] ( mm/ hr ), Fc=[ 13. 20 ] ( mm/ hr ), DCAY=[ 4. 14 ] ( / hr ),
F=[ 0. 00 ] ( mm ),
1313 Per vious areas: I Aper =[ 4. 67 ] ( mm ), SLPP=[ 0. 5 ] ( % ), LGP=[ 50 ] ( m ),
MNP=[ 0. 250 ], SCP=[ 0 ] ( mi n ),
1314 Impervious areas: I Ai mp=[ 1. 57 ] ( mm ), SLPI =[ 0. 5 ] ( % ),
LGI=[ 119. 164 ] ( m ), MNI =[ 0. 013 ], SCI =[ 0 ] ( mi n ),
1315 Continuous simulation parameters:
1316 IaRECper=[ 4 ] ( hr s ), IaRECI mp=[ 4 ] ( hr s ), Int er Event Ti me=[ 12 ] ( hr s ),
END=- 1
1317 *%-----|-----|
1318 ROUTE RESERVOI R NHYDout =[ " ST3STR" ], NHYDi n=[ " ST - 3" ], RDT=[ 1 ] ( mi n ),
1319 TABLE of ( OUTFLOW STORAGE ) values
1320 ( c ms ) - ( ha - m )
1321 [ 0. 000 , 0. 0000 ]
1322 [ 0. 063 , 0. 0010 ]
1323 [ 0. 064 , 0. 0094 ]
1324 [ - 1 , - 1 ] ( max t went y pt s )
1325 NHYDovf=[ " ST3OVF" ]
1326 *%-----|-----|
1327 *ANALYSIS POINT 2 - TOTAL FLOW AT OUTLET OF STREET 2/3 INTERSECTION
1328 *%-----|-----|
1329 ADD HYD NHYDsum=[ " PT2ST3" ], NHYDs to
add=[ " ST2 - I N" + " A7 - STR" + " A7 - OVF" + " ST3STR" + " ST3OVF" ]
1330 *%-----|-----|
1331 *ROUTE FLOW through O Keefe Drain 2
1332 ROUTE CHANNEL NHYDout =[ " DRAI N2" ], NHYDi n=[ " PT2ST3" ], RDT=[ 1 ] ( mi n ),
1333 CHLGTH=[ 592 ] { m }, CHSLOPE=[ . 23 ] ( % ), FPSLOPE=[ . 23 ] ( % ),
1334 SECNUM=[ 1 ], NSEG=[ 3 ]
1335 ( SEGROUGH, SEGDI ST ( m ) )=[ 0. 07, 12. 60 - 0. 043, 17. 40 0. 07, 30. 00 ] NSEG
ti mes
1336 ( DI STANCE ( m ), ELEVATI ON ( m ) )=[ 0. 00, 1. 70 ]
1337 ( 2. 60, 0. 95 )
1338 ( 12. 60, 0. 75 )
1339 ( 14. 10, 0. 00 )
1340 ( 15. 90, 0. 00 )
1341 ( 17. 40, 0. 75 )
1342 ( 27. 40, 0. 95 )

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1343         (30.00, 1.70)
1344 *%-----|-----|
1345 CONTINUOUS NASHYD NHYD=["D2"], DT=[1] min, AREA=[2.28](ha), DWF=[0](cms), CNVC=[84],
IA=[9.0](mm),
1346 N=[3], TP=[0.99] hrs,
1347 Continuous simulation parameters:
1348 IARECper=[4](hrs),
1349 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1350 InterEventTime=[12](hrs)
1351 Baseflow simulation parameters:
1352 BaseFlowOption=[1],
1353 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1354 VHydCond=[0.055](mm/hr), END=-1
1355 *%-----|-----|
1356 CONTINUOUS STANDHYD NHYD=["A17"], DT=[1] min, AREA=[12.04](ha), XI MP=[0.68],
TI MP=[0.85], DWF=[0](cms), LOSS=[1]:
1357 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1358 Pervious areas: IAPER=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1359 Impervious areas: IAIMP=[1.57](mm), SLPI=[0.5](%),
LGI=[490.714](m), MNI=[0.013], SCI=[0](min),
1360 Continuous simulation parameters:
1361 IARECper=[4](hrs), IARECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1362 *%-----|-----|
1363 ROUTE RESERVOIR NHYDout=["A17STR"], NHYDin=["A17"], RDT=[1](min),
1364 TABLE of ( OUTFLOW STORAGE ) values
1365 (cms) - (ha-m)
1366 [ 0.000 , 0.000 ]
1367 [ 0.169 , 0.185 ]
1368 [ 0.349 , 0.248 ]
1369 [ 0.482 , 0.283 ]
1370 [ 0.602 , 0.338 ]
1371 [ 0.771 , 0.359 ]
1372 [ 0.891 , 0.391 ]
1373 [ -1 , -1 ] (max twenty pts)
1374 NHYDovf=["A17OVF"]
1375 *%-----|-----|
1376 CONTINUOUS STANDHYD NHYD=["ST-4"], DT=[1] min, AREA=[0.35](ha), XI MP=[0.46],
TI MP=[0.57], DWF=[0](cms), LOSS=[1]:
1377 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1378 Pervious areas: IAPER=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1379 Impervious areas: IAIMP=[1.57](mm), SLPI=[0.5](%), LGI=[83.666](m),
MNI=[0.013], SCI=[0](min),
1380 Continuous simulation parameters:
1381 IARECper=[4](hrs), IARECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1382 *%-----|-----|
1383 ROUTE RESERVOIR NHYDout=["ST4STR"], NHYDin=["ST-4"], RDT=[1](min),
1384 TABLE of ( OUTFLOW STORAGE ) values
1385 (cms) - (ha-m)
1386 [ 0.000 , 0.0000 ]
1387 [ 0.031 , 0.0010 ]
1388 [ 0.032 , 0.0050 ]
1389 [ -1 , -1 ] (max twenty pts)
1390 NHYDovf=["ST4OVF"]
1391 *%-----|-----|
1392 CONTINUOUS STANDHYD NHYD=["A18"], DT=[1] min, AREA=[5.30](ha), XI MP=[0.68], TI MP=[0.85],
DWF=[0](cms), LOSS=[1]:
1393 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1394 Pervious areas: IAPER=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),

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1395      Impervious areas: I A i mp=[ 1.57] (mm), SLPI=[ 0.5] (%),
1396      LGI=[ 325.576] (m), MNI=[ 0.013], SCI=[ 0] (mi n),
1397      Continuous simulation parameters:
1397      I a RE C per=[ 4] (hr s), I a RE C i mp=[ 4] (hr s), I n t e r E v e n t T i m e=[ 12] (hr s),
1397      END=- 1
1398 *%-----|-----|
1399 ROUTE RESERVOIR NHYDout=[" A18STR"], NHYDin=[" A18"], RDT=[ 1] (mi n),
1400      TABLE of ( OUTFLOW STORAGE ) values
1401      ( cms ) - ( ha - m)
1402      [ 0.000 , 0.000 ]
1403      [ 0.074 , 0.082 ]
1404      [ 0.154 , 0.109 ]
1405      [ 0.212 , 0.125 ]
1406      [ 0.265 , 0.149 ]
1407      [ 0.339 , 0.158 ]
1408      [ 0.392 , 0.172 ]
1409      [ -1 , -1 ] (max twenty pts)
1410      NHYDovf=[" A18OVF"]
1411 *%-----|-----|
1412 *ANALYSIS POINT 3 - TOTAL FLOW AT OUTLET OF STREET 4
1413 *%-----|-----|
1414 ADD HYD NHYDs um=[" PT3ST4"], NHYDs to
1414 add=[" DRAIN2" + "D2" + "A17STR" + "A17OVF" + "ST4STR" + "ST4OVF" + "A18STR" + "A18OVF"]
1415 *%-----|-----|
1416 *ROUTE FLOW through O Keefe Drain 3
1417 ROUTE CHANNEL NHYDout=[" DRAIN3"], NHYDin=[" PT3ST4"], RDT=[ 1] (mi n),
1418      CHLGTH=[ 525] {m}, CHSLOPE=[ .23] (%), FPSLOPE=[ .23] (%),
1419      SECNUM=[ 1], NSEG=[ 3]
1420      ( SEGROUGH, SEGDI ST (m))=[ 0.07, 12.50 -0.043, 17.50 0.07, 30.00] NSEG
1421      t i m e s
1421      ( DI STANCE (m), ELEVATI ON (m))=[ 0.00, 1.70]
1422      (2.50, 1.00)
1423      (12.50, 0.80)
1424      (14.10, 0.00)
1425      (15.90, 0.00)
1426      (17.50, 0.80)
1427      (27.50, 1.00)
1428      (30.00, 1.70)
1429 *%-----|-----|
1430 CONTINUOUS NASHYD NHYD=[" D3"], DT=[ 1] mi n, AREA=[ 2.51] (ha),
1431      DWF=[ 0] (cms), CNVC=[ 86], IA=[ 8.7] (mm), N=[ 3], TP=[ 0.73] hr s,
1432      Continuous simulation parameters:
1433      I a RE C per=[ 4] (hr s),
1434      SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
1435      I n t e r E v e n t T i m e=[ 12] (hr s)
1436      Baseflow simulation parameters:
1437      BaseFlowOpt ion=[ 1] ,
1438      I n i t G W R e s V o l =[ 50] (mm), G W R e s K=[ 0.96] (mm/ day/ mm)
1439      VHydCond=[ 0.055] (mm/ hr), END=- 1
1440 *%-----|-----|
1441 CONTINUOUS STANDHYD NHYD=[" C1"], DT=[ 1] mi n, AREA=[ 3.41] (ha), XI MP=[ 0.68], TI MP=[ 0.85],
1441      DWF=[ 0] (cms), LOSS=[ 1]:
1442      Hort on: Fo=[ 76.20] (mm/ hr), Fc=[ 13.20] (mm/ hr), DCAY=[ 4.14] (/ hr),
1442      F=[ 0.00] (mm),
1443      P e r v i o u s a r e a s: I A p e r =[ 4.67] (mm), SLPP=[ 0.5] (%), LGP=[ 50] (m),
1443      MNP=[ 0.250], SCP=[ 0] (mi n),
1444      I m p e r v i o u s a r e a s: I A i m p =[ 1.57] (mm), SLPI=[ 0.5] (%),
1444      LGI=[ 261.151] (m), MNI=[ 0.013], SCI=[ 0] (mi n),
1445      Continuous simulation parameters:
1446      I a RE C per=[ 4] (hr s), I a RE C i mp=[ 4] (hr s), I n t e r E v e n t T i m e=[ 12] (hr s),
1446      END=- 1
1447 *%-----|-----|
1448 ROUTE RESERVOIR NHYDout=[" C1- STR"], NHYDin=[" C1"], RDT=[ 1] (mi n),
1449      TABLE of ( OUTFLOW STORAGE ) values
1450      ( cms ) - ( ha - m)
1451      [ 0.000 , 0.000 ]

```

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1452         [ 0.048 , 0.052 ]
1453         [ 0.099 , 0.070 ]
1454         [ 0.136 , 0.080 ]
1455         [ 0.170 , 0.096 ]
1456         [ 0.218 , 0.102 ]
1457         [ 0.252 , 0.111 ]
1458         [ -1 , -1 ] (max twenty pts)
1459         NHYDovf=["C1-OVF"]
1460 *%-----|-----|
1461 CONTINUOUS STANDHYD NHYD=["ST-5"], DT=[1] min, AREA=[0.45](ha), XI MP=[0.46],
TI MP=[0.57], DWF=[0](cms), LOSS=[1]:
1462 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1463 Previous areas: I A per=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1464 Impervious areas: I A i mp=[1.57](mm), SLPI=[0.5](%), LGI=[94.868](m),
MNI=[0.013], SCI=[0](min),
1465 Continuous simulation parameters:
1466 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
1467 *%-----|-----|
1468 ROUTE RESERVOIR NHYDout=["ST5STR"], NHYDin=["ST-5"], RDT=[1](min),
1469 TABLE of ( OUTFLOW STORAGE ) values
1470 (cms) - (ha-m)
1471 [ 0.000 , 0.0000 ]
1472 [ 0.040 , 0.0010 ]
1473 [ 0.041 , 0.0062 ]
1474 [ -1 , -1 ] (max twenty pts)
1475 NHYDovf=["ST5OVF"]
1476 *%-----|-----|
1477 ADD HYD NHYDsum=["ST5-E"], NHYDs to
add=["DRAIN3"+"D3"+"C1-STR"+"C1-OVF"+"ST5STR"+"ST5OVF"]
1478 *%-----|-----|
1479 CONTINUOUS STANDHYD NHYD=["STRAND"], DT=[1](min), AREA=[7.59](ha),
1480 XI MP=[0.64], TI MP=[0.85], DWF=[0](cms), LOSS=[1]:
1481 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1482 Previous areas: I A per=[4.67](mm), SLPP=[0.5](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
1483 Impervious areas: I A i mp=[1.57](mm), SLPI=[0.5](%), LGI=[1230](m),
MNI=[0.013], SCI=[0](min),
1484 Continuous simulation parameters:
1485 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
1486 *%-----|-----|
1487 ROUTE RESERVOIR NHYDout=["S-POND"], NHYDin=["STRAND"], RDT=[1](min),
1488 TABLE of ( OUTFLOW STORAGE ) values
1489 (cms) - (ha-m)
1490 [ 0.000 , 0.000 ]
1491 [ 0.033 , 0.188 ]
1492 [ 0.057 , 0.253 ]
1493 [ 0.104 , 0.287 ]
1494 [ 0.160 , 0.336 ]
1495 [ 0.340 , 0.346 ]
1496 [ 0.471 , 0.360 ]
1497 [ 0.824 , 0.390 ]
1498 [ -1 , -1 ] (max twenty pts)
1499 NHYDovf=["S-OVF"]
1500 *%-----|-----|
1501 ADD HYD NHYDsum=["SSAOUT"], NHYDs to add=["ST5-E"+"S-POND"+"S-OVF"]
1502 *%-----|-----|
1503 SAVE HYD NHYD=["SSAOUT"], # OF PCYCLES=[5], I CASEs h=[1]
1504 HYD_COMMENT=["SSAOUT"]
1505 *%-----|-----|
1506 CONTINUOUS STANDHYD NHYD=["Area-A"], DT=[1] min, AREA=[66.75](ha), XI MP=[0.64],
TI MP=[0.80], DWF=[0](cms), LOSS=[1]:

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1507      Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
1508      F=[ 0.00](mm),
1509      Pervious areas: IAper=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 50](m),
1510      MNP=[ 0.250], SCP=[ 0](min),
1511      Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 0.5](%),
1512      LGI=[ 1155.422](m), MNI=[ 0.013], SCI=[ 0](min),
1513      Continuous simulation parameters:
1514      IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
1515      END=- 1
1516  *%-----|-----|
1517  SAVE HYD      NHYD=["Area-A"], # OF PCYCLES=[ 1], ICASEsh=[ 1]
1518  HYD_COMMENT=["SWMF-A Inflow"]
1519  *%-----|-----|
1520  ROUTE RESERVOIR  NHYDout=["SWMF-A"], NHYDin=["Area-A"], RDT=[ 1](min),
1521  TABLE of ( OUTFLOW STORAGE ) values
1522  (cms) - (ha-m)
1523  [ 0.000 , 0.000 ]
1524  [ 0.103 , 1.077 ]
1525  [ 0.128 , 1.749 ]
1526  [ 0.382 , 2.282 ]
1527  [ 0.703 , 2.582 ]
1528  [ 1.256 , 2.978 ]
1529  [ 1.567 , 3.202 ]
1530  [ 1.955 , 3.493 ]
1531  [ 2.100 , 3.600 ]
1532  [ -1 , -1 ] (max twenty pts)
1533  NHYDovf=["SWWAOV"]
1534  *%-----|-----|
1535  SAVE HYD      NHYD=["SWMF-A"], # OF PCYCLES=[ 1], ICASEsh=[ 1]
1536  HYD_COMMENT=["SWMF-A Outflow"]
1537  *%-----|-----|
1538  *ANALYSIS POINT 4 - TOTAL FLOW AT OUTLET OF STREET 5
1539  *%-----|-----|
1540  ADD HYD      NHYDsum=["PT4ST5"], NHYDs to add=["SSAOUT"+"SWMF-A"+"SWWAOV"]
1541  *%-----|-----|
1542  CONTINUOUS STANDHYD NHYD=["C6"], DT=[ 1]min, AREA=[ 1.87](ha), XI MP=[ 0.68], TI MP=[ 0.85],
1543  DWF=[ 0](cms), LOSS=[ 1]:
1544      Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
1545      F=[ 0.00](mm),
1546      Pervious areas: IAper=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 50](m),
1547      MNP=[ 0.250], SCP=[ 0](min),
1548      Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 0.5](%),
1549      LGI=[ 193.391](m), MNI=[ 0.013], SCI=[ 0](min),
1550      Continuous simulation parameters:
1551      IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
1552      END=- 1
1553  *%-----|-----|
1554  ROUTE RESERVOIR  NHYDout=["C6-STR"], NHYDin=["C6"], RDT=[ 1](min),
1555  TABLE of ( OUTFLOW STORAGE ) values
1556  (cms) - (ha-m)
1557  [ 0.000 , 0.000 ]
1558  [ 0.026 , 0.029 ]
1559  [ 0.054 , 0.038 ]
1560  [ 0.075 , 0.044 ]
1561  [ 0.093 , 0.052 ]
1562  [ 0.120 , 0.056 ]
1563  [ 0.138 , 0.061 ]
1564  [ -1 , -1 ] (max twenty pts)
1565  NHYDovf=["C6-OVF"]
1566  *%-----|-----|
1567  CONTINUOUS STANDHYD NHYD=["C7"], DT=[ 1]min, AREA=[ 1.62](ha), XI MP=[ 0.68], TI MP=[ 0.85],
1568  DWF=[ 0](cms), LOSS=[ 1]:
1569      Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
1570      F=[ 0.00](mm),
1571      Pervious areas: IAper=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 50](m),
1572      MNP=[ 0.250], SCP=[ 0](min),

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1561      Impervious areas: I Aimp=[ 1.57](mm), SLPI=[ 0.5](%),
1562      LGL=[ 180.000](m), MNI=[ 0.013], SCI=[ 0](min),
1563      Continuous simulation parameters:
1564      IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
1565      END=- 1
1566 *%-----|-----|
1567 ROUTE RESERVOIR NHYDout=["C7-STR"], NHYDin=["C7"], RDT=[ 1](min),
1568      TABLE of ( OUTFLOW STORAGE ) values
1569      (cms) - (ha-m)
1570      [ 0.000 , 0.000 ]
1571      [ 0.023 , 0.025 ]
1572      [ 0.047 , 0.033 ]
1573      [ 0.065 , 0.038 ]
1574      [ 0.081 , 0.045 ]
1575      [ 0.104 , 0.048 ]
1576      [ 0.120 , 0.053 ]
1577      [ -1 , -1 ] (max twenty pts)
1578      NHYDovf=["C7-OVF"]
1579 *%-----|-----|
1580 CONTINUOUS STANDHYD NHYD=["ST-6"], DT=[ 1]min, AREA=[ 0.41](ha), XI MP=[ 0.46], TI MP=[ 0.57],
1581 DWF=[ 0](cms), LOSS=[ 1]:
1582 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
1583 F=[ 0.00](mm),
1584 Pervious areas: I Aper=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 50](m),
1585 MNP=[ 0.250], SCP=[ 0](min),
1586 Impervious areas: I Aimp=[ 1.57](mm), SLPI=[ 0.5](%), LGL=[ 90.554](m),
1587 MNI=[ 0.013], SCI=[ 0](min),
1588 Continuous simulation parameters:
1589 IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
1590 END=- 1
1591 *%-----|-----|
1592 ROUTE RESERVOIR NHYDout=["ST6STR"], NHYDin=["ST-6"], RDT=[ 1](min),
1593      TABLE of ( OUTFLOW STORAGE ) values
1594      (cms) - (ha-m)
1595      [ 0.000 , 0.0000 ]
1596      [ 0.036 , 0.0010 ]
1597      [ 0.037 , 0.0058 ]
1598      [ -1 , -1 ] (max twenty pts)
1599      NHYDovf=["ST6OVF"]
1600 *%-----|-----|
1601 *ANALYSIS POINT 5 - TOTAL FLOW AT OUTLET OF STREET 6
1602 *%-----|-----|
1603 ADD HYD NHYDsum=["PT5ST6"], NHYDsto
1604 add=["PT4ST5"+"C6-STR"+"C6-OVF"+"C7-STR"+"C7-OVF"+"ST6STR"+"ST6OVF"]
1605 *%-----|-----|
1606 *ROUTE FLOW through O Keefe Drain 4
1607 ROUTE CHANNEL NHYDout=["DRAIN4"], NHYDin=["PT5ST6"], RDT=[ 1](min),
1608      CHLGTH=[ 324]{m}, CHSLOPE=[.10](%), FPSLOPE=[.10](%),
1609      SECNUM=[ 1], NSEG=[ 3]
1610      ( SEGROUGH, SEGDIST (m))=[ 0.07, 12.00 -0.043, 18.00 0.07, 30.00] NSEG
1611      times
1612      ( DISTANCE (m), ELEVATION (m))=[ 0.00, 2.00]
1613      ( 2.00, 1.20)
1614      ( 12.00, 1.00)
1615      ( 14.00, 0.00)
1616      ( 16.00, 0.00)
1617      ( 18.00, 1.00)
1618      ( 28.00, 1.20)
1619      ( 30.00, 2.00)
1620 *%-----|-----|
1621 CONTINUOUS NASHYD NHYD=["D4"], DT=[ 1]min, AREA=[ 1.73](ha), DWF=[ 0](cms), CNVC=[ 88],
1622 IA=[ 8.4](mm),
1623 N=[ 3], TP=[ 0.60]hrs,
1624 Continuous simulation parameters:
1625 IARECper=[ 4](hrs),
1626 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),

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1617 InterEventTime=[ 12]( hrs)
1618 Baseflow simulation parameters:
1619 BaseFlowOption=[ 1] ,
1620 InitGWResVol=[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
1621 VHydCond=[ 0.055]( mm/ hr) , END=- 1
1622 *%-----|-----|
1623 CONTINUOUS STANDHYD NHYD=[ "Area- B" ] , DT=[ 1] mi n , AREA=[ 24.04]( ha) , XI MP=[ 0.62] ,
TI MP=[ 0.77] , DWF=[ 0]( cms) , LOSS=[ 1] :
1624 Horton: Fo=[ 76.20]( mm/ hr) , Fc=[ 13.20]( mm/ hr) , DCAY=[ 4.14]( / hr) ,
F=[ 0.00]( mm) ,
1625 Pervious areas: IAper=[ 4.67]( mm) , SLPP=[ 1.4]( %) , LGP=[ 50]( m) ,
MNP=[ 0.250] , SCP=[ 0]( mi n) ,
1626 Impervious areas: IAimp=[ 1.57]( mm) , SLPI=[ 1.4]( %) ,
LGI=[ 693.397]( m) , MNI=[ 0.013] , SCI=[ 0]( mi n) ,
1627 Continuous simulation parameters:
1628 IaRECper=[ 4]( hrs) , IaRECI mp=[ 4]( hrs) , InterEventTime=[ 12]( hrs) ,
END=- 1
1629 *%-----|-----|
1630 ROUTE RESERVOIR NHYDout=[ "SWMF- B" ] , NHYDin=[ "Area- B" ] , RDT=[ 1]( mi n) ,
1631 TABLE of ( OUTFLOW STORAGE ) values
1632 ( cms) - ( ha- m)
1633 [ 0.000 , 0.000 ]
1634 [ 0.025 , 0.090 ]
1635 [ 0.175 , 0.510 ]
1636 [ 0.350 , 0.710 ]
1637 [ 0.495 , 0.820 ]
1638 [ 0.648 , 0.980 ]
1639 [ 0.965 , 1.045 ]
1640 [ 1.072 , 1.140 ]
1641 [ -1 , -1 ] (max twenty pts)
1642 NHYDovf=[ "SWMBOVF" ]
1643 *%-----|-----|
1644 ADD HYD NHYDs um=[ "D4- EX" ] , NHYDs to add=[ "DRAIN4"+"D4"+"SWMF- B"+"SWMBOVF" ]
1645 *%-----|-----|
1646 *ROUTE FLOW THROUGH O'Keefe Drain 5
1647 * JFSA: Nov. 2020, added en points to close X-Section
1648 ROUTE CHANNEL NHYDout=[ "DRAIN5" ] , NHYDin=[ "D4- EX" ] , RDT=[ 1]( mi n) ,
1649 CHLGTH=[ 413.0]( m) , CHSLOPE=[ 0.16]( %) , FPSLOPE=[ 0.16]( %) ,
1650 SECNUM=[ 1] , NSEG=[ 3]
1651 ( SEGROUGH, SEGDI ST ( m) )=[ 0.043, 12.29 -0.033, 17.97
1652 0.043, 32.84] NSEG times
1653 ( DI STANCE ( m) , ELEVATI ON ( m) )=(-0.01, 2.50)
1654 [ 0.00, 1.41]
1655 [ 6.13, 0.97]
1656 [ 12.29, 0.89]
1657 [ 15.71, 0.00]
1658 [ 17.97, 0.39]
1659 [ 23.04, 0.35]
1660 [ 32.83, 0.96]
1661 ( 32.84, 2.50)
1662 *%-----|-----|
1663 CONTINUOUS NASHYD NHYD=[ "D5" ] , DT=[ 1] mi n , AREA=[ 1.90]( ha) ,
1664 DWF=[ 0]( cms) , CN C=[ 86] , IA=[ 8.7]( mm) , N=[ 3] , TP=[ 0.69] hr s ,
1665 Continuous simulation parameters:
1666 IaRECper=[ 4]( hrs) ,
1667 SMN=[ -1]( mm) , SMAX=[ -1]( mm) , SK=[ 0.010]/( mm) ,
1668 InterEventTime=[ 12]( hrs)
1669 Baseflow simulation parameters:
1670 BaseFlowOption=[ 1] ,
1671 InitGWResVol=[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
1672 VHydCond=[ 0.055]( mm/ hr) , END=- 1
1673 *%-----|-----|
1674 *EXTERNAL FLOWS SOUTHEAST OF THE SITE NORTH OF MCKENNA CASEY DR.
1675 CONTINUOUS NASHYD NHYD=[ "O-13SDF" ] , DT=[ 1] mi n , AREA=[ 9.74]( ha) ,
1676 DWF=[ 0]( cms) , CN C=[ 81] , IA=[ 4.0]( mm) , N=[ 3] , TP=[ .43] hr s ,
1677 Continuous simulation parameters:

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1678 IaREcper=[ 4] (hrs),
1679 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010]/(mm),
1680 InterEventTime=[ 12] (hrs)
1681 Baseflow simulation parameters:
1682 BaseFlowOption=[ 1] ,
1683 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/day/mm)
1684 VHydCond=[ 0.055] (mm/hr), END=-1
1685 *%-----|-----
1686 *SNOW DISPOSAL FACILITY
1687 *PARAMETERS BASED ON ROBINSON 2006 MODEL
1688 ROUTE RESERVOIR NHYDout=["SDF"], NHYDin=["O-13SDF"], RDT=[ 1] (min),
1689 TABLE of ( OUTFLOW STORAGE ) values
1690 (cms) - (ha-m)
1691 [0.000, 0.000]
1692 [0.150, 0.600]
1693 (0.200, 1.500)
1694 [ -1 , -1 ] (max twenty pts)
1695 NHYDovf=["OVFSDF"]
1696 *%-----|-----
1697 *ANALYSIS POINT 6 - McKenna Casey Dr.
1698 *%-----|-----
1699 ADD HYD NHYDs um=["PT6MC"], NHYDs to add=["DRAIN5"+"D5"+"SDF"]
1700 *%-----|-----
1701 CONTINUOUS NASHYD NHYD=["O-15"], DT=[ 1] min, AREA=[ 10.67] (ha),
1702 DWF=[ 0] (cms), CNVC=[ 82], IA=[ 7.5] (mm), N=[ 3], TP=[ 0.30] hrs,
1703 Continuous simulation parameters:
1704 IaREcper=[ 4] (hrs),
1705 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010]/(mm),
1706 InterEventTime=[ 12] (hrs)
1707 Baseflow simulation parameters:
1708 BaseFlowOption=[ 1] ,
1709 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/day/mm)
1710 VHydCond=[ 0.055] (mm/hr), END=-1
1711 *%-----|-----
1712 *TOTAL FLOW NORTH OF MCKENNA CASEY DR.
1713 ADD HYD NHYDs um=["MC"], NHYDs to add=["PT6MC"+"O-15"]
1714 *%-----|-----
1715 *ROUTE FLOW THROUGH AREA O-14
1716 * JFSA: Nov. 2020, added end points to close X-section
1717 ROUTE CHANNEL NHYDout=["O-14Ch"], NHYDin=["MC"], RDT=[ 1] (min),
1718 CHLGTH=[ 845.3] (m), CHSLOPE=[ 0.10] (%), FPSLOPE=[ 0.10] (%),
1719 SECNUM=[ 1], NSEG=[ 3]
1720 ( SEGROUGH, SEGDIST (m))=[ 0.06, 15.00 -0.033, 18.04 0.06, 31.85] NSEG
times
1721 ( DISTANCE (m), ELEVATION (m))=[ -0.01, 2.5
1722 (0.00, 1.53]
1723 (5.56, 1.47)
1724 (9.21, 1.45)
1725 (12.45, 1.53)
1726 (13.70, 1.50)
1727 (15.00, 0.69)
1728 (15.34, 0.00)
1729 (16.51, 0.05)
1730 (17.30, 0.17)
1731 (18.04, 0.74)
1732 (19.29, 1.32)
1733 (22.73, 1.47)
1734 (31.84, 1.41)
1735 (31.85, 2.50)
1736 *%-----|-----
1737 *% -Change O-14 from NASHYD to STANDHYD, name it "S-1-Okeefe" and add it to S-1
subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
1738 *% -JFSA 2021-02-16, add detailed subcatchment drainage area for each subcatchment
in Corrigan sub-catchment. After adding part of O-14 to S_1 sub-catchment so O-14
becomes 5 ha instead of 30.02 ha and TP becomes 0.133 (5*0.8/30.02) instead of 0.8
1739 CONTINUOUS NASHYD NHYD=["O-14"], DT=[ 1] min, AREA=[ 5] (ha),

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1740 DWF=[ 0](cms), CN C=[ 82], IA=[ 7.5](mm), N=[ 3], TP=[ 0.133]hrs,
1741 Continuous simulation parameters:
1742 IaRECper=[ 4](hrs),
1743 SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1744 InterEventTime=[ 12](hrs)
1745 Baseflow simulation parameters:
1746 BaseFlowOption=[ 1],
1747 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
1748 VHydCond=[ 0.055](mm/hr), END=- 1
1749 *
1750 *%-----|-----|
1751 *ANALYSIS POINT 7 - JOCK RIVER
1752 * 2020-12-01 To Foster Drain
1753 * 2020-12-01 replace ("PT7JR") by ("OKEEFE")
1754 *%-----|-----|
1755 ADD HYD NHYDsum=[ "OKEEFE"], NHYDs to add=[ "O-14Ch"+"O-14"]
1756 *%-----|-----|
1757 *CONTINUOUS STANDHYD NHYD=[ "OKEEFE"], DT=[ 1](min), AREA=[ 448](ha),
1758 * XI MP=[ 0.65], TI MP=[ 0.65], DWF=[ 0](cms), LOSS=[ 2],
1759 * SCS curve number CN=[ 77],
1760 * Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 0.5](%),
1761 * LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
1762 * Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 0.5](%),
1763 * LGI=[ 1728](m), MNI=[ 0.013], SCI=[ 0](min),
1764 * Continuous simulation parameters:
1765 * IaRECper=[ 4](hrs), IaRECimp=[ 4](hrs),
1766 * SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1767 * InterEventTime=[ 18](hrs), END=- 1
1768 *#*****
1769 *# Okeefe Pond
1770 *# - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1771 *# and a ratio of the catchment area to the West Clarke pond rating curve
1772 *# from the MS for the next coordinates
1773 *#*****
1774 *ROUTE RESERVOIR NHYDout=[ "P_OKE"], NHYDin=[ "OKEEFE"],
1775 * RDT=[ 1](min),
1776 * TABLE of ( OUTFLOW STORAGE ) values
1777 * (cms) - (ha-m)
1778 * [ 0.0 , 0.0]
1779 * [ 14.13 , 13.0]
1780 * [ -1 , -1 ] (maximum one hundred pairs of points)
1781 * NHYDovf=[ "ok-OVF"],
1782 *%-----|-----|
1783 * -JFSA 2021-02-25 "S-1-D2" and "S-1-D3" are part of S-1 sub-catchment. They are
1784 * moved to drain before station 6215 on Jock River
1785 *CONTINUOUS STANDHYD NHYD=[ "S-1-D2"], DT=[ 1](min), AREA=[ 18.67](ha), XI MP=[ 0.65],
1786 * TI MP=[ 0.65], DWF=[ 0](cms),
1787 * LOSS=[ 2], SCS curve number CN=[ 75], Pervious surfaces:
1788 * IAper=[ 4.67](mm), SLPP=[ 2.0](%),
1789 * LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min), Impervious surfaces:
1790 * IAimp=[ 1.57](mm), SLPI=[ 0.75](%),
1791 * LGI=[ 352.798](m), MNI=[ 0.013], SCI=[ 0](min),
1792 *
1793 * IaRECper=[ 4](hrs), IaRECimp=[ 4](hrs),
1794 * SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1795 * InterEventTime=[ 12](hrs), END=- 1
1796 *%-----|-----|
1797 CONTINUOUS NASHYD NHYD=[ "S-1-D2"], DT=[ 1]min, AREA=[ 18.67](ha),
1798 DWF=[ 0](cms), CN C=[ 77], IA=[ 4.67](mm),
1799 N=[ 3], TP=[ 1.120]hrs,
1800 Continuous simulation parameters:
1801 IaRECper=[ 4](hrs),
1802 SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1803 InterEventTime=[ 12](hrs)
1804 Baseflow simulation parameters:

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1801 BaseFlowOpt ion=[ 1] ,
1802 Ini t GWRes Vol =[ 50] ( mm) , GWRes K=[ 0. 96] ( mm/ day/ mm)
1803 VHydCond=[ 0. 055] ( mm/ hr) , END=- 1
1804 *%-----|-----|
1805 *COMPUTE DUALHYD NHYDi n=[ " S- 1- D2" ] , CI NLET=[ 2. 062] ( cms) , NI NLET=[ 1] ,
1806 * Mj NHYD=[ " S- 1- D2J" ]
1807 * M nNHYD=[ " S- 1- D2N" ]
1808 * TM STO=[ 9999999] ( cu- m)
1809 *%-----|-----|
1810 *ADD HYD NHYDs um=[ " S- 1- D2S" ] , NHYDs t o add=[ " S- 1- D2J" +" S- 1- D2N" ]
1811 *%-----|-----|
1812 *ROUTE RESERVOIR NHYDout =[ " S- 1- D2R" ] , NHYDi n=[ " S- 1- D2S" ] ,
1813 * RDT=[ 1] ( mi n) ,
1814 * TABLE of ( OUTFLOW STORAGE ) values
1815 * ( cms) - ( ha- m)
1816 * [ 0. 0 , 0. 0 ]
1817 * [ 0. 2231, 0. 7445 ]
1818 * [ -1 , -1 ] (max twenty pts)
1819 * NHYDovf=[ " S- 1- D2Rovf" ]
1820 *%-----|-----|
1821 *CONTINUOUS STANDHYD NHYD=[ " S- 1- D3" ] , DT=[ 1] ( mi n) , AREA=[ 6. 79] ( ha) , XI MP=[ 0. 65] ,
1822 TI MP=[ 0. 65] , DWF=[ 0] ( cms) ,
1823 * LOSS=[ 2] , SCS curve number CN=[ 75] , Pervious surfaces:
1824 I Aper =[ 4. 67] ( mm) , SLPP=[ 2. 0] ( % ) ,
1825 * LGP=[ 40] ( m) , MNP=[ 0. 25] , SCP=[ 0] ( mi n) , Impervious surfaces:
1826 I Ai mp=[ 1. 57] ( mm) , SLPI =[ 0. 75] ( % ) ,
1827 * LGI =[ 212. 760] ( m) , MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
1828 * Continuous simulation parameters:
1829 I aRECper =[ 4] ( hr s) , I aRECI mp=[ 4] ( hr s) ,
1830 * SM N=[ -1] ( mm) , SMAX=[ -1] ( mm) , SK=[ 0. 010] / ( mm) ,
1831 * InterEvent Ti me=[ 12] ( hr s) , END=- 1
1832 *%-----|-----|
1833 CONTINUOUS NASHYD NHYD=[ " S- 1- D3" ] , DT=[ 1] mi n , AREA=[ 6. 79] ( ha) ,
1834 DWF=[ 0] ( cms) , CN C=[ 77] , I A=[ 4. 67] ( mm) ,
1835 N=[ 3] , TP=[ 1. 281] hr s ,
1836 * Continuous simulation parameters:
1837 I aRECper =[ 4] ( hr s) ,
1838 * SM N=[ -1] ( mm) , SMAX=[ -1] ( mm) , SK=[ 0. 010] / ( mm) ,
1839 * InterEvent Ti me=[ 12] ( hr s)
1840 * Baseflow simulation parameters:
1841 BaseFlowOpt ion=[ 1] ,
1842 Ini t GWRes Vol =[ 50] ( mm) , GWRes K=[ 0. 96] ( mm/ day/ mm)
1843 VHydCond=[ 0. 055] ( mm/ hr) , END=- 1
1844 *%-----|-----|
1845 *COMPUTE DUALHYD NHYDi n=[ " S- 1- D3" ] , CI NLET=[ 0. 719] ( cms) , NI NLET=[ 1] ,
1846 * Mj NHYD=[ " S- 1- D3J" ]
1847 * M nNHYD=[ " S- 1- D3N" ]
1848 * TM STO=[ 9999999] ( cu- m)
1849 *%-----|-----|
1850 *ADD HYD NHYDs um=[ " S- 1- D3S" ] , NHYDs t o add=[ " S- 1- D3J" +" S- 1- D3N" ]
1851 *%-----|-----|
1852 *ROUTE RESERVOIR NHYDout =[ " S- 1- D3R" ] , NHYDi n=[ " S- 1- D3S" ] ,
1853 * RDT=[ 1] ( mi n) ,
1854 * TABLE of ( OUTFLOW STORAGE ) values
1855 * ( cms) - ( ha- m)
1856 * [ 0. 0 , 0. 0 ]
1857 * [ 0. 0811, 0. 2708 ]
1858 * [ -1 , -1 ] (max twenty pts)
1859 * NHYDovf=[ " S- 1- D3Rovf" ]
1860 *%-----|-----|
1861 ADD HYD NHYDs um=[ " SN_ OK" ] , NHYDs t o add=[ " N_ OK" +" OKEEFE" +" S- 1- D2" +" S- 1- D3" ]
1862 *%-----|-----|
1863 SAVE HYD NHYD=[ " SN_ OK" ] , # OF PCYCLES=[ -1] , I CASEs h=[ 1]
1864 HYD_ COMMENT=[ "Tot al Fl ows at Okeefe Dr ai n" ]
1865 *%-----|-----|
1866 *#

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1864  *# Hydrograph from Node Okeefe routed to Node at Foster Drain
1865  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
1866  *#
1867  ROUTE CHANNEL      NHYDout=[ "N_FO" ] , NHYDin=[ "SN_OK" ] ,
1868                    RDT=[ 1 ] ( min ),
1869                    CHLGTH=[ 1183 ] ( m ) ,    CHSLOPE=[ 0.0761 ] ( % ) ,
1870                    FPSLOPE=[ 0.0761 ] ( % ) ,
1871                    SECNUM=[ 1.0 ] ,          NSEG=[ 3 ]
1872                    ( SEGROUGH, SEGDIST ( m ) ) =
1873                    [ 0.050, -33.89
1874                    -0.035, 31.59
1875                    0.050, 34.41 ] NSEG times
1876                    ( DISTANCE ( m ) , ELEVATION ( m ) ) =
1877                    [ -794.18, 91.00 ]
1878                    [ -775.41, 91.50 ]
1879                    [ -702.63, 91.50 ]
1880                    [ -546.19, 91.50 ]
1881                    [ -529.54, 91.50 ]
1882                    [ -323.44, 91.00 ]
1883                    [ -320.71, 91.00 ]
1884                    [ -183.59, 91.00 ]
1885                    [ -182.54, 90.50 ]
1886                    [ -181.36, 90.00 ]
1887                    [ -177.37, 90.00 ]
1888                    [ -87.70, 90.00 ]
1889                    [ -33.89, 90.00 ]
1890                    [ -18.52, 86.88 ]
1891                    [ 0.00, 85.20 ]
1892                    [ 16.20, 86.83 ]
1893                    [ 31.59, 90.00 ]
1894                    [ 33.03, 90.50 ]
1895                    [ 34.41, 91.00 ]
1896  *%-----|-----|
1897  *#*****
1898  *# Catchment FOSTER
1899  *# - To Foster ditch (north of the Jock)
1900  *# - Partially developed (medium density); remaining agricultural
1901  *# - 2020-12-01 JFSA Foster area is 332 as per Foster SWF Environmental Study
1902  *# - 2020-12-01 decrease Foster drainage area from (373 HA) to (307.98 HA) after
1903  *# - 2021-02-12 update Foster area to 325.44 ha as measured from QGIS
1904  *#*****
1905  CONTINUOUS STANDHYD NHYD=[ "FOSTER" ] , DT=[ 1 ] min , AREA=[ 325.44 ] ( ha ) ,
1906                    XI MP=[ 0.55 ] , TI MP=[ 0.55 ] , DWF=[ 0 ] ( cms ) , LOSS=[ 2 ] ,
1907                    SCS curve number CN=[ 74 ] ,
1908                    Pervious surfaces: I A per=[ 4.67 ] ( mm ) , SLPP=[ 0.5 ] ( % ) ,
1909                    LGP=[ 40 ] ( m ) , MNP=[ 0.25 ] , SCP=[ 0 ] ( min ) ,
1910                    Impervious surfaces: I A i mp=[ 1.57 ] ( mm ) , SLPI=[ 0.5 ] ( % ) ,
1911                    LGI=[ 1472.956 ] ( m ) , MNI=[ 0.013 ] , SCI=[ 0 ] ( min ) ,
1912                    Continuous simulation parameters:
1913                    I a REC per=[ 4 ] ( hrs ) , I a REC i mp=[ 4 ] ( hrs ) ,
1914                    SM N=[ -1 ] ( mm ) , SMAX=[ -1 ] ( mm ) , SK=[ 0.010 ] / ( mm ) ,
1915                    Inter Event Time=[ 18 ] ( hrs ) , END=- 1
1916  *#*****
1917  *# Foster Pond
1918  *# - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1919  *# and a ratio of the catchment area to the West Clarke pond rating curve
1920  *# from the MSS for the next coordinates
1921  *#*****
1922  ROUTE RESERVOIR    NHYDout=[ "P_FOS" ] , NHYDin=[ "FOSTER" ] ,
1923                    RDT=[ 1 ] ( min ) ,
1924                    TABLE of ( OUTFLOW STORAGE ) values
1925                    ( cms ) - ( ha-m )
1926                    [ 0.0 , 0.0 ]

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1927             [ 10.34 , 10]
1928             [ -1 , -1 ] (max twenty pts)
1929             NHYDovf=[ "FO- OVF" ]
1930 *%-----|-----|
1931 ADD HYD             NHYDsum=[ "FOSTER- OUT" ], NHYDs to add=[ "P_FOS"+"FO- OVF" ]
1932 *%-----|-----|
1933 *#*****|
1934 * -Brazeau area from P 1800-19 =[71.751], change to 63.59 ha based on GIS measurements
1935 * -JFSA, 2021-01-19 update "W_CLAR_BRAZ" to 73.29 ha based on GIS measurements
1936 * -JFSA, 2021-01-22 Brazeau ("MS_P10"+"P10-OVF")brazeau pond discharges directly
to the jock river through a road side ditch on the west side of Borrisokane road
(station 6016)
1937 CONTINUOUS STANDHYD NHYD=[ "W_CLAR_BRAZ" ], DT=[ 1]mi n, AREA=[ 73.29](ha),
1938 XI MP=[ 0.6], TI MP=[ 0.65], DWF=[ 0](cms), LOSS=[ 2],
1939 SCS curve number CN=[ 77],
1940 Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
1941 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n),
1942 Impervious surfaces: I A i mp=[ 1.57](mm), SLPI=[ 0.5](%),
1943 LGI=[ 699.00](m), MNI=[ 0.013], SCI=[ 0](mi n),
1944 Continuous simulation parameters:
1945 I a REC per=[ 4](hr s), I a REC i mp=[ 4](hr s),
1946 SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1947 I nter Event Ti me=[ 18](hr s), END=- 1
1948 *%-----|-----|
1949 * 2020-12-01 correct pond curve values
1950 ROUTE RESERVOIR NHYDout =["MS_P10"], NHYDi n=["W_CLAR_BRAZ"],
1951 RDT=[ 1](mi n),
1952 TABLE of ( OUTFLOW STORAGE ) values
1953 (cms) - (ha-m)
1954 [ 0.0 , 0.0 ]
1955 [ 0.068 , 0.001 ]
1956 [ 0.271 , 0.022 ]
1957 [ 0.379 , 0.051 ]
1958 [ 0.48 , 0.091 ]
1959 [ 0.853 , 0.341 ]
1960 [ 1.005 , 0.61 ]
1961 [ 1.128 , 1.231 ]
1962 [ 1.155 , 1.592 ]
1963 [ 1.194 , 1.876 ]
1964 [ 1.2 , 1.921 ]
1965 [ 1.259 , 2.369 ]
1966 [ 1.3 , 2.665 ]
1967 [ 1.349 , 2.813 ]
1968 [ -1 , -1 ] (max twenty pts)
1969 NHYDovf=[ "P10- OVF" ]
1970 *%-----|-----|
1971 * -JFSA 2021-02-26 "S-1-FO-D2" is a part of S-1 sub-catchment. It is moved to drain
before station 980 on Foster Drain
1972 *CONTINUOUS STANDHYD NHYD=[ "S-1-FO-D2" ], DT=[ 1]mi n, AREA=[ 4.94](ha),
1973 * XI MP=[ 0.55], TI MP=[ 0.55], DWF=[ 0](cms), LOSS=[ 2],
1974 * SCS curve number CN=[ 74],
1975 * Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 0.5](%),
1976 * LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n),
1977 * Impervious surfaces: I A i mp=[ 1.57](mm), SLPI=[ 0.5](%),
1978 * LGI=[ 181.475](m), MNI=[ 0.013], SCI=[ 0](mi n),
1979 * Continuous simulation parameters:
1980 * I a REC per=[ 4](hr s), I a REC i mp=[ 4](hr s),
1981 * SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1982 * I nter Event Ti me=[ 18](hr s), END=- 1
1983 *%-----|-----|
1984 CONTINUOUS NASHYD NHYD=[ "S-1-FO-D2" ], DT=[ 1]mi n, AREA=[ 4.94](ha),
1985 DWF=[ 0](cms), CN C=[ 77], I A=[ 4.67](mm),
1986 N=[ 3], TP=[ 1.10]hr s,
1987 Continuous simulation parameters:
1988 I a REC per=[ 4](hr s),
1989 SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),

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1990 InterEventTime=[ 12](hrs)
1991 Baseflow simulation parameters:
1992 BaseFlowOption=[ 1] ,
1993 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
1994 VHydCond=[ 0.055](mm/hr), END=- 1
1995 *%-----|-----|
1996 *COMPUTE DUALHYD NHYDin=["S-1-FO-D2"], CINLET=[ 0.508](cms), NINLET=[ 1],
1997 * MjNHYD=["S-1-FO-D2J"]
1998 * MnNHYD=["S-1-FO-D2N"]
1999 * TMSTO=[ 9999999](cu-m)
2000 *%-----|-----|
2001 *ADD HYD NHYDsum=["S-1-FO-D2S"], NHYDsto add=["S-1-FO-D2J"+"S-1-FO-D2N"]
2002 *%-----|-----|
2003 *ROUTE RESERVOIR NHYDout=["S-1-FO-D2R"], NHYDin=["S-1-FO-D2S"],
2004 * RDT=[ 1](min),
2005 * TABLE of ( OUTFLOW STORAGE ) values
2007 * [ 0.0 , 0.0 ]
2008 * [ 0.0590, 0.1970 ]
2009 * [ -1 , -1 ] (max twenty pts)
2010 * NHYDovf=["S-1FOD2ovf"]
2011 *%-----|-----|
2012 ADD HYD NHYDsum=["980"], NHYDsto add=["FOSTER-OUT"+"S-1-FO-D2"]
2013 *%-----|-----|
2014 SAVE HYD NHYD=["980"], # OF PCYCLES=[ -1], ICASEsh=[ 1]
2015 HYD_COMMENT=["Total Flows at Station 980 on Foster Drain"]
2016 *%-----|-----|
2017 *#
2018 *# Hydrograph from Node Foster SWM (Station 980) to Node at station 520
2019 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 980
2020 *#
2021 ROUTE CHANNEL NHYDout=["980-out"], NHYDin=["980"],
2022 RDT=[ 1](min),
2023 CHLGTH=[ 460](m), CHSLOPE=[ 0.04348](%),
2024 FPSLOPE=[ 0.04348](%),
2025 SECNUM=[ 1.0], NSEG=[ 3]
2026 ( SEGROUGH, SEGDI ST (m)) =
2027 [ 0.050, 45.90
2028 -0.035, 53.30
2029 0.050, 100] NSEG times
2030 ( DISTANCE (m), ELEVATION (m)) =
2031 [ 0, 91.75 ]
2032 [ 42.4, 92.18 ]
2033 [ 43.5, 92.16 ]
2034 [ 44.1, 92.1 ]
2035 [ 44.6, 92 ]
2036 [ 44.8, 91.86 ]
2037 [ 45.9, 91.04 ]
2038 [ 46.4, 90.65 ]
2039 [ 46.8, 90.36 ]
2040 [ 47.9, 90.32 ]
2041 [ 48.7, 90.35 ]
2042 [ 50.7, 90.33 ]
2043 [ 52.2, 90.38 ]
2044 [ 52.5, 90.59 ]
2045 [ 53.3, 91.28 ]
2046 [ 54, 91.83 ]
2047 [ 54.3, 92 ]
2048 [ 54.8, 92.08 ]
2049 [ 55.4, 92.12 ]
2050 [ 100, 91.84 ]
2051 *%-----|-----|
2052 * -JFSA 2021-02-26 "S-1-FO-D1" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2053 *CONTINUOUS STANDHYD NHYD=["S-1-FO-D1"], DT=[ 1]min, AREA=[ 5.11](ha),
2054 * XI MP=[ 0.65], TI MP=[ 0.65], DWF=[ 0](cms), LOSS=[ 2],

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2055 *          SCS curve number CN=[ 74],
2056 *          Pervious surfaces: I Aper=[ 4.67] (mm), SLPP=[ 0.5] (%),
2057 *          LGP=[ 40] (m), MNP=[ 0.25], SCP=[ 0] (min),
2058 *          Impervious surfaces: I Aimp=[ 1.57] (mm), SLPI=[ 0.5] (%),
2059 *          LGI=[ 184.572] (m), MNI=[ 0.013], SCI=[ 0] (min),
2060 *          Continuous simulation parameters:
2061 *          I aRECper=[ 4] (hrs), I aRECimp=[ 4] (hrs),
2062 *          SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
2063 *          InterEventTime=[ 18] (hrs), END=- 1
2064 *%-----|-----|
2065 CONTINUOUS NASHYD NHYD=[ "S-1-FO-DI" ], DT=[ 1] min, AREA=[ 5.11] (ha),
2066 DWF=[ 0] (cms), CNVC=[ 77], IA=[ 4.67] (mm),
2067 N=[ 3], TP=[ 1.10] hrs,
2068 Continuous simulation parameters:
2069 I aRECper=[ 4] (hrs),
2070 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
2071 InterEventTime=[ 12] (hrs)
2072 Baseflow simulation parameters:
2073 BaseFlowOption=[ 1],
2074 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm3/day/mm)
2075 VHydCond=[ 0.055] (mm/hr), END=- 1
2076 *%-----|-----|
2077 *COMPUTE DUALHYD NHYDin=[ "S-1-FO-DI" ], CINLET=[ 0.605] (cms), NINLET=[ 1],
2078 *          MajNHYD=[ "S-1-FO-DIJ" ]
2079 *          MinNHYD=[ "S-1-FO-DIN" ]
2080 *          TMLSTO=[ 9999999] (cu-m)
2081 *%-----|-----|
2082 *ADD HYD NHYDsum=[ "S-1-FO-DIS" ], NHYDsto add=[ "S-1-FO-DIN"+"S-1-FO-DIJ" ]
2083 *%-----|-----|
2084 *ROUTE RESERVOIR NHYDout=[ "S-1-FO-DIR" ], NHYDin=[ "S-1-FO-DIS" ],
2085 *          RDT=[ 1] (min),
2086 *          TABLE of ( OUTFLOW STORAGE ) values
2087 *          ( cms ) - ( ha-m)
2088 *          [ 0.0 , 0.0 ]
2089 *          [ 0.0611, 0.2038 ]
2090 *          [ -1 , -1 ] (max twenty pts)
2091 *          NHYDovf=[ "S-1FODlovf" ]
2092 *%-----|-----|
2093 ADD HYD NHYDsum=[ "520" ], NHYDsto add=[ "980-out"+"S-1-FO-DI" ]
2094 *%-----|-----|
2095 SAVE HYD NHYD=[ "520" ], # OF PCYCLES=[ -1], ICASEsh=[ 1]
2096 HYD_COMMENT=[ "Total Flows at Sation 520 on Foster Drain" ]
2097 *%-----|-----|
2098 *# Hydrograph from Node at Station 520 (Foster Drain) to Node at station 6016 (Jock
River)
2099 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 520
2100 *#
2101 ROUTE CHANNEL NHYDout=[ "520-out" ], NHYDin=[ "520" ],
2102 RDT=[ 1] (min),
2103 CHLGTH=[ 860] (m), CHSLOPE=[ 0.5872] (%),
2104 FPSLOPE=[ 0.5872] (%),
2105 SECNUM=[ 1.0], NSEG=[ 3]
2106 ( SEGROUGH, SEGDIST (m))=
2107 [ 0.050, 45.90
2108 -0.035, 54.3
2109 0.050, 100.1097] NSEG times
2110 ( DISTANCE (m), ELEVATION (m))=
2111 [ 0, 91.26 ]
2112 [ 44.9, 91.46 ]
2113 [ 45.1, 91.37 ]
2114 [ 45.9, 90.84 ]
2115 [ 47, 90.32 ]
2116 [ 47.5, 90.22 ]
2117 [ 48, 90.17 ]
2118 [ 50.7, 90.19 ]
2119 [ 51.5, 90.17 ]

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2120 [ 52.2, 90.13 ]
2121 [ 52.7, 90.12 ]
2122 [ 53.3, 90.14 ]
2123 [ 53.5, 90.31 ]
2124 [ 53.9, 90.59 ]
2125 [ 54.3, 90.87 ]
2126 [ 54.7, 91.04 ]
2127 [ 55.3, 91.24 ]
2128 [ 55.5, 91.26 ]
2129 [ 63.7, 91.37 ]
2130 [ 100.1097, 91.43 ]
2131 *%-----|-----|
2132 * -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2133 *CONTINUOUS STANDHYD NHYD=["S-1-FO-F-D"], DT=[1]mi n, AREA=[14.96](ha),
2134 * XI MP=[0.65], TI MP=[0.65], DWF=[0](cms), LOSS=[2],
2135 * SCS curve number CN=[74],
2136 * Pervious surfaces: I A per=[4.67](mm), SLPP=[0.5](%),
2137 * LGP=[40](m), MNP=[0.25], SCP=[0](mi n),
2138 * Impervious surfaces: I A i mp=[1.57](mm), SLPI=[0.5](%),
2139 * LGI=[315.806](m), MNI=[0.013], SCI=[0](mi n),
2140 * Continuous simulation parameters:
2141 * I a RE C per=[4](hrs), I a RE C i mp=[4](hrs),
2142 * SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2143 * Inter Event Time=[18](hrs), END=-1
2144 *%-----|-----|
2145 CONTINUOUS NASHYD NHYD=["S-1-FO-F-D"], DT=[1]mi n, AREA=[14.96](ha),
2146 DWF=[0](cms), CN C=[77], I A=[4.67](mm),
2147 N=[3], TP=[1.007]hrs,
2148 Continuous simulation parameters:
2149 I a RE C per=[4](hrs),
2150 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2151 Inter Event Time=[12](hrs)
2152 Baseflow simulation parameters:
2153 BaseFlowOption=[1],
2154 Ini t GW Res Vol=[50](mm), GW Res K=[0.96](mm/ day/ mm)
2155 VHydCond=[0.055](mm/ hr), END=-1
2156 *%-----|-----|
2157 *COMPUTE DUALHYD NHYD i n=["S-1-FO-F-D"], CI NLET=[1.749](cms), NI NLET=[1],
2158 * M i j NHYD=["S-1FO-F-DJ"]
2159 * M nNHYD=["S-1FO-F-DN"]
2160 * TM I STO=[9999999](cu-m)
2161 *%-----|-----|
2162 *ADD HYD NHYDs um=["S-1FO-F-DS"], NHYDs to add=["S-1FO-F-DJ"+"S-1FO-F-DN"]
2163 *%-----|-----|
2164 *ROUTE RESERVOIR NHYDout=["S-1FO-F-DR"], NHYD i n=["S-1FO-F-DS"],
2165 * RDT=[1](mi n),
2166 * TABLE of ( OUTFLOW STORAGE ) values
2167 * ( cms ) - ( ha-m )
2168 * [ 0.0 , 0.0 ]
2169 * [ 0.1788, 0.5966 ]
2170 * [ -1 , -1 ] (max twenty pts)
2171 * NHYDovf=["S-1FoFDovf"]
2172 *%-----|-----|
2173 * -JFSA 2021-02-26 "S-1-D8" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2174 * -JFSA 2021-03-02 "S-1-D8" is Borriskane Rd. so it will remain STANDHYD in all
scenarios
2175 CONTINUOUS STANDHYD NHYD=["S-1-D8"], DT=[1](mi n), AREA=[5.27](ha), XI MP=[0.65],
TI MP=[0.65], DWF=[0](cms),
2176 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
I A per=[4.67](mm), SLPP=[2.0](%),
2177 LGP=[40](m), MNP=[0.25], SCP=[0](mi n), Impervious surfaces:
I A i mp=[1.57](mm), SLPI=[0.75](%),
2178 LGI=[187.439](m), MNI=[0.013], SCI=[0](mi n),
2179 Continuous simulation parameters:

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2180 IaRECper=[ 4](hr s), IaRECI mp=[ 4](hr s),
2181 SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2182 InterEventTime=[ 12](hr s), END=- 1
2183 *%-----|-----
2184 * This is a road so it is always STANDHYD
2185 *CONTINUOUS NASHYD NHYD=["S-1-D8"], DT=[ 1]mi n, AREA=[ 5.27](ha),
2186 * DWF=[ 0](cms), CNV C=[ 77], IA=[ 4.67](mm),
2187 * N=[ 3], TP=[ 1.10]hr s,
2188 * Continuous simulation parameters:
2189 * IaRECper=[ 4](hr s),
2190 * SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2191 * InterEventTime=[ 12](hr s)
2192 * Baseflow simulation parameters:
2193 * BaseFlowOption=[ 1],
2194 * InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2195 * VHydCond=[ 0.055](mm/hr), END=- 1
2196 *%-----|-----
2197 *COMPUTE DUALHYD NHYDin=["S-1-D8"], CINLET=[ 2.279](cms), NINLET=[ 1],
2198 * MjNHYD=["S-1-D8J"]

2200 * TMSTO=[ 9999999](cu-m)
2201 *%-----|-----
2202 *ADD HYD NHYDsum=["S-1-D8S"], NHYDs to add=["S-1-D8J"+"S-1-D8N"]
2203 *%-----|-----
2204 *ADD HYD NHYDsum=["S-1-D"], NHYDs to add=["S-1-Okeefe"+"S-1"+"S-1-Fost"]
2205 *%-----|-----
2206 *COMPUTE DUALHYD NHYDin=["S-1-D"], CINLET=[ 11.616](cms), NINLET=[ 1],
2207 * MjNHYD=["S-1-D-M"]
2208 * MnNHYD=["S-1-D-MN"]
2209 * TMSTO=[ 5974](cu-m)
2210 *%-----|-----
2211 *ADD HYD NHYDsum=["S-1-DEV"], NHYDs to add=["S-1-D-M"+"S-1-D-MN"]
2212 *%-----|-----
2213 *ROUTE RESERVOIR NHYDout=["S-1-D8R"], NHYDin=["S-1-D8S"],
2214 * RDT=[ 1](mi n),
2215 * TABLE of ( OUTFLOW STORAGE ) values
2216 * ( cms ) - ( ha-m)
2217 * [ 0.0 , 0.0 ]
2218 * [ 0.0630, 0.2102 ]
2219 * [ -1 , -1 ] (max twenty pts)
2220 * NHYDovf=["S-1-D8Rovf"]
2221 *%-----|-----
2222 * -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock Ri ver
2223 CONTINUOUS NASHYD NHYD=["S-1-A"], DT=[ 1]mi n, AREA=[ 75.88](ha),
2224 DWF=[ 0](cms), CNV C=[ 77], IA=[ 4.67](mm),
2225 N=[ 3], TP=[ 0.619]hr s,
2226 Continuous simulation parameters:
2227 IaRECper=[ 4](hr s),
2228 SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2229 InterEventTime=[ 12](hr s)
2230 Baseflow simulation parameters:
2231 BaseFlowOption=[ 1],
2232 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2233 VHydCond=[ 0.055](mm/hr), END=- 1
2234 *%-----|-----
2235 * -JFSA 2021-01-22 "W_CLAR_UNDE" (west of Clarke sub-catchment) discharges
directly to the jock river through a road side ditch on the west side of Borrisokane
road (station 6016)
2236 CONTINUOUS NASHYD NHYD=["W_CLAR_UNDE"], DT=[ 1]mi n, AREA=[ 35.65](ha),
2237 DWF=[ 0](cms), CNV C=[ 77], IA=[ 4.67](mm),
2238 N=[ 3], TP=[ 1.10]hr s,
2239 Continuous simulation parameters:
2240 IaRECper=[ 4](hr s),
2241 SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2242 InterEventTime=[ 12](hr s)

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2243 Baseflow simulation parameters:
2244 BaseFlowOption=[ 1] ,
2245 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
2246 VHydCond=[ 0.055] (mm/ hr), END=- 1
2247 *%-----|-----
2248 ADD HYD NHYDsum=[ "SN_FO" ], NHYDs to
add=[ "N_FO"+"520-out"+"MS_P10"+"P10-OVF"+"W_CLAR_UNDE"+"S-1-FO-F-D"+"S-1-D8"+"S-1-A"]
2249 *%-----|-----
2250 SAVE HYD NHYD=[ "SN_FO" ], # OF PCYCLES=[ -1], ICASEsh=[ 1]
2251 HYD_COMMENT=[ "Total Flows at Foster Drain"]
2252 *%-----|-----
2253 *# Hydrograph from Node Foster routed to Node at Cedarview Road
2254 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6016
2255 *#
2256 ROUTE CHANNEL NHYDout=[ "N_CE" ], NHYDin=[ "SN_FO" ],
2257 RDT=[ 1] (min),
2258 CHLGTH=[ 159] (m), CHSLOPE=[ 0.0818] ( %),
2259 FPSLOPE=[ 0.0818] ( %),
2260 SECNUM=[ 1.0], NSEG=[ 3]
2261 ( SEGROUGH, SEGDI ST (m))=
2262 [ 0.050, -15.46
2263 -0.035, 26.55
2264 0.050, 116.76] NSEG times
2265 ( DI STANCE (m), ELEVATI ON (m))=
2266 [- 645.23, 91.50]
2267 [- 391.20, 91.50]
2268 [- 91.00, 91.50]
2269 [- 85.52, 91.50]
2270 [- 15.46, 89.40]
2271 [- 9.79, 89.31]
2272 [- 3.22, 86.24]
2273 [ 3.22, 85.07]
2274 [ 10.96, 85.79]
2275 [ 16.44, 86.49]
2276 [ 26.55, 89.45]
2277 [ 29.03, 90.27]
2278 [ 35.76, 90.67]
2279 [ 36.67, 91.00]
2280 [ 108.08, 91.00]
2281 [ 109.82, 90.50]
2282 [ 112.04, 90.50]
2283 [ 114.62, 91.00]
2284 [ 116.76, 91.50]
2285 *%-----|-----
2286 *#*****
2287 *# Catchment S-1
2288 *# - To Jock River (north and south of Jock)
2289 *# - Primarily agricultural fields; portion of sand quarry
2290 *%-----|-----
2291 *% -2020-12-17 "S-1-Undev" and "S-1-Fost" was a part of Foster drain, they are below
the foster pond. Now they are added to S-1 subcatchment based on Project 1474-BCDC,
JFSA, Nov. 2020
2292 *% -2020-12-17 Change O-14 (it was part of Okeefe drain) to "S-1-Okeefe" and add it
to S-1 subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
2293 *% -2020-12-17 Add "S-1-BCDC" as NASHYD
2294 *% -2020-12-17 all other S-1 subcatchment as STANDHYD with DUALHYD and ROUTE RESERVOIR
2295 *%-----|-----
2296 *#*****
2297 * -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2298 *CONTINUOUS NASHYD NHYD=[ "S-1-A" ], DT=[ 1] min, AREA=[ 75.88] (ha),
2299 * DWF=[ 0] (cms), CNVC=[ 77], IA=[ 4.67] (mm),
2300 * N=[ 3], TP=[ 0.619] hrs,
2301 * Continuous simulation parameters:
2302 * IaRECper=[ 4] (hrs),
2303 * SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),

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2304 * InterEventTime=[ 12](hrs)
2305 * Baseflow simulation parameters:
2306 * BaseFlowOption=[ 1] ,
2307 * InitGWResVol=[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2308 * VHydCond=[ 0.055](mm/hr) , END=- 1
2309 *%-----|-----|
2310 CONTINUOUS NASHYD NHYD=["S-1-B"], DT=[ 1]min, AREA=[ 55.36](ha),
2311 DWF=[ 0](cms) , CNVC=[ 77] , IA=[ 4.67](mm) ,
2312 N=[ 3] , TP=[ 0.451]hrs ,
2313 Continuous simulation parameters:
2314 IaRECper=[ 4](hrs) ,
2315 SMN=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2316 InterEventTime=[ 12](hrs)
2317 Baseflow simulation parameters:
2318 BaseFlowOption=[ 1] ,
2319 InitGWResVol=[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2320 VHydCond=[ 0.055](mm/hr) , END=- 1
2321 *%-----|-----|
2322 *# - JFSA 2021-02-24 change the name from S-1-BCDC to S-1-A and S-1-B. Change their
TP values based on the new areas compared to the old ones.
2323 *CONTINUOUS NASHYD NHYD=["S-1-BCDC"], DT=[ 1]min, AREA=[ 134.9](ha),
2324 * DWF=[ 0](cms) , CNVC=[ 77] , IA=[ 4.67](mm) ,
2325 * N=[ 3] , TP=[ 1.10]hrs ,
2326 * Continuous simulation parameters:
2327 * IaRECper=[ 4](hrs) ,
2328 * SMN=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2329 * InterEventTime=[ 12](hrs)
2330 * Baseflow simulation parameters:
2331 * BaseFlowOption=[ 1] ,
2332 * InitGWResVol=[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2333 * VHydCond=[ 0.055](mm/hr) , END=- 1
2334 *%-----|-----|
2335 *# - JFSA 2021-02-24 "S-1-BCDC-1" and "S-1-BCDC-2" are not existing anymore.
"S-1-BCDC-1" is part of "S-1-FO-D2" and "S-1-BCDC-2" is part of "S-1-D2" and "S-1-D3"
2336 *CONTINUOUS NASHYD NHYD=["S-1-BCDC-1"], DT=[ 1]min, AREA=[ 0.3](ha),
2337 * DWF=[ 0](cms) , CNVC=[ 77] , IA=[ 4.67](mm) ,
2338 * N=[ 3] , TP=[ 1.10]hrs ,
2339 * Continuous simulation parameters:
2340 * IaRECper=[ 4](hrs) ,
2341 * SMN=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2342 * InterEventTime=[ 12](hrs)
2343 * Baseflow simulation parameters:
2344 * BaseFlowOption=[ 1] ,
2345 * InitGWResVol=[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2346 * VHydCond=[ 0.055](mm/hr) , END=- 1
2347 *%-----|-----|
2348 *CONTINUOUS NASHYD NHYD=["S-1-BCDC-2"], DT=[ 1]min, AREA=[ 1.3](ha),
2349 * DWF=[ 0](cms) , CNVC=[ 77] , IA=[ 4.67](mm) ,
2350 * N=[ 3] , TP=[ 1.10]hrs ,
2351 * Continuous simulation parameters:
2352 * IaRECper=[ 4](hrs) ,
2353 * SMN=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2354 * InterEventTime=[ 12](hrs)
2355 * Baseflow simulation parameters:
2356 * BaseFlowOption=[ 1] ,
2357 * InitGWResVol=[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2358 * VHydCond=[ 0.055](mm/hr) , END=- 1
2359 *%-----|-----|
2360 *# - JFSA 2021-01-19, after adding Greenbank pond, "S-1-BCDC-3" is not existing
anymore
2361 *CONTINUOUS NASHYD NHYD=["S-1-BCDC-3"], DT=[ 1]min, AREA=[ 3.9](ha),
2362 * DWF=[ 0](cms) , CNVC=[ 77] , IA=[ 4.67](mm) ,
2363 * N=[ 3] , TP=[ 1.10]hrs ,
2364 * Continuous simulation parameters:
2365 * IaRECper=[ 4](hrs) ,
2366 * SMN=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,

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2367 * InterEventTime=[ 12](hrs)
2368 * Baseflow simulation parameters:
2369 * BaseFlowOption=[ 1] ,
2370 * InitGWResVol=[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2371 * VHydCond=[ 0.055](mm/hr) , END=- 1
2372 *%-----|-----
2373 * -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
before station 7245 on Jock River
2374 *CONTINUOUS STANDHYD NHYD=["S-1-Okeefe"], DT=[ 1](min) , AREA=[ 44.93](ha) , XI MP=[ 0.65] ,
TI MP=[ 0.65] , DWF=[ 0](cms) ,
2375 * LOSS=[ 2] , SCS curve number CN=[ 75] , Pervious surfaces:
I Aper=[ 4.67](mm) , SLPP=[ 2.0](%) ,
2376 * LGP=[ 40](m) , MNP=[ 0.25] , SCP=[ 0](min) , Impervious surfaces:
I Ai mp=[ 1.57](mm) , SLPI=[ 0.75](%) ,
2377 * LGI=[ 547.296](m) , MNI=[ 0.013] , SCI=[ 0](min) ,
2378 * Continuous simulation parameters:
2379 * IaRECper=[ 4](hrs) , IaRECI mp=[ 4](hrs) ,
2380 * SM N=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2381 * InterEventTime=[ 12](hrs) , END=- 1
2382 *%-----|-----
2383 *COMPUTE DUALHYD NHYDin=["S-1-Okeefe"], CI NLET=[ 4.796](cms) , NI NLET=[ 1] ,
2384 * M aj NHYD=["S-1-OkM "]
2385 * M nNHYD=["S-1-OkMN"]
2386 * TM I STO=[ 9999999](cu-m)
2387 *%-----|-----
2388 *ADD HYD NHYDs um=["S-1-OkS"] , NHYDs to add=["S-1-OkM "+"S-1-OkMN"]
2389 *%-----|-----
2390 *ROUTE RESERVOIR NHYDout=["S-1-OkSR"] , NHYDin=["S-1-OkS"] ,
2391 * RDT=[ 1](min) ,
2392 * TABLE of ( OUTFLOW STORAGE ) values
2393 * ( cms ) - ( ha-m)
2394 * [ 0.0 , 0.0 ]
2395 * [ 0.5370, 1.7917 ]
2396 * [ -1 , -1 ] (max twenty pts)
2397 * NHYDovf=["S-1-OkSovf"]
2398 *%-----|-----
2399 *CONTINUOUS NASHYD NHYD=["S-1-Okeefe"], DT=[ 1]mi n , AREA=[ 44.93](ha) ,
2400 * DWF=[ 0](cms) , CN C=[ 77] , I A=[ 4.67](mm) ,
2401 * N=[ 3] , TP=[ 1.049]hrs ,
2402 * Continuous simulation parameters:
2403 * IaRECper=[ 4](hrs) ,
2404 * SM N=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2405 * InterEventTime=[ 12](hrs)
2406 * Baseflow simulation parameters:
2407 * BaseFlowOption=[ 1] ,
2408 * InitGWResVol=[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2409 * VHydCond=[ 0.055](mm/hr) , END=- 1
2410 *%-----|-----
2411 * -JFSA 2021-02-26 "S-1-FO-DI" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2412 *CONTINUOUS STANDHYD NHYD=["S-1-FO-DI"] , DT=[ 1]mi n , AREA=[ 5.11](ha) ,
2413 * XI MP=[ 0.65] , TI MP=[ 0.65] , DWF=[ 0](cms) , LOSS=[ 2] ,
2414 * SCS curve number CN=[ 74] ,
2415 * Pervious surfaces: I Aper=[ 4.67](mm) , SLPP=[ 0.5](%) ,
2416 * LGP=[ 40](m) , MNP=[ 0.25] , SCP=[ 0](min) ,
2417 * Impervious surfaces: I Ai mp=[ 1.57](mm) , SLPI=[ 0.5](%) ,
2418 * LGI=[ 184.572](m) , MNI=[ 0.013] , SCI=[ 0](min) ,
2419 * Continuous simulation parameters:
2420 * IaRECper=[ 4](hrs) , IaRECI mp=[ 4](hrs) ,
2421 * SM N=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2422 * InterEventTime=[ 18](hrs) , END=- 1
2423 *%-----|-----
2424 *COMPUTE DUALHYD NHYDin=["S-1-FO-DI"] , CI NLET=[ 0.605](cms) , NI NLET=[ 1] ,
2425 * M aj NHYD=["S-1-FO-DI"]
2426 * M nNHYD=["S-1-FO-DI N"]
2427 * TM I STO=[ 9999999](cu-m)

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2428 *%-----|-----|
2429 *ADD HYD          NHYDs um=[ " S- 1- FO- DIS" ], NHYDs to add=[ " S- 1- FO- DIN" +" S- 1- FO- DIJ" ]
2430 *%-----|-----|
2431 *ROUTE RESERVOIR NHYDout=[ " S- 1- FO- DIR" ] , NHYDin=[ " S- 1- FO- DIS" ] ,
2432 *              RDT=[ 1 ] ( mi n ),
2433 *              TABLE of ( OUTFLOW STORAGE ) values
2434 *                  ( cms ) - ( ha- m )
2435 *                  [ 0.0      , 0.0 ]
2436 *                  [ 0.0611, 0.2038 ]
2437 *                  [   -1   ,  -1   ] (max twenty pts)
2438 *              NHYDovf=[ " S- 1FOD1ovf" ]
2439 *%-----|-----|
2440 *CONTINUOUS NASHYD NHYD=[ " S- 1- FO- DI" ], DT=[ 1 ] mi n, AREA=[ 5.11 ] ( ha ),
2441 *              DWF=[ 0 ] ( cms ), CN C=[ 77 ], IA=[ 4.67 ] ( mm ),
2442 *              N=[ 3 ], TP=[ 1.10 ] hr s,
2443 *              Continuous simulation parameters:
2444 *              IaRECper=[ 4 ] ( hr s ),
2445 *              SM N=[ - 1 ] ( mm ), SMAX=[ - 1 ] ( mm ), SK=[ 0.010 ] / ( mm ),
2446 *              InterEvent Time=[ 12 ] ( hr s )
2447 *              Baseflow simulation parameters:
2448 *              BaseFlowOption=[ 1 ] ,
2449 *              InitGWResVol=[ 50 ] ( mm ), GWResK=[ 0.96 ] ( mm/ day/ mm )
2450 *              VHydCond=[ 0.055 ] ( mm/ hr ), END=- 1
2451 *%-----|-----|
2452 * -JFSA 2021-02-26 " S- 1- FO- D2" is a part of S- 1 sub-catchment. It is moved to drain
before station 980 on Foster Drain
2453 *CONTINUOUS STANDHYD NHYD=[ " S- 1- FO- D2" ], DT=[ 1 ] mi n, AREA=[ 4.94 ] ( ha ),
2454 *              XI MP=[ 0.55 ], TI MP=[ 0.55 ], DWF=[ 0 ] ( cms ), LOSS=[ 2 ],
2455 *              SCS curve number CN=[ 74 ],
2456 *              Pervious surfaces: IAper=[ 4.67 ] ( mm ), SLPP=[ 0.5 ] ( % ),
2457 *              LGP=[ 40 ] ( m ), MNP=[ 0.25 ], SCP=[ 0 ] ( mi n ),
2458 *              Impervious surfaces: IAi mp=[ 1.57 ] ( mm ), SLPI=[ 0.5 ] ( % ),
2459 *              LGI=[ 181.475 ] ( m ), MNI=[ 0.013 ], SCI=[ 0 ] ( mi n ),
2460 *              Continuous simulation parameters:
2461 *              IaRECper=[ 4 ] ( hr s ), IaRECI mp=[ 4 ] ( hr s ),
2462 *              SM N=[ - 1 ] ( mm ), SMAX=[ - 1 ] ( mm ), SK=[ 0.010 ] / ( mm ),
2463 *              InterEvent Time=[ 18 ] ( hr s ), END=- 1
2464 *%-----|-----|
2465 *CONTINUOUS NASHYD NHYD=[ " S- 1- FO- D2" ], DT=[ 1 ] mi n, AREA=[ 4.94 ] ( ha ),
2466 *              DWF=[ 0 ] ( cms ), CN C=[ 77 ], IA=[ 4.67 ] ( mm ),
2467 *              N=[ 3 ], TP=[ 1.10 ] hr s,
2468 *              Continuous simulation parameters:
2469 *              IaRECper=[ 4 ] ( hr s ),
2470 *              SM N=[ - 1 ] ( mm ), SMAX=[ - 1 ] ( mm ), SK=[ 0.010 ] / ( mm ),
2471 *              InterEvent Time=[ 12 ] ( hr s )
2472 *              Baseflow simulation parameters:
2473 *              BaseFlowOption=[ 1 ] ,
2474 *              InitGWResVol=[ 50 ] ( mm ), GWResK=[ 0.96 ] ( mm/ day/ mm )
2475 *              VHydCond=[ 0.055 ] ( mm/ hr ), END=- 1
2476 *%-----|-----|
2477 *COMPUTE DUALHYD NHYDin=[ " S- 1- FO- D2" ], CINLET=[ 0.508 ] ( cms ), NINLET=[ 1 ],
2478 *              Mij NHYD=[ " S- 1- FO- D2J" ]
2479 *              MnNHYD=[ " S- 1- FO- D2N" ]
2480 *              TMISTO=[ 9999999 ] ( cu- m )
2481 *%-----|-----|
2482 *ADD HYD          NHYDs um=[ " S- 1- FO- D2S" ], NHYDs to add=[ " S- 1- FO- D2J" +" S- 1- FO- D2N" ]
2483 *%-----|-----|
2484 *ROUTE RESERVOIR NHYDout=[ " S- 1- FO- D2R" ] , NHYDin=[ " S- 1- FO- D2S" ] ,
2485 *              RDT=[ 1 ] ( mi n ),
2486 *              TABLE of ( OUTFLOW STORAGE ) values
2487 *                  ( cms ) - ( ha- m )
2488 *                  [ 0.0      , 0.0 ]
2489 *                  [ 0.0590, 0.1970 ]
2490 *                  [   -1   ,  -1   ] (max twenty pts)
2491 *              NHYDovf=[ " S- 1FOD2ovf" ]
2492 *%-----|-----|

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2493 * -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2494 *CONTINUOUS STANDHYD NHYD=["S-1-FO-F-D"], DT=[1]mi n, AREA=[14.96](ha),
2495 * XI MP=[0.65], TI MP=[0.65], DWF=[0](cms), LOSS=[2],
2496 * SCS curve number CN=[74],
2497 * Pervious surfaces: I A per=[4.67](mm), SLPP=[0.5](%),
2498 * LGP=[40](m), MNP=[0.25], SCP=[0](mi n),
2499 * Imper vious surfaces: I A i mp=[1.57](mm), SLPI =[0.5](%),
2500 * LGI =[315.806](m), MNI =[0.013], SCI =[0](mi n),
2501 * Continuous simulation parameters:
2502 * I a REC per =[4](hr s), I a REC i mp =[4](hr s),
2503 * SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2504 * Inter Event Ti me =[18](hr s), END=- 1
2505 *%-----|-----|
2506 *CONTINUOUS NASHYD NHYD=["S-1-FO-F-D"], DT=[1]mi n, AREA=[14.96](ha),
2507 * DWF=[0](cms), CN C=[77], I A=[4.67](mm),
2508 * N=[3], TP=[1.007]hr s,
2509 * Continuous simulation parameters:
2510 * I a REC per =[4](hr s),
2511 * SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2512 * Inter Event Ti me =[12](hr s)
2513 * Baseflow simulation parameters:
2514 * BaseFl owOpt ion=[1],
2515 * Ini t GWRes Vol =[50](mm), GWRes K=[0.96](mm/ day/ mm)
2516 * VHydCond=[0.055](mm/ hr), END=- 1
2517 *%-----|-----|
2518 *COMPUTE DUALHYD NHYD i n=["S-1-FO-F-D"], CI NLET=[1.749](cms), NI NLET=[1],
2519 * M a j NHYD=["S-1FO-F-DJ"]
2520 * M nNHYD=["S-1FO-F-DN"]
2521 * TM I STO=[9999999](cu-m)
2522 *%-----|-----|
2523 *ADD HYD NHYDs um=["S-1FO-F-DS"], NHYDs to add=["S-1FO-F-DJ"+"S-1FO-F-DN"]
2524 *%-----|-----|
2525 *ROUTE RESERVOIR NHYDout=["S-1FO-F-DR"], NHYD i n=["S-1FO-F-DS"],
2526 * RDT=[1](mi n),
2527 * TABLE of ( OUTFLOW STORAGE ) values
2528 * ( cms ) - ( ha-m)
2529 * [ 0.0 , 0.0 ]
2530 * [ 0.1788, 0.5966 ]
2531 * [ -1 , -1 ] (max twenty pts)
2532 * NHYDovf=["S-1FoFDovf"]
2533 *%-----|-----|
2534 *CONTINUOUS STANDHYD NHYD=["S-1-DI"], DT=[1](mi n), AREA=[21.67](ha), XI MP=[0.65],
TI MP=[0.65], DWF=[0](cms),
2535 * LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
I A per=[4.67](mm), SLPP=[2.0](%),
2536 * LGP=[40](m), MNP=[0.25], SCP=[0](mi n), Imper vious surfaces:
I A i mp=[1.57](mm), SLPI =[0.75](%),
2537 * LGI =[380.088](m), MNI =[0.013], SCI =[0](mi n),
2538 * Continuous simulation parameters:
2539 * I a REC per =[4](hr s), I a REC i mp =[4](hr s),
2540 * SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2541 * Inter Event Ti me =[12](hr s), END=- 1
2542 *%-----|-----|
2543 CONTINUOUS NASHYD NHYD=["S-1-DI"], DT=[1]mi n, AREA=[21.67](ha),
2544 DWF=[0](cms), CN C=[77], I A=[4.67](mm),
2545 N=[3], TP=[1.066]hr s,
2546 Continuous simulation parameters:
2547 I a REC per =[4](hr s),
2548 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2549 Inter Event Ti me =[12](hr s)
2550 Baseflow simulation parameters:
2551 BaseFl owOpt ion=[1],
2552 Ini t GWRes Vol =[50](mm), GWRes K=[0.96](mm/ day/ mm)
2553 VHydCond=[0.055](mm/ hr), END=- 1
2554 *%-----|-----|

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2614 * IaRECper=[ 4](hr s), IaRECImp=[ 4](hr s),
2615 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2616 * InterEventTime=[ 12](hr s), END=- 1
2617 *%-----|-----
2618 *CONTINUOUS NASHYD NHYD=["S-1-D3"], DT=[ 1]mi n, AREA=[ 6.79](ha),
2619 * DWF=[ 0](cms), CN C=[ 77], IA=[ 4.67](mm),
2620 * N=[ 3], TP=[ 1.281]hr s,
2621 * Continuous simulation parameters:
2622 * IaRECper=[ 4](hr s),
2623 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2624 * InterEventTime=[ 12](hr s)
2625 * Baseflow simulation parameters:
2626 * BaseFlowOption=[ 1],
2627 * InItGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2628 * VHydCond=[ 0.055](mm/hr), END=- 1
2629 *%-----|-----
2630 *COMPUTE DUALHYD NHYDin=["S-1-D3"], CINLET=[ 0.719](cms), NINLET=[ 1],
2631 * MjNHYD=["S-1-D3J"]
2632 * MnNHYD=["S-1-D3N"]
2633 * TMSTO=[ 9999999](cu-m)
2634 *%-----|-----
2635 *ADD HYD NHYDsum=["S-1-D3S"], NHYDs to add=["S-1-D3J"+"S-1-D3N"]
2636 *%-----|-----
2637 *ROUTE RESERVOIR NHYDout=["S-1-D3R"], NHYDin=["S-1-D3S"],
2638 * RDT=[ 1](mi n),
2639 * TABLE of ( OUTFLOW STORAGE ) values
2640 * ( cms ) - ( ha-m)
2641 * [ 0.0 , 0.0 ]
2642 * [ 0.0811, 0.2708 ]
2643 * [ -1 , -1 ] (max twenty pts)
2644 * NHYDovf=["S-1-D3Rovf"]
2645 *%-----|-----
2646 *CONTINUOUS STANDHYD NHYD=["S-1-D4"], DT=[ 1](mi n), AREA=[ 3.28](ha), XI MP=[ 0.65],
TI MP=[ 0.65], DWF=[ 0](cms),
2647 * LOSS=[ 2], SCS curve number CN=[ 75], Pervious surfaces:
I Aper=[ 4.67](mm), SLPP=[ 2.0](%),
2648 * LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n), Impervious surfaces:
I Ai mp=[ 1.57](mm), SLPI=[ 0.75](%),
2649 * LGI=[ 147.874](m), MNI=[ 0.013], SCI=[ 0](mi n),
2650 * Continuous simulation parameters:
2651 * IaRECper=[ 4](hr s), IaRECImp=[ 4](hr s),
2652 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2653 * InterEventTime=[ 12](hr s), END=- 1
2654 *%-----|-----
2655 CONTINUOUS NASHYD NHYD=["S-1-D4"], DT=[ 1]mi n, AREA=[ 3.28](ha),
2656 DWF=[ 0](cms), CN C=[ 77], IA=[ 4.67](mm),
2657 N=[ 3], TP=[ 1.10]hr s,
2658 Continuous simulation parameters:
2659 IaRECper=[ 4](hr s),
2660 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2661 InterEventTime=[ 12](hr s)
2662 Baseflow simulation parameters:
2663 BaseFlowOption=[ 1],
2664 InItGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2665 VHydCond=[ 0.055](mm/hr), END=- 1
2666 *%-----|-----
2667 *COMPUTE DUALHYD NHYDin=["S-1-D4"], CINLET=[ 0.373](cms), NINLET=[ 1],
2668 * MjNHYD=["S-1-D4J"]
2669 * MnNHYD=["S-1-D4N"]
2670 * TMSTO=[ 9999999](cu-m)
2671 *%-----|-----
2672 *ADD HYD NHYDsum=["S-1-D4S"], NHYDs to add=["S-1-D4J"+"S-1-D4N"]
2673 *%-----|-----
2674 *ROUTE RESERVOIR NHYDout=["S-1-D4R"], NHYDin=["S-1-D4S"],
2675 * RDT=[ 1](mi n),
2676 * TABLE of ( OUTFLOW STORAGE ) values

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2677 *                ( cms ) - ( ha - m )
2678 *                [ 0.0      , 0.0 ]
2679 *                [ 0.0392, 0.1308 ]
2680 *                [ -1      , -1      ] (max twenty pts)
2681 *                NHYDovf=[ "S-1-D4Rovf" ]
2682 *%-----|-----|
2683 *CONTINUOUS STANDHYD NHYD=[ "S-1-D5" ], DT=[ 1 ](mi n), AREA=[ 12.84 ](ha), XI MP=[ 0.65 ],
TI MP=[ 0.65 ], DWF=[ 0 ]( cms ),
2685 *                LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](mi n), Impervious surfaces:
I Ai mp=[ 1.57 ](mm), SLPI=[ 0.75 ]( % ),
2686 *                LGI=[ 292.57 ](m), MNI=[ 0.013 ], SCI=[ 0 ](mi n),
2687 *                Continuous simulation parameters:
2688 *                IaRECper=[ 4 ](hrs), IaRECI mp=[ 4 ](hrs),
2689 *                SM N=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2690 *                InterEvent Time=[ 12 ](hrs), END=- 1
2691 *%-----|-----|
2692 CONTINUOUS NASHYD NHYD=[ "S-1-D5" ], DT=[ 1 ]mi n, AREA=[ 12.84 ](ha),
2693 DWF=[ 0 ]( cms ), CNV C=[ 77 ], IA=[ 4.67 ](mm),
2694 N=[ 3 ], TP=[ 1.10 ]hrs,
2695 Continuous simulation parameters:
2696 IaRECper=[ 4 ](hrs),
2697 SM N=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2698 InterEvent Time=[ 12 ](hrs)
2699 Baseflow simulation parameters:
2700 BaseFlowOption=[ 1 ],
2701 Ini tGWRes Vol=[ 50 ](mm), GWRes K=[ 0.96 ](mm/ day/ mm)
2702 VHydCond=[ 0.055 ](mm/ hr), END=- 1
2703 *%-----|-----|
2704 *COMPUTE DUALHYD NHYDi n=[ "S-1-D5" ], CI NLET=[ 1.395 ]( cms ), NI NLET=[ 1 ],
2705 *                Mi j NHYD=[ "S-1-D5J" ]
2706 *                M nNHYD=[ "S-1-D5N" ]
2707 *                TM I STO=[ 9999999 ](cu - m)
2708 *%-----|-----|
2709 *ADD HYD NHYDs um=[ "S-1-D5S" ], NHYDs to add=[ "S-1-D5J" + "S-1-D5N" ]
2710 *%-----|-----|
2711 *ROUTE RESERVOIR NHYDout=[ "S-1-D5R" ], NHYDi n=[ "S-1-D5S" ],
2712 *                RDT=[ 1 ](mi n),
2713 *                TABLE of ( OUTFLOW STORAGE ) values
2714 *                ( cms ) - ( ha - m )
2715 *                [ 0.0      , 0.0 ]
2717 *                [ -1      , -1      ] (max twenty pts)
2718 *                NHYDovf=[ "S-1-D5Rovf" ]
2719 *%-----|-----|
2720 *CONTINUOUS STANDHYD NHYD=[ "S-1-D6" ], DT=[ 1 ](mi n), AREA=[ 1.75 ](ha), XI MP=[ 0.65 ],
TI MP=[ 0.65 ], DWF=[ 0 ]( cms ),
2721 *                LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
I Aper=[ 4.67 ](mm), SLPP=[ 2.0 ]( % ),
2722 *                LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](mi n), Impervious surfaces:
I Ai mp=[ 1.57 ](mm), SLPI=[ 0.75 ]( % ),
2723 *                LGI=[ 108.01 ](m), MNI=[ 0.013 ], SCI=[ 0 ](mi n),
2724 *                Continuous simulation parameters:
2725 *                IaRECper=[ 4 ](hrs), IaRECI mp=[ 4 ](hrs),
2726 *                SM N=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2727 *                InterEvent Time=[ 12 ](hrs), END=- 1
2728 *%-----|-----|
2729 CONTINUOUS NASHYD NHYD=[ "S-1-D6" ], DT=[ 1 ]mi n, AREA=[ 1.75 ](ha),
2730 DWF=[ 0 ]( cms ), CNV C=[ 77 ], IA=[ 4.67 ](mm),
2731 N=[ 3 ], TP=[ 1.10 ]hrs,
2732 Continuous simulation parameters:
2733 IaRECper=[ 4 ](hrs),
2734 SM N=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2735 InterEvent Time=[ 12 ](hrs)
2736 Baseflow simulation parameters:

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2737 BaseFlowOpt ion=[ 1] ,
2738 Ini t GWRes Vol =[ 50] ( mm) , GWRes K=[ 0. 96] ( mm/ day/ mm)
2739 VHydCond=[ 0. 055] ( mm/ hr) , END=- 1
2740 *%-----|-----
2741 *COMPUTE DUALHYD NHYDi n=[ "S- 1- D6" ] , CI NLET=[ 0. 218] ( cms) , NI NLET=[ 1] ,
2742 * Mj NHYD=[ "S- 1- D6J" ]
2743 * M nNHYD=[ "S- 1- D6N" ]
2744 * TMJ STO=[ 9999999] ( cu- m)
2745 *%-----|-----
2746 *ADD HYD NHYDs um=[ "S- 1- D6S" ] , NHYDs to add=[ "S- 1- D6J" +"S- 1- D6N" ]
2747 *%-----|-----
2748 *ROUTE RESERVOIR NHYDout =[ "S- 1- D6R" ] , NHYDi n=[ "S- 1- D6S" ] ,
2749 * RDT=[ 1] ( mi n) ,
2750 * TABLE of ( OUTFLOW STORAGE ) values
2751 * ( cms) - ( ha- m)
2752 * [ 0. 0 , 0. 0 ]
2753 * [ 0. 0209, 0. 0698 ]
2754 * [ -1 , -1 ] (max twenty pts)
2755 * NHYDovf=[ "S- 1- D6Rovf" ]
2756 *%-----|-----
2757 *CONTINUOUS STANDHYD NHYD=[ "S- 1- D7" ] , DT=[ 1] ( mi n) , AREA=[ 2. 03] ( ha) , XI MP=[ 0. 65] ,
TI MP=[ 0. 65] , DWF=[ 0] ( cms) ,
2758 * LOSS=[ 2] , SCS curve number CN=[ 75] , Pervious surfaces:
IAper=[ 4. 67] ( mm) , SLPP=[ 2. 0] ( % ) ,

2760 * LGI=[ 116. 33] ( m) , MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
2761 * Continuous simulation parameters:
2762 * IaRECper=[ 4] ( hr s) , IaRECI mp=[ 4] ( hr s) ,
2763 * SMN=[ -1] ( mm) , SMAX=[ -1] ( mm) , SK=[ 0. 010] / ( mm) ,
2764 * InterEvent Ti me=[ 12] ( hr s) , END=- 1
2765 *%-----|-----
2766 CONTINUOUS NASHYD NHYD=[ "S- 1- D7" ] , DT=[ 1] mi n , AREA=[ 2. 03] ( ha) ,
2767 DWF=[ 0] ( cms) , CN C=[ 77] , IA=[ 4. 67] ( mm) ,
2768 N=[ 3] , TP=[ 1. 10] hr s ,
2769 Continuous simulation parameters:
2770 IaRECper=[ 4] ( hr s) ,
2771 SMN=[ -1] ( mm) , SMAX=[ -1] ( mm) , SK=[ 0. 010] / ( mm) ,
2772 InterEvent Ti me=[ 12] ( hr s)
2773 Baseflow simulation parameters:
2774 BaseFlowOpt ion=[ 1] ,
2775 Ini t GWRes Vol =[ 50] ( mm) , GWRes K=[ 0. 96] ( mm/ day/ mm)
2776 VHydCond=[ 0. 055] ( mm/ hr) , END=- 1
2777 *%-----|-----
2778 *COMPUTE DUALHYD NHYDi n=[ "S- 1- D7" ] , CI NLET=[ 2. 279] ( cms) , NI NLET=[ 1] ,
2779 * Mj NHYD=[ "S- 1- D7J" ]
2780 * M nNHYD=[ "S- 1- D7N" ]
2781 * TMJ STO=[ 9999999] ( cu- m)
2782 *%-----|-----
2783 *ADD HYD NHYDs um=[ "S- 1- D7S" ] , NHYDs to add=[ "S- 1- D7J" +"S- 1- D7N" ]
2784 *%-----|-----
2785 *ROUTE RESERVOIR NHYDout =[ "S- 1- D7R" ] , NHYDi n=[ "S- 1- D7S" ] ,
2786 * RDT=[ 1] ( mi n) ,
2787 * TABLE of ( OUTFLOW STORAGE ) values
2788 * ( cms) - ( ha- m)
2789 * [ 0. 0 , 0. 0 ]
2790 * [ 0. 0243, 0. 0810 ]
2791 * [ -1 , -1 ] (max twenty pts)
2792 * NHYDovf=[ "S- 1- D8Rovf" ]
2793 *%-----|-----
2794 * -JFSA 2021-02-26 "S-1-D8" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2795 *CONTINUOUS STANDHYD NHYD=[ "S- 1- D8" ] , DT=[ 1] ( mi n) , AREA=[ 5. 27] ( ha) , XI MP=[ 0. 65] ,
TI MP=[ 0. 65] , DWF=[ 0] ( cms) ,
2796 * LOSS=[ 2] , SCS curve number CN=[ 75] , Pervious surfaces:
IAper=[ 4. 67] ( mm) , SLPP=[ 2. 0] ( % ) ,

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2797 *                LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min), Impervious surfaces:
I Ai mp=[ 1.57](mm), SLPI=[ 0.75](%),
2798 *                LGI=[ 187.439](m), MNI=[ 0.013], SCI=[ 0](min),
2799 *                Continuous simulation parameters:
2800 *                IaRECPper=[ 4](hrs), IaRECImp=[ 4](hrs),
2801 *                SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2802 *                InterEventTime=[ 12](hrs), END=- 1
2803 *%-----|-----
2804 *CONTINUOUS NASHYD NHYD=[ "S-1-D8"], DT=[ 1]min, AREA=[ 5.27](ha),
2805 *                DWF=[ 0](cms), CN/C=[ 77], IA=[ 4.67](mm),
2806 *                N=[ 3], TP=[ 1.10]hrs,
2807 *                Continuous simulation parameters:
2808 *                IaRECPper=[ 4](hrs),
2809 *                SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2810 *                InterEventTime=[ 12](hrs)
2811 *                Baseflow simulation parameters:
2812 *                BaseFlowOption=[ 1],
2813 *                InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2814 *                VHydCond=[ 0.055](mm/hr), END=- 1
2815 *%-----|-----
2816 *COMPUTE DUALHYD NHYDin=[ "S-1-D8"], CINLET=[ 2.279](cms), NI NLET=[ 1],
2817 *                Mij NHYD=[ "S-1-D8J"]
2818 *                MnNHYD=[ "S-1-D8N"]
2819 *                TMI STO=[ 9999999](cu-m)
2820 *%-----|-----
2821 *ADD HYD NHYDs um=[ "S-1-D8S"], NHYDs to add=[ "S-1-D8J"+"S-1-D8N"]
2822 *%-----|-----
2823 *ADD HYD NHYDs um=[ "S-1-D"], NHYDs to add=[ "S-1-Okeefe"+"S-1"+"S-1-Fost"]
2824 *%-----|-----
2825 *COMPUTE DUALHYD NHYDin=[ "S-1-D"], CINLET=[ 11.616](cms), NI NLET=[ 1],
2826 *                Mij NHYD=[ "S-1-D-M"]
2827 *                MnNHYD=[ "S-1-D-MN"]
2828 *                TMI STO=[ 5974](cu-m)
2829 *%-----|-----
2830 *ADD HYD NHYDs um=[ "S-1-DEV"], NHYDs to add=[ "S-1-D-M"+"S-1-D-MN"]
2831 *%-----|-----
2832 *ROUTE RESERVOIR NHYDout=[ "S-1-D8R"], NHYDin=[ "S-1-D8S"],
2833 *                RDT=[ 1](min),
2834 *                TABLE of ( OUTFLOW STORAGE ) values
2835 *                (cms) - (ha-m)
2836 *                [ 0.0, 0.0 ]
2837 *                [ 0.0630, 0.2102 ]
2838 *                [ -1, -1 ] (max twenty pts)
2839 *                NHYDovf=[ "S-1-D8Rovf"]
2840 *%-----|-----
2841 *%-----|-----
2842 *                -JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
(W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
2843 *# Catchment W_CLAR
2844 *# - To West Clarke Drain (south of the Jock)
2845 *# - Subdivision with 43% imp. as per Barrhaven South MS
2846 *# - 2020-11-30 update CLARKE Tributary Drainage Area to = 121 ha based on
P598(04)-11
2847 *# - 2020-11-30 split CLARKE Drainage Area to MAJOR and ALL
2848 *#*****
2849 CONTINUOUS STANDHYD NHYD=[ "W_CLAR_M"], DT=[ 1]min, AREA=[ 1.772](ha),
2850 *                XI MP=[ 0.46], TI MP=[ 0.59], DWF=[ 0](cms), LOSS=[ 2],
2851 *                SCS curve number CN=[ 77],
2852 *                Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
2853 *                LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
2854 *                Impervious surfaces: I Ai mp=[ 1.57](mm), SLPI=[ 1](%),
2855 *                LGI=[ 109](m), MNI=[ 0.013], SCI=[ 0](min),
2856 *                Continuous simulation parameters:
2857 *                IaRECPper=[ 4](hrs), IaRECImp=[ 4](hrs),
2858 *                SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2859 *                InterEventTime=[ 18](hrs), END=- 1

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2860 *%-----|-----|
2861 *COMPUTE DUALHYD      NHYDin=["W_CLAR_M"],  CILET=[ 0.213](cms),  NILET=[ 1],
2862 *                      MjNHYD=["W_CLAR_Mj"]
2863 *                      MnNHYD=["W_CLAR_Mn"]
2864 *                      TMSTO=[ 0.1](cu-m)
2865 *%-----|-----|
2866 *# 5-Year + 12% Capture
2867 ROUTE RESERVOIR      NHYDout=["W_CLAR_Mn"],  NHYDin=["W_CLAR_M"],
2868                      RDT=[ 1](min),
2869                      TABLE of ( OUTFLOW STORAGE ) values
2870                      (cms) - (ha-m)
2871                      [ 0.0      , 0.0 ]
2872                      [ 0.213 , 0.0001 ]
2873                      [ -1      , -1      ] (max twenty pts)
2874                      NHYDovf=["W_CLAR_Mj"],
2875 *%-----|-----|
2876 *      -Clarke_All area from P 598(04)-11 = 120.207 ha, change to 127.298 ha based on
GIS measurements,
2877 *      -JFSA, 2021-01-19 update W_CLAR_ALL to (121.17-1.772=119.398) ha based on GIS
measurements W_CLAR is 121.17 ha and W_CLAR_M is 1.772 ha
2878 CONTINUOUS STANDHYD NHYD=["W_CLAR_ALL"],  DT=[ 1]min,  AREA=[ 119.398](ha),
2879                      XI MP=[ 0.60],  TI MP=[ 0.65],  DWF=[ 0](cms),  LOSS=[ 2],
2880                      SCS curve number CN=[ 77],
2881                      Pervious surfaces: IAper=[ 4.67](mm),  SLPP=[ 1](%),
2882                      LGP=[ 40](m),  MNP=[ 0.25],  SCP=[ 0](min),
2883                      Impervious surfaces: IAimp=[ 1.57](mm),  SLPI=[ 1](%),
2884                      LGI=[ 892.18](m),  MNI=[ 0.013],  SCI=[ 0](min),
2885                      Continuous simulation parameters:
2886                      IaREcper=[ 4](hrs),  IaREcimp=[ 4](hrs),
2887                      SMN=[ -1](mm),  SMAX=[ -1](mm),  SK=[ 0.010]/(mm),
2888                      InterEventTime=[ 18](hrs),  END=-1
2889 *%-----|-----|
2890 ADD HYD              NHYDsum=["W_CLAR"],  NHYDs to add=["W_CLAR_ALL"+"W_CLAR_Mj"]
2891 *%-----|-----|
2892 SAVE HYD            NHYD=["W_CLAR"],  # OF PCYCLES=[ -1],  ICASEsh=[ 1]
2893                      HYD_COMMENT=["Total Flows to West Clarke"]
2894 *#*****
2895 *#      West Clarke Pond 2
2896 *#      - Rating curve obtained from Barrhaven South M&S modeling
2897 *#      - Tributary Drainage Area to M&S Pond 2 = 241 ha
2898 *#*****
2899 ROUTE RESERVOIR      NHYDout=["MS_P2"],  NHYDin=["W_CLAR"],
2900                      RDT=[ 1](min),
2901                      TABLE of ( OUTFLOW STORAGE ) values
2902                      (cms) - (ha-m)
2903                      [ 0.0      , 0.0 ]
2904                      [ 0.128 , 0.161 ]
2905                      [ 0.138 , 0.409 ]
2906                      [ 0.148 , 0.68 ]
2907                      [ 0.227 , 0.931 ]
2908                      [ 0.354 , 1.223 ]
2909                      [ 0.505 , 1.52 ]
2910                      [ 0.666 , 1.821 ]
2911                      [ 0.831 , 2.123 ]
2912                      [ 0.995 , 2.434 ]
2913                      [ 1.069 , 2.583 ]
2914                      [ 1.51  , 2.647 ]
2915                      [ 4.904 , 2.861 ]
2916                      [ 13.048 , 3.188 ]
2917                      [ 23.745 , 3.523 ]
2918                      [ 36.474 , 3.871 ]
2919                      [ 45.938 , 4.127 ]
2920                      [ 61.652 , 4.539 ]
2921                      [ -1      , -1      ] (max twenty pts)
2922                      NHYDovf=["P2-OVF"]
2923 *%-----|-----|

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2924 *#*****
2925 * -JFSA 2021-01-22 "W_CLAR_UNDE" (west of Clarke sub-catchment) discharges
directly to the jock river through a road side ditch on the west side of Borrisokane
road (station 6016)
2926 *CONTINUOUS NASHYD NHYD=["W_CLAR_UNDE"], DT=[1] min, AREA=[35.65](ha),
2927 * DWF=[0](cms), CNVC=[77], IA=[4.67](mm),
2928 * N=[3], TP=[1.10]hrs,
2929 * Continuous simulation parameters:
2930 * IaRECper=[4](hrs),
2931 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2932 * InterEventTime=[12](hrs)
2933 * Baseflow simulation parameters:
2934 * BaseFlowOption=[1],
2935 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2936 * VHydCond=[0.055](mm/hr), END=-1
2937 *%-----|-----
2938 ADD HYD NHYDsum=["SN_CE"], NHYDs to add=["N_CE"+
2939 +"S-1-D4"+"S-1-D5"+"MS_P2"+"P2-OVF"]
2940 *%-----|-----
2941 SAVE HYD NHYD=["SN_CE"], # OF PCYCLES=[-1], ICASEsh=[1]
2942 HYD_COMMENT=["Total Flows before Station 5737 on Jock River"]
2943 *%-----|-----
2944 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5737
2945 *# JFSA 2021-02-25 add station 5737 before station 5002. Station 5737 was extracted
from the HEC-RAS model
T:\PROJ\1474-16\Design\20201026-QuantityControlAnalysis\HEC-RAS\JockLidar2005
2946 *# JFSA 2021-03-02 change the slope to 0.1% instead of 0.0175 to stabilize the model
2947 ROUTE CHANNEL NHYDout=["5737"], NHYDin=["SN_CE"],
2948 RDT=[1](min),
2949 CHLGTH=[270](m), CHSLOPE=[0.0175](%),
2950 FPSLOPE=[0.0175](%),
2951 SECNUM=[1.0], NSEG=[3]
2952 (SEGROUGH, SEGDI ST (m))=
2953 [0.050, -24.04
2954 -0.035, 23.92
2955 0.050, 1130.8] NSEG times
2956 (DISTANCE (m), ELEVATION (m))=
2957 [-1060.52, 94]
2958 [-268.6, 91.5]
2959 [-259.43, 91.5]
2960 [-179.48, 91.5]
2961 [-67.9, 91.5]
2962 [-59.21, 91.5]
2963 [-33.19, 91]
2964 [-26.08, 90.5]
2965 [-24.04, 90]
2966 [-13.14, 86.77]
2967 [0, 85]
2968 [14.68, 86.74]
2969 [23.92, 90]
2970 [25.78, 90.5]
2971 [31.91, 91]
2972 [91.95, 91.5]
2973 [772.15, 92]
2974 [961.49, 92.5]
2975 [1044.69, 93]
2976 [1130.8, 95]
2977 *%-----|-----
2978 ADD HYD NHYDsum=["5002"], NHYDs to add=["5737"+
2979 +"S-1-D1"+"S-1-D6"+"S-1-D7"]
2980 *%-----|-----
2981 SAVE HYD NHYD=["5002"], # OF PCYCLES=[-1], ICASEsh=[1]
2982 HYD_COMMENT=["Total Flows before Station 5002 on Jock River"]
2983 *%-----|-----
2984 *# Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain
2985 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5002

```


2986 *# JFSA 2021-02-19 Change the slope from 0.01 % (as per Stantec Report 2007) to 0.0255
 % so the model will be more stable and give reasonable results. It is justifiable as
 ROUTE CHANNELs aren't well suited to really flat slopes.
 2987 *# JFSA 2021-02-19 Change to three ROUTE CHANNEL with length 275 m each instead of one
 with 825 m length so the model will be more stable
 2988 *# JFSA 2021-02-26 change the length of 5002 route channel from 825 m to 736 m That is
 because of adding station 5737 between station 6016 and station 5002. Then the length
 from station 5737 to station 5002 is 736 m Change the slope from 0.0255 % to 0.09511 %

2989 *
 2990 ROUTE CHANNEL NHYDout=["N_WCa"] , NHYDin=["5002"] ,
 2991 RDT=[1] (mi n) ,
 2992 CHLGTH=[245.33333] (m) , CHSLOPE=[0.09511] (%) ,
 2993 FPSLOPE=[0.09511] (%) ,
 2994 SECNUM=[1.0] , NSEG=[3]
 2995 (SEGROUGH, SEGDI ST (m)) =
 2996 [0.050, -37.5
 2997 -0.035, 37.50
 2998 0.050, 157.05] NSEG t i m e s
 2999 (DI STANCE (m) , ELEVATI ON (m)) =
 3000 [-601.81, 91.5]
 3001 [-37.50, 90.00]
 3002 [-19.61, 87.04]
 3003 [0.00, 85.70]
 3004 [14.87, 86.93]
 3005 [37.50, 90.00]
 3006 [38.54, 90.50]
 3007 [42.23, 91]
 3008 [157.05, 91.50]
 3009 * [161.44, 91.50]
 3010 * [236.48, 93.00]
 3011 * [385.47, 92.50]
 3012 * [390.78, 92.50]

3013 *%-----|
 3014 ROUTE CHANNEL NHYDout=["N_WCb"] , NHYDin=["N_WCa"] ,
 3015 RDT=[1] (mi n) ,
 3016 CHLGTH=[245.33333] (m) , CHSLOPE=[0.09511] (%) ,
 3017 FPSLOPE=[0.09511] (%) ,
 3018 SECNUM=[1.0] , NSEG=[3]
 3019 (SEGROUGH, SEGDI ST (m)) =
 3020 [0.050, -37.5
 3021 -0.035, 37.50
 3022 0.050, 157.05] NSEG t i m e s
 3023 (DI STANCE (m) , ELEVATI ON (m)) =
 3024 [-601.81, 91.5]
 3025 [-37.50, 90.00]
 3026 [-19.61, 87.04]
 3027 [0.00, 85.70]
 3028 [14.87, 86.93]
 3029 [37.50, 90.00]
 3030 [38.54, 90.50]
 3031 [42.23, 91]
 3032 [157.05, 91.50]

3033 *%-----|
 3034 ROUTE CHANNEL NHYDout=["N_WC"] , NHYDin=["N_WCb"] ,
 3035 RDT=[1] (mi n) ,
 3036 CHLGTH=[245.33333] (m) , CHSLOPE=[0.09511] (%) ,
 3037 FPSLOPE=[0.09511] (%) ,
 3038 SECNUM=[1.0] , NSEG=[3]
 3039 (SEGROUGH, SEGDI ST (m)) =
 3040 [0.050, -37.5
 3041 -0.035, 37.50
 3042 0.050, 157.05] NSEG t i m e s
 3043 (DI STANCE (m) , ELEVATI ON (m)) =
 3044 [-601.81, 91.5]
 3045 [-37.50, 90.00]
 3046 [-19.61, 87.04]

```

3047 [ 0.00, 85.70]
3048 [ 14.87, 86.93]
3049 [ 37.50, 90.00]
3050 [ 38.54, 90.50]
3051 [ 42.23, 91]
3052 [ 157.05, 91.50]
3053 *#*****
3054 * -JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
(W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
3055 *ADD HYD NHYDs um=["SN_WC"], NHYDs to
add=["MS_P2"+"P2-OVF"+"N_WC"+"W_CLAR_UNDE"]
3056 *%-----|-----|
3057 *SAVE HYD NHYD=["SN_WC"], # OF PCYCLES=[-1], ICASEsh=[1]
3058 * HYD_COMMENT=["Total Flows at West Clarke Pond Outlet"]
3059 *%-----|-----|
3060 *# Hydrograph from Node West Clarke routed to Node at Kennedy - Burnett Drain
3061 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4534
3062 *#
3063 ROUTE CHANNEL NHYDout=["N_KB"], NHYDin=["N_WC"],
3064 RDT=[1](min),
3065 CHLGTH=[1020](m), CHSLOPE=[0.0498](%),
3066 FPSLOPE=[0.0498](%),
3067 SECNUM=[1.0], NSEG=[3]
3068 ( SEGROUGH, SEGDI ST (m))=
3069 [0.050, -23.63
3070 -0.035, 23.63
3071 0.050, 728.3] NSEG times
3072 ( DISTANCE (m), ELEVATION (m))=
3073 [-1082.01, 94]
3074 [-1028.17, 92.5]
3075 [-992.3, 93.5]
3076 [-279.34, 90]
3077 [-23.63, 90]
3078 [-13.45, 87.13]
3079 [-0.07, 86.24]
3080 [10.54, 87.15]
3081 [23.63, 90]
3082 [24.86, 90.5]
3083 [26.72, 91]
3084 [45.07, 91.5]
3085 [128.17, 91.5]
3086 [270.7, 92.5]
3087 [728.3, 95]
3088 *%-----|-----|
3089 *#*****
3090 *# Catchment KEN_BU
3091 *# - To Kennedy-Burnett SWM Facility
3092 *# - Outlets to Fraser-Clarke drain (north of the Jock)
3093 *# - Medium density residential subdivision
3094 * - Add Kennedy Burnett model (Convert PCSWMM from NOVATECH June, 2020 to SWWHYMD)
3095 *#*****
3096 *CONTINUOUS STANDHYD NHYD=["KEN_BU"], DT=[1]min, AREA=[281](ha),
3097 * XI MP=[0.55], TI MP=[0.55], DWF=[0](cms), LOSS=[2],
3098 * SCS curve number CN=[71],
3099 * Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
3100 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3101 * Impervious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
3102 * LGI=[1369](m), MNI=[0.013], SCI=[0](min),
3103 * Continuous simulation parameters:
3104 * I a REC per=[4](hrs), I a REC i mp=[4](hrs),
3105 * SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3106 * Inter Event Time=[18](hrs), END=-1
3107 *%-----|-----|
3108 *#*****
3109 *# Existing Kennedy-Burnett SWM Facility
3110 *# - Rating curve obtained from URTKBP

```

```

3111 *# - Tributary Drainage Area to Pond = 160 ha
3112 *#*****
3113 *ROUTE RESERVOIR NHYDout=[ "KEN_P"], NHYDin=[ "KEN_BU"],
3114 * RDT=[ 1](mi n),
3115 * TABLE of ( OUTFLOW STORAGE ) values
3116 * (cms) - (ha-m)
3117 * [ 0.0 , 0.0 ]
3118 * [ 0.13 , 0.26]
3119 * [ 0.43 , 0.56]
3120 * [ 0.67 , 0.90]
3121 * [ 0.86 , 1.32]
3122 * [ 1.01 , 1.79]
3123 * [ 1.15 , 2.33]
3124 * [ -1 , -1 ] (max twenty pts)
3125 * NHYDovf=[ "KEN-OV" ]
3126 *%-----|-----
3127 * -JFSA, 2021-01-19 update all KEN_BU areas based on GIS measurements
3128 CONTINUOUS STANDHYD NHYD=[ "KB-01A"], DT=[ 1]mi n, AREA=[ 40.82](ha), XI MP=[ 0.097],
3129 T I M P=[ 0.4], DWF=[ 0](cms), LOSS=[ 1]:
3129 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3130 F=[ 0.00](mm),
3130 Pervious areas: I A p e r=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 40](m),
3131 M N P=[ 0.250], S C P=[ 0](mi n),
3131 Impervious areas: I A i m p=[ 0.785](mm), SLPI=[ 0.5](%),
3132 L G I=[ 521.664](m), M N I=[ 0.013], S C I=[ 0](mi n),
3132 Continuous simulation parameters:
3133 I a R E C p e r=[ 4](hrs), I a R E C i m p=[ 4](hrs), I n t e r E v e n t T i m e=[ 12](hrs),
3133 E N D=- 1
3134 *%-----|-----
3135 COMPUTE DUALHYD NHYDin=[ "KB-01A"], CI NLET=[ 3.6](cms), NI NLET=[ 1],
3136 M a j N H Y D=[ "KB-01A-M"]
3137 M n N H Y D=[ "KB-01A-MN"]
3138 T M S T O=[ 4995](cu-m)
3139 *%-----|-----
3140 ADD HYD NHYDs um=[ "KB-01A-S"], NHYDs t o a d d=[ "KB-01A-M"+"KB-01A-MN"]
3141 *%-----|-----
3142 CONTINUOUS STANDHYD NHYD=[ "KB-01B"], DT=[ 1]mi n, AREA=[ 31.1](ha), XI MP=[ 0.1875],
3143 T I M P=[ 0.375], DWF=[ 0](cms), LOSS=[ 1]:
3143 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3144 F=[ 0.00](mm),
3144 Pervious areas: I A p e r=[ 4.67](mm), SLPP=[ 0.42](%), LGP=[ 40](m),
3145 M N P=[ 0.250], S C P=[ 0](mi n),
3145 Impervious areas: I A i m p=[ 0.785](mm), SLPI=[ 0.42](%),
3146 L G I=[ 455.339](m), M N I=[ 0.013], S C I=[ 0](mi n),
3146 Continuous simulation parameters:
3147 I a R E C p e r=[ 4](hrs), I a R E C i m p=[ 4](hrs), I n t e r E v e n t T i m e=[ 12](hrs),
3147 E N D=- 1
3148 *%-----|-----
3149 COMPUTE DUALHYD NHYDin=[ "KB-01B"], CI NLET=[ 1.585](cms), NI NLET=[ 1],
3150 M a j N H Y D=[ "KB-01B-M"]
3151 M n N H Y D=[ "KB-01B-MN"]
3152 T M S T O=[ 6075](cu-m)
3153 *%-----|-----
3154 ADD HYD NHYDs um=[ "KB-01B-S"], NHYDs t o a d d=[ "KB-01B-M"+"KB-01B-MN"]
3155 *%-----|-----
3156 CONTINUOUS STANDHYD NHYD=[ "KB-01C"], DT=[ 1]mi n, AREA=[ 13.78](ha), XI MP=[ 0.2045],
3157 T I M P=[ 0.409], DWF=[ 0](cms), LOSS=[ 1]:
3157 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3158 F=[ 0.00](mm),
3158 Pervious areas: I A p e r=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3159 M N P=[ 0.250], S C P=[ 0](mi n),
3159 Impervious areas: I A i m p=[ 0.785](mm), SLPI=[ 0.5](%),
3160 L G I=[ 303.095](m), M N I=[ 0.013], S C I=[ 0](mi n),
3160 Continuous simulation parameters:
3161 I a R E C p e r=[ 4](hrs), I a R E C i m p=[ 4](hrs), I n t e r E v e n t T i m e=[ 12](hrs),
3161 E N D=- 1

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```

3162 *%-----|-----|
3163 COMPUTE DUALHYD NHYDin=["KB-01C"], CILET=[1.35](cms), NILET=[1],
3164 Maj NHYD=["KB-01C-M"]
3165 MnNHYD=["KB-01C-MN"]
3166 TMSTO=[1880](cu-m)
3167 *%-----|-----|
3168 ADD HYD NHYDsum=["KB-01C-S"], NHYDs to add=["KB-01C-M"+"KB-01C-MN"]
3169 *%-----|-----|
3170 CONTINUOUS STANDHYD NHYD=["KB-03"], DT=[1]min, AREA=[84.78](ha), XI MP=[0.197],
TI MP=[0.394], DWF=[0](cms), LOSS=[1]:
3171 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3172 Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3173 Impervious areas: I A i mp=[0.785](mm), SLPI=[0.63](%),
LGI=[751.798](m), MNI=[0.013], SCI=[0](min),
3174 Continuous simulation parameters:
3175 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
3176 *%-----|-----|
3177 COMPUTE DUALHYD NHYDin=["KB-03"], CILET=[5.27](cms), NILET=[1],
3178 Maj NHYD=["KB-03-M"]
3179 MnNHYD=["KB-03-MN"]
3180 TMSTO=[15500](cu-m)
3181 *%-----|-----|
3182 ADD HYD NHYDsum=["KB-03-S"], NHYDs to add=["KB-03-M"+"KB-03-MN"]
3183 *%-----|-----|
3184 CONTINUOUS STANDHYD NHYD=["KB-04"], DT=[1]min, AREA=[6.95](ha), XI MP=[0.85],
TI MP=[0.85], DWF=[0](cms), LOSS=[1]:
3185 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3186 Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3187 Impervious areas: I A i mp=[0.942](mm), SLPI=[0.5](%),
LGI=[215.252](m), MNI=[0.013], SCI=[0](min),
3188 Continuous simulation parameters:
3189 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
3190 *%-----|-----|
3191 COMPUTE DUALHYD NHYDin=["KB-04"], CILET=[0.503](cms), NILET=[1],
3192 Maj NHYD=["KB-04-M"]
3193 MnNHYD=["KB-04-MN"]
3194 TMSTO=[1972](cu-m)
3195 *%-----|-----|
3196 ADD HYD NHYDsum=["KB-04-S"], NHYDs to add=["KB-04-M"+"KB-04-MN"]
3197 *%-----|-----|
3198 CONTINUOUS STANDHYD NHYD=["KB-05"], DT=[1]min, AREA=[5.19](ha), XI MP=[0.93],
TI MP=[0.93], DWF=[0](cms), LOSS=[1]:
3199 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3200 Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3201 Impervious areas: I A i mp=[1.57](mm), SLPI=[0.5](%),
LGI=[186.011](m), MNI=[0.013], SCI=[0](min),
3202 Continuous simulation parameters:
3203 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
3204 *%-----|-----|
3205 *%-----|-----|
3206 CONTINUOUS STANDHYD NHYD=["KB-06"], DT=[1]min, AREA=[12.93](ha), XI MP=[0.873],
TI MP=[0.873], DWF=[0](cms), LOSS=[1]:
3207 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3208 Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3209 Impervious areas: I A i mp=[0.942](mm), SLPI=[4.75](%),

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3210          LGI=[ 293.598](m), MNI=[ 0.013], SCI=[ 0](min),
3211          Continuous simulation parameters:
3212          I aRECper=[ 4](hrs), I aRECI mp=[ 4](hrs), I nterEventTime=[ 12](hrs),
          END=- 1
3212  *%-----|-----|
3213  COMPUTE DUALHYD  NHYDin=["KB-06"], CINLET=[ 2.262](cms), NINLET=[ 1],
3214                   MajNHYD=["KB-06-M"]
3215                   MnNHYD=["KB-06-MN"]
3216                   TMSTO=[ 1950](cu-m)
3217  *%-----|-----|
3218  ADD HYD          NHYDs um=["KB-06-S"], NHYDs to add=["KB-06-M"+"KB-06-MN"]
3219  *%-----|-----|
3220  CONTINUOUS STANDHYD  NHYD=["KB-11"], DT=[ 1]min, AREA=[ 4.03](ha), XI MP=[ 0.675],
          TIMP=[ 0.675], DWF=[ 0](cms), LOSS=[ 1]:
3221          Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
          F=[ 0.00](mm),
3222          Pervious areas: I Aper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
          MNP=[ 0.250], SCP=[ 0](min),
3223          Impervious areas: I Ai mp=[ 0.785](mm), SLPI=[ 2.0](%),
          LGI=[ 163.911](m), MNI=[ 0.013], SCI=[ 0](min),
3224          Continuous simulation parameters:
3225          I aRECper=[ 4](hrs), I aRECI mp=[ 4](hrs), I nterEventTime=[ 12](hrs),
          END=- 1
3226  *%-----|-----|
3227  COMPUTE DUALHYD  NHYDin=["KB-11"], CINLET=[ 0.5773](cms), NINLET=[ 1],
3228                   MajNHYD=["KB-11-M"]
3229                   MnNHYD=["KB-11-MN"]
3230                   TMSTO=[ 597](cu-m)
3231  *%-----|-----|
3232  ADD HYD          NHYDs um=["KB-11-S"], NHYDs to add=["KB-11-M"+"KB-11-MN"]
3233  *%-----|-----|
3234  CONTINUOUS STANDHYD  NHYD=["S1"], DT=[ 1]min, AREA=[ 4.99](ha), XI MP=[ 0.93], TIMP=[ 0.93],
          DWF=[ 0](cms), LOSS=[ 1]:
3235          Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
          F=[ 0.00](mm),
3236          Pervious areas: I Aper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
          MNP=[ 0.250], SCP=[ 0](min),
3237          Impervious areas: I Ai mp=[ 1.57](mm), SLPI=[ 2.0](%),
          LGI=[ 182.392](m), MNI=[ 0.013], SCI=[ 0](min),
3238          Continuous simulation parameters:
3239          I aRECper=[ 4](hrs), I aRECI mp=[ 4](hrs), I nterEventTime=[ 12](hrs),
          END=- 1
3240  *%-----|-----|
3241  CONTINUOUS STANDHYD  NHYD=["KB-15"], DT=[ 1]min, AREA=[ 2.15](ha), XI MP=[ 0.79],
          TIMP=[ 0.79], DWF=[ 0](cms), LOSS=[ 1]:
3242          Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
          F=[ 0.00](mm),
3243          Pervious areas: I Aper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
          MNP=[ 0.250], SCP=[ 0](min),
3244          Impervious areas: I Ai mp=[ 0.157](mm), SLPI=[ 0.3](%),
          LGI=[ 119.722](m), MNI=[ 0.013], SCI=[ 0](min),
3245          Continuous simulation parameters:
3246          I aRECper=[ 4](hrs), I aRECI mp=[ 4](hrs), I nterEventTime=[ 12](hrs),
          END=- 1
3247  *%-----|-----|
3248  *%-----|-----|
3249  ADD HYD          NHYDs um=["KB-P1"], NHYDs to
          add=["KB-01A-S"+"KB-01B-S"+"KB-01C-S"+"KB-03-S"+"KB-04-S"+"KB-05"+"KB-06-S"+"KB-11-S"+"KB
          -15"+"S1"]
3250  *%-----|-----|
3251  ROUTE RESERVOIR  NHYDout=["KB-P1R"], NHYDin=["KB-P1"],
3252                   RDT=[ 1](min),
3253                   TABLE of ( OUTFLOW STORAGE ) values
3254                   ( cms ) - ( ha-m)
3255                   [ 0.0 , 0.0 ]
3256                   [ 0.076, 0.003 ]

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```

3257 [ 0.088, 0.006]
3258 [ 0.136, 0.011]
3259 [ 0.301, 0.017]
3260 [ 0.454, 0.027]
3261 [ 0.631, 0.041]
3262 [ 1.173, 0.068]
3263 [ 1.91, 0.111]
3264 [ 4.847, 0.231]
3265 [ 9.813, 0.436]
3266 [ 12.134, 0.617]
3267 [ 12.438, 0.732]
3268 [ 12.424, 0.811]
3269 [ 12.425, 0.894]
3270 [ -1 , -1 ] (max twenty pts)
3271 NHYDovf=["KB- P1ovf"]
3272 *%-----|-----|
3273 ADD HYD NHYDsum=["KB- Pond1"], NHYDs to add=["KB- P1R"+"KB- P1ovf"]
3274 *%-----|-----|
3275 SAVE HYD NHYD=["KB- Pond1"], # OF PCYCLES=[- 1], ICASEsh=[ 1]
3276 HYD_COMMENT=["Total Flows at KB first pond"]
3277 *%-----|-----|
3278 CONTINUOUS STANDHYD NHYD=["KB- 07"], DT=[ 1]mi n, AREA=[ 10.86](ha), XI MP=[ 0.86],
TI MP=[ 0.86], DWF=[ 0](c ms), LOSS=[ 1]:
3279 Hort on: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
F=[ 0.00](mm),
3280 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
MNP=[ 0.250], SCP=[ 0](mi n),
3281 Impervious areas: IAi mp=[ 0.785](mm), SLPI=[ 2.0](%),
LGI=[ 269.072](m), MNI=[ 0.013], SCI=[ 0](mi n),
3282 Continuous simulation parameters:
3283 IaREcper=[ 4](hrs), IaRECi mp=[ 4](hrs), InterEvent Ti me=[ 12](hrs),
END=- 1
3284 *%-----|-----|
3285 COMPUTE DUALHYD NHYDi n=["KB- 07"], CI NLET=[ 2.094](c ms), NI NLET=[ 1],
3286 Mij NHYD=["KB- 07- M"]
3287 MnNHYD=["KB- 07- MN"]
3288 TM STO=[ 1378](cu- m)
3289 *%-----|-----|
3290 ADD HYD NHYDsum=["KB- 07- S"], NHYDs to add=["KB- 07- M"+"KB- 07- MN"]
3291 *%-----|-----|
3292 CONTINUOUS STANDHYD NHYD=["KB- 08"], DT=[ 1]mi n, AREA=[ 6.61](ha), XI MP=[ 0.64],
TI MP=[ 0.64], DWF=[ 0](c ms), LOSS=[ 1]:
3293 Hort on: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
F=[ 0.00](mm),
3294 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
MNP=[ 0.250], SCP=[ 0](mi n),
3295 Impervious areas: IAi mp=[ 0.785](mm), SLPI=[ 2.0](%),
LGI=[ 209.921](m), MNI=[ 0.013], SCI=[ 0](mi n),
3296 Continuous simulation parameters:
3297 IaREcper=[ 4](hrs), IaRECi mp=[ 4](hrs), InterEvent Ti me=[ 12](hrs),
END=- 1
3298 *%-----|-----|
3299 COMPUTE DUALHYD NHYDi n=["KB- 08"], CI NLET=[ 1.058](c ms), NI NLET=[ 1],
3300 Mij NHYD=["KB- 08- M"]
3301 MnNHYD=["KB- 08- MN"]
3302 TM STO=[ 787](cu- m)
3303 *%-----|-----|
3304 ADD HYD NHYDsum=["KB- 08- S"], NHYDs to add=["KB- 08- M"+"KB- 08- MN"]
3305 *%-----|-----|
3306 CONTINUOUS STANDHYD NHYD=["KB- 09"], DT=[ 1]mi n, AREA=[ 2.6](ha), XI MP=[ 0.86],
TI MP=[ 0.86], DWF=[ 0](c ms), LOSS=[ 1]:
3307 Hort on: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
F=[ 0.00](mm),
3308 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
MNP=[ 0.250], SCP=[ 0](mi n),
3309 Impervious areas: IAi mp=[ 1.57](mm), SLPI=[ 2.0](%),

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3310          LGI=[ 131.656](m), MNI=[ 0.013], SCI=[ 0](min),
3311          Continuous simulation parameters:
3312          IaRECPer=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3313          END=- 1
3314          *%-----|-----|
3315          CONTINUOUS STANDHYD NHYD=["KB- 10_1"], DT=[ 1]min, AREA=[ 2.37](ha), XI MP=[ 0.86],
3316          T I MP=[ 0.86], DWF=[ 0](cms), LOSS=[ 1]:
3317          Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3318          F=[ 0.00](mm),
3319          Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3320          MNP=[ 0.250], SCP=[ 0](min),
3321          Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 2.0](%),
3322          LGI=[ 125.698](m), MNI=[ 0.013], SCI=[ 0](min),
3323          Continuous simulation parameters:
3324          IaRECPer=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3325          END=- 1
3326          *%-----|-----|
3327          CONTINUOUS STANDHYD NHYD=["KB- 10_2"], DT=[ 1]min, AREA=[ 1.14](ha), XI MP=[ 0.86],
3328          T I MP=[ 0.86], DWF=[ 0](cms), LOSS=[ 1]:
3329          Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3330          F=[ 0.00](mm),
3331          Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3332          MNP=[ 0.250], SCP=[ 0](min),
3333          Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 2.0](%), LGI=[ 87.178](m),
3334          MNI=[ 0.013], SCI=[ 0](min),
3335          Continuous simulation parameters:
3336          IaRECPer=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3337          END=- 1
3338          *%-----|-----|
3339          CONTINUOUS STANDHYD NHYD=["KB- 12"], DT=[ 1]min, AREA=[ 4.86](ha), XI MP=[ 0.79],
3340          T I MP=[ 0.79], DWF=[ 0](cms), LOSS=[ 1]:
3341          Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3342          F=[ 0.00](mm),
3343          Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3344          MNP=[ 0.250], SCP=[ 0](min),
3345          Impervious areas: IAimp=[ 1.099](mm), SLPI=[ 2.0](%),
3346          LGI=[ 180.000](m), MNI=[ 0.013], SCI=[ 0](min),
3347          Continuous simulation parameters:
3348          IaRECPer=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3349          END=- 1
3350          *%-----|-----|
3351          COMPUTE DUALHYD NHYDin=["KB- 12"], C I NLET=[ 0.8665](cms), N I NLET=[ 1],
3352          M a j NHYD=["KB- 12- M"]
3353          M n NHYD=["KB- 12- MN"]
3354          T M S T O=[ 632](cu-m)
3355          *%-----|-----|
3356          ADD HYD NHYDs um=["KB- 12- S"], NHYDs t o a d d=["KB- 12- M"+"KB- 12- MN"]
3357          *%-----|-----|
3358          CONTINUOUS STANDHYD NHYD=["KB- 13"], DT=[ 1]min, AREA=[ 10.19](ha), XI MP=[ 0.64],
3359          T I MP=[ 0.64], DWF=[ 0](cms), LOSS=[ 1]:
3360          Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3361          F=[ 0.00](mm),
3362          Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3363          MNP=[ 0.250], SCP=[ 0](min),
3364          Impervious areas: IAimp=[ 0.785](mm), SLPI=[ 2.0](%),
3365          LGI=[ 260.640](m), MNI=[ 0.013], SCI=[ 0](min),
3366          Continuous simulation parameters:
3367          IaRECPer=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3368          END=- 1
3369          *%-----|-----|
3370          COMPUTE DUALHYD NHYDin=["KB- 13"], C I NLET=[ 1.722](cms), N I NLET=[ 1],
3371          M a j NHYD=["KB- 13- M"]
3372          M n NHYD=["KB- 13- MN"]
3373          T M S T O=[ 1077](cu-m)

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3354 *%-----|-----|
3355 ADD HYD          NHYDs um=[ "KB- 13- S" ], NHYDs to add=[ "KB- 13- M" +"KB- 13- MN" ]
3356 *%-----|-----|
3357 CONTINUOUS STANDHYD NHYD=[ "KB- 14" ], DT=[ 1] mi n, AREA=[ 5. 47] (ha), XI MP=[ 0. 64],
TI MP=[ 0. 64], DWF=[ 0] (cms), LOSS=[ 1]:
3358 Horton: Fo=[ 76. 20] (mm/ hr), Fc=[ 13. 20] (mm/ hr), DCAY=[ 4. 14] (/ hr),
F=[ 0. 00] (mm),
3359 Pervious areas: IAper=[ 4. 67] (mm), SLPP=[ 2. 0] (%), LGP=[ 40] (m),
MNP=[ 0. 250], SCP=[ 0] (mi n),
3360 Impervious areas: IAi mp=[ 0. 785] (mm), SLPI =[ 2. 0] (%),
LGI =[ 190. 962] (m), MNI =[ 0. 013], SCI =[ 0] (mi n),
3361 Continuous simulation parameters:
3362 IaREcper=[ 4] (hr s), IaRECi mp=[ 4] (hr s), InterEvent Ti me=[ 12] (hr s),
END=- 1
3363 *%-----|-----|
3364 COMPUTE DUALHYD   NHYDi n=[ "KB- 14" ], CI NLET=[ 0. 8734] (cms), NI NLET=[ 1],
3365 Mj NHYD=[ "KB- 14- M" ]
3366 MnNHYD=[ "KB- 14- MN" ]
3367 TMSTO=[ 631] (cu- m)
3368 *%-----|-----|
3369 ADD HYD          NHYDs um=[ "KB- 14- S" ], NHYDs to add=[ "KB- 14- M" +"KB- 14- MN" ]
3370 *%-----|-----|
3371 *%-----|-----|
3372 CONTINUOUS STANDHYD NHYD=[ "KB- 16_2" ], DT=[ 1] mi n, AREA=[ 3. 42] (ha), XI MP=[ 0. 71],
TI MP=[ 0. 71], DWF=[ 0] (cms), LOSS=[ 1]:
3373 Horton: Fo=[ 76. 20] (mm/ hr), Fc=[ 13. 20] (mm/ hr), DCAY=[ 4. 14] (/ hr),
F=[ 0. 00] (mm),
3374 Pervious areas: IAper=[ 4. 67] (mm), SLPP=[ 2. 0] (%), LGP=[ 40] (m),
MNP=[ 0. 250], SCP=[ 0] (mi n),
3375 Impervious areas: IAi mp=[ 0. 157] (mm), SLPI =[ 0. 3] (%),
LGI =[ 150. 997] (m), MNI =[ 0. 013], SCI =[ 0] (mi n),
3376 Continuous simulation parameters:
3377 IaREcper=[ 4] (hr s), IaRECi mp=[ 4] (hr s), InterEvent Ti me=[ 12] (hr s),
END=- 1
3378 *%-----|-----|
3379 ADD HYD          NHYDs um=[ "KB- P2" ], NHYDs to
add=[ "KB- Pond1" +"KB- 07- S" +"KB- 08- S" +"KB- 09" +"KB- 10_1" +"KB- 10_2" +"KB- 12- S" +"KB- 13- S" +"KB- 1
4- S" +"KB- 16_2" ]
3380 *%-----|-----|
3381 ROUTE RESERVOIR  NHYDout =[ "KB- P2R" ], NHYDi n=[ "KB- P2" ],
3382 RDT=[ 1] (mi n),
3383 TABLE of ( OUTFLOW STORAGE ) values
3384 ( cms ) - ( ha- m)
3385 [ 0. 0 , 0. 0 ]
3386 [ 0. 053, 0. 005]
3387 [ 0. 132, 0. 009]
3388 [ 0. 269, 0. 014]
3389 [ 0. 455, 0. 023]
3390 [ 0. 699, 0. 037]
3391 [ 0. 947, 0. 056]
3392 [ 1. 853, 0. 09]
3393 [ 2. 712, 0. 146]
3394 [ 6. 626, 0. 287]
3395 [ 11. 228, 0. 515]
3396 [ 14. 885, 0. 738]
3397 [ 16. 473, 0. 893]
3398 [ 17. 311, 0. 998]
3399 [ 17. 633, 1. 063]
3400 [ 17. 634, 1. 112]
3401 [ -1 , -1 ] (max twenty pts)
3402 NHYDovf=[ "KB- P2ovf" ]
3403 *%-----|-----|
3404 ADD HYD          NHYDs um=[ "KB- Pond2" ], NHYDs to add=[ "KB- P2R" +"KB- P2ovf" ]
3405 *%-----|-----|
3406 SAVE HYD        NHYD=[ "KB- Pond2" ], # OF PCYCLES=[ -1], ICASEsh=[ 1]
3407 HYD_COMMENT=[ "Total Flows at KB second pond" ]

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3408 *%-----|-----|
3409 CONTINUOUS STANDHYD NHYD=["KB-16_1"], DT=[1]min, AREA=[2.8](ha), XI MP=[0.75],
TI MP=[0.75], DWF=[0](cms), LOSS=[1]:
3410 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3411 Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3412 Impervious areas: I A i mp=[0.157](mm), SLPI=[0.3](%),
LGI=[136.626](m), MNI=[0.013], SCI=[0](min),
3413 Continuous simulation parameters:
3414 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
3415 *%-----|-----|
3416 ADD HYD NHYDsum=["KB-P3"], NHYDs to add=["KB-Pond2"+"KB-16_1"]
3417 *%-----|-----|
3418 *%-----|-----|
3419 * One inflow node from pond 3 is added to the model (ROUTE RESERVOIR)
3420 * Another inflow node from right side of pond 3 is not added to the model
3421 ROUTE RESERVOIR NHYDout=["KB-P3R"], NHYDin=["KB-P3"],
3422 RDT=[1](min),
3423 TABLE of ( OUTFLOW STORAGE ) values
3424 (cms) - (ha-m)
3425 [ 0.0 , 0.0 ]
3426 [0.051,0.002]
3427 [0.048,0.003]
3428 [0.057,0.029]
3429 [0.089,0.045]
3430 [0.133,0.069]
3431 [0.199,0.106]
3432 [0.321,0.172]
3433 [1.029,0.306]
3434 [4.036,0.527]
3435 [8.332,0.761]
3436 [11.727,0.941]
3437 [14.125,1.067]
3438 [15.675,1.149]
3439 [16.555,1.196]
3440 [16.911,1.214]
3441 [ -1 , -1 ] (max twenty pts)
3442 NHYDovf=["KB-P3ovf"]
3443 *%-----|-----|
3444 ADD HYD NHYDsum=["KB-Pond3"], NHYDs to add=["KB-P3R"+"KB-P3ovf"]
3445 *%-----|-----|
3446 SAVE HYD NHYD=["KB-Pond3"], # OF PCYCLES=[-1], I CASEs h=[1]
3447 HYD_COMMENT=["Total Flows at KB third pond"]
3448 *%-----|-----|
3449 *#*****
3450 *# EXISTING / PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118080), SWM
Modeling Approach, NOVATECH Report June, 2020)
3451 *# - TO FRASER-CLARKE DRAIN
3452 *#*****
3453 CONTINUOUS STANDHYD NHYD=["FC-01"], DT=[1]min, AREA=[8.03](ha), XI MP=[0.47],
TI MP=[0.47], DWF=[0](cms), LOSS=[1]:
3454 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3455 Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3456 Impervious areas: I A i mp=[1.57](mm), SLPI=[1.0](%),
LGI=[231.373](m), MNI=[0.013], SCI=[0](min),
3457 Continuous simulation parameters:
3458 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
3459 *%-----|-----|
3460 COMPUTE DUALHYD NHYDin=["FC-01"], C I NLET=[0.756](cms), N I NLET=[1],
3461 M i j NHYD=["FC-01-M"]
3462 M n NHYD=["FC-01-MN"]

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3463          TMI STO=[ 714] ( cu- m)
3464 *%------|-----|
3465 ADD HYD      NHYDs um=[ "FC- 01- S" ], NHYDs  to  add=[ "FC- 01- M" +"FC- 01- MN" ]
3466 *%------|-----|
3467 CONTI NUOUS STANDHYD NHYD=[ "FC- 02" ], DT=[ 1] mi n, AREA=[ 16. 05] ( ha), XI MP=[ 0. 93],
TI MP=[ 0. 93], DWF=[ 0] ( cms), LOSS=[ 1]:
3468          Hort on: Fo=[ 76. 20] ( mm/ hr), Fc=[ 13. 20] ( mm/ hr), DCAY=[ 4. 14] (/ hr),
F=[ 0. 00] ( mm),
3469          Perv ious  areas: IAper=[ 4. 67] ( mm), SLPP=[ 2. 0] ( %), LGP=[ 40] ( m),
MNP=[ 0. 250], SCP=[ 0] ( mi n),
3470          Imperv ious  areas: IAi mp=[ 1. 57] ( mm), SLPI=[ 1. 0] ( %),
LGI=[ 327. 109] ( m), MNI=[ 0. 013], SCI=[ 0] ( mi n),
3471          Continuous simulation parameters:
3472          IaRECper=[ 4] ( hr s), IaRECI mp=[ 4] ( hr s), Int er Event Ti me=[ 12] ( hr s),
END=- 1
3473 *%------|-----|
3474 COMPUTE DUALHYD  NHYDi n=[ "FC- 02" ], CI NLET=[ 1. 159] ( cms), NI NLET=[ 1],
3475          Mj NHYD=[ "FC- 02- M" ]
3476          MnNHYD=[ "FC- 02- MN" ]
3477          TMI STO=[ 2385] ( cu- m)
3478 *%------|-----|
3479 ADD HYD      NHYDs um=[ "FC- 02- S" ], NHYDs  to  add=[ "FC- 02- M" +"FC- 02- MN" ]
3480 *%------|-----|
3481 CONTI NUOUS STANDHYD NHYD=[ "FC- 03" ], DT=[ 1] mi n, AREA=[ 7. 37] ( ha), XI MP=[ 0. 64],
TI MP=[ 0. 64], DWF=[ 0] ( cms), LOSS=[ 1]:
3482          Hort on: Fo=[ 76. 20] ( mm/ hr), Fc=[ 13. 20] ( mm/ hr), DCAY=[ 4. 14] (/ hr),
F=[ 0. 00] ( mm),
3483          Perv ious  areas: IAper=[ 4. 67] ( mm), SLPP=[ 2. 0] ( %), LGP=[ 40] ( m),
MNP=[ 0. 250], SCP=[ 0] ( mi n),
3484          Imperv ious  areas: IAi mp=[ 1. 57] ( mm), SLPI=[ 1. 0] ( %),
LGI=[ 221. 660] ( m), MNI=[ 0. 013], SCI=[ 0] ( mi n),
3485          Continuous simulation parameters:
3486          IaRECper=[ 4] ( hr s), IaRECI mp=[ 4] ( hr s), Int er Event Ti me=[ 12] ( hr s),
END=- 1
3487 *%------|-----|
3488 COMPUTE DUALHYD  NHYDi n=[ "FC- 03" ], CI NLET=[ 0. 358] ( cms), NI NLET=[ 1],
3489          Mj NHYD=[ "FC- 03- M" ]
3490          MnNHYD=[ "FC- 03- MN" ]
3491          TMI STO=[ 1131] ( cu- m)
3492 *%------|-----|
3493 ADD HYD      NHYDs um=[ "FC- 03- S" ], NHYDs  to  add=[ "FC- 03- M" +"FC- 03- MN" ]
3494 *%------|-----|
3495 CONTI NUOUS STANDHYD NHYD=[ "FC- 04" ], DT=[ 1] mi n, AREA=[ 12. 87] ( ha), XI MP=[ 0. 64],
TI MP=[ 0. 64], DWF=[ 0] ( cms), LOSS=[ 1]:
3496          Hort on: Fo=[ 76. 20] ( mm/ hr), Fc=[ 13. 20] ( mm/ hr), DCAY=[ 4. 14] (/ hr),
F=[ 0. 00] ( mm),
3497          Perv ious  areas: IAper=[ 4. 67] ( mm), SLPP=[ 2. 0] ( %), LGP=[ 40] ( m),
MNP=[ 0. 250], SCP=[ 0] ( mi n),
3498          Imperv ious  areas: IAi mp=[ 1. 57] ( mm), SLPI=[ 1. 0] ( %),
LGI=[ 292. 916] ( m), MNI=[ 0. 013], SCI=[ 0] ( mi n),
3499          Continuous simulation parameters:
3500          IaRECper=[ 4] ( hr s), IaRECI mp=[ 4] ( hr s), Int er Event Ti me=[ 12] ( hr s),
END=- 1
3501 *%------|-----|
3502 COMPUTE DUALHYD  NHYDi n=[ "FC- 04" ], CI NLET=[ 0. 741] ( cms), NI NLET=[ 1],
3503          Mj NHYD=[ "FC- 04- M" ]
3504          MnNHYD=[ "FC- 04- MN" ]
3505          TMI STO=[ 1794] ( cu- m)
3506 *%------|-----|
3507 ADD HYD      NHYDs um=[ "FC- 04- S" ], NHYDs  to  add=[ "FC- 04- M" +"FC- 04- MN" ]
3508 *%------|-----|
3509 *#*****
3510 *#      PROPOSED Subcatchments ( Kennedy- Burnett SWM Facility ( 118080), SWM Mdeling
Approach, NOVATECH Report June, 2020)
3511 *#      - TO JOCK RI VER
3512 *#*****

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3513 CONTINUOUS STANDHYD NHYD=["JR-01"], DT=[1] min, AREA=[8.24](ha), XI MP=[0.64],
TI MP=[0.64], DWF=[0](cms), LOSS=[1]:
3514 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3515 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3516 Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
LGI=[234.379](m), MNI=[0.013], SCI=[0](min),
3517 Continuous simulation parameters:
3518 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3519 *%-----|
3520 COMPUTE DUALHYD NHYDin=["JR-01"], CINLET=[0.563](cms), NINLET=[1],
3521 MajNHYD=["JR-01-M"]
3522 MinNHYD=["JR-01-MN"]
3523 TMSSTO=[1040](cu-m)
3524 *%-----|
3525 ADD HYD NHYDsum=["JR-01-S"], NHYDstoadd=["JR-01-M"+"JR-01-MN"]
3526 *%-----|
3527 CONTINUOUS STANDHYD NHYD=["JR-02"], DT=[1] min, AREA=[1.59](ha), XI MP=[0.64],
TI MP=[0.64], DWF=[0](cms), LOSS=[1]:
3528 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3529 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3530 Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
LGI=[102.956](m), MNI=[0.013], SCI=[0](min),
3531 Continuous simulation parameters:
3532 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3533 *%-----|
3534 COMPUTE DUALHYD NHYDin=["JR-02"], CINLET=[0.153](cms), NINLET=[1],
3535 MajNHYD=["JR-02-M"]
3536 MinNHYD=["JR-02-MN"]
3537 TMSSTO=[153](cu-m)
3538 *%-----|
3539 ADD HYD NHYDsum=["JR-02-S"], NHYDstoadd=["JR-02-M"+"JR-02-MN"]
3540 *%-----|
3541 *#*****
3542 *# Catchment FRASER
3543 *# - To Fraser-Clarke drain (north of the Jock)
3544 *# - Developed land with assumed 43% imp.
3545 *# - 2020-12-17 Change Fraser area to be 35.1 as measured from QGIS
3546 *# - 2020-12-17 All Fraser is undeveloped (Nashyd)
3547 *#*****
3548 CONTINUOUS NASHYD NHYD=["FRASER-DRN"], DT=[1] min, AREA=[13.65](ha),
3549 DWF=[0](cms), CNVC=[77], IA=[4.67](mm),
3550 N=[3], TP=[0.4258]hrs,
3551 Continuous simulation parameters:
3552 IaRECper=[4](hrs),
3553 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3554 InterEventTime=[12](hrs)
3555 Baseflow simulation parameters:
3556 BaseFlowOption=[1],
3557 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
3558 VHydCond=[0.055](mm/hr), END=-1
3559 *%-----|
3560 *CONTINUOUS STANDHYD NHYD=["FRASER-D"], DT=[1] min, AREA=[21.61](ha),
3561 * XI MP=[0.585], TI MP=[0.585], DWF=[0](cms), LOSS=[2],
3562 * SCS curve number CN=[80],
3563 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3564 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3565 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3566 * LGI=[379.561](m), MNI=[0.013], SCI=[0](min),
3567 * Continuous simulation parameters:
3568 * IaRECper=[4](hrs), IaRECImp=[4](hrs),

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3569 * SMN=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
3570 * InterEventTime=[ 18 ] ( hr s ) , END=- 1
3571 *%-----|-----|
3572 CONTINUOUS NASHYD NHYD=[ " FRASER- D' ] , DT=[ 1 ] mi n , AREA=[ 21. 61 ] ( ha ) ,
3573 DWF=[ 0 ] ( cms ) , CNVC=[ 77 ] , IA=[ 4. 67 ] ( mm ) ,
3574 N=[ 3 ] , TP=[ 0. 674 ] hr s ,
3575 Continuous simulation parameters:
3576 IaRECper=[ 4 ] ( hr s ) ,
3577 SMN=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
3578 InterEventTime=[ 12 ] ( hr s )
3579 Baseflow simulation parameters:
3580 BaseFlowOption=[ 1 ] ,
3581 InitGWResVol=[ 50 ] ( mm ) , GWResK=[ 0. 96 ] ( mm/ day/ mm)
3582 VHydCond=[ 0. 055 ] ( mm/ hr ) , END=- 1
3583 *%-----|-----|
3584 * COMPUTE DUALHYD NHYDin=[ " FRASER- D' ] , CINLET=[ 3. 545 ] ( cms ) , NINLET=[ 1 ] ,
3585 * MjNHYD=[ " FRASER- J " ]
3586 * MnNHYD=[ " FRASER- N' ]
3587 * TMSTO=[ 9999999 ] ( cu- m)
3588 *%-----|-----|
3589 * ADD HYD NHYDs um=[ " FRASER- S' ] , NHYDs to add=[ " FRASER- J'+"FRASER- N' ]
3590 *%-----|-----|
3591 * ROUTE RESERVOIR NHYDout=[ " MS_P20' ] , NHYDin=[ " FRASER' ] ,
3592 * RDT=[ 1 ] ( mi n) ,
3593 * TABLE of ( OUTFLOW STORAGE ) values
3594 * ( cms ) - ( ha- m)
3595 * [ 0. 0 , 0. 0 ]
3596 * [ 0. 04 , 0. 36 ]
3597 * [ - 1 , - 1 ] ( max twenty pts)
3598 * NHYDovf=[ " P20- OVF' ]
3599 *%-----|-----|
3600 * ADD HYD NHYDs um=[ " 4241' ] , NHYDs to
add=[ " KB- Pond3'+"S- 1- B'+"FRASER- DRN'+"FRASER- D'+"N_KB'+"FC- 01- S'+"FC- 02- S'+"FC- 03- S' ]
3601 *%-----|-----|
3602 * SAVE HYD NHYD=[ " 4241' ] , # OF PCYCLES=[ - 1 ] , ICASEsh=[ 1 ]
3603 * HYD_COMMENT=[ " Total Flows at Ken- Burnett Outlet " ]
3604 *%-----|-----|
3605 *# Hydrograph from Node Ken- Burnett to station 3633
3606 *# Channel X- Section obtained from RVCA Hydraulic Model - Station 4241
3607 *#
3608 * ROUTE CHANNEL NHYDout=[ " 4241- out' ] , NHYDin=[ " 4241' ] , RDT=[ 1 ] ( mi n) ,
3609 * CHLGT=[ 294 ] ( m ) , CHSLOPE=[ 0. 1088 ] ( % ) , FPSLOPE=[ 0. 1088 ] ( % ) ,
3610 * SECNUM=[ 1. 0 ] , NSEG=[ 3 ]
3611 * ( SEGROUGH, SEGDIST ( m ) )=[ 0. 05 , - 20. 12
3612 * - 0. 035 , 45. 26
3613 * 0. 05 , 403. 84 ] NSEG times
3614 * ( DISTANCE ( m ) , ELEVATION ( m ) )=[ ]
3615 * [ - 909. 72 , 95 ]
3616 * [ - 907. 09 , 94. 5 ]
3617 * [ - 904. 65 , 94 ]
3618 * [ - 902. 26 , 93. 5 ]
3619 * [ - 44. 51 , 91. 5 ]
3620 * [ - 25. 1 , 91. 5 ]
3621 * [ - 20. 98 , 91 ]
3622 * [ - 20. 61 , 90. 5 ]
3623 * [ - 20. 12 , 90 ]
3624 * [ - 6. 13 , 87. 26 ]
3625 * [ 17. 51 , 86. 56 ]
3626 * [ 31. 37 , 87. 2 ]
3627 * [ 45. 26 , 90 ]
3628 * [ 50. 41 , 90. 5 ]
3629 * [ 63. 06 , 91 ]
3630 * [ 134. 5 , 91. 5 ]
3631 * [ 190. 63 , 92 ]
3632 * [ 251. 98 , 92. 5 ]
3633 * [ 321. 32 , 93. 5 ]

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3634 [ 403.84, 95 ]
3635 *%-----|-----|
3636 ADD HYD NHYDsum=["SN_KB"], NHYDs to
add=["4241-out"+"FC-04-S"+"JR-01-S"+"JR-02-S"]
3637 *%-----|-----|
3638 SAVE HYD NHYD=["SN_KB"], # OF PCYCLES=[-1], ICASEsh=[1]
3639 HYD_COMMENT=["Total Flows before Station 3633"]
3640 *%-----|-----|
3641 *# Hydrograph from Station 3633 to Node Todd
3642 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 3633
3643 *# JFSA 2021-02-26 change the channel length (at station 3633) from 650m to 608m and
change the slope from 0.0498% to 0.24671% That is because of adding station 4241
between station 4534 and station 3633
3644 *#
3645 ROUTE CHANNEL NHYDout=["N_TO"], NHYDin=["SN_KB"], RDT=[1](min),
3646 CHLGTH=[608](m), CHSLOPE=[0.24671](%), FPSLOPE=[0.24671](%),
3647 SECNUM=[1.0], NSEG=[3]
3648 (SEGROUGH, SEGDI ST (m))=[0.05, -23.74
3649 -0.035, 23.74
3650 0.05, 26.50] NSEG times
3651 (DISTANCE (m), ELEVATION (m))=[
3652 -29.24, 91.0
3653 -27.41, 90.5
3654 -25.64, 90
3655 -23.74, 89.5
3656 -22, 89.26
3657 -20, 88.51
3658 -19, 88.32
3659 -15, 88.1
3660 -10, 88.11
3661 -5, 88.17
3662 0, 88.27
3663 5, 88.19
3664 10, 88.06
3665 15, 88.48
3666 16, 88.7
3667 23.74, 89.5
3668 24.68, 90
3669 25.57, 90.5
3670 26.50, 91.0
3671 * [-29.24, 91]
3672 * [-27.41, 90.5]
3673 * [-25.64, 90]
3674 * [-23.74, 89.5]
3675 * [-22, 89.26]
3676 * [-20, 88.51]
3677 * [-19, 88.32]
3678 * [-15, 88.1]
3679 * [-10, 88.11]
3680 * [-5, 88.17]
3681 * [0, 88.27]
3682 * [5, 88.19]
3683 * [10, 88.06]
3684 * [15, 88.48]
3685 * [16, 88.7]
3686 * [23.74, 89.5]
3687 * [24.68, 90]
3688 * [25.57, 90.5]
3689 *%-----|-----|
3690 *#*****
3691 *# Catchment Greenbank
3692 *# - To Greenbank Drain (south of the Jock)
3693 *# - JFSA 2021-01-18 add Greenbank pond as per JFSA, P598(06)-15, June 2016
3694 *# - JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GIS measurements
3695 *#*****
3696 CONTINUOUS STANDHYD NHYD=["Greenbank"], DT=[1]min, AREA=[36.6](ha),

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3697      XI MP=[ 0. 639], TI MP=[ 0. 682], DWF=[ 0](cms), LOSS=[ 2],
3698      SCS curve number CN=[ 77],
3699      Pervious surfaces: IAper=[ 4. 67](mm), SLPP=[ 1](%),
3700      LGP=[ 40](m), MNP=[ 0. 25], SCP=[ 0](min),
3701      Impervious surfaces: IAimp=[ 1. 57](mm), SLPI=[ 1](%),
3702      LGI=[ 493. 96](m), MNI=[ 0. 013], SCI=[ 0](min),
3703      Continuous simulation parameters:
3704      IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
3705      SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0. 010]/(mm),
3706      InterEventTime=[ 18](hrs), END=- 1
3707  *%-----|-----|
3708  ROUTE RESERVOIR  NHYDout=["GreenB_MN"], NHYDin=["Greenbank"],
3709      RDT=[ 1](min),
3710      TABLE of ( OUTFLOW STORAGE ) values
3711      (cms) - (ha-m)
3712      [ 0. 0 , 0. 0 ]
3713      [ 0. 033 , 0. 084 ]
3714      [ 0. 039 , 0. 201 ]
3715      [ 0. 113 , 0. 292 ]
3716      [ 0. 237 , 0. 386 ]
3717      [ 0. 382 , 0. 484 ]
3718      [ 0. 539 , 0. 585 ]
3719      [ 0. 7 , 0. 692 ]
3720      [ 0. 86 , 0. 804 ]
3721      [ 4. 684 , 0. 922 ]
3722      [ 11. 539 , 1. 052 ]
3723      [ 20. 867 , 1. 168 ]
3724      [ 103. 616 , 1. 974 ]
3725      [ -1 , -1 ] (max twenty pts)
3726      NHYDovf=["GreenB_M"],
3727  *%-----|-----|
3728  *%-----|-----|
3729  ADD HYD          NHYDs um=["GreenB"], NHYDs to add=["N_TO"+"GreenB_M"+"GreenB_MN"]
3730  *%-----|-----|
3731  SAVE HYD        NHYD=["GreenB"], # OF PCYCLES=[ -1], ICASEsh=[ 1]
3732      HYD_COMMENT=["Total Flows at Greenbank Drain"]
3733  *%-----|-----|
3734  *#*****|*****|
3735  *# Catchment TODD
3736  *# - To Todd Drain (south of the Jock)
3737  *# - Subdivision with 43% imp. as per Barrhaven South MSS
3738  *# - 2020-11-30 increase imp. based on P598(04)-11
3739  *# - 2020-11-30 update TODD Tributary Drainage Area to = 146.015 ha based on
3740  *# - 2020-11-30 split TODD Drainage Area to MAJOR, MINOR, POND and ALL
3741  *#*****|*****|
3742  *# - JFSA 2021-01-19 add "TODD_MN1" as part of Clarke("W_CLAR_M") and remove it
3743  *# from Todd
3744  *CONTINUOUS STANDHYD NHYD=["TODD_MN1"], DT=[ 1]min, AREA=[ 1. 772](ha),
3745  *      XI MP=[ 0. 53], TI MP=[ 0. 57], DWF=[ 0](cms), LOSS=[ 2],
3746  *      SCS curve number CN=[ 77],
3747  *      Pervious surfaces: IAper=[ 4. 67](mm), SLPP=[ 1](%),
3748  *      LGP=[ 40](m), MNP=[ 0. 25], SCP=[ 0](min),
3749  *      Impervious surfaces: IAimp=[ 1. 57](mm), SLPI=[ 1](%),
3750  *      LGI=[ 108. 689](m), MNI=[ 0. 013], SCI=[ 0](min),
3751  *      Continuous simulation parameters:
3752  *      IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
3753  *      SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0. 010]/(mm),
3754  *      InterEventTime=[ 18](hrs), END=- 1
3755  *%-----|-----|
3756  CONTINUOUS STANDHYD NHYD=["TODD_MN2"], DT=[ 1]min, AREA=[ 2. 1](ha),
3757  *      XI MP=[ 0. 53], TI MP=[ 0. 57], DWF=[ 0](cms), LOSS=[ 2],
3758  *      SCS curve number CN=[ 77],
3759  *      Pervious surfaces: IAper=[ 4. 67](mm), SLPP=[ 1](%),
3760  *      LGP=[ 40](m), MNP=[ 0. 25], SCP=[ 0](min),
3761  *      Impervious surfaces: IAimp=[ 1. 57](mm), SLPI=[ 1](%),

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3761             LGI=[ 118.322](m), MNI=[ 0.013], SCI=[ 0](min),
3762 Continuous simulation parameters:
3763 IaRECPER=[ 4](hrs), IaRECI MP=[ 4](hrs),
3764 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
3765 InterEventTime=[ 18](hrs), END=- 1
3766 *%-----|-----|
3767 CONTINUOUS STANDHYD NHYD=["TODD_MN3"], DT=[ 1]min, AREA=[ 0.117](ha),
3768 XI MP=[ 0.53], TI MP=[ 0.57], DWF=[ 0](cms), LOSS=[ 2],
3769 SCS curve number CN=[ 77],
3770 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
3771             LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
3772 Impervious surfaces: IAi mp=[ 1.57](mm), SLPI=[ 1](%),
3773             LGI=[ 27.928](m), MNI=[ 0.013], SCI=[ 0](min),
3774 Continuous simulation parameters:
3775 IaRECPER=[ 4](hrs), IaRECI MP=[ 4](hrs),
3776 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
3777 InterEventTime=[ 18](hrs), END=- 1
3778 *%-----|-----|
3779 CONTINUOUS STANDHYD NHYD=["TODD_M"], DT=[ 1]min, AREA=[ 30.230](ha),
3780 XI MP=[ 0.52], TI MP=[ 0.64], DWF=[ 0](cms), LOSS=[ 2],
3781 SCS curve number CN=[ 77],
3782 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
3783             LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
3784 Impervious surfaces: IAi mp=[ 1.57](mm), SLPI=[ 1](%),
3785             LGI=[ 448.925](m), MNI=[ 0.013], SCI=[ 0](min),
3786 Continuous simulation parameters:
3787 IaRECPER=[ 4](hrs), IaRECI MP=[ 4](hrs),
3788 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
3789 InterEventTime=[ 18](hrs), END=- 1
3790 *%-----|-----|
3791 * -JFSA, 2021-01-19 update "TODD_ALL" area from 108.741 ha to 112.908 ha based on
GIS measurements (148.41-30.23-0.117-2.1-3.055=112.908 ha)
3792 CONTINUOUS STANDHYD NHYD=["TODD_ALL"], DT=[ 1]min, AREA=[ 112.908](ha),
3793 XI MP=[ 0.52], TI MP=[ 0.57], DWF=[ 0](cms), LOSS=[ 2],
3794 SCS curve number CN=[ 77],
3795 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
3796             LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
3797 Impervious surfaces: IAi mp=[ 1.57](mm), SLPI=[ 1](%),
3798             LGI=[ 867.594](m), MNI=[ 0.013], SCI=[ 0](min),
3799 Continuous simulation parameters:
3800 IaRECPER=[ 4](hrs), IaRECI MP=[ 4](hrs),
3801 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
3802 InterEventTime=[ 18](hrs), END=- 1
3803 *%-----|-----|
3804 CONTINUOUS STANDHYD NHYD=["TODD_P"], DT=[ 1]min, AREA=[ 3.055](ha),
3805 XI MP=[ 0.63], TI MP=[ 0.63], DWF=[ 0](cms), LOSS=[ 2],
3806 SCS curve number CN=[ 77],
3807 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
3808             LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
3809 Impervious surfaces: IAi mp=[ 1.57](mm), SLPI=[ 1](%),
3810             LGI=[ 142.712](m), MNI=[ 0.013], SCI=[ 0](min),
3811 Continuous simulation parameters:
3812 IaRECPER=[ 4](hrs), IaRECI MP=[ 4](hrs),
3813 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
3814 InterEventTime=[ 18](hrs), END=- 1
3815 *%-----|-----|
3816 *%-----|-----|
3817 * -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"
and its parameters remain the same.
3818 *CONTINUOUS STANDHYD NHYD=["TODD_DEVL"], DT=[ 1]min, AREA=[ 15.87](ha),
3819 * XI MP=[ 0.63], TI MP=[ 0.63], DWF=[ 0](cms), LOSS=[ 2],
3820 * SCS curve number CN=[ 77],
3821 * Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
3822 *             LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
3823 * Impervious surfaces: IAi mp=[ 1.57](mm), SLPI=[ 1](%),

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3824 *                LGI=[ 325.27](m), MNI=[ 0.013], SCI=[ 0](min),
3825 *                Continuous simulation parameters:
3826 *                IaRECper=[ 4](hrs), IaRECimp=[ 4](hrs),
3827 *                SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
3828 *                InterEventTime=[ 18](hrs), END=- 1
3829 *%-----|-----
3830 *                -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
3831 *                is called "corr2" and its parameters remain the same.
3832 *CONTINUOUS NASHYD NHYD=["TODD_UnD"], DT=[ 1]min, AREA=[ 12.47](ha),
3833 *                DWF=[ 0](cms), CNVC=[ 77], IA=[ 4.67](mm),
3834 *                N=[ 3], TP=[ 1.10]hrs,
3835 *                Continuous simulation parameters:
3836 *                IaRECper=[ 4](hrs),
3837 *                SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
3838 *                InterEventTime=[ 12](hrs)
3839 *                Baseflow simulation parameters:
3840 *                BaseFlowOption=[ 1],
3841 *                InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
3842 *                VHydCond=[ 0.055](mm/hr), END=- 1
3843 *%-----|-----
3844 *# 5-Year + 12% Capture
3845 *COMPUTE DUALHYD NHYDin=["TODD_Mj"], CINLET=[ 3.314](cms), NINLET=[ 1],
3846 *                MjNHYD=["TODD_Mj"]
3847 *                MnNHYD=["TODD_Mjn"]
3848 *                TMSTO=[ 0.1](cu-m)
3849 ROUTE RESERVOIR NHYDout=["TODD_Mjn"], NHYDin=["TODD_Mj"],
3850 RDT=[ 1](min),
3851 TABLE of ( OUTFLOW STORAGE ) values
3852 (cms) - (ha-m)
3853 [ 0.0 , 0.0 ]
3854 [ 3.314 , 0.0001 ]
3855 [ -1 , -1 ] (max twenty pts)
3856 NHYDovf=["TODD_Mj"],
3857 *%-----|-----
3858 *# 5-Year + 12% Capture
3859 *COMPUTE DUALHYD NHYDin=["TODD_MN1"], CINLET=[ 0.227](cms), NINLET=[ 1],
3860 *                MjNHYD=["TODD_MN1j"]
3861 *                MnNHYD=["TODD_MN1n"]
3862 *                TMSTO=[ 0.1](cu-m)
3863 ROUTE RESERVOIR NHYDout=["TODD_MN1n"], NHYDin=["TODD_MN1"],
3864 RDT=[ 1](min),
3865 TABLE of ( OUTFLOW STORAGE ) values
3866 (cms) - (ha-m)
3867 [ 0.0 , 0.0 ]
3868 [ 0.227 , 0.0001 ]
3869 [ -1 , -1 ] (max twenty pts)
3870 NHYDovf=["TODD_MN1j"],
3871 *%-----|-----
3872 *COMPUTE DUALHYD NHYDin=["TODD_MN2"], CINLET=[ 0.268](cms), NINLET=[ 1],
3873 *                MjNHYD=["TODD_MN2j"]
3874 *                MnNHYD=["TODD_MN2n"]
3875 *                TMSTO=[ 0.1](cu-m)
3876 ROUTE RESERVOIR NHYDout=["TODD_MN2n"], NHYDin=["TODD_MN2"],
3877 RDT=[ 1](min),
3878 TABLE of ( OUTFLOW STORAGE ) values
3879 (cms) - (ha-m)
3880 [ 0.0 , 0.0 ]
3881 [ 0.268 , 0.0001 ]
3882 [ -1 , -1 ] (max twenty pts)
3883 NHYDovf=["TODD_MN2j"],
3884 *%-----|-----
3885 *COMPUTE DUALHYD NHYDin=["TODD_MN3"], CINLET=[ 0.016](cms), NINLET=[ 1],
3886 *                MjNHYD=["TODD_MN3j"]
3887 *                MnNHYD=["TODD_MN3n"]
3888 *                TMSTO=[ 0.1](cu-m)
3889 ROUTE RESERVOIR NHYDout=["TODD_MN3n"], NHYDin=["TODD_MN3"],

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3889          RDT=[ 1 ] ( m i n ) ,
3890          TABLE of ( OUTFLOW STORAGE ) values
3891              ( c m s ) - ( h a - m )
3892              [ 0.0 , 0.0 ]
3893              [ 0.016 , 0.0001 ]
3894              [ -1 , -1 ] ( m a x t w e n t y p t s )
3895          NHYDovf=[ " TODD_MN3j " ] ,
3896 *%-----|-----
3897 * -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
major system from A2 can be added to Todd
3898 CONTINUOUS STANDHYD NHYD=[ " A2 " ] , DT=[ 1 ] m i n , AREA=[ 25.5 ] ( h a ) ,
3899 XI MP=[ 0.42 ] , TI MP=[ 0.52 ] , DWF=[ 0 ] ( c m s ) , LOSS=[ 2 ] ,
3900 SCS curve number CN=[ 75 ] ,
3901 Pervious surfaces: I A p e r=[ 4.67 ] ( m m ) , SLPP=[ 1 ] ( % ) ,
3902 L G P=[ 40 ] ( m ) , M N P=[ 0.25 ] , S C P=[ 0 ] ( m i n ) ,
3903 I m p e r v i o u s s u r f a c e s : I A i m p=[ 1.57 ] ( m m ) , S L P I=[ 1 ] ( % ) ,
3904 L G I=[ 566 ] ( m ) , M N I=[ 0.013 ] , S C I=[ 0 ] ( m i n ) ,
3905 C o n t i n u o u s s i m u l a t i o n p a r a m e t e r s :
3906 I a R E C p e r=[ 4 ] ( h r s ) , I a R E C i m p=[ 4 ] ( h r s ) ,
3907 S M N=[ -1 ] ( m m ) , S M A X=[ -1 ] ( m m ) , S K=[ 0.010 ] / ( m m ) ,
3908 I n t e r E v e n t T i m e=[ 18 ] ( h r s ) , E N D=-1
3909 *%-----|-----
3910 COMPUTE DUALHYD NHYD i n=[ " A2 " ] , C I N L E T=[ 1.818 ] ( c m s ) , N I N L E T=[ 1 ] ,
3911 M a j N H Y D=[ " A2 - M " ]
3912 M i n N H Y D=[ " A2 - M N " ]
3913 T M S T O=[ 924 ] ( c u - m )
3914 *%-----|-----
3915 ADD HYD NHYDs u m=[ " TODD " ] , NHYDs t o
add=[ " TODD_MN2n " + " TODD_MN3n " + " TODD_Mj " + " TODD_P " + " TODD_ALL " + " W_CLAR_Mn " ]
3916 *%-----|-----
3917 SAVE HYD NHYD=[ " TODD " ] , # O F P C Y C L E S=[ -1 ] , I C A S E s h=[ 1 ]
3918 HYD_COMMENT=[ " T o t a l F l o w s a t T o d d D r a i n " ]
3919 *%-----|-----
3920 *#*****
3921 *# Todd Pond 3
3922 *# - Rating curve obtained from Barrhaven South M&S modeling
3923 *# - stantec 2007, Tributary Drainage Area to M&S Pond 3 = 193 ha
3924 *#*****
3925 ROUTE RESERVOIR NHYDout=[ " M&S_P3 " ] , NHYD i n=[ " TODD " ] ,
3926 RDT=[ 1 ] ( m i n ) ,
3927 TABLE of ( OUTFLOW STORAGE ) values
3928 ( c m s ) - ( h a - m )
3929 [ 0.0 , 0.0 ]
3930 [ 0.014 , 0.155 ]
3931 [ 0.048 , 0.394 ]
3932 [ 0.061 , 0.56 ]
3933 [ 0.08 , 0.909 ]
3934 [ 0.088 , 1.089 ]
3935 [ 0.109 , 1.652 ]
3936 [ 0.118 , 1.952 ]
3937 [ 0.122 , 2.099 ]
3938 [ 1.972 , 2.269 ]
3939 [ 9.135 , 2.598 ]
3940 [ 15.608 , 2.826 ]
3941 [ 19.256 , 2.942 ]
3942 [ 27.282 , 3.181 ]
3943 [ 40.957 , 3.55 ]
3944 [ 56.372 , 3.929 ]
3945 [ 73.349 , 4.317 ]
3946 [ 85.469 , 4.579 ]
3947 [ 104.771 , 4.977 ]
3948 [ -1 , -1 ] ( m a x t w e n t y p t s )
3949 NHYDovf=[ " P3 - O V F " ]
3950 *%-----|-----
3951 ADD HYD NHYDs u m=[ " SN_TO " ] , NHYDs t o
add=[ " GreenB " + " M&S_P3 " + " P3 - O V F " + " TODD_MN2j " + " A2 - M " ]

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3952 *%-----|-----|
3953 SAVE HYD      NHYD=[ "SN_TO" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
3954              HYD_COMMENT=[ "Total Flows at Todd Drain" ]
3955 *%-----|-----|
3956 *#
3957 *# Hydrograph from Todd Drain routed to Corrigan Drain
3958 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
3959 *# 2021-02-19 Change the slope from 0.033 % (as per Stantec Report 2007) to 0.05 % so
the model will be more stable and give reasonable results. It is justifiable as ROUTE
CHANNELs aren't well suited to really flat slopes.
*
3960
3961 ROUTE CHANNEL  NHYDout =["N_TO" ] , NHYDin=["SN_TO" ] ,
3962              RDT=[ 1 ] ( min ),
3963              CHLGTH=[ 280 ] ( m ), CHSLOPE=[ 0.05 ] ( % ),
3964              FPSLOPE=[ 0.05 ] ( % ),
3965              SECNUM=[ 1.0 ], NSEG=[ 3 ]
3966              ( SEGROUGH, SEGDI ST ( m ) ) =
3967              [ 0.075, - 17.72
3968              - 0.045, 17.72
3969              0.075, 80.62 ] NSEG times
3970              ( DI STANCE ( m ), ELEVATI ON ( m ) ) =
3971              [ - 83.32, 90.00 ]
3972              [ - 81.36, 89.50 ]
3973              [ - 79.12, 89.00 ]
3974              [ - 76.13, 88.50 ]
3975              [ - 20.46, 88.00 ]
3976              [ - 19.36, 87.50 ]
3977              [ - 18.51, 87.00 ]
3978              [ - 17.72, 86.50 ]
3979              [ - 11.95, 85.24 ]
3980              [ - 0.11, 85.12 ]
3981              [ 11.49, 85.20 ]
3982              [ 17.72, 86.50 ]
3983              [ 19.74, 87.00 ]
3984              [ 21.22, 87.50 ]
3985              [ 22.68, 88.00 ]
3986              [ 24.28, 88.50 ]
3987              [ 26.79, 89.00 ]
3988              [ 71.98, 90.00 ]
3989              [ 80.62, 90.50 ]
3990 *%-----|-----|
3991 SAVE HYD      NHYD=[ "N_TO" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
3992              HYD_COMMENT=[ "Total inflows at Station 2462" ]
3993 *%-----|-----|
3994 *#*****
3995 *# Catchment CORRIG
3996 *# - To Corrigan Drain (south of the Jock)
3997 *# - Primarily Developed (medium density)
3998 *# - JFSA JAN 2021, add Corrigan subcatchments as per IBI, July 2008
3999 *#*****
4000 *ROUTE RESERVOIR NHYDout=["MS_P1" ], NHYDin=["CORRIG" ],
4001 *              RDT=[ 1 ] ( min ),
4002 *              TABLE of ( OUTFLOW STORAGE ) values
4003 *              ( cms ) - ( ha-m )
4004 *              [ 0.0 , 0.0 ]
4005 *              [ 0.06 , 0.58 ]
4006 *              [ - 1 , - 1 ] (max twenty pts)
4007 *              NHYDovf=["P1-OVF" ]
4008 *%-----|-----|
4009 *ADD HYD      NHYDsum=["SN_CO" ], NHYDs to add=["N_TO"+"P1-OVF"+"MS_P1" ]
4010 *%-----|-----|
4011 *SAVE HYD      NHYD=["SN_CO" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
4012 *              HYD_COMMENT=[ "Total Flows at Corrigan Drain" ]
4013 *%-----|-----|
4014 * -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"

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and its parameters remain the same.
4015 CONTINUOUS STANDHYD NHYD=["corr1"], DT=[1]min, AREA=[15.87](ha),
4016 XI MP=[0.63], TI MP=[0.63], DWF=[0](cms), LOSS=[2],
4017 SCS curve number CN=[77],
4018 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4019 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4020 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4021 LGI=[325.27](m), MNI=[0.013], SCI=[0](min),
4022 Continuous simulation parameters:
4023 IaRECper=[4](hrs), IaRECImp=[4](hrs),
4024 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4025 InterEventTime=[18](hrs), END=-1
4026 *%-----|-----|
4027 * -JFSA 2021-02-23 add DUALHYD for "corr1". "corr1" DUALHYD Parameters are the
same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to "corr1".
4028 * At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for
Al-Corrig
4029 COMPUTE DUALHYD NHYDin=["corr1"], CINLET=[1.818](cms), NINLET=[1],
4030 MjNHYD=["corr1-M"]
4031 MnNHYD=["corr1-MN"]
4032 TMSTO=[924](cu-m)
4033 *%-----|-----|
4034 * -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
is called "corr2" and its parameters remain the same.
4035 CONTINUOUS NASHYD NHYD=["corr2"], DT=[1]min, AREA=[12.47](ha),
4036 DWF=[0](cms), CN C=[77], IA=[4.67](mm),
4037 N=[3], TP=[1.10]hrs,
4038 Continuous simulation parameters:
4039 IaRECper=[4](hrs),
4040 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4041 InterEventTime=[12](hrs)
4042 Baseflow simulation parameters:
4043 BaseFlowOption=[1],
4044 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4045 VHydCond=[0.055](mm/hr), END=-1
4046 *%-----|-----|
4047 * -JFSA 2021-01-19 change Al-Corrig to be developed as per geottawa website and
apply the parameters of A2, the nearest sub-catchment to Al-Corrig, LGI is calculated
based on Al-Corrig area
4048 * -JFSA 2021-01-19 update all Corrigan areas based on GIS measurements, and keep
LGI as it is from Corrigan Report, IBI Group, 2008 because LGI calculated is less than
LGI from the Corrigan Report
4049 CONTINUOUS STANDHYD NHYD=["Al-Corrig"], DT=[1]min, AREA=[15.75](ha),
4050 XI MP=[0.42], TI MP=[0.52], DWF=[0](cms), LOSS=[2],
4051 SCS curve number CN=[75],
4052 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4053 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4054 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4055 LGI=[324.037](m), MNI=[0.013], SCI=[0](min),
4056 Continuous simulation parameters:
4057 IaRECper=[4](hrs), IaRECImp=[4](hrs),
4058 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4059 InterEventTime=[18](hrs), END=-1
4060 *
4061 * -JFSA 2021-01-25 add DUALHYD for Al-Corrig. Al-Corrig DUALHYD Parameters are the
same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to Al-Corrig.
4062 * At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for
Al-Corrig
4063 COMPUTE DUALHYD NHYDin=["Al-Corrig"], CINLET=[1.818](cms), NINLET=[1],
4064 MjNHYD=["Al-M"]
4065 MnNHYD=["Al-MN"]
4066 TMSTO=[924](cu-m)
4067 *%-----|-----|
4068 *CONTINUOUS NASHYD NHYD=["Al-Corrig"], DT=[1]min, AREA=[15.75](ha),
4069 * DWF=[0](cms), CN C=[66], IA=[2.5](mm),
4070 * N=[3.0], TP=[0.36]hrs,

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4071 *          Continuous simulation parameters:
4072 *          IaRECper=[ 4]( hrs ),
4073 *          SMN=[ -1]( mm),   SMAX=[ -1]( mm),   SK=[ 0.010]/( mm),
4074 *          InterEventTime=[ 12]( hrs)
4075 *          Baseflow simulation parameters:
4076 *          BaseFlowOption=[ 1] ,
4077 *          InitGWResVol =[ 50]( mm),   GWResK=[ 0.96]( mm/ day/ mm)
4078 *          VHydCond=[ 0.055]( mm/ hr),   END=- 1
4079 *%-----|-----
4080 CONTINUOUS NASHYD  NHYD=[ "B1" ], DT=[ 1] mi n, AREA=[ 2.77]( ha),
4081 DWF=[ 0]( cms),   CN C=[ 56], IA=[ 2.5]( mm),
4082 N=[ 3.0], TP=[ 0.23] hr s,
4083 Continuous simulation parameters:
4084 IaRECper=[ 4]( hrs),
4085 SMN=[ -1]( mm),   SMAX=[ -1]( mm),   SK=[ 0.010]/( mm),
4086 InterEventTime=[ 12]( hrs)
4087 Baseflow simulation parameters:
4088 BaseFlowOption=[ 1] ,
4089 InitGWResVol =[ 50]( mm),   GWResK=[ 0.96]( mm/ day/ mm)
4090 VHydCond=[ 0.055]( mm/ hr),   END=- 1
4091 *%-----|-----
4092 CONTINUOUS STANDHYD  NHYD=[ "A4" ], DT=[ 1] mi n, AREA=[ 1.27]( ha),
4093 XI MP=[ 0.65], TI MP=[ 0.65], DWF=[ 0]( cms), LOSS=[ 2],
4094 SCS curve number CN=[ 75],
4095 Pervious surfaces: IAper=[ 4.67]( mm), SLPP=[ 1]( %),
4096 LGP=[ 40]( m), MNP=[ 0.25], SCP=[ 0]( mi n),
4097 Impervious surfaces: IAi mp=[ 1.57]( mm), SLPI=[ 1]( %),
4098 LGI=[ 253]( m), MNI =[ 0.013], SCI=[ 0]( mi n),
4099 Continuous simulation parameters:
4100 IaRECper=[ 4]( hrs),   IaRECI mp=[ 4]( hr s),
4101 SMN=[ -1]( mm),   SMAX=[ -1]( mm), SK=[ 0.010]/( mm),
4102 InterEventTime=[ 18]( hr s),   END=- 1
4103 *%-----|-----
4104 COMPUTE DUALHYD  NHYDin=[ "A4" ], CINLET=[ 0.405]( cms), NI NLET=[ 1],
4105 Maj NHYD=[ "A4- M" ]
4106 MnNHYD=[ "A4- MN" ]
4107 TMI STO=[ 68]( cu- m)
4108 *%-----|-----
4109 ADD HYD  NHYDsum=[ "MH101" ], NHYDs to
add=[ "A1- M" +"A1- MN" +"corr1- M" +"corr1- MN" +"corr2" +"B1" +"A4- MN" ]
4110 *%-----|-----
4111 SAVE HYD  NHYD=[ "MH101" ], # OF PCYCLES=[ -1], ICASEsh=[ 1]
4112 HYD_COMMENT=[ "Total Flows at MH101" ]
4113 *%-----|-----
4114 ROUTE PIPE  PTYPE=[ 1] circ, NHYDout=[ "101- 102" ], RNUMBER=[ 1.0], PDI AM=[ 1050]( mm),
4115 PLNGTH=[ 368]( m), PROUGH=[ 0.013], PSLOPE=[ 0.0054]( m/ m),
NHYDin=[ "MH101" ], RDT=[ 1]
4116 *%-----|-----
4117 * -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
major system from A2 can be added to Todd
4118 *CONTINUOUS STANDHYD  NHYD=[ "A2" ], DT=[ 1] mi n, AREA=[ 25.5]( ha),
4119 * XI MP=[ 0.42], TI MP=[ 0.52], DWF=[ 0]( cms), LOSS=[ 2],
4120 * SCS curve number CN=[ 75],
4121 * Pervious surfaces: IAper=[ 4.67]( mm), SLPP=[ 1]( %),
4122 * LGP=[ 40]( m), MNP=[ 0.25], SCP=[ 0]( mi n),
4123 * Impervious surfaces: IAi mp=[ 1.57]( mm), SLPI=[ 1]( %),
4124 * LGI=[ 566]( m), MNI =[ 0.013], SCI=[ 0]( mi n),
4125 * Continuous simulation parameters:
4126 * IaRECper=[ 4]( hrs),   IaRECI mp=[ 4]( hr s),
4127 * SMN=[ -1]( mm),   SMAX=[ -1]( mm), SK=[ 0.010]/( mm),
4128 * InterEventTime=[ 18]( hr s),   END=- 1
4129 *%-----|-----
4130 *COMPUTE DUALHYD  NHYDin=[ "A2" ], CINLET=[ 1.818]( cms), NI NLET=[ 1],
4131 * Maj NHYD=[ "A2- M" ]
4132 * MnNHYD=[ "A2- MN" ]
4133 * TMI STO=[ 924]( cu- m)

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4134 *%-----|-----|
4135 ADD HYD          NHYDs um=[ "MH102" ], NHYDs to add=[ "A2-MN"+"101-102" ]
4136 *%-----|-----|
4137 SAVE HYD         NHYD=[ "MH102" ], # OF PCYCLES=[ -1 ], I CASEs h=[ 1 ]
4138 HYD_COMMENT=[ "Total Flows at MH102" ]
4139 *%-----|-----|
4140 CONTINUOUS STANDHYD NHYD=[ "A5" ], DT=[ 1 ] mi n, AREA=[ 1.6 ] (ha),
4141 XI MP=[ 0.71 ], TI MP=[ 0.71 ], DWF=[ 0 ] (cms), LOSS=[ 2 ],
4142 SCS curve number CN=[ 75 ],
4143 Pervious surfaces: I Aper=[ 4.67 ] (mm), SLPP=[ 1 ] ( % ),
4144                    LGP=[ 40 ] (m), MNP=[ 0.25 ], SCP=[ 0 ] (mi n),
4145 ImperVIOUS surfaces: I Ai mp=[ 1.57 ] (mm), SLPI=[ 1 ] ( % ),
4146                    LGI=[ 300 ] (m), MNI=[ 0.013 ], SCI=[ 0 ] (mi n),
4147 Continuous simulation parameters:
4148 I a RE Cper=[ 4 ] (hrs), I a RE Ci mp=[ 4 ] (hrs),
4149 SM N=[ -1 ] (mm), SMAX=[ -1 ] (mm), SK=[ 0.010 ] / (mm),
4150 InterEvent Ti me=[ 18 ] (hrs), END=- 1
4151 *%-----|-----|
4152 ADD HYD          NHYDs um=[ "A5T" ], NHYDs to add=[ "A4-M"+"A5" ]
4153 *%-----|-----|
4154 COMPUTE DUALHYD  NHYDi n=[ "A5T" ], CI NLET=[ 0.357 ] (cms), NI NLET=[ 1 ],
4155 M aj NHYD=[ "A5-M" ]
4156 M nNHYD=[ "A5-MN" ]
4157 TM STO=[ 60 ] (cu-m)
4158 *%-----|-----|
4159 * -JFSA Jan. 2021, A3 is a part of Todd so it is removed
4160 * -JFSA Jan. 2021, "A2-M" added to "Todd"
4161 *CONTINUOUS STANDHYD NHYD=[ "A3" ], DT=[ 1 ] mi n, AREA=[ 18.4 ] (ha),
4162 * XI MP=[ 0.58 ], TI MP=[ 0.65 ], DWF=[ 0 ] (cms), LOSS=[ 2 ],
4163 * SCS curve number CN=[ 75 ],
4164 * Pervious surfaces: I Aper=[ 4.67 ] (mm), SLPP=[ 1 ] ( % ),
4165 *                    LGP=[ 40 ] (m), MNP=[ 0.25 ], SCP=[ 0 ] (mi n),
4166 * ImperVIOUS surfaces: I Ai mp=[ 1.57 ] (mm), SLPI=[ 1 ] ( % ),
4167 *                    LGI=[ 450 ] (m), MNI=[ 0.013 ], SCI=[ 0 ] (mi n),
4168 * Continuous simulation parameters:
4169 * I a RE Cper=[ 4 ] (hrs), I a RE Ci mp=[ 4 ] (hrs),
4170 * SM N=[ -1 ] (mm), SMAX=[ -1 ] (mm), SK=[ 0.010 ] / (mm),
4171 * InterEvent Ti me=[ 18 ] (hrs), END=- 1
4172 *%-----|-----|
4173 *ADD HYD          NHYDs um=[ "A3-A2M" ], NHYDs to add=[ "A2-M"+"A3" ]
4174 *%-----|-----|
4175 *COMPUTE DUALHYD  NHYDi n=[ "A3-A2M" ], CI NLET=[ 2.208 ] (cms), NI NLET=[ 1 ],
4176 * M aj NHYD=[ "A3R-M" ]
4177 * M nNHYD=[ "A3R-MN" ]
4178 * TM STO=[ 908 ] (cu-m)
4179 *%-----|-----|
4180 ROUTE PIPE       PTYPE=[ 1 ] circ, NHYDout=[ "102-103" ], RNUMBER=[ 1.0 ], PDI AM=[ 1500 ] (mm),
4181 PLNGTH=[ 504 ] (m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0028 ] (m/m),
NHYDi n=[ "MH102" ], RDT=[ 1 ]
4182 *%-----|-----|
4183 ADD HYD          NHYDs um=[ "MH103" ], NHYDs to add=[ "102-103"+"A5-MN" ]
4184 *%-----|-----|
4185 SAVE HYD         NHYD=[ "MH103" ], # OF PCYCLES=[ -1 ], I CASEs h=[ 1 ]
4186 HYD_COMMENT=[ "Total Flows at MH103" ]
4187 *%-----|-----|
4188 ROUTE PIPE       PTYPE=[ 1 ] circ, NHYDout=[ "103-104" ], RNUMBER=[ 1.0 ], PDI AM=[ 1650 ] (mm),
4189 PLNGTH=[ 438 ] (m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0046 ] (m/m),
NHYDi n=[ "MH103" ], RDT=[ 1 ]
4190 *%-----|-----|
4191 CONTINUOUS STANDHYD NHYD=[ "A6" ], DT=[ 1 ] mi n, AREA=[ 1.56 ] (ha),
4192 XI MP=[ 0.71 ], TI MP=[ 0.71 ], DWF=[ 0 ] (cms), LOSS=[ 2 ],
4193 SCS curve number CN=[ 75 ],
4194 Pervious surfaces: I Aper=[ 4.67 ] (mm), SLPP=[ 1 ] ( % ),
4195                    LGP=[ 40 ] (m), MNP=[ 0.25 ], SCP=[ 0 ] (mi n),
4196 ImperVIOUS surfaces: I Ai mp=[ 1.57 ] (mm), SLPI=[ 1 ] ( % ),
4197                    LGI=[ 280 ] (m), MNI=[ 0.013 ], SCI=[ 0 ] (mi n),

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4198 Continuous simulation parameters:
4199 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4200 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4201 InterEventTime=[ 18](hrs), END=- 1
4202 *%-----|
4203 ADD HYD NHYDsum=[ "A6T" ], NHYDs to add=[ "A5-M" +"A6" ]
4204 *%-----|
4205 COMPUTE DUALHYD NHYDin=[ "A6T" ], CINLET=[ 0.357](cms), NINLET=[ 1],
4206 MjNHYD=[ "A6-M" ]
4207 MnNHYD=[ "A6-MN" ]
4208 TMSSTO=[ 60](cu-m)
4209 *%-----|
4210 * -JFSA Jan. 2021, A7-corrig is a part of Todd so it is removed
4211 *CONTINUOUS STANDHYD NHYD=[ "A7-corrig" ], DT=[ 1]min, AREA=[ 11.8](ha),
4212 * XIMP=[ 0.41], TIMP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4213 * SCS curve number CN=[ 75],
4214 * Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4215 * LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4216 * Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4217 * LGI=[ 438](m), MNI=[ 0.013], SCI=[ 0](min),
4218 * Continuous simulation parameters:
4219 * IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4220 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4221 * InterEventTime=[ 18](hrs), END=- 1
4222 *%-----|
4223 *ADD HYD NHYDsum=[ "A7-A3RM" ], NHYDs to add=[ "A3R-M" +"A7-corrig" ]
4224 *%-----|
4225 *COMPUTE DUALHYD NHYDin=[ "A7-A3RM" ], CINLET=[ 1.003](cms), NINLET=[ 1],
4226 * MjNHYD=[ "A7R-M" ]
4227 * MnNHYD=[ "A7R-MN" ]
4228 * TMSSTO=[ 496](cu-m)
4229 *%-----|
4230 ADD HYD NHYDsum=[ "MH104" ], NHYDs to add=[ "A6-MN" +"103-104" +"TODD_Min" ]
4231 *%-----|
4232 SAVE HYD NHYD=[ "MH104" ], # OF PCYCLES=[ -1], ICASEsh=[ 1]
4233 HYD_COMMENT=[ "Total Flows at MH104" ]
4234 *%-----|
4235 CONTINUOUS STANDHYD NHYD=[ "B2" ], DT=[ 1]min, AREA=[ 12.31](ha),
4236 XIMP=[ 0.41], TIMP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4237 SCS curve number CN=[ 75],
4238 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4239 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4240 Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4241 LGI=[ 417](m), MNI=[ 0.013], SCI=[ 0](min),
4242 Continuous simulation parameters:
4243 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4244 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4245 InterEventTime=[ 18](hrs), END=- 1
4246 *%-----|
4247 COMPUTE DUALHYD NHYDin=[ "B2" ], CINLET=[ 1.029](cms), NINLET=[ 1],
4248 MjNHYD=[ "B2-M" ]
4249 MnNHYD=[ "B2-MN" ]
4250 TMSSTO=[ 508](cu-m)
4251 *%-----|
4252 ROUTE PIPE PTYPE=[ 1]circ, NHYDout=[ "315-333" ], RNUMBER=[ 1.0], PDIAM=[ 1200](mm),
4253 PLNGTH=[ 254](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
NHYDin=[ "B2-MN" ], RDT=[ 1]
4254 *%-----|
4255 CONTINUOUS STANDHYD NHYD=[ "B3" ], DT=[ 1]min, AREA=[ 5.59](ha),
4256 XIMP=[ 0.41], TIMP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4257 SCS curve number CN=[ 75],
4258 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4259 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4260 Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4261 LGI=[ 345](m), MNI=[ 0.013], SCI=[ 0](min),
4262 Continuous simulation parameters:

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4263 IaRECper=[ 4](hr s), IaRECImp=[ 4](hr s),
4264 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4265 InterEventTime=[ 18](hr s), END=- 1
4266 *%-----|-----|
4267 COMPUTE DUALHYD NHYDin=[" B3"], CI NLET=[ 0.459](cms), NI NLET=[ 1],
4268 Mj NHYD=[" B3- M"]
4269 MnNHYD=[" B3- MN"]
4270 TM STO=[ 227](cu- m)
4271 *%-----|-----|
4272 ADD HYD NHYDs um=[" MH333"], NHYDs to add=[" B3- MN"+" 315- 333"]
4273 *%-----|-----|
4274 SAVE HYD NHYD=[" MH333"], # OF PCYCLES=[ -1], I CASEs h=[ 1]
4275 HYD_COMMENT=[" Total Fl ows at MH333"]
4276 *%-----|-----|
4277 ROUTE PI PE PTYPE=[ 1]circ, NHYDout=[" 333- 335"], RNUMBER=[ 1.0], PDI AM=[ 1200](mm),
4278 PLNGTH=[ 251](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
NHYDin=[" MH333"], RDT=[ 1]
4279 *%-----|-----|
4280 ROUTE PI PE PTYPE=[ 1]circ, NHYDout=[" 335- 338"], RNUMBER=[ 1.0], PDI AM=[ 1200](mm),
4281 PLNGTH=[ 185](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
NHYDin=[" 333- 335"], RDT=[ 1]
4282 *%-----|-----|
4283 ROUTE PI PE PTYPE=[ 1]circ, NHYDout=[" 338- 340"], RNUMBER=[ 1.0], PDI AM=[ 1350](mm),
4284 PLNGTH=[ 233](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
NHYDin=[" 335- 338"], RDT=[ 1]
4285 *%-----|-----|
4286 CONTINUOUS STANDHYD NHYD=[" B4"], DT=[ 1]min, AREA=[ 7.6](ha),
4287 XI MP=[ 0.41], TI MP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4288 SCS curve number CN=[ 75],
4289 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4290 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4291 ImperVIOUS surfaces: IAi mp=[ 1.57](mm), SLPI =[ 1](%),
4292 LGI =[ 388](m), MNI =[ 0.013], SCI =[ 0](min),
4293 Continuous simulation parameters:
4294 IaRECper=[ 4](hr s), IaRECImp=[ 4](hr s),
4295 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4296 InterEventTime=[ 18](hr s), END=- 1
4297 *%-----|-----|
4298 COMPUTE DUALHYD NHYDin=[" B4"], CI NLET=[ 0.655](cms), NI NLET=[ 1],
4299 Mj NHYD=[" B4- M"]
4300 MnNHYD=[" B4- MN"]
4301 TM STO=[ 323](cu- m)
4302 *%-----|-----|
4303 ADD HYD NHYDs um=[" MH340"], NHYDs to add=[" 338- 340"+" B4- MN"]
4304 *%-----|-----|
4305 SAVE HYD NHYD=[" MH340"], # OF PCYCLES=[ -1], I CASEs h=[ 1]
4306 HYD_COMMENT=[" Total Fl ows at MH340"]
4307 *%-----|-----|
4308 ROUTE PI PE PTYPE=[ 1]circ, NHYDout=[" 340- 104"], RNUMBER=[ 1.0], PDI AM=[ 1650](mm),
4309 PLNGTH=[ 240](m), PROUGH=[ 0.013], PSLOPE=[ 0.0015](m/m),
NHYDin=[" MH340"], RDT=[ 1]
4310 *%-----|-----|
4311 ADD HYD NHYDs um=[" MH104T"], NHYDs to add=[" 340- 104"+" MH104"]
4312 *%-----|-----|
4313 ROUTE PI PE PTYPE=[ 2]rect, NHYDout=[" 104- 105"], RNUMBER=[ 1.0],
4314 PW DTH=[ 2400](mm) by PHEI GHT=[ 2100](mm),
PLNGTH=[ 380](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
NHYDin=[" MH104T"], RDT=[ 1]
4315 *%-----|-----|
4316 CONTINUOUS STANDHYD NHYD=[" B5"], DT=[ 1]min, AREA=[ 2.2](ha),
4317 XI MP=[ 0.57], TI MP=[ 0.57], DWF=[ 0](cms), LOSS=[ 2],
4318 SCS curve number CN=[ 75],
4319 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4320 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4321 ImperVIOUS surfaces: IAi mp=[ 1.57](mm), SLPI =[ 1](%),

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4322             LGI=[ 187](m), MNI=[ 0.013], SCI=[ 0](min),
4323 Continuous simulation parameters:
4324 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4325 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4326 InterEventTime=[ 18](hrs), END=- 1
4327 *%-----|
4328 COMPUTE DUALHYD NHYDin=[ "B5" ], CINLET=[ 0.260](cms), NINLET=[ 1],
4329 MijNHYD=[ "B5-M" ]
4330 MnNHYD=[ "B5-MN" ]
4331 TMSSTO=[ 250](cu-m)
4332 *%-----|
4333 CONTINUOUS STANDHYD NHYD=[ "A8" ], DT=[ 1]min, AREA=[ 0.96](ha),
4334 XI MP=[ 0.71], TIMP=[ 0.71], DWF=[ 0](cms), LOSS=[ 2],
4335 SCS curve number CN=[ 75],
4336 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4337 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4338 Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4339 LGI=[ 186](m), MNI=[ 0.013], SCI=[ 0](min),
4340 Continuous simulation parameters:
4341 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4342 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4343 InterEventTime=[ 18](hrs), END=- 1
4344 *%-----|
4345 ADD HYD NHYDs um=[ "A8T" ], NHYDs to add=[ "A6-M" + "A8" ]
4346 *%-----|
4347 COMPUTE DUALHYD NHYDin=[ "A8T" ], CINLET=[ 0.238](cms), NINLET=[ 1],
4348 MijNHYD=[ "A8-M" ]
4349 MnNHYD=[ "A8-MN" ]
4350 TMSSTO=[ 40](cu-m)
4351 *%-----|
4352 ADD HYD NHYDs um=[ "MH105" ], NHYDs to
4353 add=[ "104-105" + "B5-MN" + "A8-MN" + "TODD_MN3j" ]
4354 *%-----|
4355 SAVE HYD NHYD=[ "MH105" ], # OF PCYCLES=[ -1], ICASEsh=[ 1]
4356 HYD_COMMENT=[ "Total Flows at MH105" ]
4357 *%-----|
4358 DI VERT HYD NHYDin=[ "A8-M" ] NIDout=[ 2]max five,
4359 outflow hydrographs (NHYDs)=[ "A8-M-JR" "A8-M-B6" ]
4360 flow distribution table: (modify as necessary)
4361 Note: all flows are in (cms)
4362 QIDi + QIDi = QTOTAL
4363 [ 0 + 0 = 0 ]
4364 [ 50 + 50 = 100 ] end
4365 *%-----|
4366 DI VERT HYD NHYDin=[ "MH105" ] NIDout=[ 2]max five,
4367 outflow hydrographs (NHYDs)=[ "MH105-JR" "MH105-B6" ]
4368 flow distribution table: (modify as necessary)
4369 Note: all flows are in (cms)
4370 QIDi + QIDi = QTOTAL
4371 [ 0 + 0 = 0 ]
4372 [ 0 + 3.0 = 3.0 ]
4373 [ 96.9+ 3.1 = 100 ] end
4374 *%-----|
4375 CONTINUOUS STANDHYD NHYD=[ "B7" ], DT=[ 1]min, AREA=[ 7.19](ha),
4376 XI MP=[ 0.41], TIMP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4377 SCS curve number CN=[ 75],
4378 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4379 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4380 Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4381 LGI=[ 211](m), MNI=[ 0.013], SCI=[ 0](min),
4382 Continuous simulation parameters:
4383 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4384 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4385 InterEventTime=[ 18](hrs), END=- 1

```



```

4385 *%-----|-----|
4386 ADD HYD NHYDs um=[ " B7- B4M " ], NHYDs to add=[ " B4- M " + " B7 " ]
4387 *%-----|-----|
4388 COMPUTE DUALHYD NHYD i n=[ " B7- B4M " ], CI NLET=[ 0. 629 ] ( c m s ), NI NLET=[ 1 ],
4389 M a j NHYD=[ " B7R- M " ]
4390 M nNHYD=[ " B7R- MN " ]
4391 T M S T O=[ 311 ] ( c u- m )
4392 *%-----|-----|
4393 ROUTE PI PE PTYPE=[ 1 ] c i r c, NHYD out=[ " 360- 106A " ], RNUMBER=[ 1. 0 ], PDI AM=[ 1050 ] ( m m ),
4394 PLNGTH=[ 167 ] ( m ), PROUGH=[ 0. 013 ], PSLOPE=[ 0. 001 ] ( m / m ),
NHYD i n=[ " B7R- MN " ], RDT=[ 1 ]
4395 *%-----|-----|
4396 * -JFSA 2021-01-19 change B6 to be developed as per geottawa website and apply the
parameters of A7, the nearest sub-catchment to B6, LGI is calculated based on B6 area
CONTINUOUS STANDHYD NHYD=[ " B6 " ], DT=[ 1 ] m i n, AREA=[ 3. 29 ] ( h a ),
4397 XI MP=[ 0. 41 ], TI MP=[ 0. 54 ], DWF=[ 0 ] ( c m s ), LOSS=[ 2 ],
4398 SCS curve number CN=[ 75 ],
4400 P e r v i o u s s u r f a c e s : I A p e r=[ 4. 67 ] ( m m ), S L P P=[ 1 ] ( % ),
4401 L G P=[ 40 ] ( m ), M N P=[ 0. 25 ], S C P=[ 0 ] ( m i n ),
4402 I m p e r v i o u s s u r f a c e s : I A i m p=[ 1. 57 ] ( m m ), S L P I=[ 1 ] ( % ),
4403 L G I=[ 148. 099 ] ( m ), M N I=[ 0. 013 ], S C I=[ 0 ] ( m i n ),
4404 C o n t i n u o u s s i m u l a t i o n p a r a m e t e r s :
4405 I a R E C p e r=[ 4 ] ( h r s ), I a R E C i m p=[ 4 ] ( h r s ),
4406 S M N=[ - 1 ] ( m m ), S M A X=[ - 1 ] ( m m ), S K=[ 0. 010 ] / ( m m ),
4407 I n t e r E v e n t T i m e=[ 18 ] ( h r s ), E N D=- 1
4408 *%-----|-----|
4409 * -JFSA 2021-01-25 add B1 DUALHYD as per Corrigan Report, IBI Group, 2008
COMPUTE DUALHYD NHYD i n=[ " B6 " ], CI NLET=[ 0. 064 ] ( c m s ), NI NLET=[ 1 ],
4410 M a j NHYD=[ " B6- M " ]
4411 M nNHYD=[ " B6- MN " ]
4412 T M S T O=[ 5484 ] ( c u- m )
4413 *%-----|-----|
4414 *CONTINUOUS NASHYD NHYD=[ " B6 " ], DT=[ 1 ] m i n, AREA=[ 3. 29 ] ( h a ),
4415 DWF=[ 0 ] ( c m s ), C N C=[ 75 ], I A=[ 2. 5 ] ( m m ),
4416 N=[ 3. 0 ], T P=[ 0. 36 ] h r s,
4417 C o n t i n u o u s s i m u l a t i o n p a r a m e t e r s :
4418 I a R E C p e r=[ 4 ] ( h r s ),
4419 S M N=[ - 1 ] ( m m ), S M A X=[ - 1 ] ( m m ), S K=[ 0. 010 ] / ( m m ),
4420 I n t e r E v e n t T i m e=[ 12 ] ( h r s )
4421 B a s e f l o w s i m u l a t i o n p a r a m e t e r s :
4422 B a s e F l o w O p t i o n=[ 1 ],
4423 I n i t G W R e s V o l=[ 50 ] ( m m ), G W R e s K=[ 0. 96 ] ( m m / d a y / m m )
4424 V H y d C o n d=[ 0. 055 ] ( m m / h r ), E N D=- 1
4425 *%-----|-----|
4426 *% -EX-LAND is external land. It is a part of JOCKVA sub-catchment as per Corrigan
Report, IBI Group, 2008
CONTINUOUS STANDHYD NHYD=[ " EX- LAND " ], DT=[ 1 ] m i n, AREA=[ 32. 5 ] ( h a ),
4427 XI MP=[ 0. 50 ], TI MP=[ 0. 50 ], DWF=[ 0 ] ( c m s ), LOSS=[ 2 ],
4428 SCS curve number CN=[ 74 ],
4429 P e r v i o u s s u r f a c e s : I A p e r=[ 4. 67 ] ( m m ), S L P P=[ 1 ] ( % ),
4430 L G P=[ 40 ] ( m ), M N P=[ 0. 25 ], S C P=[ 0 ] ( m i n ),
4431 I m p e r v i o u s s u r f a c e s : I A i m p=[ 1. 57 ] ( m m ), S L P I=[ 1 ] ( % ),
4432 L G I=[ 465. 475 ] ( m ), M N I=[ 0. 013 ], S C I=[ 0 ] ( m i n ),
4433 C o n t i n u o u s s i m u l a t i o n p a r a m e t e r s :
4434 I a R E C p e r=[ 4 ] ( h r s ), I a R E C i m p=[ 4 ] ( h r s ),
4435 S M N=[ - 1 ] ( m m ), S M A X=[ - 1 ] ( m m ), S K=[ 0. 010 ] / ( m m ),
4436 I n t e r E v e n t T i m e=[ 18 ] ( h r s ), E N D=- 1
4437 *%-----|-----|
4438 COMPUTE DUALHYD NHYD i n=[ " EX- LAND " ], CI NLET=[ 2. 275 ] ( c m s ), NI NLET=[ 1 ],
4439 M a j NHYD=[ " EX- LAND- M " ]
4440 M nNHYD=[ " EX- LAND- MN " ]
4441 T M S T O=[ 1365 ] ( c u- m )
4442 *%-----|-----|
4443 ADD HYD NHYDs um=[ " B6- B7ExM " ], NHYDs to
4444 add=[ " B7R- M " + " EX- LAND- M " + " B5- M " + " B6- M " + " B6- MN " + " A8- M - B6 " ]
4445 *%-----|-----|
4446

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4447 COMPUTE DUALHYD      NHYDIn=[ " B6- B7ExM " ], CI NLET=[ 0. 064 ] ( cms ), NI NLET=[ 1 ],
4448                        Mj NHYD=[ " B6R- M " ]
4449                        MnNHYD=[ " B6R- MN " ]
4450                        TM STO=[ 5484 ] ( cu- m )
4451 *%-----|-----|
4452 ROUTE PIPE            PTYPE=[ 1 ] circ, NHYDout=[ " 105- 106A " ], RNUMBER=[ 1. 0 ], PDI AM=[ 1800 ] ( mm ),
4453                        PLNGTH=[ 208 ] ( m ), PROUGH=[ 0. 013 ], PSLOPE=[ 0. 001 ] ( m/ m ),
                        NHYDIn=[ " MHI 05- B6 " ], RDT=[ 1 ]
4454 *%-----|-----|
4455 ADD HYD              NHYDsum=[ " MHI 06A " ], NHYDs to
add=[ " 360- 106A " + " 105- 106A " + " B6R- MN " + " B6R- M " ]
4456 *%-----|-----|
4457 SAVE HYD             NHYD=[ " MHI 06A " ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
4458                        HYD_COMMENT=[ " Tot al Fl ows at MHI 06A " ]
4459 *%-----|-----|
4460 *%      -JFSA 2021-01-12 THE MANHOLE MHI06 is called MHI17/106 in Corrigan Report, IBI
Group, July 2008
4461 *%
4462 ROUTE PIPE            PTYPE=[ 1 ] circ, NHYDout=[ " 106A- 106 " ], RNUMBER=[ 1. 0 ], PDI AM=[ 1800 ] ( mm ),
4463                        PLNGTH=[ 190 ] ( m ), PROUGH=[ 0. 013 ], PSLOPE=[ 0. 001 ] ( m/ m ),
                        NHYDIn=[ " MHI 06A " ], RDT=[ 1 ]
4464 *%-----|-----|
4465 CONTINUOUS STANDHYD NHYD=[ " A9 " ], DT=[ 1 ] mi n, AREA=[ 2. 44 ] ( ha ),
4466                        XI MP=[ 0. 71 ], TI MP=[ 0. 71 ], DWF=[ 0 ] ( cms ), LOSS=[ 2 ],
4467                        SCS curve number CN=[ 75 ],
4468                        Pervious surfaces: I Aper=[ 4. 67 ] ( mm ), SLPP=[ 1 ] ( % ),
4469                        LGP=[ 40 ] ( m ), MNP=[ 0. 25 ], SCP=[ 0 ] ( mi n ),
4470                        Impervious surfaces: I Ai mp=[ 1. 57 ] ( mm ), SLPI=[ 1 ] ( % ),
4471                        LGI=[ 262 ] ( m ), MNI =[ 0. 013 ], SCI =[ 0 ] ( mi n ),
4472                        Continuous simulation parameters:
4473                        IaRECper=[ 4 ] ( hrs ), IaRECI mp=[ 4 ] ( hrs ),
4474                        SM N=[ - 1 ] ( mm ), SMAX=[ - 1 ] ( mm ), SK=[ 0. 010 ] / ( mm ),
4475                        InterEvent Ti me=[ 18 ] ( hrs ), END=- 1
4476 *%-----|-----|
4477 COMPUTE DUALHYD      NHYDIn=[ " A9 " ], CI NLET=[ 0. 547 ] ( cms ), NI NLET=[ 1 ],
4478                        Mj NHYD=[ " A9- M " ]
4479                        MnNHYD=[ " A9- MN " ]
4480                        TM STO=[ 0 ] ( cu- m )
4481 *%-----|-----|
4482 ADD HYD              NHYDsum=[ " MHI 06 " ], NHYDs to add=[ " 106A- 106 " + " A9- MN " ]
4483 *%-----|-----|
4484 SAVE HYD             NHYD=[ " MHI 06 " ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
4485                        HYD_COMMENT=[ " Tot al Fl ows at MHI 06 " ]
4486 *%-----|-----|
4487 *%      -JFSA 2021-01-12 THE MANHOLE MHI07 is called MHI18/107 in Corrigan Report, IBI
Group, July 2008
4488 *%
4489 ROUTE PIPE            PTYPE=[ 1 ] circ, NHYDout=[ " 106- 107 " ], RNUMBER=[ 1. 0 ], PDI AM=[ 1800 ] ( mm ),
4490                        PLNGTH=[ 122. 5 ] ( m ), PROUGH=[ 0. 013 ], PSLOPE=[ 0. 001 ] ( m/ m ),
                        NHYDIn=[ " MHI 06 " ], RDT=[ 1 ]
4491 *%-----|-----|
4492 CONTINUOUS STANDHYD NHYD=[ " A10 " ], DT=[ 1 ] mi n, AREA=[ 4. 14 ] ( ha ),
4493                        XI MP=[ 0. 35 ], TI MP=[ 0. 47 ], DWF=[ 0 ] ( cms ), LOSS=[ 2 ],
4494                        SCS curve number CN=[ 75 ],
4495                        Pervious surfaces: I Aper=[ 4. 67 ] ( mm ), SLPP=[ 1 ] ( % ),
4496                        LGP=[ 40 ] ( m ), MNP=[ 0. 25 ], SCP=[ 0 ] ( mi n ),
4497                        Impervious surfaces: I Ai mp=[ 1. 57 ] ( mm ), SLPI=[ 1 ] ( % ),
4498                        LGI=[ 183 ] ( m ), MNI =[ 0. 013 ], SCI =[ 0 ] ( mi n ),
4499                        Continuous simulation parameters:
4500                        IaRECper=[ 4 ] ( hrs ), IaRECI mp=[ 4 ] ( hrs ),
4501                        SM N=[ - 1 ] ( mm ), SMAX=[ - 1 ] ( mm ), SK=[ 0. 010 ] / ( mm ),
4502                        InterEvent Ti me=[ 18 ] ( hrs ), END=- 1
4503 *%-----|-----|
4504 COMPUTE DUALHYD      NHYDIn=[ " A10 " ], CI NLET=[ 0. 310 ] ( cms ), NI NLET=[ 1 ],
4505                        Mj NHYD=[ " A10- M " ]
4506                        MnNHYD=[ " A10- MN " ]

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4507          TMI STO=[ 228] (cu-m)
4508 *%-----|-----|
4509 CONTINUOUS STANDHYD NHYD=[ "A11"], DT=[ 1] min, AREA=[ 10.61] (ha),
4510          XI MP=[ 0.53], TI MP=[ 0.62], DWF=[ 0] (cms), LOSS=[ 2],
4511          SCS curve number CN=[ 75],
4512          Pervious surfaces: IAper=[ 4.67] (mm), SLPP=[ 1] (%),
4513          LGP=[ 40] (m), MNP=[ 0.25], SCP=[ 0] (min),
4514          Impervious surfaces: IAimp=[ 1.57] (mm), SLPI=[ 1] (%),
4515          LGI=[ 379] (m), MNI=[ 0.013], SCI=[ 0] (min),
4516          Continuous simulation parameters:
4517          IaRECper=[ 4] (hrs), IaRECImp=[ 4] (hrs),
4518          SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
4519          InterEventTime=[ 18] (hrs), END=- 1
4520 *%-----|-----|
4521 COMPUTE DUALHYD      NHYDin=[ "A11"], CILET=[ 0.993] (cms), NILET=[ 1],
4522          MajNHYD=[ "A11-M"]
4523          MnNHYD=[ "A11-MN"]
4524          TMI STO=[ 556] (cu-m)
4525 *%-----|-----|
4526 ADD HYD              NHYDsum=[ "MH107"], NHYDs to add=[ "106-107"+"A10-MN"+"A11-MN"]
4527 *%-----|-----|
4528 SAVE HYD             NHYD=[ "MH107"], # OF PCYCLES=[ -1], ICASEsh=[ 1]
4529          HYD_COMMENT=[ "Total Flows at MH107"]
4530 *%-----|-----|
4531 ROUTE PIPE           PTYPE=[ 1] circ, NHYDout=[ "107-119"], RNUMBER=[ 1.0], PDIAM=[ 1800] (mm),
4532          PLNGTH=[ 114] (m), PROUGH=[ 0.013], PSLOPE=[ 0.0012] (m/m),
4533          NHYDin=[ "MH107"], RDT=[ 1]
4534 *%-----|-----|
4534 *% -JFSA 2021-01-12 THE MANHOLE MH108 is called MH20/108 in Corrigan Report, IBI
4535          Group, July 2008
4536 *%
4537 ROUTE PIPE           PTYPE=[ 1] circ, NHYDout=[ "119-108"], RNUMBER=[ 1.0], PDIAM=[ 1800] (mm),
4538          PLNGTH=[ 65.8] (m), PROUGH=[ 0.013], PSLOPE=[ 0.0012] (m/m),
4539          NHYDin=[ "107-119"], RDT=[ 1]
4540 *%-----|-----|
4541 CONTINUOUS STANDHYD NHYD=[ "A12"], DT=[ 1] min, AREA=[ 12.29] (ha),
4542          XI MP=[ 0.41], TI MP=[ 0.54], DWF=[ 0] (cms), LOSS=[ 2],
4543          SCS curve number CN=[ 75],
4544          Pervious surfaces: IAper=[ 4.67] (mm), SLPP=[ 1] (%),
4545          LGP=[ 40] (m), MNP=[ 0.25], SCP=[ 0] (min),
4546          Impervious surfaces: IAimp=[ 1.57] (mm), SLPI=[ 1] (%),
4547          LGI=[ 183] (m), MNI=[ 0.013], SCI=[ 0] (min),
4548          Continuous simulation parameters:
4549          IaRECper=[ 4] (hrs), IaRECImp=[ 4] (hrs),
4550          SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
4551          InterEventTime=[ 18] (hrs), END=- 1
4552 *%-----|-----|
4553 COMPUTE DUALHYD      NHYDin=[ "A12"], CILET=[ 1.029] (cms), NILET=[ 1],
4554          MajNHYD=[ "A12-M"]
4555          MnNHYD=[ "A12-MN"]
4556          TMI STO=[ 672] (cu-m)
4557 *%-----|-----|
4558 CONTINUOUS STANDHYD NHYD=[ "A13"], DT=[ 1] min, AREA=[ 2.59] (ha),
4559          XI MP=[ 0.71], TI MP=[ 0.71], DWF=[ 0] (cms), LOSS=[ 2],
4560          SCS curve number CN=[ 75],
4561          Pervious surfaces: IAper=[ 4.67] (mm), SLPP=[ 1] (%),
4562          LGP=[ 40] (m), MNP=[ 0.25], SCP=[ 0] (min),
4563          Impervious surfaces: IAimp=[ 1.57] (mm), SLPI=[ 1] (%),
4564          LGI=[ 379] (m), MNI=[ 0.013], SCI=[ 0] (min),
4565          Continuous simulation parameters:
4566          IaRECper=[ 4] (hrs), IaRECImp=[ 4] (hrs),
4567          SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
4568          InterEventTime=[ 18] (hrs), END=- 1
4569 *%-----|-----|
4570 COMPUTE DUALHYD      NHYDin=[ "A13"], CILET=[ 0.571] (cms), NILET=[ 1],
4571          MajNHYD=[ "A13-M"]

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4570 M nNHYD=[ " A13- MN" ]
4571 TMJ STO=[ 0] ( cu- m)
4572 *%-----|-----
4573 * -JFSA 2021-01-22 add the Corrigan pond area ("Pond-Block")
4574 CONTINUOUS STANDHYD NHYD=[ " Pond- Block" ], DT=[ 1] mi n, AREA=[ 2.94] ( ha),
4575 XI MP=[ 0.415], TI MP=[ 0.415], DWF=[ 0] ( cms), LOSS=[ 2],
4576 SCS curve number CN=[ 75],
4577 Pervious surfaces: I Aper=[ 4.67] ( mm), SLPP=[ 1] ( %),
4578 LGP=[ 40] ( m), MNP=[ 0.25], SCP=[ 0] ( mi n),
4579 ImperVIOUS surfaces: I Ai mp=[ 1.57] ( mm), SLPI = [ 1] ( %),
4580 LGI = [ 183] ( m), MNI = [ 0.013], SCI = [ 0] ( mi n),
4581 Continuous simulation parameters:
4582 IaREcper=[ 4] ( hrs), IaRECi mp=[ 4] ( hrs),
4583 SM N=[ -1] ( mm), SMAX=[ -1] ( mm), SK=[ 0.010] / ( mm),
4584 InterEvent Time=[ 18] ( hrs), END=- 1
4585 *%-----|-----
4586 ADD HYD NHYDs um=[ " MHI08" ], NHYDs to add=[ " 119- 108" + " A13- MN" + " A12- MN" ]
4587 *%-----|-----
4588 SAVE HYD NHYD=[ " MHI08" ], # OF PCYCLES=[ -1], ICASEsh=[ 1]
4589 HYD_COMMENT=[ " Total Flows at MHI08" ]
4590 *%-----|-----
4591 ROUTE PIPE PTYPE=[ 1] circ, NHYDout=[ " 108- 116" ], RNUMBER=[ 1.0], PDI AM=[ 1800] ( mm),
4592 PLNGTH=[ 76.6] ( m), PROUGH=[ 0.013], PSLOPE=[ 0.0013] ( m/ m),
4593 NHYDi n=[ " MHI08" ], RDT=[ 1]
4594 *%-----|-----
4595 ROUTE PIPE PTYPE=[ 1] circ, NHYDout=[ " 116- corrig" ], RNUMBER=[ 1.0],
4596 PDI AM=[ 1800] ( mm),
4597 PLNGTH=[ 79.5] ( m), PROUGH=[ 0.013], PSLOPE=[ 0.0013] ( m/ m),
4598 NHYDi n=[ " 108- 116" ], RDT=[ 1]
4599 *%-----|-----
4600 ADD HYD NHYDs um=[ " Corrigan" ], NHYDs to add=[ " 116- corrig" + " Pond- Block" ]
4601 *%-----|-----
4602 SAVE HYD NHYD=[ " Corrigan" ], # OF PCYCLES=[ -1], ICASEsh=[ 1]
4603 HYD_COMMENT=[ " Total Flows at Corrigan Pond" ]
4604 *%-----|-----
4605 ROUTE RESERVOIR NHYDout = [ " Co- P" ], NHYDi n=[ " Corrigan" ],
4606 RDT=[ 1] ( mi n),
4607 TABLE of ( OUTFLOW STORAGE ) values
4608 ( cms ) - ( ha- m)
4609 [ 0.0 , 0.0 ]
4610 [ 0.015 , 0.04118]
4611 [ 0.030 , 0.08297]
4612 [ 0.045 , 0.12537]
4613 [ 0.060 , 0.16837]
4614 [ 0.075 , 0.21199]
4615 [ 0.090 , 0.27545]
4616 [ 0.105 , 0.34650]
4617 [ 0.120 , 0.42049]
4618 [ 0.135 , 0.50188]
4619 [ 0.186 , 0.60307]
4620 [ 2.110 , 0.79083]
4621 [ 5.874 , 1.00271]
4622 [ 11.395 , 1.29643]
4623 [ 18.770 , 1.62054]
4624 [ 28.143 , 1.97516]
4625 [ -1 , -1 ] (max twenty pts)
4626 NHYDovf=[ " Co- P- OVF" ]
4627 *%-----|-----
4628 ADD HYD NHYDs um=[ " corrig" ], NHYDs to
4629 add=[ " Co- P- OVF" + " Co- P" + " N_ TO" + " MHI05- JR" + " A8- M" + " JR" + " A9- M" + " A10- M" + " A11- M" + " A12- M" + " A
4630 13- M" ]
4631 *%-----|-----
4632 SAVE HYD NHYD=[ " corrig" ], # OF PCYCLES=[ -1], ICASEsh=[ 1]
4633 HYD_COMMENT=[ " Total Flows at Corrigan Pond" ]
4634 *%-----|-----
4635 *#*****

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4631  *#      Corrigan Pond 1
4632  *#      - Rating curve obtained from Barrhaven South M&S modeling
4633  *#      - Tributary Drainage Area to M&S Pond 1 = 145 ha
4634  *#*****
4635  *ROUTE RESERVOIR      NHYDout=[ "M&S_P1" ],  NHYDin=[ "CORRIG" ],
4636  *                      RDT=[ 1 ] ( mi n ),
4637  *                      TABLE of ( OUTFLOW STORAGE ) values
4638  *                      ( cms ) - ( ha - m )
4639  *                      [ 0.0 , 0.0 ]
4640  *                      [ 0.06 , 0.58 ]
4641  *                      [ -1 , -1 ] (max twenty pts)
4642  *                      NHYDovf=[ "P1-OVF" ]
4643  *%-----|-----|
4644  *ADD HYD              NHYDsum=[ "SN_CO" ], NHYDs to add=[ "N_TO"+"P1-OVF"+"M&S_P1" ]
4645  *%-----|-----|
4646  *SAVE HYD            NHYD=[ "SN_CO" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4647  *                      HYD_COMMENT=[ "Total Flows at Corrigan Drain" ]
4648  *%-----|-----|
4649  *#
4650  *# Hydrograph from Corrigan Drain routed to Jockvale Road
4651  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
4652  *#
4653  ROUTE CHANNEL      NHYDout=[ "N_M" ] , NHYDin=[ "corrig" ] ,
4654  RDT=[ 1 ] ( mi n ),
4655  CHLGTH=[ 580 ] ( m ),  CHSLOPE=[ 0.4448 ] ( % ),
4656  FPSLOPE=[ 0.4448 ] ( % ),
4657  SECNUM=[ 1.0 ],      NSEG=[ 3 ]
4658  ( SEGROUGH, SEGDI ST ( m ) ) =
4659  [ 0.075, -17.72
4660  -0.045, 17.72
4661  0.075, 80.62 ] NSEG times
4662  ( DI STANCE ( m ), ELEVATI ON ( m ) ) =
4663  [ -83.32, 90.00 ]
4664  [ -81.36, 89.50 ]
4665  [ -79.12, 89.00 ]
4666  [ -76.13, 88.50 ]
4667  [ -20.46, 88.00 ]
4668  [ -19.36, 87.50 ]
4669  [ -18.51, 87.00 ]
4670  [ -17.72, 86.50 ]
4671  [ -11.95, 85.24 ]
4672  [ -0.11, 85.12 ]
4673  [ 11.49, 85.20 ]
4674  [ 17.72, 86.50 ]
4675  [ 19.74, 87.00 ]
4676  [ 21.22, 87.50 ]
4677  [ 22.68, 88.00 ]
4678  [ 24.28, 88.50 ]
4679  [ 26.79, 89.00 ]
4680  [ 71.98, 90.00 ]
4681  [ 80.62, 90.50 ]
4682  *%-----|-----|
4683  *#*****
4684  *#      Catchment MLLS
4685  *#      - To SWM Facility north of the Jock
4686  *#      - Primarily residential development
4687  *#*****
4688  CONTINUOUS STANDHYD NHYD=[ "MLLS" ], DT=[ 1 ] mi n, AREA=[ 175.99 ] ( ha ),
4689  XI MP=[ 0.38 ], TI MP=[ 0.38 ], DWF=[ 0 ] ( cms ), LOSS=[ 2 ],
4690  SCS curve number CN=[ 74 ],
4691  Pervious surfaces: I A per=[ 4.67 ] ( mm ), SLPP=[ 1 ] ( % ),
4692  LGP=[ 40 ] ( m ), MNP=[ 0.25 ], SCP=[ 0 ] ( mi n ),
4693  Impervious surfaces: I A i mp=[ 1.57 ] ( mm ), SLPI=[ 1 ] ( % ),
4694  LGI=[ 1118.123 ] ( m ), MNI=[ 0.013 ], SCI=[ 0 ] ( mi n ),
4695  Continuous simulation parameters:
4696  I a REC per=[ 4 ] ( hr s ), I a REC i mp=[ 4 ] ( hr s ),

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4697 SMN=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
4698 Inter Event Time=[ 18 ] ( hr s ) , END=- 1
4699 *%-----|-----|
4700 *#*****|
4701 *# Chapman Mills SWM Pond
4702 *# - Rating curve obtained from CCL hydraulic modeling
4703 *#*****|
4704 ROUTE RESERVOIR NHYDout =[" M LL_P" ] , NHYDin =[" M LLS" ] ,
4705 RDT=[ 1 ] ( mi n ) ,
4706 TABLE of ( OUTFLOW STORAGE ) values
4707 ( cms ) - ( ha- m )
4708 [ 0. 0 , 0. 0 ]
4709 [ 0. 01 , 0. 01 ]
4710 [ 0. 05 , 0. 06 ]
4711 [ 0. 09 , 0. 11 ]
4712 [ 0. 13 , 0. 15 ]
4713 [ 0. 18 , 0. 19 ]
4714 [ 0. 28 , 0. 28 ]
4715 [ 0. 37 , 0. 34 ]
4716 [ 0. 45 , 0. 40 ]
4717 [ 0. 51 , 0. 44 ]
4718 [ 0. 56 , 0. 47 ]
4719 [ 0. 64 , 0. 52 ]
4720 [ 0. 76 , 0. 59 ]
4721 [ 0. 86 , 0. 65 ]
4722 [ 1. 09 , 0. 78 ]
4723 [ 1. 44 , 0. 96 ]
4724 [ 3. 18 , 1. 84 ]
4725 [ 4. 05 , 2. 31 ]
4726 [ - 1 , - 1 ] ( max t went y pts )
4727 NHYDovf =[" M L- OV" ]
4728 *%-----|-----|
4729 ADD HYD NHYDs um=[" SN_M " ] , NHYDs to add=[" N_M "+" M L- OV"+" M LL_P" ]
4730 *%-----|-----|
4731 SAVE HYD NHYD=[" SN_M " ] , # OF PCYCLES=[ - 1 ] , I CASEs h=[ 1 ]
4732 HYD_COMMENT=[" Tot al Fl ows at Jockval e Road" ]
4733 *%-----|-----|
4734 *#
4735 *# Hydrograph from Jockvale Road routed to Heart's Desire
4736 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 689
4737 *#
4738 ROUTE CHANNEL NHYDout =[" N_DE" ] , NHYDin =[" SN_M " ] ,
4739 RDT=[ 1 ] ( mi n ) ,
4740 CHLGTH=[ 1962 ] ( m ) , CHSLOPE=[ 0. 2227 ] ( % ) ,
4741 FPSLOPE=[ 0. 2227 ] ( % ) ,
4742 SECNUM=[ 1. 0 ] , NSEG=[ 3 ]
4743 ( SEGROUGH, SEGDI ST ( m ) ) =
4744 [ 0. 075 , - 17. 56
4745 - 0. 045 , 18. 27
4746 0. 075 , 32. 51 ] NSEG t i mes
4747 ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
4748 [ - 54. 07 , 85. 00 ]
4749 [ - 39. 43 , 84. 50 ]
4750 [ - 28. 30 , 84. 00 ]
4751 [ - 24. 12 , 83. 50 ]
4752 [ - 22. 30 , 83. 00 ]
4753 [ - 20. 55 , 82. 50 ]
4754 [ - 17. 56 , 82. 00 ]
4755 [ - 12. 63 , 81. 22 ]
4756 [ - 0. 11 , 80. 75 ]
4757 [ 11. 55 , 81. 22 ]
4758 [ 18. 27 , 82. 00 ]
4759 [ 19. 82 , 82. 50 ]
4760 [ 22. 48 , 83. 00 ]
4761 [ 27. 90 , 83. 50 ]
4762 [ 29. 31 , 84. 00 ]

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4763 [ 30.81, 84.50]
4764 [ 32.51, 85.00]
4765 *%-----|-----|
4766 *#*****|
4767 *# Catchment DESIRE
4768 *# - To Jock River (north of the Jock)
4769 *# - Rural-estate subdivision (Heart's Desire Community)
4770 *#*****|
4771 CONTINUOUS STANDHYD NHYD=["DESIRE"], DT=[ 1] mi n, AREA=[ 23.78](ha),
4772 XI MP=[ 0.25], TI MP=[ 0.25], DWF=[ 0](cms), LOSS=[ 2],
4773 SCS curve number CN=[ 77],
4774 Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
4775 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n),
4776 Impervious surfaces: I A i mp=[ 1.57](mm), SLPI=[ 1](%),
4777 LGI=[ 400](m), MNI=[ 0.013], SCI=[ 0](mi n),
4778 Continuous simulation parameters:
4779 I a REC per=[ 4](hrs), I a REC i mp=[ 4](hrs),
4780 SM N=[ - 1](mm), SMAX=[ - 1](mm), SK=[ 0.010]/(mm),
4781 Inter Event Ti me=[ 18](hrs), END=- 1
4782 *%-----|-----|
4783 *#*****|
4784 *# Catchment JOCKVA
4785 *# - To Jockvale SWM Facility
4786 *# - Residential development & golf course
4787 *# - JFSA 2021-01-11 update JOCKVA after updating CORRIG as per IBI GROUP, July 2008.
4788 *# JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two
areas JOCKVA and EX-LAND 32.5 ha as per IBI GROUP, July 2008.
4789 *#*****|
4790 CONTINUOUS STANDHYD NHYD=["JOCKVA"], DT=[ 1] mi n, AREA=[ 225.13](ha),
4791 XI MP=[ 0.50], TI MP=[ 0.50], DWF=[ 0](cms), LOSS=[ 2],
4792 SCS curve number CN=[ 74],
4793 Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
4794 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n),
4795 Impervious surfaces: I A i mp=[ 1.57](mm), SLPI=[ 1](%),
4796 LGI=[ 1310.55](m), MNI=[ 0.013], SCI=[ 0](mi n),
4797 Continuous simulation parameters:
4798 I a REC per=[ 4](hrs), I a REC i mp=[ 4](hrs),
4799 SM N=[ - 1](mm), SMAX=[ - 1](mm), SK=[ 0.010]/(mm),
4800 Inter Event Ti me=[ 18](hrs), END=- 1
4801 *%-----|-----|
4802 ADD HYD NHYDsum=["JOCKVA-TO"], NHYDsto
add=["EX-LAND-MN"+"JOCKVA"+"B2-M"+"B3-M"]
4803 *%-----|-----|
4804 SAVE HYD NHYD=["JOCKVA-TO"], # OF PCYCLES=[ - 1], I CASEs h=[ 1]
4805 HYD_COMMENT=["Total Flows at KB first pond"]
4806 *%-----|-----|
4807 *#*****|
4808 *# Jockvale SWM Facility
4809 *# - Rating curve obtained from Jockvale Servicing Study (CCL 1999)
4810 *#*****|
4811 ROUTE RESERVOIR NHYDout=["JOCK_P"], NHYDin=["JOCKVA-TO"],
4812 RDT=[ 1](mi n),
4813 TABLE of ( OUTFLOW STORAGE ) values
4814 (cms) - (ha-m)
4815 [ 0.0 , 0.0 ]
4816 [ 0.27 , 0.03]
4817 [ 0.28 , 0.55]
4818 [ 0.29 , 1.14]
4819 [ 0.30 , 1.80]
4820 [ 0.31 , 2.32]
4821 [ 1.12 , 2.87]
4822 [ 2.92 , 3.45]
4823 [ 4.64 , 4.07]
4824 [ 6.69 , 4.72]
4825 [ 9.02 , 5.39]
4826 [ 11.62 , 6.10]

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4827 [ 14.42 , 6.85]
4828 [ 17.45 , 7.62]
4829 [ 20.69 , 8.44]
4830 [ 24.08 , 9.28]
4831 [ 27.68 , 10.17]
4832 [ -1 , -1 ] (max twenty pts)
4833 NHYDovf=["JO-OVF"]
4834 *%-----|-----|
4835 ADD HYD NHYDs um=["SN_DE"], NHYDs to add=["N_DE"+"DESIRE"+"JO-OVF"+"JOCK_P"]
4836 *%-----|-----|
4837 SAVE HYD NHYD=["SN_DE"], # OF PCYCLES=[-1], ICASEsh=[1]
4838 HYD_COMMENT=["Total Flows at Heart's Desire"]
4839 *%-----|-----|
4840 *#
4841 *# Hydrograph from Heart's Desire routed to Rideau River
4842 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 0
4843 *#
4844 ROUTE CHANNEL NHYDout=["NI"], NHYDin=["SN_DE"],
4845 RDT=[1](min),
4846 CHLGTH=[563](m), CHSLOPE=[0.9668](%),
4847 FPSLOPE=[0.9668](%),
4848 SECNUM=[1.0], NSEG=[3]
4849 ( SEGROUGH, SEGDIST (m))=
4850 [0.075, -30.20
4851 -0.045, 30.20
4852 0.075, 48.48] NSEG times
4853 ( DISTANCE (m), ELEVATION (m))=
4854 [-98.46, 81.50]
4855 [-92.24, 81.00]
4856 [-86.88, 80.50]
4857 [-81.54, 80.00]
4858 [-74.36, 79.50]
4859 [-63.54, 79.00]
4860 [-39.23, 78.50]
4861 [-34.51, 78.00]
4862 [-33.01, 77.50]
4863 [-30.20, 77.00]
4864 [-13.42, 76.18]
4865 [-1.14, 76.09]
4866 [17.06, 76.18]
4867 [30.20, 77.00]
4868 [32.95, 77.50]
4869 [34.06, 78.00]
4870 [35.11, 78.50]
4871 [36.32, 79.00]
4872 [37.74, 79.50]
4873 [48.48, 81.50]
4874 *%-----|-----|
4875 *#*****
4876 *# Catchment S-2
4877 *# - To Jock River (north and south)
4878 *# - Undeveloped floodplain and river
4879 *#*****
4880 CONTINUOUS NASHYD NHYD=["S-2"], DT=[1]min, AREA=[102.94](ha),
4881 DWF=[0](cms), CN/C=[72], IA=[4.67](mm),
4882 N=[3], TP=[0.40]hrs,
4883 Continuous simulation parameters:
4884 IareCper=[4](hrs),
4885 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4886 InterEventTime=[12](hrs)
4887 Baseflow simulation parameters:
4888 BaseFlowOption=[1],
4889 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4890 VHydCond=[0.055](mm/hr), END=-1
4891 *%-----|-----|
4892 ADD HYD NHYDs um=["SN_NI"], NHYDs to add=["NI"+"S-2"]

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4893 *%-----|-----|
4894 SAVE HYD          NHYD=["SN_NI"], # OF PCYCLES=[-1], ICASEs h=[1]
4895                  HYD_COMMENT=["Total Flows at Rideau River"]
4896 *%-----|-----|
4897 *#####
4898 *% 5 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4899 START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[5]
4900 *%              ["C24SC005.stm"] <--storm filename, one per line for NSTORMtime
4901 *%-----|-----|
4902 *% 10 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4903 START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[10]
4904 *%              ["C24SC010.stm"] <--storm filename, one per line for NSTORMtime
4905 *%-----|-----|
4906 *% 25 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4907 START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[25]
4908 *%              ["C24SC025.stm"] <--storm filename, one per line for NSTORMtime
4909 *%-----|-----|
4910 *% 50 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4911 START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[50]
4912 *%              ["C24SC050.stm"] <--storm filename, one per line for NSTORMtime
4913 *%-----|-----|
4914 *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4915 *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4916 *%              ["100YC3H.STM"] <--storm filename, one per line for NSTORMtime
4917 *%-----|-----|
4918 *% 100 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4919 START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4920 *%              ["C24SC100.stm"] <--storm filename, one per line for NSTORMtime
4921 *%-----|-----|
4922 *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4923 *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4924 *%              ["C24SC100.stm"] <--storm filename, one per line for NSTORMtime
4925 *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[101]
4926 *%              ["A24SC100.stm"] <--storm filename, one per line for NSTORMtime
4927 *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[102]
4928 *%              ["A24SC100_60.stm"] <--storm filename, one per line for NSTORMtime
4929 FINISH
4930

```


Table with columns: ID, Name, Parameters, Date, Time, Location. Includes entries like 014979, 014980, 014981, etc., covering various computational nodes and system parameters.

Table with columns: ID, Name, Parameters, Date, Time, Location. Includes entries like 016845, 016846, 016847, etc., covering various computational nodes and system parameters.

```

018715 # - 2020-11-30 Increase Imp. based on P598(04) 11
018725 # - 2020-11-30 modify Tributary Drainage Area to = 146,015 ha based on P598(04) 11
018735 # - 2020-11-30 split TODD Drainage Area to SWWR, MNRR, POND and ALL
018745 # - 2020-11-30 add TODD_MNI as part of Clark's WCLAR.MI and remove it from Todd
018755 # - JFSA 2021-01-19 add TODD_MNI as part of Clark's WCLAR.MI and remove it from Todd
018765 # R0002:CO0276 ..... DfIn n-ID NND ..... AREHA-QPEAkm-TpeAkdTt-hh-mm-Rvmm-R-C- ..... DfWcm
018775 # CONTI NIXES STANDHYD 1.0 01: TODD.MN 2.10 1.179 Ndate 28:00 28.91 6.55 0000
018785 # [X]Mps: 53: TlMps: 57]
018795 # [LGSs: 2: Cn: 77.0]
018805 # [Pervious area: Iper: 4.67: SLPpl: 00: LEP: 40: MNP: 250: SCP: 0]
018815 # [Impervious area: IAm: 1.57: SLPpl: 00: LGA: 118: MN: 013: SCl: 0]
018825 # [IARECmp: 4.00: IARECmp: 4.00]
018835 # [SMN: 31.15: SMMV: 225.43: SKe: 010]
018845 # R0002:CO0284 ..... DfIn n-ID NND ..... AREHA-QPEAkm-TpeAkdTt-hh-mm-Rvmm-R-C- ..... DfWcm
018855 # CONTI NIXES STANDHYD 1.0 01: TODD.MN 12 0.011 Ndate 28:00 28.91 6.55 0000
018865 # [X]Mps: 53: TlMps: 57]
018875 # [LGSs: 2: Cn: 77.0]
018885 # [Pervious area: Iper: 4.67: SLPpl: 00: LEP: 40: MNP: 250: SCP: 0]
018895 # [Impervious area: IAm: 1.57: SLPpl: 00: LGA: 118: MN: 013: SCl: 0]
018905 # [IARECmp: 4.00: IARECmp: 4.00]
018915 # [SMN: 31.15: SMMV: 225.43: SKe: 010]
018925 # R0002:CO0278 ..... DfIn n-ID NND ..... AREHA-QPEAkm-TpeAkdTt-hh-mm-Rvmm-R-C- ..... DfWcm
018935 # CONTI NIXES STANDHYD 1.0 01: TODD.MN 30.23 2.154 Ndate 28:03 29.64 6.51 0000
018945 # [X]Mps: 52: TlMps: 64]
018955 # [LGSs: 2: Cn: 77.0]
018965 # [Pervious area: Iper: 4.67: SLPpl: 00: LEP: 40: MNP: 250: SCP: 0]
018975 # [Impervious area: IAm: 1.57: SLPpl: 00: LGA: 118: MN: 013: SCl: 0]
018985 # [IARECmp: 4.00: IARECmp: 4.00]
018995 # [SMN: 31.15: SMMV: 225.43: SKe: 010]
019005 # R0002:CO0280 ..... DfIn n-ID NND ..... AREHA-QPEAkm-TpeAkdTt-hh-mm-Rvmm-R-C- ..... DfWcm
019015 # CONTI NIXES STANDHYD 1.0 01: TODD.AL 112.91 6.553 Ndate 28:06 28.70 6.31 0000
019025 # [X]Mps: 52: TlMps: 57]
019035 # [LGSs: 2: Cn: 77.0]
019045 # [Pervious area: Iper: 4.67: SLPpl: 00: LEP: 40: MNP: 250: SCP: 0]
019055 # [Impervious area: IAm: 1.57: SLPpl: 00: LGA: 118: MN: 013: SCl: 0]
019065 # [IARECmp: 4.00: IARECmp: 4.00]
019075 # [SMN: 31.15: SMMV: 225.43: SKe: 010]
019085 # R0002:CO0282 ..... DfIn n-ID NND ..... AREHA-QPEAkm-TpeAkdTt-hh-mm-Rvmm-R-C- ..... DfWcm
019095 # CONTI NIXES STANDHYD 1.0 01: TODD.P 3.06 2.995 Ndate 28:00 31.76 6.98 0000
019105 # [X]Mps: 63: TlMps: 63]
019115 # [LGSs: 2: Cn: 77.0]
019125 # [Pervious area: Iper: 4.67: SLPpl: 00: LEP: 40: MNP: 250: SCP: 0]
019135 # [Impervious area: IAm: 1.57: SLPpl: 00: LGA: 143: MN: 013: SCl: 0]
019145 # [IARECmp: 4.00: IARECmp: 4.00]
019155 # [SMN: 31.15: SMMV: 225.43: SKe: 010]
019165 # 5 Year + 12% Capture
019175 # ROUTE RESERVOIR > 1.0 02: TODD.MN 30.23 2.154 Ndate 28:03 29.64 n/a 0000
019185 # out < 1.0 01: TODD.MN 30.23 2.154 Ndate 28:03 29.64 n/a 0000
019195 # overflow < 1.0 01: TODD.MN 30.23 2.154 Ndate 28:03 29.64 n/a 0000
019205 # [MS: 0.00: 6556.04: 04: 00: TotOfVol: 000000E+00: NOf: 0: TotDurOf: 0: hrs:]
019215 # 019225 # 5 Year + 12% Capture
019235 # R0002:CO0282 ..... DfIn n-ID NND ..... AREHA-QPEAkm-TpeAkdTt-hh-mm-Rvmm-R-C- ..... DfWcm
019245 # ROUTE RESERVOIR > 1.0 02: TODD.MN 30.23 2.154 Ndate 28:03 29.64 n/a 0000
019255 # out < 1.0 01: TODD.MN 30.23 2.154 Ndate 28:03 29.64 n/a 0000
019265 # overflow < 1.0 03: TODD.MN 30.23 2.154 Ndate 28:00 0.00 n/a 0000
019275 # [MS: 0.00: 6556.04: 04: 00: TotOfVol: 000000E+00: NOf: 0: TotDurOf: 0: hrs:]
019285 # R0002:CO0283 ..... DfIn n-ID NND ..... AREHA-QPEAkm-TpeAkdTt-hh-mm-Rvmm-R-C- ..... DfWcm
019295 # ROUTE RESERVOIR > 1.0 02: TODD.MN 12 0.010 Ndate 28:00 28.91 n/a 0000
019305 # out < 1.0 01: TODD.MN 12 0.010 Ndate 28:00 28.91 n/a 0000
019315 # overflow < 1.0 03: TODD.MN 12 0.010 Ndate 28:00 0.00 n/a 0000
019325 # [MS: 0.00: 6556.04: 04: 00: TotOfVol: 000000E+00: NOf: 0: TotDurOf: 0: hrs:]
019335 # R0002:CO0284 ..... DfIn n-ID NND ..... AREHA-QPEAkm-TpeAkdTt-hh-mm-Rvmm-R-C- ..... DfWcm
019345 # CONTI NIXES STANDHYD 1.0 01: AI: 25.50 1.427 Ndate 28:04 25.60 5.63 0000
019355 # [X]Mps: 42: TlMps: 52]
019365 # [LGSs: 2: Cn: 75.0]
019375 # [Pervious area: Iper: 4.67: SLPpl: 00: LEP: 40: MNP: 250: SCP: 0]
019385 # [Impervious area: IAm: 1.57: SLPpl: 00: LGA: 566: MN: 013: SCl: 0]
019395 # [IARECmp: 4.00: IARECmp: 4.00]
019405 # [SMN: 33.81: SMMV: 225.43: SKe: 010]
019415 # R0002:CO0311 ..... DfIn n-ID NND ..... AREHA-QPEAkm-TpeAkdTt-hh-mm-Rvmm-R-C- ..... DfWcm
019425 # COMPUTE DUALJHD 1.0 01: AI: 25.50 1.427 Ndate 28:04 25.60 n/a 0000
019435 # Mjr System 1.0 01: AI: 25.50 1.427 Ndate 28:04 25.60 n/a 0000
019445 # Mjr System 1.0 01: AI: 25.50 1.427 Ndate 28:04 25.60 n/a 0000
019455 # [MSystem: 000000E+00: TotOfVol: 000000E+00: NOf: 0: TotDurOf: 0: hrs:]
019465 # R0002:CO0317 ..... DfIn n-ID NND ..... AREHA-QPEAkm-TpeAkdTt-hh-mm-Rvmm-R-C- ..... DfWcm
019475 # ADD HYD 1.0 02: TODD.MN 2.10 1.179 Ndate 28:00 28.91 n/a 0000
019485 # + 1.0 02: TODD.MJ 0.00 0.000 Ndate 0.00 0.00 n/a 0000
019495 # + 1.0 02: TODD.MI 0.00 0.000 Ndate 0.00 0.00 n/a 0000
019505 # + 1.0 02: TODD.MK 12 0.010 Ndate 28:00 28.91 n/a 0000
019515 # + 1.0 02: TODD.ML 112.91 6.553 Ndate 28:06 28.70 n/a 0000
019525 # + 1.0 02: WCLAR.MI 1.77 1.41 Ndate 28:00 27.78 n/a 0000
019535 # [IARECmp: 4.00: IARECmp: 4.00]
019545 # R0002:CO0287 ..... DfIn n-ID NND ..... AREHA-QPEAkm-TpeAkdTt-hh-mm-Rvmm-R-C- ..... DfWcm
019555 # SAVE HYD 1.0 01: TODD 119.95 6.882 Ndate 28:05 28.77 n/a 0000
019565 # [Vms: 730: Dmax: 2.134]
019575 # [IARECmp: 4.00: IARECmp: 4.00]
019585 # remark: Total Flow at Todd Train
019595 # *****
019605 # *****
019615 # *****
019625 # *****
019635 # *****
019645 # *****
019655 # *****
019665 # *****
019675 # *****
019685 # *****
019695 # *****
019705 # *****
019715 # *****
019725 # *****
019735 # *****
019745 # *****
019755 # *****
019765 # *****
019775 # *****
019785 # *****
019795 # *****
019805 # *****
019815 # *****
019825 # *****
019835 # *****
019845 # *****
019855 # *****
019865 # *****
019875 # *****
019885 # *****
019895 # *****
019905 # *****
019915 # *****
019925 # *****
019935 # *****
019945 # *****
019955 # *****
019965 # *****
019975 # *****
019985 # *****
019995 # *****
020005 # *****
020015 # *****
020025 # *****
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020045 # *****
020055 # *****
020065 # *****
020075 # *****
020085 # *****
020095 # *****
020105 # *****
020115 # *****
020125 # *****
020135 # *****
020145 # *****
020155 # *****
020165 # *****
020175 # *****
020185 # *****
020195 # *****
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020415 # *****
020425 # *****
020435 # *****
020445 # *****
020455 # *****
020465 # *****
020475 # *****
020485 # *****
020495 # *****
020505 # *****
020515 # *****
020525 # *****
020535 # *****
020545 # *****
020555 # *****
020565 # *****
020575 # *****

```

Table with columns: ID, Description, Area, and various numerical values. The table lists numerous items, including road names (e.g., ROUTE 100, ROUTE 101), utility lines (e.g., MJSysStn, Mjr System), and specific locations (e.g., CATCHMENT MILLS, JACKVILLE SWM FACILITY). Each row contains a unique identifier followed by a detailed description of the asset and its associated data points.

Table with columns for ID, description, date, time, and other numerical data. Includes text-based annotations such as 'overflows', 'Channel X-Section', and 'Routing hydrographs'. Contains various technical parameters and results.

Table with columns: ID, Description, Parameters, Coordinates, Dates, and Values. The table lists various infrastructure items including roads, utilities, and land parcels with their respective details.

Table with multiple columns: ID (e.g., 044889), Description (e.g., [M.P. 52; T.M.P. 57]), and Data (e.g., 2.10, 2.19, 28.00, 38.41, n/a, 0.00). The table lists various infrastructure components and their associated parameters across numerous rows.

Table with columns for ID, description, and numerical data. Includes entries for hydrographs, subwatersheds, and various model parameters across multiple nodes and sections.

Table with multiple columns containing technical specifications, IDs, and data points. The table is organized into rows, each representing a specific data entry or record. Key columns include numerical values, alphanumeric codes, and descriptive text.

Table containing hydrograph data for various nodes (ROUTES, ADD HYD, ROUTE CHANNEL, SIMM, etc.) and contour lines (CONTOUR NSASD). Columns include node ID, description, flow values, dates, and various parameters like IRRFC, IRRPC, IRRSQ, etc.

09531# CONTI NLSX STANDHID 1.0 01:KB-13 10.19 1.690 N.Date 28:00 53.97 726 .000
 09532# [X]Mpa: 75 Tlmpa: 64
 09533# [Horton parameters: Fow: 76.20; Fc: 13.20; DCAV: 14; Fw: 00]
 09534# [Perivous area: IArea: 4.67; SLP: 0.0; LGA: 40; MNP: 250; SCP: 0]
 09535# [Impervious area: IAmp: 1.57; SLP: 0.0; LGA: 261; MNP: 013; SCI: 0]
 09536# [IARCCmp: 4.00; IAREPerc: 4.00]
 09537# COMPUTE D/L/D 1.0 01:KB-13 10.19 1.930 N.Date 28:00 53.97 n/a .000
 09538# Mjr System + 1.0 02:PC-01-M 0.00 0.00 N.Date 0.00 0.00 n/a .000
 09539# Mjor System + 1.0 02:PC-01-M 0.00 0.00 N.Date 0.00 0.00 n/a .000
 09540# Mjor System + 1.0 03:PC-03-MN 10.19 1.722 N.Date 27:57 53.98 n/a .000
 09541# [M SystSoc: 4703E+02, Tot Of Vol= 0.000E+00, N Of V= 0, Tot Dur Of V= 0 hrs.]
 09542# 09543# CONTI NLSX STANDHID 1.0 01:KB-14 5.47 1.075 N.Date 28:00 53.97 726 .000
 09544# [X]Mpa: 64 Tlmpa: 64
 09545# [Horton parameters: Fow: 76.20; Fc: 13.20; DCAV: 14; Fw: 00]
 09546# [Perivous area: IArea: 4.67; SLP: 0.0; LGA: 40; MNP: 250; SCP: 0]
 09547# [Impervious area: IAmp: 1.57; SLP: 0.0; LGA: 261; MNP: 013; SCI: 0]
 09548# [IARCCmp: 4.00; IAREPerc: 4.00]
 09549# COMPUTE D/L/D 1.0 01:KB-14 5.47 1.075 N.Date 28:00 53.97 n/a .000
 09550# Mjr System + 1.0 02:PC-01-M 0.00 0.00 N.Date 0.00 0.00 n/a .000
 09551# Mjor System + 1.0 02:PC-01-M 0.00 0.00 N.Date 0.00 0.00 n/a .000
 09552# Mjor System + 1.0 03:PC-03-MN 10.19 1.722 N.Date 27:57 53.98 n/a .000
 09553# [M SystSoc: 4703E+02, Tot Of Vol= 0.000E+00, N Of V= 0, Tot Dur Of V= 0 hrs.]
 09554# 09555# CONTI NLSX STANDHID 1.0 01:FRASER-DN 21.61 .681 N.Date 28:40 34.14 459 .000
 09556# [X]Mpa: 75 Tlmpa: 64
 09557# [Horton parameters: Fow: 76.20; Fc: 13.20; DCAV: 14; Fw: 00]
 09558# [Perivous area: IArea: 4.67; SLP: 0.0; LGA: 40; MNP: 250; SCP: 0]
 09559# [Impervious area: IAmp: 1.57; SLP: 0.0; LGA: 261; MNP: 013; SCI: 0]
 09560# [IARCCmp: 4.00; IAREPerc: 4.00]
 09561# COMPUTE D/L/D 1.0 01:KB-14 5.47 1.075 N.Date 28:00 53.97 n/a .000
 09562# Mjr System + 1.0 02:PC-01-M 0.00 0.00 N.Date 0.00 0.00 n/a .000
 09563# Mjor System + 1.0 02:PC-01-M 0.00 0.00 N.Date 0.00 0.00 n/a .000
 09564# Mjor System + 1.0 03:PC-03-MN 10.19 1.722 N.Date 27:57 53.98 n/a .000
 09565# [M SystSoc: 6018E+02, Tot Of Vol= 0.000E+00, N Of V= 0, Tot Dur Of V= 0 hrs.]
 09566# 09567# ADD IHD + 1.0 02:KB-14-M 5.47 1.075 N.Date 28:00 53.98 n/a .000
 09568# + 1.0 02:KB-14-M 5.47 1.075 N.Date 28:00 53.98 n/a .000
 09569# + 1.0 02:KB-14-M 5.47 1.075 N.Date 28:00 53.98 n/a .000
 09570# SIML + 1.0 01:KB-14-S 5.47 1.075 N.Date 28:00 53.98 n/a .000
 09571# [M SystSoc: 6018E+02, Tot Of Vol= 0.000E+00, N Of V= 0, Tot Dur Of V= 0 hrs.]
 09572# 09573# CONTI NLSX STANDHID 1.0 01:KB-14 5.47 1.075 N.Date 28:00 53.97 726 .000
 09574# [X]Mpa: 75 Tlmpa: 71
 09575# [Horton parameters: Fow: 76.20; Fc: 13.20; DCAV: 14; Fw: 00]
 09576# [Perivous area: IArea: 4.67; SLP: 0.0; LGA: 40; MNP: 250; SCP: 0]
 09577# [Impervious area: IAmp: 1.57; SLP: 0.0; LGA: 261; MNP: 013; SCI: 0]
 09578# [IARCCmp: 4.00; IAREPerc: 4.00]
 09579# COMPUTE D/L/D 1.0 01:KB-14 5.47 1.075 N.Date 28:00 53.97 n/a .000
 09580# Mjr System + 1.0 02:KB-14-M 5.47 1.075 N.Date 28:00 53.98 n/a .000
 09581# Mjor System + 1.0 02:KB-14-M 5.47 1.075 N.Date 28:00 53.98 n/a .000
 09582# Mjor System + 1.0 03:KB-14-MN 10.19 1.722 N.Date 27:57 53.98 n/a .000
 09583# [M SystSoc: 6018E+02, Tot Of Vol= 0.000E+00, N Of V= 0, Tot Dur Of V= 0 hrs.]
 09584# 09585# 09586# 09587# 09588# 09589# 09590# 09591# 09592# 09593# 09594# 09595# 09596# 09597# 09598# 09599# 09600# 09601# 09602# 09603# 09604# 09605# 09606# 09607# 09608# 09609# 09610# 09611# 09612# 09613# 09614# 09615# 09616# 09617# 09618# 09619# 09620# 09621# 09622# 09623# 09624# 09625# 09626# 09627# 09628# 09629# 09630# 09631# 09632# 09633# 09634# 09635# 09636# 09637# 09638# 09639# 09640# 09641# 09642# 09643# 09644# 09645# 09646# 09647# 09648# 09649# 09650# 09651# 09652# 09653# 09654# 09655# 09656# 09657# 09658# 09659# 09660# 09661# 09662# 09663# 09664# 09665# 09666# 09667# 09668# 09669# 09670# 09671# 09672# 09673# 09674# 09675# 09676# 09677# 09678# 09679# 09680# 09681# 09682# 09683# 09684# 09685# 09686# 09687# 09688# 09689# 09690# 09691# 09692# 09693# 09694# 09695# 09696# 09697# 09698# 09699# 09700# 09701# 09702# 09703# 09704# 09705# 09706# 09707# 09708# 09709# 09710# 09711# 09712# 09713# 09714# 09715# 09716# 09717# 09718# 09719# 09720# 09721# 09722# 09723# 09724# 09725# 09726# 09727# 09728# 09729# 09730# 09731# 09732# 09733# 09734# 09735# 09736# 09737# 09738# 09739# 09740# 09741# 09742# 09743# 09744# 09745# 09746# 09747# 09748# 09749# 09750# 09751# 09752# 09753# 09754# 09755# 09756# 09757# 09758# 09759# 09760# 09761# 09762# 09763# 09764# 09765# 09766# 09767# 09768# 09769# 09770# 09771# 09772# 09773# 09774# 09775# 09776# 09777# 09778# 09779# 09780# 09781# 09782# 09783# 09784# 09785# 09786# 09787# 09788# 09789# 09790# 09791# 09792# 09793# 09794# 09795# 09796# 09797# 09798# 09799# 09800# 09801# 09802# 09803# 09804# 09805# 09806# 09807# 09808# 09809# 09810# 09811# 09812# 09813# 09814# 09815# 09816# 09817# 09818# 09819# 09820# 09821# 09822# 09823# 09824# 09825# 09826# 09827# 09828# 09829# 09830# 09831# 09832# 09833# 09834# 09835# 09836# 09837# 09838# 09839# 09840# 09841# 09842# 09843# 09844# 09845# 09846# 09847# 09848# 09849# 09850# 09851# 09852# 09853# 09854# 09855# 09856# 09857# 09858# 09859# 09860# 09861# 09862# 09863# 09864# 09865# 09866# 09867# 09868# 09869# 09870# 09871# 09872# 09873# 09874# 09875# 09876# 09877# 09878# 09879# 09880# 09881# 09882# 09883# 09884# 09885# 09886# 09887# 09888# 09889# 09890# 09891# 09892# 09893# 09894# 09895# 09896# 09897# 09898# 09899# 09900# 09901# 09902# 09903# 09904# 09905# 09906# 09907# 09908# 09909# 09910# 09911# 09912# 09913# 09914# 09915# 09916# 09917# 09918# 09919# 09920# 09921# 09922# 09923# 09924# 09925# 09926# 09927# 09928# 09929# 09930# 09931# 09932# 09933# 09934# 09935# 09936# 09937# 09938# 09939# 09940# 09941# 09942# 09943# 09944# 09945# 09946# 09947# 09948# 09949# 09950# 09951# 09952# 09953# 09954# 09955# 09956# 09957# 09958# 09959# 09960# 09961# 09962# 09963# 09964# 09965# 09966# 09967# 09968# 09969# 09970# 09971# 09972# 09973# 09974# 09975# 09976# 09977# 09978# 09979# 09980# 09981# 09982# 09983# 09984# 09985# 09986# 09987# 09988# 09989# 09990# 09991# 09992# 09993# 09994# 09995# 09996# 09997# 09998# 09999# 10000#

Table with multiple columns containing technical specifications, flow rates, dates, and system identifiers. The table is organized into several sections, with some entries having asterisks and others having more detailed sub-sections. The data is presented in a structured, tabular format typical of engineering or scientific reports.

Table with columns for ID, Name, Location, Type, Date, and other parameters. The table contains a large number of rows, each representing a different station or data point with its specific characteristics and coordinates.

Table of simulation results with columns for ID, description, parameters, and numerical outputs. Includes sections for various models like CONTINUES STANWHD, COMPUTE DUALHYD, and ROUTE RESERVOIR.

Table with columns for ID, description, and parameters. Includes sections for 134855-134900, 134901-134950, 134951-135000, 135001-135050, 135051-135100, 135101-135150, 135151-135200, 135201-135250, 135251-135300, 135301-135350, 135351-135400, 135401-135450, 135451-135500, 135501-135550, 135551-135600, 135601-135650, 135651-135700, 135701-135750, 135751-135800, 135801-135850, 135851-135900, 135901-135950, 135951-136000, 136001-136050, 136051-136100, 136101-136150, 136151-136200, 136201-136250, 136251-136300, 136301-136350, 136351-136400, 136401-136450, 136451-136500, 136501-136550, 136551-136600, 136601-136650, 136651-136700, 136701-136750, 136751-136800, 136801-136850, 136851-136900, 136901-136950, 136951-137000, 137001-137050, 137051-137100, 137101-137150, 137151-137200, 137201-137250, 137251-137300, 137301-137350, 137351-137400, 137401-137450, 137451-137500, 137501-137550, 137551-137600, 137601-137650, 137651-137700, 137701-137750, 137751-137800, 137801-137850, 137851-137900, 137901-137950, 137951-138000, 138001-138050, 138051-138100, 138101-138150, 138151-138200, 138201-138250, 138251-138300, 138301-138350, 138351-138400, 138401-138450, 138451-138500, 138501-138550, 138551-138600, 138601-138650, 138651-138700, 138701-138750, 138751-138800, 138801-138850, 138851-138900, 138901-138950, 138951-139000.

145878 remark Total Flow at KB second pond
145888 R0100-CO0247-11.D NND.....AREHA-QPEAGm-TpeakDte-hh-mm-Rvmm-R.C---DfWcm
145889 # CONTI NIXS STANDIHD 1.0 01: FC-03 14.0 686 No.Date 28:00 72.68 821 000
145890 # [XfMps: 75.30; TImps: 75]

147776 # Catchment Greenbank
147777 # To Greenbank Drain (south of the Jack)
147778 # FJSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on QS measurements
147779 # FJSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on QS measurements
147780 R0100-CO0272-11.D NND.....AREHA-QPEAGm-TpeakDte-hh-mm-Rvmm-R.C---DfWcm

Table with multiple columns containing system identifiers, component names, status, and various numerical values. The table is organized into vertical sections, with each section starting with a header row (e.g., 149613, 149614, etc.) and followed by several rows of data. The data includes system names like 'Major System', 'Minor System', and 'Mjr System', along with various parameters and values.

Table with columns for ID, Description, Area, Date, and various numerical values. The table contains detailed engineering data for various systems and components, including major systems, minor systems, and specific infrastructure like roads and bridges.

```
157098 *** WARNING: New pipe size used for routing.
157108 R0100: C00370 ROUTE PIPE ->
157118 *** WARNING: New pipe size used for routing.
157128 R0050: C00378 ROUTE PIPE ->
157138 *** WARNING: New pipe size used for routing.
157148 R0050: C00379 ROUTE PIPE ->
157158 *** WARNING: New pipe size used for routing.
157168 R0100: C00303 ROUTE PIPE ->
157178 *** WARNING: New pipe size used for routing.
157188 R0100: C00309 ROUTE PIPE ->
157198 *** WARNING: New pipe size used for routing.
157208 R0100: C00325 ROUTE PIPE ->
157218 *** WARNING: New pipe size used for routing.
157228 R0100: C00326 ROUTE PIPE ->
157238 *** WARNING: New pipe size used for routing.
157248 R0100: C00334 ROUTE PIPE ->
157258 *** WARNING: New pipe size used for routing.
157268 R0100: C00342 IR VERT HYD ->
157278 *** NOTE: Inflow hyd. is dry and cannot be diverted.
157288 R0100: C00357 ROUTE PIPE ->
157298 *** WARNING: New pipe size used for routing.
157308 R0100: C00362 ROUTE PIPE ->
157318 *** WARNING: New pipe size used for routing.
157328 R0100: C00369 ROUTE PIPE ->
157338 *** WARNING: New pipe size used for routing.
157348 R0100: C00370 ROUTE PIPE ->
157358 *** WARNING: New pipe size used for routing.
157368 R0100: C00378 ROUTE PIPE ->
157378 *** WARNING: New pipe size used for routing.
157388 R0100: C00379 ROUTE PIPE ->
157398 *** WARNING: New pipe size used for routing.
157408 Simulation ended on 2021-03-04 at 11:53:36
157418 =====
157428
157438
```

Attachment D

Model 4A – Jock River Reach One Future Conditions – Without SWM controls

JFSA, 2021

SWMHYMO Input & Summary files

```

1  20      Metric units / ID numbers OFF
2  *****
3  *# SWHYMO Ver: 5.02/Jan 2001 <BETA> / INPUT DATA FILE
4  *****
5  *# Project Name: [Jock River]      Project Number: [1474-16]
6  *# Date       : 04-03-2021
7  *# Modeller   : [MM]
8  *# Company    : JFSA Inc.
9  *# License #  : 2549237
10 *****
11 *# CALIBRATION OF SUMMER MODEL PARAMETERS
12 *# USING CONTINUOUS SIMULATIONS
13 *# Rainfall data from JFSA raingauge installed at site + other gauges by the City
14 *# Use data collected from May 1st to July 14, 2003
15 *# 2020-11-30 change TMSSTO in COMPUTE DUALHYD (TMSSTO = 0.1 instead of 0.0001)
16 *# 2020-12-01 correct pond curve values
17 *# 2020-12-01 change WCLAR_BRAZ_XIMP to 0.55, SLPI=[0.5](%) (impervious slope), and
18 LGI up to 700m
19 *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 2462 (NHYDout=["N_TO"]
20 ,NHYDin=["SN_TO"]) from 0.033 % (as per Stantec Report 2007) to 0.05 % so the model
21 will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELS
22 aren't well suited to really flat slopes.
23 *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHYDout=["N_WC"]
24 ,NHYDin=["SN_CE"]) from 0.01 % (as per Stantec Report 2007) to 0.0255 % so the model
25 will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELS
26 aren't well suited to really flat slopes.
27 *
28 * Calibrated parameters for Summer 2003 data: APII=50, APIK=0.85, CN=varies,
29 *                                               SK=0.01, InterEventTime=12,
30 *                                               GWResk=0.96, VHydCond=0.055
31 *
32 *# -----
33 *
34 *START          TZERO=[2003.0501], METOUT=[2], NSTORM=[1], NRUN=[001]
35 *              ["XAVG0315.STM"] average storm data a 15 minute time step
36 *              The above rainf file is an average of the JFSA gauge data
37 *              with the City of Ottawa rainfall data collected during
38 *              the same period.
39 *% 2 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
40 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[2]
41 ["C24SC002.stm"] <-- storm filename, one per line for NSTORM time
42 *%-----|-----|
43 *%-----|-----|
44 READ STORM     STORM_FILENAME=["storm 001"]
45 *%-----|-----|
46 MODIFY STORM   ICASEms=[1], NSHIFT=[96],
47               RedFACT=[1],
48 *%-----|-----|
49 DEFAULT VALUES ICASEdef=[1], read and print values
50 DEFVAL_FILENAME=["CitiGate.DEF"]
51 *%-----|-----|
52 *%-----|-----|
53 COMPUTE API    APII=[50], APIK=[.85]/day
54 *%-----|-----|
55 *%-----|-----|
56 *#
57 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
58 *# of 1.32
59 *%-----|-----|
60 CONTINUOUS NASHYD NHYD=["JR_HW"], DT=[1]min, AREA=[3680](ha),
61 DWF=[0](cms), CNVC=[64], IA=[2.5](mm),
62 N=[3.0], TP=[7.13]hrs,
63 Continuous simulation parameters:
64 IARECper=[4](hrs),
65 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
66 InterEventTime=[12](hrs)
67 Baseflow simulation parameters:

```

```

60 BaseFlowOption=[ 1] ,
61 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
62 VHydCond=[ 0.055](mm/hr), END=- 1
63 *%-----|-----
64 *#
65 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
66 *# of 1.32
67 *%-----|-----
68 CONTINUOUS NASHYD NHYD=["SW_13"], DT=[ 1]min, AREA=[ 971](ha),
69 DWF=[ 0](cms), CNVC=[ 61], IA=[ 2.5](mm),
70 N=[ 3.0], TP=[ 3.76]hrs,
71 Continuous simulation parameters:
72 IaRECper=[ 4](hrs),
73 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
74 InterEventTime=[ 12](hrs)
75 Baseflow simulation parameters:
76 BaseFlowOption=[ 1] ,
77 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
78 VHydCond=[ 0.055](mm/hr), END=- 1
79 *%-----|-----
80 *#
81 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
82 *# of 1.80
83 *%-----|-----
84 CONTINUOUS NASHYD NHYD=["JR_GWM"], DT=[ 1]min, AREA=[ 3074](ha),
85 DWF=[ 0](cms), CNVC=[ 55], IA=[ 2.5](mm),
86 N=[ 3], TP=[ 11.33]hrs,
87 Continuous simulation parameters:
88 IaRECper=[ 4](hrs),
89 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
90 InterEventTime=[ 12](hrs)
91 Baseflow simulation parameters:
92 BaseFlowOption=[ 1] ,
93 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
94 VHydCond=[ 0.055](mm/hr), END=- 1
95 *%-----|-----
96 CONTINUOUS NASHYD NHYD=["JR_ASH"], DT=[ 1]min, AREA=[ 1781](ha),
97 DWF=[ 0](cms), CNVC=[ 72], IA=[ 2.5](mm),
98 N=[ 3.0], TP=[ 3.91]hrs,
99 Continuous simulation parameters:
100 IaRECper=[ 4](hrs),
101 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
102 InterEventTime=[ 12](hrs)
103 Baseflow simulation parameters:
104 BaseFlowOption=[ 1] ,
105 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
106 VHydCond=[ 0.055](mm/hr), END=- 1
107 *%-----|-----
108 CONTINUOUS NASHYD NHYD=["SW_11"], DT=[ 1]min, AREA=[ 500](ha),
109 DWF=[ 0](cms), CNVC=[ 66], IA=[ 2.5](mm),
110 N=[ 3.0], TP=[ 1.24]hrs,
111 Continuous simulation parameters:
112 IaRECper=[ 4](hrs),
113 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
114 InterEventTime=[ 12](hrs)
115 Baseflow simulation parameters:
116 BaseFlowOption=[ 1] ,
117 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
118 VHydCond=[ 0.055](mm/hr), END=- 1
119 *%-----|-----
120 *#
121 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
122 *# of 1.80
123 *%-----|-----
124 CONTINUOUS NASHYD NHYD=["NN_CK"], DT=[ 1]min, AREA=[ 1917](ha),
125 DWF=[ 0](cms), CNVC=[ 66], IA=[ 2.5](mm),

```

```

126 N=[ 3. 0], TP=[ 5. 29] hrs,
127 Continuous simulation parameters:
128 IaRECPper=[ 4] (hrs),
129 SMN=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
130 InterEventTime=[ 12] (hrs)
131 Baseflow simulation parameters:
132 BaseFlowOption=[ 1] ,
133 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
134 VHydCond=[ 0. 055] (mm/ hr), END=- 1
135 *%-----|-----
136 *#
137 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
138 *# of 1.52
139 *%-----|-----
140 CONTINUOUS NASHYD NHYD=[ "SW_10"], DT=[ 1] min, AREA=[ 5666] (ha),
141 DWF=[ 0] (cms), CNVC=[ 72], IA=[ 2. 5] (mm),
142 N=[ 3. 0], TP=[ 8. 00] hrs,
143 Continuous simulation parameters:
144 IaRECPper=[ 4] (hrs),
145 SMN=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
146 InterEventTime=[ 12] (hrs)
147 Baseflow simulation parameters:
148 BaseFlowOption=[ 1] ,
149 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
150 VHydCond=[ 0. 055] (mm/ hr), END=- 1
151 *%-----|-----
152 *#
153 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
154 *# of 1.75
155 *%-----|-----
156 CONTINUOUS NASHYD NHYD=[ "KG_CK"], DT=[ 1] min, AREA=[ 8376] (ha),
157 DWF=[ 0] (cms), CNVC=[ 66], IA=[ 2. 5] (mm),
158 N=[ 3. 0], TP=[ 11. 66] hrs,
159 Continuous simulation parameters:
160 IaRECPper=[ 4] (hrs),
161 SMN=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
162 InterEventTime=[ 12] (hrs)
163 Baseflow simulation parameters:
164 BaseFlowOption=[ 1] ,
165 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
166 VHydCond=[ 0. 055] (mm/ hr), END=- 1
167 *%-----|-----
168 *#
169 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
170 *# of 1.68
171 *%-----|-----
172 CONTINUOUS NASHYD NHYD=[ "SW_9"], DT=[ 1] min, AREA=[ 1132] (ha),
173 DWF=[ 0] (cms), CNVC=[ 70], IA=[ 2. 5] (mm),
174 N=[ 3. 0], TP=[ 2. 51] hrs,
175 Continuous simulation parameters:
176 IaRECPper=[ 4] (hrs),
177 SMN=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
178 InterEventTime=[ 12] (hrs)
179 Baseflow simulation parameters:
180 BaseFlowOption=[ 1] ,
181 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
182 VHydCond=[ 0. 055] (mm/ hr), END=- 1
183 *%-----|-----
184 *#
185 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
186 *# of 1.82
187 *%-----|-----
188 CONTINUOUS NASHYD NHYD=[ "NC_CK"], DT=[ 1] min, AREA=[ 4464] (ha),
189 DWF=[ 0] (cms), CNVC=[ 62], IA=[ 2. 5] (mm),
190 N=[ 3. 0], TP=[ 11. 32] hrs,
191 Continuous simulation parameters:

```



```

192 IaREcper=[ 4] (hr s),
193 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
194 InterEventTime=[ 12] (hr s)
195 Baseflow simulation parameters:
196 BaseFlowOption=[ 1] ,
197 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
198 VHydCond=[ 0. 055] (mm/ hr), END=- 1
199 *%-----|-----
200 *#
201 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
202 *# of 1.80
203 *%-----|-----
204 CONTINUOUS NASHYD NHYD=[ "SW_8" ], DT=[ 1] mi n, AREA=[ 131] (ha),
205 DWF=[ 0] (cms), CN C=[ 63], IA=[ 2. 5] (mm),
206 N=[ 3. 0], TP=[ 0. 90] hr s,
207 Continuous simulation parameters:
208 IaREcper=[ 4] (hr s),
209 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
210 InterEventTime=[ 12] (hr s)
211 Baseflow simulation parameters:
212 BaseFlowOption=[ 1] ,
213 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
214 VHydCond=[ 0. 055] (mm/ hr), END=- 1
215 *%-----|-----
216 *#
217 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
218 *# of 1.65
219 *%-----|-----
220 CONTINUOUS NASHYD NHYD=[ "HB_DR" ], DT=[ 1] mi n, AREA=[ 3854] (ha),
221 DWF=[ 0] (cms), CN C=[ 66], IA=[ 2. 5] (mm),
222 N=[ 3. 0], TP=[ 8. 42] hr s,
223 Continuous simulation parameters:
224 IaREcper=[ 4] (hr s),
225 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
226 InterEventTime=[ 12] (hr s)
227 Baseflow simulation parameters:
228 BaseFlowOption=[ 1] ,
229 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
230 VHydCond=[ 0. 055] (mm/ hr), END=- 1
231 *%-----|-----
232 *#
233 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
234 *# of 1.82
235 *%-----|-----
236 CONTINUOUS NASHYD NHYD=[ "SW_7" ], DT=[ 1] mi n, AREA=[ 3197] (ha),
237 DWF=[ 0] (cms), CN C=[ 57], IA=[ 2. 5] (mm),
238 N=[ 3. 0], TP=[ 6. 65] hr s,
239 Continuous simulation parameters:
240 IaREcper=[ 4] (hr s),
241 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
242 InterEventTime=[ 12] (hr s)
243 Baseflow simulation parameters:
244 BaseFlowOption=[ 1] ,
245 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
246 VHydCond=[ 0. 055] (mm/ hr), END=- 1
247 *%-----|-----
248 *#
249 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
250 *# of 1.75
251 *%-----|-----
252 CONTINUOUS NASHYD NHYD=[ "SW_6" ], DT=[ 1] mi n, AREA=[ 165] (ha),
253 DWF=[ 0] (cms), CN C=[ 67], IA=[ 2. 5] (mm),
254 N=[ 3. 0], TP=[ 4. 18] hr s,
255 Continuous simulation parameters:
256 IaREcper=[ 4] (hr s),
257 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),

```

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258 InterEventTime=[ 12] (hrs)
259 Baseflow simulation parameters:
260 BaseFlowOption=[ 1] ,
261 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
262 VHydCond=[ 0.055] (mm/ hr), END=- 1
263 *%-----|-----
264 *#
265 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
266 *# of 1.67
267 *%-----|-----
268 CONTINUOUS NASHYD NHYD=[ "VG_DR" ], DT=[ 1] min, AREA=[ 1332] (ha),
269 DWF=[ 0] (cms), CNVC=[ 72], IA=[ 2.5] (mm),
270 N=[ 3.0], TP=[ 5.95] hrs,
271 Continuous simulation parameters:
272 IaRECper=[ 4] (hrs),
273 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
274 InterEventTime=[ 12] (hrs)
275 Baseflow simulation parameters:
276 BaseFlowOption=[ 1] ,
277 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
278 VHydCond=[ 0.055] (mm/ hr), END=- 1
279 *%-----|-----
280 CONTINUOUS NASHYD NHYD=[ "SW_5" ], DT=[ 1] min, AREA=[ 224] (ha),
281 DWF=[ 0] (cms), CNVC=[ 77], IA=[ 2.5] (mm),
282 N=[ 3.0], TP=[ 0.75] hrs,
283 Continuous simulation parameters:
284 IaRECper=[ 4] (hrs),
285 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
286 InterEventTime=[ 12] (hrs)
287 Baseflow simulation parameters:
288 BaseFlowOption=[ 1] ,
289 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
290 VHydCond=[ 0.055] (mm/ hr), END=- 1
291 *%-----|-----
292 *#
293 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
294 *# of 1.20
295 *%-----|-----
296 CONTINUOUS NASHYD NHYD=[ "FL_CK" ], DT=[ 1] min, AREA=[ 4945] (ha),
297 DWF=[ 0] (cms), CNVC=[ 74], IA=[ 2.5] (mm),
298 N=[ 3.0], TP=[ 4.45] hrs,
299 Continuous simulation parameters:
300 IaRECper=[ 4] (hrs),
301 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
302 InterEventTime=[ 12] (hrs)
303 Baseflow simulation parameters:
304 BaseFlowOption=[ 1] ,
305 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
306 VHydCond=[ 0.055] (mm/ hr), END=- 1
307 *%-----|-----
308 CONTINUOUS NASHYD NHYD=[ "SW_5A2" ], DT=[ 1] min, AREA=[ 20] (ha),
309 DWF=[ 0] (cms), CNVC=[ 81], IA=[ 2.5] (mm),
310 N=[ 3.0], TP=[ 0.62] hrs,
311 Continuous simulation parameters:
312 IaRECper=[ 4] (hrs),
313 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
314 InterEventTime=[ 12] (hrs)
315 Baseflow simulation parameters:
316 BaseFlowOption=[ 1] ,
317 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
318 VHydCond=[ 0.055] (mm/ hr), END=- 1
319 *%-----|-----
320 *#
321 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
322 *# of 1.61
323 *%-----|-----

```

324 CONTI NUOUS NASHYD NYHD=["SW_5A1"], DT=[1] mi n, AREA=[1412] (ha),
325 DWF=[0] (cms), CNV C=[75], IA=[2. 5] (mm),
326 N=[3. 0], TP=[8. 00] hr s,
327 Continuous simulation parameters:
328 IaRECper=[4] (hr s),
329 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
330 InterEventTime=[12] (hr s)
331 Baseflow simulation parameters:
332 BaseFlowOpti on=[1] ,
333 In it GWRes Vol = [50] (mm), GWRes K=[0. 96] (mm / day / mm)
334 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

336 CONTI NUOUS NASHYD NYHD=["SW_4"], DT=[1] mi n, AREA=[585] (ha),
337 DWF=[0] (cms), CNV C=[81], IA=[2. 5] (mm),
338 N=[3. 0], TP=[1. 75] hr s,
339 Continuous simulation parameters:
340 IaRECper=[4] (hr s),
341 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
342 InterEventTime=[12] (hr s)
343 Baseflow simulation parameters:
344 BaseFlowOpti on=[1] ,
345 In it GWRes Vol = [50] (mm), GWRes K=[0. 96] (mm / day / mm)
346 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

348 CONTI NUOUS NASHYD NYHD=["LM_CK"], DT=[1] mi n, AREA=[1021] (ha),
349 DWF=[0] (cms), CNV C=[80], IA=[2. 5] (mm),
350 N=[3. 0], TP=[2. 46] hr s,
351 Continuous simulation parameters:
352 IaRECper=[4] (hr s),
353 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
354 InterEventTime=[12] (hr s)
355 Baseflow simulation parameters:
356 BaseFlowOpti on=[1] ,
357 In it GWRes Vol = [50] (mm), GWRes K=[0. 96] (mm / day / mm)
358 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

360 CONTI NUOUS NASHYD NYHD=["SW_2"], DT=[1] mi n, AREA=[177] (ha),
361 DWF=[0] (cms), CNV C=[77], IA=[2. 5] (mm),
362 N=[3. 0], TP=[0. 75] hr s,
363 Continuous simulation parameters:
364 IaRECper=[4] (hr s),
365 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
366 InterEventTime=[12] (hr s)
367 Baseflow simulation parameters:
368 BaseFlowOpti on=[1] ,
369 In it GWRes Vol = [50] (mm), GWRes K=[0. 96] (mm / day / mm)
370 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

372 CONTI NUOUS NASHYD NYHD=["SM_DR"], DT=[1] mi n, AREA=[1122] (ha),
373 DWF=[0] (cms), CNV C=[81], IA=[2. 5] (mm),
374 N=[3. 0], TP=[3. 25] hr s,
375 Continuous simulation parameters:
376 IaRECper=[4] (hr s),
377 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
378 InterEventTime=[12] (hr s)
379 Baseflow simulation parameters:
380 BaseFlowOpti on=[1] ,
381 In it GWRes Vol = [50] (mm), GWRes K=[0. 96] (mm / day / mm)
382 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

384 CONTI NUOUS NASHYD NYHD=["MO_DR"], DT=[1] mi n, AREA=[2737] (ha),
385 DWF=[0] (cms), CNV C=[76], IA=[2. 5] (mm),
386 N=[3. 0], TP=[3. 03] hr s,
387 Continuous simulation parameters:
388 IaRECper=[4] (hr s),
389 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),

```

390 InterEventTime=[ 12]( hrs)
391 Baseflow simulation parameters:
392 BaseFlowOption=[ 1] ,
393 InitGWResVol=[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
394 VHydCond=[ 0.055]( mm/ hr) , END=- 1
395 *%-----|-----|
396 * -JFSA 2020 replaced SW_1 with a detailed model from Stantec Report 2007
397 *CONTINUOUS NASHYD NHYD=["SW_1"], DT=[ 1]mi n, AREA=[ 3176]( ha),
398 * DWF=[ 0]( cms) , CN/C=[ 78] , IA=[ 2.5]( mm),
399 * N=[ 3.0] , TP=[ 3.56]hrs,
400 * Continuous simulation parameters:
401 * IaRECper=[ 4]( hrs),
402 * SMN=[ -1]( mm) , SMAX=[ -1]( mm) , SK=[ 0.010]/( mm),
403 * InterEventTime=[ 12]( hrs)
404 * Baseflow simulation parameters:
405 * BaseFlowOption=[ 1] ,
406 * InitGWResVol=[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
407 * VHydCond=[ 0.055]( mm/ hr) , END=- 1
408 *%-----|-----|
409 *#
410 *# Routing hydrographs
411 *#
412 *# Starting with the addition of Jock River Headwater and Subwatershed 13
413 *#
414 ADD HYD NHYDsum=["S_N13"], NHYDs to add=["JR_HW"+"SW_13"]
415 *%-----|-----|
416 *#
417 *# Sum of hydrographs from Node 13 routed to Node 13A
418 *# (Approximated cross-section - see cross-section 258)
419 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
420 *#
421 ROUTE CHANNEL NHYDout=["N13A"] , NHYDin=["S_N13"],
422 RDT=[ 1]( mi n),
423 CHLGTH=[ 9074]( m) , CHSLOPE=[ 0.0220]( %),
424 FPSLOPE=[ 0.0220]( %),
425 SECNUM=[ 1.0] , NSEG=[ 1]
426 ( SEGROUGH, SEGDIST ( m) )=[ 0.04, 15.5] NSEG times
427 ( DISTANCE ( m) , ELEVATION ( m) )=
428 [- 40, 132.5]
429 [- 30, 132]
430 [- 25, 131.5]
431 [- 13, 130]
432 [- 8, 127.00]
433 [- 7, 126.50]
434 [- 6, 126]
435 [- 5.5, 125.50]
436 [0, 123.75]
437 [4.5, 125.50]
438 [6, 126]
439 [7.5, 126.5]
440 [9, 127]
441 [10, 127.5]
442 [11.5, 128.0]
443 [15.5, 129.5]
444 *%-----|-----|
445 *#
446 *# Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
447 *#
448 ADD HYD NHYDsum=["SN13A"], NHYDs to add=["N13A"+"JR_GWM"]
449 *%-----|-----|
450 *#
451 *# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
452 *#
453 ROUTE RESERVOIR NHYDout=["RES_GM"] , NHYDin=["SN13A"],
454 RDT=[ 1]( mi n),
455 TABLE of ( OUTFLOW STORAGE ) values

```

```

456 (cms) - (ha-m)
457 [ 0.0 , 0.0 ]
458 [ 1.991, 2.144 ]
459 [ 2.693, 39.826 ]
460 [ 3.509, 81.697 ]
461 [ 4.578, 318.774 ]
462 [ 5.647, 594.947 ]
463 [ 7.109, 910.219 ]
464 [ 8.616, 1264.589 ]
465 [ 10.371, 1658.057 ]
466 [ 12.402, 2090.622 ]
467 [ 22.056, 3462.487 ]
468 [ -1 , -1 ] (max twenty pts)
469
470 NHYDovf=[ " " ] ,
471 *%-----|-----|
472 *#
473 SAVE HYD NHYD=[ "RES_GM" ], # OF PCYCLES=[ -1 ], I CASEs h=[ -1 ]
474 HYD_FILENAMES=[ "H_RESGM" ]
475 HYD_COMMENT=[ "Out flow from Res GM" ]
476 *%-----|-----|
477 *# Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
478 *# (Approximated cross-section - see cross-section 258)
479 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
480 ROUTE CHANNEL NHYDout=[ "N12" ] , NHYDin=[ "RES_GM" ] ,
481 RDT=[ 1 ] (min) ,
482 CHLGTH=[ 5926 ] (m) , CHSLOPE=[ 0.0759 ] ( % ) ,
483 FPSLOPE=[ 0.0759 ] ( % ) ,
484 SECNUM=[ 1.0 ] , NSEG=[ 1 ]
485 ( SEGROUGH, SEGDIST (m) )=[ 0.04, 15.5 ] NSEG times
486 ( DISTANCE (m) , ELEVATION (m) )=
487 [- 40, 132.5]
488 [- 30, 132]
489 [- 25, 131.5]
490 [- 13, 130]
491 [- 8, 127.00]
492 [- 7, 126.50]
493 [- 6, 126]
494 [- 5.5, 125.50]
495 [ 0, 123.75]
496 [ 4.5, 125.50]
497 [ 6, 126]
498 [ 7.5, 126.5]
499 [ 9, 127]
500 [ 10, 127.5]
501 [ 11.5, 128.00]
502 [ 15.5, 129.5]
503 *%-----|-----|
504 *#
505 *# Addition of Subwatershed Jock River at Ashton to Node 12
506 *#
507 ADD HYD NHYDsum=[ "S_N12" ] , NHYDsto add=[ "N12"+"JR_ASH" ]
508 SAVE HYD NHYD=[ "S_N12" ] , # OF PCYCLES=[ -1 ], I CASEs h=[ -1 ]
509 HYD_FILENAMES=[ "H_SN12" ]
510 HYD_COMMENT=[ "flow at S_N12 near Ashton" ]
511 *%-----|-----|
512 *#
513 *# Sum of hydrographs from Node 12 routed to Node 11
514 *# (Approximated cross-section - see cross-section 258)
515 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
516 *ROUTE CHANNEL NHYDout=[ "N11" ] , NHYDin=[ "S_N12" ] ,
517 * RDT=[ 1 ] (min) ,
518 * CHLGTH=[ 972 ] (m) , CHSLOPE=[ 0.0514 ] ( % ) ,
519 * FPSLOPE=[ 0.0514 ] ( % ) ,
520 * SECNUM=[ 1.0 ] , NSEG=[ 1 ]
521 * ( SEGROUGH, SEGDIST (m) )=[ 0.04, 15.5 ] NSEG times
522 * ( DISTANCE (m) , ELEVATION (m) )=

```

```

522 * [- 40, 132.5]
523 * [- 30, 132]
524 * [- 25, 131.5]
525 * [- 13, 130]
526 * [- 8, 127.00]
527 * [- 7, 126.50]
528 * [- 6, 126]
529 * [- 5.5, 125.50]
530 * [0, 123.75]
531 * [4.5, 125.50]
532 * [6, 126]
533 * [7.5, 126.5]
534 * [9, 127]
535 * [10, 127.5]
536 * [11.5, 128.00]
537 * [15.5, 129.5]
538 *%-----|-----
539 *#
540 *# Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
541 *#
542 ROUTE CHANNEL NHYDout=["Duml1"], NHYDin=["S_N12"],
543 RDT=[1](min),
544 CHLGTH=[972](m), CHSLOPE=[0.054](%),
545 FPSLOPE=[0.054](%),
546 SECNUM=[1.0], NSEG=[1]
547 ( SEGROUGH, SEGDIST (m))=[0.04, 15.5] NSEG times
548 ( DISTANCE (m), ELEVATION (m))=
549 [- 40, 132.5]
550 [- 30, 132]
551 [- 25, 131.5]
552 [- 13, 130]
553 [- 8, 127.00]
554 [- 7, 126.50]
555 [- 6, 126]
556 [- 5.5, 125.50]
557 [0, 123.75]
558 [4.5, 125.50]
559 [6, 126]
560 [7.5, 126.5]
561 [9, 127]
562 [10, 127.5]
563 [11.5, 128.00]
564 [15.5, 129.5]
565 *%-----|-----
566 *#
567 *# Addition of Subwatershed 11 and No Name Creek to Node 11
568 *#
569 ADD HYD NHYDsum=["S_N11"], NHYDstoadd=["Duml1"+"SW_11"+"NN_CK"]
570 *%-----|-----
571 *#
572 *# Sum of hydrographs from Node 11 routed to Node 10
573 *# Section 1
574 *#
575 ROUTE CHANNEL NHYDout=["N10"], NHYDin=["S_N11"],
576 RDT=[1](min),
577 CHLGTH=[14028](m), CHSLOPE=[0.1568](%),
578 FPSLOPE=[0.1568](%),
579 SECNUM=[1.0], NSEG=[5]
580 ( SEGROUGH, SEGDIST (m))=
581 [0.04, -52.82
582 0.1, -6.47
583 -0.05, 6.47
584 0.1, 45.36
585 0.04, 423.88] NSEG times
586 ( DISTANCE (m), ELEVATION (m))=
587 [- 226.24 , 112.50]

```

```

588             [- 167. 50 , 111. 50]
589             [- 106. 81 , 111. 00]
590             [- 92. 37 , 110. 00]
591             [- 52. 82 , 109. 00]
592             [- 24. 90, 109. 00]
593             [- 17. 02, 108. 50]
594             [- 6. 47, 108. 00]
595             [ 6. 47, 108. 00]
596             [ 15. 67, 108. 50]
597             [ 18. 95, 109. 00]
598             [ 45. 36, 109. 50]
599             [ 120. 79, 110. 00]
600             [ 145. 72, 111. 00]
601             [ 181. 56, 111. 50]
602             [ 423. 88, 112. 50]
603 *%-----|-----
604 *#
605 *# Addition of Subwatershed 10 to Node 10
606 *#
607 ADD HYD          NHYDs um=["S_N10"], NHYDs to add=["N10"+"SW_10"]
608 *%-----|-----
609 SAVE HYD        NHYD=["S_N10"], # OF PCYCLES=[- 1], I CASEs h=[- 1]
610                HYD_ FI LENAME=["H_SN10"]
611                HYD_ COMMENT=["flow at S_N10: N10 + SW_10"]
612 *%-----|-----
613 *# Addition of Kings Creek to S_N10
614 *#
615 ADD HYD          NHYDs um=["S_N10A"], NHYDs to add=["S_N10"+"KG_CK"]
616 *%-----|-----
617 *#
618 *# Sum of hydrographs from Node 10 routed to Node 9
619 *# Section 2
620 *#
621 ROUTE CHANNEL    NHYDout=["N9"] , NHYDin=["S_N10A"] ,
622                RDT=[ 1] ( mi n) ,
623                CHLGTH=[ 3982] ( m) ,    CHSLOPE=[ 0. 0753] ( % ) ,
624                FPSLOPE=[ 0. 0753] ( % ) ,
625                SECNUM=[ 1. 0] ,        NSEG=[ 4]
626                ( SEGROUGH, SEGDI ST ( m) ) =
627                [ 0. 04, - 30. 27
628                0. 05, - 18. 42
629                - 0. 05, 18. 42
630                0. 04, 131. 58] NSEG t i m e s
631                ( DI STANCE ( m) , ELEVATI ON ( m) ) =
632                [- 446. 74, 106. 00]
633                [- 415. 68, 105. 50]
634                [- 285. 40, 105. 00]
635                [- 173. 77, 104. 50]
636                [- 144. 95, 104. 00]
637                [- 111. 18, 103. 50]
638                [- 94. 06, 103. 00]
639                [- 71. 02, 102. 50]
640                [- 30. 27, 102. 00]
641                [- 19. 33, 100. 00]
642                [- 18. 42, 99. 50]
643                [ 18. 42, 99. 50]
644                [ 20. 77, 100. 00]
645                [ 27. 93, 101. 00]
646                [ 52. 29, 101. 00]
647                [ 68. 80, 101. 50]
648                [ 79. 66, 103. 00]
649                [ 91. 50, 103. 50]
650                [ 131. 58, 104. 00]
651 *%-----|-----
652 *#
653 *# Addition of Subwatershed 9 and Nichols Creek to Node 9

```

```

654  *#
655  ADD HYD          NHYDs um=[ "S_N9" ], NHYDs to add=[ "N9"+"SW_9"+"NC_CK" ]
656  *%-----|-----|
657  *#
658  *# Sum of hydrographs from Node 9 routed to Node 8
659  *# Section 3
660  *#
661  ROUTE CHANNEL    NHYDout =[ "N8" ] , NHYDin =[ "S_N9" ] ,
662                  RDT=[ 1 ] ( mi n ) ,
663                  CHLGTH=[ 2269 ] ( m ) ,   CHSLOPE=[ 0.0882 ] ( % ) ,
664                                                    FPSLOPE=[ 0.0882 ] ( % ) ,
665                  SECNUM=[ 1.0 ] ,          NSEG=[ 3 ]
666                  ( SEGROUGH, SEGDI ST ( m ) ) =
667                    [ 0.1, -17.99
668                      -0.045, 17.31
669                      0.1, 456.58 ] NSEG t i m e s
670                  ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
671                    [ -201.19, 100.50 ]
672                    [ -135.21, 100.00 ]
673                    [ -94.83, 99.50 ]
674                    [ -67.05, 99.00 ]
675                    [ -17.99, 98.50 ]
676                    [ -16.02, 98.00 ]
677                    [ -13.95, 97.50 ]
678                    [ 13.95, 97.50 ]
679                    [ 15.64, 98.00 ]
680                    [ 17.31, 98.50 ]
681                    [ 162.02, 98.50 ]
682                    [ 172.89 , 99.00 ]
683                    [ 314.38, 99.00 ]
684                    [ 343.78, 99.50 ]
685                    [ 365.67, 100.00 ]
686                    [ 376.68, 100.00 ]
687                    [ 393.11, 99.50 ]
688                    [ 404.97, 99.50 ]
689                    [ 431.70, 100.00 ]
690                    [ 456.58, 100.50 ]
691  *%-----|-----|
692  *#
693  *# Addition of Subwatershed 8 and Hobb's Drain to Node 8
694  *#
695  ADD HYD          NHYDs um=[ "S_N8" ], NHYDs to add=[ "N8"+"SW_8"+"HB_DR" ]
696  *%-----|-----|
697  *#
698  *# Sum of hydrographs from Node 8 routed to Node 7
699  *# Section 4
700  *#
701  ROUTE CHANNEL    NHYDout =[ "N7" ] , NHYDin =[ "S_N8" ] ,
702                  RDT=[ 1 ] ( mi n ) ,
703                  CHLGTH=[ 3750 ] ( m ) ,   CHSLOPE=[ 0.0533 ] ( % ) ,
704                                                    FPSLOPE=[ 0.0533 ] ( % ) ,
705                  SECNUM=[ 1.0 ] ,          NSEG=[ 3 ]
706                  ( SEGROUGH, SEGDI ST ( m ) ) =
707                    [ 0.12, -18.11
708                      -0.07, 17.22
709                      0.12, 590.05 ] NSEG t i m e s
710                  ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
711                    [ -433.21, 102.00 ]
712                    [ -425.34, 101.50 ]
713                    [ -377.56, 101.50 ]
714                    [ -366.23, 101.00 ]
715                    [ -202.60, 100.50 ]
716                    [ -96.25, 99.50 ]
717                    [ -68.36 99.00 ]
718                    [ -18.11, 98.50 ]
719                    [ -13.81, 97.50 ]

```



```

720 [ 13. 81, 97. 50]
721 [ 17. 22, 98. 50]
722 [ 161. 95, 98. 50]
723 [ 173. 11, 99. 00]
724 [ 314. 05, 99. 00]
725 [ 365. 52, 100. 00]
726 [ 404. 70, 99. 50]
727 [ 476. 74, 100. 50]
728 [ 502. 31, 101. 00]
729 [ 584. 69, 101. 00]
730 [ 585. 79, 101. 00]
731 [ 590. 05, 102. 00]
732 *%-----|-----
733 *#
734 *# Addition of Subwatershed 7 to Node 7
735 *#
736 ADD HYD          NHYDs um=[ "S_N7" ], NHYDs to add=[ "N7"+"SW_7" ]
737 *%-----|-----
738 SAVE HYD         NHYD=[ "S_N7" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ - 1 ]
739                 HYD_FI LENAME=[ "H_SN7" ]
740                 HYD_COMMENT=[ "flow at S_N7: N7 + SW_7" ]
741 *%-----|-----
742 *# Insertion of a reservoir to simulate the effects of the Richmond Fen.
743 *# Storage area and volumes were estimated from available topo maps.
744 *# Release rate from fen was assumed to be controlled by the downstream
745 *# river cross-section for summer conditions. It is was assumed that for up to
746 *# 0.75 m of water, the main channel of the river provided the storage. Above
747 *# this depth, the wetland starts to signigicantly store water.
748 *#
749 ROUTE RESERVOIR NHYDout =[ "RES_RF" ] , NHYDi n=[ "S_N7" ] ,
750                 RDT=[ 1 ] ( mi n ) ,
751                 TABLE of ( OUTFLOW STORAGE ) values
752                         ( cms ) - ( ha- m )
753                 TABLE of ( OUTFLOW STORAGE ) values
754                         ( cms ) - ( ha- m )
755                         [ 0. 0 , 0. 0 ]
756                         [ 0. 9051, 2. 40]
757                         [ 2. 907, 4. 13]
758                         [ 9. 744, 9. 18]
759                         [ 20. 304, 14. 96]
760                         [ 34. 167, 310. 21]
761                         [ 74. 993, 605. 46]
762                         [ 104. 876, 900. 71]
763                         [ 140. 56, 2892. 00]
764                         [ 225. 00, 3615. 63]
765                         [ - 1 , - 1 ] (max t wenty pts)
766                 NHYDovf=[ " " ] ,
767 *%-----|-----
768 SAVE HYD         NHYD=[ "RES_RF" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ - 1 ]
769                 HYD_FI LENAME=[ "H_Res RF" ]
770                 HYD_COMMENT=[ "out flow of Ri chmond Fen" ]
771 *%-----|-----
772 *#
773 *# Sum of hydrographs from Node 7 routed to Node 6
774 *# Section 5
775 *#
776 ROUTE CHANNEL   NHYDout =[ "N6" ] , NHYDi n=[ "RES_RF" ] ,
777                 RDT=[ 1 ] ( mi n ) ,
778                 CHLGTH=[ 3056 ] ( m ) , CHSLOPE=[ 0. 0818 ] ( % ) ,
779                 FPSLOPE=[ 0. 0818 ] ( % ) ,
780                 SECNUM=[ 1. 0 ] , NSEG=[ 5 ]
781                 ( SEGROUGH, SEGDI ST ( m ) ) =
782                 [ 0. 025, - 70. 8
783                 0. 1, - 23. 9
784                 - 0. 05, 23. 9
785                 0. 06, 39. 8

```

```

786           0. 05, 96. 3] NSEG times
787           ( DI STANCE ( m), ELEVATI ON ( m))=
788             [- 100. 8, 97. 00]
789             [- 70. 8, 96. 50]
790             [- 52. 0, 96. 00]
791             [- 35. 1, 95. 50]
792             [- 30. 6, 95. 00]
793             [- 23. 9, 94. 54]
794             [ 23. 9, 94. 54]
795             [ 39. 8, 95. 00]
796             [ 50. 4, 95. 50]
797             [ 93. 5, 96. 00]
798             [ 94. 9, 96. 50]
799             [ 96. 3, 97. 00]
800 *%-----|-----
801 *#
802 *# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
803 *#
804 ADD HYD           NHYDs um=[ "S_N6" ], NHYDs to add=[ "N6"+"SW_6"+"VG_DR" ]
805 *%-----|-----
806 *#
807 *# Sum of hydrographs from Node 6 routed to Node 5
808 *# Section 6
809 *#
810 ROUTE CHANNEL     NHYDout =[ "N5" ] , NHYDin =[ "S_N6" ] ,
811                   RDT=[ 1] ( mi n),
812                   CHLGTH=[ 1852] ( m),   CHSLOPE=[ 0. 0540] ( %),
813                                           FPSLOPE=[ 0. 0540] ( %),
814                   SECNUM=[ 1. 0],       NSEG=[ 3]
815                   ( SEGROUGH, SEGDI ST ( m))=
816                     [ 0. 035, - 131. 59
817                     - 0. 045, 48. 96
818                     0. 1, 239. 04] NSEG times
819                   ( DI STANCE ( m), ELEVATI ON ( m))=
820                     [- 686. 30, 94. 50]
821                     [- 675. 70, 94. 00]
822                     [- 492. 52, 93. 00]
823                     [- 467. 28, 94. 00]
824                     [- 131. 59, 94. 00]
825                     [- 92. 79, 92. 50]
826                     [- 18. 06, 91. 00]
827                     [ 18. 06, 91. 00]
828                     [ 43. 47, 92. 50]
829                     [ 48. 96, 94. 00]
830                     [ 177. 43, 94. 00]
831                     [ 239. 04, 94. 50]
832 *%-----|-----
833 *#
834 *# Addition of Subwatershed 5 and Flowing Creek to Node 5
835 *#
836 ADD HYD           NHYDs um=[ "S_N5" ], NHYDs to add=[ "N5"+"SW_5"+"FL_CK" ]
837 *%-----|-----
838 *#
839 *# Sum of hydrographs from Node 5 routed to Node 5A
840 *# Section 7
841 *#
842 ROUTE CHANNEL     NHYDout =[ "N5A" ] , NHYDin =[ "S_N5" ] ,
843                   RDT=[ 1] ( mi n),
844                   CHLGTH=[ 556] ( m),   CHSLOPE=[ 0. 0900] ( %),
845                                           FPSLOPE=[ 0. 0900] ( %),
846                   SECNUM=[ 1. 0],       NSEG=[ 4]
847                   ( SEGROUGH, SEGDI ST ( m))=
848                     [ 0. 04, - 41. 5
849                     0. 1, - 14. 0
850                     - 0. 045, 14. 0
851                     0. 1, 41. 1] NSEG times

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```

852 ( DI STANCE ( m) , ELEVATI ON ( m) ) =
853 [- 275. 8, 93. 00]
854 [- 248. 6, 92. 50]
855 [- 237. 0, 92. 00]
856 [- 219. 3, 91. 50]
857 [- 202. 1, 91. 50]
858 [- 186. 0, 92. 00]
859 [- 129. 2, 92. 00]
860 [- 117. 6, 91. 50]
861 [- 100. 6, 91. 00]
862 [- 41. 5, 91. 00]
863 [- 20. 0, 91. 00]
864 [- 14. 0, 90. 54]
865 [ 14. 0, 90. 54]
866 [ 15. 3, 91. 00]
867 [ 17. 3, 91. 50]
868 [ 38. 4, 92. 00]
869 [ 39. 8, 92. 50]
870 [ 41. 1, 93. 00]
871 *%-----|-----|
872 *#
873 *# Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
874 *#
875 ADD HYD NHYDs um=[ "S_N5A" ] , NHYDs t o add=[ "N5A"+"SW_5A2"+"SW_5A1" ]
876 *%-----|-----|
877 *#
878 *# Sum of hydrographs from Node 5A routed to Node 4
879 *# Section 8
880 *#
881 ROUTE CHANNEL NHYDout =[ "N4" ] , NHYDi n=[ "S_N5A" ] ,
882 RDT=[ 1 ] ( mi n) ,
883 CHLGTH=[ 4630 ] ( m) , CHSLOPE=[ 0. 0432 ] ( % ) ,
884 FPSLOPE=[ 0. 0432 ] ( % ) ,
885 SECNUM=[ 1. 0 ] , NSEG=[ 3 ]
886 ( SEGROUGH, SEGDI ST ( m) ) =
887 [ 0. 05, -28. 2
888 -0. 035, 28. 2
889 0. 05, 173. 1 ] NSEG t i mes
890 ( DI STANCE ( m) , ELEVATI ON ( m) ) =
891 [- 38. 9, 92. 00]
892 [- 35. 8, 91. 50]
893 [- 33. 3, 91. 00]
894 [- 28. 2, 90. 50]
895 [- 15. 0, 87. 48]
896 [- 5. 0, 88. 34]
897 [ 5. 0, 86. 20]
898 [ 15. 0, 88. 55]
899 [ 28. 2, 90. 50]
900 [ 29. 7, 91. 00]
901 [ 46. 5, 91. 00]
902 [ 127. 8, 91. 00]
903 [ 148. 7, 91. 50]
904 [ 173. 1, 92. 00]
905 *%-----|-----|
906 *#
907 *# Addition of Subwatershed 4 and Leamy Creek to Node 4
908 *#
909 ADD HYD NHYDs um=[ "S_N4" ] , NHYDs t o add=[ "N4"+"SW_4"+"LM_CK" ]
910 SAVE HYD NHYD=[ "S_N4" ] , # OF PCYCLES=[ - 1 ] , I CASEs h=[ 1 ]
911 HYD_COMMENT=[ "f l ow at S_N4" ]
912 *%-----|-----|
913 *#
914 *# Sum of hydrographs from Node 4 routed to Node 2
915 *# Section 9
916 *#
917 ROUTE CHANNEL NHYDout =[ "N2" ] , NHYDi n=[ "S_N4" ] ,

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918 RDT=[ 1] ( mi n),
919 CHLGTH=[ 1667] ( m), CHSLOPE=[ 0. 0600] ( %),
920 FPSLOPE=[ 0. 0600] ( %),
921 SECNUM=[ 1. 0], NSEG=[ 4]
922 ( SEGROUGH, SEGDI ST ( m))=
923 [ 0. 1, - 28. 0
924 - 0. 04, 28. 4
925 0. 06, 31. 7
926 0. 04, 80. 2] NSEG times
927 ( DI STANCE ( m), ELEVATI ON ( m))=
928 [- 36. 3, 92. 00]
929 [- 32. 6, 91. 50]
930 [- 30. 2, 91. 00]
931 [- 28. 0, 90. 45]
932 [- 15. 0, 87. 48]
933 [- 5. 0, 88. 34]
934 [ 5. 0, 86. 20]
935 [ 15. 0, 88. 55]
936 [ 28. 0, 90. 45]
937 [ 28. 4, 90. 50]
938 [ 30. 4, 91. 00]
939 [ 31. 7, 91. 50]
940 [ 80. 2, 92. 00]
941 *%-----|-----|
942 *#
943 *# Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2
944 *#
945 ADD HYD NHYDs um=[ "S_N2" ], NHYDs to add=[ "N2"+"SW_2"+"SM_DR"+"MO_DR" ]
946 *%-----|-----|
947 SAVE HYD NHYD=[ "S_N2" ], # OF PCYCLES=[ - 1], ICASEs h=[ - 1]
948 HYD_FI LENAME=[ "H_SN2" ]
949 HYD_COMMENT=[ "flow at S_N2 Jock River Gauge at Modie Dr." ]
950 *%-----|-----|
951 *#
952 *# Sum of hydrographs from Node 2 routed to Node 1
953 *# Section 10
954 *#
955 *#*****
956 *%READ HYD NHYD=[ "S_N2" ],
957 *% HYD_FI LENAME=[ "H_S_N2" ]
958 *%-----|-----|
959 *#
960 *# Hydrograph from Node 2 routed to Node 416
961 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 9025
962 *#
963 ROUTE CHANNEL NHYDout =["N_416" ] , NHYDin=["S_N2" ] ,
964 RDT=[ 1] ( mi n),
965 CHLGTH=[ 2327] ( m), CHSLOPE=[ 0. 0498] ( %),
966 FPSLOPE=[ 0. 0498] ( %),
967 SECNUM=[ 1. 0], NSEG=[ 3]
968 ( SEGROUGH, SEGDI ST ( m))=
969 [ 0. 075, - 23. 96
970 - 0. 055, 23. 96
971 0. 075, 157. 38] NSEG times
972 ( DI STANCE ( m), ELEVATI ON ( m))=
973 [- 336. 97, 93. 5]
974 [- 318. 85, 93]
975 [- 259, 92. 5]
976 [- 133. 18, 92]
977 [- 33. 17, 92]
978 [- 27. 21, 92]
979 [- 26. 14, 91. 5]
980 [- 24. 99, 91]
981 [- 23. 96, 90. 5]
982 [- 14. 33, 88. 26]
983 [- 0. 68, 88. 12]

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984 [ 14. 33, 88. 26]
985 [ 23. 96, 90. 5]
986 [ 32. 12, 91]
987 [ 43. 74, 91. 5]
988 [ 57. 09, 92]
989 [ 73. 53, 92. 5]
990 [ 108. 27, 93]
991 [ 125. 88, 93. 5]
992 [ 144. 81, 94]
993 [ 157. 38, 94. 5]
994 *%-----|-----|
995 *#*****|*****|
996 *# Catchment SW1a
997 *# - Portion of RVCA catchment SW1 outside of Reach 1 subwatershed
998 *# - Undeveloped agricultural land
999 *#*****|*****|
1000 CONTINUOUS NASHYD NHYD=[ "SW_1a" ], DT=[ 1] (mi n), AREA=[ 536. 42] ( ha),
1001 DWF=[ 0] ( cms), CN C=[ 72], IA=[ 4. 67] ( mm),
1002 N=[ 3], TP=[ 2. 79] hr s,
1003 Continuous simulation parameters:
1004 IaREcper=[ 4] ( hr s),
1005 SM N=[ - 1] ( mm), SMAX=[ - 1] ( mm), SK=[ 0. 010] / ( mm),
1006 InterEvent Time=[ 12] ( hr s)
1007 Baseflow simulation parameters:
1008 BaseFlowOption=[ 1],
1009 InitGWResVol=[ 50] ( mm), GWResK=[ 0. 96] ( mm/ day/ mm)
1010 VHydCond=[ 0. 055] ( mm/ hr), END=- 1
1011 *%-----|-----|
1012 * -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
before station 7245 on Jock River
1013 CONTINUOUS STANDHYD NHYD=[ "S-1-Okeefe" ], DT=[ 1] ( mi n), AREA=[ 44. 93] ( ha), XI MP=[ 0. 65],
TI MP=[ 0. 65], DWF=[ 0] ( cms),
1014 LOSS=[ 2], SCS curve number CN=[ 75], Pervious surfaces:
I A per=[ 4. 67] ( mm), SLPP=[ 2. 0] ( %),
1015 LGP=[ 40] ( m), MNP=[ 0. 25], SCP=[ 0] ( mi n), Impervious surfaces:
I A i mp=[ 1. 57] ( mm), SLPI=[ 0. 75] ( %),
1016 LGI=[ 547. 296] ( m), MNI=[ 0. 013], SCI=[ 0] ( mi n),
1017 Continuous simulation parameters:
1018 IaREcper=[ 4] ( hr s), IaRECI mp=[ 4] ( hr s),
1019 SM N=[ - 1] ( mm), SMAX=[ - 1] ( mm), SK=[ 0. 010] / ( mm),
1020 InterEvent Time=[ 12] ( hr s), END=- 1
1021 *%-----|-----|
1022 *COMPUTE DUALHYD NHYDin=[ "S-1-Okeefe" ], CINLET=[ 4. 796] ( cms), NI NLET=[ 1],
1023 * Mij NHYD=[ "S-1-OkM" ]
1024 * M nNHYD=[ "S-1-OkMN" ]
1025 * TM I STO=[ 9999999] ( cu- m)
1026 *%-----|-----|
1027 *ADD HYD NHYDs um=[ "S-1-OkS" ], NHYDs t o add=[ "S-1-OkM" +"S-1-OkMN" ]
1028 *%-----|-----|
1029 *ROUTE RESERVOIR NHYDout=[ "S-1-OkSR" ], NHYDin=[ "S-1-OkS" ],
1030 * RDT=[ 1] ( mi n),
1031 * TABLE of ( OUTFLOW STORAGE ) values
1032 * ( cms) - ( ha- m)
1033 * [ 0. 0, 0. 0 ]
1034 * [ 0. 5370, 1. 7917 ]
1035 * [ - 1, - 1 ] (max twenty pts)
1036 * NHYDovf=[ "S-1-OkSovf" ]
1037 *%-----|-----|
1038 ADD HYD NHYDs um=[ "SN_416" ], NHYDs t o add=[ "N_416"+"SW_1a"+"S-1-Okeefe" ]
1039 *%-----|-----|
1040 SAVE HYD NHYD=[ "SN_416" ], # OF PCYCLES=[ - 1], I CASEs h=[ 1]
1041 HYD_COMMENT=[ "Total Flows at Highway 416" ]
1042 *%-----|-----|
1043 *#
1044 *# Hydrograph from Node 416 routed to Node at Okeefe drain
1045 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 7245

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1046 *#
1047 ROUTE CHANNEL NHYDout =["N_OK"] , NHYDin=["SN_416"] ,
1048 RDT=[ 1]( min),
1049 CHLGTH=[ 497]( m), CHSLOPE=[ 0.3018]( %),
1050 FPSLOPE=[ 0.3018]( %),
1051 SECNUM=[ 1.0], NSEG=[ 3]
1052 ( SEGROUGH, SEGDI ST ( m))=
1053 [ 0.075, - 19.40
1054 - 0.055, 19.40
1055 0.075, 377.02] NSEG times
1056 ( DI STANCE ( m), ELEVATI ON ( m))=
1057 [- 1061.41, 92.50]
1058 [- 945.91, 92.00]
1059 [- 783.64, 91.50]
1060 [- 136.74, 91.00]
1061 [- 86.04, 91.00]
1062 [- 20.86, 91.00]
1063 [- 20.18, 90.50]
1064 [- 19.40, 90.00]
1065 [- 11.68, 86.89]
1066 [ 0.00, 86.10]
1067 [ 12.09, 86.81]
1068 [ 19.40, 90.00]
1069 [ 34.68, 90.50]
1070 [ 60.56, 91.00]
1071 [ 170.14, 91.00]
1072 [ 175.05, 90.50]
1073 [ 180.29, 90.00]
1074 [ 193.41, 90.00]
1075 [ 195.98, 90.50]
1076 [ 377.02, 92.50]
1077 *%-----|-----|
1078 *#*****|
1079 *# Catchment OKEEFE
1080 *# - To O'Keefe drain (north of the Jock)
1081 *# - Developed with assumed 43% imp.
1082 *# - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area
1083 513.02 HA)
1084 *# - 2020-11-20 Okeefe detailed model was added as per the NOVATECH SWWHYMD model
1085 (Citi-Gate 2014).
1086 *%-----|-----|
1087 *#*****|
1088 CONTINUOUS NASHYD NHYD=["O-1"], DT=[ 1] min, AREA=[ 63.72]( ha),
1089 DWF=[ 0]( cms), CNVC=[ 61], IA=[ 6.2]( mm), N=[ 3], TP=[ .9] hrs,
1090 Continuous simulation parameters:
1091 IaRECper=[ 4]( hrs),
1092 SMN=[ - 1]( mm), SMAX=[ - 1]( mm), SK=[ 0.010]/( mm),
1093 InterEventTime=[ 12]( hrs)
1094 Baseflow simulation parameters:
1095 BaseFlowOption=[ 1] ,
1096 InitGWResVol=[ 50]( mm), GWResK=[ 0.96]( mm/ day/ mm)
1097 VHydCond=[ 0.055]( mm/ hr), END=- 1
1098 *%-----|-----|
1099 *ROUTE FLOW THROUGH AREA 0-2
1100 ROUTE CHANNEL NHYDout =["O-1R"], NHYDin=["O-1"], RDT=[ 1]( min),
1101 CHLGTH=[ 960]( m), CHSLOPE=[ 0.63]( %), FPSLOPE=[ 0.63]( %),
1102 SECNUM=[ 1], NSEG=[ 3]
1103 ( SEGROUGH, SEGDI ST ( m))=[ 0.06, 4 -.043, 6 0.06, 10] NSEG times
1104 ( DI STANCE ( m), ELEVATI ON ( m))=[ 0.00, 2.0]
1105 [ 0.0, 2.0]
1106 [ 4.0, 0.0]
1107 [ 6.0, 0.0]
1108 [ 10.0, 2.0]

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1109 *%-----|-----|
1110 CONTINUOUS NASHYD NHYD=["O-2"], DT=[1] min, AREA=[28.61] (ha),
1111 DWF=[0] (cms), CN C=[57], IA=[5.2] (mm), N=[3], TP=[1.1] hrs,
1112 Continuous simulation parameters:
1113 IaRECper=[4] (hrs),
1114 SMN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1115 InterEventTime=[12] (hrs)
1116 Baseflow simulation parameters:
1117 BaseFlowOption=[1],
1118 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
1119 VHydCond=[0.055] (mm/hr), END=-1
1120 *%-----|-----|
1121 CONTINUOUS NASHYD NHYD=["O-4"], DT=[1] min, AREA=[46.94] (ha),
1122 DWF=[0] (cms), CN C=[49], IA=[9.2] (mm), N=[3], TP=[0.9] hrs,
1123 Continuous simulation parameters:
1124 IaRECper=[4] (hrs),
1125 SMN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1126 InterEventTime=[12] (hrs)
1127 Baseflow simulation parameters:
1128 BaseFlowOption=[1],
1129 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
1130 VHydCond=[0.055] (mm/hr), END=-1
1131 *%-----|-----|
1132 *TOTAL EXTERNAL FLOW NORTH OF O'KEEFE CT. CROSSING
1133 ADD HYD NHYDsum=["OKF-N"], NHYDstoadd=["O-1R"+"O-2"+"O-4"]
1134 *%-----|-----|
1135 *ROUTE FLOW THROUGH AREA O-6
1136 ROUTE CHANNEL ROUTE CHANNEL NHYDout=["OKF-NR"], NHYDin=["OKF-N"], RDT=[1] (min),
1137 CHLGTH=[210] (m), CHSLOPE=[.81] (%), FPSLOPE=[.81] (%),
1138 SECNUM=[1], NSEG=[3]
1139 (SEGROUGH, SEGDIST (m))=[0.043, 22.43 - 0.043, 25.07
1140 0.043, 45.54] NSEG times
1141 (DISTANCE (m), ELEVATION (m))=[0.00, 3.73]
1142 (14.62, 1.56)
1143 (18.41, 1.44)
1144 (22.43, 0.00)
1145 (25.07, 0.70)
1146 (29.10, 1.79)
1147 (33.73, 2.71)
1148 (45.54, 3.58)
1149 *%-----|-----|
1150 CONTINUOUS NASHYD NHYD=["O-6"], DT=[1] min, AREA=[16.46] (ha),
1151 DWF=[0] (cms), CN C=[43], IA=[9.2] (mm), N=[3], TP=[0.7] hrs,
1152 Continuous simulation parameters:
1153 IaRECper=[4] (hrs),
1154 SMN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1155 InterEventTime=[12] (hrs)
1156 Baseflow simulation parameters:
1157 BaseFlowOption=[1],
1158 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
1159 VHydCond=[0.055] (mm/hr), END=-1
1160 *%-----|-----|
1161 CONTINUOUS STANDHYD NHYD=["O-3"], DT=[1] (min), AREA=[39.67] (ha), XI MP=[0.15],
1162 T I MP=[0.30], DWF=[0] (cms),
1163 LOSS=[2], SCS curve number CN=[50], Pervious surfaces:
1164 IAper=[4.67] (mm), SLPP=[0.32] (%),
1165 LGP=[440] (m), MNP=[0.035], SCP=[0] (min), Impervious surfaces:
1166 IAimp=[1.57] (mm), SLPI=[0.32] (%),
1167 LGI=[1880] (m), MNI=[0.013], SCI=[0] (min),
1168 Continuous simulation parameters:
1169 IaRECper=[4] (hrs), IaRECimp=[4] (hrs),
1170 SMN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1171 InterEventTime=[12] (hrs), END=-1
1172 *%-----|-----|
1173 CONTINUOUS STANDHYD NHYD=["O-5"], DT=[1] (min), AREA=[60.63] (ha), XI MP=[0.13],
1174 T I MP=[0.26], DWF=[0] (cms),

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1171      LOSS=[ 2], SCS curve number CN=[ 61],
1172      Pervious surfaces: I Aper=[ 4.67] (mm), SLPP=[ 1.38] (%),
1173      LGP=[ 550] (m), MNP=[ 0.035], SCP=[ 0] (min), Impervious surfaces:
1174      I Aimp=[ 1.57] (mm), SLPI=[ 1.38] (%),
1175      LGI=[ 1450] (m), MNI=[ 0.013], SCI=[ 0] (min),
1176      Continuous simulation parameters:
1177      I aRECper=[ 4] (hrs), I aRECimp=[ 4] (hrs),
1178      SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
1179      InterEventTime=[ 12] (hrs), END=- 1
1180      *%-----|-----|
1181      *TOTAL EXTERNAL FLOWS WEST OF THE SITE AND NORTH OF O'KEEFE CRT
1182      *%-----|-----|
1183      ADD HYD      NHYDsum=[ "PT1"], NHYDs to add=[ "OKF-NR"+"O-3"+"O-5"+"O-6"]
1184      *%-----|-----|
1185      CONTINUOUS NASHYD      NHYD=[ "O-7"], DT=[ 1] min, AREA=[ 5.28] (ha),
1186      DWF=[ 0] (cms), CNC=[ 54], IA=[ 7.5] (mm), N=[ 3], TP=[ 0.6] hrs,
1187      Continuous simulation parameters:
1188      I aRECper=[ 4] (hrs),
1189      SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
1190      InterEventTime=[ 12] (hrs)
1191      Baseflow simulation parameters:
1192      BaseFlowOption=[ 1] ,
1193      InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm3/day/mm)
1194      VHydCond=[ 0.055] (mm/hr), END=- 1
1195      *%-----|-----|
1196      *ANALYSIS POINT 1 - TOTAL FLOW NORTH OF FALLOWFIELD DR. AND O'KEEFE CRT.
1197      ADD HYD      NHYDsum=[ "FF"], NHYDs to add=[ "PT1"+"O-7"]
1198      *%-----|-----|
1199      *ROUTE FLOW through O'Keefe Drain 1
1200      ROUTE CHANNEL      NHYDout=[ "DRAIN1"], NHYDin=[ "FF"], RDT=[ 1] (min),
1201      CHLGT=[ 302] (m), CHSLOPE=[ 1.00] (%), FPSLOPE=[ 1.00] (%),
1202      SECNUM=[ 1], NSEG=[ 3]
1203      ( SEGROUGH, SEGDIST (m))=[ 0.07, 13.45 -0.043, 16.55 0.07, 30.00] NSEG
1204      times
1205      ( DISTANCE (m), ELEVATION (m))=[ 0.00, 1.70]
1206      ( 3.45, 0.60)
1207      ( 13.45, 0.50)
1208      ( 14.45, 0.00)
1209      ( 15.55, 0.00)
1210      ( 16.55, 0.50)
1211      ( 26.55, 0.60)
1212      ( 30.00, 1.70)
1213      *%-----|-----|
1214      CONTINUOUS NASHYD      NHYD=[ "DI"], DT=[ 1] min, AREA=[ 1.17] (ha),
1215      DWF=[ 0] (cms), CNC=[ 84], IA=[ 9.0] (mm), N=[ 3], TP=[ 0.28] hrs,
1216      Continuous simulation parameters:
1217      I aRECper=[ 4] (hrs),
1218      SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
1219      InterEventTime=[ 12] (hrs)
1220      Baseflow simulation parameters:
1221      BaseFlowOption=[ 1] ,
1222      InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm3/day/mm)
1223      VHydCond=[ 0.055] (mm/hr), END=- 1
1224      *%-----|-----|
1225      CONTINUOUS STANDHYD      NHYD=[ "AI"], DT=[ 1] min, AREA=[ 2.50] (ha), XIMP=[ 0.68], TIMP=[ 0.85],
1226      DWF=[ 0] (cms), LOSS=[ 1]:
1227      Horton: Fo=[ 76.20] (mm/hr), Fc=[ 13.20] (mm/hr), DCAY=[ 4.14] (/hr),
1228      F=[ 0.00] (mm),
1229      Pervious areas: I Aper=[ 4.67] (mm), SLPP=[ 0.5] (%), LGP=[ 50] (m),
1230      MNP=[ 0.250], SCP=[ 0] (min),
1231      Impervious areas: I Aimp=[ 1.57] (mm), SLPI=[ 0.5] (%),
1232      LGI=[ 223.607] (m), MNI=[ 0.013], SCI=[ 0] (min),
1233      Continuous simulation parameters:
1234      I aRECper=[ 4] (hrs), I aRECimp=[ 4] (hrs), InterEventTime=[ 12] (hrs),
1235      END=- 1
1236      *%-----|-----|

```


1230 ROUTE RESERVOIR NHYDout=["A1-STR"], NHYDin=["A1"], RDT=[1](min),
1231 TABLE of (OUTFLOW STORAGE) values
1232 (cms) - (ha-m)
1233 [0.000 , 0.000]
1234 [0.035 , 0.038]
1235 [0.072 , 0.051]
1236 [0.100 , 0.059]
1237 [0.125 , 0.070]
1238 [0.160 , 0.074]
1239 [0.185 , 0.081]
1240 [-1 , -1] (max twenty pts)
1241 NHYDovf=["A1-OVF"]
1242 *%-----|-----|
1243 CONTINUOUS STANDHYD NHYD=["ST-2"], DT=[1]min, AREA=[0.59](ha), XI MP=[0.46],
1244 TIMP=[0.57], DWF=[0](cms), LOSS=[1]:
1245 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1246 F=[0.00](mm),
1247 Pervious areas: I A per=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1248 MNP=[0.250], SCP=[0](min),
1249 ImperVIOUS areas: I Ai mp=[1.57](mm), SLPI=[0.5](%),
1250 LGI=[108.628](m), MNI=[0.013], SCI=[0](min),
1251 Continuous simulation parameters:
1252 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
1253 END=-1
1254 *%-----|-----|
1255 ROUTE RESERVOIR NHYDout=["ST2STR"], NHYDin=["ST-2"], RDT=[1](min),
1256 TABLE of (OUTFLOW STORAGE) values
1257 (cms) - (ha-m)
1258 [0.000 , 0.0000]
1259 [0.052 , 0.0010]
1260 [0.053 , 0.0080]
1261 [-1 , -1] (max twenty pts)
1262 NHYDovf=["ST2OVF"]
1263 *%-----|-----|
1264 *%-----|-----|
1265 *TOTAL FLOW NORTH OF STRANDHERD DR. (EAST BRANCH) CROSSING
1266 *%-----|-----|
1267 CONTINUOUS NASHYD NHYD=["O-8"], DT=[1]min, AREA=[60.55](ha),
1268 DWF=[0](cms), CNV C=[69], I A=[4.0](mm), N=[3], TP=[1.0]hrs,
1269 Continuous simulation parameters:
1270 I a REC per=[4](hrs),
1271 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1272 I n t e r E v e n t T i m e=[12](hrs)
1273 Baseflow simulation parameters:
1274 BaseFlowOption=[1],
1275 I n i t G W R e s V o l=[50](mm), G W R e s K=[0.96](mm/day/mm)
1276 VHydCond=[0.055](mm/hr), END=-1
1277 *%-----|-----|
1278 ROUTE PIPE PTYPE=[2]rect, NHYDout=["O8PIPE"], RNUMBER=[1], PWDTH=[1800](mm),
1279 PHEIGHT=[1200](mm), PLNGTH=[335.1](m),
1280 PROUGH=[0.013], PSLOPE=[0.001](m/m), NHYDin=["O-8"], RDT=[1](min)
1281 *%-----|-----|
1282 *%-----|-----|
1283 ADD HYD NHYDs um=["ST2-IN"], NHYDs to
1284 add=["DRAINI"+"DI"+"A1-STR"+"A1-OVF"+"ST2STR"+"ST2OVF"+"O8PIPE"]
1285 *%-----|-----|
1286 CONTINUOUS STANDHYD NHYD=["A7"], DT=[1]min, AREA=[3.51](ha), XI MP=[0.68], TIMP=[0.85],
1287 DWF=[0](cms), LOSS=[1]:
1288 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1289 F=[0.00](mm),
1290 Pervious areas: I A per=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1291 MNP=[0.250], SCP=[0](min),
1292 ImperVIOUS areas: I Ai mp=[1.57](mm), SLPI=[0.5](%),
1293 LGI=[264.953](m), MNI=[0.013], SCI=[0](min),
1294 Continuous simulation parameters:
1295 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),

END=- 1

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1285 *%-----|-----|
1286 ROUTE RESERVOIR NHYDout=["A7-STR"], NHYDin=["A7"], RDT=[1](min),
1287 TABLE of ( OUTFLOW STORAGE ) values
1288 (cms) - (ha-m)
1289 [ 0.000 , 0.000 ]
1290 [ 0.049 , 0.054 ]
1291 [ 0.102 , 0.072 ]
1292 [ 0.140 , 0.082 ]
1293 [ 0.175 , 0.099 ]
1294 [ 0.225 , 0.105 ]
1295 [ 0.260 , 0.114 ]
1296 [ -1 , -1 ] (max twenty pts)
1297 NHYDovf=["A7-OVF"]
1298 *%-----|-----|
1299 CONTINUOUS STANDHYD NHYD=["ST-3"], DT=[1]min, AREA=[0.71](ha), XI MP=[0.46],
TI MP=[0.57], DWF=[0](cms), LOSS=[1]:
1300 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1301 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1302 ImperVIOUS areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[119.164](m), MNI=[0.013], SCI=[0](min),
1303 Continuous simulation parameters:
1304 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=- 1
1305 *%-----|-----|
1306 ROUTE RESERVOIR NHYDout=["ST3STR"], NHYDin=["ST-3"], RDT=[1](min),
1307 TABLE of ( OUTFLOW STORAGE ) values
1308 (cms) - (ha-m)
1309 [ 0.000 , 0.0000 ]
1310 [ 0.063 , 0.0010 ]
1311 [ 0.064 , 0.0094 ]
1312 [ -1 , -1 ] (max twenty pts)
1313 NHYDovf=["ST3OVF"]
1314 *%-----|-----|
1315 *ANALYSIS POINT 2 - TOTAL FLOW AT OUTLET OF STREET 2/3 INTERSECTION
1316 *%-----|-----|
1317 ADD HYD NHYDsum=["PT2ST3"], NHYDsto
add=["ST2-IN"+"A7-STR"+"A7-OVF"+"ST3STR"+"ST3OVF"]
1318 *%-----|-----|
1319 *ROUTE FLOW through O Keefe Drain 2
1320 ROUTE CHANNEL NHYDout=["DRAIN2"], NHYDin=["PT2ST3"], RDT=[1](min),
1321 CHLGTH=[592](m), CHSLOPE=[.23](%), FPSLOPE=[.23](%),
1322 SECNUM=[1], NSEG=[3]
1323 ( SEGROUGH, SEGDIST (m))=[0.07, 12.60 -0.043, 17.40 0.07, 30.00] NSEG
times
1324 ( DISTANCE (m), ELEVATION (m))=[0.00, 1.70]
1325 (2.60, 0.95)
1326 (12.60, 0.75)
1327 (14.10, 0.00)
1328 (15.90, 0.00)
1329 (17.40, 0.75)
1330 (27.40, 0.95)
1331 (30.00, 1.70)
1332 *%-----|-----|
1333 CONTINUOUS NASHYD NHYD=["D2"], DT=[1]min, AREA=[2.28](ha), DWF=[0](cms), CNVC=[84],
IA=[9.0](mm),
1334 N=[3], TP=[0.99]hrs,
1335 Continuous simulation parameters:
1336 IaRECper=[4](hrs),
1337 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1338 InterEventTime=[12](hrs)
1339 Baseflow simulation parameters:
1340 BaseFlowOption=[1],
1341 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
```

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1342          VHydCond=[ 0. 055] ( mm/ hr ) ,      END=- 1
1343 *%-----|-----|
1344 CONTINUOUS STANDHYD NHYD=[ " A17" ] , DT=[ 1] mi n , AREA=[ 12. 04] ( ha) , XI MP=[ 0. 68] ,
TI MP=[ 0. 85] , DWF=[ 0] ( cms) , LOSS=[ 1] :
1345 Horton: Fo=[ 76. 20] ( mm/ hr) , Fc=[ 13. 20] ( mm/ hr) , DCAY=[ 4. 14] ( / hr) ,
F=[ 0. 00] ( mm) ,
1346 Pervious areas: I A per =[ 4. 67] ( mm) , SLPP=[ 0. 5] ( % ) , LGP=[ 50] ( m) ,
MNP=[ 0. 250] , SCP=[ 0] ( mi n) ,
1347 ImperVIOUS areas: I A i mp=[ 1. 57] ( mm) , SLPI =[ 0. 5] ( % ) ,
LGI =[ 490. 714] ( m) , MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
1348 Continuous simulation parameters:
1349 I a REC per =[ 4] ( hr s) , I a REC i mp=[ 4] ( hr s) , I n t e r E v e n t T i m e =[ 12] ( hr s) ,
END=- 1
1350 *%-----|-----|
1351 ROUTE RESERVOIR NHYDout =[ " A17STR" ] , NHYD i n =[ " A17" ] , RDT=[ 1] ( mi n) ,
1352 TABLE of ( OUTFLOW STORAGE ) values
1353 ( cms) - ( ha- m)
1354 [ 0. 000 , 0. 000 ]
1355 [ 0. 169 , 0. 185 ]
1356 [ 0. 349 , 0. 248 ]
1357 [ 0. 482 , 0. 283 ]
1358 [ 0. 602 , 0. 338 ]
1359 [ 0. 771 , 0. 359 ]
1360 [ 0. 891 , 0. 391 ]
1361 [ - 1 , - 1 ] ( m a x t w e n t y p t s)
1362 NHYDovf =[ " A17OVF" ]
1363 *%-----|-----|
1364 CONTINUOUS STANDHYD NHYD=[ " ST- 4" ] , DT=[ 1] mi n , AREA=[ 0. 35] ( ha) , XI MP=[ 0. 46] ,
TI MP=[ 0. 57] , DWF=[ 0] ( cms) , LOSS=[ 1] :
1365 Horton: Fo=[ 76. 20] ( mm/ hr) , Fc=[ 13. 20] ( mm/ hr) , DCAY=[ 4. 14] ( / hr) ,
F=[ 0. 00] ( mm) ,
1366 Pervious areas: I A per =[ 4. 67] ( mm) , SLPP=[ 0. 5] ( % ) , LGP=[ 50] ( m) ,
MNP=[ 0. 250] , SCP=[ 0] ( mi n) ,
1367 ImperVIOUS areas: I A i mp=[ 1. 57] ( mm) , SLPI =[ 0. 5] ( % ) , LGI =[ 83. 666] ( m) ,
MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
1368 Continuous simulation parameters:
1369 I a REC per =[ 4] ( hr s) , I a REC i mp=[ 4] ( hr s) , I n t e r E v e n t T i m e =[ 12] ( hr s) ,
END=- 1
1370 *%-----|-----|
1371 ROUTE RESERVOIR NHYDout =[ " ST4STR" ] , NHYD i n =[ " ST- 4" ] , RDT=[ 1] ( mi n) ,
1372 TABLE of ( OUTFLOW STORAGE ) values
1373 ( cms) - ( ha- m)
1374 [ 0. 000 , 0. 0000 ]
1375 [ 0. 031 , 0. 0010 ]
1376 [ 0. 032 , 0. 0050 ]
1377 [ - 1 , - 1 ] ( m a x t w e n t y p t s)
1378 NHYDovf =[ " ST4OVF" ]
1379 *%-----|-----|
1380 CONTINUOUS STANDHYD NHYD=[ " A18" ] , DT=[ 1] mi n , AREA=[ 5. 30] ( ha) , XI MP=[ 0. 68] , TI MP=[ 0. 85] ,
DWF=[ 0] ( cms) , LOSS=[ 1] :
1381 Horton: Fo=[ 76. 20] ( mm/ hr) , Fc=[ 13. 20] ( mm/ hr) , DCAY=[ 4. 14] ( / hr) ,
F=[ 0. 00] ( mm) ,
1382 Pervious areas: I A per =[ 4. 67] ( mm) , SLPP=[ 0. 5] ( % ) , LGP=[ 50] ( m) ,
MNP=[ 0. 250] , SCP=[ 0] ( mi n) ,
1383 ImperVIOUS areas: I A i mp=[ 1. 57] ( mm) , SLPI =[ 0. 5] ( % ) ,
LGI =[ 325. 576] ( m) , MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
1384 Continuous simulation parameters:
1385 I a REC per =[ 4] ( hr s) , I a REC i mp=[ 4] ( hr s) , I n t e r E v e n t T i m e =[ 12] ( hr s) ,
END=- 1
1386 *%-----|-----|
1387 ROUTE RESERVOIR NHYDout =[ " A18STR" ] , NHYD i n =[ " A18" ] , RDT=[ 1] ( mi n) ,
1388 TABLE of ( OUTFLOW STORAGE ) values
1389 ( cms) - ( ha- m)
1390 [ 0. 000 , 0. 000 ]
1391 [ 0. 074 , 0. 082 ]
1392 [ 0. 154 , 0. 109 ]

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1393         [ 0.212 , 0.125 ]
1394         [ 0.265 , 0.149 ]
1395         [ 0.339 , 0.158 ]
1396         [ 0.392 , 0.172 ]
1397         [ -1 , -1 ] (max twenty pts)
1398         NHYDovf=[ "A18OVF" ]
1399 *%-----|-----|
1400 *ANALYSIS POINT 3 - TOTAL FLOW AT OUTLET OF STREET 4
1401 *%-----|-----|
1402 ADD HYD          NHYDsum=[ "PT3ST4" ], NHYDsto
add=[ "DRAIN2"+"D2"+"A17STR"+"A17OVF"+"ST4STR"+"ST4OVF"+"A18STR"+"A18OVF" ]
1403 *%-----|-----|
1404 *ROUTE FLOW through O Keefe Drain 3
1405 ROUTE CHANNEL   NHYDout=[ "DRAIN3" ], NHYDin=[ "PT3ST4" ], RDT=[ 1 ] (min),
1406                CHLGTH=[ 525 ] (m), CHSLOPE=[ .23 ] (%), FPSLOPE=[ .23 ] (%),
1407                SECNUM=[ 1 ], NSEG=[ 3 ]
1408                ( SEGROUGH, SEGDIST (m) )=[ 0.07, 12.50 -0.043, 17.50 0.07, 30.00 ] NSEG
times
1409                ( DISTANCE (m), ELEVATION (m) )=[ 0.00, 1.70 ]
1410                ( 2.50, 1.00 )
1411                ( 12.50, 0.80 )
1412                ( 14.10, 0.00 )
1413                ( 15.90, 0.00 )
1414                ( 17.50, 0.80 )
1415                ( 27.50, 1.00 )
1416                ( 30.00, 1.70 )
1417 *%-----|-----|
1418 CONTINUOUS NASHYD NHYD=[ "D3" ], DT=[ 1 ] min, AREA=[ 2.51 ] (ha),
1419                DWF=[ 0 ] (cms), CNVC=[ 86 ], IA=[ 8.7 ] (mm), N=[ 3 ], TP=[ 0.73 ] hrs,
1420                Continuous simulation parameters:
1421                IaRECper=[ 4 ] (hrs),
1422                SMN=[ -1 ] (mm), SMAX=[ -1 ] (mm), SK=[ 0.010 ] / (mm),
1423                InterEventTime=[ 12 ] (hrs)
1424                Baseflow simulation parameters:
1425                BaseFlowOption=[ 1 ],
1426                InitGWResVol=[ 50 ] (mm), GWResK=[ 0.96 ] (mm/day/mm)
1427                VHydCond=[ 0.055 ] (mm/hr), END=-1
1428 *%-----|-----|
1429 CONTINUOUS STANDHYD NHYD=[ "C1" ], DT=[ 1 ] min, AREA=[ 3.41 ] (ha), XI MP=[ 0.68 ], TI MP=[ 0.85 ],
DWF=[ 0 ] (cms), LOSS=[ 1 ]:
1430                Horton: Fo=[ 76.20 ] (mm/hr), Fc=[ 13.20 ] (mm/hr), DCAY=[ 4.14 ] (/hr),
F=[ 0.00 ] (mm),
1431                Pervious areas: IAper=[ 4.67 ] (mm), SLPP=[ 0.5 ] (%), LGP=[ 50 ] (m),
MNP=[ 0.250 ], SCP=[ 0 ] (min),
1432                Impervious areas: IAimp=[ 1.57 ] (mm), SLPI=[ 0.5 ] (%),
LGI=[ 261.151 ] (m), MNI=[ 0.013 ], SCI=[ 0 ] (min),
1433                Continuous simulation parameters:
1434                IaRECper=[ 4 ] (hrs), IaRECimp=[ 4 ] (hrs), InterEventTime=[ 12 ] (hrs),
END=-1
1435 *%-----|-----|
1436 ROUTE RESERVOIR NHYDout=[ "C1-STR" ], NHYDin=[ "C1" ], RDT=[ 1 ] (min),
1437                TABLE of ( OUTFLOW STORAGE ) values
1438                ( cms ) - ( ha-m )
1439                [ 0.000 , 0.000 ]
1440                [ 0.048 , 0.052 ]
1441                [ 0.099 , 0.070 ]
1442                [ 0.136 , 0.080 ]
1443                [ 0.170 , 0.096 ]
1444                [ 0.218 , 0.102 ]
1445                [ 0.252 , 0.111 ]
1446                [ -1 , -1 ] (max twenty pts)
1447                NHYDovf=[ "C1-OVF" ]
1448 *%-----|-----|
1449 CONTINUOUS STANDHYD NHYD=[ "ST-5" ], DT=[ 1 ] min, AREA=[ 0.45 ] (ha), XI MP=[ 0.46 ],
TI MP=[ 0.57 ], DWF=[ 0 ] (cms), LOSS=[ 1 ]:
1450                Horton: Fo=[ 76.20 ] (mm/hr), Fc=[ 13.20 ] (mm/hr), DCAY=[ 4.14 ] (/hr),

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1451 F=[ 0. 00] ( mm) ,
Pervious areas: I A per=[ 4. 67] ( mm) , SLPP=[ 0. 5] ( % ) , LGP=[ 50] ( m) ,
MNP=[ 0. 250] , SCP=[ 0] ( mi n) ,
1452 Impervious areas: I A i mp=[ 1. 57] ( mm) , SLPI=[ 0. 5] ( % ) , LGI =[ 94. 868] ( m) ,
MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
1453 Continuous simulation parameters:
1454 I a REC per=[ 4] ( hrs) , I a REC i mp=[ 4] ( hrs) , I nter Event Ti me=[ 12] ( hrs) ,
END=- 1
1455 *%-----|
1456 ROUTE RESERVOIR NHYDout =[ " ST5STR" ] , NHYDi n=[ " ST- 5" ] , RDT=[ 1] ( mi n) ,
1457 TABLE of ( OUTFLOW STORAGE ) values
1458 ( cms) - ( ha- m)
1459 [ 0. 000 , 0. 0000 ]
1460 [ 0. 040 , 0. 0010 ]
1461 [ 0. 041 , 0. 0062 ]
1462 [ - 1 , - 1 ] ( max t went y pt s)
1463 NHYDovf=[ " ST5OVF" ]
1464 *%-----|
1465 ADD HYD NHYDs um=[ " ST5- E" ] , NHYDs to
add=[ " DRAI N3" +" D3" +" C1- STR" +" C1- OVF" +" ST5STR" +" ST5OVF" ]
1466 *%-----|
1467 CONTINUOUS STANDHYD NHYD=[ " STRAND" ] , DT=[ 1] ( mi n) , AREA=[ 7. 59] ( ha) ,
1468 XI MP=[ 0. 64] , TI MP=[ 0. 85] , DWF=[ 0] ( cms) , LOSS=[ 1] :
1469 Horton: Fo=[ 76. 20] ( mm/ hr) , Fc=[ 13. 20] ( mm/ hr) , DCAY=[ 4. 14] ( / hr) ,
F=[ 0. 00] ( mm) ,
1470 Pervious areas: I A per=[ 4. 67] ( mm) , SLPP=[ 0. 5] ( % ) , LGP=[ 40] ( m) ,
MNP=[ 0. 250] , SCP=[ 0] ( mi n) ,
1471 Impervious areas: I A i mp=[ 1. 57] ( mm) , SLPI=[ 0. 5] ( % ) , LGI =[ 1230] ( m) ,
MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
1472 Continuous simulation parameters:
1473 I a REC per=[ 4] ( hrs) , I a REC i mp=[ 4] ( hrs) , I nter Event Ti me=[ 12] ( hrs) ,
END=- 1
1474 *%-----|
1475 ROUTE RESERVOIR NHYDout =[ " S- POND" ] , NHYDi n=[ " STRAND" ] , RDT=[ 1] ( mi n) ,
1476 TABLE of ( OUTFLOW STORAGE ) values
1477 ( cms) - ( ha- m)
1478 [ 0. 000 , 0. 000 ]
1479 [ 0. 033 , 0. 188 ]
1480 [ 0. 057 , 0. 253 ]
1481 [ 0. 104 , 0. 287 ]
1482 [ 0. 160 , 0. 336 ]
1483 [ 0. 340 , 0. 346 ]
1484 [ 0. 471 , 0. 360 ]
1485 [ 0. 824 , 0. 390 ]
1486 [ - 1 , - 1 ] ( max t went y pt s)
1487 NHYDovf=[ " S- OVF" ]
1488 *%-----|
1489 ADD HYD NHYDs um=[ " SSAOUT" ] , NHYDs to add=[ " ST5- E" +" S- POND" +" S- OVF" ]
1490 *%-----|
1491 SAVE HYD NHYD=[ " SSAOUT" ] , # OF PCYCLES=[ 5] , I CASEs h=[ 1]
1492 HYD_ COMMENT=[ " SSAOUT" ]
1493 *%-----|
1494 CONTINUOUS STANDHYD NHYD=[ " Area- A" ] , DT=[ 1] mi n , AREA=[ 66. 75] ( ha) , XI MP=[ 0. 64] ,
TI MP=[ 0. 80] , DWF=[ 0] ( cms) , LOSS=[ 1] :
1495 Horton: Fo=[ 76. 20] ( mm/ hr) , Fc=[ 13. 20] ( mm/ hr) , DCAY=[ 4. 14] ( / hr) ,
F=[ 0. 00] ( mm) ,
1496 Pervious areas: I A per=[ 4. 67] ( mm) , SLPP=[ 0. 5] ( % ) , LGP=[ 50] ( m) ,
MNP=[ 0. 250] , SCP=[ 0] ( mi n) ,
1497 Impervious areas: I A i mp=[ 1. 57] ( mm) , SLPI=[ 0. 5] ( % ) ,
LGI =[ 1155. 422] ( m) , MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
1498 Continuous simulation parameters:
1499 I a REC per=[ 4] ( hrs) , I a REC i mp=[ 4] ( hrs) , I nter Event Ti me=[ 12] ( hrs) ,
END=- 1
1500 *%-----|
1501 SAVE HYD NHYD=[ " Area- A" ] , # OF PCYCLES=[ 1] , I CASEs h=[ 1]
1502 HYD_ COMMENT=[ " SMMF- A I nflow" ]

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1503 *%-----|-----|
1504 ROUTE RESERVOIR NHYDout=["SWMF-A"], NHYDin=["Area-A"], RDT=[1](min),
1505 TABLE of ( OUTFLOW STORAGE ) values
1506 (cms) - (ha-m)
1507 [ 0.000 , 0.000 ]
1508 [ 0.103 , 1.077 ]
1509 [ 0.128 , 1.749 ]
1510 [ 0.382 , 2.282 ]
1511 [ 0.703 , 2.582 ]
1512 [ 1.256 , 2.978 ]
1513 [ 1.567 , 3.202 ]
1514 [ 1.955 , 3.493 ]
1515 [ 2.100 , 3.600 ]
1516 [ -1 , -1 ] (max twenty pts)
1517 NHYDovf=["SWVAOV"]
1518 *%-----|-----|
1519 SAVE HYD NHYD=["SWMF-A"], # OF PCYCLES=[1], ICASEsh=[1]
1520 HYD_COMMENT=["SMMF-A Outflow"]
1521 *%-----|-----|
1522 *ANALYSIS POINT 4 - TOTAL FLOW AT OUTLET OF STREET 5
1523 *%-----|-----|
1524 ADD HYD NHYDs um=["PT4ST5"], NHYDs to add=["SSAOUT"+"SWMF-A"+"SWVAOV"]
1525 *%-----|-----|
1526 CONTINUOUS STANDHYD NHYD=["C6"], DT=[1]min, AREA=[1.87](ha), XI MP=[0.68], TI MP=[0.85],
DWF=[0](cms), LOSS=[1]:
1527 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1528 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1529 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[193.391](m), MNI=[0.013], SCI=[0](min),
1530 Continuous simulation parameters:
1531 IARECper=[4](hrs), IARECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1532 *%-----|-----|
1533 ROUTE RESERVOIR NHYDout=["C6-STR"], NHYDin=["C6"], RDT=[1](min),
1534 TABLE of ( OUTFLOW STORAGE ) values
1535 (cms) - (ha-m)
1536 [ 0.000 , 0.000 ]
1537 [ 0.026 , 0.029 ]
1538 [ 0.054 , 0.038 ]
1539 [ 0.075 , 0.044 ]
1540 [ 0.093 , 0.052 ]
1541 [ 0.120 , 0.056 ]
1542 [ 0.138 , 0.061 ]
1543 [ -1 , -1 ] (max twenty pts)
1544 NHYDovf=["C6-OVF"]
1545 *%-----|-----|
1546 CONTINUOUS STANDHYD NHYD=["C7"], DT=[1]min, AREA=[1.62](ha), XI MP=[0.68], TI MP=[0.85],
DWF=[0](cms), LOSS=[1]:
1547 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1548 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1549 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[180.000](m), MNI=[0.013], SCI=[0](min),
1550 Continuous simulation parameters:
1551 IARECper=[4](hrs), IARECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1552 *%-----|-----|
1553 ROUTE RESERVOIR NHYDout=["C7-STR"], NHYDin=["C7"], RDT=[1](min),
1554 TABLE of ( OUTFLOW STORAGE ) values
1555 (cms) - (ha-m)
1556 [ 0.000 , 0.000 ]
1557 [ 0.023 , 0.025 ]
1558 [ 0.047 , 0.033 ]

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1559          [ 0.065 , 0.038 ]
1560          [ 0.081 , 0.045 ]
1561          [ 0.104 , 0.048 ]
1562          [ 0.120 , 0.053 ]
1563          [ -1 , -1 ] (max twenty pts)
1564          NHYDovf=["C7-OVF"]
1565 *%-----|-----|
1566 CONTINUOUS STANDHYD NHYD=["ST-6"], DT=[1] min, AREA=[0.41](ha), XI MP=[0.46], TI MP=[0.57],
DWF=[0](cms), LOSS=[1]:
1567 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1568 Pervious areas: I A per=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1569 Impervious areas: I A i mp=[1.57](mm), SLPI=[0.5](%), LGI=[90.554](m),
MNI=[0.013], SCI=[0](min),
1570 Continuous simulation parameters:
1571 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
1572 *%-----|-----|
1573 ROUTE RESERVOIR NHYDout=["ST6STR"], NHYDin=["ST-6"], RDT=[1](min),
1574 TABLE of ( OUTFLOW STORAGE ) values
1575 (cms) - (ha-m)
1576 [ 0.000 , 0.0000 ]
1577 [ 0.036 , 0.0010 ]
1578 [ 0.037 , 0.0058 ]
1579 [ -1 , -1 ] (max twenty pts)
1580          NHYDovf=["ST6OVF"]
1581 *%-----|-----|
1582 *ANALYSIS POINT 5 - TOTAL FLOW AT OUTLET OF STREET 6
1583 *%-----|-----|
1584 ADD HYD NHYDsum=["PT5ST6"], NHYDsto
add=["PT4ST5"+"C6-STR"+"C6-OVF"+"C7-STR"+"C7-OVF"+"ST6STR"+"ST6OVF"]
1585 *%-----|-----|
1586 ROUTE FLOW through O Keefe Drain 4
1587 ROUTE CHANNEL NHYDout=["DRAIN4"], NHYDin=["PT5ST6"], RDT=[1](min),
1588 CHLGTH=[324](m), CHSLOPE=[.10](%), FPSLOPE=[.10](%),
1589 SECNUM=[1], NSEG=[3]
1590 ( SEGROUGH, SEGDI ST (m))=[0.07, 12.00 -0.043, 18.00 0.07, 30.00] NSEG
t i m e s
1591 ( DI STANCE (m), ELEVATION (m))=[0.00, 2.00]
1592 (2.00, 1.20)
1593 (12.00, 1.00)
1594 (14.00, 0.00)
1595 (16.00, 0.00)
1596 (18.00, 1.00)
1597 (28.00, 1.20)
1598 (30.00, 2.00)
1599 *%-----|-----|
1600 CONTINUOUS NASHYD NHYD=["D4"], DT=[1] min, AREA=[1.73](ha), DWF=[0](cms), CNV C=[88],
I A=[8.4](mm),
1601 N=[3], TP=[0.60] hrs,
1602 Continuous simulation parameters:
1603 I a REC per=[4](hrs),
1604 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1605 I n t e r E v e n t T i m e=[12](hrs)
1606 Baseflow simulation parameters:
1607 BaseFlowOption=[1],
1608 I n i t G W R e s V o l=[50](mm), G W R e s K=[0.96](mm/day/mm)
1609 VHydCond=[0.055](mm/hr), END=-1
1610 *%-----|-----|
1611 CONTINUOUS STANDHYD NHYD=["Area-B"], DT=[1] min, AREA=[24.04](ha), XI MP=[0.62],
TI MP=[0.77], DWF=[0](cms), LOSS=[1]:
1612 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1613 Pervious areas: I A per=[4.67](mm), SLPP=[1.4](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),

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1614      Impervious areas: IAImp=[ 1.57](mm), SLPI=[ 1.4](%),
1615      LGI=[ 693.397](m), MNI=[ 0.013], SCI=[ 0](min),
1616      Continuous simulation parameters:
1617      IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
1618      END=- 1
1619
1620 *%-----|-----|
1621 ROUTE RESERVOIR      NHYDout=["SWMF- B"], NHYDin=["Area- B"], RDT=[ 1](min),
1622      TABLE of ( OUTFLOW STORAGE ) values
1623      (cms) - (ha-m)
1624      [ 0.000 , 0.000 ]
1625      [ 0.025 , 0.090 ]
1626      [ 0.175 , 0.510 ]
1627      [ 0.350 , 0.710 ]
1628      [ 0.495 , 0.820 ]
1629      [ 0.648 , 0.980 ]
1630      [ 0.965 , 1.045 ]
1631      [ 1.072 , 1.140 ]
1632      [ -1 , -1 ] (max twenty pts)
1633      NHYDovf=["SWMBOVF"]
1634
1635 *%-----|-----|
1636 ADD HYD              NHYDsum=["D4- EX"], NHYDs to add=["DRAIN4"+"D4"+"SWMF- B"+"SWMBOVF"]
1637
1638 *%-----|-----|
1639 *ROUTE FLOW THROUGH O Keefe Drain 5
1640 * JFSA: Nov. 2020, added endpoints to close X-Section
1641 ROUTE CHANNEL      NHYDout=["DRAIN5"], NHYDin=["D4- EX"], RDT=[ 1](min),
1642      CHLGTH=[ 413.0](m), CHSLOPE=[ 0.16](%), FPSLOPE=[ 0.16](%),
1643      SECNUM=[ 1], NSEG=[ 3]
1644      ( SEGROUGH, SEGDIST (m))=[ 0.043, 12.29 -0.033, 17.97
1645      0.043, 32.84] NSEG times
1646      ( DISTANCE (m), ELEVATION (m))=(-0.01, 2.50)
1647      [ 0.00, 1.41]
1648      [ 6.13, 0.97]
1649      [ 12.29, 0.89]
1650      [ 15.71, 0.00]
1651      [ 17.97, 0.39]
1652      [ 23.04, 0.35]
1653      [ 32.83, 0.96]
1654      (32.84, 2.50)
1655
1656 *%-----|-----|
1657 CONTINUOUS NASHYD   NHYD=["D5"], DT=[ 1]min, AREA=[ 1.90](ha),
1658      DWF=[ 0](cms), CNVC=[ 86], IA=[ 8.7](mm), N=[ 3], TP=[ 0.69]hrs,
1659      Continuous simulation parameters:
1660      IARECper=[ 4](hrs),
1661      SMIN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1662      InterEventTime=[ 12](hrs)
1663      Baseflow simulation parameters:
1664      BaseFlowOption=[ 1],
1665      InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
1666      VHydCond=[ 0.055](mm/hr), END=- 1
1667
1668 *%-----|-----|
1669 *EXTERNAL FLOWS SOUTHEAST OF THE SITE NORTH OF McKENNA CASEY DR.
1670 CONTINUOUS NASHYD   NHYD=["O-13SDF"], DT=[ 1]min, AREA=[ 9.74](ha),
1671      DWF=[ 0](cms), CNVC=[ 81], IA=[ 4.0](mm), N=[ 3], TP=[ .43]hrs,
1672      Continuous simulation parameters:
1673      IARECper=[ 4](hrs),
1674      SMIN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1675      InterEventTime=[ 12](hrs)
1676      Baseflow simulation parameters:
1677      BaseFlowOption=[ 1],
1678      InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
1679      VHydCond=[ 0.055](mm/hr), END=- 1
1680
1681 *%-----|-----|
1682 *SNOW DISPOSAL FACILITY
1683 *PARAMETERS BASED ON ROBINSON 2006 MODEL
1684 ROUTE RESERVOIR      NHYDout=["SDF"], NHYDin=["O-13SDF"], RDT=[ 1](min),
1685      TABLE of ( OUTFLOW STORAGE ) values

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1678             ( cms ) - ( ha - m )
1679             [ 0. 000, 0. 000 ]
1680             [ 0. 150, 0. 600 ]
1681             ( 0. 200, 1. 500 )
1682             [ - 1 , - 1 ] ( max t w e n t y p t s )
1683             NHYDovf=[ " OVFSDF " ]
1684 *%-----|-----|
1685 *ANALYSIS POINT 6 - McKenna Casey Dr.
1686 *%-----|-----|
1687 ADD HYD             NHYDsum=[ " PT6MC " ], NHYDs to add=[ " DRAIN5 "+" D5 "+" SDF " ]
1688 *%-----|-----|
1689 CONTINUOUS NASHYD  NHYD=[ " O- 15 " ], DT=[ 1 ] mi n , AREA=[ 10. 67 ] ( ha ) ,
1690                   DWF=[ 0 ] ( cms ) , CN C=[ 82 ] , I A=[ 7. 5 ] ( mm ) , N=[ 3 ] , TP=[ 0. 30 ] hr s ,
1691                   Continuous simulation parameters:
1692                   IaREcper=[ 4 ] ( hr s ) ,
1693                   SM N=[ - 1 ] ( mm ) ,   SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
1694                   InterEventTime=[ 12 ] ( hr s )
1695                   Baseflow simulation parameters:
1696                   BaseFlowOption=[ 1 ] ,
1697                   InitGWResVol=[ 50 ] ( mm ) ,   GWResK=[ 0. 96 ] ( mm / day / mm )
1698                   VHydCond=[ 0. 055 ] ( mm / hr ) ,   END=- 1
1699 *%-----|-----|
1700 *TOTAL FLOW NORTH OF McKenna Casey Dr.
1701 ADD HYD             NHYDsum=[ " M C " ], NHYDs to add=[ " PT6MC "+" O- 15 " ]
1702 *%-----|-----|
1703 *ROUTE FLOW THROUGH AREA O- 14
1704 * JFSA: Nov. 2020, added end points to close X-section
1705 ROUTE CHANNEL      NHYDout=[ " O- 14Ch " ], NHYDin=[ " M C " ], RDT=[ 1 ] ( mi n ) ,
1706                   CHLGH=[ 845. 3 ] ( m ) , CHSLOPE=[ 0. 10 ] ( % ) , FPSLOPE=[ 0. 10 ] ( % ) ,
1707                   SECNUM=[ 1 ] , NSEG=[ 3 ]
1708                   ( SEGROUGH, SEGDI ST ( m ) )=[ 0. 06, 15. 00 - 0. 033, 18. 04 0. 06, 31. 85 ] NSEG
1709                   t i m e s
1710                   ( DI STANCE ( m ) , ELEVATI ON ( m ) )=[ - 0. 01, 2. 5
1711                   ( 0. 00, 1. 53 ]
1712                   ( 5. 56, 1. 47 )
1713                   ( 9. 21, 1. 45 )
1714                   ( 12. 45, 1. 53 )
1715                   ( 13. 70, 1. 50 )
1716                   ( 15. 00, 0. 69 )
1717                   ( 15. 34, 0. 00 )
1718                   ( 16. 51, 0. 05 )
1719                   ( 17. 30, 0. 17 )
1720                   ( 18. 04, 0. 74 )
1721                   ( 19. 29, 1. 32 )
1722                   ( 22. 73, 1. 47 )
1723                   ( 31. 84, 1. 41 )
1724                   ( 31. 85, 2. 50 )
1725 *%-----|-----|
1726 *% -Change O- 14 from NASHYD to STANDHYD, name it " S- 1- Okeefe " and add it to S- 1
1727 subcatchment based on Project 1474- BCDC, JFSA, Nov. 2020
1728 *% -JFSA 2021- 02- 16, add detailed subcatchment drainage area for each subcatchment
1729 in Corrigan sub- catchment. After adding part of O- 14 to S_ 1 sub- catchment so O- 14
1730 becomes 5 ha instead of 30. 02 ha and TP becomes 0. 133 ( 5 * 0. 8 / 30. 02 ) instead of 0. 8
1731 CONTINUOUS NASHYD  NHYD=[ " O- 14 " ], DT=[ 1 ] mi n , AREA=[ 5 ] ( ha ) ,
1732                   DWF=[ 0 ] ( cms ) , CN C=[ 82 ] , I A=[ 7. 5 ] ( mm ) , N=[ 3 ] , TP=[ 0. 133 ] hr s ,
1733                   Continuous simulation parameters:
1734                   IaREcper=[ 4 ] ( hr s ) ,
1735                   SM N=[ - 1 ] ( mm ) ,   SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
1736                   InterEventTime=[ 12 ] ( hr s )
1737                   Baseflow simulation parameters:
1738                   BaseFlowOption=[ 1 ] ,
1739                   InitGWResVol=[ 50 ] ( mm ) ,   GWResK=[ 0. 96 ] ( mm / day / mm )
1740                   VHydCond=[ 0. 055 ] ( mm / hr ) ,   END=- 1
1741 *
1742 *%-----|-----|
1743 *ANALYSIS POINT 7 - JOCK RIVER

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1740 * 2020-12-01 To Foster Drain
1741 * 2020-12-01 replace ("PT7JR") by ("OKEEFE")
1742 *%-----|-----
1743 ADD HYD          NHYDs um=["OKEEFE"], NHYDs  to add=["O-14Ch"+"O-14"]
1744 *%-----|-----
1745 *CONTINUOUS STANDHYD NHYD=["OKEEFE"], DT=[1](mi n), AREA=[448](ha),
1746 *          XI MP=[0.65], TI MP=[0.65], DWF=[0](cms), LOSS=[2],
1747 *          SCS curve number CN=[77],
1748 *          Pervious surfaces: I A per=[4.67](mm), SLPP=[0.5](%),
1749 *          LGP=[40](m), MNP=[0.25], SCP=[0](mi n),
1750 *          Impervious surfaces: I A i mp=[1.57](mm), SLPI=[0.5](%),
1751 *          LGI=[1728](m), MNI=[0.013], SCI=[0](mi n),
1752 *          Continuous simulation parameters:
1753 *          I a REC per=[4](hrs), I a REC i mp=[4](hrs),
1754 *          SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1755 *          Inter Event Ti me=[18](hrs), END=-1
1756 *#*****
1757 *#      Okeefe Pond
1758 *#      - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1759 *#      and a ratio of the catchment area to the West Clarke pond rating curve
1760 *#      from the M55 for the next coordinates
1761 *#*****
1762 *ROUTE RESERVOIR  NHYDout=["P_OKE"], NHYDi n=["OKEEFE"],
1763 *          RDT=[1](mi n),
1764 *          TABLE of ( OUTFLOW STORAGE ) values
1765 *          (cms) - (ha-m)
1766 *          [ 0.0 , 0.0]
1767 *          [ 14.13 , 13.0]
1768 *          [ -1 , -1 ] (maximum one hundred pairs of points)
1769 *          NHYDovf=["ok-OVF"],
1770 *%-----|-----
1771 * -JFSA 2021-02-25 "S-1-D2" and "S-1-D3" are part of S-1 sub-catchment. They are
1772 * moved to drain before station 6215 on Jock River
1773 *CONTINUOUS STANDHYD NHYD=["S-1-D2"], DT=[1](mi n), AREA=[18.67](ha), XI MP=[0.65],
1774 *          TI MP=[0.65], DWF=[0](cms),
1775 *          LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
1776 *          I A per=[4.67](mm), SLPP=[2.0](%),
1777 *          LGP=[40](m), MNP=[0.25], SCP=[0](mi n), Impervious surfaces:
1778 *          I A i mp=[1.57](mm), SLPI=[0.75](%),
1779 *          LGI=[352.798](m), MNI=[0.013], SCI=[0](mi n),
1780 *          Continuous simulation parameters:
1781 *          I a REC per=[4](hrs), I a REC i mp=[4](hrs),
1782 *          SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1783 *          Inter Event Ti me=[12](hrs), END=-1
1784 *%-----|-----
1785 *CONTINUOUS NASHYD  NHYD=["S-1-D2"], DT=[1]mi n, AREA=[18.67](ha),
1786 *          DWF=[0](cms), CNV C=[77], I A=[4.67](mm),
1787 *          N=[3], TP=[1.120]hrs,
1788 *          Continuous simulation parameters:
1789 *          I a REC per=[4](hrs),
1790 *          SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1791 *          Inter Event Ti me=[12](hrs)
1792 *          Baseflow simulation parameters:
1793 *          BaseFl owOpt ion=[1] ,
1794 *          I ni t GWRes Vol =[50](mm), GWRes K=[0.96](mm/day/mm)
1795 *          VHydCond=[0.055](mm/hr), END=-1
1796 *%-----|-----
1797 *COMPUTE DUALHYD  NHYDi n=["S-1-D2"], CI NLET=[2.062](cms), NI NLET=[1],
1798 *          M a j NHYD=["S-1-D2J"]
1799 *          M nNHYD=["S-1-D2N"]
1800 *          TMJ STO=[9999999](cu-m)
1801 *%-----|-----
1802 *ADD HYD          NHYDs um=["S-1-D2S"], NHYDs  to add=["S-1-D2J"+"S-1-D2N"]
1803 *%-----|-----
1804 *ROUTE RESERVOIR  NHYDout=["S-1-D2R"] ,NHYDi n=["S-1-D2S"] ,

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```

1801 *          RDT=[ 1](mi n),
1802 *          TABLE of ( OUTFLOW STORAGE ) values
1803 *                ( cms ) - ( ha- m)
1804 *                [ 0.0      , 0.0 ]
1805 *                [ 0.2231, 0.7445 ]
1806 *                [   -1   ,  -1   ] (max twenty pts)
1807 *          NHYDovf=[ "S- 1- D2Rovf" ]
1808 *%-----|-----
1809 CONTINUOUS STANDHYD NHYD=[ "S- 1- D3" ], DT=[ 1](mi n), AREA=[ 6.79](ha), XI MP=[ 0.65],
TI MP=[ 0.65], DWF=[ 0](cms),
1810 LOSS=[ 2], SCS curve number CN=[ 75], Pervious surfaces:
1811 IAper=[ 4.67](mm), SLPP=[ 2.0](%),
LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n), Impervious surfaces:
1812 IAi mp=[ 1.57](mm), SLPI=[ 0.75](%),
1813 LGI=[ 212.760](m), MNI=[ 0.013], SCI=[ 0](mi n),
1814 Continuous simulation parameters:
1815 IaRECPper=[ 4](hrs), IaRECI mp=[ 4](hrs),
1816 SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1817 InterEvent Ti me=[ 12](hrs), END=- 1
1818 *%-----|-----
1819 *CONTINUOUS NASHYD NHYD=[ "S- 1- D3" ], DT=[ 1]mi n, AREA=[ 6.79](ha),
1820 * DWF=[ 0](cms), CN C=[ 77], IA=[ 4.67](mm),
1821 * N=[ 3], TP=[ 1.281]hrs,
1822 * Continuous simulation parameters:
1823 * IaRECPper=[ 4](hrs),
1824 * SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1825 * InterEvent Ti me=[ 12](hrs)
1826 * Baseflow simulation parameters:
1827 * BaseFl owOpt ion=[ 1],
1828 * Ini tGWRes Vol =[ 50](mm), GWRes K=[ 0.96](mm/ day/ mm)
1829 * VHydCond=[ 0.055](mm/ hr), END=- 1
1830 *%-----|-----
1831 *COMPUTE DUALHYD NHYDi n=[ "S- 1- D3" ], CI NLET=[ 0.719](cms), NI NLET=[ 1],
1832 * Mj NHYD=[ "S- 1- D3J" ]
1833 * M nNHYD=[ "S- 1- D3N" ]
1834 * TM STO=[ 9999999](cu- m)
1835 *%-----|-----
1836 *ADD HYD NHYDs um=[ "S- 1- D3S" ], NHYDs to add=[ "S- 1- D3J"+"S- 1- D3N" ]
1837 *%-----|-----
1838 *ROUTE RESERVOIR NHYDout=[ "S- 1- D3R" ], NHYDi n=[ "S- 1- D3S" ],
1839 * RDT=[ 1](mi n),
1840 *          TABLE of ( OUTFLOW STORAGE ) values
1841 *                ( cms ) - ( ha- m)
1842 *                [ 0.0      , 0.0 ]
1843 *                [ 0.0811, 0.2708 ]
1844 *                [   -1   ,  -1   ] (max twenty pts)
1845 *          NHYDovf=[ "S- 1- D3Rovf" ]
1846 *%-----|-----
1847 *ADD HYD NHYDs um=[ "SN_OK" ], NHYDs to add=[ "N_OK"+"OKEEFE"+"S- 1- D2"+"S- 1- D3" ]
1848 *%-----|-----
1849 *SAVE HYD NHYD=[ "SN_OK" ], # OF PCYCLES=[ -1], I CASEs h=[ 1]
HYD_COMMENT=[ "Total Fl ows at Okeefe Drain" ]
1850 *%-----|-----
1851 *#
1852 *# Hydrograph from Node Okeefe routed to Node at Foster Drain
1853 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
1854 *#
1855 *ROUTE CHANNEL NHYDout=[ "N_FO" ], NHYDi n=[ "SN_OK" ],
1856 * RDT=[ 1](mi n),
1857 * CHLGTH=[ 1183](m), CHSLOPE=[ 0.0761](%),
1858 * FPSLOPE=[ 0.0761](%),
1859 * SECNUM=[ 1.0], NSEG=[ 3]
1860 * ( SEGROUGH, SEGDI ST (m))=
1861 * [ 0.050, -33.89
1862 * -0.035, 31.59
1863 * 0.050, 34.41] NSEG ti mes

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1864      ( DI STANCE ( m), ELEVATI ON ( m) ) =
1865      [- 794. 18, 91. 00]
1866      [- 775. 41, 91. 50]
1867      [- 702. 63, 91. 50]
1868      [- 546. 19, 91. 50]
1869      [- 529. 54, 91. 50]
1870      [- 323. 44, 91. 00]
1871      [- 320. 71, 91. 00]
1872      [- 183. 59, 91. 00]
1873      [- 182. 54, 90. 50]
1874      [- 181. 36, 90. 00]
1875      [- 177. 37, 90. 00]
1876      [- 87. 70, 90. 00]
1877      [- 33. 89, 90. 00]
1878      [- 18. 52, 86. 88]
1879      [ 0. 00, 85. 20]
1880      [ 16. 20, 86. 83]
1881      [ 31. 59, 90. 00]
1882      [ 33. 03, 90. 50]
1883      [ 34. 41, 91. 00]
1884      *%-----|-----|
1885      *#*****|
1886      *#      Catchment FOSTER
1887      *#      - To Foster ditch (north of the Jock)
1888      *#      - Partially developed (medium density); remaining agricultural
1889      *#      - 2020-12-01 JFSA Foster area is 332 as per Foster SWF Environmental Study
1890      *#      - 2020-12-01 decrease Foster drainage area from (373 HA) to (307.98 HA) after
1891      *#      - 2021-02-12 update Foster area to 325.44 ha as measured from QGIS
1892      *#*****|
1893      CONTINUOUS STANDHYD NHYD=[ "FOSTER" ], DT=[ 1] mi n, AREA=[ 325. 44] ( ha),
1894      XI MP=[ 0. 55], TI MP=[ 0. 55], DWF=[ 0] ( cms), LOSS=[ 2],
1895      SCS curve number CN=[ 74],
1896      Pervious surfaces: I A per=[ 4. 67] ( mm), SLPP=[ 0. 5] ( %),
1897      LGP=[ 40] ( m), MNP=[ 0. 25], SCP=[ 0] ( mi n),
1898      Impervious surfaces: I A i mp=[ 1. 57] ( mm), SLPI=[ 0. 5] ( %),
1899      LGI=[ 1472. 956] ( m), MNI=[ 0. 013], SCI=[ 0] ( mi n),
1900      Continuous simulation parameters:
1901      I a REC per=[ 4] ( hr s), I a REC i mp=[ 4] ( hr s),
1902      SM N=[ - 1] ( mm), SMAX=[ - 1] ( mm), SK=[ 0. 010] / ( mm),
1903      Inter Event Ti me=[ 18] ( hr s), END=- 1
1904      *#*****|
1905      *#      Foster Pond
1906      *#      - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1907      *#      and a ratio of the catchment area to the West Clarke pond rating curve
1908      *#      from the MS for the next coordinates
1909      *#*****|
1910      ROUTE RESERVOIR      NHYDout =[" P_FOS" ],      NHYDin=[" FOSTER" ],
1911      RDT=[ 1] ( mi n),
1912      TABLE of ( OUTFLOW STORAGE ) values
1913      ( cms ) - ( ha- m)
1914      [ 0. 0 , 0. 0 ]
1915      [ 10. 34 , 10]
1916      [ - 1 , - 1 ] ( max twenty pts)
1917      NHYDovf=[" FO- OVF" ]
1918      *%-----|-----|
1919      ADD HYD      NHYDsum=[" FOSTER- OUT" ], NHYDs to add=[" P_FOS"+" FO- OVF" ]
1920      *%-----|-----|
1921      *#*****|
1922      *#      -Brazeau area from P 1800-19 =[71.751], change to 63.59 ha based on GIS measurements
1923      *#      -JFSA, 2021-01-19 update "W_CLAR_BRAZ" to 73.29 ha based on GIS measurements
1924      *#      -JFSA, 2021-01-22 Brazeau ("MS_P10"+"P10-OVF")brazeau pond discharges directly
1925      to the jock river through a road side ditch on the west side of Borrisokane road
1926      (station 6016)

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1925 CONTINUOUS STANDHYD NHYD=[ "W_CLAR_BRAZ" ], DT=[ 1 ] mi n, AREA=[ 73.29 ] ( ha ),
1926 XI MP=[ 0.6 ], TI MP=[ 0.65 ], DWF=[ 0 ] ( cms ), LOSS=[ 2 ],
1927 SCS curve number CN=[ 77 ],
1928 Pervious surfaces: I A per=[ 4.67 ] ( mm ), SLPP=[ 1 ] ( % ),
1929 LGP=[ 40 ] ( m ), MNP=[ 0.25 ], SCP=[ 0 ] ( mi n ),
1930 Impervious surfaces: I A i mp=[ 1.57 ] ( mm ), SLPI=[ 0.5 ] ( % ),
1931 LGI=[ 699.00 ] ( m ), MNI=[ 0.013 ], SCI=[ 0 ] ( mi n ),
1932 Continuous simulation parameters:
1933 I a REC per=[ 4 ] ( hr s ), I a REC i mp=[ 4 ] ( hr s ),
1934 SM N=[ -1 ] ( mm ), SMAX=[ -1 ] ( mm ), SK=[ 0.010 ] / ( mm ),
1935 Inter Event Ti me=[ 18 ] ( hr s ), END=- 1
1936 *%-----|-----|
1937 * 2020-12-01 correct pond curve values
1938 ROUTE RESERVOIR NHYDout=[ "MS_P10" ], NHYDin=[ "W_CLAR_BRAZ" ],
1939 RDT=[ 1 ] ( mi n ),
1940 TABLE of ( OUTFLOW STORAGE ) values
1941 ( cms ) - ( ha - m )
1942 [ 0.0 , 0.0 ]
1943 [ 0.068 , 0.001 ]
1944 [ 0.271 , 0.022 ]
1945 [ 0.379 , 0.051 ]
1946 [ 0.48 , 0.091 ]
1947 [ 0.853 , 0.341 ]
1948 [ 1.005 , 0.61 ]
1949 [ 1.128 , 1.231 ]
1950 [ 1.155 , 1.592 ]
1951 [ 1.194 , 1.876 ]
1952 [ 1.2 , 1.921 ]
1953 [ 1.259 , 2.369 ]
1954 [ 1.3 , 2.665 ]
1955 [ 1.349 , 2.813 ]
1956 [ -1 , -1 ] (max twenty pts)
1957 NHYDovf=[ "P10-OVF" ]
1958 *%-----|-----|
1959 * -JFSA 2021-02-26 "S-1-FO-D2" is a part of S-1 sub-catchment. It is moved to drain
before station 980 on Foster Drain
1960 CONTINUOUS STANDHYD NHYD=[ "S-1-FO-D2" ], DT=[ 1 ] mi n, AREA=[ 4.94 ] ( ha ),
1961 XI MP=[ 0.55 ], TI MP=[ 0.55 ], DWF=[ 0 ] ( cms ), LOSS=[ 2 ],
1962 SCS curve number CN=[ 74 ],
1963 Pervious surfaces: I A per=[ 4.67 ] ( mm ), SLPP=[ 0.5 ] ( % ),
1964 LGP=[ 40 ] ( m ), MNP=[ 0.25 ], SCP=[ 0 ] ( mi n ),
1965 Impervious surfaces: I A i mp=[ 1.57 ] ( mm ), SLPI=[ 0.5 ] ( % ),
1966 LGI=[ 181.475 ] ( m ), MNI=[ 0.013 ], SCI=[ 0 ] ( mi n ),
1967 Continuous simulation parameters:
1968 I a REC per=[ 4 ] ( hr s ), I a REC i mp=[ 4 ] ( hr s ),
1969 SM N=[ -1 ] ( mm ), SMAX=[ -1 ] ( mm ), SK=[ 0.010 ] / ( mm ),
1970 Inter Event Ti me=[ 18 ] ( hr s ), END=- 1
1971 *%-----|-----|
1972 *CONTINUOUS NASHYD NHYD=[ "S-1-FO-D2" ], DT=[ 1 ] mi n, AREA=[ 4.94 ] ( ha ),
1973 * DWF=[ 0 ] ( cms ), CNV C=[ 77 ], I A=[ 4.67 ] ( mm ),
1974 * N=[ 3 ], TP=[ 1.10 ] hr s,
1975 * Continuous simulation parameters:
1976 * I a REC per=[ 4 ] ( hr s ),
1977 * SM N=[ -1 ] ( mm ), SMAX=[ -1 ] ( mm ), SK=[ 0.010 ] / ( mm ),
1978 * Inter Event Ti me=[ 12 ] ( hr s )
1979 * Baseflow simulation parameters:
1980 * BaseFl owOpt ion=[ 1 ] ,
1981 * I ni t GWRes Vol =[ 50 ] ( mm ), GWRes K=[ 0.96 ] ( mm / day / mm )
1982 * VHydCond=[ 0.055 ] ( mm / hr ), END=- 1
1983 *%-----|-----|
1984 *COMPUTE DUALHYD NHYDin=[ "S-1-FO-D2" ], CI NLET=[ 0.508 ] ( cms ), NI NLET=[ 1 ],
1985 * M a j NHYD=[ "S-1-FO-D2J" ]
1986 * M nNHYD=[ "S-1-FO-D2N" ]
1987 * TM I STO=[ 9999999 ] ( cu - m )
1988 *%-----|-----|
1989 *ADD HYD NHYDs um=[ "S-1-FO-D2S" ], NHYDs to add=[ "S-1-FO-D2J"+"S-1-FO-D2N" ]

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1990 *%-----|-----|
1991 *ROUTE RESERVOIR      NHYDout=["S-1-FO-D2R"] , NHYDin=["S-1-FO-D2S"] ,
1992 *                      RDT=[1](min),
1993 *                      TABLE of ( OUTFLOW STORAGE ) values
1994 *                      (cms) - (ha-m)
1995 *                      [ 0.0      , 0.0 ]
1996 *                      [ 0.0590, 0.1970 ]
1997 *                      [   -1   ,  -1   ] (max twenty pts)
1998 *                      NHYDovf=["S-1FOD2ovf"]
1999 *%-----|-----|
2000 ADD HYD              NHYDsum=["980"], NHYDsto add=["FOSTER-OUT"+"S-1-FO-D2"]
2001 *%-----|-----|
2002 SAVE HYD            NHYD=["980"], # OF PCYCLES=[-1], ICASEsh=[1]
2003                    HYD_COMMENT=["Total Flows at Station 980 on Foster Drain"]
2004 *%-----|-----|
2005 *#
2006 *# Hydrograph from Node Foster SWM (Station 980) to Node at station 520
2007 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 980
2008 *#
2009 ROUTE CHANNEL       NHYDout=["980-out"] , NHYDin=["980"] ,
2010                    RDT=[1](min),
2011                    CHLGTH=[460](m),  CHSLOPE=[0.04348](%),
2012                    FPSLOPE=[0.04348](%),
2013                    SECNUM=[1.0],    NSEG=[3]
2014                    ( SEGROUGH, SEGDI ST (m))=
2015                    [ 0.050, 45.90
2016                    -0.035, 53.30
2017                    0.050, 100] NSEG times
2018                    ( DISTANCE (m), ELEVATION (m))=
2019                    [ 0, 91.75 ]
2020                    [ 42.4, 92.18 ]
2021                    [ 43.5, 92.16 ]
2022                    [ 44.1, 92.1 ]
2023                    [ 44.6, 92 ]
2024                    [ 44.8, 91.86 ]
2025                    [ 45.9, 91.04 ]
2026                    [ 46.4, 90.65 ]
2027                    [ 46.8, 90.36 ]
2028                    [ 47.9, 90.32 ]
2029                    [ 48.7, 90.35 ]
2030                    [ 50.7, 90.33 ]
2031                    [ 52.2, 90.38 ]
2032                    [ 52.5, 90.59 ]
2033                    [ 53.3, 91.28 ]
2034                    [ 54, 91.83 ]
2035                    [ 54.3, 92 ]
2036                    [ 54.8, 92.08 ]
2037                    [ 55.4, 92.12 ]
2038                    [ 100, 91.84 ]
2039 *%-----|-----|
2040 * -JFSA 2021-02-26 "S-1-FO-DI" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2041 CONTINUOUS STANDHYD NHYD=["S-1-FO-DI"], DT=[1]min, AREA=[5.11](ha),
2042                    XI MP=[0.65], TI MP=[0.65], DWF=[0](cms), LOSS=[2],
2043                    SCS curve number CN=[74],
2044                    Pervious surfaces: I A per=[4.67](mm), SLPP=[0.5](%),
2045                    LGP=[40](m), MNP=[0.25], SCP=[0](min),
2046                    Impervious surfaces: I A i mp=[1.57](mm), SLPI=[0.5](%),
2047                    LGI=[184.572](m), MNI=[0.013], SCI=[0](min),
2048                    Continuous simulation parameters:
2049                    I a REC per=[4](hrs), I a REC i mp=[4](hrs),
2050                    SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2051                    Inter Event Time=[18](hrs), END=-1
2052 *%-----|-----|
2053 *COMPUTE DUALHYD    NHYDin=["S-1-FO-DI"], C I NLET=[0.605](cms), NI NLET=[1],
2054 *                    M i j NHYD=["S-1-FO-DIJ"]

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2055 * M nNHYD=[ "S- 1- FO- DIN" ]
2056 * TM STO=[ 9999999 ] ( cu- m)
2057 *%-----|-----|
2058 *ADD HYD NHYDs um=[ "S- 1- FO- DIS" ], NHYDs t o add=[ "S- 1- FO- DIN" + "S- 1- FO- DIJ" ]
2059 *%-----|-----|
2060 *ROUTE RESERVOIR NHYDout=[ "S- 1- FO- DIR" ] , NHYDi n=[ "S- 1- FO- DIS" ] ,
2061 * RDT=[ 1 ] ( mi n) ,
2062 * TABLE of ( OUTFLOW STORAGE ) values
2063 * ( cms ) - ( ha- m)
2064 * [ 0. 0 , 0. 0 ]
2065 * [ 0. 0611, 0. 2038 ]
2066 * [ -1 , -1 ] (max twenty pts)
2067 * NHYDovf=[ "S- 1FODlovf" ]
2068 *%-----|-----|
2069 ADD HYD NHYDs um=[ "520" ], NHYDs t o add=[ "980- out " + "S- 1- FO- DI" ]
2070 *%-----|-----|
2071 SAVE HYD NHYD=[ "520" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
2072 HYD_ COMMENT=[ "Total Flows at Sation 520 on Foster Drain" ]
2073 *%-----|-----|
2074 *# Hydrograph from Node at Station 520 (Foster Drain) to Node at station 6016 (Jock
River)
2075 *# Channel X- Section obtained from RVCA Hydraulic Model - Station 520
2076 *#
2077 ROUTE CHANNEL NHYDout = [ "520- out " ] , NHYDi n=[ "520" ] ,
2078 RDT=[ 1 ] ( mi n) ,
2079 CHLGTH=[ 860 ] ( m) , CHSLOPE=[ 0. 5872 ] ( % ) ,
2080 FPSLOPE=[ 0. 5872 ] ( % ) ,
2081 SECNUM=[ 1. 0 ] , NSEG=[ 3 ]
2082 ( SEGROUGH, SEGDI ST ( m) ) =
2083 [ 0. 050, 45. 90
2084 - 0. 035, 54. 3
2085 0. 050, 100. 1097 ] NSEG times
2086 ( DI STANCE ( m) , ELEVATI ON ( m) ) =
2087 [ 0 , 91. 26 ]
2088 [ 44. 9 , 91. 46 ]
2089 [ 45. 1 , 91. 37 ]
2090 [ 45. 9 , 90. 84 ]
2091 [ 47 , 90. 32 ]
2092 [ 47. 5 , 90. 22 ]
2093 [ 48 , 90. 17 ]
2094 [ 50. 7 , 90. 19 ]
2095 [ 51. 5 , 90. 17 ]
2096 [ 52. 2 , 90. 13 ]
2097 [ 52. 7 , 90. 12 ]
2098 [ 53. 3 , 90. 14 ]
2099 [ 53. 5 , 90. 31 ]
2100 [ 53. 9 , 90. 59 ]
2101 [ 54. 3 , 90. 87 ]
2102 [ 54. 7 , 91. 04 ]
2103 [ 55. 3 , 91. 24 ]
2104 [ 55. 5 , 91. 26 ]
2105 [ 63. 7 , 91. 37 ]
2106 [ 100. 1097 , 91. 43 ]
2107 *%-----|-----|
2108 * -JFSA 2021-02-26 "S- 1- FO- F- D" is a part of S- 1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2109 CONTINUOUS STANDHYD NHYD=[ "S- 1- FO- F- D" ], DT=[ 1 ] mi n , AREA=[ 14. 96 ] ( ha) ,
2110 XI MP=[ 0. 65 ] , TI MP=[ 0. 65 ] , DWF=[ 0 ] ( cms ) , LOSS=[ 2 ] ,
2111 SCS curve number CN=[ 74 ] ,
2112 Pervious surfaces: I A per=[ 4. 67 ] ( mm) , SLPP=[ 0. 5 ] ( % ) ,
2113 LGP=[ 40 ] ( m) , MNP=[ 0. 25 ] , SCP=[ 0 ] ( mi n) ,
2114 Impervious surfaces: I A i mp=[ 1. 57 ] ( mm) , SLPI=[ 0. 5 ] ( % ) ,
2115 LGI=[ 315. 806 ] ( m) , MNI =[ 0. 013 ] , SCI =[ 0 ] ( mi n) ,
2116 Continuous simulation parameters:
2117 I a REC per=[ 4 ] ( hr s) , I a REC i mp=[ 4 ] ( hr s) ,
2118 SM N=[ - 1 ] ( mm) , SMAX=[ - 1 ] ( mm) , SK=[ 0. 010 ] / ( mm) ,

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2119      InterEventTime=[ 18](hrs),      END=- 1
2120  *%-----|-----|
2121  *CONTINUOUS NASHYD  NHYD=["S-1-FO-F-D"], DT=[ 1]min, AREA=[ 14.96](ha),
2122  *                   DWF=[ 0](cms), CNVC=[ 77], IA=[ 4.67](mm),
2123  *                   N=[ 3], TP=[ 1.007]hrs,
2124  *                   Continuous simulation parameters:
2125  *                   IaRECper=[ 4](hrs),
2126  *                   SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2127  *                   InterEventTime=[ 12](hrs)
2128  *                   Baseflow simulation parameters:
2129  *                   BaseFlowOption=[ 1],
2130  *                   InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2131  *                   VHydCond=[ 0.055](mm/hr),      END=- 1
2132  *%-----|-----|
2133  *COMPUTE DUALHYD   NHYDin=["S-1-FO-F-D"], CINLET=[ 1.749](cms), NINLET=[ 1],
2134  *                   MajNHYD=["S-1FO-F-DJ"]
2135  *                   MnNHYD=["S-1FO-F-DN"]
2136  *                   TMSSTO=[ 9999999](cu-m)
2137  *%-----|-----|
2138  *ADD HYD            NHYDsum=["S-1FO-F-DS"], NHYDs to add=["S-1FO-F-DJ"+"S-1FO-F-DN"]
2139  *%-----|-----|
2140  *ROUTE RESERVOIR  NHYDout=["S-1FO-F-DR"], NHYDin=["S-1FO-F-DS"],
2141  *                   RDT=[ 1](min),
2142  *                   TABLE of ( OUTFLOW STORAGE ) values
2143  *                   ( cms ) - ( ha-m )
2144  *                   [ 0.0      , 0.0 ]
2145  *                   [ 0.1788, 0.5966 ]
2146  *                   [ -1      , -1 ] (max twenty pts)
2147  *                   NHYDovf=["S-1FoFDovf"]
2148  *%-----|-----|
2149  * -JFSA 2021-02-26 "S-1-D8" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2150  CONTINUOUS STANDHYD NHYD=["S-1-D8"], DT=[ 1]min, AREA=[ 5.27](ha), XI MP=[ 0.325],
TI MP=[ 0.65], DWF=[ 0](cms), LOSS=[ 1]:
2151  Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
F=[ 0.00](mm),
2152  Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
MNP=[ 0.250], SCP=[ 0](min),
2153  Impervious areas: IAimp=[ 0.785](mm), SLPI=[ 0.75](%),
LGI=[ 187.439](m), MNI=[ 0.013], SCI=[ 0](min),
2154  Continuous simulation parameters:
2155  IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
END=- 1
2156  *%-----|-----|
2157  *CONTINUOUS NASHYD  NHYD=["S-1-D8"], DT=[ 1]min, AREA=[ 5.27](ha),
2158  *                   DWF=[ 0](cms), CNVC=[ 77], IA=[ 4.67](mm),
2159  *                   N=[ 3], TP=[ 1.10]hrs,
2160  *                   Continuous simulation parameters:
2161  *                   IaRECper=[ 4](hrs),
2162  *                   SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2163  *                   InterEventTime=[ 12](hrs)
2164  *                   Baseflow simulation parameters:
2165  *                   BaseFlowOption=[ 1],
2166  *                   InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2167  *                   VHydCond=[ 0.055](mm/hr),      END=- 1
2168  *%-----|-----|
2169  *COMPUTE DUALHYD   NHYDin=["S-1-D8"], CINLET=[ 2.279](cms), NINLET=[ 1],
2170  *                   MajNHYD=["S-1-D8J"]
2171  *                   MnNHYD=["S-1-D8N"]
2172  *                   TMSSTO=[ 9999999](cu-m)
2173  *%-----|-----|
2174  *ADD HYD            NHYDsum=["S-1-D8S"], NHYDs to add=["S-1-D8J"+"S-1-D8N"]
2175  *%-----|-----|
2176  *ADD HYD            NHYDsum=["S-1-D"], NHYDs to add=["S-1-Okeefe"+"S-1"+"S-1-Fost"]
2177  *%-----|-----|
2178  *COMPUTE DUALHYD   NHYDin=["S-1-D"], CINLET=[ 11.616](cms), NINLET=[ 1],

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2179 *           Mj NHYD=[ " S- 1- D- M " ]
2180 *           MnNHYD=[ " S- 1- D- MN" ]
2181 *           TM STO=[ 5974 ] ( cu- m)
2182 *%-----|-----
2183 *ADD HYD           NHYDs um=[ " S- 1- DEV" ] , NHYDs t o add=[ " S- 1- D- M" +" S- 1- D- MN" ]
2184 *%-----|-----
2185 *ROUTE RESERVOIR  NHYDout =[ " S- 1- D8R" ] , NHYDin =[ " S- 1- D8S" ] ,
2186 *           RDT=[ 1 ] ( mi n) ,
2187 *           TABLE of ( OUTFLOW STORAGE ) values
2188 *                   ( cms ) - ( ha- m)
2189 *                   [ 0. 0      , 0. 0 ]
2190 *                   [ 0. 0630, 0. 2102 ]
2191 *                   [      -1 , -1      ] (max twenty pts)
2192 *           NHYDovf=[ " S- 1- D8Rovf" ]
2193 *%-----|-----
2194 * -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2195 CONTINUOUS NASHYD NHYD=[ " S- 1- A" ] , DT=[ 1 ] mi n, AREA=[ 75. 88 ] ( ha) ,
2196 DWF=[ 0 ] ( cms ) , CN C=[ 77 ] , IA=[ 4. 67 ] ( mm) ,
2197 N=[ 3 ] , TP=[ 0. 619 ] hr s ,
2198 Continuous simulation parameters:
2199 IaRECper=[ 4 ] ( hr s) ,
2200 SM N=[ - 1 ] ( mm) , SMAX=[ - 1 ] ( mm) , SK=[ 0. 010 ] / ( mm) ,
2201 InterEvent Time=[ 12 ] ( hr s)
2202 Baseflow simulation parameters:
2203 BaseFlowOption=[ 1 ] ,
2204 Init GWRes Vol =[ 50 ] ( mm) , GWRes K=[ 0. 96 ] ( mm/ day/ mm)
2205 VHydCond=[ 0. 055 ] ( mm/ hr) , END=- 1
2206 *%-----|-----
2207 * -JFSA, 2021-01-22 "W_CLAR_UNDE" (west of Clarke sub-catchment) discharges
directly to the jock river through a road side ditch on the west side of Borrisokane
road (station 6016)
2208 CONTINUOUS NASHYD NHYD=[ " W_CLAR_UNDE" ] , DT=[ 1 ] mi n, AREA=[ 35. 65 ] ( ha) ,
2209 DWF=[ 0 ] ( cms ) , CN C=[ 77 ] , IA=[ 4. 67 ] ( mm) ,
2210 N=[ 3 ] , TP=[ 1. 10 ] hr s ,
2211 Continuous simulation parameters:
2212 IaRECper=[ 4 ] ( hr s) ,
2213 SM N=[ - 1 ] ( mm) , SMAX=[ - 1 ] ( mm) , SK=[ 0. 010 ] / ( mm) ,
2214 InterEvent Time=[ 12 ] ( hr s)
2215 Baseflow simulation parameters:
2216 BaseFlowOption=[ 1 ] ,
2217 Init GWRes Vol =[ 50 ] ( mm) , GWRes K=[ 0. 96 ] ( mm/ day/ mm)
2218 VHydCond=[ 0. 055 ] ( mm/ hr) , END=- 1
2219 *%-----|-----
2220 ADD HYD           NHYDs um=[ " SN_FO" ] , NHYDs t o
add=[ " N_FO" +" 520- out " +" MS_P10" +" P10- OVF" +" W_CLAR_UNDE" +" S- 1- FO- F- D" +" S- 1- D8" +" S- 1- A" ]
2221 *%-----|-----
2222 SAVE HYD          NHYD=[ " SN_FO" ] , # OF PCYCLES=[ - 1 ] , I CASEs h=[ 1 ]
2223 HYD_COMMENT=[ " Total Flows at Foster Drain" ]
2224 *%-----|-----
2225 *# Hydrograph from Node Foster routed to Node at Cedarview Road
2226 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6016
2227 *#
2228 ROUTE CHANNEL     NHYDout =[ " N_CE" ] , NHYDin =[ " SN_FO" ] ,
2229 RDT=[ 1 ] ( mi n) ,
2230 CHLGTH=[ 159 ] ( m) , CHSLOPE=[ 0. 0818 ] ( % ) ,
2231 FPSLOPE=[ 0. 0818 ] ( % ) ,
2232 SECNUM=[ 1. 0 ] , NSEG=[ 3 ]
2233 ( SEGROUGH, SEGDI ST ( m) ) =
2234 [ 0. 050, - 15. 46
2235 - 0. 035, 26. 55
2236 0. 050, 116. 76 ] NSEG times
2237 ( DI STANCE ( m) , ELEVATI ON ( m) ) =
2238 [ - 645. 23, 91. 50 ]
2239 [ - 391. 20, 91. 50 ]
2240 [ - 91. 00, 91. 50 ]

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2241          [- 85.52, 91.50]
2242          [- 15.46, 89.40]
2243          [- 9.79, 89.31]
2244          [- 3.22, 86.24]
2245          [ 3.22, 85.07]
2246          [10.96, 85.79]
2247          [16.44, 86.49]
2248          [26.55, 89.45]
2249          [29.03, 90.27]
2250          [35.76, 90.67]
2251          [36.67, 91.00]
2252          [108.08, 91.00]
2253          [109.82, 90.50]
2254          [112.04, 90.50]
2255          [114.62, 91.00]
2256          [116.76, 91.50]
2257  *%-----|-----|
2258  *#*****|
2259  *#      Catchment S-1
2260  *#      - To Jock River (north and south of Jock)
2261  *#      - Primarily agricultural fields; portion of sand quarry
2262  *%-----|-----|
2263  *%      -2020-12-17 "S-1-Undev" and "S-1-Fost" was a part of Foster drain, they are below
the foster pond. Now they are added to S-1 subcatchment based on Project 1474-BCDC,
JFSA, Nov. 2020
2264  *%      -2020-12-17 Change O-14 (it was part of Okeefe drain) to "S-1-Okeefe" and add it
to S-1 subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
2265  *%      -2020-12-17 Add "S-1-BCDC" as NASHYD
2266  *%      -2020-12-17 all other S-1 subcatchment as STANDHYD with DUALHYD and ROUTE RESERVOIR
2267  *%-----|-----|
2268  *#*****|
2269  *      -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2270  *CONTINUOUS NASHYD  NHYD=["S-1-A"], DT=[1]min, AREA=[75.88](ha),
2271  *                    DWF=[0](cms), CNVC=[77], IA=[4.67](mm),
2272  *                    N=[3], TP=[0.619]hrs,
2273  *                    Continuous simulation parameters:
2274  *                    IaRECper=[4](hrs),
2275  *                    SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2276  *                    InterEventTime=[12](hrs)
2277  *                    Baseflow simulation parameters:
2278  *                    BaseFlowOption=[1],
2279  *                    InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2280  *                    VHydCond=[0.055](mm/hr), END=-1
2281  *%-----|-----|
2282  CONTINUOUS NASHYD  NHYD=["S-1-B"], DT=[1]min, AREA=[55.36](ha),
2283  *                    DWF=[0](cms), CNVC=[77], IA=[4.67](mm),
2284  *                    N=[3], TP=[0.451]hrs,
2285  *                    Continuous simulation parameters:
2286  *                    IaRECper=[4](hrs),
2287  *                    SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2288  *                    InterEventTime=[12](hrs)
2289  *                    Baseflow simulation parameters:
2290  *                    BaseFlowOption=[1],
2291  *                    InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2292  *                    VHydCond=[0.055](mm/hr), END=-1
2293  *%-----|-----|
2294  *#      - JFSA 2021-02-24 change the name from S-1-BCDC to S-1-A and S-1-B. Change their
TP values based on the new areas compared to the old ones.
2295  *CONTINUOUS NASHYD  NHYD=["S-1-BCDC"], DT=[1]min, AREA=[134.9](ha),
2296  *                    DWF=[0](cms), CNVC=[77], IA=[4.67](mm),
2297  *                    N=[3], TP=[1.10]hrs,
2298  *                    Continuous simulation parameters:
2299  *                    IaRECper=[4](hrs),
2300  *                    SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2301  *                    InterEventTime=[12](hrs)

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2302 *          Baseflow simulation parameters:
2303 *          BaseFlowOption=[ 1] ,
2304 *          InitGWResVol =[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2305 *          VHydCond=[ 0.055](mm/hr) ,    END=- 1
2306 *%-----|-----
2307 *# - JFSA 2021-02-24 "S-1-BCDC-1" and "S-1-BCDC-2" are not existing anymore.
      "S-1-BCDC-1" is part of "S-1-FO-D2" and "S-1-BCDC-2" is part of "S-1-D2" and "S-1-D3"
2308 *CONTINUOUS NASHYD  NHYD=["S-1-BCDC-1"], DT=[ 1]min, AREA=[ 0.3](ha),
2309 *          DWF=[ 0](cms) , CN/C=[ 77] , IA=[ 4.67](mm) ,
2310 *          N=[ 3] , TP=[ 1.10]hrs ,
2311 *          Continuous simulation parameters:
2312 *          IaRECper=[ 4](hrs) ,
2313 *          SMN=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2314 *          InterEventTime=[ 12](hrs)
2315 *          Baseflow simulation parameters:
2316 *          BaseFlowOption=[ 1] ,
2317 *          InitGWResVol =[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2318 *          VHydCond=[ 0.055](mm/hr) ,    END=- 1
2319 *%-----|-----
2320 *CONTINUOUS NASHYD  NHYD=["S-1-BCDC-2"], DT=[ 1]min, AREA=[ 1.3](ha),
2321 *          DWF=[ 0](cms) , CN/C=[ 77] , IA=[ 4.67](mm) ,
2322 *          N=[ 3] , TP=[ 1.10]hrs ,
2323 *          Continuous simulation parameters:
2324 *          IaRECper=[ 4](hrs) ,
2325 *          SMN=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2326 *          InterEventTime=[ 12](hrs)
2327 *          Baseflow simulation parameters:
2328 *          BaseFlowOption=[ 1] ,
2329 *          InitGWResVol =[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2330 *          VHydCond=[ 0.055](mm/hr) ,    END=- 1
2331 *%-----|-----
2332 *# - JFSA 2021-01-19, after adding Greenbank pond, "S-1-BCDC-3" is not existing
      anymore
2333 *CONTINUOUS NASHYD  NHYD=["S-1-BCDC-3"], DT=[ 1]min, AREA=[ 3.9](ha),
2334 *          DWF=[ 0](cms) , CN/C=[ 77] , IA=[ 4.67](mm) ,
2335 *          N=[ 3] , TP=[ 1.10]hrs ,
2336 *          Continuous simulation parameters:
2337 *          IaRECper=[ 4](hrs) ,
2338 *          SMN=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2339 *          InterEventTime=[ 12](hrs)
2340 *          Baseflow simulation parameters:
2341 *          BaseFlowOption=[ 1] ,
2342 *          InitGWResVol =[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2343 *          VHydCond=[ 0.055](mm/hr) ,    END=- 1
2344 *%-----|-----
2345 * -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
      before station 7245 on Jock River
2346 *CONTINUOUS STANDHYD NHYD=["S-1-Okeefe"], DT=[ 1](min) , AREA=[ 44.93](ha) , XI MP=[ 0.65] ,
      TI MP=[ 0.65] , DWF=[ 0](cms) ,
2347 *          LOSS=[ 2] , SCS curve number CN=[ 75] , Pervious surfaces:
      IAper=[ 4.67](mm) , SLPP=[ 2.0](%) ,
2348 *          LGP=[ 40](m) , MNP=[ 0.25] , SCP=[ 0](min) , Impervious surfaces:
      IAi mp=[ 1.57](mm) , SLPI =[ 0.75](%) ,
2349 *          LGI=[ 547.296](m) , MNI =[ 0.013] , SCI =[ 0](min) ,
2350 *          Continuous simulation parameters:
2351 *          IaRECper=[ 4](hrs) , IaRECI mp=[ 4](hrs) ,
2352 *          SMN=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2353 *          InterEventTime=[ 12](hrs) ,    END=- 1
2354 *%-----|-----
2355 *COMPUTE DUALHYD  NHYDin=["S-1-Okeefe"] , CINLET=[ 4.796](cms) , NI NLET=[ 1] ,
2356 *          Maj NHYD=["S-1-OkM"]
2357 *          MnNHYD=["S-1-OkMN"]
2358 *          TMI STO=[ 9999999](cu-m)
2359 *%-----|-----
2360 *ADD HYD          NHYDs um=["S-1-OkS"] , NHYDs to add=["S-1-OkM"+"S-1-OkMN"]
2361 *%-----|-----

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2362 *ROUTE RESERVOIR      NHYDout=[ "S-1-OkSR" ] , NHYDin=[ "S-1-OkS" ] ,
2363 *                      RDT=[ 1 ] (mi n),
2364 *                      TABLE of ( OUTFLOW STORAGE ) values
2365 *                      ( cms ) - ( ha-m)
2366 *                      [ 0.0      , 0.0 ]
2367 *                      [ 0.5370, 1.7917 ]
2368 *                      [ -1      , -1      ] (max twenty pts)
2369 *                      NHYDovf=[ "S-1-OkSovf" ]
2370 *%-----|-----
2371 *CONTINUOUS NASHYD     NHYD=[ "S-1-Okeefe" ], DT=[ 1 ] mi n, AREA=[ 44.93 ] (ha),
2372 *                      DWF=[ 0 ] (cms), CN C=[ 77 ], IA=[ 4.67 ] (mm),
2373 *                      N=[ 3 ], TP=[ 1.049 ] hrs,
2374 *                      Continuous simulation parameters:
2375 *                      IaRECper=[ 4 ] (hrs),
2376 *                      SMN=[ -1 ] (mm), SMAX=[ -1 ] (mm), SK=[ 0.010 ] / (mm),
2377 *                      InterEventTime=[ 12 ] (hrs)
2378 *                      Baseflow simulation parameters:
2379 *                      BaseFlowOption=[ 1 ] ,
2380 *                      InitGWResVol=[ 50 ] (mm), GWResK=[ 0.96 ] (mm/ day/ mm)
2381 *                      VHydCond=[ 0.055 ] (mm/ hr), END=- 1
2382 *%-----|-----
2383 * -JFSA 2021-02-26 "S-1-FO-DI" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2384 *CONTINUOUS STANDHYD NHYD=[ "S-1-FO-DI" ], DT=[ 1 ] mi n, AREA=[ 5.11 ] (ha),
2385 *                      XI MP=[ 0.65 ], TI MP=[ 0.65 ], DWF=[ 0 ] (cms), LOSS=[ 2 ],
2386 *                      SCS curve number CN=[ 74 ],
2387 *                      Pervious surfaces: IAper=[ 4.67 ] (mm), SLPP=[ 0.5 ] ( % ),
2388 *                      LGP=[ 40 ] (m), MNP=[ 0.25 ], SCP=[ 0 ] (mi n),
2389 *                      Impervious surfaces: IAimp=[ 1.57 ] (mm), SLPI=[ 0.5 ] ( % ),
2390 *                      LGI=[ 184.572 ] (m), MNI=[ 0.013 ], SCI=[ 0 ] (mi n),
2391 *                      Continuous simulation parameters:
2392 *                      IaRECper=[ 4 ] (hrs), IaRECImp=[ 4 ] (hrs),
2393 *                      SMN=[ -1 ] (mm), SMAX=[ -1 ] (mm), SK=[ 0.010 ] / (mm),
2394 *                      InterEventTime=[ 18 ] (hrs), END=- 1
2395 *%-----|-----
2396 *COMPUTE DUALHYD      NHYDin=[ "S-1-FO-DI" ], CINLET=[ 0.605 ] (cms), NINLET=[ 1 ],
2397 *                      MajNHYD=[ "S-1-FO-DIJ" ]
2398 *                      MnNHYD=[ "S-1-FO-DIN" ]
2399 *                      TMSTO=[ 9999999 ] (cu-m)
2400 *%-----|-----
2401 *ADD HYD               NHYDsum=[ "S-1-FO-DIS" ], NHYDsto add=[ "S-1-FO-DIN"+"S-1-FO-DIJ" ]
2402 *%-----|-----
2403 *ROUTE RESERVOIR      NHYDout=[ "S-1-FO-DIR" ] , NHYDin=[ "S-1-FO-DIS" ] ,
2404 *                      RDT=[ 1 ] (mi n),
2405 *                      TABLE of ( OUTFLOW STORAGE ) values
2406 *                      ( cms ) - ( ha-m)
2407 *                      [ 0.0      , 0.0 ]
2408 *                      [ 0.0611, 0.2038 ]
2409 *                      [ -1      , -1      ] (max twenty pts)
2410 *                      NHYDovf=[ "S-1FODlovf" ]
2411 *%-----|-----
2412 *CONTINUOUS NASHYD     NHYD=[ "S-1-FO-DI" ], DT=[ 1 ] mi n, AREA=[ 5.11 ] (ha),
2413 *                      DWF=[ 0 ] (cms), CN C=[ 77 ], IA=[ 4.67 ] (mm),
2414 *                      N=[ 3 ], TP=[ 1.10 ] hrs,
2415 *                      Continuous simulation parameters:
2416 *                      IaRECper=[ 4 ] (hrs),
2417 *                      SMN=[ -1 ] (mm), SMAX=[ -1 ] (mm), SK=[ 0.010 ] / (mm),
2418 *                      InterEventTime=[ 12 ] (hrs)
2419 *                      Baseflow simulation parameters:
2420 *                      BaseFlowOption=[ 1 ] ,
2421 *                      InitGWResVol=[ 50 ] (mm), GWResK=[ 0.96 ] (mm/ day/ mm)
2422 *                      VHydCond=[ 0.055 ] (mm/ hr), END=- 1
2423 *%-----|-----
2424 * -JFSA 2021-02-26 "S-1-FO-D2" is a part of S-1 sub-catchment. It is moved to drain
before station 980 on Foster Drain
2425 *CONTINUOUS STANDHYD NHYD=[ "S-1-FO-D2" ], DT=[ 1 ] mi n, AREA=[ 4.94 ] (ha),

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2426 * XI MP=[ 0.55], TI MP=[ 0.55], DWF=[ 0](cms), LOSS=[ 2],
2427 * SCS curve number CN=[ 74],
2428 * Previous surfaces: IAper=[ 4.67](mm), SLPP=[ 0.5](%),
2429 * LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
2430 * Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 0.5](%),
2431 * LGI=[ 181.475](m), MNI=[ 0.013], SCI=[ 0](min),
2432 * Continuous simulation parameters:
2433 * IaRECper=[ 4](hrs), IaRECimp=[ 4](hrs),
2434 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2435 * InterEventTime=[ 18](hrs), END=- 1
2436 %-----|-----
2437 *CONTINUOUS NASHYD NHYD=[ "S-1-FO-D2"], DT=[ 1]min, AREA=[ 4.94](ha),
2438 * DWF=[ 0](cms), CN C=[ 77], IA=[ 4.67](mm),
2439 * N=[ 3], TP=[ 1.10]hrs,
2440 * Continuous simulation parameters:
2441 * IaRECper=[ 4](hrs),
2442 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2443 * InterEventTime=[ 12](hrs)
2444 * Baseflow simulation parameters:
2445 * BaseFlowOption=[ 1],
2446 * InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2447 * VHydCond=[ 0.055](mm/hr), END=- 1
2448 %-----|-----
2449 *COMPUTE DUALHYD NHYDin=[ "S-1-FO-D2"], CINLET=[ 0.508](cms), NINLET=[ 1],
2450 * MajNHYD=[ "S-1-FO-D2J"]
2451 * MnNHYD=[ "S-1-FO-D2N"]
2452 * TMS TO=[ 9999999](cu-m)
2453 %-----|-----
2454 *ADD HYD NHYDsum=[ "S-1-FO-D2S"], NHYDsto add=[ "S-1-FO-D2J"+"S-1-FO-D2N"]
2455 %-----|-----
2456 *ROUTE RESERVOIR NHYDout=[ "S-1-FO-D2R"], NHYDin=[ "S-1-FO-D2S"],
2457 * RDT=[ 1](min),
2458 * TABLE of ( OUTFLOW STORAGE ) values
2459 * (cms) - (ha-m)
2460 * [ 0.0 , 0.0 ]
2461 * [ 0.0590, 0.1970 ]
2462 * [ -1 , -1 ] (max twenty pts)
2463 * NHYDovf=[ "S-1FOD2ovf"]
2464 %-----|-----
2465 * -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2466 *CONTINUOUS STANDHYD NHYD=[ "S-1-FO-F-D"], DT=[ 1]min, AREA=[ 14.96](ha),
2467 * XI MP=[ 0.65], TI MP=[ 0.65], DWF=[ 0](cms), LOSS=[ 2],
2468 * SCS curve number CN=[ 74],
2469 * Previous surfaces: IAper=[ 4.67](mm), SLPP=[ 0.5](%),
2470 * LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
2471 * Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 0.5](%),
2472 * LGI=[ 315.806](m), MNI=[ 0.013], SCI=[ 0](min),
2473 * Continuous simulation parameters:
2474 * IaRECper=[ 4](hrs), IaRECimp=[ 4](hrs),
2475 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2476 * InterEventTime=[ 18](hrs), END=- 1
2477 %-----|-----
2478 *CONTINUOUS NASHYD NHYD=[ "S-1-FO-F-D"], DT=[ 1]min, AREA=[ 14.96](ha),
2479 * DWF=[ 0](cms), CN C=[ 77], IA=[ 4.67](mm),
2480 * N=[ 3], TP=[ 1.007]hrs,
2481 * Continuous simulation parameters:
2482 * IaRECper=[ 4](hrs),
2483 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2484 * InterEventTime=[ 12](hrs)
2485 * Baseflow simulation parameters:
2486 * BaseFlowOption=[ 1],
2487 * InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2488 * VHydCond=[ 0.055](mm/hr), END=- 1
2489 %-----|-----
2490 *COMPUTE DUALHYD NHYDin=[ "S-1-FO-F-D"], CINLET=[ 1.749](cms), NINLET=[ 1],

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2491 *           Mj NHYD=[ "S- 1FO- F- DJ" ]
2492 *           MnNHYD=[ "S- 1FO- F- DN" ]
2493 *           TMJ STO=[ 9999999 ] ( cu- m)
2494 *%-----|-----|
2495 *ADD HYD           NHYDs um=[ "S- 1FO- F- DS" ], NHYDs to add=[ "S- 1FO- F- DJ"+"S- 1FO- F- DN" ]
2496 *%-----|-----|
2497 *ROUTE RESERVOIR  NHYDout=[ "S- 1FO- F- DR" ] , NHYDin=[ "S- 1FO- F- DS" ] ,
2498 *           RDT=[ 1 ] ( mi n),
2499 *           TABLE of ( OUTFLOW STORAGE ) values
2500 *                   ( cms ) - ( ha- m)
2501 *                   [ 0.0      , 0.0 ]
2502 *                   [ 0.1788, 0.5966 ]
2503 *                   [    -1   ,  -1   ] (max twenty pts)
2504 *           NHYDovf=[ "S- 1FoFDovf" ]
2505 *%-----|-----|
2506 *CONTINUOUS STANDHYD NHYD=[ "S- 1- D1" ], DT=[ 1 ] ( mi n), AREA=[ 21.67 ] ( ha), XI MP=[ 0.65 ],
TI MP=[ 0.65 ], DWF=[ 0 ] ( cms),
2507 *           LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
I Aper=[ 4.67 ] ( mm), SLPP=[ 2.0 ] ( %),
2508 *           LGP=[ 40 ] ( m), MNP=[ 0.25 ], SCP=[ 0 ] ( mi n), Impervious surfaces:
I Ai mp=[ 1.57 ] ( mm), SLPI=[ 0.75 ] ( %),
2509 *           LGI=[ 380.088 ] ( m), MNI=[ 0.013 ], SCI=[ 0 ] ( mi n),
2510 *           Continuous simulation parameters:
2511 *           IaRECper=[ 4 ] ( hr s), IaRECI mp=[ 4 ] ( hr s),
2512 *           SMN=[ -1 ] ( mm), SMAX=[ -1 ] ( mm), SK=[ 0.010 ] / ( mm),
2513 *           InterEvent Time=[ 12 ] ( hr s), END=- 1
2514 *%-----|-----|
2515 *CONTINUOUS NASHYD NHYD=[ "S- 1- D1" ], DT=[ 1 ] mi n, AREA=[ 21.67 ] ( ha),
2516 *           DWF=[ 0 ] ( cms), CN C=[ 77 ], IA=[ 4.67 ] ( mm),
2517 *           N=[ 3 ], TP=[ 1.066 ] hr s,
2518 *           Continuous simulation parameters:
2519 *           IaRECper=[ 4 ] ( hr s),
2520 *           SMN=[ -1 ] ( mm), SMAX=[ -1 ] ( mm), SK=[ 0.010 ] / ( mm),
2521 *           InterEvent Time=[ 12 ] ( hr s)
2522 *           Baseflow simulation parameters:
2523 *           BaseFlowOption=[ 1 ] ,
2524 *           InitGWRes Vol=[ 50 ] ( mm), GWRes K=[ 0.96 ] ( mm/ day/ mm)
2525 *           VHydCond=[ 0.055 ] ( mm/ hr ), END=- 1
2526 *%-----|-----|
2527 *COMPUTE DUALHYD  NHYDin=[ "S- 1- D1" ], CINLET=[ 2.482 ] ( cms), NI NLET=[ 1 ],
2528 *           Mj NHYD=[ "S- 1- DIJ" ]
2529 *           MnNHYD=[ "S- 1- DIN" ]
2530 *           TMJ STO=[ 9999999 ] ( cu- m)
2531 *%-----|-----|
2532 *ADD HYD           NHYDs um=[ "S- 1- DIS" ], NHYDs to add=[ "S- 1- DIJ"+"S- 1- DIN" ]
2533 *%-----|-----|
2534 *ROUTE RESERVOIR  NHYDout=[ "S- 1- DIR" ] , NHYDin=[ "S- 1- DIS" ] ,
2535 *           RDT=[ 1 ] ( mi n),
2536 *           TABLE of ( OUTFLOW STORAGE ) values
2537 *                   ( cms ) - ( ha- m)
2538 *                   [ 0.0      , 0.0 ]
2539 *                   [ 0.2590, 0.8642 ]
2540 *                   [    -1   ,  -1   ] (max twenty pts)
2541 *           NHYDovf=[ "S- 1- DIRovf" ]
2542 *%-----|-----|
2543 *           -JFSA 2021-02-25 "S- 1- D2" and "S- 1- D3" are part of S- 1 sub-catchment. They are
moved to drain before station 6215 on Jock River
2544 *CONTINUOUS STANDHYD NHYD=[ "S- 1- D2" ], DT=[ 1 ] ( mi n), AREA=[ 18.67 ] ( ha), XI MP=[ 0.65 ],
TI MP=[ 0.65 ], DWF=[ 0 ] ( cms),
2545 *           LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
I Aper=[ 4.67 ] ( mm), SLPP=[ 2.0 ] ( %),
2546 *           LGP=[ 40 ] ( m), MNP=[ 0.25 ], SCP=[ 0 ] ( mi n), Impervious surfaces:
I Ai mp=[ 1.57 ] ( mm), SLPI=[ 0.75 ] ( %),
2547 *           LGI=[ 352.798 ] ( m), MNI=[ 0.013 ], SCI=[ 0 ] ( mi n),
2548 *           Continuous simulation parameters:
2549 *           IaRECper=[ 4 ] ( hr s), IaRECI mp=[ 4 ] ( hr s),

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2550 * SMN=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
2551 * InterEventTime=[ 12 ] ( hr s ) , END=- 1
2552 *%-----|-----
2553 *CONTINUOUS NASHYD NHYD=[ " S- 1- D2 " ] , DT=[ 1 ] mi n , AREA=[ 18. 67 ] ( ha ) ,
2554 * DWF=[ 0 ] ( cms ) , CNVC=[ 77 ] , IA=[ 4. 67 ] ( mm ) ,
2555 * N=[ 3 ] , TP=[ 1. 120 ] hr s ,
2556 * Continuous simulation parameters:
2557 * IaRECper=[ 4 ] ( hr s ) ,
2558 * SMN=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
2559 * InterEventTime=[ 12 ] ( hr s )
2560 * Baseflow simulation parameters:
2561 * BaseFlowOption=[ 1 ] ,
2562 * InitGWResVol=[ 50 ] ( mm ) , GWResK=[ 0. 96 ] ( mm/ day/ mm)
2563 * VHydCond=[ 0. 055 ] ( mm/ hr ) , END=- 1
2564 *%-----|-----
2565 *COMPUTE DUALHYD NHYDin=[ " S- 1- D2 " ] , CINLET=[ 2. 062 ] ( cms ) , NINLET=[ 1 ] ,
2566 * MajNHYD=[ " S- 1- D2J " ]
2567 * MnNHYD=[ " S- 1- D2N " ]
2568 * TMSTO=[ 9999999 ] ( cu- m)
2569 *%-----|-----
2570 *ADD HYD NHYDs um=[ " S- 1- D2S " ] , NHYDs to add=[ " S- 1- D2J " + " S- 1- D2N " ]
2571 *%-----|-----
2572 *ROUTE RESERVOIR NHYDout=[ " S- 1- D2R " ] , NHYDin=[ " S- 1- D2S " ] ,
2573 * RDT=[ 1 ] ( mi n ) ,
2574 * TABLE of ( OUTFLOW STORAGE ) values
2575 * ( cms ) - ( ha- m)
2576 * [ 0. 0 , 0. 0 ]
2577 * [ 0. 2231 , 0. 7445 ]
2578 * [ - 1 , - 1 ] ( max twenty pts)
2579 * NHYDovf=[ " S- 1- D2Rovf " ]
2580 *%-----|-----
2581 *CONTINUOUS STANDHYD NHYD=[ " S- 1- D3 " ] , DT=[ 1 ] ( mi n ) , AREA=[ 6. 79 ] ( ha ) , XI MP=[ 0. 65 ] ,
TI MP=[ 0. 65 ] , DWF=[ 0 ] ( cms ) ,
2582 * LOSS=[ 2 ] , SCS curve number CN=[ 75 ] , Pervious surfaces:
I Aper=[ 4. 67 ] ( mm ) , SLPP=[ 2. 0 ] ( % ) ,
2583 * LGP=[ 40 ] ( m ) , MNP=[ 0. 25 ] , SCP=[ 0 ] ( mi n ) , Impervious surfaces:
I Ai mp=[ 1. 57 ] ( mm ) , SLPI=[ 0. 75 ] ( % ) ,
2584 * LGI=[ 212. 760 ] ( m ) , MNI=[ 0. 013 ] , SCI=[ 0 ] ( mi n ) ,
2585 * Continuous simulation parameters:
2586 * IaRECper=[ 4 ] ( hr s ) , IaRECi mp=[ 4 ] ( hr s ) ,
2587 * SMN=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
2588 * InterEventTime=[ 12 ] ( hr s ) , END=- 1
2589 *%-----|-----
2590 *CONTINUOUS NASHYD NHYD=[ " S- 1- D3 " ] , DT=[ 1 ] mi n , AREA=[ 6. 79 ] ( ha ) ,
2591 * DWF=[ 0 ] ( cms ) , CNVC=[ 77 ] , IA=[ 4. 67 ] ( mm ) ,
2592 * N=[ 3 ] , TP=[ 1. 281 ] hr s ,
2593 * Continuous simulation parameters:
2594 * IaRECper=[ 4 ] ( hr s ) ,
2595 * SMN=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
2596 * InterEventTime=[ 12 ] ( hr s )
2597 * Baseflow simulation parameters:
2598 * BaseFlowOption=[ 1 ] ,
2599 * InitGWResVol=[ 50 ] ( mm ) , GWResK=[ 0. 96 ] ( mm/ day/ mm)
2600 * VHydCond=[ 0. 055 ] ( mm/ hr ) , END=- 1
2601 *%-----|-----
2602 *COMPUTE DUALHYD NHYDin=[ " S- 1- D3 " ] , CINLET=[ 0. 719 ] ( cms ) , NINLET=[ 1 ] ,
2603 * MajNHYD=[ " S- 1- D3J " ]
2604 * MnNHYD=[ " S- 1- D3N " ]
2605 * TMSTO=[ 9999999 ] ( cu- m)
2606 *%-----|-----
2607 *ADD HYD NHYDs um=[ " S- 1- D3S " ] , NHYDs to add=[ " S- 1- D3J " + " S- 1- D3N " ]
2608 *%-----|-----
2609 *ROUTE RESERVOIR NHYDout=[ " S- 1- D3R " ] , NHYDin=[ " S- 1- D3S " ] ,
2610 * RDT=[ 1 ] ( mi n ) ,
2611 * TABLE of ( OUTFLOW STORAGE ) values
2612 * ( cms ) - ( ha- m)

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2613 * [ 0.0 , 0.0 ]
2614 * [ 0.0811, 0.2708 ]
2615 * [ -1 , -1 ] (max twenty pts)
2616 * NHYDovf=[ "S-1-D3Rovf" ]
2617 *%-----|-----
2618 CONTINUOUS STANDHYD NHYD=[ "S-1-D4" ], DT=[ 1 ](mi n), AREA=[ 3.28 ](ha), XI MP=[ 0.65 ],
TI MP=[ 0.65 ], DWF=[ 0 ](cms),
2619 LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
I Aper=[ 4.67 ](mm), SLPP=[ 2.0 ]( % ),
2620 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](mi n), Impervious surfaces:
I Ai mp=[ 1.57 ](mm), SLPI=[ 0.75 ]( % ),
2621 LGI=[ 147.874 ](m), MNI=[ 0.013 ], SCI=[ 0 ](mi n),
2622 Continuous simulation parameters:
I aRECper=[ 4 ](hrs), I aRECI mp=[ 4 ](hrs),
2623 SM N=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2624 SM N=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2625 InterEventTime=[ 12 ](hrs), END=- 1
2626 *%-----|-----
2627 *CONTINUOUS NASHYD NHYD=[ "S-1-D4" ], DT=[ 1 ]mi n, AREA=[ 3.28 ](ha),
2628 * DWF=[ 0 ](cms), CN C=[ 77 ], I A=[ 4.67 ](mm),
2629 * N=[ 3 ], TP=[ 1.10 ]hrs,
2630 * Continuous simulation parameters:
2631 * I aRECper=[ 4 ](hrs),
2632 * SM N=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2633 * InterEventTime=[ 12 ](hrs)
2634 * Baseflow simulation parameters:
2635 * BaseFlowOption=[ 1 ],
2636 * I nitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2637 * VHydCond=[ 0.055 ](mm/hr), END=- 1
2638 *%-----|-----
2639 *COMPUTE DUALHYD NHYDi n=[ "S-1-D4" ], CI NLET=[ 0.373 ](cms), NI NLET=[ 1 ],
2640 * Mi j NHYD=[ "S-1-D4J" ]
2641 * M nNHYD=[ "S-1-D4N" ]
2642 * TM I STO=[ 9999999 ](cu-m)
2643 *%-----|-----
2644 *ADD HYD NHYDs um=[ "S-1-D4S" ], NHYDs to add=[ "S-1-D4J"+"S-1-D4N" ]
2645 *%-----|-----
2646 *ROUTE RESERVOIR NHYDout=[ "S-1-D4R" ], NHYDi n=[ "S-1-D4S" ],
2647 * RDT=[ 1 ](mi n),
2648 * TABLE of ( OUTFLOW STORAGE ) values
2649 * (cms) - (ha-m)
2650 * [ 0.0 , 0.0 ]
2651 * [ 0.0392, 0.1308 ]
2652 * [ -1 , -1 ] (max twenty pts)
2653 * NHYDovf=[ "S-1-D4Rovf" ]
2654 *%-----|-----
2655 CONTINUOUS STANDHYD NHYD=[ "S-1-D5" ], DT=[ 1 ](mi n), AREA=[ 12.84 ](ha), XI MP=[ 0.65 ],
TI MP=[ 0.65 ], DWF=[ 0 ](cms),
2656 LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
I Aper=[ 4.67 ](mm), SLPP=[ 2.0 ]( % ),
2657 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](mi n), Impervious surfaces:
I Ai mp=[ 1.57 ](mm), SLPI=[ 0.75 ]( % ),
2658 LGI=[ 292.57 ](m), MNI=[ 0.013 ], SCI=[ 0 ](mi n),
2659 Continuous simulation parameters:
I aRECper=[ 4 ](hrs), I aRECI mp=[ 4 ](hrs),
2660 SM N=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2661 SM N=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2662 InterEventTime=[ 12 ](hrs), END=- 1
2663 *%-----|-----
2664 *CONTINUOUS NASHYD NHYD=[ "S-1-D5" ], DT=[ 1 ]mi n, AREA=[ 12.84 ](ha),
2665 * DWF=[ 0 ](cms), CN C=[ 77 ], I A=[ 4.67 ](mm),
2666 * N=[ 3 ], TP=[ 1.10 ]hrs,
2667 * Continuous simulation parameters:
2668 * I aRECper=[ 4 ](hrs),
2669 * SM N=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2670 * InterEventTime=[ 12 ](hrs)
2671 * Baseflow simulation parameters:
2672 * BaseFlowOption=[ 1 ],

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2673 *          I n i t G W R e s V o l =[ 50 ] ( m m ) ,   G W R e s K =[ 0. 96 ] ( m m / d a y / m m )
2674 *          V H y d C o n d =[ 0. 055 ] ( m m / h r ) ,   E N D = - 1
2675 *%-----|-----
2676 *COMPUTE DUALHYD  N H Y D i n =[ " S - 1 - D 5 " ] ,   C I N L E T =[ 1. 395 ] ( c m s ) ,   N I N L E T =[ 1 ] ,
2677 *          M a j N H Y D =[ " S - 1 - D 5 J " ]
2678 *          M n N H Y D =[ " S - 1 - D 5 N " ]
2679 *          T M I S T O =[ 9999999 ] ( c u - m )
2680 *%-----|-----
2681 *ADD HYD          N H Y D s u m =[ " S - 1 - D 5 S " ] ,   N H Y D s t o a d d =[ " S - 1 - D 5 J " + " S - 1 - D 5 N " ]
2682 *%-----|-----
2683 *ROUTE RESERVOIR N H Y D o u t =[ " S - 1 - D 5 R " ] ,   N H Y D i n =[ " S - 1 - D 5 S " ] ,
2684 *          R D T =[ 1 ] ( m i n ) ,
2685 *          T A B L E o f ( O U T F L O W S T O R A G E ) v a l u e s
2686 *          ( c m s ) - ( h a - m )
2687 *          [ 0. 0      , 0. 0 ]
2688 *          [ 0. 1535, 0. 5120 ]
2689 *          [ - 1      , - 1      ] ( m a x t w e n t y p t s )
2690 *          N H Y D o v f =[ " S - 1 - D 5 R o v f " ]
2691 *%-----|-----
2692 CONTINUOUS STANDHYD N H Y D =[ " S - 1 - D 6 " ] ,   D T =[ 1 ] ( m i n ) ,   A R E A =[ 1. 75 ] ( h a ) ,   X I M P =[ 0. 65 ] ,
T I M P =[ 0. 65 ] ,   D W F =[ 0 ] ( c m s ) ,
2693 LOSS =[ 2 ] ,   S C S c u r v e n u m b e r C N =[ 75 ] ,   P e r v i o u s s u r f a c e s :
I A p e r =[ 4. 67 ] ( m m ) ,   S L P P =[ 2. 0 ] ( % ) ,
2694 L G P =[ 40 ] ( m ) ,   M N P =[ 0. 25 ] ,   S C P =[ 0 ] ( m i n ) ,   I m p e r v i o u s s u r f a c e s :
I A i m p =[ 1. 57 ] ( m m ) ,   S L P I =[ 0. 75 ] ( % ) ,
2695 L G I =[ 108. 01 ] ( m ) ,   M N I =[ 0. 013 ] ,   S C I =[ 0 ] ( m i n ) ,
2696 C o n t i n u o u s s i m u l a t i o n p a r a m e t e r s :
2697 I a R E C p e r =[ 4 ] ( h r s ) ,   I a R E C i m p =[ 4 ] ( h r s ) ,
2698 S M N =[ - 1 ] ( m m ) ,   S M A X =[ - 1 ] ( m m ) ,   S K =[ 0. 010 ] / ( m m ) ,
2699 I n t e r E v e n t T i m e =[ 12 ] ( h r s ) ,   E N D = - 1
2700 *%-----|-----
2701 *CONTINUOUS NASHYD  N H Y D =[ " S - 1 - D 6 " ] ,   D T =[ 1 ] m i n ,   A R E A =[ 1. 75 ] ( h a ) ,
2702 *          D W F =[ 0 ] ( c m s ) ,   C N C =[ 77 ] ,   I A =[ 4. 67 ] ( m m ) ,
2703 *          N =[ 3 ] ,   T P =[ 1. 10 ] h r s ,
2704 *          C o n t i n u o u s s i m u l a t i o n p a r a m e t e r s :
2705 *          I a R E C p e r =[ 4 ] ( h r s ) ,
2706 *          S M N =[ - 1 ] ( m m ) ,   S M A X =[ - 1 ] ( m m ) ,   S K =[ 0. 010 ] / ( m m ) ,
2707 *          I n t e r E v e n t T i m e =[ 12 ] ( h r s )
2708 *          B a s e f l o w s i m u l a t i o n p a r a m e t e r s :
2709 *          B a s e F l o w O p t i o n =[ 1 ] ,
2710 *          I n i t G W R e s V o l =[ 50 ] ( m m ) ,   G W R e s K =[ 0. 96 ] ( m m / d a y / m m )
2711 *          V H y d C o n d =[ 0. 055 ] ( m m / h r ) ,   E N D = - 1
2712 *%-----|-----
2713 *COMPUTE DUALHYD  N H Y D i n =[ " S - 1 - D 6 " ] ,   C I N L E T =[ 0. 218 ] ( c m s ) ,   N I N L E T =[ 1 ] ,
2714 *          M a j N H Y D =[ " S - 1 - D 6 J " ]
2715 *          M n N H Y D =[ " S - 1 - D 6 N " ]
2716 *          T M I S T O =[ 9999999 ] ( c u - m )
2717 *%-----|-----
2718 *ADD HYD          N H Y D s u m =[ " S - 1 - D 6 S " ] ,   N H Y D s t o a d d =[ " S - 1 - D 6 J " + " S - 1 - D 6 N " ]
2719 *%-----|-----
2720 *ROUTE RESERVOIR N H Y D o u t =[ " S - 1 - D 6 R " ] ,   N H Y D i n =[ " S - 1 - D 6 S " ] ,
2721 *          R D T =[ 1 ] ( m i n ) ,
2722 *          T A B L E o f ( O U T F L O W S T O R A G E ) v a l u e s
2723 *          ( c m s ) - ( h a - m )
2724 *          [ 0. 0      , 0. 0 ]
2725 *          [ 0. 0209, 0. 0698 ]
2726 *          [ - 1      , - 1      ] ( m a x t w e n t y p t s )
2727 *          N H Y D o v f =[ " S - 1 - D 6 R o v f " ]
2728 *%-----|-----
2729 CONTINUOUS STANDHYD N H Y D =[ " S - 1 - D 7 " ] ,   D T =[ 1 ] ( m i n ) ,   A R E A =[ 2. 03 ] ( h a ) ,   X I M P =[ 0. 65 ] ,
T I M P =[ 0. 65 ] ,   D W F =[ 0 ] ( c m s ) ,
2730 LOSS =[ 2 ] ,   S C S c u r v e n u m b e r C N =[ 75 ] ,   P e r v i o u s s u r f a c e s :
I A p e r =[ 4. 67 ] ( m m ) ,   S L P P =[ 2. 0 ] ( % ) ,
2731 L G P =[ 40 ] ( m ) ,   M N P =[ 0. 25 ] ,   S C P =[ 0 ] ( m i n ) ,   I m p e r v i o u s s u r f a c e s :
I A i m p =[ 1. 57 ] ( m m ) ,   S L P I =[ 0. 75 ] ( % ) ,
2732 L G I =[ 116. 33 ] ( m ) ,   M N I =[ 0. 013 ] ,   S C I =[ 0 ] ( m i n ) ,

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2733 Continuous simulation parameters:
2734 IaRECper=[ 4](hr s), IaRECImp=[ 4](hr s),
2735 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2736 InterEventTime=[ 12](hr s), END=- 1
2737 *%-----|-----
2738 *CONTINUOUS NASHYD NHYD=["S-1-D7"], DT=[ 1]min, AREA=[ 2.03](ha),
2739 * DWF=[ 0](cms), CN C=[ 77], IA=[ 4.67](mm),
2740 * N=[ 3], TP=[ 1.10]hr s,
2741 * Continuous simulation parameters:
2742 * IaRECper=[ 4](hr s),
2743 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2744 * InterEventTime=[ 12](hr s)
2745 * Baseflow simulation parameters:
2746 * BaseFlowOption=[ 1],
2747 * InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2748 * VHydCond=[ 0.055](mm/hr), END=- 1
2749 *%-----|-----
2750 *COMPUTE DUALHYD NHYDin=["S-1-D7"], CINLET=[ 2.279](cms), NINLET=[ 1],
2751 * MjNHYD=["S-1-D7J"]
2752 * MnNHYD=["S-1-D7N"]
2753 * TMS TO=[ 9999999](cu-m)
2754 *%-----|-----
2755 *ADD HYD NHYDsum=["S-1-D7S"], NHYDs to add=["S-1-D7J"+"S-1-D7N"]
2756 *%-----|-----
2757 *ROUTE RESERVOIR NHYDout=["S-1-D7R"], NHYDin=["S-1-D7S"],
2758 * RDT=[ 1](min),
2759 * TABLE of ( OUTFLOW STORAGE ) values
2760 * (cms) - (ha-m)
2761 * [ 0.0 , 0.0 ]
2762 * [ 0.0243, 0.0810 ]
2763 * [ -1 , -1 ] (max twenty pts)
2764 * NHYDovf=["S-1-D8Rovf"]
2765 *%-----|-----
2766 * -JFSA 2021-02-26 "S-1-D8" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2767 *CONTINUOUS STANDHYD NHYD=["S-1-D8"], DT=[ 1](min), AREA=[ 5.27](ha), XI MP=[ 0.65],
TI MP=[ 0.65], DWF=[ 0](cms),
2768 * LOSS=[ 2], SCS curve number CN=[ 75], Pervious surfaces:
I Aper=[ 4.67](mm), SLPP=[ 2.0](%),
2769 * LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min), Impervious surfaces:
I Ai mp=[ 1.57](mm), SLPI=[ 0.75](%),
2770 * LGI=[ 187.439](m), MNI=[ 0.013], SCI=[ 0](min),
2771 * Continuous simulation parameters:
2772 * IaRECper=[ 4](hr s), IaRECImp=[ 4](hr s),
2773 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2774 * InterEventTime=[ 12](hr s), END=- 1
2775 *%-----|-----
2776 *CONTINUOUS NASHYD NHYD=["S-1-D8"], DT=[ 1]min, AREA=[ 5.27](ha),
2777 * DWF=[ 0](cms), CN C=[ 77], IA=[ 4.67](mm),
2778 * N=[ 3], TP=[ 1.10]hr s,
2779 * Continuous simulation parameters:
2780 * IaRECper=[ 4](hr s),
2781 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2782 * InterEventTime=[ 12](hr s)
2783 * Baseflow simulation parameters:
2784 * BaseFlowOption=[ 1],
2785 * InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2786 * VHydCond=[ 0.055](mm/hr), END=- 1
2787 *%-----|-----
2788 *COMPUTE DUALHYD NHYDin=["S-1-D8"], CINLET=[ 2.279](cms), NINLET=[ 1],
2789 * MjNHYD=["S-1-D8J"]
2790 * MnNHYD=["S-1-D8N"]
2791 * TMS TO=[ 9999999](cu-m)
2792 *%-----|-----
2793 *ADD HYD NHYDsum=["S-1-D8S"], NHYDs to add=["S-1-D8J"+"S-1-D8N"]
2794 *%-----|-----

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2795 *ADD HYD NHYDsum=["S-1-D"], NHYDs to add=["S-1-Okeefe"+"S-1"+"S-1-Fost"]
2796 *%-----|-----|
2797 *COMPUTE DUALHYD NHYDin=["S-1-D"], C/NLET=[11.616](cms), N/NLET=[1],
2798 * Mj NHYD=["S-1-D-M"]
2799 * MnNHYD=["S-1-D-MN"]
2800 * T/STO=[5974](cu-m)
2801 *%-----|-----|
2802 *ADD HYD NHYDsum=["S-1-DEV"], NHYDs to add=["S-1-D-M"+"S-1-D-MN"]
2803 *%-----|-----|
2804 *ROUTE RESERVOIR NHYDout=["S-1-D&R"], NHYDin=["S-1-D&S"],
2805 * RDT=[1](min),
2806 * TABLE of ( OUTFLOW STORAGE ) values
2807 * (cms) - (ha-m)
2808 * [ 0.0 , 0.0 ]
2809 * [ 0.0630, 0.2102 ]
2810 * [ -1 , -1 ] (max twenty pts)
2811 * NHYDovf=["S-1-D&Rovf"]
2812 *%-----|-----|
2813 *%-----|-----|
2814 * -JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
(W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
2815 *# Catchment W_CLAR
2816 *# - To West Clarke Drain (south of the Jock)
2817 *# - Subdivision with 43% imp. as per Barrhaven South MS
2818 *# - 2020-11-30 update CLARKE Tributary Drainage Area to = 121 ha based on
P598(04)-11
2819 *# - 2020-11-30 split CLARKE Drainage Area to MAJOR and ALL
2820 *#*****
2821 CONTINUOUS STANDHYD NHYD=["W_CLAR_M"], DT=[1]min, AREA=[1.772](ha),
2822 XI MP=[0.46], TI MP=[0.59], DWF=[0](cms), LOSS=[2],
2823 SCS curve number CN=[77],
2824 Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
2825 LGP=[40](m), MNP=[0.25], SCP=[0](min),
2826 Impervious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
2827 LGI=[109](m), MNI=[0.013], SCI=[0](min),
2828 Continuous simulation parameters:
2829 I a REC per=[4](hrs), I a REC i mp=[4](hrs),
2830 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2831 Inter Event Time=[18](hrs), END=-1
2832 *%-----|-----|
2833 *COMPUTE DUALHYD NHYDin=["W_CLAR_M"], C/NLET=[0.213](cms), N/NLET=[1],
2834 * Mj NHYD=["W_CLAR_Mj"]
2835 * MnNHYD=["W_CLAR_Mn"]
2836 * T/STO=[0.1](cu-m)
2837 *%-----|-----|
2838 *# 5-Year + 12% Capture
2839 ROUTE RESERVOIR NHYDout=["W_CLAR_Mn"], NHYDin=["W_CLAR_M"],
2840 * RDT=[1](min),
2841 * TABLE of ( OUTFLOW STORAGE ) values
2842 * (cms) - (ha-m)
2843 * [ 0.0 , 0.0 ]
2844 * [ 0.213 , 0.0001 ]
2845 * [ -1 , -1 ] (max twenty pts)
2846 * NHYDovf=["W_CLAR_Mj"],
2847 *%-----|-----|
2848 * -Clarke_All area from P 598(04)-11 = 120.207 ha, change to 127.298 ha based on
GIS measurements,
2849 * -JFSA 2021-01-19 update W_CLAR_ALL to (121.17-1.772=119.398) ha based on GIS
measurements W_CLAR is 121.17 ha and W_CLAR_M is 1.772 ha
2850 CONTINUOUS STANDHYD NHYD=["W_CLAR_ALL"], DT=[1]min, AREA=[119.398](ha),
2851 XI MP=[0.60], TI MP=[0.65], DWF=[0](cms), LOSS=[2],
2852 SCS curve number CN=[77],
2853 Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
2854 LGP=[40](m), MNP=[0.25], SCP=[0](min),
2855 Impervious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
2856 LGI=[892.18](m), MNI=[0.013], SCI=[0](min),

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2857 Continuous simulation parameters:
2858 IaRECper=[ 4](hrs), IaRECimp=[ 4](hrs),
2859 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2860 InterEventTime=[ 18](hrs), END=- 1
2861 *%-----|-----|
2862 ADD HYD NHYDsum=["W_CLAR"], NHYDsto add=["W_CLAR_ALL"+"W_CLAR_Mj"]
2863 *%-----|-----|
2864 SAVE HYD NHYD=["W_CLAR"], # OF PCYCLES=[ -1], ICASEsh=[ 1]
2865 HYD_COMMENT=["Total Flows to West Clarke"]
2866 *#*****
2867 *# West Clarke Pond 2
2868 *# - Rating curve obtained from Barrhaven South M&S modeling
2869 *# - Tributary Drainage Area to M&S Pond 2 = 241 ha
2870 *#*****
2871 ROUTE RESERVOIR NHYDout=["MS_P2"], NHYDin=["W_CLAR"],
2872 RDT=[ 1](min),
2873 TABLE of ( OUTFLOW STORAGE ) values
2874 (cms) - (ha-m)
2875 [ 0.0 , 0.0 ]
2876 [ 0.128 , 0.161 ]
2877 [ 0.138 , 0.409 ]
2878 [ 0.148 , 0.68 ]
2879 [ 0.227 , 0.931 ]
2880 [ 0.354 , 1.223 ]
2881 [ 0.505 , 1.52 ]
2882 [ 0.666 , 1.821 ]
2883 [ 0.831 , 2.123 ]
2884 [ 0.995 , 2.434 ]
2885 [ 1.069 , 2.583 ]
2886 [ 1.51 , 2.647 ]
2887 [ 4.904 , 2.861 ]
2888 [ 13.048 , 3.188 ]
2889 [ 23.745 , 3.523 ]
2890 [ 36.474 , 3.871 ]
2891 [ 45.938 , 4.127 ]
2892 [ 61.652 , 4.539 ]
2893 [ -1 , -1 ] (max twenty pts)
2894 NHYDovf=["P2-OVF"]
2895 *%-----|-----|
2896 *#*****
2897 * -JFSA, 2021-01-22 "W_CLAR_UNDE" (west of Clarke sub-catchment) discharges
directly to the jock river through a road side ditch on the west side of Borrisokane
road (station 6016)
2898 *CONTINUOUS NASHYD NHYD=["W_CLAR_UNDE"], DT=[ 1]min, AREA=[ 35.65](ha),
2899 * DWF=[ 0](cms), CNVC=[ 77], IA=[ 4.67](mm),
2900 * N=[ 3], TP=[ 1.10]hrs,
2901 * Continuous simulation parameters:
2902 * IaRECper=[ 4](hrs),
2903 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2904 * InterEventTime=[ 12](hrs)
2905 * Baseflow simulation parameters:
2906 * BaseFlowOption=[ 1],
2907 * InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2908 * VHydCond=[ 0.055](mm/hr), END=- 1
2909 *%-----|-----|
2910 ADD HYD NHYDsum=["SN_CE"], NHYDsto
add=["N_CE"+"S-1-D4"+"S-1-D5"+"MS_P2"+"P2-OVF"]
2911 *%-----|-----|
2912 SAVE HYD NHYD=["SN_CE"], # OF PCYCLES=[ -1], ICASEsh=[ 1]
2913 HYD_COMMENT=["Total Flows before Station 5737 on Jock River"]
2914 *%-----|-----|
2915 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5737
2916 *# 2021-02-25 add station 5737 before station 5002. Station 5737 was extracted from the
HEC-RAS model
T:\PROJ\1474-16\Design\20201026-QuantityControlAnalysis\HEC-RAS\JockLidar2005
2917 *# JFSA 2021-03-02 change the slope to 0.0175% instead of 0.02593 to stabilize the model

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2918 ROUTE CHANNEL      NHYDout =[" 5737" ] , NHYDin=[" SN_CE" ] ,
2919                    RDT=[ 1 ] ( m i n ) ,
2920                    CHLGTH=[ 270 ] ( m ) ,    CHSLOPE=[ 0. 0175 ] ( % ) ,
2921                    FPSLOPE=[ 0. 0175 ] ( % ) ,
2922                    SECNUM=[ 1. 0 ] ,        NSEG=[ 3 ]
2923                    ( SEGROUGH, SEGDI ST ( m ) ) =
2924                    [ 0. 050, - 24. 04
2925                    - 0. 035, 23. 92
2926                    0. 050, 1130. 8 ] NSEG t i m e s
2927                    ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
2928                    [ - 1060. 52, 94 ]
2929                    [ - 268. 6, 91. 5 ]
2930                    [ - 259. 43, 91. 5 ]
2931                    [ - 179. 48, 91. 5 ]
2932                    [ - 67. 9, 91. 5 ]
2933                    [ - 59. 21, 91. 5 ]
2934                    [ - 33. 19, 91 ]
2935                    [ - 26. 08, 90. 5 ]
2936                    [ - 24. 04, 90 ]
2937                    [ - 13. 14, 86. 77 ]
2938                    [ 0, 85 ]
2939                    [ 14. 68, 86. 74 ]
2940                    [ 23. 92, 90 ]
2941                    [ 25. 78, 90. 5 ]
2942                    [ 31. 91, 91 ]
2943                    [ 91. 95, 91. 5 ]
2944                    [ 772. 15, 92 ]
2945                    [ 961. 49, 92. 5 ]
2946                    [ 1044. 69, 93 ]
2947                    [ 1130. 8, 95 ]
2948 *%-----|-----|
2949 ADD HYD           NHYDs um=[" 5002" ] , NHYDs t o add=[" 5737"+"S- 1- D1"+"S- 1- D6"+"S- 1- D7" ]
2950 *%-----|-----|
2951 SAVE HYD         NHYD=[" 5002" ] ,    # OF PCYCLES=[ - 1 ] ,    I CASEs h=[ 1 ]
2952                 HYD_COMMENT=[" Total Flows before Station 5002 on Jock Ri ver" ]
2953 *%-----|-----|
2954 *# Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain
2955 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5002
2956 *# JFSA 2021-02-19 Change the slope from 0.01 % (as per Stantec Report 2007) to 0.0255
% so the model will be more stable and give reasonable results. It is justifiable as
ROUTE CHANNELs aren't well suited to really flat slopes.
2957 *# JFSA 2021-02-19 Change to three ROUTE CHANNEL with length 275 m each instead of one
with 825 m length so the model will be more stable
2958 *# JFSA 2021-02-26 change the length of 5002 route channel from 825 m to 736 m That is
because of adding station 5737 between station 6016 and station 5002. Then the length
from station 5737 to station 5002 is 736 m Change the slope from 0.0255 % to 0.09511 %
2959 *
2960 ROUTE CHANNEL      NHYDout =[" N_VCa" ] , NHYDin=[" 5002" ] ,
2961                    RDT=[ 1 ] ( m i n ) ,
2962                    CHLGTH=[ 245. 33333 ] ( m ) ,    CHSLOPE=[ 0. 09511 ] ( % ) ,
2963                    FPSLOPE=[ 0. 09511 ] ( % ) ,
2964                    SECNUM=[ 1. 0 ] ,        NSEG=[ 3 ]
2965                    ( SEGROUGH, SEGDI ST ( m ) ) =
2966                    [ 0. 050, - 37. 5
2967                    - 0. 035, 37. 50
2968                    0. 050, 157. 05 ] NSEG t i m e s
2969                    ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
2970                    [ - 601. 81, 91. 5 ]
2971                    [ - 37. 50, 90. 00 ]
2972                    [ - 19. 61, 87. 04 ]
2973                    [ 0. 00, 85. 70 ]
2974                    [ 14. 87, 86. 93 ]
2975                    [ 37. 50, 90. 00 ]
2976                    [ 38. 54, 90. 50 ]
2977                    [ 42. 23, 91 ]
2978                    [ 157. 05, 91. 50 ]

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2979 * [ 161.44, 91.50]
2980 * [ 236.48, 93.00]
2981 * [ 385.47, 92.50]
2982 * [ 390.78, 92.50]
2983 *%-----|
2984 ROUTE CHANNEL NHYDout=["N_WCb"] , NHYDin=["N_WCa"] ,
2985 RDT=[ 1]( m n),
2986 CHLGTH=[ 245.33333]( m), CHSLOPE=[ 0.09511]( %),
2987 FPSLOPE=[ 0.09511]( %),
2988 SECNUM=[ 1.0], NSEG=[ 3]
2989 ( SEGROUGH, SEGDI ST ( m))=
2990 [ 0.050, -37.5
2991 -0.035, 37.50
2992 0.050, 157.05] NSEG t i m e s
2993 ( DI STANCE ( m), ELEVATI ON ( m))=
2994 [- 601.81, 91.5]
2995 [- 37.50, 90.00]
2996 [- 19.61, 87.04]
2997 [ 0.00, 85.70]
2998 [ 14.87, 86.93]
2999 [ 37.50, 90.00]
3000 [ 38.54, 90.50]
3001 [ 42.23, 91]
3002 [ 157.05, 91.50]
3003 *%-----|
3004 ROUTE CHANNEL NHYDout=["N_WC"] , NHYDin=["N_WCb"] ,
3005 RDT=[ 1]( m n),
3006 CHLGTH=[ 245.33333]( m), CHSLOPE=[ 0.09511]( %),
3007 FPSLOPE=[ 0.09511]( %),
3008 SECNUM=[ 1.0], NSEG=[ 3]
3009 ( SEGROUGH, SEGDI ST ( m))=
3010 [ 0.050, -37.5
3011 -0.035, 37.50
3012 0.050, 157.05] NSEG t i m e s
3013 ( DI STANCE ( m), ELEVATI ON ( m))=
3014 [- 601.81, 91.5]
3015 [- 37.50, 90.00]
3016 [- 19.61, 87.04]
3017 [ 0.00, 85.70]
3018 [ 14.87, 86.93]
3019 [ 37.50, 90.00]
3020 [ 38.54, 90.50]
3021 [ 42.23, 91]
3022 [ 157.05, 91.50]
3023 ##*****
3024 * -JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
(W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
3025 *ADD HYD NHYDsum=["SN_WC"], NHYDs to
add=["MS_P2"+"P2-OVF"+"N_WC"+"W_CLAR_UNDE"]
3026 *%-----|
3027 *SAVE HYD NHYD=["SN_WC"], # OF PCYCLES=[ -1], I CASEs h=[ 1]
3028 * HYD_COMMENT=["Total Flows at West Clarke Pond Outlet"]
3029 *%-----|
3030 *# Hydrograph from Node West Clarke routed to Node at Kennedy - Burnett Drain
3031 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4534
3032 *#
3033 ROUTE CHANNEL NHYDout=["N_KB"] , NHYDin=["N_WC"] ,
3034 RDT=[ 1]( m n),
3035 CHLGTH=[ 1020]( m), CHSLOPE=[ 0.0498]( %),
3036 FPSLOPE=[ 0.0498]( %),
3037 SECNUM=[ 1.0], NSEG=[ 3]
3038 ( SEGROUGH, SEGDI ST ( m))=
3039 [ 0.050, -23.63
3040 -0.035, 23.63
3041 0.050, 728.3] NSEG t i m e s
3042 ( DI STANCE ( m), ELEVATI ON ( m))=

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3043 [- 1082. 01, 94]
3044 [- 1028. 17, 92. 5]
3045 [- 992. 3, 93. 5]
3046 [- 279. 34, 90]
3047 [- 23. 63, 90]
3048 [- 13. 45, 87. 13]
3049 [- 0. 07, 86. 24]
3050 [ 10. 54, 87. 15]
3051 [ 23. 63, 90]
3052 [ 24. 86, 90. 5]
3053 [ 26. 72, 91]
3054 [ 45. 07, 91. 5]
3055 [ 128. 17, 91. 5]
3056 [ 270. 7, 92. 5]
3057 [ 728. 3, 95]
3058 *%-----|-----|
3059 *#*****|*****|
3060 *# Catchment KEN_BU
3061 *# - To Kennedy-Burnett SWM Facility
3062 *# - Outlets to Fraser-Clarke drain (north of the Jock)
3063 *# - Medium density residential subdivision
3064 * - Add Kennedy Burnett model (Convert PCSWMM from NOVATECH June, 2020 to SWWHYMO)
3065 *#*****|*****|
3066 *CONTINUOUS STANDHYD NHYD=["KEN_BU"], DT=[ 1] mi n, AREA=[ 281] (ha),
3067 * XI MP=[ 0. 55], TI MP=[ 0. 55], DWF=[ 0] (cms), LOSS=[ 2],
3068 * SCS curve number CN=[ 71],
3069 * Pervious surfaces: I A per=[ 4. 67] (mm), SLPP=[ 1] (%),
3070 * LGP=[ 40] (m), MNP=[ 0. 25], SCP=[ 0] (mi n),
3071 * Impervious surfaces: I A i mp=[ 1. 57] (mm), SLPI=[ 1] (%),
3072 * LGI=[ 1369] (m), MNI=[ 0. 013], SCI=[ 0] (mi n),
3073 * Continuous simulation parameters:
3074 * I a REC per=[ 4] (hrs), I a REC i mp=[ 4] (hrs),
3075 * SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
3076 * Int er Event Ti me=[ 18] (hrs), END=- 1
3077 *%-----|-----|
3078 *#*****|*****|
3079 *# Existing Kennedy-Burnett SWM Facility
3080 *# - Rating curve obtained from URTKBP
3081 *# - Tributary Drainage Area to Pond = 160 ha
3082 *#*****|*****|
3083 *ROUTE RESERVOIR NHYDout=["KEN_P"], NHYDin=["KEN_BU"],
3084 * RDT=[ 1] (mi n),
3085 * TABLE of ( OUTFLOW STORAGE ) values
3086 * ( cms ) - ( ha- m)
3087 * [ 0. 0 , 0. 0 ]
3088 * [ 0. 13 , 0. 26]
3089 * [ 0. 43 , 0. 56]
3090 * [ 0. 67 , 0. 90]
3091 * [ 0. 86 , 1. 32]
3092 * [ 1. 01 , 1. 79]
3093 * [ 1. 15 , 2. 33]
3094 * [ - 1 , - 1 ] (max twenty pts)
3095 * NHYDovf=["KEN-OV"]
3096 *%-----|-----|
3097 * -JFSA, 2021-01-19 update all KEN_BU areas based on GIS measurements
3098 CONTINUOUS STANDHYD NHYD=["KB-01A"], DT=[ 1] mi n, AREA=[ 40. 82] (ha), XI MP=[ 0. 097],
3099 TI MP=[ 0. 4], DWF=[ 0] (cms), LOSS=[ 1]:
3099 Horton: Fo=[ 76. 20] (mm/ hr), Fc=[ 13. 20] (mm/ hr), DCAY=[ 4. 14] (/ hr),
3100 F=[ 0. 00] (mm),
3100 Pervious areas: I A per=[ 4. 67] (mm), SLPP=[ 0. 5] (%), LGP=[ 40] (m),
3101 MNP=[ 0. 250], SCP=[ 0] (mi n),
3101 Impervious areas: I A i mp=[ 0. 785] (mm), SLPI=[ 0. 5] (%),
3102 LGI=[ 521. 664] (m), MNI=[ 0. 013], SCI=[ 0] (mi n),
3102 Continuous simulation parameters:
3103 I a REC per=[ 4] (hrs), I a REC i mp=[ 4] (hrs), Int er Event Ti me=[ 12] (hrs),
3103 END=- 1

```

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3104 *%-----|-----|
3105 COMPUTE DUALHYD NHYDin=[ " KB- 01A" ], CI NLET=[ 3. 6 ] ( cms ), NI NLET=[ 1 ],
3106 Māj NHYD=[ " KB- 01A- M " ]
3107 M nNHYD=[ " KB- 01A- MN" ]
3108 TM STO=[ 4995 ] ( cu- m )
3109 *%-----|-----|
3110 ADD HYD NHYDsum=[ " KB- 01A- S" ], NHYDs to add=[ " KB- 01A- M " + " KB- 01A- MN" ]
3111 *%-----|-----|
3112 CONTINUOUS STANDHYD NHYD=[ " KB- 01B" ], DT=[ 1 ] mi n, AREA=[ 31. 1 ] ( ha ), XI MP=[ 0. 1875 ],
TI MP=[ 0. 375 ], DWF=[ 0 ] ( cms ), LOSS=[ 1 ] :
3113 Horton: Fo=[ 76. 20 ] ( mm/ hr ), Fc=[ 13. 20 ] ( mm/ hr ), DCAY=[ 4. 14 ] ( / hr ),
F=[ 0. 00 ] ( mm ),
3114 Pervious areas: I A per=[ 4. 67 ] ( mm ), SLPP=[ 0. 42 ] ( % ), LGP=[ 40 ] ( m ),
MNP=[ 0. 250 ], SCP=[ 0 ] ( mi n ),
3115 Impervious areas: I A i mp=[ 0. 785 ] ( mm ), SLPI=[ 0. 42 ] ( % ),
LGI=[ 455. 339 ] ( m ), MNI=[ 0. 013 ], SCI=[ 0 ] ( mi n ),
3116 Continuous simulation parameters:
3117 I a REC per=[ 4 ] ( hrs ), I a REC i mp=[ 4 ] ( hrs ), Int er Event Ti me=[ 12 ] ( hrs ),
END=- 1
3118 *%-----|-----|
3119 COMPUTE DUALHYD NHYDin=[ " KB- 01B" ], CI NLET=[ 1. 585 ] ( cms ), NI NLET=[ 1 ],
3120 Māj NHYD=[ " KB- 01B- M " ]
3121 M nNHYD=[ " KB- 01B- MN" ]
3122 TM STO=[ 6075 ] ( cu- m )
3123 *%-----|-----|
3124 ADD HYD NHYDsum=[ " KB- 01B- S" ], NHYDs to add=[ " KB- 01B- M " + " KB- 01B- MN" ]
3125 *%-----|-----|
3126 CONTINUOUS STANDHYD NHYD=[ " KB- 01C" ], DT=[ 1 ] mi n, AREA=[ 13. 78 ] ( ha ), XI MP=[ 0. 2045 ],
TI MP=[ 0. 409 ], DWF=[ 0 ] ( cms ), LOSS=[ 1 ] :
3127 Horton: Fo=[ 76. 20 ] ( mm/ hr ), Fc=[ 13. 20 ] ( mm/ hr ), DCAY=[ 4. 14 ] ( / hr ),
F=[ 0. 00 ] ( mm ),
3128 Pervious areas: I A per=[ 4. 67 ] ( mm ), SLPP=[ 2. 0 ] ( % ), LGP=[ 40 ] ( m ),
MNP=[ 0. 250 ], SCP=[ 0 ] ( mi n ),
3129 Impervious areas: I A i mp=[ 0. 785 ] ( mm ), SLPI=[ 0. 5 ] ( % ),
LGI=[ 303. 095 ] ( m ), MNI=[ 0. 013 ], SCI=[ 0 ] ( mi n ),
3130 Continuous simulation parameters:
3131 I a REC per=[ 4 ] ( hrs ), I a REC i mp=[ 4 ] ( hrs ), Int er Event Ti me=[ 12 ] ( hrs ),
END=- 1
3132 *%-----|-----|
3133 COMPUTE DUALHYD NHYDin=[ " KB- 01C" ], CI NLET=[ 1. 35 ] ( cms ), NI NLET=[ 1 ],
3134 Māj NHYD=[ " KB- 01C- M " ]
3135 M nNHYD=[ " KB- 01C- MN" ]
3136 TM STO=[ 1880 ] ( cu- m )
3137 *%-----|-----|
3138 ADD HYD NHYDsum=[ " KB- 01C- S" ], NHYDs to add=[ " KB- 01C- M " + " KB- 01C- MN" ]
3139 *%-----|-----|
3140 CONTINUOUS STANDHYD NHYD=[ " KB- 03" ], DT=[ 1 ] mi n, AREA=[ 84. 78 ] ( ha ), XI MP=[ 0. 197 ],
TI MP=[ 0. 394 ], DWF=[ 0 ] ( cms ), LOSS=[ 1 ] :
3141 Horton: Fo=[ 76. 20 ] ( mm/ hr ), Fc=[ 13. 20 ] ( mm/ hr ), DCAY=[ 4. 14 ] ( / hr ),
F=[ 0. 00 ] ( mm ),
3142 Pervious areas: I A per=[ 4. 67 ] ( mm ), SLPP=[ 2. 0 ] ( % ), LGP=[ 40 ] ( m ),
MNP=[ 0. 250 ], SCP=[ 0 ] ( mi n ),
3143 Impervious areas: I A i mp=[ 0. 785 ] ( mm ), SLPI=[ 0. 63 ] ( % ),
LGI=[ 751. 798 ] ( m ), MNI=[ 0. 013 ], SCI=[ 0 ] ( mi n ),
3144 Continuous simulation parameters:
3145 I a REC per=[ 4 ] ( hrs ), I a REC i mp=[ 4 ] ( hrs ), Int er Event Ti me=[ 12 ] ( hrs ),
END=- 1
3146 *%-----|-----|
3147 COMPUTE DUALHYD NHYDin=[ " KB- 03" ], CI NLET=[ 5. 27 ] ( cms ), NI NLET=[ 1 ],
3148 Māj NHYD=[ " KB- 03- M " ]
3149 M nNHYD=[ " KB- 03- MN" ]
3150 TM STO=[ 15500 ] ( cu- m )
3151 *%-----|-----|
3152 ADD HYD NHYDsum=[ " KB- 03- S" ], NHYDs to add=[ " KB- 03- M " + " KB- 03- MN" ]
3153 *%-----|-----|
3154 CONTINUOUS STANDHYD NHYD=[ " KB- 04" ], DT=[ 1 ] mi n, AREA=[ 6. 95 ] ( ha ), XI MP=[ 0. 85 ],

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3155 TI MP=[0.85], DWF=[0](cms), LOSS=[1]:
 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
 F=[0.00](mm),
 3156 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
 MNP=[0.250], SCP=[0](min),
 3157 Impervious areas: IAimp=[0.942](mm), SLPI=[0.5](%),
 LGI=[215.252](m), MNI=[0.013], SCI=[0](min),
 3158 Continuous simulation parameters:
 3159 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
 END=- 1
 3160 *%-----|
 3161 COMPUTE DUALHYD NHYDin=["KB- 04"], CINLET=[0.503](cms), NINLET=[1],
 3162 MajNHYD=["KB- 04- M"]
 3163 MnNHYD=["KB- 04- MN"]
 3164 TMSTO=[1972](cu-m)
 3165 *%-----|
 3166 ADD HYD NHYDsum=["KB- 04- S"], NHYDs to add=["KB- 04- M"+"KB- 04- MN"]
 3167 *%-----|
 3168 CONTINUOUS STANDHYD NHYD=["KB- 05"], DT=[1]min, AREA=[5.19](ha), XI MP=[0.93],
 TI MP=[0.93], DWF=[0](cms), LOSS=[1]:
 3169 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
 F=[0.00](mm),
 3170 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
 MNP=[0.250], SCP=[0](min),
 3171 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
 LGI=[186.011](m), MNI=[0.013], SCI=[0](min),
 3172 Continuous simulation parameters:
 3173 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
 END=- 1
 3174 *%-----|
 3175 *%-----|
 3176 CONTINUOUS STANDHYD NHYD=["KB- 06"], DT=[1]min, AREA=[12.93](ha), XI MP=[0.873],
 TI MP=[0.873], DWF=[0](cms), LOSS=[1]:
 3177 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
 F=[0.00](mm),
 3178 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
 MNP=[0.250], SCP=[0](min),
 3179 Impervious areas: IAimp=[0.942](mm), SLPI=[4.75](%),
 LGI=[293.598](m), MNI=[0.013], SCI=[0](min),
 3180 Continuous simulation parameters:
 3181 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
 END=- 1
 3182 *%-----|
 3183 COMPUTE DUALHYD NHYDin=["KB- 06"], CINLET=[2.262](cms), NINLET=[1],
 3184 MajNHYD=["KB- 06- M"]
 3185 MnNHYD=["KB- 06- MN"]
 3186 TMSTO=[1950](cu-m)
 3187 *%-----|
 3188 ADD HYD NHYDsum=["KB- 06- S"], NHYDs to add=["KB- 06- M"+"KB- 06- MN"]
 3189 *%-----|
 3190 CONTINUOUS STANDHYD NHYD=["KB- 11"], DT=[1]min, AREA=[4.03](ha), XI MP=[0.675],
 TI MP=[0.675], DWF=[0](cms), LOSS=[1]:
 3191 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
 F=[0.00](mm),
 3192 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
 MNP=[0.250], SCP=[0](min),
 3193 Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%),
 LGI=[163.911](m), MNI=[0.013], SCI=[0](min),
 3194 Continuous simulation parameters:
 3195 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
 END=- 1
 3196 *%-----|
 3197 COMPUTE DUALHYD NHYDin=["KB- 11"], CINLET=[0.5773](cms), NINLET=[1],
 3198 MajNHYD=["KB- 11- M"]
 3199 MnNHYD=["KB- 11- MN"]
 3200 TMSTO=[597](cu-m)

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3201  *%-----|-----|
3202  ADD HYD      NHYDsum=["KB-11-S"], NHYDs to add=["KB-11-M"+"KB-11-MN"]
3203  *%-----|-----|
3204  CONTINUOUS STANDHYD NHYD=["S1"], DT=[1] min, AREA=[4.99](ha), XI MP=[0.93], TI MP=[0.93],
DWF=[0](cms), LOSS=[1]:
3205  Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3206  Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3207  Impervious areas: I A i mp=[1.57](mm), SLPI=[2.0](%),
LGI=[182.392](m), MNI=[0.013], SCI=[0](min),
3208  Continuous simulation parameters:
3209  I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
3210  *%-----|-----|
3211  CONTINUOUS STANDHYD NHYD=["KB-15"], DT=[1] min, AREA=[2.15](ha), XI MP=[0.79],
TI MP=[0.79], DWF=[0](cms), LOSS=[1]:
3212  Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3213  Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3214  Impervious areas: I A i mp=[0.157](mm), SLPI=[0.3](%),
LGI=[119.722](m), MNI=[0.013], SCI=[0](min),
3215  Continuous simulation parameters:
3216  I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
3217  *%-----|-----|
3218  *%-----|-----|
3219  ADD HYD      NHYDsum=["KB-P1"], NHYDs to
add=["KB-01A-S"+"KB-01B-S"+"KB-01C-S"+"KB-03-S"+"KB-04-S"+"KB-05-S"+"KB-06-S"+"KB-11-S"+"KB-
-15"+"S1"]
3220  *%-----|-----|
3221  ROUTE RESERVOIR NHYDout=["KB-P1R"], NHYDin=["KB-P1"],
3222  RDT=[1](min),
3223  TABLE of ( OUTFLOW STORAGE ) values
3224  (cms) - (ha-m)
3225  [ 0.0 , 0.0 ]
3226  [0.076,0.003]
3227  [0.088,0.006]
3228  [0.136,0.011]
3229  [0.301,0.017]
3230  [0.454,0.027]
3231  [0.631,0.041]
3232  [1.173,0.068]
3233  [1.91,0.111]
3234  [4.847,0.231]
3235  [9.813,0.436]
3236  [12.134,0.617]
3237  [12.438,0.732]
3238  [12.424,0.811]
3239  [12.425,0.894]
3240  [ -1 , -1 ] (max twenty pts)
3241  NHYDovf=["KB-P1ovf"]
3242  *%-----|-----|
3243  ADD HYD      NHYDsum=["KB-Pond1"], NHYDs to add=["KB-P1R"+"KB-P1ovf"]
3244  *%-----|-----|
3245  SAVE HYD     NHYD=["KB-Pond1"], # OF PCYCLES=[-1], I CASEs h=[1]
3246  HYD_COMMENT=["Total Flows at KB first pond"]
3247  *%-----|-----|
3248  CONTINUOUS STANDHYD NHYD=["KB-07"], DT=[1] min, AREA=[10.86](ha), XI MP=[0.86],
TI MP=[0.86], DWF=[0](cms), LOSS=[1]:
3249  Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3250  Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3251  Impervious areas: I A i mp=[0.785](mm), SLPI=[2.0](%),

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3252 LGI=[ 269.072](m), MNI=[ 0.013], SCI=[ 0](min),
3253 Continuous simulation parameters:
3253 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3254 END=- 1
3254 *%-----|
3255 COMPUTE DUALHYD NHYDin=["KB-07"], CINLET=[ 2.094](cms), NINLET=[ 1],
3256 MajNHYD=["KB-07-M"]
3257 MnNHYD=["KB-07-MN"]
3258 TMSTO=[ 1378](cu-m)
3259 *%-----|
3260 ADD HYD NHYDsum=["KB-07-S"], NHYDsto add=["KB-07-M"+"KB-07-MN"]
3261 *%-----|
3262 CONTINUOUS STANDHYD NHYD=["KB-08"], DT=[ 1]min, AREA=[ 6.61](ha), XI MP=[ 0.64],
3263 TIMP=[ 0.64], DWF=[ 0](cms), LOSS=[ 1]:
3263 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3264 F=[ 0.00](mm),
3264 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3265 MNP=[ 0.250], SCP=[ 0](min),
3265 Impervious areas: IAimp=[ 0.785](mm), SLPI=[ 2.0](%),
3266 LGI=[ 209.921](m), MNI=[ 0.013], SCI=[ 0](min),
3266 Continuous simulation parameters:
3267 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3268 END=- 1
3268 *%-----|
3269 COMPUTE DUALHYD NHYDin=["KB-08"], CINLET=[ 1.058](cms), NINLET=[ 1],
3270 MajNHYD=["KB-08-M"]
3271 MnNHYD=["KB-08-MN"]
3272 TMSTO=[ 787](cu-m)
3273 *%-----|
3274 ADD HYD NHYDsum=["KB-08-S"], NHYDsto add=["KB-08-M"+"KB-08-MN"]
3275 *%-----|
3276 CONTINUOUS STANDHYD NHYD=["KB-09"], DT=[ 1]min, AREA=[ 2.6](ha), XI MP=[ 0.86],
3277 TIMP=[ 0.86], DWF=[ 0](cms), LOSS=[ 1]:
3277 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3278 F=[ 0.00](mm),
3278 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3279 MNP=[ 0.250], SCP=[ 0](min),
3279 Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 2.0](%),
3280 LGI=[ 131.656](m), MNI=[ 0.013], SCI=[ 0](min),
3280 Continuous simulation parameters:
3281 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3282 END=- 1
3282 *%-----|
3283 *%-----|
3284 CONTINUOUS STANDHYD NHYD=["KB-10_1"], DT=[ 1]min, AREA=[ 2.37](ha), XI MP=[ 0.86],
3285 TIMP=[ 0.86], DWF=[ 0](cms), LOSS=[ 1]:
3285 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3286 F=[ 0.00](mm),
3286 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3287 MNP=[ 0.250], SCP=[ 0](min),
3287 Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 2.0](%),
3288 LGI=[ 125.698](m), MNI=[ 0.013], SCI=[ 0](min),
3288 Continuous simulation parameters:
3289 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3290 END=- 1
3290 *%-----|
3291 CONTINUOUS STANDHYD NHYD=["KB-10_2"], DT=[ 1]min, AREA=[ 1.14](ha), XI MP=[ 0.86],
3292 TIMP=[ 0.86], DWF=[ 0](cms), LOSS=[ 1]:
3292 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3293 F=[ 0.00](mm),
3293 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3294 MNP=[ 0.250], SCP=[ 0](min),
3294 Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 2.0](%), LGI=[ 87.178](m),
3295 MNI=[ 0.013], SCI=[ 0](min),
3295 Continuous simulation parameters:
3296 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),

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END=- 1

3297 *%-----|-----|
3298 *%-----|-----|
3299 CONTINUOUS STANDHYD NHYD=[" KB- 12"], DT=[1] mi n, AREA=[4. 86] (ha), XI MP=[0. 79],
TI MP=[0. 79], DWF=[0] (cms), LOSS=[1]:
3300 Horton: Fo=[76. 20] (mm/ hr), Fc=[13. 20] (mm/ hr), DCAY=[4. 14] (/ hr),
F=[0. 00] (mm),
3301 Pervious areas: IAper=[4. 67] (mm), SLPP=[2. 0] (%), LGP=[40] (m),
MNP=[0. 250], SCP=[0] (mi n),
3302 Impervious areas: IAi mp=[1. 099] (mm), SLPI =[2. 0] (%),
LGI =[180. 000] (m), MNI =[0. 013], SCI =[0] (mi n),
3303 Continuous simulation parameters:
3304 IaRECper=[4] (hrs), IaRECI mp=[4] (hrs), InterEvent Time=[12] (hrs),
END=- 1
3305 *%-----|-----|
3306 COMPUTE DUALHYD NHYDi n=[" KB- 12"], CI NLET=[0. 8665] (cms), NI NLET=[1],
3307 Ma j NHYD=[" KB- 12- M"]
3308 M nNHYD=[" KB- 12- MN"]
3309 TM STO=[632] (cu- m)
3310 *%-----|-----|
3311 ADD HYD NHYDs um=[" KB- 12- S"], NHYDs to add=[" KB- 12- M" +" KB- 12- MN"]
3312 *%-----|-----|
3313 CONTINUOUS STANDHYD NHYD=[" KB- 13"], DT=[1] mi n, AREA=[10. 19] (ha), XI MP=[0. 64],
TI MP=[0. 64], DWF=[0] (cms), LOSS=[1]:
3314 Horton: Fo=[76. 20] (mm/ hr), Fc=[13. 20] (mm/ hr), DCAY=[4. 14] (/ hr),
F=[0. 00] (mm),
3315 Pervious areas: IAper=[4. 67] (mm), SLPP=[2. 0] (%), LGP=[40] (m),
MNP=[0. 250], SCP=[0] (mi n),
3316 Impervious areas: IAi mp=[0. 785] (mm), SLPI =[2. 0] (%),
LGI =[260. 640] (m), MNI =[0. 013], SCI =[0] (mi n),
3317 Continuous simulation parameters:
3318 IaRECper=[4] (hrs), IaRECI mp=[4] (hrs), InterEvent Time=[12] (hrs),
END=- 1
3319 *%-----|-----|
3320 COMPUTE DUALHYD NHYDi n=[" KB- 13"], CI NLET=[1. 722] (cms), NI NLET=[1],
3321 Ma j NHYD=[" KB- 13- M"]
3322 M nNHYD=[" KB- 13- MN"]
3323 TM STO=[1077] (cu- m)
3324 *%-----|-----|
3325 ADD HYD NHYDs um=[" KB- 13- S"], NHYDs to add=[" KB- 13- M" +" KB- 13- MN"]
3326 *%-----|-----|
3327 CONTINUOUS STANDHYD NHYD=[" KB- 14"], DT=[1] mi n, AREA=[5. 47] (ha), XI MP=[0. 64],
TI MP=[0. 64], DWF=[0] (cms), LOSS=[1]:
3328 Horton: Fo=[76. 20] (mm/ hr), Fc=[13. 20] (mm/ hr), DCAY=[4. 14] (/ hr),
F=[0. 00] (mm),
3329 Pervious areas: IAper=[4. 67] (mm), SLPP=[2. 0] (%), LGP=[40] (m),
MNP=[0. 250], SCP=[0] (mi n),
3330 Impervious areas: IAi mp=[0. 785] (mm), SLPI =[2. 0] (%),
LGI =[190. 962] (m), MNI =[0. 013], SCI =[0] (mi n),
3331 Continuous simulation parameters:
3332 IaRECper=[4] (hrs), IaRECI mp=[4] (hrs), InterEvent Time=[12] (hrs),
END=- 1
3333 *%-----|-----|
3334 COMPUTE DUALHYD NHYDi n=[" KB- 14"], CI NLET=[0. 8734] (cms), NI NLET=[1],
3335 Ma j NHYD=[" KB- 14- M"]
3336 M nNHYD=[" KB- 14- MN"]
3337 TM STO=[631] (cu- m)
3338 *%-----|-----|
3339 ADD HYD NHYDs um=[" KB- 14- S"], NHYDs to add=[" KB- 14- M" +" KB- 14- MN"]
3340 *%-----|-----|
3341 *%-----|-----|
3342 CONTINUOUS STANDHYD NHYD=[" KB- 16_2"], DT=[1] mi n, AREA=[3. 42] (ha), XI MP=[0. 71],
TI MP=[0. 71], DWF=[0] (cms), LOSS=[1]:
3343 Horton: Fo=[76. 20] (mm/ hr), Fc=[13. 20] (mm/ hr), DCAY=[4. 14] (/ hr),
F=[0. 00] (mm),
3344 Pervious areas: IAper=[4. 67] (mm), SLPP=[2. 0] (%), LGP=[40] (m),

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3345 MNP=[ 0.250], SCP=[ 0]( mi n),
Impervious areas: I A i mp=[ 0.157]( mm), SLPI=[ 0.3]( %),
3346 LGI=[ 150.997]( m), MNI=[ 0.013], SCI=[ 0]( mi n),
3347 Continuous simulation parameters:
I a RE C per=[ 4]( hr s), I a RE C i mp=[ 4]( hr s), I n t e r E v e n t T i m e=[ 12]( hr s),
END=- 1
3348 *%-----|-----|
3349 ADD HYD NHYDs um=[ "KB- P2"], NHYDs t o
add=[ "KB- Pond1"+"KB- 07- S"+"KB- 08- S"+"KB- 09"+"KB- 10_1"+"KB- 10_2"+"KB- 12- S"+"KB- 13- S"+"KB- 1
4- S"+"KB- 16_2"]
3350 *%-----|-----|
3351 ROUTE RESERVOIR NHYDout =[ "KB- P2R"], NHYDi n=[ "KB- P2"],
3352 RDT=[ 1]( mi n),
3353 TABLE of ( OUTFLOW STORAGE ) values
3354 ( cms ) - ( ha- m)
3355 [ 0.0 , 0.0 ]
3356 [ 0.053, 0.005]
3357 [ 0.132, 0.009]
3358 [ 0.269, 0.014]
3359 [ 0.455, 0.023]
3360 [ 0.699, 0.037]
3361 [ 0.947, 0.056]
3362 [ 1.853, 0.09]
3363 [ 2.712, 0.146]
3364 [ 6.626, 0.287]
3365 [ 11.228, 0.515]
3366 [ 14.885, 0.738]
3367 [ 16.473, 0.893]
3368 [ 17.311, 0.998]
3369 [ 17.633, 1.063]
3370 [ 17.634, 1.112]
3371 [ -1 , -1 ] (max t went y pt s)
3372 NHYDovf=[ "KB- P2ovf"]
3373 *%-----|-----|
3374 ADD HYD NHYDs um=[ "KB- Pond2"], NHYDs t o add=[ "KB- P2R"+"KB- P2ovf"]
3375 *%-----|-----|
3376 SAVE HYD NHYD=[ "KB- Pond2"], # OF PCYCLES=[ -1], I CASEs h=[ 1]
3377 HYD_COMMENT=[ "Total Flows at KB second pond"]
3378 *%-----|-----|
3379 CONTINUOUS STANDHYD NHYD=[ "KB- 16_1"], DT=[ 1] mi n, AREA=[ 2.8]( ha), XI MP=[ 0.75],
TI MP=[ 0.75], DWF=[ 0]( cms), LOSS=[ 1]:
3380 Horton: Fo=[ 76.20]( mm/ hr), Fc=[ 13.20]( mm/ hr), DCAY=[ 4.14]( / hr),
F=[ 0.00]( mm),
3381 Pervious areas: I A p e r=[ 4.67]( mm), SLPP=[ 2.0]( %), LGP=[ 40]( m),
MNP=[ 0.250], SCP=[ 0]( mi n),
3382 Impervious areas: I A i mp=[ 0.157]( mm), SLPI=[ 0.3]( %),
LGI=[ 136.626]( m), MNI=[ 0.013], SCI=[ 0]( mi n),
3383 Continuous simulation parameters:
3384 I a RE C per=[ 4]( hr s), I a RE C i mp=[ 4]( hr s), I n t e r E v e n t T i m e=[ 12]( hr s),
END=- 1
3385 *%-----|-----|
3386 ADD HYD NHYDs um=[ "KB- P3"], NHYDs t o add=[ "KB- Pond2"+"KB- 16_1"]
3387 *%-----|-----|
3388 *%-----|-----|
3389 * One inflow node from pond 3 is added to the model (ROUTE RESERVOIR)
3390 * Another inflow node from right side of pond 3 is not added to the model
3391 ROUTE RESERVOIR NHYDout =[ "KB- P3R"], NHYDi n=[ "KB- P3"],
3392 RDT=[ 1]( mi n),
3393 TABLE of ( OUTFLOW STORAGE ) values
3394 ( cms ) - ( ha- m)
3395 [ 0.0 , 0.0 ]
3396 [ 0.051, 0.002]
3397 [ 0.048, 0.003]
3398 [ 0.057, 0.029]
3399 [ 0.089, 0.045]
3400 [ 0.133, 0.069]

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3401 [ 0.199, 0.106]
3402 [ 0.321, 0.172]
3403 [ 1.029, 0.306]
3404 [ 4.036, 0.527]
3405 [ 8.332, 0.761]
3406 [ 11.727, 0.941]
3407 [ 14.125, 1.067]
3408 [ 15.675, 1.149]
3409 [ 16.555, 1.196]
3410 [ 16.911, 1.214]
3411 [ -1 , -1 ] (max twenty pts)
3412 NHYDovf=["KB- P3ovf"]
3413 *%-----|-----|
3414 ADD HYD NHYDsum=["KB- Pond3"], NHYDs to add=["KB- P3R"+"KB- P3ovf"]
3415 *%-----|-----|
3416 SAVE HYD NHYD=["KB- Pond3"], # OF PCYCLES=[- 1], I CASEs h=[ 1]
3417 HYD_COMMENT=["Total Flows at KB third pond"]
3418 *%-----|-----|
3419 *#*****|*****|
3420 *# EXISTING / PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118080), SWM
3421 Modeling Approach, NOVATECH Report June, 2020)
3422 *# - TO FRASER-CLARKE DRAIN
3423 *#*****|*****|
3424 CONTINUOUS STANDHYD NHYD=["FC- 01"], DT=[1] min, AREA=[ 8.03](ha), XI MP=[ 0.47],
3425 TI MP=[ 0.47], DWF=[ 0](cms), LOSS=[ 1]:
3426 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3427 F=[ 0.00](mm),
3428 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3429 MNP=[ 0.250], SCP=[ 0](min),
3430 Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 1.0](%),
3431 LGI=[ 231.373](m), MNI=[ 0.013], SCI=[ 0](min),
3432 Continuous simulation parameters:
3433 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3434 END=- 1
3435 *%-----|-----|
3436 COMPUTE DUALHYD NHYDin=["FC- 01"], CINLET=[ 0.756](cms), NINLET=[ 1],
3437 Maj NHYD=["FC- 01- M"],
3438 MinNHYD=["FC- 01- MN"],
3439 TMSTO=[ 714](cu-m)
3440 *%-----|-----|
3441 ADD HYD NHYDsum=["FC- 01- S"], NHYDs to add=["FC- 01- M"+"FC- 01- MN"]
3442 *%-----|-----|
3443 CONTINUOUS STANDHYD NHYD=["FC- 02"], DT=[1] min, AREA=[ 16.05](ha), XI MP=[ 0.93],
3444 TI MP=[ 0.93], DWF=[ 0](cms), LOSS=[ 1]:
3445 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3446 F=[ 0.00](mm),
3447 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3448 MNP=[ 0.250], SCP=[ 0](min),
3449 Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 1.0](%),
3450 LGI=[ 327.109](m), MNI=[ 0.013], SCI=[ 0](min),
3451 Continuous simulation parameters:
3452 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3453 END=- 1
3454 *%-----|-----|
3455 COMPUTE DUALHYD NHYDin=["FC- 02"], CINLET=[ 1.159](cms), NINLET=[ 1],
3456 Maj NHYD=["FC- 02- M"],
3457 MinNHYD=["FC- 02- MN"],
3458 TMSTO=[ 2385](cu-m)
3459 *%-----|-----|
3460 ADD HYD NHYDsum=["FC- 02- S"], NHYDs to add=["FC- 02- M"+"FC- 02- MN"]
3461 *%-----|-----|
3462 CONTINUOUS STANDHYD NHYD=["FC- 03"], DT=[1] min, AREA=[ 7.37](ha), XI MP=[ 0.64],
3463 TI MP=[ 0.64], DWF=[ 0](cms), LOSS=[ 1]:
3464 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3465 F=[ 0.00](mm),
3466 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),

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3454 MNP=[ 0.250], SCP=[ 0](mi n),
Impervious areas: IAi mp=[ 1.57](mm), SLPI =[ 1.0](%),
LGI=[ 221.660](m), MNI =[ 0.013], SCI=[ 0](mi n),
3455 Continuous simulation parameters:
3456 IaREcper=[ 4](hrs), IaRECi mp=[ 4](hrs), InterEvent Time=[ 12](hrs),
END=- 1
3457 *%-----|-----|
3458 COMPUTE DUALHYD NHYDin=[ "FC-03"], CINLET=[ 0.358](cms), NINLET=[ 1],
3459 Maj NHYD=[ "FC-03-M"]
3460 MnNHYD=[ "FC-03-MN"]
3461 TMS TO=[ 1131](cu-m)
3462 *%-----|-----|
3463 ADD HYD NHYDsum=[ "FC-03-S"], NHYDs to add=[ "FC-03-M"+"FC-03-MN"]
3464 *%-----|-----|
3465 CONTINUOUS STANDHYD NHYD=[ "FC-04"], DT=[ 1]mi n, AREA=[ 12.87](ha), XI MP=[ 0.64],
TI MP=[ 0.64], DWF=[ 0](cms), LOSS=[ 1]:
3466 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
F=[ 0.00](mm),
3467 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
MNP=[ 0.250], SCP=[ 0](mi n),
3468 Impervious areas: IAi mp=[ 1.57](mm), SLPI =[ 1.0](%),
LGI=[ 292.916](m), MNI =[ 0.013], SCI=[ 0](mi n),
3469 Continuous simulation parameters:
3470 IaREcper=[ 4](hrs), IaRECi mp=[ 4](hrs), InterEvent Time=[ 12](hrs),
END=- 1
3471 *%-----|-----|
3472 COMPUTE DUALHYD NHYDin=[ "FC-04"], CINLET=[ 0.741](cms), NINLET=[ 1],
3473 Maj NHYD=[ "FC-04-M"]
3474 MnNHYD=[ "FC-04-MN"]
3475 TMS TO=[ 1794](cu-m)
3476 *%-----|-----|
3477 ADD HYD NHYDsum=[ "FC-04-S"], NHYDs to add=[ "FC-04-M"+"FC-04-MN"]
3478 *%-----|-----|
3479 *#*****
3480 *# PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118080), SWM Modeling
Approach, NOVATECH Report June, 2020)
3481 *# - TO JOCK RIVER
3482 *#*****
3483 CONTINUOUS STANDHYD NHYD=[ "JR-01"], DT=[ 1]mi n, AREA=[ 8.24](ha), XI MP=[ 0.64],
TI MP=[ 0.64], DWF=[ 0](cms), LOSS=[ 1]:
3484 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
F=[ 0.00](mm),
3485 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
MNP=[ 0.250], SCP=[ 0](mi n),
3486 Impervious areas: IAi mp=[ 1.57](mm), SLPI =[ 1.0](%),
LGI=[ 234.379](m), MNI =[ 0.013], SCI=[ 0](mi n),
3487 Continuous simulation parameters:
3488 IaREcper=[ 4](hrs), IaRECi mp=[ 4](hrs), InterEvent Time=[ 12](hrs),
END=- 1
3489 *%-----|-----|
3490 COMPUTE DUALHYD NHYDin=[ "JR-01"], CINLET=[ 0.563](cms), NINLET=[ 1],
3491 Maj NHYD=[ "JR-01-M"]
3492 MnNHYD=[ "JR-01-MN"]
3493 TMS TO=[ 1040](cu-m)
3494 *%-----|-----|
3495 ADD HYD NHYDsum=[ "JR-01-S"], NHYDs to add=[ "JR-01-M"+"JR-01-MN"]
3496 *%-----|-----|
3497 CONTINUOUS STANDHYD NHYD=[ "JR-02"], DT=[ 1]mi n, AREA=[ 1.59](ha), XI MP=[ 0.64],
TI MP=[ 0.64], DWF=[ 0](cms), LOSS=[ 1]:
3498 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
F=[ 0.00](mm),
3499 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
MNP=[ 0.250], SCP=[ 0](mi n),
3500 Impervious areas: IAi mp=[ 1.57](mm), SLPI =[ 1.0](%),
LGI=[ 102.956](m), MNI =[ 0.013], SCI=[ 0](mi n),
3501 Continuous simulation parameters:

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3502 IaRECper=[ 4]( hrs), IaRECI mp=[ 4]( hrs), InterEventTime=[ 12]( hrs),
END=- 1
3503 *%-----|-----|
3504 COMPUTE DUALHYD NHYDin=["JR-02"], CI NLET=[ 0.153]( cms), NI NLET=[ 1],
3505 Mj NHYD=["JR-02-M"]
3506 MnNHYD=["JR-02-MN"]
3507 TM STO=[ 153]( cu- m)
3508 *%-----|-----|
3509 ADD HYD NHYDsum=["JR-02-S"], NHYDs to add=["JR-02-M"+"JR-02-MN"]
3510 *%-----|-----|
3511 *#*****|*****|
3512 *# Catchment FRASER
3513 *# - To Fraser-Clarke drain (north of the Jock)
3514 *# - Developed land with assumed 43% imp.
3515 *# - 2020-12-17 Change Fraser area to be 35.1 as measured from QGIS
3516 *# - 2020-12-17 All Fraser is undeveloped (Nashyd)
3517 *#*****|*****|
3518 CONTINUOUS NASHYD NHYD=["FRASER-DRN"], DT=[ 1] min, AREA=[ 13.65]( ha),
3519 DWF=[ 0]( cms), CN C=[ 77], IA=[ 4.67]( mm),
3520 N=[ 3], TP=[ 0.4258] hrs,
3521 Continuous simulation parameters:
3522 IaRECper=[ 4]( hrs),
3523 SMN=[ -1]( mm), SMAX=[ -1]( mm), SK=[ 0.010]/( mm),
3524 InterEventTime=[ 12]( hrs)
3525 Baseflow simulation parameters:
3526 BaseFlowOption=[ 1],
3527 InitGWResVol=[ 50]( mm), GWResK=[ 0.96]( mm/ day/ mm)
3528 VHydCond=[ 0.055]( mm/ hr), END=- 1
3529 *
3530 CONTINUOUS STANDHYD NHYD=["FRASER-D"], DT=[ 1] min, AREA=[ 21.61]( ha),
3531 XI MP=[ 0.585], TI MP=[ 0.585], DWF=[ 0]( cms), LOSS=[ 2],
3532 SCS curve number CN=[ 80],
3533 Pervious surfaces: IAper=[ 4.67]( mm), SLPP=[ 1]( %),
3534 LGP=[ 40]( m), MNP=[ 0.25], SCP=[ 0]( min),
3535 Impervious surfaces: IAimp=[ 1.57]( mm), SLPI=[ 1]( %),
3536 LGI=[ 379.561]( m), MNI=[ 0.013], SCI=[ 0]( min),
3537 Continuous simulation parameters:
3538 IaRECper=[ 4]( hrs), IaRECI mp=[ 4]( hrs),
3539 SMN=[ -1]( mm), SMAX=[ -1]( mm), SK=[ 0.010]/( mm),
3540 InterEventTime=[ 18]( hrs), END=- 1
3541 *%-----|-----|
3542 COMPUTE DUALHYD NHYDin=["FRASER-D"], CI NLET=[ 2.281]( cms), NI NLET=[ 1],
3543 Mj NHYD=["FRASER-J"]
3544 MnNHYD=["FRASER-N"]
3545 TM STO=[ 9999999]( cu- m)
3546 *%-----|-----|
3547 ADD HYD NHYDsum=["FRASER-S"], NHYDs to add=["FRASER-J"+"FRASER-N"]
3548 *%-----|-----|
3549 *ROUTE RESERVOIR NHYDout=["MS_P20"], NHYDin=["FRASER"],
3550 * RDT=[ 1]( min),
3551 * TABLE of ( OUTFLOW STORAGE ) values
3552 * ( cms ) - ( ha- m)
3553 * [ 0.0 , 0.0 ]
3554 * [ 0.04 , 0.36 ]
3555 * [ -1 , -1 ] (max twenty pts)
3556 * NHYDovf=["P20-OVF"]
3557 *%-----|-----|
3558 ADD HYD NHYDsum=["4241"], NHYDs to
add=["KB-Pond3"+"S-1-B"+"FRASER-DRN"+"FRASER-S"+"N_KB"+"FC-01-S"+"FC-02-S"+"FC-03-S"]
3559 *%-----|-----|
3560 SAVE HYD NHYD=["4241"], # OF PCYCLES=[ -1], ICASEsh=[ 1]
3561 HYD_COMMENT=["Total Flows at Ken-Burnett Outlet"]
3562 *%-----|-----|
3563 *# Hydrograph from Node Ken-Burnett to station 3633
3564 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4241
3565 *#

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3566 ROUTE CHANNEL      NHYDout =[" 4241- out "], NHYDin=[" 4241"],   RDT=[ 1](mi n),
3567                   CHLGTH=[ 294](m),   CHSLOPE=[ 0.1088](%), FPSLOPE=[ 0.1088](%),
3568                   SECNUM=[ 1.0],       NSEG=[ 3]
3569                   ( SEGROUGH, SEGDI ST (m))=[ 0.05, -20.12
3570                                     -0.035, 45.26
3571                                     0.05, 403.84] NSEG times
3572                   ( DI STANCE (m), ELEVATI ON (m))=[ ]
3573                   [-909.72, 95 ]
3574                   [-907.09, 94.5 ]
3575                   [-904.65, 94 ]
3576                   [-902.26, 93.5 ]
3577                   [-44.51, 91.5 ]
3578                   [-25.1, 91.5 ]
3579                   [-20.98, 91 ]
3580                   [-20.61, 90.5 ]
3581                   [-20.12, 90 ]
3582                   [-6.13, 87.26 ]
3583                   [17.51, 86.56 ]
3584                   [31.37, 87.2 ]
3585                   [45.26, 90 ]
3586                   [50.41, 90.5 ]
3587                   [63.06, 91 ]
3588                   [134.5, 91.5 ]
3589                   [190.63, 92 ]
3590                   [251.98, 92.5 ]
3591                   [321.32, 93.5 ]
3592                   [403.84, 95 ]
3593 *%-----|-----|
3594 ADD HYD           NHYDsum=["SN_KB"], NHYDs to
add=[" 4241- out "+"FC-04- S"+"JR-01- S"+"JR-02- S"]
3595 *%-----|-----|
3596 SAVE HYD         NHYD=["SN_KB"], # OF PCYCLES=[-1], ICASEsh=[1]
3597 HYD_COMMENT=["Total Flows before Station 3633]
3598 *%-----|-----|
3599 *# Hydrograph from Station 3633 to Node Todd
3600 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 3633
3601 *# JFSA 2021-02-26 change the channel length (at station 3633) from 650m to 608m and
change the slope from 0.0498% to 0.24671% That is because of adding station 4241
between station 4534 and station 3633
*#
3602 ROUTE CHANNEL      NHYDout =["N_TO"], NHYDin=["SN_KB"],   RDT=[ 1](mi n),
3603                   CHLGTH=[ 608](m),   CHSLOPE=[ 0.24671](%), FPSLOPE=[ 0.24671](%),
3604                   SECNUM=[ 1.0],       NSEG=[ 3]
3605                   ( SEGROUGH, SEGDI ST (m))=[ 0.05, -23.74
3606                                     -0.035, 23.74
3607                                     0.05, 26.50] NSEG times
3608                   ( DI STANCE (m), ELEVATI ON (m))=[ ]
3609                   [-29.24, 91.0
3610                   [-27.41, 90.5
3611                   [-25.64, 90
3612                   [-23.74, 89.5
3613                   [-22, 89.26
3614                   [-20, 88.51
3615                   [-19, 88.32
3616                   [-15, 88.1
3617                   [-10, 88.11
3618                   [-5, 88.17
3619                   0, 88.27
3620                   5, 88.19
3621                   10, 88.06
3622                   15, 88.48
3623                   16, 88.7
3624                   23.74, 89.5
3625                   24.68, 90
3626                   25.57, 90.5
3627                   26.50, 91.0

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3629 * [-29.24, 91]
3630 * [-27.41, 90.5]
3631 * [-25.64, 90]
3632 * [-23.74, 89.5]
3633 * [-22, 89.26]
3634 * [-20, 88.51]
3635 * [-19, 88.32]
3636 * [-15, 88.1]
3637 * [-10, 88.11]
3638 * [-5, 88.17]
3639 * [0, 88.27]
3640 * [5, 88.19]
3641 * [10, 88.06]
3642 * [15, 88.48]
3643 * [16, 88.7]
3644 * [23.74, 89.5]
3645 * [24.68, 90]
3646 * [25.57, 90.5]
3647 *%-----|-----|
3648 *#*****|*****|
3649 *# Catchment Greenbank
3650 *# - To Greenbank Drain (south of the Jock)
3651 *# - JFSA 2021-01-18 add Greenbank pond as per JFSA, P598(06)-15, June 2016
3652 *# - JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GIS measurements
3653 *#*****|*****|
3654 CONTINUOUS STANDHYD NHYD=["Greenbank"], DT=[1] min, AREA=[36.6] (ha),
3655 XI MP=[0.639], TI MP=[0.682], DWF=[0] (cms), LOSS=[2],
3656 SCS curve number CN=[77],
3657 Pervious surfaces: I A per=[4.67] (mm), SLPP=[1] (%),
3658 LGP=[40] (m), MNP=[0.25], SCP=[0] (min),
3659 Impervious surfaces: I A i mp=[1.57] (mm), SLPI=[1] (%),
3660 LGI=[493.96] (m), MNI=[0.013], SCI=[0] (min),
3661 Continuous simulation parameters:
3662 I a REC per=[4] (hrs), I a REC i mp=[4] (hrs),
3663 S M N=[-1] (mm), S M A X=[-1] (mm), S K=[0.010] / (mm),
3664 I n t e r E v e n t T i m e=[18] (hrs), E N D=-1
3665 *%-----|-----|
3666 ROUTE RESERVOIR NHYDout=["GreenB_MN"], NHYDin=["Greenbank"],
3667 RDT=[1] (min),
3668 TABLE of ( OUTFLOW STORAGE ) values
3669 ( cms ) - ( ha-m )
3670 [ 0.0 , 0.0 ]
3671 [ 0.033 , 0.084 ]
3672 [ 0.039 , 0.201 ]
3673 [ 0.113 , 0.292 ]
3674 [ 0.237 , 0.386 ]
3675 [ 0.382 , 0.484 ]
3676 [ 0.539 , 0.585 ]
3677 [ 0.7 , 0.692 ]
3678 [ 0.86 , 0.804 ]
3679 [ 4.684 , 0.922 ]
3680 [ 11.539 , 1.052 ]
3681 [ 20.867 , 1.168 ]
3682 [ 103.616 , 1.974 ]
3683 [ -1 , -1 ] (max twenty pts)
3684 NHYDovf=["GreenB_M"],
3685 *%-----|-----|
3686 *%-----|-----|
3687 ADD HYD NHYDsum=["GreenB"], NHYDs to add=["N_TO"+"GreenB_M"+"GreenB_MN"]
3688 *%-----|-----|
3689 SAVE HYD NHYD=["GreenB"], # OF PCYCLES=[-1], I CASEs h=[1]
3690 HYD_COMMENT=["Total Flows at Greenbank Drain"]
3691 *%-----|-----|
3692 *#*****|*****|
3693 *# Catchment TODD
3694 *# - To Todd Drain (south of the Jock)

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3695 *# - Subdivision with 43% imp. as per Barrhaven South M5S
3696 *# - 2020-11-30 increase imp. based on P598(04)-11
3697 *# - 2020-11-30 update TODD Tributary Drainage Area to = 146.015 ha based on
P598(04)-11
3698 *# - 2020-11-30 split TODD Drainage Area to MAJOR, MINOR, POND and ALL
3699 *#*****
3700 *# - JFSA 2021-01-19 add "TODD_MN1" as part of Clarke("W_CLAR_M") and remove it
from Todd
3701 *CONTINUOUS STANDHYD NHYD=["TODD_MN1"], DT=[1] min, AREA=[1.772](ha),
3702 * XI MP=[0.53], TI MP=[0.57], DWF=[0](cms), LOSS=[2],
3703 * SCS curve number CN=[77],
3704 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3705 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3706 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3707 * LGI=[108.689](m), MNI=[0.013], SCI=[0](min),
3708 * Continuous simulation parameters:
3709 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
3710 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3711 * InterEventTime=[18](hrs), END=-1
3712 *%-----|-----
3713 CONTINUOUS STANDHYD NHYD=["TODD_MN2"], DT=[1] min, AREA=[2.1](ha),
3714 * XI MP=[0.53], TI MP=[0.57], DWF=[0](cms), LOSS=[2],
3715 * SCS curve number CN=[77],
3716 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3717 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3718 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3719 * LGI=[118.322](m), MNI=[0.013], SCI=[0](min),
3720 * Continuous simulation parameters:
3721 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
3722 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3723 * InterEventTime=[18](hrs), END=-1
3724 *%-----|-----
3725 CONTINUOUS STANDHYD NHYD=["TODD_MN3"], DT=[1] min, AREA=[0.117](ha),
3726 * XI MP=[0.53], TI MP=[0.57], DWF=[0](cms), LOSS=[2],
3727 * SCS curve number CN=[77],
3728 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3729 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3730 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3731 * LGI=[27.928](m), MNI=[0.013], SCI=[0](min),
3732 * Continuous simulation parameters:
3733 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
3734 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3735 * InterEventTime=[18](hrs), END=-1
3736 *%-----|-----
3737 CONTINUOUS STANDHYD NHYD=["TODD_M1"], DT=[1] min, AREA=[30.230](ha),
3738 * XI MP=[0.52], TI MP=[0.64], DWF=[0](cms), LOSS=[2],
3739 * SCS curve number CN=[77],
3740 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3741 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3742 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3743 * LGI=[448.925](m), MNI=[0.013], SCI=[0](min),
3744 * Continuous simulation parameters:
3745 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
3746 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3747 * InterEventTime=[18](hrs), END=-1
3748 *%-----|-----
3749 * -JFSA 2021-01-19 update "TODD_ALL" area from 108.741 ha to 112.908 ha based on
GIS measurements (148.41-30.23-0.117-2.1-3.055=112.908 ha)
3750 CONTINUOUS STANDHYD NHYD=["TODD_ALL"], DT=[1] min, AREA=[112.908](ha),
3751 * XI MP=[0.52], TI MP=[0.57], DWF=[0](cms), LOSS=[2],
3752 * SCS curve number CN=[77],
3753 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3754 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3755 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3756 * LGI=[867.594](m), MNI=[0.013], SCI=[0](min),
3757 * Continuous simulation parameters:

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3758 IaREcper=[ 4](hrs), IaREcImp=[ 4](hrs),
3759 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
3760 InterEventTime=[ 18](hrs), END=- 1
3761 *%-----|-----
3762 CONTINUOUS STANDHYD NHYD=["TODD_P"], DT=[ 1]min, AREA=[ 3.055](ha),
3763 XI MP=[ 0.63], TI MP=[ 0.63], DWF=[ 0](cms), LOSS=[ 2],
3764 SCS curve number CN=[ 77],
3765 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
3766 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
3767 Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
3768 LGI=[ 142.712](m), MNI=[ 0.013], SCI=[ 0](min),
3769 Continuous simulation parameters:
3770 IaREcper=[ 4](hrs), IaREcImp=[ 4](hrs),
3771 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
3772 InterEventTime=[ 18](hrs), END=- 1
3773 *%-----|-----
3774 *%-----|-----
3775 * -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"
and its parameters remain the same.
3776 *CONTINUOUS STANDHYD NHYD=["TODD_DEVL"], DT=[ 1]min, AREA=[ 15.87](ha),
3777 * XI MP=[ 0.63], TI MP=[ 0.63], DWF=[ 0](cms), LOSS=[ 2],
3778 * SCS curve number CN=[ 77],
3779 * Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
3780 * LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
3781 * Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
3782 * LGI=[ 325.27](m), MNI=[ 0.013], SCI=[ 0](min),
3783 * Continuous simulation parameters:
3784 * IaREcper=[ 4](hrs), IaREcImp=[ 4](hrs),
3785 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
3786 * InterEventTime=[ 18](hrs), END=- 1
3787 *%-----|-----
3788 * -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
is called "corr2" and its parameters remain the same.
3789 *CONTINUOUS NASHYD NHYD=["TODD_UnD"], DT=[ 1]min, AREA=[ 12.47](ha),
3790 * DWF=[ 0](cms), CN C=[ 77], IA=[ 4.67](mm),
3791 * N=[ 3], TP=[ 1.10]hrs,
3792 * Continuous simulation parameters:
3793 * IaREcper=[ 4](hrs),
3794 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
3795 * InterEventTime=[ 12](hrs)
3796 * Baseflow simulation parameters:
3797 * BaseFlowOption=[ 1],
3798 * InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
3799 * VHydCond=[ 0.055](mm/hr), END=- 1
3800 *%-----|-----
3801 *# 5- Year + 12% Capture
3802 *COMPUTE DUALHYD NHYDin=["TODD_Mj"], CINLET=[ 3.314](cms), NINLET=[ 1],
3803 * MjNHYD=["TODD_Mj"]
3804 * MnNHYD=["TODD_Mn"]
3805 * TMSTO=[ 0.1](cu-m)
3806 ROUTE RESERVOIR NHYDout=["TODD_Mn"], NHYDin=["TODD_Mj"],
3807 RDT=[ 1](min),
3808 TABLE of ( OUTFLOW STORAGE ) values
3809 ( cms ) - ( ha-m)
3810 [ 0.0 , 0.0 ]
3811 [ 3.314 , 0.0001 ]
3812 [ -1 , -1 ] (max twenty pts)
3813 NHYDovf=["TODD_Mj"],
3814 *%-----|-----
3815 *# 5- Year + 12% Capture
3816 *COMPUTE DUALHYD NHYDin=["TODD_MN1"], CINLET=[ 0.227](cms), NINLET=[ 1],
3817 * MjNHYD=["TODD_MN1j"]
3818 * MnNHYD=["TODD_MN1n"]
3819 * TMSTO=[ 0.1](cu-m)
3820 *ROUTE RESERVOIR NHYDout=["TODD_MN1n"], NHYDin=["TODD_MN1"],

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3821 *          RDT=[ 1](mi n),
3822 *          TABLE of ( OUTFLOW STORAGE ) values
3823 *                ( cms ) - ( ha- m)
3824 *                [ 0.0 , 0.0 ]
3825 *                [ 0.227 , 0.0001 ]
3826 *                [ -1 , -1 ] (max t went y pts)
3827 *          NHYDovf=[ "TODD_MN1j" ] ,
3828 *%-----|-----|
3829 *COMPUTE DUALHYD  NHYDi n=[ "TODD_MN2" ], CI NLET=[ 0.268]( cms ), NI NLET=[ 1],
3830 *                Mj NHYD=[ "TODD_MN2j" ]
3831 *                MnNHYD=[ "TODD_MN2n" ]
3832 *                TM STO=[ 0.1]( cu- m)
3833 ROUTE RESERVOIR NHYDout =[ "TODD_MN2n" ] , NHYDi n=[ "TODD_MN2" ] ,
3834 RDT=[ 1](mi n),
3835          TABLE of ( OUTFLOW STORAGE ) values
3836                ( cms ) - ( ha- m)
3837                [ 0.0 , 0.0 ]
3838                [ 0.268 , 0.0001 ]
3839                [ -1 , -1 ] (max t went y pts)
3840          NHYDovf=[ "TODD_MN2j" ] ,
3841 *%-----|-----|
3842 *COMPUTE DUALHYD  NHYDi n=[ "TODD_MN3" ], CI NLET=[ 0.016]( cms ), NI NLET=[ 1],
3843 *                Mj NHYD=[ "TODD_MN3j" ]
3844 *                MnNHYD=[ "TODD_MN3n" ]
3845 *                TM STO=[ 0.1]( cu- m)
3846 ROUTE RESERVOIR NHYDout =[ "TODD_MN3n" ] , NHYDi n=[ "TODD_MN3" ] ,
3847 RDT=[ 1](mi n),
3848          TABLE of ( OUTFLOW STORAGE ) values
3849                ( cms ) - ( ha- m)
3850                [ 0.0 , 0.0 ]
3851                [ 0.016 , 0.0001 ]
3852                [ -1 , -1 ] (max t went y pts)
3853          NHYDovf=[ "TODD_MN3j" ] ,
3854 *%-----|-----|
3855 *          -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
major system from A2 can be added to Todd
3856 CONTINUOUS STANDHYD NHYD=[ "A2" ], DT=[ 1]mi n, AREA=[ 25.5]( ha),
3857 XI MP=[ 0.42], TI MP=[ 0.52], DWF=[ 0]( cms ), LOSS=[ 2],
3858 SCS curve number CN=[ 75],
3859 Pervious surfaces: I Aper=[ 4.67]( mm), SLPP=[ 1]( %),
3860                LGP=[ 40]( m), MNP=[ 0.25], SCP=[ 0]( mi n),
3861 Impervious surfaces: I Ai mp=[ 1.57]( mm), SLPI =[ 1]( %),
3862                LGI =[ 566]( m), MNI =[ 0.013], SCI =[ 0]( mi n),
3863 Continuous simulation parameters:
3864 I aRECper=[ 4]( hrs), I aRECI mp=[ 4]( hrs),
3865 SM N=[ -1]( mm), SMAX=[ -1]( mm), SK=[ 0.010]/( mm),
3866 Inter Event Ti me=[ 18]( hrs), END=- 1
3867 *%-----|-----|
3868 COMPUTE DUALHYD  NHYDi n=[ "A2" ], CI NLET=[ 1.818]( cms ), NI NLET=[ 1],
3869 Mj NHYD=[ "A2- M" ]
3870 MnNHYD=[ "A2- MN" ]
3871 TM STO=[ 924]( cu- m)
3872 *%-----|-----|
3873 ADD HYD          NHYDs um=[ "TODD" ], NHYDs to
add=[ "TODD_MN2n"+"TODD_MN3n"+"TODD_Mj"+"TODD_P"+"TODD_ALL"+"W_CLAR_Mn" ]
3874 *%-----|-----|
3875 SAVE HYD        NHYD=[ "TODD" ], # OF PCYCLES=[ -1], I CASEs h=[ 1]
3876 HYD_COMMENT=[ "Total Flows at Todd Drain" ]
3877 *%-----|-----|
3878 *#*****|*****|
3879 *# Todd Pond 3
3880 *# - Rating curve obtained from Barrhaven South MS modeling
3881 *# - stantec 2007, Tributary Drainage Area to MS Pond 3 = 193 ha
3882 *#*****|*****|
3883 ROUTE RESERVOIR NHYDout =[ "MS_P3" ], NHYDi n=[ "TODD" ],
3884 RDT=[ 1](mi n),

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3885          TABLE of ( OUTFLOW STORAGE ) values
3886          ( cms ) - ( ha - m )
3887          [ 0.0 , 0.0 ]
3888          [ 0.014 , 0.155 ]
3889          [ 0.048 , 0.394 ]
3890          [ 0.061 , 0.56 ]
3891          [ 0.08 , 0.909 ]
3892          [ 0.088 , 1.089 ]
3893          [ 0.109 , 1.652 ]
3894          [ 0.118 , 1.952 ]
3895          [ 0.122 , 2.099 ]
3896          [ 1.972 , 2.269 ]
3897          [ 9.135 , 2.598 ]
3898          [ 15.608 , 2.826 ]
3899          [ 19.256 , 2.942 ]
3900          [ 27.282 , 3.181 ]
3901          [ 40.957 , 3.55 ]
3902          [ 56.372 , 3.929 ]
3903          [ 73.349 , 4.317 ]
3904          [ 85.469 , 4.579 ]
3905          [ 104.771 , 4.977 ]
3906          [ -1 , -1 ] (max twenty pts)
3907          NHYDovf=[ "P3- OVF" ]
3908          *%-----|-----|
3909          ADD HYD          NHYDs um=[ "SN_TO" ], NHYDs to
add=[ "GreenB"+"MS_P3"+"P3- OVF"+"TODD_MN2j"+"A2- M" ]
3910          *%-----|-----|
3911          SAVE HYD          NHYD=[ "SN_TO" ], # OF PCYCLES=[ -1 ], I CASEs h=[ 1 ]
3912          HYD_COMMENT=[ "Total Flows at Todd Drain" ]
3913          *%-----|-----|
3914          *#
3915          *# Hydrograph from Todd Drain routed to Corrigan Drain
3916          *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
3917          *# 2021-02-19 Change the slope from 0.033 % (as per Stantec Report 2007) to 0.05 % so
the model will be more stable and give reasonable results. It is justifiable as ROUTE
CHANNELs aren't well suited to really flat slopes.
3918          *
3919          ROUTE CHANNEL          NHYDout = [ "N_TO" ] , NHYDin = [ "SN_TO" ] ,
3920          RDT=[ 1 ] ( min ),
3921          CHLGTH=[ 280 ] ( m ), CHSLOPE=[ 0.05 ] ( % ),
3922          FPSLOPE=[ 0.05 ] ( % ),
3923          SECNUM=[ 1.0 ] , NSEG=[ 3 ]
3924          ( SEGROUGH, SEGDI ST ( m ) ) =
3925          [ 0.075, -17.72
3926          -0.045, 17.72
3927          0.075, 80.62 ] NSEG times
3928          ( DI STANCE ( m ), ELEVATI ON ( m ) ) =
3929          [ -83.32, 90.00 ]
3930          [ -81.36, 89.50 ]
3931          [ -79.12, 89.00 ]
3932          [ -76.13, 88.50 ]
3933          [ -20.46, 88.00 ]
3934          [ -19.36, 87.50 ]
3935          [ -18.51, 87.00 ]
3936          [ -17.72, 86.50 ]
3937          [ -11.95, 85.24 ]
3938          [ -0.11, 85.12 ]
3939          [ 11.49, 85.20 ]
3940          [ 17.72, 86.50 ]
3941          [ 19.74, 87.00 ]
3942          [ 21.22, 87.50 ]
3943          [ 22.68, 88.00 ]
3944          [ 24.28, 88.50 ]
3945          [ 26.79, 89.00 ]
3946          [ 71.98, 90.00 ]
3947          [ 80.62, 90.50 ]

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3948 *%-----|-----|
3949 SAVE HYD      NHYD=["N_TO"], # OF PCYCLES=[-1], ICASEsh=[1]
3950              HYD_COMMENT=["Total inflows at Station 2462"]
3951 *%-----|-----|
3952 *#*****|-----|
3953 *#    Catchment CORRIG
3954 *#    - To Corrigan Drain (south of the Jock)
3955 *#    - Primarily Developed (medium density)
3956 *#    - JFSA JAN 2021, add Corrigan subcatchments as per IBI, July 2008
3957 *#*****|-----|
3958 *ROUTE RESERVOIR  NHYDout=["MS_P1"], NHYDin=["CORRIG"],
3959 *              RDT=[1](min),
3960 *              TABLE of ( OUTFLOW STORAGE ) values
3961 *              (cms) - (ha-m)
3962 *              [ 0.0 , 0.0 ]
3963 *              [ 0.06 , 0.58]
3964 *              [ -1 , -1 ] (max twenty pts)
3965 *              NHYDovf=["P1-OVF"]
3966 *%-----|-----|
3967 *ADD HYD      NHYDsum=["SN_CO"], NHYDs to add=["N_TO"+"P1-OVF"+"MS_P1"]
3968 *%-----|-----|
3969 *SAVE HYD      NHYD=["SN_CO"], # OF PCYCLES=[-1], ICASEsh=[1]
3970 *              HYD_COMMENT=["Total Flows at Corrigan Drain"]
3971 *%-----|-----|
3972 *    -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"
and its parameters remain the same.

3973 CONTINUOUS STANDHYD NHYD=["corr1"], DT=[1]min, AREA=[15.87](ha),
3974 XI MP=[0.63], TI MP=[0.63], DWF=[0](cms), LOSS=[2],
3975 SCS curve number CN=[77],
3976 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3977 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3978 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3979 LGL=[325.27](m), MNI=[0.013], SCI=[0](min),
3980 Continuous simulation parameters:
3981 IARECper=[4](hrs), IARECimp=[4](hrs),
3982 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3983 InterEventTime=[18](hrs), END=-1
3984 *%-----|-----|
3985 *    -JFSA 2021-02-23 add DUALHYD for "corr1". "corr1" DUALHYD Parameters are the
same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to "corr1".
3986 *    At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for
Al-Corrig
3987 COMPUTE DUALHYD NHYDin=["corr1"], CNLET=[1.818](cms), NI NLET=[1],
3988 Maj NHYD=["corr1-M"]
3989 MnNHYD=["corr1-MN"]
3990 TM STO=[924](cu-m)
3991 *%-----|-----|
3992 *    -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
is called "corr2" and its parameters remain the same.

3993 CONTINUOUS NASHYD NHYD=["corr2"], DT=[1]min, AREA=[12.47](ha),
3994 DWF=[0](cms), CN C=[77], IA=[4.67](mm),
3995 N=[3], TP=[1.10]hrs,
3996 Continuous simulation parameters:
3997 IARECper=[4](hrs),
3998 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3999 InterEventTime=[12](hrs)
4000 Baseflow simulation parameters:
4001 BaseFlowOption=[1],
4002 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4003 VHydCond=[0.055](mm/hr), END=-1
4004 *%-----|-----|
4005 *    -JFSA 2021-01-19 change Al-Corrig to be developed as per geottawa website and
apply the parameters of A2, the nearest sub-catchment to Al-Corrig, LGI is calculated
based on Al-Corrig area
4006 *    -JFSA 2021-01-19 update all Corrigan areas based on GIS measurements, and keep

```

LGI as it is from Corrigan Report, IBI Group, 2008 because LGI calculated is less than LGI from the Corrigan Report

```
4007 CONTINUOUS STANDHYD NHYD=["Al-Corrig"], DT=[1] min, AREA=[15.75](ha),
4008 XI MP=[0.42], TI MP=[0.52], DWF=[0](cms), LOSS=[2],
4009 SCS curve number CN=[75],
4010 Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4011 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4012 Impervious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
4013 LGI=[324.037](m), MNI=[0.013], SCI=[0](min),
4014 Continuous simulation parameters:
4015 I a REC per=[4](hrs), I a REC i mp=[4](hrs),
4016 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4017 Inter Event Time=[18](hrs), END=-1
4018 *
4019 * -JFSA 2021-01-25 add DUALHYD for Al-Corrig. Al-Corrig DUALHYD Parameters are the
same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to Al-Corrig.
4020 * At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for
Al-Corrig
4021 COMPUTE DUALHYD NHYD i n=["Al-Corrig"], CI NLET=[1.818](cms), NI NLET=[1],
4022 M a j NHYD=["Al-M"]
4023 M n NHYD=["Al-MN"]
4024 T M I STO=[924](cu-m)
4025 *%-----|-----|
4026 *CONTINUOUS NASHYD NHYD=["Al-Corrig"], DT=[1] min, AREA=[15.75](ha),
4027 * DWF=[0](cms), CN C=[66], I A=[2.5](mm),
4028 * N=[3.0], TP=[0.36] hrs,
4029 * Continuous simulation parameters:
4030 * I a REC per=[4](hrs),
4031 * SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4032 * Inter Event Time=[12](hrs)
4033 * Baseflow simulation parameters:
4034 * BaseFl owOpt ion=[1],
4035 * I n i t GWR es Vol =[50](mm), GWR es K=[0.96](mm/day/mm)
4036 * VHydCond=[0.055](mm/hr), END=-1
4037 *%-----|-----|
4038 CONTINUOUS NASHYD NHYD=["B1"], DT=[1] min, AREA=[2.77](ha),
4039 DWF=[0](cms), CN C=[56], I A=[2.5](mm),
4040 N=[3.0], TP=[0.23] hrs,
4041 Continuous simulation parameters:
4042 I a REC per=[4](hrs),
4043 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4044 Inter Event Time=[12](hrs)
4045 Baseflow simulation parameters:
4046 BaseFl owOpt ion=[1],
4047 I n i t GWR es Vol =[50](mm), GWR es K=[0.96](mm/day/mm)
4048 VHydCond=[0.055](mm/hr), END=-1
4049 *%-----|-----|
4050 CONTINUOUS STANDHYD NHYD=["A4"], DT=[1] min, AREA=[1.27](ha),
4051 XI MP=[0.65], TI MP=[0.65], DWF=[0](cms), LOSS=[2],
4052 SCS curve number CN=[75],
4053 Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4054 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4055 Impervious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
4056 LGI=[253](m), MNI=[0.013], SCI=[0](min),
4057 Continuous simulation parameters:
4058 I a REC per=[4](hrs), I a REC i mp=[4](hrs),
4059 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4060 Inter Event Time=[18](hrs), END=-1
4061 *%-----|-----|
4062 COMPUTE DUALHYD NHYD i n=["A4"], CI NLET=[0.405](cms), NI NLET=[1],
4063 M a j NHYD=["A4-M"]
4064 M n NHYD=["A4-MN"]
4065 T M I STO=[68](cu-m)
4066 *%-----|-----|
4067 ADD HYD NHYDs um=["MH101"], NHYDs to
add=["Al-M"+"Al-MN"+"corr1-M"+"corr1-MN"+"corr2"+"B1"+"A4-MN"]
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4068 *%-----|-----|
4069 SAVE HYD      NHYD=["MHI01"], # OF PCYCLES=[ - 1], I CASEs h=[ 1]
4070              HYD_COMMENT=["Tot al Fl ows at MHI01"]
4071 *%-----|-----|
4072 ROUTE PIPE     PTYPE=[ 1] circ, NHYDout=[" 101- 102"], RNUMBER=[ 1. 0], PDI AM=[ 1050] ( mm),
4073              PLNGTH=[ 368] ( m), PROUGH=[ 0. 013], PSLOPE=[ 0. 0054] ( m/ m),
              NHYDin=["MHI01"], RDT=[ 1]
4074 *%-----|-----|
4075 * -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
major system from A2 can be added to Todd
4076 *CONTINUOUS STANDHYD NHYD=["A2"], DT=[ 1] mi n, AREA=[ 25. 5] ( ha),
4077 *              XI MP=[ 0. 42], TI MP=[ 0. 52], DWF=[ 0] ( cms), LOSS=[ 2],
4078 *              SCS curve number CN=[ 75],
4079 *              Pervious surfaces: I A per=[ 4. 67] ( mm), SLPP=[ 1] ( %),
4080 *              LGP=[ 40] ( m), MNP=[ 0. 25], SCP=[ 0] ( mi n),
4081 *              Impervious surfaces: I A i mp=[ 1. 57] ( mm), SLPI =[ 1] ( %),
4082 *              LGI =[ 566] ( m), MNI =[ 0. 013], SCI =[ 0] ( mi n),
4083 *              Continuous simulation parameters:
4084 *              I a REC per=[ 4] ( hr s), I a REC i mp=[ 4] ( hr s),
4085 *              SM N=[ - 1] ( mm), SMAX=[ - 1] ( mm), SK=[ 0. 010] / ( mm),
4086 *              Inter Event Ti me=[ 18] ( hr s), END=- 1
4087 *%-----|-----|
4088 *COMPUTE DUALHYD NHYDin=["A2"], CI NLET=[ 1. 818] ( cms), NI NLET=[ 1],
4089 *              M a j NHYD=["A2- M"]
4090 *              M nNHYD=["A2- MN"]
4091 *              TM STO=[ 924] ( cu- m)
4092 *%-----|-----|
4093 ADD HYD        NHYDs um=["MHI02"], NHYDs to add=["A2- MN"+"101- 102"]
4094 *%-----|-----|
4095 SAVE HYD      NHYD=["MHI02"], # OF PCYCLES=[ - 1], I CASEs h=[ 1]
4096              HYD_COMMENT=["Tot al Fl ows at MHI02"]
4097 *%-----|-----|
4098 CONTINUOUS STANDHYD NHYD=["A5"], DT=[ 1] mi n, AREA=[ 1. 6] ( ha),
4099 *              XI MP=[ 0. 71], TI MP=[ 0. 71], DWF=[ 0] ( cms), LOSS=[ 2],
4100 *              SCS curve number CN=[ 75],
4101 *              Pervious surfaces: I A per=[ 4. 67] ( mm), SLPP=[ 1] ( %),
4102 *              LGP=[ 40] ( m), MNP=[ 0. 25], SCP=[ 0] ( mi n),
4103 *              Impervious surfaces: I A i mp=[ 1. 57] ( mm), SLPI =[ 1] ( %),
4104 *              LGI =[ 300] ( m), MNI =[ 0. 013], SCI =[ 0] ( mi n),
4105 *              Continuous simulation parameters:
4106 *              I a REC per=[ 4] ( hr s), I a REC i mp=[ 4] ( hr s),
4107 *              SM N=[ - 1] ( mm), SMAX=[ - 1] ( mm), SK=[ 0. 010] / ( mm),
4108 *              Inter Event Ti me=[ 18] ( hr s), END=- 1
4109 *%-----|-----|
4110 ADD HYD        NHYDs um=["A5T"], NHYDs to add=["A4- M"+"A5"]
4111 *%-----|-----|
4112 COMPUTE DUALHYD NHYDin=["A5T"], CI NLET=[ 0. 357] ( cms), NI NLET=[ 1],
4113 *              M a j NHYD=["A5- M"]
4114 *              M nNHYD=["A5- MN"]
4115 *              TM STO=[ 60] ( cu- m)
4116 *%-----|-----|
4117 * -JFSA Jan. 2021, A3 is a part of Todd so it is removed
4118 * -JFSA Jan. 2021, "A2- M" added to "Todd"
4119 *CONTINUOUS STANDHYD NHYD=["A3"], DT=[ 1] mi n, AREA=[ 18. 4] ( ha),
4120 *              XI MP=[ 0. 58], TI MP=[ 0. 65], DWF=[ 0] ( cms), LOSS=[ 2],
4121 *              SCS curve number CN=[ 75],
4122 *              Pervious surfaces: I A per=[ 4. 67] ( mm), SLPP=[ 1] ( %),
4123 *              LGP=[ 40] ( m), MNP=[ 0. 25], SCP=[ 0] ( mi n),
4124 *              Impervious surfaces: I A i mp=[ 1. 57] ( mm), SLPI =[ 1] ( %),
4125 *              LGI =[ 450] ( m), MNI =[ 0. 013], SCI =[ 0] ( mi n),
4126 *              Continuous simulation parameters:
4127 *              I a REC per=[ 4] ( hr s), I a REC i mp=[ 4] ( hr s),
4128 *              SM N=[ - 1] ( mm), SMAX=[ - 1] ( mm), SK=[ 0. 010] / ( mm),
4129 *              Inter Event Ti me=[ 18] ( hr s), END=- 1
4130 *%-----|-----|
4131 *ADD HYD        NHYDs um=["A3- A2M"], NHYDs to add=["A2- M"+"A3"]

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4132 *%-----|-----|
4133 *COMPUTE DUALHYD   NHYDin=[" A3- A2M"], CI NLET=[ 2.208](cms), NI NLET=[ 1],
4134 *                   Mj NHYD=[" A3R- M"]
4135 *                   MnNHYD=[" A3R- MN"]
4136 *                   TM STO=[ 908](cu-m)
4137 *%-----|-----|
4138 ROUTE PIPE         PTYPE=[ 1]circ, NHYDout=[" 102- 103"], RNUMBER=[ 1.0], PDI AM=[ 1500](mm),
4139                   PLNGTH=[ 504](m), PROUGH=[ 0.013], PSLOPE=[ 0.0028](m/m),
                   NHYDin=[" MHI02"], RDT=[ 1]
4140 *%-----|-----|
4141 ADD HYD            NHYDsum=[" MHI03"], NHYDs to add=[" 102- 103"+" A5- MN"]
4142 *%-----|-----|
4143 SAVE HYD          NHYD=[" MHI03"], # OF PCYCLES=[ -1], I CASEs h=[ 1]
4144                   HYD_COMMENT=[" Total Flows at MHI03"]
4145 *%-----|-----|
4146 ROUTE PIPE         PTYPE=[ 1]circ, NHYDout=[" 103- 104"], RNUMBER=[ 1.0], PDI AM=[ 1650](mm),
4147                   PLNGTH=[ 438](m), PROUGH=[ 0.013], PSLOPE=[ 0.0046](m/m),
                   NHYDin=[" MHI03"], RDT=[ 1]
4148 *%-----|-----|
4149 CONTINUOUS STANDHYD NHYD=[" A6"], DT=[ 1]min, AREA=[ 1.56](ha),
4150                   XI MP=[ 0.71], TI MP=[ 0.71], DWF=[ 0](cms), LOSS=[ 2],
4151                   SCS curve number CN=[ 75],
4152                   Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4153                   LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4154                   Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4155                   LGI=[ 280](m), MNI=[ 0.013], SCI=[ 0](min),
4156                   Continuous simulation parameters:
4157                   IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4158                   SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4159                   InterEventTime=[ 18](hrs), END=- 1
4160 *%-----|-----|
4161 ADD HYD            NHYDsum=[" A6T"], NHYDs to add=[" A5- M"+" A6"]
4162 *%-----|-----|
4163 COMPUTE DUALHYD   NHYDin=[" A6T"], CI NLET=[ 0.357](cms), NI NLET=[ 1],
4164 *                   Mj NHYD=[" A6- M"]
4165 *                   MnNHYD=[" A6- MN"]
4166 *                   TM STO=[ 60](cu-m)
4167 *%-----|-----|
4168 * -JFSA Jan. 2021, A7-corrig is a part of Todd so it is removed
4169 *CONTINUOUS STANDHYD NHYD=[" A7-corrig"], DT=[ 1]min, AREA=[ 11.8](ha),
4170 *                   XI MP=[ 0.41], TI MP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4171 *                   SCS curve number CN=[ 75],
4172 *                   Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4173 *                   LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4174 *                   Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4175 *                   LGI=[ 438](m), MNI=[ 0.013], SCI=[ 0](min),
4176 *                   Continuous simulation parameters:
4177 *                   IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4178 *                   SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4179 *                   InterEventTime=[ 18](hrs), END=- 1
4180 *%-----|-----|
4181 *ADD HYD            NHYDsum=[" A7- A3RM"], NHYDs to add=[" A3R- M"+" A7-corrig"]
4182 *%-----|-----|
4183 *COMPUTE DUALHYD   NHYDin=[" A7- A3RM"], CI NLET=[ 1.003](cms), NI NLET=[ 1],
4184 *                   Mj NHYD=[" A7R- M"]
4185 *                   MnNHYD=[" A7R- MN"]
4186 *                   TM STO=[ 496](cu-m)
4187 *%-----|-----|
4188 ADD HYD            NHYDsum=[" MHI04"], NHYDs to add=[" A6- MN"+" 103- 104"+" TODD_Mn"]
4189 *%-----|-----|
4190 SAVE HYD          NHYD=[" MHI04"], # OF PCYCLES=[ -1], I CASEs h=[ 1]
4191                   HYD_COMMENT=[" Total Flows at MHI04"]
4192 *%-----|-----|
4193 CONTINUOUS STANDHYD NHYD=[" B2"], DT=[ 1]min, AREA=[ 12.31](ha),
4194                   XI MP=[ 0.41], TI MP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4195                   SCS curve number CN=[ 75],

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4196          Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
4197          LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4198          Impervious surfaces: I A i mp=[ 1.57](mm), SLPI=[ 1](%),
4199          LGI=[ 417](m), MNI=[ 0.013], SCI=[ 0](min),
4200          Continuous simulation parameters:
4201          I a RE C per=[ 4](hrs), I a RE C i mp=[ 4](hrs),
4202          SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4203          Inter Event Ti me=[ 18](hrs), END=- 1
4204  *%-----|
4205  COMPUTE DUALHYD  NHYD i n=[ "B2"], CI NLET=[ 1.029](cms), NI NLET=[ 1],
4206                   M a j NHYD=[ "B2- M "]
4207                   M n NHYD=[ "B2- MN"]
4208                   TM I STO=[ 508](cu-m)
4209  *%-----|
4210  ROUTE PI PE      PTYPE=[ 1]circ, NHYDout=[ "315-333"], RNUMBER=[ 1.0], PDI AM=[ 1200](mm),
4211                   PLNGTH=[ 254](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
4212                   NHYD i n=[ "B2- MN"], RDT=[ 1]
4213  *%-----|
4214  CONTINUOUS STANDHYD  NHYD=[ "B3"], DT=[ 1]min, AREA=[ 5.59](ha),
4215                   XI MP=[ 0.41], TI MP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4216                   SCS curve number CN=[ 75],
4217                   Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
4218                   LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4219                   Impervious surfaces: I A i mp=[ 1.57](mm), SLPI=[ 1](%),
4220                   LGI=[ 345](m), MNI=[ 0.013], SCI=[ 0](min),
4221                   Continuous simulation parameters:
4222                   I a RE C per=[ 4](hrs), I a RE C i mp=[ 4](hrs),
4223                   SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4224                   Inter Event Ti me=[ 18](hrs), END=- 1
4225  *%-----|
4226  COMPUTE DUALHYD  NHYD i n=[ "B3"], CI NLET=[ 0.459](cms), NI NLET=[ 1],
4227                   M a j NHYD=[ "B3- M "]
4228                   M n NHYD=[ "B3- MN"]
4229                   TM I STO=[ 227](cu-m)
4230  *%-----|
4231  ADD HYD          NHYDs um=[ "MH333"], NHYDs to add=[ "B3- MN"+"315-333"]
4232  *%-----|
4233  SAVE HYD         NHYD=[ "MH333"], # OF PCYCLES=[ -1], I CASEs h=[ 1]
4234                   HYD_COMMENT=[ "Total Flows at MH333"]
4235  *%-----|
4236  ROUTE PI PE      PTYPE=[ 1]circ, NHYDout=[ "333-335"], RNUMBER=[ 1.0], PDI AM=[ 1200](mm),
4237                   PLNGTH=[ 251](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
4238                   NHYD i n=[ "MH333"], RDT=[ 1]
4239  *%-----|
4240  ROUTE PI PE      PTYPE=[ 1]circ, NHYDout=[ "335-338"], RNUMBER=[ 1.0], PDI AM=[ 1200](mm),
4241                   PLNGTH=[ 185](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
4242                   NHYD i n=[ "333-335"], RDT=[ 1]
4243  *%-----|
4244  ROUTE PI PE      PTYPE=[ 1]circ, NHYDout=[ "338-340"], RNUMBER=[ 1.0], PDI AM=[ 1350](mm),
4245                   PLNGTH=[ 233](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
4246                   NHYD i n=[ "335-338"], RDT=[ 1]
4247  *%-----|
4248  CONTINUOUS STANDHYD  NHYD=[ "B4"], DT=[ 1]min, AREA=[ 7.6](ha),
4249                   XI MP=[ 0.41], TI MP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4250                   SCS curve number CN=[ 75],
4251                   Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
4252                   LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4253                   Impervious surfaces: I A i mp=[ 1.57](mm), SLPI=[ 1](%),
4254                   LGI=[ 388](m), MNI=[ 0.013], SCI=[ 0](min),
4255                   Continuous simulation parameters:
4256                   I a RE C per=[ 4](hrs), I a RE C i mp=[ 4](hrs),
4257                   SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4258                   Inter Event Ti me=[ 18](hrs), END=- 1
4259  *%-----|
4260  COMPUTE DUALHYD  NHYD i n=[ "B4"], CI NLET=[ 0.655](cms), NI NLET=[ 1],
4261                   M a j NHYD=[ "B4- M "]

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4258 M nNHYD=[ " B4- MN" ]
4259 TM STO=[ 323] ( cu- m)
4260 *%-----|-----|
4261 ADD HYD NHYDs um=[ " M340" ], NHYDs to add=[ " 338- 340" + " B4- MN" ]
4262 *%-----|-----|
4263 SAVE HYD NHYD=[ " M340" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
4264 HYD_ COMMENT=[ " Tot al Fl ows at M340" ]
4265 *%-----|-----|
4266 ROUTE PI PE PTYPE=[ 1] circ, NHYDout=[ " 340- 104" ], RNUMBER=[ 1. 0 ], PDI AM=[ 1650] ( mm) ,
4267 PLNGTH=[ 240] ( m) , PROUGH=[ 0. 013 ], PSLOPE=[ 0. 0015] ( m/ m) ,
NHYDin=[ " M340" ], RDT=[ 1 ]
4268 *%-----|-----|
4269 ADD HYD NHYDs um=[ " M104T" ], NHYDs to add=[ " 340- 104" + " M104" ]
4270 *%-----|-----|
4271 ROUTE PI PE PTYPE=[ 2] rect, NHYDout=[ " 104- 105" ], RNUMBER=[ 1. 0 ],
4272 PW DTH=[ 2400] ( mm) by PHEI GHT=[ 2100] ( mm) ,
PLNGTH=[ 380] ( m) , PROUGH=[ 0. 013 ], PSLOPE=[ 0. 001] ( m/ m) ,
NHYDin=[ " M104T" ], RDT=[ 1 ]
4273 *%-----|-----|
4274 CONTINUOUS STANDHYD NHYD=[ " B5" ], DT=[ 1] mi n, AREA=[ 2. 2] ( ha) ,
4275 XI MP=[ 0. 57] , TI MP=[ 0. 57] , DWF=[ 0] ( cms) , LOSS=[ 2] ,
4276 SCS curve number CN=[ 75] ,
4277 Pervious surfaces: IAper=[ 4. 67] ( mm) , SLPP=[ 1] ( % ) ,
4278 LGP=[ 40] ( m) , MNP=[ 0. 25] , SCP=[ 0] ( mi n) ,
4279 Impervious surfaces: IAi mp=[ 1. 57] ( mm) , SLPI =[ 1] ( % ) ,
4280 LGI =[ 187] ( m) , MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
4281 Continuous simulation parameters:
4282 IaRECper=[ 4] ( hrs) , IaRECI mp=[ 4] ( hrs) ,
4283 SM N=[ - 1] ( mm) , SMAX=[ - 1] ( mm) , SK=[ 0. 010] / ( mm) ,
4284 InterEvent Ti me=[ 18] ( hrs) , END=- 1
4285 *%-----|-----|
4286 COMPUTE DUALHYD NHYDin=[ " B5" ], CI NLET=[ 0. 260] ( cms) , NI NLET=[ 1] ,
4287 MAj NHYD=[ " B5- M" ]
4288 M nNHYD=[ " B5- MN" ]
4289 TM STO=[ 250] ( cu- m)
4290 *%-----|-----|
4291 CONTINUOUS STANDHYD NHYD=[ " A8" ], DT=[ 1] mi n, AREA=[ 0. 96] ( ha) ,
4292 XI MP=[ 0. 71] , TI MP=[ 0. 71] , DWF=[ 0] ( cms) , LOSS=[ 2] ,
4293 SCS curve number CN=[ 75] ,
4294 Pervious surfaces: IAper=[ 4. 67] ( mm) , SLPP=[ 1] ( % ) ,
4295 LGP=[ 40] ( m) , MNP=[ 0. 25] , SCP=[ 0] ( mi n) ,
4296 Impervious surfaces: IAi mp=[ 1. 57] ( mm) , SLPI =[ 1] ( % ) ,
4297 LGI =[ 186] ( m) , MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
4298 Continuous simulation parameters:
4299 IaRECper=[ 4] ( hrs) , IaRECI mp=[ 4] ( hrs) ,
4300 SM N=[ - 1] ( mm) , SMAX=[ - 1] ( mm) , SK=[ 0. 010] / ( mm) ,
4301 InterEvent Ti me=[ 18] ( hrs) , END=- 1
4302 *%-----|-----|
4303 ADD HYD NHYDs um=[ " A8T" ], NHYDs to add=[ " A6- M" + " A8" ]
4304 *%-----|-----|
4305 COMPUTE DUALHYD NHYDin=[ " A8T" ], CI NLET=[ 0. 238] ( cms) , NI NLET=[ 1] ,
4306 MAj NHYD=[ " A8- M" ]
4307 M nNHYD=[ " A8- MN" ]
4308 TM STO=[ 40] ( cu- m)
4309 *%-----|-----|
4310 ADD HYD NHYDs um=[ " M105" ], NHYDs to
4311 add=[ " 104- 105" + " B5- MN" + " A8- MN" + " TODD_ MN3j " ]
4312 *%-----|-----|
4313 SAVE HYD NHYD=[ " M105" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
4314 HYD_ COMMENT=[ " Tot al Fl ows at M105" ]
4315 *%-----|-----|
4316 DI VERT HYD NHYDin=[ " A8- M" ] NI Dout=[ 2] max five,
4317 outflow hydr ographs ( NHYDs)=[ " A8- M- JR" " A8- M- B6" ]
4318 flow distribution table: ( modify as necessary)
Note: all flows are in ( cms)

```

```

4319          QI Di + QI Di i = QTOTAL
4320          [ 0 + 0 = 0 ]
4321          [ 50 + 50 = 100 ] end
4322  *%-----|-----
|
4323  DI VERT HYD  NHYDin=["MHI05"] NI Dout=[2] max five,
4324              outflow hydrographs (NHYDs)=["MHI05-JR" "MHI05-B6"]
4325              flow distribution table: (modify as necessary)
4326              Note: all flows are in (cms)
4327              QI Di + QI Di i = QTOTAL
4328              [ 0 + 0 = 0 ]
4329              [ 0 + 3.0 = 3.0 ]
4330              [ 96.9+ 3.1 = 100 ] end
4331  *%-----|-----
|
4332  CONTINUOUS STANDHYD  NHYD=["B7"], DT=[1] min, AREA=[7.19](ha),
4333                    XI MP=[0.41], TI MP=[0.54], DWF=[0](cms), LOSS=[2],
4334                    SCS curve number CN=[75],
4335                    Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4336                    LGP=[40](m), MNP=[0.25], SCP=[0](min),
4337                    Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4338                    LGI=[211](m), MNI=[0.013], SCI=[0](min),
4339                    Continuous simulation parameters:
4340                    IaRECper=[4](hrs), IaRECImp=[4](hrs),
4341                    SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4342                    InterEventTime=[18](hrs), END=-1
4343  *%-----|-----
4344  ADD HYD      NHYDsum=["B7-B4M"], NHYDs to add=["B4-M"+"B7"]
4345  *%-----|-----
4346  COMPUTE DUALHYD  NHYDin=["B7-B4M"], CINLET=[0.629](cms), NINLET=[1],
4347                    MijNHYD=["B7R-M"]
4348                    MnNHYD=["B7R-MN"]
4349                    TMSTO=[311](cu-m)
4350  *%-----|-----
4351  ROUTE PIPE    PTYPE=[1] circ, NHYDout=["360-106A"], RNUMBER=[1.0], PDIAM=[1050](mm),
4352                    PLNGTH=[167](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
4353                    NHYDin=["B7R-MN"], RDT=[1]
4354  *%-----|-----
4355  * -JFSA 2021-01-19 change B6 to be developed as per geottawa website and apply the
4356  parameters of A7, the nearest sub-catchment to B6, LGI is calculated based on B6 area
4357  CONTINUOUS STANDHYD  NHYD=["B6"], DT=[1] min, AREA=[3.29](ha),
4358                    XI MP=[0.41], TI MP=[0.54], DWF=[0](cms), LOSS=[2],
4359                    SCS curve number CN=[75],
4360                    Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4361                    LGP=[40](m), MNP=[0.25], SCP=[0](min),
4362                    Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4363                    LGI=[148.099](m), MNI=[0.013], SCI=[0](min),
4364                    Continuous simulation parameters:
4365                    IaRECper=[4](hrs), IaRECImp=[4](hrs),
4366                    SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4367                    InterEventTime=[18](hrs), END=-1
4368  *%-----|-----
4369  * -JFSA 2021-01-25 add B1 DUALHYD as per Corrigan Report, IBI Group, 2008
4370  COMPUTE DUALHYD  NHYDin=["B6"], CINLET=[0.064](cms), NINLET=[1],
4371                    MijNHYD=["B6-M"]
4372                    MnNHYD=["B6-MN"]
4373                    TMSTO=[5484](cu-m)
4374  *%-----|-----
4375  * CONTINUOUS NASHHYD  NHYD=["B6"], DT=[1] min, AREA=[3.29](ha),
4376  *                    DWF=[0](cms), CN C=[75], IA=[2.5](mm),
4377  *                    N=[3.0], TP=[0.36]hrs,
4378  *                    Continuous simulation parameters:
4379  *                    IaRECper=[4](hrs),
4380  *                    SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4381  *                    InterEventTime=[12](hrs)
4382  *                    Baseflow simulation parameters:

```

```

4381 * BaseFlowOption=[ 1 ] ,
4382 * InitGWResVol =[ 50 ] ( mm ) , GWResK=[ 0.96 ] ( mm/ day/ mm)
4383 * VHydCond=[ 0.055 ] ( mm/ hr ) , END=- 1
4384 *%-----|-----|
4385 *% -EX-LAND is external land. It is a part of JOCKVA sub-catchment as per Corrigan
Report, IBI Group, 2008
4386 CONTINUOUS STANDHYD NHYD=[ "EX-LAND" ] , DT=[ 1 ] mi n , AREA=[ 32.5 ] ( ha ) ,
4387 XI MP=[ 0.50 ] , TI MP=[ 0.50 ] , DWF=[ 0 ] ( cms ) , LOSS=[ 2 ] ,
4388 SCS curve number CN=[ 74 ] ,
4389 Pervious surfaces: I A per =[ 4.67 ] ( mm ) , SLPP=[ 1 ] ( % ) ,
4390 LGP=[ 40 ] ( m ) , MNP=[ 0.25 ] , SCP=[ 0 ] ( mi n ) ,
4391 Impervious surfaces: I A i mp =[ 1.57 ] ( mm ) , SLPI =[ 1 ] ( % ) ,
4392 LGI =[ 465.475 ] ( m ) , MNI =[ 0.013 ] , SCI =[ 0 ] ( mi n ) ,
4393 Continuous simulation parameters:
4394 I a REC per =[ 4 ] ( hrs ) , I a REC i mp =[ 4 ] ( hrs ) ,
4395 SM N =[ - 1 ] ( mm ) , SMAX =[ - 1 ] ( mm ) , SK =[ 0.010 ] / ( mm ) ,
4396 InterEventTi me =[ 18 ] ( hrs ) , END=- 1
4397 *%-----|-----|
4398 COMPUTE DUALHYD NHYD i n =[ "EX-LAND" ] , CI NLET =[ 2.275 ] ( cms ) , NI NLET =[ 1 ] ,
4399 M a j NHYD =[ "EX-LAND- M " ]
4400 M nNHYD =[ "EX-LAND- MN" ]
4401 TM S TO =[ 1365 ] ( cu- m)
4402 *%-----|-----|
4403 ADD HYD NHYDs um =[ " B6- B7ExM " ] , NHYDs t o
add =[ " B7R- M " + " EX-LAND- M " + " B5- M " + " B6- M " + " B6- MN" + " A8- M - B6 " ]
4404 *%-----|-----|
4405 COMPUTE DUALHYD NHYD i n =[ " B6- B7ExM " ] , CI NLET =[ 0.064 ] ( cms ) , NI NLET =[ 1 ] ,
4406 M a j NHYD =[ " B6R- M " ]
4407 M nNHYD =[ " B6R- MN" ]
4408 TM S TO =[ 5484 ] ( cu- m)
4409 *%-----|-----|
4410 ROUTE PI PE PTYPE =[ 1 ] circ , NHYDout =[ " 105- 106A " ] , RNUMBER =[ 1.0 ] , PDI AM =[ 1800 ] ( mm ) ,
4411 PLNGTH =[ 208 ] ( m ) , PROUGH =[ 0.013 ] , PSLOPE =[ 0.001 ] ( m/ m ) ,
NHYD i n =[ " MHI 05- B6 " ] , RDT =[ 1 ]
4412 *%-----|-----|
4413 ADD HYD NHYDs um =[ " MHI 06A " ] , NHYDs t o
add =[ " 360- 106A " + " 105- 106A " + " B6R- MN" + " B6R- M " ]
4414 *%-----|-----|
4415 SAVE HYD NHYD =[ " MHI 06A " ] , # OF PCYCLES =[ - 1 ] , I CASEs h =[ 1 ]
4416 HYD_COMMENT =[ " Total Flows at MHI 06A " ]
4417 *%-----|-----|
4418 *% -JFSA 2021-01-12 THE MANHOLE MHI06 is called MHI17/106 in Corrigan Report, IBI
Group, July 2008
4419 *%
4420 ROUTE PI PE PTYPE =[ 1 ] circ , NHYDout =[ " 106A- 106 " ] , RNUMBER =[ 1.0 ] , PDI AM =[ 1800 ] ( mm ) ,
4421 PLNGTH =[ 190 ] ( m ) , PROUGH =[ 0.013 ] , PSLOPE =[ 0.001 ] ( m/ m ) ,
NHYD i n =[ " MHI 06A " ] , RDT =[ 1 ]
4422 *%-----|-----|
4423 CONTINUOUS STANDHYD NHYD=[ " A9 " ] , DT=[ 1 ] mi n , AREA=[ 2.44 ] ( ha ) ,
4424 XI MP=[ 0.71 ] , TI MP=[ 0.71 ] , DWF=[ 0 ] ( cms ) , LOSS=[ 2 ] ,
4425 SCS curve number CN=[ 75 ] ,
4426 Pervious surfaces: I A per =[ 4.67 ] ( mm ) , SLPP=[ 1 ] ( % ) ,
4427 LGP=[ 40 ] ( m ) , MNP=[ 0.25 ] , SCP=[ 0 ] ( mi n ) ,
4428 Impervious surfaces: I A i mp =[ 1.57 ] ( mm ) , SLPI =[ 1 ] ( % ) ,
4429 LGI =[ 262 ] ( m ) , MNI =[ 0.013 ] , SCI =[ 0 ] ( mi n ) ,
4430 Continuous simulation parameters:
4431 I a REC per =[ 4 ] ( hrs ) , I a REC i mp =[ 4 ] ( hrs ) ,
4432 SM N =[ - 1 ] ( mm ) , SMAX =[ - 1 ] ( mm ) , SK =[ 0.010 ] / ( mm ) ,
4433 InterEventTi me =[ 18 ] ( hrs ) , END=- 1
4434 *%-----|-----|
4435 COMPUTE DUALHYD NHYD i n =[ " A9 " ] , CI NLET =[ 0.547 ] ( cms ) , NI NLET =[ 1 ] ,
4436 M a j NHYD =[ " A9- M " ]
4437 M nNHYD =[ " A9- MN" ]
4438 TM S TO =[ 0 ] ( cu- m)
4439 *%-----|-----|
4440 ADD HYD NHYDs um =[ " MHI 06 " ] , NHYDs t o add =[ " 106A- 106 " + " A9- MN" ]

```

```

4441  *%-----|-----|
4442  SAVE HYD      NHYD=["MHI06"], # OF PCYCLES=[ - 1], I CASEs h=[ 1]
4443              HYD_COMMENT=["Tot al Fl ows at MHI06"]
4444  *%-----|-----|
4445  *%    -JFSA 2021-01-12 THE MANHOLE MHI07 is called MHI18/107 in Corrigan Report, IBI
Group, July 2008
4446  *%
4447  ROUTE PIPE    PTYPE=[ 1]circ, NHYDout=["106-107"], RNUMBER=[ 1.0], PDI AM=[ 1800](mm),
4448              PLNGTH=[ 122.5](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
              NHYDin=["MHI06"], RDT=[ 1]
4449  *%-----|-----|
4450  CONTINUOUS STANDHYD NHYD=["A10"], DT=[ 1]mi n, AREA=[ 4.14](ha),
4451              XI MP=[ 0.35], TI MP=[ 0.47], DWF=[ 0](cms), LOSS=[ 2],
4452              SCS curve number CN=[ 75],
4453              Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
4454              LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n),
4455              Impervious surfaces: I Ai mp=[ 1.57](mm), SLPI=[ 1](%),
4456              LGI=[ 183](m), MNI =[ 0.013], SCI =[ 0](mi n),
4457              Continuous simulation parameters:
4458              I a REC per=[ 4](hrs), I a REC i mp=[ 4](hrs),
4459              SM N=[ - 1](mm), SMAX=[ - 1](mm), SK=[ 0.010]/(mm),
4460              Inter Event Ti me=[ 18](hrs), END=- 1
4461  *%-----|-----|
4462  COMPUTE DUALHYD NHYDin=["A10"], CI NLET=[ 0.310](cms), NI NLET=[ 1],
4463              M aj NHYD=["A10- M "]
4464              M nNHYD=["A10- MN"]
4465              TM STO=[ 228](cu-m)
4466  *%-----|-----|
4467  CONTINUOUS STANDHYD NHYD=["A11"], DT=[ 1]mi n, AREA=[ 10.61](ha),
4468              XI MP=[ 0.53], TI MP=[ 0.62], DWF=[ 0](cms), LOSS=[ 2],
4469              SCS curve number CN=[ 75],
4470              Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
4471              LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n),
4472              Impervious surfaces: I Ai mp=[ 1.57](mm), SLPI=[ 1](%),
4473              LGI=[ 379](m), MNI =[ 0.013], SCI =[ 0](mi n),
4474              Continuous simulation parameters:
4475              I a REC per=[ 4](hrs), I a REC i mp=[ 4](hrs),
4476              SM N=[ - 1](mm), SMAX=[ - 1](mm), SK=[ 0.010]/(mm),
4477              Inter Event Ti me=[ 18](hrs), END=- 1
4478  *%-----|-----|
4479  COMPUTE DUALHYD NHYDin=["A11"], CI NLET=[ 0.993](cms), NI NLET=[ 1],
4480              M aj NHYD=["A11- M "]
4481              M nNHYD=["A11- MN"]
4482              TM STO=[ 556](cu-m)
4483  *%-----|-----|
4484  ADD HYD       NHYDs um=["MHI07"], NHYDs to add=["106-107"+"A10- MN"+"A11- MN"]
4485  *%-----|-----|
4486  SAVE HYD      NHYD=["MHI07"], # OF PCYCLES=[ - 1], I CASEs h=[ 1]
4487              HYD_COMMENT=["Tot al Fl ows at MHI07"]
4488  *%-----|-----|
4489  ROUTE PIPE    PTYPE=[ 1]circ, NHYDout=["107-119"], RNUMBER=[ 1.0], PDI AM=[ 1800](mm),
4490              PLNGTH=[ 114](m), PROUGH=[ 0.013], PSLOPE=[ 0.0012](m/m),
              NHYDin=["MHI07"], RDT=[ 1]
4491  *%-----|-----|
4492  *%    -JFSA 2021-01-12 THE MANHOLE MHI08 is called MHI20/108 in Corrigan Report, IBI
Group, July 2008
4493  *%
4494  ROUTE PIPE    PTYPE=[ 1]circ, NHYDout=["119-108"], RNUMBER=[ 1.0], PDI AM=[ 1800](mm),
4495              PLNGTH=[ 65.8](m), PROUGH=[ 0.013], PSLOPE=[ 0.0012](m/m),
              NHYDin=["107-119"], RDT=[ 1]
4496  *%-----|-----|
4497  CONTINUOUS STANDHYD NHYD=["A12"], DT=[ 1]mi n, AREA=[ 12.29](ha),
4498              XI MP=[ 0.41], TI MP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4499              SCS curve number CN=[ 75],
4500              Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
4501              LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n),

```

```

4502      Impervious surfaces: I A i mp=[ 1.57](mm), SLPI=[ 1](%),
4503              LGI=[ 183](m), MNI=[ 0.013], SCI=[ 0](mi n),
4504      Continuous simulation parameters:
4505      I a RE C per=[ 4](hrs), I a RE C i mp=[ 4](hrs),
4506      SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4507      Inter Event Ti me=[ 18](hrs), END=- 1
4508  *%-----|
4509  COMPUTE DUALHYD      NHYD i n=[ "A12"], CI NLET=[ 1.029](cms), NI NLET=[ 1],
4510                      M i j NHYD=[ "A12- M "]
4511                      M n NHYD=[ "A12- MN"]
4512                      TM I STO=[ 672](cu- m)
4513  *%-----|
4514  CONTINUOUS STANDHYD      NHYD=[ "A13"], DT=[ 1]mi n, AREA=[ 2.59](ha),
4515                      XI MP=[ 0.71], TI MP=[ 0.71], DWF=[ 0](cms), LOSS=[ 2],
4516                      SCS curve number CN=[ 75],
4517                      Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
4518                      LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n),
4519                      Impervious surfaces: I A i mp=[ 1.57](mm), SLPI=[ 1](%),
4520                      LGI=[ 379](m), MNI=[ 0.013], SCI=[ 0](mi n),
4521                      Continuous simulation parameters:
4522                      I a RE C per=[ 4](hrs), I a RE C i mp=[ 4](hrs),
4523                      SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4524                      Inter Event Ti me=[ 18](hrs), END=- 1
4525  *%-----|
4526  COMPUTE DUALHYD      NHYD i n=[ "A13"], CI NLET=[ 0.571](cms), NI NLET=[ 1],
4527                      M i j NHYD=[ "A13- M "]
4528                      M n NHYD=[ "A13- MN"]
4529                      TM I STO=[ 0](cu- m)
4530  *%-----|
4531  * -JFSA 2021-01-22 add the Corrigan pond area ("Pond-Block")
4532  CONTINUOUS STANDHYD      NHYD=[ "Pond- Bl ock"], DT=[ 1]mi n, AREA=[ 2.94](ha),
4533                      XI MP=[ 0.415], TI MP=[ 0.415], DWF=[ 0](cms), LOSS=[ 2],
4534                      SCS curve number CN=[ 75],
4535                      Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
4536                      LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n),
4537                      Impervious surfaces: I A i mp=[ 1.57](mm), SLPI=[ 1](%),
4538                      LGI=[ 183](m), MNI=[ 0.013], SCI=[ 0](mi n),
4539                      Continuous simulation parameters:
4540                      I a RE C per=[ 4](hrs), I a RE C i mp=[ 4](hrs),
4541                      SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4542                      Inter Event Ti me=[ 18](hrs), END=- 1
4543  *%-----|
4544  ADD HYD      NHYDs um=[ "MH108"], NHYDs to add=[ "119-108"+"A13- MN"+"A12- MN"]
4545  *%-----|
4546  SAVE HYD      NHYD=[ "MH108"], # OF PCYCLES=[ -1], I CASEs h=[ 1]
4547                      HYD_ COMMENT=[ "Tot al Fl ows at MH108"]
4548  *%-----|
4549  ROUTE PI PE      PTYPE=[ 1]circ, NHYDout=[ "108-116"], RNUMBER=[ 1.0], PDI AM=[ 1800](mm),
4550                      PLNGTH=[ 76.6](m), PROUGH=[ 0.013], PSLOPE=[ 0.0013](m/m),
4551                      NHYD i n=[ "MH108"], RDT=[ 1]
4552  *%-----|
4553  ROUTE PI PE      PTYPE=[ 1]circ, NHYDout=[ "116-corrig"], RNUMBER=[ 1.0],
4554                      PDI AM=[ 1800](mm),
4555                      PLNGTH=[ 79.5](m), PROUGH=[ 0.013], PSLOPE=[ 0.0013](m/m),
4556                      NHYD i n=[ "108-116"], RDT=[ 1]
4557  *%-----|
4558  ADD HYD      NHYDs um=[ "Corrigan"], NHYDs to add=[ "116-corrig"+"Pond- Bl ock"]
4559  *%-----|
4560  SAVE HYD      NHYD=[ "Corrigan"], # OF PCYCLES=[ -1], I CASEs h=[ 1]
4561                      HYD_ COMMENT=[ "Tot al Fl ows at Corrigan Pond"]
4562  *%-----|
4563  ROUTE RESERVOIR      NHYDout=[ "Co- P"], NHYD i n=[ "Corrigan"],
4564                      RDT=[ 1](mi n),
4565                      TABLE of ( OUTFLOW STORAGE ) values
4566                      (cms) - (ha- m)
4567                      [ 0.0 , 0.0 ]

```



```

4565 [ 0.015 , 0.04118]
4566 [ 0.030 , 0.08297]
4567 [ 0.045 , 0.12537]
4568 [ 0.060 , 0.16837]
4569 [ 0.075 , 0.21199]
4570 [ 0.090 , 0.27545]
4571 [ 0.105 , 0.34650]
4572 [ 0.120 , 0.42049]
4573 [ 0.135 , 0.50188]
4574 [ 0.186 , 0.60307]
4575 [ 2.110 , 0.79083]
4576 [ 5.874 , 1.00271]
4577 [ 11.395 , 1.29643]
4578 [ 18.770 , 1.62054]
4579 [ 28.143 , 1.97516]
4580 [ -1 , -1 ] (max twenty pts)
4581 NHYDovf=[ "Co- P- OVF" ]
4582 *%-----|-----|
4583 ADD HYD NHYDsum=[ "corrig" ], NHYDs to
add=[ "Co- P- OVF" + "Co- P" + "N_TO" + "M105- JR" + "A8- M- JR" + "A9- M" + "A10- M" + "A11- M" + "A12- M" + "A
13- M" ]
4584 *%-----|-----|
4585 SAVE HYD NHYD=[ "corrig" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1]
4586 HYD_COMMENT=[ "Total Flows at Corrigan Pond" ]
4587 *%-----|-----|
4588 *#*****|
4589 *# Corrigan Pond 1
4590 *# - Rating curve obtained from Barrhaven South M&S modeling
4591 *# - Tributary Drainage Area to M&S Pond 1 = 145 ha
4592 *#*****|
4593 *ROUTE RESERVOIR NHYDout=[ "MS_P1" ], NHYDin=[ "CORRIG" ],
4594 * RDT=[ 1 ] (min),
4595 * TABLE of ( OUTFLOW STORAGE ) values
4596 * (cms) - (ha-m)
4597 * [ 0.0 , 0.0 ]
4598 * [ 0.06 , 0.58]
4599 * [ -1 , -1 ] (max twenty pts)
4600 * NHYDovf=[ "P1- OVF" ]
4601 *%-----|-----|
4602 *ADD HYD NHYDsum=[ "SN_CO" ], NHYDs to add=[ "N_TO" + "P1- OVF" + "MS_P1" ]
4603 *%-----|-----|
4604 *SAVE HYD NHYD=[ "SN_CO" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1]
4605 * HYD_COMMENT=[ "Total Flows at Corrigan Drain" ]
4606 *%-----|-----|
4607 *#
4608 *# Hydrograph from Corrigan Drain routed to Jockvale Road
4609 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
4610 *#
4611 ROUTE CHANNEL NHYDout=[ "N_M" ], NHYDin=[ "corrig" ],
4612 RDT=[ 1 ] (min),
4613 CHLGTH=[ 580 ] (m), CHSLOPE=[ 0.4448 ] ( % ),
4614 FPSLOPE=[ 0.4448 ] ( % ),
4615 SECNUM=[ 1.0 ], NSEG=[ 3]
4616 ( SEGROUGH, SEGDI ST (m) ) =
4617 [ 0.075, -17.72
4618 -0.045, 17.72
4619 0.075, 80.62 ] NSEG times
4620 ( DI STANCE (m), ELEVATI ON (m) ) =
4621 [ -83.32, 90.00]
4622 [ -81.36, 89.50]
4623 [ -79.12, 89.00]
4624 [ -76.13, 88.50]
4625 [ -20.46, 88.00]
4626 [ -19.36, 87.50]
4627 [ -18.51, 87.00]
4628 [ -17.72, 86.50]

```

4629 [- 11.95, 85.24]
4630 [- 0.11, 85.12]
4631 [11.49, 85.20]
4632 [17.72, 86.50]
4633 [19.74, 87.00]
4634 [21.22, 87.50]
4635 [22.68, 88.00]
4636 [24.28, 88.50]
4637 [26.79, 89.00]
4638 [71.98, 90.00]
4639 [80.62, 90.50]

*%-----|-----|
*#*****|

*# Catchment MLLS
*# - To SWM Facility north of the Jock
*# - Primarily residential development

*#*****|

CONTINUOUS STANDHYD NHYD=["MLLS"], DT=[1]min, AREA=[175.99](ha),
XIMP=[0.38], TIMP=[0.38], DWF=[0](cms), LOSS=[2],
SCS curve number CN=[74],
PerVIOUS surfaces: IAPer=[4.67](mm), SLPP=[1](%),
LGP=[40](m), MNP=[0.25], SCP=[0](min),
ImperVIOUS surfaces: IAImp=[1.57](mm), SLPI=[1](%),
LGI=[1118.123](m), MNI=[0.013], SCI=[0](min),
Continuous simulation parameters:
IARECper=[4](hrs), IARECimp=[4](hrs),
SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
InterEventTime=[18](hrs), END=-1

*%-----|-----|
*#*****|

*# Chapman Mills SWM Pond
*# - Rating curve obtained from CCL hydraulic modeling

*#*****|

ROUTE RESERVOIR NHYDout=["MLL_P"], NHYDin=["MLLS"],
RDT=[1](min),
TABLE of (OUTFLOW STORAGE) values

	(cms) - (ha-m)
4666	[0.0 , 0.0]
4667	[0.01 , 0.01]
4668	[0.05 , 0.06]
4669	[0.09 , 0.11]
4670	[0.13 , 0.15]
4671	[0.18 , 0.19]
4672	[0.28 , 0.28]
4673	[0.37 , 0.34]
4674	[0.45 , 0.40]
4675	[0.51 , 0.44]
4676	[0.56 , 0.47]
4677	[0.64 , 0.52]
4678	[0.76 , 0.59]
4679	[0.86 , 0.65]
4680	[1.09 , 0.78]
4681	[1.44 , 0.96]
4682	[3.18 , 1.84]
4683	[4.05 , 2.31]
4684	[-1 , -1] (max twenty pts)

NHYDovf=["ML-OV"]

*%-----|-----|
*#*****|

ADD HYD NHYDsum=["SN_M"], NHYDs to add=["N_M"+"ML-OV"+"MLL_P"]

*%-----|-----|

SAVE HYD NHYD=["SN_M"], # OF PCYCLES=[-1], I CASEs h=[1]
HYD_COMMENT=["Total Flows at Jockvale Road"]

*%-----|-----|

*#
*# Hydrograph from Jockvale Road routed to Heart's Desire
*# Channel X-Section obtained from RVCA Hydraulic Model - Station 689

```

4695 *#
4696 ROUTE CHANNEL NHYDout=["N_DE"], NHYDin=["SN_M"],
4697 RDT=[1](min),
4698 CHLGTH=[1962](m), CHSLOPE=[0.2227](%),
4699 FPSLOPE=[0.2227](%),
4700 SECNUM=[1.0], NSEG=[3]
4701 (SEGROUGH, SEGDIST(m))=
4702 [0.075, -17.56
4703 -0.045, 18.27
4704 0.075, 32.51] NSEG times
4705 (DISTANCE(m), ELEVATION(m))=
4706 [-54.07, 85.00]
4707 [-39.43, 84.50]
4708 [-28.30, 84.00]
4709 [-24.12, 83.50]
4710 [-22.30, 83.00]
4711 [-20.55, 82.50]
4712 [-17.56, 82.00]
4713 [-12.63, 81.22]
4714 [-0.11, 80.75]
4715 [11.55, 81.22]
4716 [18.27, 82.00]
4717 [19.82, 82.50]
4718 [22.48, 83.00]
4719 [27.90, 83.50]
4720 [29.31, 84.00]
4721 [30.81, 84.50]
4722 [32.51, 85.00]
4723 *%-----|-----
4724 *#*****
4725 *# Catchment DESIRE
4726 *# - To Jock River (north of the Jock)
4727 *# - Rural-estate subdivision (Heart's Desire Community)
4728 *#*****
4729 CONTINUOUS STANDHYD NHYD=["DESIRE"], DT=[1]min, AREA=[23.78](ha),
4730 XI MP=[0.25], TI MP=[0.25], DWF=[0](cms), LOSS=[2],
4731 SCS curve number CN=[77],
4732 Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4733 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4734 Impervious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
4735 LGI=[400](m), MNI=[0.013], SCI=[0](min),
4736 Continuous simulation parameters:
4737 I a REC per=[4](hrs), I a REC i mp=[4](hrs),
4738 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4739 I n t e r E v e n t T i m e=[18](hrs), E N D=-1
4740 *%-----|-----
4741 *#*****
4742 *# Catchment JOCKVA
4743 *# - To Jockvale SWM Facility
4744 *# - Residential development & golf course
4745 *# - JFSA 2021-01-11 update JOCKVA after updating CORRIG as per IBI GROUP, July 2008.
4746 *# JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two
areas JOCKVA and EX-LAND 32.5 ha as per IBI GROUP, July 2008.
4747 *#*****
4748 CONTINUOUS STANDHYD NHYD=["JOCKVA"], DT=[1]min, AREA=[225.13](ha),
4749 XI MP=[0.50], TI MP=[0.50], DWF=[0](cms), LOSS=[2],
4750 SCS curve number CN=[74],
4751 Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4752 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4753 Impervious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
4754 LGI=[1310.55](m), MNI=[0.013], SCI=[0](min),
4755 Continuous simulation parameters:
4756 I a REC per=[4](hrs), I a REC i mp=[4](hrs),
4757 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4758 I n t e r E v e n t T i m e=[18](hrs), E N D=-1
4759 *%-----|-----

```

```

4760 ADD HYD          NHYDs um=[" J OCKVA- TO' ], NHYDs t o
add=[" EX- LAND- MN" +" J OCKVA" +" B2- M" +" B3- M" ]
4761 *%-----|-----|
4762 SAVE HYD         NHYD=[" J OCKVA- TO' ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
4763 HYD_COMMENT=[" Total Flows at KB first pond" ]
4764 *%-----|-----|
4765 *#*****|-----|
4766 *#   Jockvale SWM Facility
4767 *#   - Rating curve obtained from Jockvale Servicing Study (CCL 1999)
4768 *#*****|-----|
4769 ROUTE RESERVOIR  NHYDout =[" J OCK_P" ], NHYDi n=[" J OCKVA- TO' ],
4770 RDT=[ 1 ] ( mi n ),
4771             TABLE of ( OUTFLOW STORAGE ) values
4772             ( cms ) - ( ha- m )
4773             [ 0.0 , 0.0 ]
4774             [ 0.27 , 0.03 ]
4775             [ 0.28 , 0.55 ]
4776             [ 0.29 , 1.14 ]
4777             [ 0.30 , 1.80 ]
4778             [ 0.31 , 2.32 ]
4779             [ 1.12 , 2.87 ]
4780             [ 2.92 , 3.45 ]
4781             [ 4.64 , 4.07 ]
4782             [ 6.69 , 4.72 ]
4783             [ 9.02 , 5.39 ]
4784             [ 11.62 , 6.10 ]
4785             [ 14.42 , 6.85 ]
4786             [ 17.45 , 7.62 ]
4787             [ 20.69 , 8.44 ]
4788             [ 24.08 , 9.28 ]
4789             [ 27.68 , 10.17 ]
4790             [ -1 , -1 ] (max t went y pts)
4791             NHYDovf=[" J O- OVF" ]
4792 *%-----|-----|
4793 ADD HYD          NHYDs um=[" SN_DE" ], NHYDs t o add=[" N_DE" +" DESI RE" +" J O- OVF" +" J OCK_P" ]
4794 *%-----|-----|
4795 SAVE HYD         NHYD=[" SN_DE" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
4796 HYD_COMMENT=[" Total Flows at Heart's Desire" ]
4797 *%-----|-----|
4798 *#
4799 *# Hydrograph from Heart's Desire routed to Rideau River
4800 *# Channel X-Section obtained from RVCA Hydraulic Mdel - Station 0
4801 *#
4802 ROUTE CHANNEL    NHYDout =[" NI " ] , NHYDi n=[" SN_DE" ] ,
4803 RDT=[ 1 ] ( mi n ),
4804 CHLGTH=[ 563 ] ( m ), CHSLOPE=[ 0.9668 ] ( % ),
4805                      FPSLOPE=[ 0.9668 ] ( % ),
4806 SECNUM=[ 1.0 ], NSEG=[ 3 ]
4807 ( SEGROUGH, SEGDI ST ( m ) ) =
4808 [ 0.075, -30.20
4809 -0.045, 30.20
4810 0.075, 48.48 ] NSEG t i m e s
4811 ( DI STANCE ( m ), ELEVATI ON ( m ) ) =
4812 [ -98.46, 81.50 ]
4813 [ -92.24, 81.00 ]
4814 [ -86.88, 80.50 ]
4815 [ -81.54, 80.00 ]
4816 [ -74.36, 79.50 ]
4817 [ -63.54, 79.00 ]
4818 [ -39.23, 78.50 ]
4819 [ -34.51, 78.00 ]
4820 [ -33.01, 77.50 ]
4821 [ -30.20, 77.00 ]
4822 [ -13.42, 76.18 ]
4823 [ -1.14, 76.09 ]
4824 [ 17.06, 76.18 ]

```

```

4825 [ 30.20, 77.00]
4826 [ 32.95, 77.50]
4827 [ 34.06, 78.00]
4828 [ 35.11, 78.50]
4829 [ 36.32, 79.00]
4830 [ 37.74, 79.50]
4831 [ 48.48, 81.50]
4832 *%-----|-----|
4833 *#*****|
4834 *# Catchment S-2
4835 *# - To Jock River (north and south)
4836 *# - Undeveloped floodplain and river
4837 *#*****|
4838 CONTINUOUS NASHYD NHYD=[ "S-2" ], DT=[ 1 ] mi n, AREA=[ 102.94 ] ( ha ),
4839 DWF=[ 0 ] ( cms ), CNVC=[ 72 ], IA=[ 4.67 ] ( mm ),
4840 N=[ 3 ], TP=[ 0.40 ] hrs,
4841 Continuous simulation parameters:
4842 IaRECper=[ 4 ] ( hrs ),
4843 SMN=[ - 1 ] ( mm ), SMAX=[ - 1 ] ( mm ), SK=[ 0.010 ] / ( mm ),
4844 InterEventTime=[ 12 ] ( hrs )
4845 Baseflow simulation parameters:
4846 BaseFlowOption=[ 1 ] ,
4847 InitGWResVol=[ 50 ] ( mm ), GWResK=[ 0.96 ] ( mm / day / mm )
4848 VHydCond=[ 0.055 ] ( mm / hr ), END=- 1
4849 *%-----|-----|
4850 ADD HYD NHYDs um=[ "SN_NI" ], NHYDs to add=[ "NI"+"S-2" ]
4851 *%-----|-----|
4852 SAVE HYD NHYD=[ "SN_NI" ], # OF PCYCLES=[ - 1 ], ICASEsh=[ 1 ]
4853 HYD_COMMENT=[ "Total Flows at Rideau River" ]
4854 *%-----|-----|
4855 *#####|
4856 *% 5 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4857 START TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 5 ]
4858 *% ["C24SC005.stm"] <--storm filename, one per line for NSTORMtime
4859 *%-----|-----|
4860 *% 10 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4861 START TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 10 ]
4862 *% ["C24SC010.stm"] <--storm filename, one per line for NSTORMtime
4863 *%-----|-----|
4864 *% 25 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4865 START TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 25 ]
4866 *% ["C24SC025.stm"] <--storm filename, one per line for NSTORMtime
4867 *%-----|-----|
4868 *% 50 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4869 START TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 50 ]
4870 *% ["C24SC050.stm"] <--storm filename, one per line for NSTORMtime
4871 *%-----|-----|
4872 *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4873 *START TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 100 ]
4874 *% ["100YC3H.STM"] <--storm filename, one per line for NSTORMtime
4875 *%-----|-----|
4876 *% 100 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4877 START TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 100 ]
4878 *% ["C24SC100.stm"] <--storm filename, one per line for NSTORMtime
4879 *%-----|-----|
4880 *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4881 *START TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 100 ]
4882 *% ["C24SC100.stm"] <--storm filename, one per line for NSTORMtime
4883 *START TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 101 ]
4884 *% ["A24SC100.stm"] <--storm filename, one per line for NSTORMtime
4885 *START TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 102 ]
4886 *% ["A24SC100_60.stm"] <--storm filename, one per line for NSTORMtime
4887 FINISH
4888

```


Table of hydrograph data for Node 11, including sections for subwatersheds 7, 8, and 9. Columns include node ID, section, name, flow date, and volume. Includes entries like 029932, 029948, 029980, etc.

Table of hydrograph data for Node 2, including sections for subwatersheds 10, 11, and 12. Columns include node ID, section, name, flow date, and volume. Includes entries like 031800, 031811, 031822, etc.

Table with multiple columns containing alphanumeric codes (e.g., 03741, R005), descriptions (e.g., [MS] OMS offset, 5004E04), and numerical data points. The table lists various engineering or surveying data points across multiple rows.

059855 ROUTE RESERVOIR -> 1.0 0:02:ST: 5.9 0.075 No.date 28:00 38.69 n/a 0.000
059856 over flow ca 1.0 0:01:ST:STR 5.9 0.052 No.date 28:00 38.69 n/a 0.000
059857 over flow ca 1.0 0:03:ST:OPF 0.0 0.000 No.date 0:00 0.00 n/a 0.000
059858 [MS stoked=2359E+00] nb. TotOfVol=0.000E+00 nb. N.Of=0 0. TotDurOf= 0 hrs.]
059859 ROUTE10:CO1002-----DfIn n-ID NND-----AREHA-QPEAKm-TPrakDte,hb,mm-----Rvmm R.C-----DWfmm
059900 CONTNLUKES NANSHID 1.0 0:01:ST: 4.5 0.055 857 No.date 29:04 22.40 34.60 0.000
059901 [Cn# 4.0; No. 3.00; Tm= 10.0]
059902 [Iarc# 4.0; iARcPep# 4.0]
059903 [Iarc# 4.0; iARcPep# 4.0]
059904 ROUTE10:CO1003-----DfIn n-ID NND-----AREHA-QPEAKm-TPrakDte,hb,mm-----Rvmm R.C-----DWfmm
059905 ROUTE10:CO1003-----DfIn n-ID NND-----AREHA-QPEAKm-TPrakDte,hb,mm-----Rvmm R.C-----DWfmm
059906 [RDE 1.0] out ca 1.0 0:01:OP:PE 60.55 852 No.date 29:08 22.40 40 0.000
059907 [L/S n= 335 / 100 / 033]
059908 [Vnma = 1.0; Dmax = 44.7]
059909 [KDE 1.0; VDI= 1.0]
060000 ROUTE10:CO1004-----DfIn n-ID NND-----AREHA-QPEAKm-TPrakDte,hb,mm-----Rvmm R.C-----DWfmm
060001 ADD HYD 1.0 0:02:BR:NI 261.31 2.972 No.date 28:31 17.14 n/a 0.000
060002 over flow ca 1.0 0:02:ST: 1.17 0.68 No.date 28:12 29.30 n/a 0.000
060003 over flow ca 1.0 0:02:STR 3.51 1.139 No.date 28:50 50.29 n/a 0.000
060004 over flow ca 1.0 0:02:AL:OPF 0.0 0.000 No.date 0:00 0.00 n/a 0.000
060005 over flow ca 1.0 0:02:STR 3.51 1.139 No.date 28:50 50.29 n/a 0.000
060006 over flow ca 1.0 0:02:ST:OPF 0.0 0.000 No.date 0:00 0.00 n/a 0.000
060007 over flow ca 1.0 0:02:OP:PE 60.55 852 No.date 29:08 22.40 40 0.000
060008 SIM 1.0 0:01:ST:1:N 326.12 3.771 No.date 28:40 18.45 n/a 0.000
060009 ROUTE10:CO1002-----DfIn n-ID NND-----AREHA-QPEAKm-TPrakDte,hb,mm-----Rvmm R.C-----DWfmm
060100 CONTNLUKES STANHYD 1.0 0:01:ST: 4.5 0.058 No.date 28:01 50.29 77.77 0.000
060101 [X MP= 68; T IMP= 85]
060102 [Iarc# 4.0; iARcPep# 4.0]
060103 [Iarc# 4.0; iARcPep# 4.0]
060104 [Iarc# 4.0; iARcPep# 4.0]
060105 [Iarc# 4.0; iARcPep# 4.0]
060106 ROUTE10:CO1003-----DfIn n-ID NND-----AREHA-QPEAKm-TPrakDte,hb,mm-----Rvmm R.C-----DWfmm
060107 ROUTE10:CO1003-----DfIn n-ID NND-----AREHA-QPEAKm-TPrakDte,hb,mm-----Rvmm R.C-----DWfmm
060108 over flow ca 1.0 0:01:AC:STR 3.51 1.139 No.date 28:50 50.29 n/a 0.000
060109 over flow ca 1.0 0:01:AC:STR 3.51 1.139 No.date 28:50 50.29 n/a 0.000
060110 over flow ca 1.0 0:01:AC:STR 3.51 1.139 No.date 28:50 50.29 n/a 0.000
060111 over flow ca 1.0 0:01:AC:STR 3.51 1.139 No.date 28:50 50.29 n/a 0.000
060112 over flow ca 1.0 0:01:AC:STR 3.51 1.139 No.date 28:50 50.29 n/a 0.000
060113 over flow ca 1.0 0:01:AC:STR 3.51 1.139 No.date 28:50 50.29 n/a 0.000
060114 over flow ca 1.0 0:01:AC:STR 3.51 1.139 No.date 28:50 50.29 n/a 0.000
060115 over flow ca 1.0 0:01:AC:STR 3.51 1.139 No.date 28:50 50.29 n/a 0.000
060116 over flow ca 1.0 0:01:AC:STR 3.51 1.139 No.date 28:50 50.29 n/a 0.000
060117 over flow ca 1.0 0:01:AC:STR 3.51 1.139 No.date 28:50 50.29 n/a 0.000
060118 over flow ca 1.0 0:01:AC:STR 3.51 1.139 No.date 28:50 50.29 n/a 0.000
060119 over flow ca 1.0 0:01:AC:STR 3.51 1.139 No.date 28:50 50.29 n/a 0.000
060120 over flow ca 1.0 0:01:AC:STR 3.51 1.139 No.date 28:50 50.29 n/a 0.000
060121 [Iarc# 4.0; iARcPep# 4.0]
060122 [Iarc# 4.0; iARcPep# 4.0]
060123 [Iarc# 4.0; iARcPep# 4.0]
060124 [Iarc# 4.0; iARcPep# 4.0]
060125 [Iarc# 4.0; iARcPep# 4.0]
060126 [Iarc# 4.0; iARcPep# 4.0]
060127 [Iarc# 4.0; iARcPep# 4.0]
060128 [Iarc# 4.0; iARcPep# 4.0]
060129 [Iarc# 4.0; iARcPep# 4.0]
060130 [Iarc# 4.0; iARcPep# 4.0]
060131 [Iarc# 4.0; iARcPep# 4.0]
060132 [Iarc# 4.0; iARcPep# 4.0]
060133 [Iarc# 4.0; iARcPep# 4.0]
060134 [Iarc# 4.0; iARcPep# 4.0]
060135 [Iarc# 4.0; iARcPep# 4.0]
060136 [Iarc# 4.0; iARcPep# 4.0]
060137 [Iarc# 4.0; iARcPep# 4.0]
060138 [Iarc# 4.0; iARcPep# 4.0]
060139 [Iarc# 4.0; iARcPep# 4.0]
060140 [Iarc# 4.0; iARcPep# 4.0]
060141 [Iarc# 4.0; iARcPep# 4.0]
060142 [Iarc# 4.0; iARcPep# 4.0]
060143 [Iarc# 4.0; iARcPep# 4.0]
060144 [Iarc# 4.0; iARcPep# 4.0]
060145 [Iarc# 4.0; iARcPep# 4.0]
060146 [Iarc# 4.0; iARcPep# 4.0]
060147 [Iarc# 4.0; iARcPep# 4.0]
060148 [Iarc# 4.0; iARcPep# 4.0]
060149 [Iarc# 4.0; iARcPep# 4.0]
060150 [Iarc# 4.0; iARcPep# 4.0]
060151 [Iarc# 4.0; iARcPep# 4.0]
060152 [Iarc# 4.0; iARcPep# 4.0]
060153 [Iarc# 4.0; iARcPep# 4.0]
060154 [Iarc# 4.0; iARcPep# 4.0]
060155 [Iarc# 4.0; iARcPep# 4.0]
060156 [Iarc# 4.0; iARcPep# 4.0]
060157 [Iarc# 4.0; iARcPep# 4.0]
060158 [Iarc# 4.0; iARcPep# 4.0]
060159 [Iarc# 4.0; iARcPep# 4.0]
060160 [Iarc# 4.0; iARcPep# 4.0]
060161 [Iarc# 4.0; iARcPep# 4.0]
060162 [Iarc# 4.0; iARcPep# 4.0]
060163 [Iarc# 4.0; iARcPep# 4.0]
060164 [Iarc# 4.0; iARcPep# 4.0]
060165 [Iarc# 4.0; iARcPep# 4.0]
060166 [Iarc# 4.0; iARcPep# 4.0]
060167 [Iarc# 4.0; iARcPep# 4.0]
060168 [Iarc# 4.0; iARcPep# 4.0]
060169 [Iarc# 4.0; iARcPep# 4.0]
060170 [Iarc# 4.0; iARcPep# 4.0]
060171 [Iarc# 4.0; iARcPep# 4.0]

Table with columns for line numbers and detailed engineering notes. The table contains hundreds of entries, each with a unique line number (e.g., 063589, 063590) and a corresponding descriptive note. The notes specify engineering parameters such as 'Interp area', 'Slope', 'Material', and 'Remarks'. The entries are organized into sections, often separated by dashed lines, and include detailed calculations and specifications for various civil engineering projects.


```

078555 # Rating curve obtained from CCL hydraulic modeling
078560 *****
078570 ROUTE CHANNEl -> DfIn n-1D NND ..... AREhA-QPEAkM-TPEAkDtE.hh.m ..... RvM R.C. .... DfWm
078580 ROUTE RESERVOIR -> 1.0 01:SN.M 175.99 12.212 Ndate 28.07 36.76 n/a 0.00
078590 out <= 1.0 01:ML.P 175.99 4.030 Ndate 28.43 36.76 n/a 0.00
078600 overflow <= 1.0 03:ML.OV 0.00 0.00 Ndate 0.00 0.00 n/a 0.00
078610 [MSI:okded=4673]Vol. m3 TotOfVol=0000E+00 m3 NOf= 0. TotDurOf= 0 hrs.]
078620 R010: C00390 -> DfIn n-1D NND ..... AREhA-QPEAkM-TPEAkDtE.hh.m ..... RvM R.C. .... DfWm
078630 ADD HYD ..... 55194.86 85.786 Ndate 37.17 23.16 n/a 0.00
078640 + 1.0 02:ML.OV 0.00 0.00 Ndate 0.00 0.00 n/a 0.00
078650 + 1.0 02:SN.M 55194.86 85.786 Ndate 37.17 23.16 n/a 0.00
078660 SIMM ..... 55194.86 85.786 Ndate 37.17 23.16 n/a 0.00
078670 R010: C00391 -> DfIn n-1D NND ..... AREhA-QPEAkM-TPEAkDtE.hh.m ..... RvM R.C. .... DfWm
078680 SAVE HYD ..... 55194.86 85.786 Ndate 37.17 23.16 n/a 0.00
078690 *****
078700 *****
078710 *****
078720 *****
078730 *****
078740 *****
078750 *****
078760 *****
078770 *****
078780 *****
078790 *****
078800 *****
078810 *****
078820 *****
078830 *****
078840 *****
078850 *****
078860 *****
078870 *****
078880 *****
078890 *****
078900 *****
078910 *****
078920 *****
078930 *****
078940 *****
078950 *****
078960 *****
078970 *****
078980 *****
078990 *****
079000 *****
079010 *****
079020 *****
079030 *****
079040 *****
079050 *****
079060 *****
079070 *****
079080 *****
079090 *****
079100 *****
079110 *****
079120 *****
079130 *****
079140 *****
079150 *****
079160 *****
079170 *****
079180 *****
079190 *****
079200 *****
079210 *****
079220 *****
079230 *****
079240 *****
079250 *****
079260 *****
079270 *****
079280 *****
079290 *****
079300 *****
079310 *****
079320 *****
079330 *****
079340 *****
079350 *****
079360 *****
079370 *****
079380 *****
079390 *****
079400 *****
079410 *****
079420 *****
079430 *****
079440 *****
079450 *****
079460 *****
079470 *****
079480 *****
079490 *****
079500 *****
079510 *****
079520 *****
079530 *****
079540 *****
079550 *****
079560 *****
079570 *****
079580 *****
079590 *****
079600 *****
079610 *****
079620 *****
079630 *****
079640 *****
079650 *****
079660 *****
079670 *****
079680 *****
079690 *****
079700 *****
079710 *****
079720 *****
079730 *****
079740 *****
079750 *****
079760 *****
079770 *****
079780 *****
079790 *****
079800 *****
079810 *****
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082729 # [MS0105da-1192E03 ml]
082730 #
082731 R0025: C00034 DfIn a-ID NND AREAh-QPEAGcm-TpeakDte,hb,mm Rvmm R.C. DfCwm
082732 SAVE HYD 1.0 01:RES_GM 7725.00 3.678_NDate 60:27 23.52 n/a 0000
082733 # name : H_RESGM
082734 # remark : Outflow from Res GM
082735 # Output of Reservoir Groundwater cross-section from Node 13A to Node 12
082736 # (Approximated cross-section - see cross-section 258)

084166 ADD HYD 1.0 02:SA 54509.01 62.487_NDate 34:43 27.43 n/a 0000
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Table with columns for ID, description, and numerical data. Includes entries for catchment areas, road sections, and various engineering parameters.

093511	R0025	C00202	-----	Dfm-n 1-D NDD	-----	AREHA-QPEAKm-Tpeaktide-hh:mm	-----	Rvmm-R C	-----	0000
093512										
093513										
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093532										
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093536										
093537										

Table with multiple columns containing alphanumeric codes, descriptions, and numerical values. The table lists various engineering or project entries, such as '097255 [SM No. 26.32: SMW0175.50, SKG - 010]', '097256 R0025: C00266', and '097257 COMPUTE DUAL/D'. Each entry includes detailed specifications and associated data points.

Table with multiple columns containing technical specifications, codes, and numerical values. Includes headers like 'CONTINUES NASSHD', 'CONTINUES STANSHHD', and various parameters like 'Fw', 'L', 'M', 'N', 'S', 'C', 'D'. Rows represent different data entries with varying levels of detail.

Table with columns for ID, description, parameters, and values. Includes entries for various hydrograph and channel sections, such as 'Hydrograph from Node Foster SWM1 Station 98010 Node at station 520' and 'Channel X-Section obtained from RWCA Hydraulic Model - Station 980'.

Table with columns: Line Number, Description, and Data. The table contains a dense list of engineering notes and calculations, including flow rates, pipe specifications, and stationing details. It is organized into two columns of text.

Table with columns for ID, description, and values. Contains a large list of system components and their parameters, such as R0505:CO0355, R0505:CO0356, etc., with associated numerical and text data.

Table with multiple columns containing alphanumeric codes (e.g., 134655, 134656), descriptions (e.g., ADD HYD, ROUTE CHANNEL), and numerical data (e.g., 3680.00, 21.616, 36.52, 35.18). The table lists various hydrograph and channel routing details for different nodes and sections.

Table with multiple columns: ID, Description, Parameters (e.g., Flow, Pressure, Temperature), Units, and Status. The table lists various equipment and their operational settings across different sections of a facility.

149611	Major System /	1.0	0.02:FR-02-MJ	0.02	0.087	Nu.date	28:03	64.85	n/a	.000
149628	Minor System /	1.0	0.02:FR-02-MJ	1.37	1.153	Nu.date	27:44	65.34	n/a	.000
149633	[M]SysSto=1530E03, TotOfVol=Nu=1375E02, NcOf=	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
149640	ADD HYD	1.0	0.02:FR-02-MJ	0.02	0.087	Nu.date	28:03	64.85	n/a	.000
149655	ROUTERESERV >	1.0	0.02:FR-02-MJ	0.02	0.087	Nu.date	28:03	64.85	n/a	.000
149666	ROUTERESERV <	1.0	0.02:FR-02-MJ	1.57	1.153	Nu.date	27:44	65.34	n/a	.000
149675	SIMM	1.0	0.01:FR-02-MJ	1.39	1.153	Nu.date	28:03	65.34	n/a	.000
149689	Catchment FRASER									
149700	- To Fraser-Clarke drain (north of the Jack)									
149710	- Developed land with assumed 4% imp									
149725	- 2020-12-17 Change Fringe area to be 35.1 as measured from QGIS									
149735	- 2020-12-17 All Fraser is undeveloped (Nashby)									
149745	CONTINUES STANBYD 1.0 01:TOOD-MJ	1.0	0.01:TOOD-MJ	3.15	3.87	Nu.date	28:21	45.95	519	.000
149750	[X]Mps: 53:TI.Mps: 57]									
149755	[L]Sls: 2 :Cn: 77.0]									
149760	ROUTERESERV >	1.0	0.02:FR-02-MJ	0.02	0.087	Nu.date	28:03	64.85	n/a	.000
149765	ROUTERESERV <	1.0	0.02:FR-02-MJ	1.57	1.153	Nu.date	27:44	65.34	n/a	.000
149770	SIMM	1.0	0.01:FR-02-MJ	1.39	1.153	Nu.date	28:03	65.34	n/a	.000
149785	Catchment TODD									
149790	- To Todd Drain (south of the Jack)									
149800	- Subdivided with assumed 4% imp									
149810	- 2020-11-30 increase imp. based on P598(04)-11									
149820	- 2020-11-30 update tributary Drainage Area to 146.015 ha based on P598(04)-11									
149830	- 2020-11-30 update TODD Drainage Area to 146.015 ha based on P598(04)-11									
149840	- 2020-11-30 update TODD Drainage Area to 146.015 ha based on P598(04)-11									
149850	JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GCS measurements									
149860	JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GCS measurements									
149870	JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GCS measurements									
149880	JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GCS measurements									
149890	JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GCS measurements									
149900	JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GCS measurements									
149910	JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GCS measurements									
149920	JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GCS measurements									
149930	JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GCS measurements									
149940	JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GCS measurements									
149950	JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GCS measurements									
149960	JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GCS measurements									
149970	JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GCS measurements									
149980	JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GCS measurements									
149990	JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GCS measurements									
150000	JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GCS measurements									

Table with multiple columns containing technical specifications, codes, and numerical data. The table is organized in vertical columns and contains numerous rows of alphanumeric information.

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157099 + 1.0 02:40:M 0.00 0.00 No.date 0.00 0.00 n/a 0.00
157109 + 1.0 02:40:M 0.09 218 No.date 28.05 59.73 n/a 0.00
157113 + 1.0 02:41:M 16 564 No.date 28.06 67.38 n/a 0.00
157123 + 1.0 02:41:M 23 599 No.date 28.05 62.88 n/a 0.00
157133 + 1.0 02:43:M 0.00 0.00 No.date 0.00 0.00 n/a 0.00
157143 + 1.0 01:corr 5520.08 145.505 No.date 36:37 39.46 n/a 0.00
157153 R0100:CO0386.....Dfm n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm.....Rvsm R.C.....DWcm
157163 SAVE HYD 1.0 01:corr 5520.08 145.505 No.date 36:37 39.46 n/a 0.00
157173 fname : corr 0100
157183 remark: Total Flow at Corrigan Pond
157193 *****
157203 # Corrigan Pond 1
157213 # Rating curve obtained from Barrhaven South MS modeling
157223 # Tributary Drainage at Corrigan Pond 1 - 145 ha
157233 *****
157243 #
157253 # Hydrograph from Corrigan Drain routed to Jockvale Road
157263 # Channel X-Section obtained from RCVA Hydraulic Model - Station 2462
157273 *****
157283 R0100:CO0387.....Dfm n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm.....Rvsm R.C.....DWcm
157293 ROUTE CHANNEL -> 1.0 02:SN,DE 5520.08 145.490 No.date 36:40 39.46 n/a 0.00
157303 |R/S/n= 580 / 447.045|
157313 |X/M= 2.170; Dmax= 2.124|
157323 *****
157333 # Catchment MLLS
157343 # To SWM Facility north of the Lock
157353 # Primarily residential development
157363 *****
157373 R0100:CO0388.....Dfm n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm.....Rvsm R.C.....DWcm
157383 CONTINUOUS STANHYD 1.0 01:MLLS 175.99 20.390 No.date 28:06 56.87 642 000
157393 |X/M= 38.718; T= 38|
157403 |L/S/n= 2. CN= 74.0|
157413 #
157423 |Previous area: IArea 4.67; SLP=4.00; LQ= 40.; MPM= 250; SCP= 0|
157433 |Impervious area: IArea 1.57; SLP=1.00; LQ=1118.; MN= 013; SCL= 0|
157443 |IARECmp= 4.00; IARECper= 4.00|
157453 |SM.N= 36.67; SMM=244.49; SK= 010|
157463 *****
157473 # Chappin Mills SWM Pond
157483 # Rating curve obtained from CCL hydraulic modeling
157493 *****
157503 R0100:CO0389.....Dfm n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm.....Rvsm R.C.....DWcm
157513 ROUTE RESERVOIR -> 1.0 02:MLLS 175.99 20.390 No.date 28:06 56.87 n/a 0.00
157523 out = 1.0 01:MLL,P 146.22 4.050 No.date 28:08 56.87 n/a 0.00
157533 |overFlow= 2310E+01; TotDrfVol= 1693E+01; N.O.drf= 2; TotDrfOut= 1; hrs|
157543 |MS.oblck= 2310E+01; N.O.drf= 2; TotDrfVol= 1693E+01; N.O.drf= 2; TotDrfOut= 1; hrs|
157553 *****
157563 ADD HYD + 1.0 02:SN,DE 5520.08 145.490 No.date 36:40 39.46 n/a 0.00
157573 + 1.0 02:MLL,OV 29.77 16.228 No.date 28:08 56.87 n/a 0.00
157583 + 1.0 02:MLL,OV 146.22 4.050 No.date 28:08 56.87 n/a 0.00
157593 SUM + 1.0 01:SN,DE 55196.07 146.161 No.date 36:39 39.51 n/a 0.00
157603 R0100:CO0391.....Dfm n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm.....Rvsm R.C.....DWcm
157613 SAVE HYD 1.0 01:SN,DE 55196.07 146.161 No.date 36:39 39.51 n/a 0.00
157623 fname : SN,DE 0100
157633 remark: Total Flow at Jockvale Road
157643 #
157653 # Hydrograph from Jockvale Road routed to Heart's Desire
157663 # Channel X-Section obtained from RCVA Hydraulic Model - Station 689
157673 *****
157683 R0100:CO0392.....Dfm n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm.....Rvsm R.C.....DWcm
157693 ROUTE CHANNEL -> 1.0 02:SN,DE 55196.07 146.161 No.date 36:39 39.51 n/a 0.00
157703 |R/S/n= 1902 / 2271.045|
157713 |X/M= 1.000; Dmax= 2.691|
157723 *****
157733 # Catchment DESIRE
157743 # To Jock River (north of the Lock)
157753 # Rural estate subdivision (Heart's Desire Community)
157763 *****
157773 R0100:CO0393.....Dfm n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm.....Rvsm R.C.....DWcm
157783 CONTINUOUS STANHYD 1.0 01:DESIRE 23.78 3.004 No.date 28:03 53.11 600 000
157793 |X/M= 25.718; T= 25|
157803 |L/S/n= 2. CN= 77.0|
157813 #
157823 |Previous area: IArea 4.67; SLP=4.00; LQ= 40.; MPM= 250; SCP= 0|
157833 |Impervious area: IArea 1.57; SLP=1.00; LQ= 400.; MN= 013; SCL= 0|
157843 |IARECmp= 4.00; IARECper= 4.00|
157853 |SM.N= 31.15; SMM=207.66; SK= 010|
157863 *****
157873 # Catchment JOCKVA
157883 # To Jockvale SWM Facility
157893 # Residential development & golf course
157903 # JFSA 2021-01-11 update JOCKVA after updating CURRGAS per IBI GROUP July 2008.
157913 # JOCKVA area increased from 257.62 ha JOCKVA separated into two areas JOCKVA and EX LAND 32.5 ha as
157923 *****
157933 R0100:CO0394.....Dfm n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm.....Rvsm R.C.....DWcm
157943 CONTINUOUS STANHYD 1.0 01:JOCKVA 225.13 28.623 No.date 28:07 62.70 708 000
157953 |X/M= 50.718; T= 50|
157963 |L/S/n= 2. CN= 74.0|
157973 |Previous area: IArea 4.67; SLP=4.00; LQ= 40.; MPM= 250; SCP= 0|
157983 |Impervious area: IArea 1.57; SLP=1.00; LQ=1311.; MN= 013; SCL= 0|
157993 |IARECmp= 4.00; IARECper= 4.00|
158003 |SM.N= 36.67; SMM=244.49; SK= 010|
158013 R0100:CO0395.....Dfm n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm.....Rvsm R.C.....DWcm
158023 ADD HYD + 1.0 02:EX LAND AN 30.73 2.275 No.date 27:48 62.82 n/a 0.00
158033 + 1.0 02:EX LAND AN 225.13 28.623 No.date 28:07 62.70 n/a 0.00
158043 + 1.0 02:EX,DE 36 820 No.date 28:05 62.88 n/a 0.00
158053 + 1.0 02:EX,DE 19 402 No.date 28:04 62.88 n/a 0.00
158063 SUM + 1.0 01:JOCKVA,TO 256.41 31.850 No.date 28:06 62.71 n/a 0.00
158073 R0100:CO0396.....Dfm n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm.....Rvsm R.C.....DWcm
158083 SAVE HYD 1.0 01:JOCKVA,TO 256.41 31.850 No.date 28:06 62.71 n/a 0.00
158093 fname : JOCKVA,TO 0100
158103 remark: Total Flow at KB first pond
158113 *****
158123 # Jockvale SWM Facility
158133 # Rating curve obtained from Jockvale Servicing Study (CCL 1999)
158143 *****
158153 R0100:CO0397.....Dfm n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm.....Rvsm R.C.....DWcm
158163 ROUTE RESERVOIR -> 1.0 02:JOCKVA,TO 256.41 31.850 No.date 28:06 62.71 n/a 0.00
158173 |overFlow= 6430E+01; TotDrfVol= 0.0000E+00; N.O.drf= 0; TotDrfOut= 0; hrs|
158183 |MS.oblck= 6430E+01; N.O.drf= 0; TotDrfVol= 0.0000E+00; N.O.drf= 0; TotDrfOut= 0; hrs|
158193 *****
158203 R0100:CO0398.....Dfm n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm.....Rvsm R.C.....DWcm
158213 ADD HYD + 1.0 02:DE 55196.07 145.839 No.date 36:54 39.51 n/a 0.00
158223 + 1.0 02:DESIRE 23.78 3.004 No.date 28:03 53.11 n/a 0.00
158233 + 1.0 02:JO,OVF 0.00 0.00 No.date 0.00 0.00 n/a 0.00
158243 + 1.0 02:JO,OVF 256.41 12.850 No.date 28:35 62.71 n/a 0.00
158253 SUM + 1.0 01:SN,DE 55476.26 146.840 No.date 36:52 39.63 n/a 0.00
158263 R0100:CO0399.....Dfm n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm.....Rvsm R.C.....DWcm
158273 SAVE HYD 1.0 01:SN,DE 55476.26 146.840 No.date 36:52 39.63 n/a 0.00
158283 fname : SN,DE 0100
158293 remark: Total Flow at Heart's Desire
158303 #
158313 # Hydrograph from Heart's Desire routed to Rideau River
158323 # Channel X-Section obtained from RCVA Hydraulic Model - Station 0
158333 *****
158343 R0100:CO0400.....Dfm n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm.....Rvsm R.C.....DWcm
158353 ROUTE CHANNEL -> 1.0 02:SN,DE 55476.26 146.840 No.date 36:52 39.63 n/a 0.00
158363 |R/S/n= 1.001 n/c= 1.0 01:SN,DE 55476.26 146.826 No.date 36:55 39.63 n/a 0.00
158373 |L/S/n= 563 / 9677.045|
158383 |X/M= 2.138; Dmax= 1.328|
158393 *****
158403 # Catchment S-2
158413 # To Jock River (north and south)
158423 # Undeveloped floodplain and river
158433 *****
158443 R0100:CO0401.....Dfm n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm.....Rvsm R.C.....DWcm
158453 CONTINUOUS NSHYD 1.0 01:S-2 102.94 5.685 No.date 28:20 40.95 462 000
158463 |Cne 7= 2; Cne 3= 0; Tpe 4= 40|
158473 |IAREC= 4.00; SM.N= 39.75; SMM=264.99; SK= 010|
158483 *****
158493 R0100:CO0402.....Dfm n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm.....Rvsm R.C.....DWcm
158503 ADD HYD + 1.0 02:SN,DE 55476.26 146.826 No.date 36:55 39.63 n/a 0.00
158513 + 1.0 02:S-2 102.94 5.685 No.date 28:20 40.95 n/a 0.00
158523 SUM + 1.0 01:SN,DE 55579.20 147.102 No.date 36:55 39.63 n/a 0.00
158533 R0100:CO0403.....Dfm n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm.....Rvsm R.C.....DWcm
158543 SAVE HYD 1.0 01:SN,DE 55579.20 147.102 No.date 36:55 39.63 n/a 0.00
158553 fname : SN,DE 0100
158563 remark: Total Flow at Rideau River
158573 *****
158583 R0100:CO0002.....
158593 FINISH
158603 *****
158613 *****
158623 *****
158633 *****
158643 *****
158653 *****
158663 *****
158673 *****
158683 *****
158693 *****
158703 *****
158713 *****
158723 *****
158733 *****
158743 *****
158753 *****
158763 *****
158773 *****
158783 *****
158793 *****
158803 *****
158813 *****
158823 *****
158833 *****
158843 *****
158853 *****
158863 *****
158873 *****
158883 *****
158893 *****
158903 *****
158913 *****
158923 *****
158933 *****
158943 *****
158953 *****

```


Attachment E

Model 4B – Jock River Reach One Future Conditions – With SWM controls

JFSA, 2021

SWMHYMO Input & Summary files

```

1  20      Metric units / ID numbers OFF
2  *****
3  *# SWHYMO Ver: 5.02/Jan 2001 <BETA> / INPUT DATA FILE
4  *****
5  *# Project Name: [Jock River]      Project Number: [1474-16]
6  *# Date       : 04-03-2021
7  *# Modeller   : [MM]
8  *# Company    : JFSA Inc.
9  *# License #  : 2549237
10 *****
11 *# CALIBRATION OF SUMMER MODEL PARAMETERS
12 *# USING CONTINUOUS SIMULATIONS
13 *# Rainfall data from JFSA raingauge installed at site + other gauges by the City
14 *# Use data collected from May 1st to July 14, 2003
15 *# 2020-11-30 change TMSTO in COMPUTE DUALHYD (TMSTO = 0.1 instead of 0.0001)
16 *# 2020-12-01 correct pond curve values
17 *# 2020-12-01 change WCLAR_BRAZ_XIMP to 0.55, SLPI=[0.5](%) (impervious slope), and
18 LGI up to 700m
19 *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 2462 (NHYDout=["N_TO"]
20 ,NHYDin=["SN_TO"]) from 0.033 % (as per Stantec Report 2007) to 0.05 % so the model
21 will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELS
22 aren't well suited to really flat slopes.
23 *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHYDout=["N_WC"]
24 ,NHYDin=["SN_CE"]) from 0.01 % (as per Stantec Report 2007) to 0.0255 % so the model
25 will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELS
26 aren't well suited to really flat slopes.
27 *
28 * Calibrated parameters for Summer 2003 data: APII=50, APIK=0.85, CN=varies,
29 *                                               SK=0.01, InterEventTime=12,
30 *                                               GWResk=0.96, VHydCond=0.055
31 *
32 *# -----
33 *
34 *START          TZERO=[2003.0501], METOUT=[2], NSTORM=[1], NRUN=[001]
35 *              ["XAVG0315.STM"] average storm data a 15 minute time step
36 *              The above rainf file is an average of the JFSA gauge data
37 *              with the City of Ottawa rainfall data collected during
38 *              the same period.
39 *% 2 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
40 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[2]
41 ["C24SC002.stm"] <-- storm filename, one per line for NSTORM time
42 *%-----|-----|
43 *%-----|-----|
44 READ STORM     STORM_FILENAME=["storm 001"]
45 *%-----|-----|
46 MODIFY STORM   ICASEms=[1], NSHIFT=[96],
47 RedFACT=[1],
48 *%-----|-----|
49 DEFAULT VALUES ICASEdef=[1], read and print values
50 DEFVAL_FILENAME=["CitiGate.DEF"]
51 *%-----|-----|
52 *%-----|-----|
53 COMPUTE API     APII=[50], APIK=[.85]/day
54 *%-----|-----|
55 *%-----|-----|
56 *#
57 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
58 *# of 1.32
59 *%-----|-----|
60 CONTINUOUS NASHYD NHYD=["JR_HW"], DT=[1]min, AREA=[3680](ha),
61 DWF=[0](cms), CNVC=[64], IA=[2.5](mm),
62 N=[3.0], TP=[7.13]hrs,
63 Continuous simulation parameters:
64 IARECper=[4](hrs),
65 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
66 InterEventTime=[12](hrs)
67 Baseflow simulation parameters:

```

```

60 BaseFlowOption=[ 1] ,
61 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
62 VHydCond=[ 0.055](mm/hr), END=- 1
63 *%-----|-----
64 *#
65 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
66 *# of 1.32
67 *%-----|-----
68 CONTINUOUS NASHYD NHYD=[ "SW_13"], DT=[ 1]min, AREA=[ 971](ha),
69 DWF=[ 0](cms), CNVC=[ 61], IA=[ 2.5](mm),
70 N=[ 3.0], TP=[ 3.76]hrs,
71 Continuous simulation parameters:
72 IaRECper=[ 4](hrs),
73 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
74 InterEventTime=[ 12](hrs)
75 Baseflow simulation parameters:
76 BaseFlowOption=[ 1] ,
77 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
78 VHydCond=[ 0.055](mm/hr), END=- 1
79 *%-----|-----
80 *#
81 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
82 *# of 1.80
83 *%-----|-----
84 CONTINUOUS NASHYD NHYD=[ "JR_GWM"], DT=[ 1]min, AREA=[ 3074](ha),
85 DWF=[ 0](cms), CNVC=[ 55], IA=[ 2.5](mm),
86 N=[ 3], TP=[ 11.33]hrs,
87 Continuous simulation parameters:
88 IaRECper=[ 4](hrs),
89 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
90 InterEventTime=[ 12](hrs)
91 Baseflow simulation parameters:
92 BaseFlowOption=[ 1] ,
93 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
94 VHydCond=[ 0.055](mm/hr), END=- 1
95 *%-----|-----
96 CONTINUOUS NASHYD NHYD=[ "JR_ASH"], DT=[ 1]min, AREA=[ 1781](ha),
97 DWF=[ 0](cms), CNVC=[ 72], IA=[ 2.5](mm),
98 N=[ 3.0], TP=[ 3.91]hrs,
99 Continuous simulation parameters:
100 IaRECper=[ 4](hrs),
101 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
102 InterEventTime=[ 12](hrs)
103 Baseflow simulation parameters:
104 BaseFlowOption=[ 1] ,
105 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
106 VHydCond=[ 0.055](mm/hr), END=- 1
107 *%-----|-----
108 CONTINUOUS NASHYD NHYD=[ "SW_11"], DT=[ 1]min, AREA=[ 500](ha),
109 DWF=[ 0](cms), CNVC=[ 66], IA=[ 2.5](mm),
110 N=[ 3.0], TP=[ 1.24]hrs,
111 Continuous simulation parameters:
112 IaRECper=[ 4](hrs),
113 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
114 InterEventTime=[ 12](hrs)
115 Baseflow simulation parameters:
116 BaseFlowOption=[ 1] ,
117 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
118 VHydCond=[ 0.055](mm/hr), END=- 1
119 *%-----|-----
120 *#
121 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
122 *# of 1.80
123 *%-----|-----
124 CONTINUOUS NASHYD NHYD=[ "NN_CK"], DT=[ 1]min, AREA=[ 1917](ha),
125 DWF=[ 0](cms), CNVC=[ 66], IA=[ 2.5](mm),

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126 N=[ 3. 0], TP=[ 5. 29] hrs,
127 Continuous simulation parameters:
128 IaRECPper=[ 4] (hrs),
129 SMN=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
130 InterEventTime=[ 12] (hrs)
131 Baseflow simulation parameters:
132 BaseFlowOption=[ 1] ,
133 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
134 VHydCond=[ 0. 055] (mm/ hr), END=- 1
135 *%-----|-----
136 *#
137 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
138 *# of 1.52
139 *%-----|-----
140 CONTINUOUS NASHYD NHYD=[ "SW_10"], DT=[ 1] min, AREA=[ 5666] (ha),
141 DWF=[ 0] (cms), CNVC=[ 72], IA=[ 2. 5] (mm),
142 N=[ 3. 0], TP=[ 8. 00] hrs,
143 Continuous simulation parameters:
144 IaRECPper=[ 4] (hrs),
145 SMN=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
146 InterEventTime=[ 12] (hrs)
147 Baseflow simulation parameters:
148 BaseFlowOption=[ 1] ,
149 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
150 VHydCond=[ 0. 055] (mm/ hr), END=- 1
151 *%-----|-----
152 *#
153 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
154 *# of 1.75
155 *%-----|-----
156 CONTINUOUS NASHYD NHYD=[ "KG_CK"], DT=[ 1] min, AREA=[ 8376] (ha),
157 DWF=[ 0] (cms), CNVC=[ 66], IA=[ 2. 5] (mm),
158 N=[ 3. 0], TP=[ 11. 66] hrs,
159 Continuous simulation parameters:
160 IaRECPper=[ 4] (hrs),
161 SMN=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
162 InterEventTime=[ 12] (hrs)
163 Baseflow simulation parameters:
164 BaseFlowOption=[ 1] ,
165 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
166 VHydCond=[ 0. 055] (mm/ hr), END=- 1
167 *%-----|-----
168 *#
169 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
170 *# of 1.68
171 *%-----|-----
172 CONTINUOUS NASHYD NHYD=[ "SW_9"], DT=[ 1] min, AREA=[ 1132] (ha),
173 DWF=[ 0] (cms), CNVC=[ 70], IA=[ 2. 5] (mm),
174 N=[ 3. 0], TP=[ 2. 51] hrs,
175 Continuous simulation parameters:
176 IaRECPper=[ 4] (hrs),
177 SMN=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
178 InterEventTime=[ 12] (hrs)
179 Baseflow simulation parameters:
180 BaseFlowOption=[ 1] ,
181 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
182 VHydCond=[ 0. 055] (mm/ hr), END=- 1
183 *%-----|-----
184 *#
185 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
186 *# of 1.82
187 *%-----|-----
188 CONTINUOUS NASHYD NHYD=[ "NC_CK"], DT=[ 1] min, AREA=[ 4464] (ha),
189 DWF=[ 0] (cms), CNVC=[ 62], IA=[ 2. 5] (mm),
190 N=[ 3. 0], TP=[ 11. 32] hrs,
191 Continuous simulation parameters:

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192 IaREcper=[ 4] (hr s),
193 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
194 InterEventTime=[ 12] (hr s)
195 Baseflow simulation parameters:
196 BaseFlowOption=[ 1] ,
197 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
198 VHydCond=[ 0. 055] (mm/ hr), END=- 1
199 *%-----|-----
200 *#
201 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
202 *# of 1.80
203 *%-----|-----
204 CONTINUOUS NASHYD NHYD=[ "SW_8" ], DT=[ 1] mi n, AREA=[ 131] (ha),
205 DWF=[ 0] (cms), CN C=[ 63], IA=[ 2. 5] (mm),
206 N=[ 3. 0], TP=[ 0. 90] hr s,
207 Continuous simulation parameters:
208 IaREcper=[ 4] (hr s),
209 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
210 InterEventTime=[ 12] (hr s)
211 Baseflow simulation parameters:
212 BaseFlowOption=[ 1] ,
213 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
214 VHydCond=[ 0. 055] (mm/ hr), END=- 1
215 *%-----|-----
216 *#
217 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
218 *# of 1.65
219 *%-----|-----
220 CONTINUOUS NASHYD NHYD=[ "HB_DR" ], DT=[ 1] mi n, AREA=[ 3854] (ha),
221 DWF=[ 0] (cms), CN C=[ 66], IA=[ 2. 5] (mm),
222 N=[ 3. 0], TP=[ 8. 42] hr s,
223 Continuous simulation parameters:
224 IaREcper=[ 4] (hr s),
225 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
226 InterEventTime=[ 12] (hr s)
227 Baseflow simulation parameters:
228 BaseFlowOption=[ 1] ,
229 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
230 VHydCond=[ 0. 055] (mm/ hr), END=- 1
231 *%-----|-----
232 *#
233 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
234 *# of 1.82
235 *%-----|-----
236 CONTINUOUS NASHYD NHYD=[ "SW_7" ], DT=[ 1] mi n, AREA=[ 3197] (ha),
237 DWF=[ 0] (cms), CN C=[ 57], IA=[ 2. 5] (mm),
238 N=[ 3. 0], TP=[ 6. 65] hr s,
239 Continuous simulation parameters:
240 IaREcper=[ 4] (hr s),
241 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
242 InterEventTime=[ 12] (hr s)
243 Baseflow simulation parameters:
244 BaseFlowOption=[ 1] ,
245 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
246 VHydCond=[ 0. 055] (mm/ hr), END=- 1
247 *%-----|-----
248 *#
249 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
250 *# of 1.75
251 *%-----|-----
252 CONTINUOUS NASHYD NHYD=[ "SW_6" ], DT=[ 1] mi n, AREA=[ 165] (ha),
253 DWF=[ 0] (cms), CN C=[ 67], IA=[ 2. 5] (mm),
254 N=[ 3. 0], TP=[ 4. 18] hr s,
255 Continuous simulation parameters:
256 IaREcper=[ 4] (hr s),
257 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),

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258 InterEventTime=[ 12] (hrs)
259 Baseflow simulation parameters:
260 BaseFlowOption=[ 1] ,
261 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
262 VHydCond=[ 0.055] (mm/ hr), END=- 1
263 *%-----|-----
264 *#
265 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
266 *# of 1.67
267 *%-----|-----
268 CONTINUOUS NASHYD NHYD=[ "VG_DR" ], DT=[ 1] min, AREA=[ 1332] (ha),
269 DWF=[ 0] (cms), CNVC=[ 72], IA=[ 2.5] (mm),
270 N=[ 3.0], TP=[ 5.95] hrs,
271 Continuous simulation parameters:
272 IaRECper=[ 4] (hrs),
273 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
274 InterEventTime=[ 12] (hrs)
275 Baseflow simulation parameters:
276 BaseFlowOption=[ 1] ,
277 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
278 VHydCond=[ 0.055] (mm/ hr), END=- 1
279 *%-----|-----
280 CONTINUOUS NASHYD NHYD=[ "SW_5" ], DT=[ 1] min, AREA=[ 224] (ha),
281 DWF=[ 0] (cms), CNVC=[ 77], IA=[ 2.5] (mm),
282 N=[ 3.0], TP=[ 0.75] hrs,
283 Continuous simulation parameters:
284 IaRECper=[ 4] (hrs),
285 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
286 InterEventTime=[ 12] (hrs)
287 Baseflow simulation parameters:
288 BaseFlowOption=[ 1] ,
289 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
290 VHydCond=[ 0.055] (mm/ hr), END=- 1
291 *%-----|-----
292 *#
293 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
294 *# of 1.20
295 *%-----|-----
296 CONTINUOUS NASHYD NHYD=[ "FL_CK" ], DT=[ 1] min, AREA=[ 4945] (ha),
297 DWF=[ 0] (cms), CNVC=[ 74], IA=[ 2.5] (mm),
298 N=[ 3.0], TP=[ 4.45] hrs,
299 Continuous simulation parameters:
300 IaRECper=[ 4] (hrs),
301 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
302 InterEventTime=[ 12] (hrs)
303 Baseflow simulation parameters:
304 BaseFlowOption=[ 1] ,
305 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
306 VHydCond=[ 0.055] (mm/ hr), END=- 1
307 *%-----|-----
308 CONTINUOUS NASHYD NHYD=[ "SW_5A2" ], DT=[ 1] min, AREA=[ 20] (ha),
309 DWF=[ 0] (cms), CNVC=[ 81], IA=[ 2.5] (mm),
310 N=[ 3.0], TP=[ 0.62] hrs,
311 Continuous simulation parameters:
312 IaRECper=[ 4] (hrs),
313 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
314 InterEventTime=[ 12] (hrs)
315 Baseflow simulation parameters:
316 BaseFlowOption=[ 1] ,
317 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
318 VHydCond=[ 0.055] (mm/ hr), END=- 1
319 *%-----|-----
320 *#
321 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
322 *# of 1.61
323 *%-----|-----

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324 CONTI NUOUS NASHYD NYHD=["SW_5A1"], DT=[1] mi n, AREA=[1412] (ha),
325 DWF=[0] (cms), CNV C=[75], IA=[2. 5] (mm),
326 N=[3. 0], TP=[8. 00] hr s,
327 Continuous simulation parameters:
328 IaRECPper=[4] (hr s),
329 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
330 InterEventTime=[12] (hr s)
331 Baseflow simulation parameters:
332 BaseFlowOpti on=[1] ,
333 In it GWRes Vol = [50] (mm), GWRes K=[0. 96] (mm / day / mm)
334 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

336 CONTI NUOUS NASHYD NYHD=["SW_4"], DT=[1] mi n, AREA=[585] (ha),
337 DWF=[0] (cms), CNV C=[81], IA=[2. 5] (mm),
338 N=[3. 0], TP=[1. 75] hr s,
339 Continuous simulation parameters:
340 IaRECPper=[4] (hr s),
341 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
342 InterEventTime=[12] (hr s)
343 Baseflow simulation parameters:
344 BaseFlowOpti on=[1] ,
345 In it GWRes Vol = [50] (mm), GWRes K=[0. 96] (mm / day / mm)
346 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

348 CONTI NUOUS NASHYD NYHD=["LM_CK"], DT=[1] mi n, AREA=[1021] (ha),
349 DWF=[0] (cms), CNV C=[80], IA=[2. 5] (mm),
350 N=[3. 0], TP=[2. 46] hr s,
351 Continuous simulation parameters:
352 IaRECPper=[4] (hr s),
353 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
354 InterEventTime=[12] (hr s)
355 Baseflow simulation parameters:
356 BaseFlowOpti on=[1] ,
357 In it GWRes Vol = [50] (mm), GWRes K=[0. 96] (mm / day / mm)
358 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

360 CONTI NUOUS NASHYD NYHD=["SW_2"], DT=[1] mi n, AREA=[177] (ha),
361 DWF=[0] (cms), CNV C=[77], IA=[2. 5] (mm),
362 N=[3. 0], TP=[0. 75] hr s,
363 Continuous simulation parameters:
364 IaRECPper=[4] (hr s),
365 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
366 InterEventTime=[12] (hr s)
367 Baseflow simulation parameters:
368 BaseFlowOpti on=[1] ,
369 In it GWRes Vol = [50] (mm), GWRes K=[0. 96] (mm / day / mm)
370 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

372 CONTI NUOUS NASHYD NYHD=["SM_DR"], DT=[1] mi n, AREA=[1122] (ha),
373 DWF=[0] (cms), CNV C=[81], IA=[2. 5] (mm),
374 N=[3. 0], TP=[3. 25] hr s,
375 Continuous simulation parameters:
376 IaRECPper=[4] (hr s),
377 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
378 InterEventTime=[12] (hr s)
379 Baseflow simulation parameters:
380 BaseFlowOpti on=[1] ,
381 In it GWRes Vol = [50] (mm), GWRes K=[0. 96] (mm / day / mm)
382 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

384 CONTI NUOUS NASHYD NYHD=["MO_DR"], DT=[1] mi n, AREA=[2737] (ha),
385 DWF=[0] (cms), CNV C=[76], IA=[2. 5] (mm),
386 N=[3. 0], TP=[3. 03] hr s,
387 Continuous simulation parameters:
388 IaRECPper=[4] (hr s),
389 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),

```

390 InterEventTime=[ 12]( hrs)
391 Baseflow simulation parameters:
392 BaseFlowOption=[ 1] ,
393 InitGWResVol=[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
394 VHydCond=[ 0.055]( mm/ hr) , END=- 1
395 *%-----|-----|
396 * -JFSA 2020 replaced SW_1 with a detailed model from Stantec Report 2007
397 *CONTINUOUS NASHYD NHYD=["SW_1"], DT=[ 1]mi n, AREA=[ 3176]( ha),
398 * DWF=[ 0]( cms) , CN/C=[ 78] , IA=[ 2.5]( mm),
399 * N=[ 3.0] , TP=[ 3.56]hrs,
400 * Continuous simulation parameters:
401 * IaRECper=[ 4]( hrs),
402 * SMN=[ -1]( mm) , SMAX=[ -1]( mm) , SK=[ 0.010]/( mm),
403 * InterEventTime=[ 12]( hrs)
404 * Baseflow simulation parameters:
405 * BaseFlowOption=[ 1] ,
406 * InitGWResVol=[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
407 * VHydCond=[ 0.055]( mm/ hr) , END=- 1
408 *%-----|-----|
409 *#
410 *# Routing hydrographs
411 *#
412 *# Starting with the addition of Jock River Headwater and Subwatershed 13
413 *#
414 ADD HYD NHYDsum=["S_N13"], NHYDs to add=["JR_HW"+"SW_13"]
415 *%-----|-----|
416 *#
417 *# Sum of hydrographs from Node 13 routed to Node 13A
418 *# (Approximated cross-section - see cross-section 258)
419 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
420 *#
421 ROUTE CHANNEL NHYDout=["N13A"] , NHYDin=["S_N13"],
422 RDT=[ 1]( mi n),
423 CHLGTH=[ 9074]( m) , CHSLOPE=[ 0.0220]( %),
424 FPSLOPE=[ 0.0220]( %),
425 SECNUM=[ 1.0] , NSEG=[ 1]
426 ( SEGROUGH, SEGDI ST ( m) )=[ 0.04, 15.5] NSEG times
427 ( DI STANCE ( m) , ELEVATI ON ( m) )=
428 [- 40, 132.5]
429 [- 30, 132]
430 [- 25, 131.5]
431 [- 13, 130]
432 [- 8, 127.00]
433 [- 7, 126.50]
434 [- 6, 126]
435 [- 5.5, 125.50]
436 [ 0, 123.75]
437 [ 4.5, 125.50]
438 [ 6, 126]
439 [ 7.5, 126.5]
440 [ 9, 127]
441 [ 10, 127.5]
442 [ 11.5, 128.0]
443 [ 15.5, 129.5]
444 *%-----|-----|
445 *#
446 *# Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
447 *#
448 ADD HYD NHYDsum=["SN13A"], NHYDs to add=["N13A"+"JR_GWM"]
449 *%-----|-----|
450 *#
451 *# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
452 *#
453 ROUTE RESERVOIR NHYDout=["RES_GM"] , NHYDin=["SN13A"],
454 RDT=[ 1]( mi n),
455 TABLE of ( OUTFLOW STORAGE ) values

```



```

456 (cms) - (ha-m)
457 [ 0.0 , 0.0 ]
458 [ 1.991, 2.144 ]
459 [ 2.693, 39.826 ]
460 [ 3.509, 81.697 ]
461 [ 4.578, 318.774 ]
462 [ 5.647, 594.947 ]
463 [ 7.109, 910.219 ]
464 [ 8.616, 1264.589 ]
465 [ 10.371, 1658.057 ]
466 [ 12.402, 2090.622 ]
467 [ 22.056, 3462.487 ]
468 [ -1 , -1 ] (max twenty pts)
469
470 NHYDovf=[ " " ] ,
471 *%-----|-----|
472 *#
473 SAVE HYD NHYD=[ "RES_GM" ], # OF PCYCLES=[ -1 ], I CASEs h=[ -1 ]
474 HYD_FILENAMES=[ "H_RESGM" ]
475 HYD_COMMENT=[ "Out flow from Res GM" ]
476 *%-----|-----|
477 *# Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
478 *# (Approximated cross-section - see cross-section 258)
479 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
480 ROUTE CHANNEL NHYDout=[ "N12" ] , NHYDin=[ "RES_GM" ] ,
481 RDT=[ 1 ] (min) ,
482 CHLGTH=[ 5926 ] (m) , CHSLOPE=[ 0.0759 ] ( % ) ,
483 FPSLOPE=[ 0.0759 ] ( % ) ,
484 SECNUM=[ 1.0 ] , NSEG=[ 1 ]
485 ( SEGROUGH, SEGDIST (m) )=[ 0.04, 15.5 ] NSEG times
486 ( DISTANCE (m) , ELEVATION (m) )=
487 [- 40, 132.5]
488 [- 30, 132]
489 [- 25, 131.5]
490 [- 13, 130]
491 [- 8, 127.00]
492 [- 7, 126.50]
493 [- 6, 126]
494 [- 5.5, 125.50]
495 [ 0, 123.75]
496 [ 4.5, 125.50]
497 [ 6, 126]
498 [ 7.5, 126.5]
499 [ 9, 127]
500 [ 10, 127.5]
501 [ 11.5, 128.00]
502 [ 15.5, 129.5]
503 *%-----|-----|
504 *#
505 *# Addition of Subwatershed Jock River at Ashton to Node 12
506 *#
507 ADD HYD NHYDsum=[ "S_N12" ] , NHYDs to add=[ "N12"+"JR_ASH" ]
508 SAVE HYD NHYD=[ "S_N12" ] , # OF PCYCLES=[ -1 ], I CASEs h=[ -1 ]
509 HYD_FILENAMES=[ "H_SN12" ]
510 HYD_COMMENT=[ "flow at S_N12 near Ashton" ]
511 *%-----|-----|
512 *#
513 *# Sum of hydrographs from Node 12 routed to Node 11
514 *# (Approximated cross-section - see cross-section 258)
515 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
516 *ROUTE CHANNEL NHYDout=[ "N11" ] , NHYDin=[ "S_N12" ] ,
517 * RDT=[ 1 ] (min) ,
518 * CHLGTH=[ 972 ] (m) , CHSLOPE=[ 0.0514 ] ( % ) ,
519 * FPSLOPE=[ 0.0514 ] ( % ) ,
520 * SECNUM=[ 1.0 ] , NSEG=[ 1 ]
521 * ( SEGROUGH, SEGDIST (m) )=[ 0.04, 15.5 ] NSEG times
522 * ( DISTANCE (m) , ELEVATION (m) )=

```

```

522 * [- 40, 132.5]
523 * [- 30, 132]
524 * [- 25, 131.5]
525 * [- 13, 130]
526 * [- 8, 127.00]
527 * [- 7, 126.50]
528 * [- 6, 126]
529 * [- 5.5, 125.50]
530 * [0, 123.75]
531 * [4.5, 125.50]
532 * [6, 126]
533 * [7.5, 126.5]
534 * [9, 127]
535 * [10, 127.5]
536 * [11.5, 128.00]
537 * [15.5, 129.5]
538 *%-----|-----
539 *#
540 *# Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
541 *#
542 ROUTE CHANNEL NHYDout=["Duml1"], NHYDin=["S_N12"],
543 RDT=[1](min),
544 CHLGTH=[972](m), CHSLOPE=[0.054](%),
545 FPSLOPE=[0.054](%),
546 SECNUM=[1.0], NSEG=[1]
547 (SEGROUGH, SEGDIST(m))=[0.04, 15.5] NSEG times
548 (DISTANCE(m), ELEVATION(m))=
549 [- 40, 132.5]
550 [- 30, 132]
551 [- 25, 131.5]
552 [- 13, 130]
553 [- 8, 127.00]
554 [- 7, 126.50]
555 [- 6, 126]
556 [- 5.5, 125.50]
557 [0, 123.75]
558 [4.5, 125.50]
559 [6, 126]
560 [7.5, 126.5]
561 [9, 127]
562 [10, 127.5]
563 [11.5, 128.00]
564 [15.5, 129.5]
565 *%-----|-----
566 *#
567 *# Addition of Subwatershed 11 and No Name Creek to Node 11
568 *#
569 ADD HYD NHYDsum=["S_N11"], NHYDstoadd=["Duml1"+"SW_11"+"NN_CK"]
570 *%-----|-----
571 *#
572 *# Sum of hydrographs from Node 11 routed to Node 10
573 *# Section 1
574 *#
575 ROUTE CHANNEL NHYDout=["N10"], NHYDin=["S_N11"],
576 RDT=[1](min),
577 CHLGTH=[14028](m), CHSLOPE=[0.1568](%),
578 FPSLOPE=[0.1568](%),
579 SECNUM=[1.0], NSEG=[5]
580 (SEGROUGH, SEGDIST(m))=
581 [0.04, -52.82
582 0.1, -6.47
583 -0.05, 6.47
584 0.1, 45.36
585 0.04, 423.88] NSEG times
586 (DISTANCE(m), ELEVATION(m))=
587 [- 226.24 , 112.50]

```

```

588             [- 167. 50 , 111. 50]
589             [- 106. 81 , 111. 00]
590             [- 92. 37 , 110. 00]
591             [- 52. 82 , 109. 00]
592             [- 24. 90, 109. 00]
593             [- 17. 02, 108. 50]
594             [- 6. 47, 108. 00]
595             [ 6. 47, 108. 00]
596             [ 15. 67, 108. 50]
597             [ 18. 95, 109. 00]
598             [ 45. 36, 109. 50]
599             [ 120. 79, 110. 00]
600             [ 145. 72, 111. 00]
601             [ 181. 56, 111. 50]
602             [ 423. 88, 112. 50]
603 *%-----|-----
604 *#
605 *# Addition of Subwatershed 10 to Node 10
606 *#
607 ADD HYD          NHYDs um=["S_N10"], NHYDs to add=["N10"+"SW_10"]
608 *%-----|-----
609 SAVE HYD        NHYD=["S_N10"], # OF PCYCLES=[- 1], I CASEs h=[- 1]
610                HYD_ FI LENAME=["H_SN10"]
611                HYD_ COMMENT=["flow at S_N10: N10 + SW_10"]
612 *%-----|-----
613 *# Addition of Kings Creek to S_N10
614 *#
615 ADD HYD          NHYDs um=["S_N10A"], NHYDs to add=["S_N10"+"KG_CK"]
616 *%-----|-----
617 *#
618 *# Sum of hydrographs from Node 10 routed to Node 9
619 *# Section 2
620 *#
621 ROUTE CHANNEL    NHYDout=["N9"] , NHYDin=["S_N10A"] ,
622                RDT=[ 1] ( mi n) ,
623                CHLGTH=[ 3982] ( m) ,    CHSLOPE=[ 0. 0753] ( % ) ,
624                FPSLOPE=[ 0. 0753] ( % ) ,
625                SECNUM=[ 1. 0] ,        NSEG=[ 4]
626                ( SEGROUGH, SEGDI ST ( m) ) =
627                [ 0. 04, - 30. 27
628                0. 05, - 18. 42
629                - 0. 05, 18. 42
630                0. 04, 131. 58] NSEG t i m e s
631                ( DI STANCE ( m) , ELEVATI ON ( m) ) =
632                [- 446. 74, 106. 00]
633                [- 415. 68, 105. 50]
634                [- 285. 40, 105. 00]
635                [- 173. 77, 104. 50]
636                [- 144. 95, 104. 00]
637                [- 111. 18, 103. 50]
638                [- 94. 06, 103. 00]
639                [- 71. 02, 102. 50]
640                [- 30. 27, 102. 00]
641                [- 19. 33, 100. 00]
642                [- 18. 42, 99. 50]
643                [ 18. 42, 99. 50]
644                [ 20. 77, 100. 00]
645                [ 27. 93, 101. 00]
646                [ 52. 29, 101. 00]
647                [ 68. 80, 101. 50]
648                [ 79. 66, 103. 00]
649                [ 91. 50, 103. 50]
650                [ 131. 58, 104. 00]
651 *%-----|-----
652 *#
653 *# Addition of Subwatershed 9 and Nichols Creek to Node 9

```

```

654  *#
655  ADD HYD          NHYDs um=[ "S_N9" ], NHYDs  to  add=[ "N9"+"SW_9"+"NC_CK" ]
656  *%-----|-----|
657  *#
658  *# Sum of hydrographs from Node 9 routed to Node 8
659  *# Section 3
660  *#
661  ROUTE CHANNEL    NHYDout =[ "N8" ] , NHYDin =[ "S_N9" ] ,
662                  RDT=[ 1 ] ( mi n ) ,
663                  CHLGTH=[ 2269 ] ( m ) ,   CHSLOPE=[ 0.0882 ] ( % ) ,
664                                                    FPSLOPE=[ 0.0882 ] ( % ) ,
665                  SECNUM=[ 1.0 ] ,          NSEG=[ 3 ]
666                  ( SEGROUGH, SEGDI ST ( m ) ) =
667                    [ 0.1, -17.99
668                      -0.045, 17.31
669                      0.1, 456.58 ] NSEG t i m e s
670                  ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
671                    [ -201.19, 100.50 ]
672                    [ -135.21, 100.00 ]
673                    [ -94.83, 99.50 ]
674                    [ -67.05, 99.00 ]
675                    [ -17.99, 98.50 ]
676                    [ -16.02, 98.00 ]
677                    [ -13.95, 97.50 ]
678                    [ 13.95, 97.50 ]
679                    [ 15.64, 98.00 ]
680                    [ 17.31, 98.50 ]
681                    [ 162.02, 98.50 ]
682                    [ 172.89 , 99.00 ]
683                    [ 314.38, 99.00 ]
684                    [ 343.78, 99.50 ]
685                    [ 365.67, 100.00 ]
686                    [ 376.68, 100.00 ]
687                    [ 393.11, 99.50 ]
688                    [ 404.97, 99.50 ]
689                    [ 431.70, 100.00 ]
690                    [ 456.58, 100.50 ]
691  *%-----|-----|
692  *#
693  *# Addition of Subwatershed 8 and Hobb's Drain to Node 8
694  *#
695  ADD HYD          NHYDs um=[ "S_N8" ], NHYDs  to  add=[ "N8"+"SW_8"+"HB_DR" ]
696  *%-----|-----|
697  *#
698  *# Sum of hydrographs from Node 8 routed to Node 7
699  *# Section 4
700  *#
701  ROUTE CHANNEL    NHYDout =[ "N7" ] , NHYDin =[ "S_N8" ] ,
702                  RDT=[ 1 ] ( mi n ) ,
703                  CHLGTH=[ 3750 ] ( m ) ,   CHSLOPE=[ 0.0533 ] ( % ) ,
704                                                    FPSLOPE=[ 0.0533 ] ( % ) ,
705                  SECNUM=[ 1.0 ] ,          NSEG=[ 3 ]
706                  ( SEGROUGH, SEGDI ST ( m ) ) =
707                    [ 0.12, -18.11
708                      -0.07, 17.22
709                      0.12, 590.05 ] NSEG t i m e s
710                  ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
711                    [ -433.21, 102.00 ]
712                    [ -425.34, 101.50 ]
713                    [ -377.56, 101.50 ]
714                    [ -366.23, 101.00 ]
715                    [ -202.60, 100.50 ]
716                    [ -96.25, 99.50 ]
717                    [ -68.36 99.00 ]
718                    [ -18.11, 98.50 ]
719                    [ -13.81, 97.50 ]

```

```

720 [ 13. 81, 97. 50]
721 [ 17. 22, 98. 50]
722 [ 161. 95, 98. 50]
723 [ 173. 11, 99. 00]
724 [ 314. 05, 99. 00]
725 [ 365. 52, 100. 00]
726 [ 404. 70, 99. 50]
727 [ 476. 74, 100. 50]
728 [ 502. 31, 101. 00]
729 [ 584. 69, 101. 00]
730 [ 585. 79, 101. 00]
731 [ 590. 05, 102. 00]
732 *%-----|-----
733 *#
734 *# Addition of Subwatershed 7 to Node 7
735 *#
736 ADD HYD          NHYDs um=[ "S_N7" ], NHYDs to add=[ "N7"+"SW_7" ]
737 *%-----|-----
738 SAVE HYD         NHYD=[ "S_N7" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ - 1 ]
739                 HYD_FI LENAME=[ "H_SN7" ]
740                 HYD_COMMENT=[ "flow at S_N7: N7 + SW_7" ]
741 *%-----|-----
742 *# Insertion of a reservoir to simulate the effects of the Richmond Fen.
743 *# Storage area and volumes were estimated from available topo maps.
744 *# Release rate from fen was assumed to be controlled by the downstream
745 *# river cross-section for summer conditions. It is was assumed that for up to
746 *# 0.75 m of water, the main channel of the river provided the storage. Above
747 *# this depth, the wetland starts to signigicantly store water.
748 *#
749 ROUTE RESERVOIR NHYDout =[ "RES_RF" ] , NHYDi n=[ "S_N7" ] ,
750                 RDT=[ 1 ] ( mi n ) ,
751                 TABLE of ( OUTFLOW STORAGE ) values
752                         ( cms ) - ( ha- m )
753                 TABLE of ( OUTFLOW STORAGE ) values
754                         ( cms ) - ( ha- m )
755                         [ 0. 0 , 0. 0 ]
756                         [ 0. 9051, 2. 40]
757                         [ 2. 907, 4. 13]
758                         [ 9. 744, 9. 18]
759                         [ 20. 304, 14. 96]
760                         [ 34. 167, 310. 21]
761                         [ 74. 993, 605. 46]
762                         [ 104. 876, 900. 71]
763                         [ 140. 56, 2892. 00]
764                         [ 225. 00, 3615. 63]
765                         [ - 1 , - 1 ] (max t wenty pts)
766                 NHYDovf=[ " " ] ,
767 *%-----|-----
768 SAVE HYD         NHYD=[ "RES_RF" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ - 1 ]
769                 HYD_FI LENAME=[ "H_Res RF" ]
770                 HYD_COMMENT=[ "out flow of Ri chmnd Fen" ]
771 *%-----|-----
772 *#
773 *# Sum of hydrographs from Node 7 routed to Node 6
774 *# Section 5
775 *#
776 ROUTE CHANNEL   NHYDout =[ "N6" ] , NHYDi n=[ "RES_RF" ] ,
777                 RDT=[ 1 ] ( mi n ) ,
778                 CHLGTH=[ 3056 ] ( m ) , CHSLOPE=[ 0. 0818 ] ( % ) ,
779                 FPSLOPE=[ 0. 0818 ] ( % ) ,
780                 SECNUM=[ 1. 0 ] , NSEG=[ 5 ]
781                 ( SEGROUGH, SEGDI ST ( m ) ) =
782                 [ 0. 025, - 70. 8
783                 0. 1, - 23. 9
784                 - 0. 05, 23. 9
785                 0. 06, 39. 8

```

```

786           0. 05, 96. 3] NSEG times
787           ( DI STANCE ( m), ELEVATI ON ( m))=
788             [- 100. 8, 97. 00]
789             [- 70. 8, 96. 50]
790             [- 52. 0, 96. 00]
791             [- 35. 1, 95. 50]
792             [- 30. 6, 95. 00]
793             [- 23. 9, 94. 54]
794             [ 23. 9, 94. 54]
795             [ 39. 8, 95. 00]
796             [ 50. 4, 95. 50]
797             [ 93. 5, 96. 00]
798             [ 94. 9, 96. 50]
799             [ 96. 3, 97. 00]
800 *%-----|-----
801 *#
802 *# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
803 *#
804 ADD HYD           NHYDs um=[ "S_N6" ], NHYDs to add=[ "N6"+"SW_6"+"VG_DR" ]
805 *%-----|-----
806 *#
807 *# Sum of hydrographs from Node 6 routed to Node 5
808 *# Section 6
809 *#
810 ROUTE CHANNEL     NHYDout =[ "N5" ] , NHYDin =[ "S_N6" ] ,
811                   RDT=[ 1] ( mi n),
812                   CHLGTH=[ 1852] ( m),   CHSLOPE=[ 0. 0540] ( %),
813                                           FPSLOPE=[ 0. 0540] ( %),
814                   SECNUM=[ 1. 0],       NSEG=[ 3]
815                   ( SEGROUGH, SEGDI ST ( m))=
816                     [ 0. 035, - 131. 59
817                     - 0. 045, 48. 96
818                     0. 1, 239. 04] NSEG times
819                   ( DI STANCE ( m), ELEVATI ON ( m))=
820                     [- 686. 30, 94. 50]
821                     [- 675. 70, 94. 00]
822                     [- 492. 52, 93. 00]
823                     [- 467. 28, 94. 00]
824                     [- 131. 59, 94. 00]
825                     [- 92. 79, 92. 50]
826                     [- 18. 06, 91. 00]
827                     [ 18. 06, 91. 00]
828                     [ 43. 47, 92. 50]
829                     [ 48. 96, 94. 00]
830                     [ 177. 43, 94. 00]
831                     [ 239. 04, 94. 50]
832 *%-----|-----
833 *#
834 *# Addition of Subwatershed 5 and Flowing Creek to Node 5
835 *#
836 ADD HYD           NHYDs um=[ "S_N5" ], NHYDs to add=[ "N5"+"SW_5"+"FL_CK" ]
837 *%-----|-----
838 *#
839 *# Sum of hydrographs from Node 5 routed to Node 5A
840 *# Section 7
841 *#
842 ROUTE CHANNEL     NHYDout =[ "N5A" ] , NHYDin =[ "S_N5" ] ,
843                   RDT=[ 1] ( mi n),
844                   CHLGTH=[ 556] ( m),   CHSLOPE=[ 0. 0900] ( %),
845                                           FPSLOPE=[ 0. 0900] ( %),
846                   SECNUM=[ 1. 0],       NSEG=[ 4]
847                   ( SEGROUGH, SEGDI ST ( m))=
848                     [ 0. 04, - 41. 5
849                     0. 1, - 14. 0
850                     - 0. 045, 14. 0
851                     0. 1, 41. 1] NSEG times

```

```

852 ( DI STANCE ( m) , ELEVATI ON ( m) ) =
853 [- 275. 8, 93. 00]
854 [- 248. 6, 92. 50]
855 [- 237. 0, 92. 00]
856 [- 219. 3, 91. 50]
857 [- 202. 1, 91. 50]
858 [- 186. 0, 92. 00]
859 [- 129. 2, 92. 00]
860 [- 117. 6, 91. 50]
861 [- 100. 6, 91. 00]
862 [- 41. 5, 91. 00]
863 [- 20. 0, 91. 00]
864 [- 14. 0, 90. 54]
865 [ 14. 0, 90. 54]
866 [ 15. 3, 91. 00]
867 [ 17. 3, 91. 50]
868 [ 38. 4, 92. 00]
869 [ 39. 8, 92. 50]
870 [ 41. 1, 93. 00]
871 *%-----|-----|
872 *#
873 *# Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
874 *#
875 ADD HYD NHYDs um=[ "S_N5A" ] , NHYDs t o add=[ "N5A"+"SW_5A2"+"SW_5A1" ]
876 *%-----|-----|
877 *#
878 *# Sum of hydrographs from Node 5A routed to Node 4
879 *# Section 8
880 *#
881 ROUTE CHANNEL NHYDout =[ "N4" ] , NHYDi n=[ "S_N5A" ] ,
882 RDT=[ 1 ] ( mi n) ,
883 CHLGTH=[ 4630 ] ( m) , CHSLOPE=[ 0. 0432 ] ( % ) ,
884 FPSLOPE=[ 0. 0432 ] ( % ) ,
885 SECNUM=[ 1. 0 ] , NSEG=[ 3 ]
886 ( SEGROUGH, SEGDI ST ( m) ) =
887 [ 0. 05, -28. 2
888 -0. 035, 28. 2
889 0. 05, 173. 1 ] NSEG t i mes
890 ( DI STANCE ( m) , ELEVATI ON ( m) ) =
891 [- 38. 9, 92. 00]
892 [- 35. 8, 91. 50]
893 [- 33. 3, 91. 00]
894 [- 28. 2, 90. 50]
895 [- 15. 0, 87. 48]
896 [- 5. 0, 88. 34]
897 [ 5. 0, 86. 20]
898 [ 15. 0, 88. 55]
899 [ 28. 2, 90. 50]
900 [ 29. 7, 91. 00]
901 [ 46. 5, 91. 00]
902 [ 127. 8, 91. 00]
903 [ 148. 7, 91. 50]
904 [ 173. 1, 92. 00]
905 *%-----|-----|
906 *#
907 *# Addition of Subwatershed 4 and Leamy Creek to Node 4
908 *#
909 ADD HYD NHYDs um=[ "S_N4" ] , NHYDs t o add=[ "N4"+"SW_4"+"LM_CK" ]
910 SAVE HYD NHYD=[ "S_N4" ] , # OF PCYCLES=[ - 1 ] , I CASEs h=[ 1 ]
911 HYD_COMMENT=[ "fl ow at S_N4" ]
912 *%-----|-----|
913 *#
914 *# Sum of hydrographs from Node 4 routed to Node 2
915 *# Section 9
916 *#
917 ROUTE CHANNEL NHYDout =[ "N2" ] , NHYDi n=[ "S_N4" ] ,

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918 RDT=[ 1] ( mi n),
919 CHLGTH=[ 1667] ( m), CHSLOPE=[ 0. 0600] ( %),
920 FPSLOPE=[ 0. 0600] ( %),
921 SECNUM=[ 1. 0], NSEG=[ 4]
922 ( SEGROUGH, SEGDI ST ( m))=
923 [ 0. 1, - 28. 0
924 - 0. 04, 28. 4
925 0. 06, 31. 7
926 0. 04, 80. 2] NSEG t i m e s
927 ( DI STANCE ( m), ELEVATI ON ( m))=
928 [- 36. 3, 92. 00]
929 [- 32. 6, 91. 50]
930 [- 30. 2, 91. 00]
931 [- 28. 0, 90. 45]
932 [- 15. 0, 87. 48]
933 [- 5. 0, 88. 34]
934 [ 5. 0, 86. 20]
935 [ 15. 0, 88. 55]
936 [ 28. 0, 90. 45]
937 [ 28. 4, 90. 50]
938 [ 30. 4, 91. 00]
939 [ 31. 7, 91. 50]
940 [ 80. 2, 92. 00]
941 *%-----|-----|
942 *#
943 *# Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2
944 *#
945 ADD HYD NHYDs um=[ "S_N2"], NHYDs t o add=[ "N2"+"SW_2"+"SM_DR"+"MO_DR"]
946 *%-----|-----|
947 SAVE HYD NHYD=[ "S_N2"], # OF PCYCLES=[ - 1], I CAS E s h=[ - 1]
948 HYD_FI L E N A M E=[ "H_S_N2"]
949 HYD_COMMENT=[ "flow at S_N2 Jock River Gauge at Modie Dr." ]
950 *%-----|-----|
951 *#
952 *# Sum of hydrographs from Node 2 routed to Node 1
953 *# Section 10
954 *#
955 *#*****
956 *%READ HYD NHYD=[ "S_N2"],
957 *% HYD_FI L E N A M E=[ "H_S_N2"]
958 *%-----|-----|
959 *#
960 *# Hydrograph from Node 2 routed to Node 416
961 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 9025
962 *#
963 ROUTE CHANNEL NHYDout =["N_416"] , NHYDin=["S_N2"] ,
964 RDT=[ 1] ( mi n),
965 CHLGTH=[ 2327] ( m), CHSLOPE=[ 0. 0498] ( %),
966 FPSLOPE=[ 0. 0498] ( %),
967 SECNUM=[ 1. 0], NSEG=[ 3]
968 ( SEGROUGH, SEGDI ST ( m))=
969 [ 0. 075, - 23. 96
970 - 0. 055, 23. 96
971 0. 075, 157. 38] NSEG t i m e s
972 ( DI STANCE ( m), ELEVATI ON ( m))=
973 [- 336. 97, 93. 5]
974 [- 318. 85, 93]
975 [- 259, 92. 5]
976 [- 133. 18, 92]
977 [- 33. 17, 92]
978 [- 27. 21, 92]
979 [- 26. 14, 91. 5]
980 [- 24. 99, 91]
981 [- 23. 96, 90. 5]
982 [- 14. 33, 88. 26]
983 [- 0. 68, 88. 12]

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984 [ 14. 33, 88. 26]
985 [ 23. 96, 90. 5]
986 [ 32. 12, 91]
987 [ 43. 74, 91. 5]
988 [ 57. 09, 92]
989 [ 73. 53, 92. 5]
990 [ 108. 27, 93]
991 [ 125. 88, 93. 5]
992 [ 144. 81, 94]
993 [ 157. 38, 94. 5]
994 *%-----|-----|
995 *#*****|*****|
996 *# Catchment SW1a
997 *# - Portion of RVCA catchment SW1 outside of Reach 1 subwatershed
998 *# - Undeveloped agricultural land
999 *#*****|*****|
1000 CONTINUOUS NASHYD NHYD=[ "SW_1a" ], DT=[ 1] mi n, AREA=[ 536. 42] ( ha ),
1001 DWF=[ 0] ( cms ), CN C=[ 72], I A=[ 4. 67] ( mm ),
1002 N=[ 3], TP=[ 2. 79] hr s,
1003 Continuous simulation parameters:
1004 I aRECper=[ 4] ( hr s ),
1005 SM N=[ - 1] ( mm ), SMAX=[ - 1] ( mm ), SK=[ 0. 010] / ( mm ),
1006 I nterEventTi me=[ 12] ( hr s)
1007 Baseflow simulation parameters:
1008 BaseFl owOpt ion=[ 1] ,
1009 I n i t GWR es Vol =[ 50] ( mm ), GWR es K=[ 0. 96] ( mm / day / mm)
1010 VHydCond=[ 0. 055] ( mm / hr ), END=- 1
1011 *%-----|-----|
1012 * -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
before station 7245 on Jock River
1013 CONTINUOUS STANDHYD NHYD=[ "S-1-Okeefe" ], DT=[ 1] ( mi n), AREA=[ 44. 93] ( ha ), XI MP=[ 0. 65],
TI MP=[ 0. 65], DWF=[ 0] ( cms ),
1014 LOSS=[ 2], SCS curve number CN=[ 75], Pervious surfaces:
I Aper=[ 4. 67] ( mm ), SLPP=[ 2. 0] ( % ),
1015 LGP=[ 40] ( m ), MNP=[ 0. 25], SCP=[ 0] ( mi n), Impervious surfaces:
I Ai mp=[ 1. 57] ( mm ), SLPI=[ 0. 75] ( % ),
1016 LGI =[ 547. 296] ( m ), MNI =[ 0. 013], SCI =[ 0] ( mi n),
1017 Continuous simulation parameters:
1018 I aRECper=[ 4] ( hr s), I aRECI mp=[ 4] ( hr s),
1019 SM N=[ - 1] ( mm ), SMAX=[ - 1] ( mm ), SK=[ 0. 010] / ( mm ),
1020 I nterEventTi me=[ 12] ( hr s), END=- 1
1021 *%-----|-----|
1022 COMPUTE DUALHYD NHYDi n=[ "S-1-Okeefe" ], CI NLET=[ 4. 591] ( cms ), NI NLET=[ 1],
1023 M i j NHYD=[ "S-1-OkM" ]
1024 M nNHYD=[ "S-1-OkMN" ]
1025 TM I STO=[ 9999999] ( cu - m)
1026 *%-----|-----|
1027 ADD HYD NHYDs um=[ "S-1-OkS" ], NHYDs t o add=[ "S-1-OkM" +"S-1-OkMN" ]
1028 *%-----|-----|
1029 ROUTE RESERVOIR NHYDout =[ "S-1-OkSR" ], NHYDi n=[ "S-1-OkS" ],
1030 RDT=[ 1] ( mi n),
1031 TABLE of ( OUTFLOW STORAGE ) values
1032 ( cms ) - ( ha - m)
1033 [ 0. 0 , 0. 0 ]
1034 [ 0. 5370, 1. 7917 ]
1035 [ - 1 , - 1 ] ( max twenty pts)
1036 NHYDovf=[ "S-1-OkSovf" ]
1037 *%-----|-----|
1038 ADD HYD NHYDs um=[ "SN_416" ], NHYDs t o
add=[ "N_416" +"SW_1a" +"S-1-OkSR" +"S-1-OkSovf" ]
1039 *%-----|-----|
1040 SAVE HYD NHYD=[ "SN_416" ], # OF PCYCLES=[ - 1], I CASEs h=[ 1]
1041 HYD_COMMENT=[ "Total Flows at Highway 416 before Station 7245" ]
1042 *%-----|-----|
1043 *#
1044 *# Hydrograph from Node 416 routed to Node at Okeefe drain

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1045 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 7245
1046 *#
1047 ROUTE CHANNEL      NHYDout=["N_OK"], NHYDin=["SN_416"],
1048                    RDT=[1](min),
1049                    CHLGTH=[497](m),  CHSLOPE=[0.3018](%),
1050                    FPSLOPE=[0.3018](%),
1051                    SECNUM=[1.0],      NSEG=[3]
1052                    (SEGROUGH, SEGDIST(m))=
1053                    [0.075, -19.40
1054                    -0.055, 19.40
1055                    0.075, 377.02] NSEG times
1056                    (DISTANCE(m), ELEVATION(m))=
1057                    [-1061.41, 92.50]
1058                    [-945.91, 92.00]
1059                    [-783.64, 91.50]
1060                    [-136.74, 91.00]
1061                    [-86.04, 91.00]
1062                    [-20.86, 91.00]
1063                    [-20.18, 90.50]
1064                    [-19.40, 90.00]
1065                    [-11.68, 86.89]
1066                    [0.00, 86.10]
1067                    [12.09, 86.81]
1068                    [19.40, 90.00]
1069                    [34.68, 90.50]
1070                    [60.56, 91.00]
1071                    [170.14, 91.00]
1072                    [175.05, 90.50]
1073                    [180.29, 90.00]
1074                    [193.41, 90.00]
1075                    [195.98, 90.50]
1076                    [377.02, 92.50]
1077 *%-----|-----|
1078 *#*****|*****|
1079 *# Catchment OKEEFE
1080 *# - To O'Keefe drain (north of the Jock)
1081 *# - Developed with assumed 43% imp.
1082 *# - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area
1083 *# - 2020-11-20 Okeefe detailed model was added as per the NOVATECH SWWHYMD model
1084 *# - (Citi-Gate 2014).
1085 *%-----|-----|
1086 *#*****|*****|
1087 *#*****|*****|
1088 CONTINUOUS NASHYD  NHYD=["O-1R"], DT=[1]min, AREA=[63.72](ha),
1089                    DWF=[0](cms), CNVC=[61], IA=[6.2](mm), N=[3], TP=[.9]hrs,
1090                    Continuous simulation parameters:
1091                    IARECper=[4](hrs),
1092                    SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1093                    InterEventTime=[12](hrs)
1094                    Baseflow simulation parameters:
1095                    BaseFlowOption=[1],
1096                    InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1097                    VHydCond=[0.055](mm/hr), END=-1
1098 *%-----|-----|
1099 *#*****|*****|
1100 *#*****|*****|
1101 ROUTE CHANNEL      NHYDout=["O-1R"], NHYDin=["O-1"], RDT=[1](min),
1102                    CHLGTH=[960](m), CHSLOPE=[0.63](%), FPSLOPE=[0.63](%),
1103                    SECNUM=[1], NSEG=[3]
1104                    (SEGROUGH, SEGDIST(m))=[0.06, 4 -.043, 6 0.06, 10] NSEG times
1105                    (DISTANCE(m), ELEVATION(m))=[0.00, 2.0]
1106                    [0.0, 2.0]
1107                    [4.0, 0.0]
1108                    [6.0, 0.0]

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1108 [ 10.0, 2.0]
1109 *%-----|-----|
1110 CONTINUOUS NASHYD NHYD=["O-2"], DT=[1] min, AREA=[28.61] (ha),
1111 DWF=[0] (cms), CN C=[57], IA=[5.2] (mm), N=[3], TP=[1.1] hrs,
1112 Continuous simulation parameters:
1113 IaRECPper=[4] (hrs),
1114 SMN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1115 InterEventTime=[12] (hrs)
1116 Baseflow simulation parameters:
1117 BaseFlowOption=[1],
1118 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
1119 VHydCond=[0.055] (mm/hr), END=-1
1120 *%-----|-----|
1121 CONTINUOUS NASHYD NHYD=["O-4"], DT=[1] min, AREA=[46.94] (ha),
1122 DWF=[0] (cms), CN C=[49], IA=[9.2] (mm), N=[3], TP=[0.9] hrs,
1123 Continuous simulation parameters:
1124 IaRECPper=[4] (hrs),
1125 SMN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1126 InterEventTime=[12] (hrs)
1127 Baseflow simulation parameters:
1128 BaseFlowOption=[1],
1129 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
1130 VHydCond=[0.055] (mm/hr), END=-1
1131 *%-----|-----|
1132 *TOTAL EXTERNAL FLOW NORTH OF O'KEEFE CT. CROSSING
1133 ADD HYD NHYDsum=["OKF-N"], NHYDstoadd=["O-1R"+"O-2"+"O-4"]
1134 *%-----|-----|
1135 *ROUTE FLOW THROUGH AREA O-6
1136 ROUTE CHANNEL ROUTE CHANNEL NHYDout=["OKF-NR"], NHYDin=["OKF-N"], RDT=[1] (min),
1137 CHLGTH=[210] (m), CHSLOPE=[.81] (%), FPSLOPE=[.81] (%),
1138 SECNUM=[1], NSEG=[3]
1139 (SEGROUGH, SEGDIST (m))=[0.043, 22.43 - 0.043, 25.07
1140 0.043, 45.54] NSEG times
1141 (DISTANCE (m), ELEVATION (m))=[0.00, 3.73]
1142 (14.62, 1.56)
1143 (18.41, 1.44)
1144 (22.43, 0.00)
1145 (25.07, 0.70)
1146 (29.10, 1.79)
1147 (33.73, 2.71)
1148 (45.54, 3.58)
1149 *%-----|-----|
1150 CONTINUOUS NASHYD NHYD=["O-6"], DT=[1] min, AREA=[16.46] (ha),
1151 DWF=[0] (cms), CN C=[43], IA=[9.2] (mm), N=[3], TP=[0.7] hrs,
1152 Continuous simulation parameters:
1153 IaRECPper=[4] (hrs),
1154 SMN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1155 InterEventTime=[12] (hrs)
1156 Baseflow simulation parameters:
1157 BaseFlowOption=[1],
1158 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
1159 VHydCond=[0.055] (mm/hr), END=-1
1160 *%-----|-----|
1161 CONTINUOUS STANDHYD NHYD=["O-3"], DT=[1] (min), AREA=[39.67] (ha), XI MP=[0.15],
1162 TI MP=[0.30], DWF=[0] (cms),
1163 LOSS=[2], SCS curve number CN=[50], Pervious surfaces:
1164 IAper=[4.67] (mm), SLPP=[0.32] (%),
1165 LGP=[440] (m), MNP=[0.035], SCP=[0] (min), Impervious surfaces:
1166 IAimp=[1.57] (mm), SLPI=[0.32] (%),
1167 LGI=[1880] (m), MNI=[0.013], SCI=[0] (min),
1168 Continuous simulation parameters:
1169 IaRECPper=[4] (hrs), IaRECImp=[4] (hrs),
1170 SMN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1171 InterEventTime=[12] (hrs), END=-1
1172 *%-----|-----|
1173 CONTINUOUS STANDHYD NHYD=["O-5"], DT=[1] (min), AREA=[60.63] (ha), XI MP=[0.13],

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1171 TIMP=[ 0.26], DWF=[ 0](cms),
1172 LOSS=[ 2], SCS curve number CN=[ 61],
1173 Pervious surfaces: I Aper=[ 4.67](mm), SLPP=[ 1.38](%),
LGP=[ 550](m), MNP=[ 0.035], SCP=[ 0](min), Impervious surfaces:
1174 I Aimp=[ 1.57](mm), SLPI=[ 1.38](%),
LGI=[ 1450](m), MNI=[ 0.013], SCI=[ 0](min),
1175 Continuous simulation parameters:
1176 I aRECper=[ 4](hrs), I aRECImp=[ 4](hrs),
1177 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1178 InterEventTime=[ 12](hrs), END=- 1
1179 *%-----|-----|
1180 *TOTAL EXTERNAL FLOWS WEST OF THE SITE AND NORTH OF O'KEEFE CRT
1181 *%-----|-----|
1182 ADD HYD NHYDsum=[ "PT1"], NHYDs to add=[ "OKF-NR"+"O-3"+"O-5"+"O-6"]
1183 *%-----|-----|
1184 CONTINUOUS NASHYD NHYD=[ "O-7"], DT=[ 1]min, AREA=[ 5.28](ha),
1185 DWF=[ 0](cms), CNVC=[ 54], IA=[ 7.5](mm), N=[ 3], TP=[ 0.6]hrs,
1186 Continuous simulation parameters:
1187 I aRECper=[ 4](hrs),
1188 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1189 InterEventTime=[ 12](hrs)
1190 Baseflow simulation parameters:
1191 BaseFlowOption=[ 1],
1192 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
1193 VHydCond=[ 0.055](mm/hr), END=- 1
1194 *%-----|-----|
1195 *ANALYSIS POINT 1 - TOTAL FLOW NORTH OF FALLOWFIELD DR. AND O'KEEFE CRT.
1196 ADD HYD NHYDsum=[ "FF"], NHYDs to add=[ "PT1"+"O-7"]
1197 *%-----|-----|
1198 *ROUTE FLOW through O'Keefe Drain 1
1199 ROUTE CHANNEL NHYDout=[ "DRAIN1"], NHYDin=[ "FF"], RDT=[ 1](min),
1200 CHLGTH=[ 302](m), CHSLOPE=[ 1.00](%), FPSLOPE=[ 1.00](%),
1201 SECNUM=[ 1], NSEG=[ 3]
1202 (SEGROUGH, SEGDIST (m))=[ 0.07, 13.45 -0.043, 16.55 0.07, 30.00] NSEG
times
1203 (DISTANCE (m), ELEVATION (m))=[ 0.00, 1.70]
1204 (3.45, 0.60)
1205 (13.45, 0.50)
1206 (14.45, 0.00)
1207 (15.55, 0.00)
1208 (16.55, 0.50)
1209 (26.55, 0.60)
1210 (30.00, 1.70)
1211 *%-----|-----|
1212 CONTINUOUS NASHYD NHYD=[ "DI"], DT=[ 1]min, AREA=[ 1.17](ha),
1213 DWF=[ 0](cms), CNVC=[ 84], IA=[ 9.0](mm), N=[ 3], TP=[ 0.28]hrs,
1214 Continuous simulation parameters:
1215 I aRECper=[ 4](hrs),
1216 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1217 InterEventTime=[ 12](hrs)
1218 Baseflow simulation parameters:
1219 BaseFlowOption=[ 1],
1220 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
1221 VHydCond=[ 0.055](mm/hr), END=- 1
1222 *%-----|-----|
1223 CONTINUOUS STANDHYD NHYD=[ "AI"], DT=[ 1]min, AREA=[ 2.50](ha), XI MP=[ 0.68], TIMP=[ 0.85],
DWF=[ 0](cms), LOSS=[ 1]:
1224 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
F=[ 0.00](mm),
1225 Pervious areas: I Aper=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 50](m),
MNP=[ 0.250], SCP=[ 0](min),
1226 Impervious areas: I Aimp=[ 1.57](mm), SLPI=[ 0.5](%),
LGI=[ 223.607](m), MNI=[ 0.013], SCI=[ 0](min),
1227 Continuous simulation parameters:
1228 I aRECper=[ 4](hrs), I aRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
END=- 1

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1229 *%-----|-----|
1230 ROUTE RESERVOIR NHYDout=[ "A1-STR"], NHYDin=[ "A1"], RDT=[ 1](mi n),
1231          TABLE of ( OUTFLOW STORAGE ) values
1232          ( cms ) - ( ha- m)
1233          [ 0.000 , 0.000 ]
1234          [ 0.035 , 0.038 ]
1235          [ 0.072 , 0.051 ]
1236          [ 0.100 , 0.059 ]
1237          [ 0.125 , 0.070 ]
1238          [ 0.160 , 0.074 ]
1239          [ 0.185 , 0.081 ]
1240          [ -1 , -1 ] (max t went y pt s)
1241          NHYDovf=[ "A1- OVF" ]
1242 *%-----|-----|
1243 CONTINUOUS STANDHYD NHYD=[ "ST-2"], DT=[ 1]mi n, AREA=[ 0.59](ha), XI MP=[ 0.46],
1244 TIMP=[ 0.57], DWF=[ 0](cms), LOSS=[ 1]:
1245 Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
1246          F=[ 0.00](mm),
1247          Pervious areas: I A per=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 50](m),
1248          MNP=[ 0.250], SCP=[ 0](mi n),
1249          Imper vious areas: I A i mp=[ 1.57](mm), SLPI=[ 0.5](%),
1250          LGI=[ 108.628](m), MNI=[ 0.013], SCI=[ 0](mi n),
1251          Continuous simulation parameters:
1252          I a REC per=[ 4](hr s), I a REC i mp=[ 4](hr s), I nter Event Ti me=[ 12](hr s),
1253          END=- 1
1254 *%-----|-----|
1255 ROUTE RESERVOIR NHYDout=[ "ST2STR"], NHYDin=[ "ST-2"], RDT=[ 1](mi n),
1256          TABLE of ( OUTFLOW STORAGE ) values
1257          ( cms ) - ( ha- m)
1258          [ 0.000 , 0.0000 ]
1259          [ 0.052 , 0.0010 ]
1260          [ 0.053 , 0.0080 ]
1261          [ -1 , -1 ] (max t went y pt s)
1262          NHYDovf=[ "ST2OVF" ]
1263 *%-----|-----|
1264 *%-----|-----|
1265 *TOTAL FLOW NORTH OF STRANDHERD DR. (EAST BRANCH) CROSSING
1266 *%-----|-----|
1267 CONTINUOUS NASHYD NHYD=[ "O-8"], DT=[ 1]mi n, AREA=[ 60.55](ha),
1268 DWF=[ 0](cms), CNV C=[ 69], I A=[ 4.0](mm), N=[ 3], TP=[ 1.0]hr s,
1269 Continuous simulation parameters:
1270 I a REC per=[ 4](hr s),
1271 SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1272 Inter Event Ti me=[ 12](hr s)
1273 Baseflow simulation parameters:
1274 BaseFl owOpt ion=[ 1] ,
1275 I n i t GWRes Vol=[ 50](mm), GWRes K=[ 0.96](mm/ day/ mm)
1276 VHydCond=[ 0.055](mm/ hr), END=- 1
1277 *%-----|-----|
1278 ROUTE PIPE PTYPE=[ 2]rect, NHYDout=[ "O8PIPE"], RNUMBER=[ 1], PWDTH=[ 1800](mm),
1279 PHEIGHT=[ 1200](mm), PLNGTH=[ 335.1](m),
1280 PROUGH=[ 0.013], PSLOPE=[ 0.001](m/ m), NHYDin=[ "O-8"], RDT=[ 1](mi n)
1281 *%-----|-----|
1282 *%-----|-----|
1283 ADD HYD NHYDs um=[ "ST2- I N"], NHYDs to
1284 add=[ "DRAIN1"+"D1"+"A1-STR"+"A1- OVF"+"ST2STR"+"ST2OVF"+"O8PIPE" ]
1285 *%-----|-----|
1286 CONTINUOUS STANDHYD NHYD=[ "A7"], DT=[ 1]mi n, AREA=[ 3.51](ha), XI MP=[ 0.68], TIMP=[ 0.85],
1287 DWF=[ 0](cms), LOSS=[ 1]:
1288 Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
1289          F=[ 0.00](mm),
1290          Pervious areas: I A per=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 50](m),
1291          MNP=[ 0.250], SCP=[ 0](mi n),
1292          Imper vious areas: I A i mp=[ 1.57](mm), SLPI=[ 0.5](%),
1293          LGI=[ 264.953](m), MNI=[ 0.013], SCI=[ 0](mi n),
1294          Continuous simulation parameters:

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1284 IaRECPper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
END=- 1
1285 *%-----|-----|
1286 ROUTE RESERVOIR NHYDout=["A7-STR"], NHYDin=["A7"], RDT=[ 1](min),
1287 TABLE of ( OUTFLOW STORAGE ) values
1288 (cms) - (ha-m)
1289 [ 0.000 , 0.000 ]
1290 [ 0.049 , 0.054 ]
1291 [ 0.102 , 0.072 ]
1292 [ 0.140 , 0.082 ]
1293 [ 0.175 , 0.099 ]
1294 [ 0.225 , 0.105 ]
1295 [ 0.260 , 0.114 ]
1296 [ -1 , -1 ] (max twenty pts)
1297 NHYDovf=["A7-OVF"]
1298 *%-----|-----|
1299 CONTINUOUS STANDHYD NHYD=["ST-3"], DT=[ 1]min, AREA=[ 0.71](ha), XI MP=[ 0.46],
TIMP=[ 0.57], DWF=[ 0](cms), LOSS=[ 1]:
1300 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
F=[ 0.00](mm),
1301 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 50](m),
MNP=[ 0.250], SCP=[ 0](min),
1302 Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 0.5](%),
LGI=[ 119.164](m), MNI=[ 0.013], SCI=[ 0](min),
1303 Continuous simulation parameters:
1304 IaRECPper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
END=- 1
1305 *%-----|-----|
1306 ROUTE RESERVOIR NHYDout=["ST3STR"], NHYDin=["ST-3"], RDT=[ 1](min),
1307 TABLE of ( OUTFLOW STORAGE ) values
1308 (cms) - (ha-m)
1309 [ 0.000 , 0.0000 ]
1310 [ 0.063 , 0.0010 ]
1311 [ 0.064 , 0.0094 ]
1312 [ -1 , -1 ] (max twenty pts)
1313 NHYDovf=["ST3OVF"]
1314 *%-----|-----|
1315 *ANALYSIS POINT 2 - TOTAL FLOW AT OUTLET OF STREET 2/3 INTERSECTION
1316 *%-----|-----|
1317 ADD HYD NHYDsum=["PT2ST3"], NHYDsto
add=["ST2-IN"+"A7-STR"+"A7-OVF"+"ST3STR"+"ST3OVF"]
1318 *%-----|-----|
1319 *ROUTE FLOW through O Keefe Drain 2
1320 ROUTE CHANNEL NHYDout=["DRAIN2"], NHYDin=["PT2ST3"], RDT=[ 1](min),
1321 CHLGTH=[ 592](m), CHSLOPE=[.23](%), FPSLOPE=[.23](%),
1322 SECNUM=[ 1], NSEG=[ 3]
1323 ( SEGROUGH, SEGDIST (m))=[ 0.07, 12.60 -0.043, 17.40 0.07, 30.00] NSEG
times
1324 ( DISTANCE (m), ELEVATION (m))=[ 0.00, 1.70]
1325 ( 2.60, 0.95)
1326 ( 12.60, 0.75)
1327 ( 14.10, 0.00)
1328 ( 15.90, 0.00)
1329 ( 17.40, 0.75)
1330 ( 27.40, 0.95)
1331 ( 30.00, 1.70)
1332 *%-----|-----|
1333 CONTINUOUS NASHYD NHYD=["D2"], DT=[ 1]min, AREA=[ 2.28](ha), DWF=[ 0](cms), CNVC=[ 84],
IA=[ 9.0](mm),
1334 N=[ 3], TP=[ 0.99]hrs,
1335 Continuous simulation parameters:
1336 IaRECPper=[ 4](hrs),
1337 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1338 InterEventTime=[ 12](hrs)
1339 Baseflow simulation parameters:
1340 BaseFlowOption=[ 1],

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1341      Ini t GWRes Vol =[ 50] ( mm ) , GWRes K =[ 0. 96] ( mm/ day/ mm)
1342      VHydCond =[ 0. 055] ( mm/ hr ) ,      END = - 1
1343 *%-----|-----|
1344 CONTI NUOUS STANDHYD NHYD =[ " A17" ] , DT =[ 1] mi n , AREA =[ 12. 04] ( ha) , XI MP =[ 0. 68] ,
TI MP =[ 0. 85] , DWF =[ 0] ( cms) , LOSS =[ 1] :
1345      Hort on: Fo =[ 76. 20] ( mm/ hr ) , Fc =[ 13. 20] ( mm/ hr ) , DCAY =[ 4. 14] ( / hr ) ,
F =[ 0. 00] ( mm) ,
1346      Per vious areas: I Aper =[ 4. 67] ( mm) , SLPP =[ 0. 5] ( % ) , LGP =[ 50] ( m) ,
MNP =[ 0. 250] , SCP =[ 0] ( mi n) ,
1347      Impervious areas: I Ai mp =[ 1. 57] ( mm) , SLPI =[ 0. 5] ( % ) ,
LGI =[ 490. 714] ( m) , MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
1348      Continuous simulation parameters:
1349      IaRECper =[ 4] ( hrs) , IaRECI mp =[ 4] ( hrs) , Int er Event Ti me =[ 12] ( hrs) ,
END = - 1
1350 *%-----|-----|
1351 ROUTE RESERVOIR NHYDout =[ " A17STR" ] , NHYDi n =[ " A17" ] , RDT =[ 1] ( mi n) ,
1352      TABLE of ( OUTFLOW STORAGE ) values
1353      ( cms) - ( ha- m)
1354      [ 0. 000 , 0. 000 ]
1355      [ 0. 169 , 0. 185 ]
1356      [ 0. 349 , 0. 248 ]
1357      [ 0. 482 , 0. 283 ]
1358      [ 0. 602 , 0. 338 ]
1359      [ 0. 771 , 0. 359 ]
1360      [ 0. 891 , 0. 391 ]
1361      [ - 1 , - 1 ] ( max twenty pts)
1362      NHYDovf =[ " A17OVF" ]
1363 *%-----|-----|
1364 CONTI NUOUS STANDHYD NHYD =[ " ST- 4" ] , DT =[ 1] mi n , AREA =[ 0. 35] ( ha) , XI MP =[ 0. 46] ,
TI MP =[ 0. 57] , DWF =[ 0] ( cms) , LOSS =[ 1] :
1365      Hort on: Fo =[ 76. 20] ( mm/ hr ) , Fc =[ 13. 20] ( mm/ hr ) , DCAY =[ 4. 14] ( / hr ) ,
F =[ 0. 00] ( mm) ,
1366      Per vious areas: I Aper =[ 4. 67] ( mm) , SLPP =[ 0. 5] ( % ) , LGP =[ 50] ( m) ,
MNP =[ 0. 250] , SCP =[ 0] ( mi n) ,
1367      Impervious areas: I Ai mp =[ 1. 57] ( mm) , SLPI =[ 0. 5] ( % ) , LGI =[ 83. 666] ( m) ,
MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
1368      Continuous simulation parameters:
1369      IaRECper =[ 4] ( hrs) , IaRECI mp =[ 4] ( hrs) , Int er Event Ti me =[ 12] ( hrs) ,
END = - 1
1370 *%-----|-----|
1371 ROUTE RESERVOIR NHYDout =[ " ST4STR" ] , NHYDi n =[ " ST- 4" ] , RDT =[ 1] ( mi n) ,
1372      TABLE of ( OUTFLOW STORAGE ) values
1373      ( cms) - ( ha- m)
1374      [ 0. 000 , 0. 0000 ]
1375      [ 0. 031 , 0. 0010 ]
1376      [ 0. 032 , 0. 0050 ]
1377      [ - 1 , - 1 ] ( max twenty pts)
1378      NHYDovf =[ " ST4OVF" ]
1379 *%-----|-----|
1380 CONTI NUOUS STANDHYD NHYD =[ " A18" ] , DT =[ 1] mi n , AREA =[ 5. 30] ( ha) , XI MP =[ 0. 68] , TI MP =[ 0. 85] ,
DWF =[ 0] ( cms) , LOSS =[ 1] :
1381      Hort on: Fo =[ 76. 20] ( mm/ hr ) , Fc =[ 13. 20] ( mm/ hr ) , DCAY =[ 4. 14] ( / hr ) ,
F =[ 0. 00] ( mm) ,
1382      Per vious areas: I Aper =[ 4. 67] ( mm) , SLPP =[ 0. 5] ( % ) , LGP =[ 50] ( m) ,
MNP =[ 0. 250] , SCP =[ 0] ( mi n) ,
1383      Impervious areas: I Ai mp =[ 1. 57] ( mm) , SLPI =[ 0. 5] ( % ) ,
LGI =[ 325. 576] ( m) , MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
1384      Continuous simulation parameters:
1385      IaRECper =[ 4] ( hrs) , IaRECI mp =[ 4] ( hrs) , Int er Event Ti me =[ 12] ( hrs) ,
END = - 1
1386 *%-----|-----|
1387 ROUTE RESERVOIR NHYDout =[ " A18STR" ] , NHYDi n =[ " A18" ] , RDT =[ 1] ( mi n) ,
1388      TABLE of ( OUTFLOW STORAGE ) values
1389      ( cms) - ( ha- m)
1390      [ 0. 000 , 0. 000 ]
1391      [ 0. 074 , 0. 082 ]

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1392         [ 0.154 , 0.109 ]
1393         [ 0.212 , 0.125 ]
1394         [ 0.265 , 0.149 ]
1395         [ 0.339 , 0.158 ]
1396         [ 0.392 , 0.172 ]
1397         [ -1 , -1 ] (max twenty pts)
1398         NHYDovf=[ "A18OVF" ]
1399 *%-----|-----|
1400 *ANALYSIS POINT 3 - TOTAL FLOW AT OUTLET OF STREET 4
1401 *%-----|-----|
1402 ADD HYD          NHYDs um=[ "PT3ST4" ], NHYDs to
add=[ "DRAIN2"+"D2"+"A17STR"+"A17OVF"+"ST4STR"+"ST4OVF"+"A18STR"+"A18OVF" ]
1403 *%-----|-----|
1404 *ROUTE FLOW through O Keefe Drain 3
1405 ROUTE CHANNEL   NHYDout=[ "DRAIN3" ], NHYDin=[ "PT3ST4" ], RDT=[ 1 ] (min),
1406                CHLGTH=[ 525 ] (m), CHSLOPE=[ .23 ] (%), FPSLOPE=[ .23 ] (%),
1407                SECNUM=[ 1 ], NSEG=[ 3 ]
1408                ( SEGROUGH, SEGDIST (m) )=[ 0.07, 12.50 -0.043, 17.50 0.07, 30.00 ] NSEG
times
1409                ( DISTANCE (m), ELEVATION (m) )=[ 0.00, 1.70 ]
1410                ( 2.50, 1.00 )
1411                ( 12.50, 0.80 )
1412                ( 14.10, 0.00 )
1413                ( 15.90, 0.00 )
1414                ( 17.50, 0.80 )
1415                ( 27.50, 1.00 )
1416                ( 30.00, 1.70 )
1417 *%-----|-----|
1418 CONTINUOUS NASHYD NHYD=[ "D3" ], DT=[ 1 ] min, AREA=[ 2.51 ] (ha),
1419                DWF=[ 0 ] (cms), CNVC=[ 86 ], IA=[ 8.7 ] (mm), N=[ 3 ], TP=[ 0.73 ] hrs,
1420                Continuous simulation parameters:
1421                IaRECper=[ 4 ] (hrs),
1422                SMN=[ -1 ] (mm), SMAX=[ -1 ] (mm), SK=[ 0.010 ] / (mm),
1423                InterEventTime=[ 12 ] (hrs)
1424                Baseflow simulation parameters:
1425                BaseFlowOption=[ 1 ],
1426                InitGWResVol=[ 50 ] (mm), GWResK=[ 0.96 ] (mm/day/mm)
1427                VHydCond=[ 0.055 ] (mm/hr), END=- 1
1428 *%-----|-----|
1429 CONTINUOUS STANDHYD NHYD=[ "C1" ], DT=[ 1 ] min, AREA=[ 3.41 ] (ha), XI MP=[ 0.68 ], TI MP=[ 0.85 ],
DWF=[ 0 ] (cms), LOSS=[ 1 ]:
1430                Horton: Fo=[ 76.20 ] (mm/hr), Fc=[ 13.20 ] (mm/hr), DCAY=[ 4.14 ] (/hr),
1431                F=[ 0.00 ] (mm),
1432                Pervious areas: IAper=[ 4.67 ] (mm), SLPP=[ 0.5 ] (%), LGP=[ 50 ] (m),
1433                MNP=[ 0.250 ], SCP=[ 0 ] (min),
1434                Impervious areas: IAimp=[ 1.57 ] (mm), SLPI=[ 0.5 ] (%),
1435                LGL=[ 261.151 ] (m), MNI=[ 0.013 ], SCI=[ 0 ] (min),
1436                Continuous simulation parameters:
1437                IaRECper=[ 4 ] (hrs), IaRECimp=[ 4 ] (hrs), InterEventTime=[ 12 ] (hrs),
1438                END=- 1
1439 *%-----|-----|
1440 ROUTE RESERVOIR NHYDout=[ "C1-STR" ], NHYDin=[ "C1" ], RDT=[ 1 ] (min),
1441                TABLE of ( OUTFLOW STORAGE ) values
1442                ( cms ) - ( ha-m )
1443                [ 0.000 , 0.000 ]
1444                [ 0.048 , 0.052 ]
1445                [ 0.099 , 0.070 ]
1446                [ 0.136 , 0.080 ]
1447                [ 0.170 , 0.096 ]
1448                [ 0.218 , 0.102 ]
1449                [ 0.252 , 0.111 ]
1450                [ -1 , -1 ] (max twenty pts)
1451                NHYDovf=[ "C1-OVF" ]
1452 *%-----|-----|
1453 CONTINUOUS STANDHYD NHYD=[ "ST-5" ], DT=[ 1 ] min, AREA=[ 0.45 ] (ha), XI MP=[ 0.46 ],
1454                TI MP=[ 0.57 ], DWF=[ 0 ] (cms), LOSS=[ 1 ]:

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1450      Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
1451      F=[ 0.00](mm),
1452      Pervious areas: IAper=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 50](m),
1453      MNP=[ 0.250], SCP=[ 0](min),
1454      Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 0.5](%), LGI=[ 94.868](m),
1455      MNI=[ 0.013], SCI=[ 0](min),
1456      Continuous simulation parameters:
1457      IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
1458      END=- 1
1459
1460 *%-----|-----|
1461 ROUTE RESERVOIR      NHYDout=[ "ST5STR"], NHYDin=[ "ST-5"], RDT=[ 1](min),
1462      TABLE of ( OUTFLOW STORAGE ) values
1463      (cms) - (ha-m)
1464      [ 0.000 , 0.0000 ]
1465      [ 0.040 , 0.0010 ]
1466      [ 0.041 , 0.0062 ]
1467      [ -1 , -1 ] (max twenty pts)
1468      NHYDovf=[ "ST5OVF"]
1469
1470 *%-----|-----|
1471 ADD HYD              NHYDsum=[ "ST5-E"], NHYDsto
1472      add=[ "DRAIN3"+"D3"+"C1-STR"+"C1-OVF"+"ST5STR"+"ST5OVF"]
1473
1474 *%-----|-----|
1475 CONTINUOUS STANDHYD NHYD=[ "STRAND"], DT=[ 1](min), AREA=[ 7.59](ha),
1476      XI MP=[ 0.64], TI MP=[ 0.85], DWF=[ 0](cms), LOSS=[ 1]:
1477      Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
1478      F=[ 0.00](mm),
1479      Pervious areas: IAper=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 40](m),
1480      MNP=[ 0.250], SCP=[ 0](min),
1481      Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 0.5](%), LGI=[ 1230](m),
1482      MNI=[ 0.013], SCI=[ 0](min),
1483      Continuous simulation parameters:
1484      IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
1485      END=- 1
1486
1487 *%-----|-----|
1488 ROUTE RESERVOIR      NHYDout=[ "S-POND"], NHYDin=[ "STRAND"], RDT=[ 1](min),
1489      TABLE of ( OUTFLOW STORAGE ) values
1490      (cms) - (ha-m)
1491      [ 0.000 , 0.000 ]
1492      [ 0.033 , 0.188 ]
1493      [ 0.057 , 0.253 ]
1494      [ 0.104 , 0.287 ]
1495      [ 0.160 , 0.336 ]
1496      [ 0.340 , 0.346 ]
1497      [ 0.471 , 0.360 ]
1498      [ 0.824 , 0.390 ]
1499      [ -1 , -1 ] (max twenty pts)
1500      NHYDovf=[ "S-OVF"]
1501
1502 *%-----|-----|
1503 ADD HYD              NHYDsum=[ "SSAOUT"], NHYDsto add=[ "ST5-E"+"S-POND"+"S-OVF"]
1504
1505 *%-----|-----|
1506 SAVE HYD             NHYD=[ "SSAOUT"], # OF PCYCLES=[ 5], ICASEsh=[ 1]
1507      HYD_COMMENT=[ "SSAOUT"]
1508
1509 *%-----|-----|
1510 CONTINUOUS STANDHYD NHYD=[ "Area-A"], DT=[ 1]min, AREA=[ 66.75](ha), XI MP=[ 0.64],
1511      TI MP=[ 0.80], DWF=[ 0](cms), LOSS=[ 1]:
1512      Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
1513      F=[ 0.00](mm),
1514      Pervious areas: IAper=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 50](m),
1515      MNP=[ 0.250], SCP=[ 0](min),
1516      Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 0.5](%),
1517      LGI=[ 1155.422](m), MNI=[ 0.013], SCI=[ 0](min),
1518      Continuous simulation parameters:
1519      IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
1520      END=- 1
1521
1522 *%-----|-----|
1523 SAVE HYD             NHYD=[ "Area-A"], # OF PCYCLES=[ 1], ICASEsh=[ 1]

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1502 HYD_COMMENT=[ " SMMF- A Inflow" ]
1503 *%-----|-----|
1504 ROUTE RESERVOIR NHYDout=[ " SMMF- A" ], NHYDin=[ " Area- A" ], RDT=[ 1 ] (mi n),
1505 TABLE of ( OUTFLOW STORAGE ) values
1506 ( cms ) - ( ha- m)
1507 [ 0.000 , 0.000 ]
1508 [ 0.103 , 1.077 ]
1509 [ 0.128 , 1.749 ]
1510 [ 0.382 , 2.282 ]
1511 [ 0.703 , 2.582 ]
1512 [ 1.256 , 2.978 ]
1513 [ 1.567 , 3.202 ]
1514 [ 1.955 , 3.493 ]
1515 [ 2.100 , 3.600 ]
1516 [ -1 , -1 ] (max twenty pts)
1517 NHYDovf=[ " SWWAOV" ]
1518 *%-----|-----|
1519 SAVE HYD NHYD=[ " SMMF- A" ], # OF PCYCLES=[ 1 ], ICASEsh=[ 1 ]
1520 HYD_COMMENT=[ " SMMF- A Outflow" ]
1521 *%-----|-----|
1522 *ANALYSIS POINT 4 - TOTAL FLOW AT OUTLET OF STREET 5
1523 *%-----|-----|
1524 ADD HYD NHYDs um=[ " PT4ST5" ], NHYDs to add=[ " SSAOUT" + " SMMF- A" + " SWWAOV" ]
1525 *%-----|-----|
1526 CONTINUOUS STANDHYD NHYD=[ " C6" ], DT=[ 1 ] mi n, AREA=[ 1.87 ] (ha), XI MP=[ 0.68 ], TI MP=[ 0.85 ],
DWF=[ 0 ] (cms), LOSS=[ 1 ]:
1527 Horton: Fo=[ 76.20 ] (mm/ hr), Fc=[ 13.20 ] (mm/ hr), DCAY=[ 4.14 ] (/ hr),
F=[ 0.00 ] (mm),
1528 Pervious areas: I A per=[ 4.67 ] (mm), SLPP=[ 0.5 ] (%), LGP=[ 50 ] (m),
MNP=[ 0.250 ], SCP=[ 0 ] (mi n),
1529 Impervious areas: I A i mp=[ 1.57 ] (mm), SLPI=[ 0.5 ] (%),
LGI=[ 193.391 ] (m), MNI=[ 0.013 ], SCI=[ 0 ] (mi n),
1530 Continuous simulation parameters:
1531 I a REC per=[ 4 ] (hr s), I a REC i mp=[ 4 ] (hr s), I nter Event Ti me=[ 12 ] (hr s),
END=- 1
1532 *%-----|-----|
1533 ROUTE RESERVOIR NHYDout=[ " C6- STR" ], NHYDin=[ " C6" ], RDT=[ 1 ] (mi n),
1534 TABLE of ( OUTFLOW STORAGE ) values
1535 ( cms ) - ( ha- m)
1536 [ 0.000 , 0.000 ]
1537 [ 0.026 , 0.029 ]
1538 [ 0.054 , 0.038 ]
1539 [ 0.075 , 0.044 ]
1540 [ 0.093 , 0.052 ]
1541 [ 0.120 , 0.056 ]
1542 [ 0.138 , 0.061 ]
1543 [ -1 , -1 ] (max twenty pts)
1544 NHYDovf=[ " C6- OVF" ]
1545 *%-----|-----|
1546 CONTINUOUS STANDHYD NHYD=[ " C7" ], DT=[ 1 ] mi n, AREA=[ 1.62 ] (ha), XI MP=[ 0.68 ], TI MP=[ 0.85 ],
DWF=[ 0 ] (cms), LOSS=[ 1 ]:
1547 Horton: Fo=[ 76.20 ] (mm/ hr), Fc=[ 13.20 ] (mm/ hr), DCAY=[ 4.14 ] (/ hr),
F=[ 0.00 ] (mm),
1548 Pervious areas: I A per=[ 4.67 ] (mm), SLPP=[ 0.5 ] (%), LGP=[ 50 ] (m),
MNP=[ 0.250 ], SCP=[ 0 ] (mi n),
1549 Impervious areas: I A i mp=[ 1.57 ] (mm), SLPI=[ 0.5 ] (%),
LGI=[ 180.000 ] (m), MNI=[ 0.013 ], SCI=[ 0 ] (mi n),
1550 Continuous simulation parameters:
1551 I a REC per=[ 4 ] (hr s), I a REC i mp=[ 4 ] (hr s), I nter Event Ti me=[ 12 ] (hr s),
END=- 1
1552 *%-----|-----|
1553 ROUTE RESERVOIR NHYDout=[ " C7- STR" ], NHYDin=[ " C7" ], RDT=[ 1 ] (mi n),
1554 TABLE of ( OUTFLOW STORAGE ) values
1555 ( cms ) - ( ha- m)
1556 [ 0.000 , 0.000 ]
1557 [ 0.023 , 0.025 ]

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1558         [ 0.047 , 0.033 ]
1559         [ 0.065 , 0.038 ]
1560         [ 0.081 , 0.045 ]
1561         [ 0.104 , 0.048 ]
1562         [ 0.120 , 0.053 ]
1563         [ -1 , -1 ] (max twenty pts)
1564         NHYDovf=["C7-OVF"]
1565 *%-----|-----|
1566 CONTINUOUS STANDHYD NHYD=["ST-6"], DT=[1] min, AREA=[0.41](ha), XI MP=[0.46], TI MP=[0.57],
DWF=[0](cms), LOSS=[1]:
1567 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1568 Pervious areas: I A per=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1569 Impervious areas: I A i mp=[1.57](mm), SLPI=[0.5](%), LGI=[90.554](m),
MNI=[0.013], SCI=[0](min),
1570 Continuous simulation parameters:
1571 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
1572 *%-----|-----|
1573 ROUTE RESERVOIR NHYDout=["ST6STR"], NHYDin=["ST-6"], RDT=[1](min),
1574 TABLE of ( OUTFLOW STORAGE ) values
1575 (cms) - (ha-m)
1576 [ 0.000 , 0.0000 ]
1577 [ 0.036 , 0.0010 ]
1578 [ 0.037 , 0.0058 ]
1579 [ -1 , -1 ] (max twenty pts)
1580 NHYDovf=["ST6OVF"]
1581 *%-----|-----|
1582 *ANALYSIS POINT 5 - TOTAL FLOW AT OUTLET OF STREET 6
1583 *%-----|-----|
1584 ADD HYD NHYDsum=["PT5ST6"], NHYDs to
add=["PT4ST5"+"C6-STR"+"C6-OVF"+"C7-STR"+"C7-OVF"+"ST6STR"+"ST6OVF"]
1585 *%-----|-----|
1586 *ROUTE FLOW through O Keefe Drain 4
1587 ROUTE CHANNEL NHYDout=["DRAI N4"], NHYDin=["PT5ST6"], RDT=[1](min),
1588 CHLGTH=[324](m), CHSLOPE=[.10](%), FPSLOPE=[.10](%),
1589 SECNUM=[1], NSEG=[3]
1590 ( SEGROUGH, SEGDI ST (m))=[0.07, 12.00 -0.043, 18.00 0.07, 30.00] NSEG
t i m e s
1591 ( DI STANCE (m), ELEVATI ON (m))=[0.00, 2.00]
1592 (2.00, 1.20)
1593 (12.00, 1.00)
1594 (14.00, 0.00)
1595 (16.00, 0.00)
1596 (18.00, 1.00)
1597 (28.00, 1.20)
1598 (30.00, 2.00)
1599 *%-----|-----|
1600 CONTINUOUS NASHYD NHYD=["D4"], DT=[1] min, AREA=[1.73](ha), DWF=[0](cms), CNV C=[88],
I A=[8.4](mm),
1601 N=[3], TP=[0.60] hrs,
1602 Continuous simulation parameters:
1603 I a REC per=[4](hrs),
1604 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1605 I n t e r E v e n t T i m e=[12](hrs)
1606 Baseflow simulation parameters:
1607 BaseFl owOpt i on=[1] ,
1608 I n i t GWR es Vol=[50](mm), GWR es K=[0.96](mm/day/mm)
1609 VHydCond=[0.055](mm/hr), END=-1
1610 *%-----|-----|
1611 CONTINUOUS STANDHYD NHYD=["Area-B"], DT=[1] min, AREA=[24.04](ha), XI MP=[0.62],
TI MP=[0.77], DWF=[0](cms), LOSS=[1]:
1612 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1613 Pervious areas: I A per=[4.67](mm), SLPP=[1.4](%), LGP=[50](m),

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1614 MNP=[ 0.250], SCP=[ 0](mi n),
Impervious areas: IAImp=[ 1.57](mm), SLPI=[ 1.4](%),
LGI=[ 693.397](m), MNI=[ 0.013], SCI=[ 0](mi n),
1615 Continuous simulation parameters:
1616 IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
END=- 1

1617 *%-----|-----|
1618 ROUTE RESERVOIR NHYDout=["SWMF- B"], NHYDin=["Area- B"], RDT=[ 1](mi n),
1619 TABLE of ( OUTFLOW STORAGE ) values
1620 (cms) - (ha- m)
1621 [ 0.000 , 0.000 ]
1622 [ 0.025 , 0.090 ]
1623 [ 0.175 , 0.510 ]
1624 [ 0.350 , 0.710 ]
1625 [ 0.495 , 0.820 ]
1626 [ 0.648 , 0.980 ]
1627 [ 0.965 , 1.045 ]
1628 [ 1.072 , 1.140 ]
1629 [ -1 , -1 ] (max twenty pts)
1630 NHYDovf=["SWMBOVF"]

1631 *%-----|-----|
1632 ADD HYD NHYDs um=["D4- EX"], NHYDs to add=["DRAIN4"+"D4"+"SWMF- B"+"SWMBOVF"]
1633 *%-----|-----|
1634 *ROUTE FLOW THROUGH O Keefe Drain 5
1635 * JFSA: Nov. 2020, added en points to close X-Section
1636 ROUTE CHANNEL NHYDout=["DRAIN5"], NHYDin=["D4- EX"], RDT=[ 1](mi n),
1637 CHLGTH=[ 413.0](m), CHSLOPE=[ 0.16](%), FPSLOPE=[ 0.16](%),
1638 SECNUM=[ 1], NSEG=[ 3]
1639 ( SEGROUGH, SEGDIST (m))=[ 0.043, 12.29 - 0.033, 17.97
1640 0.043, 32.84] NSEG times
1641 ( DISTANCE (m), ELEVATION (m))=(- 0.01, 2.50)
1642 [ 0.00, 1.41]
1643 [ 6.13, 0.97]
1644 [ 12.29, 0.89]
1645 [ 15.71, 0.00]
1646 [ 17.97, 0.39]
1647 [ 23.04, 0.35]
1648 [ 32.83, 0.96]
1649 ( 32.84, 2.50)

1650 *%-----|-----|
1651 CONTINUOUS NASHYD NHYD=["D5"], DT=[ 1]mi n, AREA=[ 1.90](ha),
1652 DWF=[ 0](cms), CN/C=[ 86], IA=[ 8.7](mm), N=[ 3], TP=[ 0.69]hrs,
1653 Continuous simulation parameters:
1654 IARECper=[ 4](hrs),
1655 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1656 InterEventTime=[ 12](hrs)
1657 Baseflow simulation parameters:
1658 BaseFlowOption=[ 1],
1659 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
1660 VHydCond=[ 0.055](mm/hr), END=- 1

1661 *%-----|-----|
1662 *EXTERNAL FLOWS SOUTHEAST OF THE SITE NORTH OF McKenna Casey Dr.
1663 CONTINUOUS NASHYD NHYD=["O- 13SDF"], DT=[ 1]mi n, AREA=[ 9.74](ha),
1664 DWF=[ 0](cms), CN/C=[ 81], IA=[ 4.0](mm), N=[ 3], TP=[ .43]hrs,
1665 Continuous simulation parameters:
1666 IARECper=[ 4](hrs),
1667 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1668 InterEventTime=[ 12](hrs)
1669 Baseflow simulation parameters:
1670 BaseFlowOption=[ 1],
1671 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
1672 VHydCond=[ 0.055](mm/hr), END=- 1

1673 *%-----|-----|
1674 *SNOW DISPOSAL FACILITY
1675 *PARAMETERS BASED ON ROBINSON 2006 MODEL
1676 ROUTE RESERVOIR NHYDout=["SDF"], NHYDin=["O- 13SDF"], RDT=[ 1](mi n),

```

```

1677          TABLE of ( OUTFLOW STORAGE ) values
1678                ( cms ) - ( ha-m)
1679                [ 0.000, 0.000]
1680                [ 0.150, 0.600]
1681                ( 0.200, 1.500)
1682                [ -1 , -1 ] (max twenty pts)
1683                NHYDovf=[ "OVFSDF" ]
1684 *%-----|-----|
1685 *ANALYSIS POINT 6 - McKenna Casey Dr.
1686 *%-----|-----|
1687 ADD HYD          NHYDs um=[ "PT6MC" ], NHYDs to add=[ "DRAIN5"+"D5"+"SDF" ]
1688 *%-----|-----|
1689 CONTINUOUS NASHYD NHYD=[ "O-15" ], DT=[ 1] min, AREA=[ 10.67] (ha),
1690                DWF=[ 0] (cms), CNVC=[ 82], IA=[ 7.5] (mm), N=[ 3], TP=[ 0.30] hrs,
1691                Continuous simulation parameters:
1692                IARECper=[ 4] (hrs),
1693                SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
1694                InterEventTime=[ 12] (hrs)
1695                Baseflow simulation parameters:
1696                BaseFlowOption=[ 1] ,
1697                InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/day/mm)
1698                VHydCond=[ 0.055] (mm/hr), END=- 1
1699 *%-----|-----|
1700 *TOTAL FLOW NORTH OF MCKENNA CASEY DR.
1701 ADD HYD          NHYDs um=[ "MC" ], NHYDs to add=[ "PT6MC"+"O-15" ]
1702 *%-----|-----|
1703 *ROUTE FLOW THROUGH AREA O-14
1704 * JFSA: Nov. 2020, added end points to close X-section
1705 ROUTE CHANNEL   NHYDout=[ "O-14Ch" ], NHYDin=[ "MC" ], RDT=[ 1] (min),
1706                CHLGH=[ 845.3] (m), CHSLOPE=[ 0.10] (%), FPSLOPE=[ 0.10] (%),
1707                SECNUM=[ 1], NSEG=[ 3]
1708                ( SEGROUGH, SEGDI ST (m) )=[ 0.06, 15.00 -0.033, 18.04 0.06, 31.85] NSEG
1709                times
1710                ( DISTANCE (m), ELEVATION (m) )=[ -0.01, 2.5
1711                ( 0.00, 1.53]
1712                ( 5.56, 1.47)
1713                ( 9.21, 1.45)
1714                ( 12.45, 1.53)
1715                ( 13.70, 1.50)
1716                ( 15.00, 0.69)
1717                ( 15.34, 0.00)
1718                ( 16.51, 0.05)
1719                ( 17.30, 0.17)
1720                ( 18.04, 0.74)
1721                ( 19.29, 1.32)
1722                ( 22.73, 1.47)
1723                ( 31.84, 1.41)
1724                ( 31.85, 2.50)
1725 *%-----|-----|
1726 *% -Change O-14 from NASHYD to STANDHYD, name it "S-1-Okeefe" and add it to S-1
1727 subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
1728 *% -JFSA 2021-02-16, add detailed subcatchment drainage area for each subcatchment
1729 in Corrigan sub-catchment. After adding part of O-14 to S_1 sub-catchment so O-14
1730 becomes 5 ha instead of 30.02 ha and TP becomes 0.133 (5*0.8/30.02) instead of 0.8
1731 CONTINUOUS NASHYD NHYD=[ "O-14" ], DT=[ 1] min, AREA=[ 5] (ha),
1732                DWF=[ 0] (cms), CNVC=[ 82], IA=[ 7.5] (mm), N=[ 3], TP=[ 0.133] hrs,
1733                Continuous simulation parameters:
1734                IARECper=[ 4] (hrs),
1735                SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
1736                InterEventTime=[ 12] (hrs)
1737                Baseflow simulation parameters:
1738                BaseFlowOption=[ 1] ,
1739                InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/day/mm)
1740                VHydCond=[ 0.055] (mm/hr), END=- 1
1741 *
1742 *%-----|-----|

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1739 *ANALYSIS POINT 7 - JOCK RIVER
1740 * 2020-12-01 To Foster Drain
1741 * 2020-12-01 replace ("PT7JR") by ("OKEEFE")
1742 *%-----|-----
1743 ADD HYD          NHYDs um=["OKEEFE"], NHYDs to add=["O-14Ch"+"O-14"]
1744 *%-----|-----
1745 *CONTINUOUS STANDHYD NHYD=["OKEEFE"], DT=[1](min), AREA=[448](ha),
1746 *                XI MP=[0.65], TI MP=[0.65], DWF=[0](cms), LOSS=[2],
1747 *                SCS curve number CN=[77],
1748 *                Pervious surfaces: I A per=[4.67](mm), SLPP=[0.5](%),
1749 *                LGP=[40](m), MNP=[0.25], SCP=[0](min),
1750 *                Impervious surfaces: I A i mp=[1.57](mm), SLPI=[0.5](%),
1751 *                LGI=[1728](m), MNI=[0.013], SCI=[0](min),
1752 *                Continuous simulation parameters:
1753 *                I a RE C per=[4](hrs), I a RE C i mp=[4](hrs),
1754 *                SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1755 *                Inter Event Ti me=[18](hrs), END=-1
1756 *#*****
1757 *#      Okeefe Pond
1758 *#      - Rating curve obtained assuming 40m³/ha in 24 hours for quality control
1759 *#      and a ratio of the catchment area to the West Clarke pond rating curve
1760 *#      from the M5S for the next coordinates
1761 *#*****
1762 *ROUTE RESERVOIR  NHYDout=["P_OKE"], NHYDin=["OKEEFE"],
1763 *                RDT=[1](min),
1764 *                TABLE of ( OUTFLOW STORAGE ) values
1765 *                ( cms ) - ( ha-m )
1766 *                [ 0.0 , 0.0 ]
1767 *                [ 14.13 , 13.0 ]
1768 *                [ -1 , -1 ] (maximum one hundred pairs of points)
1769 *                NHYDovf=["ok-OVF"],
1770 *%-----|-----
1771 * -JFSA 2021-02-25 "S-1-D2" and "S-1-D3" are part of S-1 sub-catchment. They are
1772 * moved to drain before station 6215 on Jock River
1773 *CONTINUOUS STANDHYD NHYD=["S-1-D2"], DT=[1](min), AREA=[18.67](ha), XI MP=[0.65],
1774 *                TI MP=[0.65], DWF=[0](cms),
1775 *                LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
1776 *                I A per=[4.67](mm), SLPP=[2.0](%),
1777 *                LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
1778 *                I A i mp=[1.57](mm), SLPI=[0.75](%),
1779 *                LGI=[352.798](m), MNI=[0.013], SCI=[0](min),
1780 *                Continuous simulation parameters:
1781 *                I a RE C per=[4](hrs), I a RE C i mp=[4](hrs),
1782 *                SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1783 *                Inter Event Ti me=[12](hrs), END=-1
1784 *%-----|-----
1785 *CONTINUOUS NASHYD  NHYD=["S-1-D2"], DT=[1]min, AREA=[18.67](ha),
1786 *                DWF=[0](cms), CN C=[77], I A=[4.67](mm),
1787 *                N=[3], TP=[1.120]hrs,
1788 *                Continuous simulation parameters:
1789 *                I a RE C per=[4](hrs),
1790 *                SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1791 *                Inter Event Ti me=[12](hrs)
1792 *                Baseflow simulation parameters:
1793 *                BaseFl owOpt ion=[1],
1794 *                I ni t GWRes Vol=[50](mm), GWRes K=[0.96](mm/day/mm)
1795 *                VHydCond=[0.055](mm/hr), END=-1
1796 *%-----|-----
1797 *COMPUTE DUALHYD  NHYDin=["S-1-D2"], CI NLET=[2.097](cms), NI NLET=[1],
1798 *                M a j NHYD=["S-1-D2J"]
1799 *                M n NHYD=["S-1-D2N"]
1800 *                TMJ STO=[9999999](cu-m)
1801 *%-----|-----
1802 *ADD HYD          NHYDs um=["S-1-D2S"], NHYDs to add=["S-1-D2J"+"S-1-D2N"]
1803 *%-----|-----

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1800 ROUTE RESERVOIR      NHYDout =[" S- 1- D2R" ] , NHYDin=[" S- 1- D2S" ] ,
1801                      RDT=[ 1 ] (mi n) ,
1802                      TABLE of ( OUTFLOW STORAGE ) values
1803                          ( cms ) - ( ha- m)
1804                          [ 0. 0      , 0. 0 ]
1805                          [ 0. 2231, 0. 7445 ]
1806                          [   -1   ,  -1   ] (max twenty pts)
1807                      NHYDovf=[" S- 1- D2Rovf" ]
1808 *%-----|-----|
1809 CONTINUOUS STANDHYD NHYD=[" S- 1- D3" ], DT=[ 1 ] (mi n) , AREA=[ 6. 79 ] (ha) , XI MP=[ 0. 65 ] ,
TI MP=[ 0. 65 ] , DWF=[ 0 ] (cms) ,
1810 LOSS=[ 2 ] , SCS curve number CN=[ 75 ] , Pervious surfaces:
I Aper=[ 4. 67 ] (mm) , SLPP=[ 2. 0 ] ( % ) ,
1811 LGP=[ 40 ] (m) , MNP=[ 0. 25 ] , SCP=[ 0 ] (mi n) , Impervious surfaces:
I Ai mp=[ 1. 57 ] (mm) , SLPI=[ 0. 75 ] ( % ) ,
1812 LGI=[ 212. 760 ] (m) , MNI=[ 0. 013 ] , SCI=[ 0 ] (mi n) ,
1813 Continuous simulation parameters:
1814 IaREcper=[ 4 ] (hrs) , IaRECI mp=[ 4 ] (hrs) ,
1815 SM N=[ - 1 ] (mm) , SMAX=[ - 1 ] (mm) , SK=[ 0. 010 ] / (mm) ,
1816 InterEvent Time=[ 12 ] (hrs) , END=- 1
1817 *%-----|-----|
1818 *CONTINUOUS NASHYD  NHYD=[" S- 1- D3" ], DT=[ 1 ] mi n , AREA=[ 6. 79 ] (ha) ,
1819 * DWF=[ 0 ] (cms) , CN C=[ 77 ] , IA=[ 4. 67 ] (mm) ,
1820 * N=[ 3 ] , TP=[ 1. 281 ] hrs ,
1821 * Continuous simulation parameters:
1822 * IaREcper=[ 4 ] (hrs) ,
1823 * SM N=[ - 1 ] (mm) , SMAX=[ - 1 ] (mm) , SK=[ 0. 010 ] / (mm) ,
1824 * InterEvent Time=[ 12 ] (hrs)
1825 * Baseflow simulation parameters:
1826 * BaseFl owOpt ion=[ 1 ] ,
1827 * Ini t GWRes Vol =[ 50 ] (mm) , GWRes K=[ 0. 96 ] (mm/ day/ mm)
1828 * VHydCond=[ 0. 055 ] (mm/ hr) , END=- 1
1829 *%-----|-----|
1830 COMPUTE DUALHYD      NHYDin=[" S- 1- D3" ], CI NLET=[ 0. 831 ] (cms) , NI NLET=[ 1 ] ,
1831 M aj NHYD=[" S- 1- D3J" ]
1832 M nNHYD=[" S- 1- D3N" ]
1833 TM S TO=[ 9999999 ] (cu- m)
1834 *%-----|-----|
1835 ADD HYD              NHYDsum=[" S- 1- D3S" ], NHYDs to add=[" S- 1- D3J "+" S- 1- D3N" ]
1836 *%-----|-----|
1837 ROUTE RESERVOIR      NHYDout =[" S- 1- D3R" ] , NHYDin=[" S- 1- D3S" ] ,
1838                      RDT=[ 1 ] (mi n) ,
1839                      TABLE of ( OUTFLOW STORAGE ) values
1840                          ( cms ) - ( ha- m)
1841                          [ 0. 0      , 0. 0 ]
1842                          [ 0. 0811, 0. 2708 ]
1843                          [   -1   ,  -1   ] (max twenty pts)
1844                      NHYDovf=[" S- 1- D3Rovf" ]
1845 *%-----|-----|
1846 ADD HYD              NHYDsum=[" SN_ OK" ], NHYDs to
add=[" "_N_ OK" +" OKEEFE" +" S- 1- D2R" +" S- 1- D3R" +" S- 1- D2Rovf" +" S- 1- D3Rovf" ]
1847 *%-----|-----|
1848 SAVE HYD            NHYD=[" SN_ OK" ], # OF PCYCLES=[ - 1 ] , I CASEs h=[ 1 ]
1849 HYD_ COMMENT=[" Tot al Fl ows at Okeefe Dr ai n" ]
1850 *%-----|-----|
1851 *#
1852 *# Hydrograph from Node Okeefe routed to Node at Foster Drain
1853 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
1854 *#
1855 ROUTE CHANNEL        NHYDout =[" N_ FO" ] , NHYDin=[" SN_ OK" ] ,
1856                      RDT=[ 1 ] (mi n) ,
1857                      CHLGTH=[ 1183 ] (m) , CHSLOPE=[ 0. 0761 ] ( % ) ,
1858                      FPSLOPE=[ 0. 0761 ] ( % ) ,
1859                      SECNUM=[ 1. 0 ] , NSEG=[ 3 ]
1860                      ( SEGROUGH, SEGDI ST (m) ) =
1861                      [ 0. 050, - 33. 89

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1862         - 0.035, 31.59
1863         0.050, 34.41] NSEG times
1864         ( DISTANCE (m), ELEVATION (m)) =
1865         [- 794.18, 91.00]
1866         [- 775.41, 91.50]
1867         [- 702.63, 91.50]
1868         [- 546.19, 91.50]
1869         [- 529.54, 91.50]
1870         [- 323.44, 91.00]
1871         [- 320.71, 91.00]
1872         [- 183.59, 91.00]
1873         [- 182.54, 90.50]
1874         [- 181.36, 90.00]
1875         [- 177.37, 90.00]
1876         [- 87.70, 90.00]
1877         [- 33.89, 90.00]
1878         [- 18.52, 86.88]
1879         [0.00, 85.20]
1880         [16.20, 86.83]
1881         [31.59, 90.00]
1882         [33.03, 90.50]
1883         [34.41, 91.00]
1884 *%-----|-----|
1885 *#*****|
1886 *#   Catchment FOSTER
1887 *#   - To Foster ditch (north of the Jock)
1888 *#   - Partially developed (medium density); remaining agricultural
1889 *#   - 2020-12-01 JFSA Foster area is 332 as per Foster SWWF Environmental Study
1890 *#   - 2020-12-01 decrease Foster drainage area from (373 HA) to (307.98 HA) after
1891 *#   - 2021-02-12 update Foster area to 325.44 ha as measured from QGIS
1892 *#*****|
1893 CONTINUOUS STANDHYD NHYD=["FOSTER"], DT=[1] min, AREA=[325.44] (ha),
1894 XI MP=[0.55], TI MP=[0.55], DWF=[0] (cms), LOSS=[2],
1895 SCS curve number CN=[74],
1896 Pervious surfaces: I A per=[4.67] (mm), SLPP=[0.5] (%),
1897                 LGP=[40] (m), MNP=[0.25], SCP=[0] (min),
1898 Impervious surfaces: I A i mp=[1.57] (mm), SLPI=[0.5] (%),
1899                 LGI=[1472.956] (m), MNI=[0.013], SCI=[0] (min),
1900 Continuous simulation parameters:
1901 I a REC per=[4] (hrs), I a REC i mp=[4] (hrs),
1902 SM N=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1903 I n t e r E v e n t T i m e=[18] (hrs), E N D=-1
1904 *#*****|
1905 *#   Foster Pond
1906 *#   - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1907 *#   and a ratio of the catchment area to the West Clarke pond rating curve
1908 *#   from the MS for the next coordinates
1909 *#*****|
1910 ROUTE RESERVOIR NHYDout=["P_FOS"], NHYDin=["FOSTER"],
1911 RDT=[1] (min),
1912         TABLE of ( OUTFLOW STORAGE ) values
1913         ( cms ) - ( ha-m)
1914         [ 0.0 , 0.0 ]
1915         [ 10.34 , 10]
1916         [ -1 , -1 ] (max twenty pts)
1917         NHYDovf=["FO-OVF"]
1918 *%-----|-----|
1919 ADD HYD NHYDsum=["FOSTER-OUT"], NHYDs to add=["P_FOS"+"FO-OVF"]
1920 *%-----|-----|
1921 *#*****|
1922 *   -Brazeau area from P 1800-19 =[71.751], change to 63.59 ha based on GIS measurements
1923 *   -JFSA, 2021-01-19 update "W_CLAR_BRAZ" to 73.29 ha based on GIS measurements
1924 *   -JFSA, 2021-01-22 Brazeau ("MS_P10"+"P10-OVF")brazeau pond discharges directly

```


to the jock river through a road side ditch on the west side of Borrisokane road (station 6016)

1925 CONTINUOUS STANDHYD NHYD=["W_CLAR_BRAZ"], DT=[1] min, AREA=[73.29] (ha),
1926 XI MP=[0.6], TI MP=[0.65], DWF=[0] (cms), LOSS=[2],
1927 SCS curve number CN=[77],
1928 Pervious surfaces: I A per=[4.67] (mm), SLPP=[1] (%),
1929 LGP=[40] (m), MNP=[0.25], SCP=[0] (min),
1930 Impervious surfaces: I A i mp=[1.57] (mm), SLPI=[0.5] (%),
1931 LGI=[699.00] (m), MNI=[0.013], SCI=[0] (min),
1932 Continuous simulation parameters:
1933 I a REC per=[4] (hrs), I a REC i mp=[4] (hrs),
1934 SM N=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1935 Inter Event Time=[18] (hrs), END=-1

*%-----|-----|

* 2020-12-01 correct pond curve values

1938 ROUTE RESERVOIR NHYDout=["MS_P10"], NHYDin=["W_CLAR_BRAZ"],
1939 RDT=[1] (min),

TABLE of (OUTFLOW STORAGE) values

	(cms) - (ha - m)
1941	[0.0 , 0.0]
1942	[0.068 , 0.001]
1943	[0.271 , 0.022]
1944	[0.379 , 0.051]
1945	[0.48 , 0.091]
1946	[0.853 , 0.341]
1947	[1.005 , 0.61]
1948	[1.128 , 1.231]
1949	[1.155 , 1.592]
1950	[1.194 , 1.876]
1951	[1.2 , 1.921]
1952	[1.259 , 2.369]
1953	[1.3 , 2.665]
1954	[1.349 , 2.813]
1955	[-1 , -1] (max twenty pts)

NHYDovf=["P10-OVF"]

*%-----|-----|

* -JFSA 2021-02-26 "S-1-FO-D2" is a part of S-1 sub-catchment. It is moved to drain before station 980 on Foster Drain

1960 CONTINUOUS STANDHYD NHYD=["S-1-FO-D2"], DT=[1] min, AREA=[4.94] (ha),
1961 XI MP=[0.55], TI MP=[0.55], DWF=[0] (cms), LOSS=[2],
1962 SCS curve number CN=[74],
1963 Pervious surfaces: I A per=[4.67] (mm), SLPP=[0.5] (%),
1964 LGP=[40] (m), MNP=[0.25], SCP=[0] (min),
1965 Impervious surfaces: I A i mp=[1.57] (mm), SLPI=[0.5] (%),
1966 LGI=[181.475] (m), MNI=[0.013], SCI=[0] (min),
1967 Continuous simulation parameters:
1968 I a REC per=[4] (hrs), I a REC i mp=[4] (hrs),
1969 SM N=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1970 Inter Event Time=[18] (hrs), END=-1

*%-----|-----|

1972 *CONTINUOUS NASHYD NHYD=["S-1-FO-D2"], DT=[1] min, AREA=[4.94] (ha),
1973 * DWF=[0] (cms), CN/C=[77], I A=[4.67] (mm),
1974 * N=[3], TP=[1.10] hrs,
1975 * Continuous simulation parameters:
1976 * I a REC per=[4] (hrs),
1977 * SM N=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1978 * Inter Event Time=[12] (hrs)
1979 * Baseflow simulation parameters:
1980 * BaseFlowOption=[1],
1981 * I n i t GWR es Vol =[50] (mm), GWR es K=[0.96] (mm/day/mm)
1982 * VHydCond=[0.055] (mm/hr), END=-1

*%-----|-----|

1984 COMPUTE DUALHYD NHYDin=["S-1-FO-D2"], CI NLET=[0.508] (cms), NI NLET=[1],
1985 M i j NHYD=["S-1-FO-D2J"]
1986 M nNHYD=["S-1-FO-D2N"]
1987 T M I STO=[9999999] (cu-m)

```

1988 *%-----|-----|
1989 ADD HYD          NHYDsum=[ "S- 1- FO- D2S" ], NHYDs to add=[ "S- 1- FO- D2J" +"S- 1- FO- D2N" ]
1990 *%-----|-----|
1991 ROUTE RESERVOIR  NHYDout=[ "S- 1- FO- D2R" ] , NHYDin=[ "S- 1- FO- D2S" ] ,
1992                   RDT=[ 1 ] ( mi n ) ,
1993                   TABLE of ( OUTFLOW STORAGE ) values
1994                   ( cms ) - ( ha- m )
1995                   [ 0.0      , 0.0 ]
1996                   [ 0.0590, 0.1970 ]
1997                   [      -1 , -1      ] (max t went y pts)
1998                   NHYDovf=[ "S- 1FOD2ovf" ]
1999 *%-----|-----|
2000 ADD HYD          NHYDsum=[ "980" ], NHYDs to
add=[ "FOSTER- OUT" +"S- 1- FO- D2R" +"S- 1FOD2ovf" ]
2001 *%-----|-----|
2002 SAVE HYD        NHYD=[ "980" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
2003                 HYD_COMMENT=[ "Total Flows at Station 980 on Foster Drain" ]
2004 *%-----|-----|
2005 *#
2006 *# Hydrograph from Node Foster SWM (Station 980) to Node at station 520
2007 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 980
2008 *#
2009 ROUTE CHANNEL   NHYDout=[ "980- out " ] , NHYDin=[ "980" ] ,
2010                 RDT=[ 1 ] ( mi n ) ,
2011                 CHLGTH=[ 460 ] ( m ) ,   CHSLOPE=[ 0.04348 ] ( % ) ,
2012                                     FPSLOPE=[ 0.04348 ] ( % ) ,
2013                 SECNUM=[ 1.0 ] ,   NSEG=[ 3 ]
2014                 ( SEGROUGH, SEGDI ST ( m ) ) =
2015                 [ 0.050, 45.90
2016                 - 0.035, 53.30
2017                 0.050, 100 ] NSEG times
2018                 ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
2019                 [ 0, 91.75 ]
2020                 [ 42.4, 92.18 ]
2021                 [ 43.5, 92.16 ]
2022                 [ 44.1, 92.1 ]
2023                 [ 44.6, 92 ]
2024                 [ 44.8, 91.86 ]
2025                 [ 45.9, 91.04 ]
2026                 [ 46.4, 90.65 ]
2027                 [ 46.8, 90.36 ]
2028                 [ 47.9, 90.32 ]
2029                 [ 48.7, 90.35 ]
2030                 [ 50.7, 90.33 ]
2031                 [ 52.2, 90.38 ]
2032                 [ 52.5, 90.59 ]
2033                 [ 53.3, 91.28 ]
2034                 [ 54, 91.83 ]
2035                 [ 54.3, 92 ]
2036                 [ 54.8, 92.08 ]
2037                 [ 55.4, 92.12 ]
2038                 [ 100, 91.84 ]
2039 *%-----|-----|
2040 * -JFSA 2021-02-26 "S-1-FO-DI" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2041 CONTINUOUS STANDHYD NHYD=[ "S- 1- FO- DI" ], DT=[ 1 ] mi n , AREA=[ 5.11 ] ( ha ) ,
2042                   XI MP=[ 0.65 ] , TI MP=[ 0.65 ] , DWF=[ 0 ] ( cms ) , LOSS=[ 2 ] ,
2043                   SCS curve number CN=[ 74 ] ,
2044                   Pervious surfaces: I A per=[ 4.67 ] ( mm ) , SLPP=[ 0.5 ] ( % ) ,
2045                   LGP=[ 40 ] ( m ) , MNP=[ 0.25 ] , SCP=[ 0 ] ( mi n ) ,
2046                   Impervious surfaces: I A i mp=[ 1.57 ] ( mm ) , SLPI=[ 0.5 ] ( % ) ,
2047                   LGI=[ 184.572 ] ( m ) , MNI=[ 0.013 ] , SCI=[ 0 ] ( mi n ) ,
2048                   Continuous simulation parameters:
2049                   I a REC per=[ 4 ] ( hr s ) , I a REC i mp=[ 4 ] ( hr s ) ,
2050                   SM N=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0.010 ] / ( mm ) ,
2051                   Inter Event Ti me=[ 18 ] ( hr s ) ,   END=- 1

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2052 *%-----|-----|
2053 COMPUTE DUALHYD NHYDin=["S-1-FO-DI"], CINLET=[0.605](cms), NINLET=[1],
2054 MajNHYD=["S-1-FO-DIJ"]
2055 MnNHYD=["S-1-FO-DIN"]
2056 TMSTO=[9999999](cu-m)
2057 *%-----|-----|
2058 ADD HYD NHYDsum=["S-1-FO-DIS"], NHYDs to add=["S-1-FO-DIN"+"S-1-FO-DIJ"]
2059 *%-----|-----|
2060 ROUTE RESERVOIR NHYDout=["S-1-FO-DIR"], NHYDin=["S-1-FO-DIS"],
2061 RDT=[1](min),
2062 TABLE of ( OUTFLOW STORAGE ) values
2063 (cms) - (ha-m)
2064 [ 0.0 , 0.0 ]
2065 [ 0.0611, 0.2038 ]
2066 [ -1 , -1 ] (max twenty pts)
2067 NHYDovf=["S-1FODlovf"]
2068 *%-----|-----|
2069 ADD HYD NHYDsum=["520"], NHYDs to add=["980-out"+"S-1-FO-DIR"+"S-1FODlovf"]
2070 *%-----|-----|
2071 SAVE HYD NHYD=["520"], # OF PCYCLES=[-1], ICASEsh=[1]
2072 HYD_COMMENT=["Total Flows at Sation 520 on Foster Drain"]
2073 *%-----|-----|
2074 *# Hydrograph from Node at Station 520 (Foster Drain) to Node at station 6016 (Jock
River)
2075 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 520
2076 *#
2077 ROUTE CHANNEL NHYDout=["520-out"], NHYDin=["520"],
2078 RDT=[1](min),
2079 CHLGTH=[860](m), CHSLOPE=[0.5872](%),
2080 FPSLOPE=[0.5872](%),
2081 SECNUM=[1.0], NSEG=[3]
2082 ( SEGROUGH, SEGDI ST (m))=
2083 [0.050, 45.90
2084 -0.035, 54.3
2085 0.050, 100.1097] NSEG times
2086 ( DI STANCE (m), ELEVATI ON (m))=
2087 [0, 91.26 ]
2088 [44.9, 91.46 ]
2089 [45.1, 91.37 ]
2090 [45.9, 90.84 ]
2091 [47, 90.32 ]
2092 [47.5, 90.22 ]
2093 [48, 90.17 ]
2094 [50.7, 90.19 ]
2095 [51.5, 90.17 ]
2096 [52.2, 90.13 ]
2097 [52.7, 90.12 ]
2098 [53.3, 90.14 ]
2099 [53.5, 90.31 ]
2100 [53.9, 90.59 ]
2101 [54.3, 90.87 ]
2102 [54.7, 91.04 ]
2103 [55.3, 91.24 ]
2104 [55.5, 91.26 ]
2105 [63.7, 91.37 ]
2106 [100.1097, 91.43 ]
2107 *%-----|-----|
2108 * -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2109 CONTINUOUS STANDHYD NHYD=["S-1-FO-F-D"], DT=[1]min, AREA=[14.96](ha),
2110 XI MP=[0.65], TI MP=[0.65], DWF=[0](cms), LOSS=[2],
2111 SCS curve number CN=[74],
2112 Pervious surfaces: I A per=[4.67](mm), SLPP=[0.5](%),
2113 LGP=[40](m), MNP=[0.25], SCP=[0](min),
2114 Imper vious surfaces: I A i mp=[1.57](mm), SLPI=[0.5](%),
2115 LGI=[315.806](m), MNI=[0.013], SCI=[0](min),

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2116 Continuous simulation parameters:
2117 IaRECper=[ 4](hr s), IaRECImp=[ 4](hr s),
2118 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2119 InterEventTime=[ 18](hr s), END=- 1
2120 *%-----|-----|
2121 *CONTINUOUS NASHYD NHYD=["S-1-FO-F-D"], DT=[ 1]mi n, AREA=[ 14.96](ha),
2122 * DWF=[ 0](cms), CNVC=[ 77], IA=[ 4.67](mm),
2123 * N=[ 3], TP=[ 1.007]hr s,
2124 * Continuous simulation parameters:
2125 * IaRECper=[ 4](hr s),
2126 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2127 * InterEventTime=[ 12](hr s)
2128 * Baseflow simulation parameters:
2129 * BaseFlowOption=[ 1],
2130 * InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2131 * VHydCond=[ 0.055](mm/hr), END=- 1
2132 *%-----|-----|
2133 COMPUTE DUALHYD NHYDin=["S-1-FO-F-D"], CI NLET=[ 1.615](cms), NI NLET=[ 1],
2134 Mj NHYD=["S-1FO-F-DJ"]
2135 MnNHYD=["S-1FO-F-DN"]
2136 TMJ STO=[ 9999999](cu-m)
2137 *%-----|-----|
2138 ADD HYD NHYDs um=["S-1FO-F-DS"], NHYDs to add=["S-1FO-F-DJ"+"S-1FO-F-DN"]
2139 *%-----|-----|
2140 ROUTE RESERVOIR NHYDout=["S-1FO-F-DR"], NHYDin=["S-1FO-F-DS"],
2141 RDT=[ 1](mi n),
2142 TABLE of ( OUTFLOW STORAGE ) values
2143 (cms) - (ha-m)
2144 [ 0.0 , 0.0 ]
2145 [ 0.1788, 0.5966 ]
2146 [ -1 , -1 ] (max twenty pts)
2147 NHYDovf=["S-1FoFDovf"]
2148 *%-----|-----|
2149 * -JFSA 2021-02-26 "S-1-D8" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2150 CONTINUOUS STANDHYD NHYD=["S-1-D8"], DT=[ 1]mi n, AREA=[ 5.27](ha), XI MP=[ 0.325],
TI MP=[ 0.65], DWF=[ 0](cms), LOSS=[ 1]:
2151 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
F=[ 0.00](mm),
2152 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
MNP=[ 0.250], SCP=[ 0](mi n),
2153 Impervious areas: IAi mp=[ 0.785](mm), SLPI=[ 0.75](%),
LGI=[ 187.439](m), MNI=[ 0.013], SCI=[ 0](mi n),
2154 Continuous simulation parameters:
2155 IaRECper=[ 4](hr s), IaRECImp=[ 4](hr s), InterEventTime=[ 12](hr s),
END=- 1
2156 *%-----|-----|
2157 *CONTINUOUS NASHYD NHYD=["S-1-D8"], DT=[ 1]mi n, AREA=[ 5.27](ha),
2158 * DWF=[ 0](cms), CNVC=[ 77], IA=[ 4.67](mm),
2159 * N=[ 3], TP=[ 1.10]hr s,
2160 * Continuous simulation parameters:
2161 * IaRECper=[ 4](hr s),
2162 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2163 * InterEventTime=[ 12](hr s)
2164 * Baseflow simulation parameters:
2165 * BaseFlowOption=[ 1],
2166 * InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2167 * VHydCond=[ 0.055](mm/hr), END=- 1
2168 *%-----|-----|
2169 COMPUTE DUALHYD NHYDin=["S-1-D8"], CI NLET=[ 0.672](cms), NI NLET=[ 1],
2170 Mj NHYD=["S-1-D8J"]
2171 MnNHYD=["S-1-D8N"]
2172 TMJ STO=[ 9999999](cu-m)
2173 *%-----|-----|
2174 ADD HYD NHYDs um=["S-1-D8S"], NHYDs to add=["S-1-D8J"+"S-1-D8N"]
2175 *%-----|-----|

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2176 *ADD HYD NHYDs um=[ "S-1-D" ], NHYDs to add=[ "S-1-Okeefe"+"S-1"+"S-1-Fost" ]
2177 *%-----|-----|
2178 *COMPUTE DUALHYD NHYDi n=[ "S-1-D" ], CI NLET=[ 11.616 ] (cms), NI NLET=[ 1 ],
2179 * Maj NHYD=[ "S-1-D-M" ]
2180 * MnnNHYD=[ "S-1-D-MN" ]
2181 * TMl STO=[ 5974 ] (cu-m)
2182 *%-----|-----|
2183 *ADD HYD NHYDs um=[ "S-1-DEV" ], NHYDs to add=[ "S-1-D-M"+"S-1-D-MN" ]
2184 *%-----|-----|
2185 ROUTE RESERVOIR NHYDout =["S-1-D8R" ] , NHYDi n=["S-1-D8S" ] ,
2186 RDT=[ 1 ] (mi n),
2187 TABLE of ( OUTFLOW STORAGE ) values
2188 ( cms ) - ( ha-m)
2189 [ 0.0 , 0.0 ]
2190 [ 0.0630, 0.2102 ]
2191 [ -1 , -1 ] (max twenty pts)
2192 NHYDovf=["S-1-D8Rovf" ]
2193 *%-----|-----|
2194 * -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2195 CONTINUOUS NASHYD NHYD=["S-1-A" ], DT=[ 1 ] mi n, AREA=[ 75.88 ] (ha),
2196 DWF=[ 0 ] (cms), CNv C=[ 77 ], I A=[ 4.67 ] (mm),
2197 N=[ 3 ], TP=[ 0.619 ] hr s,
2198 Continuous simulation parameters:
2199 I a RECper=[ 4 ] (hr s),
2200 SM N=[ -1 ] (mm), SMAX=[ -1 ] (mm), SK=[ 0.010 ] / (mm),
2201 InterEvent Ti me=[ 12 ] (hr s)
2202 Baseflow simulation parameters:
2203 BaseFl owOpt ion=[ 1 ] ,
2204 Ini t GWRes Vol = [ 50 ] (mm), GWRes K=[ 0.96 ] (mm3/day/mm)
2205 VHydCond=[ 0.055 ] (mm3/hr), END=- 1
2206 *%-----|-----|
2207 * -JFSA, 2021-01-22 "WCLAR_UNDE" (west of Clarke sub-catchment) discharges
directly to the jock river through a road side ditch on the west side of Borrisokane
road (station 6016)
2208 CONTINUOUS NASHYD NHYD=[ "WCLAR_UNDE" ], DT=[ 1 ] mi n, AREA=[ 35.65 ] (ha),
2209 DWF=[ 0 ] (cms), CNv C=[ 77 ], I A=[ 4.67 ] (mm),
2210 N=[ 3 ], TP=[ 1.10 ] hr s,
2211 Continuous simulation parameters:
2212 I a RECper=[ 4 ] (hr s),
2213 SM N=[ -1 ] (mm), SMAX=[ -1 ] (mm), SK=[ 0.010 ] / (mm),
2214 InterEvent Ti me=[ 12 ] (hr s)
2215 Baseflow simulation parameters:
2216 BaseFl owOpt ion=[ 1 ] ,
2217 Ini t GWRes Vol = [ 50 ] (mm), GWRes K=[ 0.96 ] (mm3/day/mm)
2218 VHydCond=[ 0.055 ] (mm3/hr), END=- 1
2219 *%-----|-----|
2220 ADD HYD NHYDs um=[ "SN_FO" ], NHYDs to
add=[ "N_FO"+"520-out"+"MS_P10"+"P10-OVF"+"WCLAR_UNDE"+"S-1FoFDovf"+"S-1FO-F-DR"+"S-1-D8R
ovf"+"S-1-D8R"+"S-1-A" ]
2221 *%-----|-----|
2222 SAVE HYD NHYD=[ "SN_FO" ], # OF PCYCLES=[ -1 ], I CASEs h=[ 1 ]
2223 HYD_COMMENT=[ "Total Flows at Foster Drain" ]
2224 *%-----|-----|
2225 *# Hydrograph from Node Foster routed to Node at Cedarview Road
2226 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6016
2227 *#
2228 ROUTE CHANNEL NHYDout =["NCE" ] , NHYDi n=["SN_FO" ] ,
2229 RDT=[ 1 ] (mi n),
2230 CHLGTH=[ 159 ] (m), CHSLOPE=[ 0.0818 ] ( % ),
2231 FPSLOPE=[ 0.0818 ] ( % ),
2232 SECNUM=[ 1.0 ], NSEG=[ 3 ]
2233 ( SEGROUGH, SEGDI ST (m) ) =
2234 [ 0.050, -15.46
2235 -0.035, 26.55
2236 0.050, 116.76 ] NSEG times

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2237 ( DI STANCE ( m), ELEVATI ON ( m)) =
2238 [- 645. 23, 91. 50]
2239 [- 391. 20, 91. 50]
2240 [- 91. 00, 91. 50]
2241 [- 85. 52, 91. 50]
2242 [- 15. 46, 89. 40]
2243 [- 9. 79, 89. 31]
2244 [- 3. 22, 86. 24]
2245 [3. 22, 85. 07]
2246 [10. 96, 85. 79]
2247 [16. 44, 86. 49]
2248 [26. 55, 89. 45]
2249 [29. 03, 90. 27]
2250 [35. 76, 90. 67]
2251 [36. 67, 91. 00]
2252 [108. 08, 91. 00]
2253 [109. 82, 90. 50]
2254 [112. 04, 90. 50]
2255 [114. 62, 91. 00]
2256 [116. 76, 91. 50]
2257 *%-----|-----|
2258 *#*****|
2259 *# Catchment S-1
2260 *# - To Jock River (north and south of Jock)
2261 *# - Primarily agricultural fields; portion of sand quarry
2262 *%-----|-----|
2263 *% -2020-12-17 "S-1-Undev" and "S-1-Fost" was a part of Foster drain, they are below
the foster pond. Now they are added to S-1 subcatchment based on Project 1474-BCDC,
JFSA, Nov. 2020
2264 *% -2020-12-17 Change O-14 (it was part of Okeefe drain) to "S-1-Okeefe" and add it
to S-1 subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
2265 *% -2020-12-17 Add "S-1-BCDC" as NASHYD
2266 *% -2020-12-17 all other S-1 subcatchment as STANDHYD with DUALHYD and ROUTE RESERVOIR
2267 *%-----|-----|
2268 *#*****|
2269 * -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2270 *CONTINUOUS NASHYD NHYD=["S-1-A"], DT=[1] min, AREA=[75.88](ha),
2271 * DWF=[0](cms), CNVC=[77], IA=[4.67](mm),
2272 * N=[3], TP=[0.619]hrs,
2273 * Continuous simulation parameters:
2274 * IaRECper=[4](hrs),
2275 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2276 * InterEventTime=[12](hrs)
2277 * Baseflow simulation parameters:
2278 * BaseFlowOption=[1],
2279 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2280 * VHydCond=[0.055](mm/hr), END=-1
2281 *%-----|-----|
2282 CONTINUOUS NASHYD NHYD=["S-1-B"], DT=[1] min, AREA=[55.36](ha),
2283 DWF=[0](cms), CNVC=[77], IA=[4.67](mm),
2284 N=[3], TP=[0.451]hrs,
2285 Continuous simulation parameters:
2286 IaRECper=[4](hrs),
2287 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2288 InterEventTime=[12](hrs)
2289 Baseflow simulation parameters:
2290 BaseFlowOption=[1],
2291 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2292 VHydCond=[0.055](mm/hr), END=-1
2293 *%-----|-----|
2294 *# - JFSA 2021-02-24 change the name from S-1-BCDC to S-1-A and S-1-B. Change their
TP values based on the new areas compared to the old ones.
2295 *CONTINUOUS NASHYD NHYD=["S-1-BCDC"], DT=[1] min, AREA=[134.9](ha),
2296 * DWF=[0](cms), CNVC=[77], IA=[4.67](mm),
2297 * N=[3], TP=[1.10]hrs,

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2298 * Continuous simulation parameters:
2299 * IaRECper=[ 4]( hrs),
2300 * SMN=[ - 1]( mm), SMAX=[ - 1]( mm), SK=[ 0. 010]/( mm),
2301 * InterEventTime=[ 12]( hrs)
2302 * Baseflow simulation parameters:
2303 * BaseFlowOption=[ 1],
2304 * InitGWResVol=[ 50]( mm), GWResK=[ 0. 96]( mm/ day/ mm)
2305 * VHydCond=[ 0. 055]( mm/ hr), END=- 1
2306 *%-----|-----
2307 *# - JFSA 2021-02-24 "S-1-BCDC-1" and "S-1-BCDC-2" are not existing anymore.
"S-1-BCDC-1" is part of "S-1-FO-D2" and "S-1-BCDC-2" is part of "S-1-D2" and "S-1-D3"
2308 *CONTINUOUS NASHYD NHYD=["S-1-BCDC-1"], DT=[ 1]mi n, AREA=[ 0. 3]( ha),
2309 * DWF=[ 0]( cms), CN C=[ 77], IA=[ 4. 67]( mm),
2310 * N=[ 3], TP=[ 1. 10]hr s,
2311 * Continuous simulation parameters:
2312 * IaRECper=[ 4]( hrs),
2313 * SMN=[ - 1]( mm), SMAX=[ - 1]( mm), SK=[ 0. 010]/( mm),
2314 * InterEventTime=[ 12]( hrs)
2315 * Baseflow simulation parameters:
2316 * BaseFlowOption=[ 1],
2317 * InitGWResVol=[ 50]( mm), GWResK=[ 0. 96]( mm/ day/ mm)
2318 * VHydCond=[ 0. 055]( mm/ hr), END=- 1
2319 *%-----|-----
2320 *CONTINUOUS NASHYD NHYD=["S-1-BCDC-2"], DT=[ 1]mi n, AREA=[ 1. 3]( ha),
2321 * DWF=[ 0]( cms), CN C=[ 77], IA=[ 4. 67]( mm),
2322 * N=[ 3], TP=[ 1. 10]hr s,
2323 * Continuous simulation parameters:
2324 * IaRECper=[ 4]( hrs),
2325 * SMN=[ - 1]( mm), SMAX=[ - 1]( mm), SK=[ 0. 010]/( mm),
2326 * InterEventTime=[ 12]( hrs)
2327 * Baseflow simulation parameters:
2328 * BaseFlowOption=[ 1],
2329 * InitGWResVol=[ 50]( mm), GWResK=[ 0. 96]( mm/ day/ mm)
2330 * VHydCond=[ 0. 055]( mm/ hr), END=- 1
2331 *%-----|-----
2332 *# - JFSA 2021-01-19, after adding Greenbank pond, "S-1-BCDC-3" is not existing
anymore
2333 *CONTINUOUS NASHYD NHYD=["S-1-BCDC-3"], DT=[ 1]mi n, AREA=[ 3. 9]( ha),
2334 * DWF=[ 0]( cms), CN C=[ 77], IA=[ 4. 67]( mm),
2335 * N=[ 3], TP=[ 1. 10]hr s,
2336 * Continuous simulation parameters:
2337 * IaRECper=[ 4]( hrs),
2338 * SMN=[ - 1]( mm), SMAX=[ - 1]( mm), SK=[ 0. 010]/( mm),
2339 * InterEventTime=[ 12]( hrs)
2340 * Baseflow simulation parameters:
2341 * BaseFlowOption=[ 1],
2342 * InitGWResVol=[ 50]( mm), GWResK=[ 0. 96]( mm/ day/ mm)
2343 * VHydCond=[ 0. 055]( mm/ hr), END=- 1
2344 *%-----|-----
2345 * -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
before station 7245 on Jock River
2346 *CONTINUOUS STANDHYD NHYD=["S-1-Okeefe"], DT=[ 1]( mi n), AREA=[ 44. 93]( ha), XI MP=[ 0. 65],
TI MP=[ 0. 65], DWF=[ 0]( cms),
2347 * LOSS=[ 2], SCS curve number CN=[ 75], Pervious surfaces:
I Aper=[ 4. 67]( mm), SLPP=[ 2. 0]( %),
2348 * LGP=[ 40]( m), MNP=[ 0. 25], SCP=[ 0]( mi n), Impervious surfaces:
I Ai mp=[ 1. 57]( mm), SLPI=[ 0. 75]( %),
2349 * LGI=[ 547. 296]( m), MNI=[ 0. 013], SCI=[ 0]( mi n),
2350 * Continuous simulation parameters:
2351 * IaRECper=[ 4]( hrs), IaRECI mp=[ 4]( hrs),
2352 * SMN=[ - 1]( mm), SMAX=[ - 1]( mm), SK=[ 0. 010]/( mm),
2353 * InterEventTime=[ 12]( hrs), END=- 1
2354 *%-----|-----
2355 *COMPUTE DUALHYD NHYDin=["S-1-Okeefe"], CI NLET=[ 4. 796]( cms), NI NLET=[ 1],
2356 * Mi j NHYD=["S-1-OkM"]
2357 * M nNHYD=["S-1-OkMN"]

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2358 *          TMI STO=[ 9999999 ] ( cu - m)
2359 *%-----|-----
2360 *ADD HYD          NHYDs um=[ " S- 1- OkS" ], NHYDs to add=[ " S- 1- OkM" +" S- 1- OkMN" ]
2361 *%-----|-----
2362 *ROUTE RESERVOIR NHYDout=[ " S- 1- OkSR" ] , NHYDin=[ " S- 1- OkS" ] ,
2363 *          RDT=[ 1 ] ( mi n),
2364 *          TABLE of ( OUTFLOW STORAGE ) values
2365 *                  ( cms ) - ( ha - m)
2366 *                  [ 0.0      , 0.0 ]
2367 *                  [ 0.5370, 1.7917 ]
2368 *                  [    -1   ,  -1   ] (max twenty pts)
2369 *          NHYDovf=[ " S- 1- OkSovf" ]
2370 *%-----|-----
2371 *CONTINUOUS NASHYD NHYD=[ " S- 1- Okeefe" ], DT=[ 1 ] mi n, AREA=[ 44.93 ] ( ha),
2372 *          DWF=[ 0 ] ( cms), CN C=[ 77 ], IA=[ 4.67 ] ( mm),
2373 *          N=[ 3 ], TP=[ 1.049 ] hrs,
2374 *          Continuous simulation parameters:
2375 *          IaRECper=[ 4 ] ( hrs),
2376 *          SMN=[ - 1 ] ( mm), SMAX=[ - 1 ] ( mm), SK=[ 0.010 ] / ( mm),
2377 *          InterEventTime=[ 12 ] ( hrs)
2378 *          Baseflow simulation parameters:
2379 *          BaseFlowOption=[ 1 ] ,
2380 *          InitGWResVol=[ 50 ] ( mm), GWResK=[ 0.96 ] ( mm/ day/ mm)
2381 *          VHydCond=[ 0.055 ] ( mm/ hr), END=- 1
2382 *%-----|-----
2383 * -JFSA 2021-02-26 "S-1-FO-DI" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2384 *CONTINUOUS STANDHYD NHYD=[ " S- 1- FO- DI" ], DT=[ 1 ] mi n, AREA=[ 5.11 ] ( ha),
2385 *          XI MP=[ 0.65 ], TI MP=[ 0.65 ], DWF=[ 0 ] ( cms), LOSS=[ 2 ],
2386 *          SCS curve number CN=[ 74 ],
2387 *          Pervious surfaces: IAper=[ 4.67 ] ( mm), SLPP=[ 0.5 ] ( %),
2388 *          LGP=[ 40 ] ( m), MNP=[ 0.25 ], SCP=[ 0 ] ( mi n),
2389 *          Impervious surfaces: IAimp=[ 1.57 ] ( mm), SLPI=[ 0.5 ] ( %),
2390 *          LGI=[ 184.572 ] ( m), MNI=[ 0.013 ], SCI=[ 0 ] ( mi n),
2391 *          Continuous simulation parameters:
2392 *          IaRECper=[ 4 ] ( hrs), IaRECImp=[ 4 ] ( hrs),
2393 *          SMN=[ - 1 ] ( mm), SMAX=[ - 1 ] ( mm), SK=[ 0.010 ] / ( mm),
2394 *          InterEventTime=[ 18 ] ( hrs), END=- 1
2395 *%-----|-----
2396 *COMPUTE DUALHYD NHYDin=[ " S- 1- FO- DI" ], CI NLET=[ 0.605 ] ( cms), NI NLET=[ 1 ],
2397 *          Mi j NHYD=[ " S- 1- FO- DIJ" ]
2398 *          M nNHYD=[ " S- 1- FO- DIN" ]
2399 *          TMI STO=[ 9999999 ] ( cu - m)
2400 *%-----|-----
2401 *ADD HYD          NHYDs um=[ " S- 1- FO- DIS" ], NHYDs to add=[ " S- 1- FO- DIN" +" S- 1- FO- DIJ" ]
2402 *%-----|-----
2403 *ROUTE RESERVOIR NHYDout=[ " S- 1- FO- DIR" ] , NHYDin=[ " S- 1- FO- DIS" ] ,
2404 *          RDT=[ 1 ] ( mi n),
2405 *          TABLE of ( OUTFLOW STORAGE ) values
2406 *                  ( cms ) - ( ha - m)
2407 *                  [ 0.0      , 0.0 ]
2408 *                  [ 0.0611, 0.2038 ]
2409 *                  [    -1   ,  -1   ] (max twenty pts)
2410 *          NHYDovf=[ " S- 1FODIovf" ]
2411 *%-----|-----
2412 *CONTINUOUS NASHYD NHYD=[ " S- 1- FO- DI" ], DT=[ 1 ] mi n, AREA=[ 5.11 ] ( ha),
2413 *          DWF=[ 0 ] ( cms), CN C=[ 77 ], IA=[ 4.67 ] ( mm),
2414 *          N=[ 3 ], TP=[ 1.10 ] hrs,
2415 *          Continuous simulation parameters:
2416 *          IaRECper=[ 4 ] ( hrs),
2417 *          SMN=[ - 1 ] ( mm), SMAX=[ - 1 ] ( mm), SK=[ 0.010 ] / ( mm),
2418 *          InterEventTime=[ 12 ] ( hrs)
2419 *          Baseflow simulation parameters:
2420 *          BaseFlowOption=[ 1 ] ,
2421 *          InitGWResVol=[ 50 ] ( mm), GWResK=[ 0.96 ] ( mm/ day/ mm)
2422 *          VHydCond=[ 0.055 ] ( mm/ hr), END=- 1

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2423 *%-----|-----|
2424 *   -JFSA 2021-02-26 "S-1-FO-D2" is a part of S-1 sub-catchment. It is moved to drain
before station 980 on Foster Drain
2425 *CONTINUOUS STANDHYD NHYD=["S-1-FO-D2"], DT=[1] min, AREA=[4.94](ha),
2426 *   XI MP=[0.55], TI MP=[0.55], DWF=[0](cms), LOSS=[2],
2427 *   SCS curve number CN=[74],
2428 *   Pervious surfaces: I A per=[4.67](mm), SLPP=[0.5](%),
2429 *   LGP=[40](m), MNP=[0.25], SCP=[0](min),
2430 *   Impervious surfaces: I A i mp=[1.57](mm), SLPI=[0.5](%),
2431 *   LGI=[181.475](m), MNI=[0.013], SCI=[0](min),
2432 *   Continuous simulation parameters:
2433 *   I a REC per=[4](hrs), I a REC i mp=[4](hrs),
2434 *   S M N=[-1](mm), S M A X=[-1](mm), S K=[0.010]/(mm),
2435 *   I n t e r E v e n t T i m e=[18](hrs),   E N D=- 1
2436 *%-----|-----|
2437 *CONTINUOUS NASHYD NHYD=["S-1-FO-D2"], DT=[1] min, AREA=[4.94](ha),
2438 *   DWF=[0](cms), CN C=[77], I A=[4.67](mm),
2439 *   N=[3], TP=[1.10] hrs,
2440 *   Continuous simulation parameters:
2441 *   I a REC per=[4](hrs),
2442 *   S M N=[-1](mm), S M A X=[-1](mm), S K=[0.010]/(mm),
2443 *   I n t e r E v e n t T i m e=[12](hrs)
2444 *   Baseflow simulation parameters:
2445 *   B a s e F l o w O p t i o n=[1] ,
2446 *   I n i t G W R e s V o l=[50](mm), G W R e s K=[0.96](mm/day/mm)
2447 *   V H y d C o n d=[0.055](mm/hr),   E N D=- 1
2448 *%-----|-----|
2449 *COMPUTE DUALHYD NHYD i n=["S-1-FO-D2"], C I N L E T=[0.508](cms), N I N L E T=[1],
2450 *   M i j N H Y D=["S-1-FO-D2J"]
2451 *   M n N H Y D=["S-1-FO-D2N"]
2452 *   T M I S T O=[9999999](cu-m)
2453 *%-----|-----|
2454 *ADD HYD NHYD s u m=["S-1-FO-D2S"], NHYD s t o a d d=["S-1-FO-D2J"+"S-1-FO-D2N"]
2455 *%-----|-----|
2456 *ROUTE RESERVOIR NHYD o u t=["S-1-FO-D2R"], NHYD i n=["S-1-FO-D2S"],
2457 *   R D T=[1](min),
2458 *   TABLE of ( O U T F L O W S T O R A G E ) values
2459 *   (cms) - (ha-m)
2460 *   [ 0.0 , 0.0 ]
2461 *   [ 0.0590, 0.1970 ]
2462 *   [ -1 , -1 ] (max twenty pts)
2463 *   N H Y D o v f=["S-1FOD2ovf"]
2464 *%-----|-----|
2465 *   -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2466 *CONTINUOUS STANDHYD NHYD=["S-1-FO-F-D"], DT=[1] min, AREA=[14.96](ha),
2467 *   XI MP=[0.65], TI MP=[0.65], DWF=[0](cms), LOSS=[2],
2468 *   SCS curve number CN=[74],
2469 *   Pervious surfaces: I A per=[4.67](mm), SLPP=[0.5](%),
2470 *   LGP=[40](m), MNP=[0.25], SCP=[0](min),
2471 *   Impervious surfaces: I A i mp=[1.57](mm), SLPI=[0.5](%),
2472 *   LGI=[315.806](m), MNI=[0.013], SCI=[0](min),
2473 *   Continuous simulation parameters:
2474 *   I a REC per=[4](hrs), I a REC i mp=[4](hrs),
2475 *   S M N=[-1](mm), S M A X=[-1](mm), S K=[0.010]/(mm),
2476 *   I n t e r E v e n t T i m e=[18](hrs),   E N D=- 1
2477 *%-----|-----|
2478 *CONTINUOUS NASHYD NHYD=["S-1-FO-F-D"], DT=[1] min, AREA=[14.96](ha),
2479 *   DWF=[0](cms), CN C=[77], I A=[4.67](mm),
2480 *   N=[3], TP=[1.007] hrs,
2481 *   Continuous simulation parameters:
2482 *   I a REC per=[4](hrs),
2483 *   S M N=[-1](mm), S M A X=[-1](mm), S K=[0.010]/(mm),
2484 *   I n t e r E v e n t T i m e=[12](hrs)
2485 *   Baseflow simulation parameters:
2486 *   B a s e F l o w O p t i o n=[1] ,

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2487 *          I n i t G W R e s V o l =[ 50 ] ( m m ) ,   G W R e s K =[ 0. 96 ] ( m m / d a y / m m )
2488 *          V H y d C o n d =[ 0. 055 ] ( m m / h r ) ,   E N D = - 1
2489 *%-----|-----|
2490 * COMPUTE DUALHYD  N H Y D i n =[ " S - 1 - F O - F - D " ] ,   C I N L E T =[ 1. 749 ] ( c m s ) ,   N I N L E T =[ 1 ] ,
2491 *          M a j N H Y D =[ " S - 1 F O - F - D J " ]
2492 *          M n N H Y D =[ " S - 1 F O - F - D N " ]
2493 *          T M I S T O =[ 9999999 ] ( c u - m )
2494 *%-----|-----|
2495 * ADD HYD          N H Y D s u m =[ " S - 1 F O - F - D S " ] ,   N H Y D s t o a d d =[ " S - 1 F O - F - D J " + " S - 1 F O - F - D N " ]
2496 *%-----|-----|
2497 * ROUTE RESERVOIR N H Y D o u t =[ " S - 1 F O - F - D R " ] ,   N H Y D i n =[ " S - 1 F O - F - D S " ] ,
2498 *          R D T =[ 1 ] ( m i n ) ,
2499 *          T A B L E o f ( O U T F L O W S T O R A G E ) v a l u e s
2500 *                  ( c m s ) - ( h a - m )
2501 *                  [ 0. 0      , 0. 0 ]
2502 *                  [ 0. 1788 , 0. 5966 ]
2503 *                  [ - 1      , - 1      ] ( m a x t w e n t y p t s )
2504 *          N H Y D o v f =[ " S - 1 F o F D o v f " ]
2505 *%-----|-----|
2506 CONTINUOUS STANDHYD N H Y D =[ " S - 1 - D I " ] ,   D T =[ 1 ] ( m i n ) ,   A R E A =[ 21. 67 ] ( h a ) ,   X I M P =[ 0. 65 ] ,
T I M P =[ 0. 65 ] ,   D W F =[ 0 ] ( c m s ) ,
2507 LOSS =[ 2 ] ,   S C S c u r v e n u m b e r C N =[ 75 ] ,   P e r v i o u s s u r f a c e s :
I A p e r =[ 4. 67 ] ( m m ) ,   S L P P =[ 2. 0 ] ( % ) ,
2508 LGP =[ 40 ] ( m ) ,   M N P =[ 0. 25 ] ,   S C P =[ 0 ] ( m i n ) ,   I m p e r v i o u s s u r f a c e s :
I A i m p =[ 1. 57 ] ( m m ) ,   S L P I =[ 0. 75 ] ( % ) ,
2509 L G I =[ 380. 088 ] ( m ) ,   M N I =[ 0. 013 ] ,   S C I =[ 0 ] ( m i n ) ,
2510 C o n t i n u o u s s i m u l a t i o n p a r a m e t e r s :
I a R E C p e r =[ 4 ] ( h r s ) ,   I a R E C i m p =[ 4 ] ( h r s ) ,
2511 S M N =[ - 1 ] ( m m ) ,   S M A X =[ - 1 ] ( m m ) ,   S K =[ 0. 010 ] / ( m m ) ,
2512 I n t e r E v e n t T i m e =[ 12 ] ( h r s ) ,   E N D = - 1
2513
2514 *%-----|-----|
2515 * CONTINUOUS NASHYD  N H Y D =[ " S - 1 - D I " ] ,   D T =[ 1 ] m i n ,   A R E A =[ 21. 67 ] ( h a ) ,
2516 *          D W F =[ 0 ] ( c m s ) ,   C N C =[ 77 ] ,   I A =[ 4. 67 ] ( m m ) ,
2517 *          N =[ 3 ] ,   T P =[ 1. 066 ] h r s ,
2518 *          C o n t i n u o u s s i m u l a t i o n p a r a m e t e r s :
2519 *          I a R E C p e r =[ 4 ] ( h r s ) ,
2520 *          S M N =[ - 1 ] ( m m ) ,   S M A X =[ - 1 ] ( m m ) ,   S K =[ 0. 010 ] / ( m m ) ,
2521 *          I n t e r E v e n t T i m e =[ 12 ] ( h r s )
2522 *          B a s e f l o w s i m u l a t i o n p a r a m e t e r s :
2523 *          B a s e F l o w O p t i o n =[ 1 ] ,
2524 *          I n i t G W R e s V o l =[ 50 ] ( m m ) ,   G W R e s K =[ 0. 96 ] ( m m / d a y / m m )
2525 *          V H y d C o n d =[ 0. 055 ] ( m m / h r ) ,   E N D = - 1
2526 *%-----|-----|
2527 COMPUTE DUALHYD  N H Y D i n =[ " S - 1 - D I " ] ,   C I N L E T =[ 2. 409 ] ( c m s ) ,   N I N L E T =[ 1 ] ,
2528 *          M a j N H Y D =[ " S - 1 - D I J " ]
2529 *          M n N H Y D =[ " S - 1 - D I N " ]
2530 *          T M I S T O =[ 9999999 ] ( c u - m )
2531 *%-----|-----|
2532 ADD HYD          N H Y D s u m =[ " S - 1 - D I S " ] ,   N H Y D s t o a d d =[ " S - 1 - D I J " + " S - 1 - D I N " ]
2533 *%-----|-----|
2534 ROUTE RESERVOIR N H Y D o u t =[ " S - 1 - D I R " ] ,   N H Y D i n =[ " S - 1 - D I S " ] ,
2535 *          R D T =[ 1 ] ( m i n ) ,
2536 *          T A B L E o f ( O U T F L O W S T O R A G E ) v a l u e s
2537 *                  ( c m s ) - ( h a - m )
2538 *                  [ 0. 0      , 0. 0 ]
2539 *                  [ 0. 2590 , 0. 8642 ]
2540 *                  [ - 1      , - 1      ] ( m a x t w e n t y p t s )
2541 *          N H Y D o v f =[ " S - 1 - D I R o v f " ]
2542 *%-----|-----|
2543 * - J F S A 2021-02-25 " S - 1 - D 2 " a n d " S - 1 - D 3 " a r e p a r t o f S - 1 s u b - c a t c h m e n t . T h e y a r e
m o v e d t o d r a i n b e f o r e s t a t i o n 6215 o n J o c k R i v e r
2544 * CONTINUOUS STANDHYD N H Y D =[ " S - 1 - D 2 " ] ,   D T =[ 1 ] ( m i n ) ,   A R E A =[ 18. 67 ] ( h a ) ,   X I M P =[ 0. 65 ] ,
T I M P =[ 0. 65 ] ,   D W F =[ 0 ] ( c m s ) ,
2545 *          L O S S =[ 2 ] ,   S C S c u r v e n u m b e r C N =[ 75 ] ,   P e r v i o u s s u r f a c e s :
I A p e r =[ 4. 67 ] ( m m ) ,   S L P P =[ 2. 0 ] ( % ) ,
2546 *          L G P =[ 40 ] ( m ) ,   M N P =[ 0. 25 ] ,   S C P =[ 0 ] ( m i n ) ,   I m p e r v i o u s s u r f a c e s :

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2547 * I Ai mp=[ 1. 57] ( mm) , SLPI =[ 0. 75] ( %),
2548 * LGI =[ 352. 798] ( m) , MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
2549 * Continuous simulation parameters:
2550 * IaRECper =[ 4] ( hr s) , IaRECI mp =[ 4] ( hr s) ,
2551 * SM N=[ - 1] ( mm) , SMAX=[ - 1] ( mm) , SK=[ 0. 010] / ( mm) ,
2552 * InterEvent Time =[ 12] ( hr s) , END=- 1
2553 *%-----|-----
2553 *CONTINUOUS NASHYD NHYD=[ " S- 1- D2" ] , DT=[ 1] mi n , AREA=[ 18. 67] ( ha) ,
2554 * DWF=[ 0] ( cms) , CN C=[ 77] , IA=[ 4. 67] ( mm) ,
2555 * N=[ 3] , TP=[ 1. 120] hr s ,
2556 * Continuous simulation parameters:
2557 * IaRECper =[ 4] ( hr s) ,
2558 * SM N=[ - 1] ( mm) , SMAX=[ - 1] ( mm) , SK=[ 0. 010] / ( mm) ,
2559 * InterEvent Time =[ 12] ( hr s)
2560 * Baseflow simulation parameters:
2561 * BaseFlowOpt ion=[ 1] ,
2562 * In it GWRes Vol =[ 50] ( mm) , GWRes K=[ 0. 96] ( mm/ day/ mm)
2563 * VHydCond=[ 0. 055] ( mm/ hr) , END=- 1
2564 *%-----|-----
2565 *COMPUTE DUALHYD NHYDi n=[ " S- 1- D2" ] , CI NLET=[ 2. 062] ( cms) , NI NLET=[ 1] ,
2566 * M aj NHYD=[ " S- 1- D2J" ]
2567 * M nNHYD=[ " S- 1- D2N" ]
2568 * TM I STO=[ 9999999] ( cu- m)
2569 *%-----|-----
2570 *ADD HYD NHYDs um=[ " S- 1- D2S" ] , NHYDs to add=[ " S- 1- D2J" +" S- 1- D2N" ]
2571 *%-----|-----
2572 *ROUTE RESERVOIR NHYDout =[ " S- 1- D2R" ] , NHYDi n=[ " S- 1- D2S" ] ,
2573 * RDT=[ 1] ( mi n) ,
2574 * TABLE of ( OUTFLOW STORAGE ) values
2575 * ( cms) - ( ha- m)
2576 * [ 0. 0 , 0. 0 ]
2577 * [ 0. 2231, 0. 7445 ]
2578 * [ - 1 , - 1 ] (max twenty pts)
2579 * NHYDovf=[ " S- 1- D2Rovf" ]
2580 *%-----|-----
2581 *CONTINUOUS STANDHYD NHYD=[ " S- 1- D3" ] , DT=[ 1] ( mi n) , AREA=[ 6. 79] ( ha) , XI MP=[ 0. 65] ,
2582 * TI MP=[ 0. 65] , DWF=[ 0] ( cms) ,
2583 * LOSS=[ 2] , SCS curve number CN=[ 75] , Pervious surfaces:
I Aper =[ 4. 67] ( mm) , SLPP=[ 2. 0] ( %),
2584 * LGP=[ 40] ( m) , MNP=[ 0. 25] , SCP=[ 0] ( mi n) , Impervious surfaces:
I Ai mp=[ 1. 57] ( mm) , SLPI =[ 0. 75] ( %),
2585 * LGI =[ 212. 760] ( m) , MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
2586 * Continuous simulation parameters:
2587 * IaRECper =[ 4] ( hr s) , IaRECI mp =[ 4] ( hr s) ,
2588 * SM N=[ - 1] ( mm) , SMAX=[ - 1] ( mm) , SK=[ 0. 010] / ( mm) ,
2589 * InterEvent Time =[ 12] ( hr s) , END=- 1
2590 *%-----|-----
2590 *CONTINUOUS NASHYD NHYD=[ " S- 1- D3" ] , DT=[ 1] mi n , AREA=[ 6. 79] ( ha) ,
2591 * DWF=[ 0] ( cms) , CN C=[ 77] , IA=[ 4. 67] ( mm) ,
2592 * N=[ 3] , TP=[ 1. 281] hr s ,
2593 * Continuous simulation parameters:
2594 * IaRECper =[ 4] ( hr s) ,
2595 * SM N=[ - 1] ( mm) , SMAX=[ - 1] ( mm) , SK=[ 0. 010] / ( mm) ,
2596 * InterEvent Time =[ 12] ( hr s)
2597 * Baseflow simulation parameters:
2598 * BaseFlowOpt ion=[ 1] ,
2599 * In it GWRes Vol =[ 50] ( mm) , GWRes K=[ 0. 96] ( mm/ day/ mm)
2600 * VHydCond=[ 0. 055] ( mm/ hr) , END=- 1
2601 *%-----|-----
2602 *COMPUTE DUALHYD NHYDi n=[ " S- 1- D3" ] , CI NLET=[ 0. 719] ( cms) , NI NLET=[ 1] ,
2603 * M aj NHYD=[ " S- 1- D3J" ]
2604 * M nNHYD=[ " S- 1- D3N" ]
2605 * TM I STO=[ 9999999] ( cu- m)
2606 *%-----|-----
2607 *ADD HYD NHYDs um=[ " S- 1- D3S" ] , NHYDs to add=[ " S- 1- D3J" +" S- 1- D3N" ]
2608 *%-----|-----

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2609 *ROUTE RESERVOIR      NHYDout=["S-1-D3R"] ,NHYDin=["S-1-D3S"] ,
2610 *                      RDT=[1](min),
2611 *                      TABLE of ( OUTFLOW STORAGE ) values
2612 *                      (cms) - (ha-m)
2613 *                      [ 0.0      , 0.0 ]
2614 *                      [ 0.0811, 0.2708 ]
2615 *                      [ -1      , -1      ] (max twenty pts)
2616 *                      NHYDovf=["S-1-D3Rovf"]
2617 *%-----|-----
2618 CONTINUOUS STANDHYD NHYD=["S-1-D4"], DT=[1](min), AREA=[3.28](ha), XI MP=[0.65],
TI MP=[0.65], DWF=[0](cms),
2619 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
I Aper=[4.67](mm), SLPP=[2.0](%),
2620 LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
I Ai mp=[1.57](mm), SLPI=[0.75](%),
2621 LGI=[147.874](m), MNI=[0.013], SCI=[0](min),
2622 Continuous simulation parameters:
2623 I aRE Cper=[4](hrs), I aRE Ci mp=[4](hrs),
2624 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2625 Inter Event Ti me=[12](hrs), END=-1
2626 *%-----|-----
2627 *CONTINUOUS NASHYD    NHYD=["S-1-D4"], DT=[1]min, AREA=[3.28](ha),
2628 *                      DWF=[0](cms), CN C=[77], I A=[4.67](mm),
2629 *                      N=[3], TP=[1.10]hrs,
2630 *                      Continuous simulation parameters:
2631 *                      I aRE Cper=[4](hrs),
2632 *                      SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2633 *                      Inter Event Ti me=[12](hrs)
2634 *                      Baseflow simulation parameters:
2635 *                      BaseFl owOpt ion=[1] ,
2636 *                      Ini tGW Res Vol =[50](mm), GW Res K=[0.96](mm/day/mm)
2637 *                      VHyd Cond=[0.055](mm/hr), END=-1
2638 *%-----|-----
2639 COMPUTE DUALHYD      NHYDin=["S-1-D4"], CI NLET=[0.421](cms), NI NLET=[1],
2640 *                      M aj NHYD=["S-1-D4J"]
2641 *                      M nNHYD=["S-1-D4N"]
2642 *                      TM I STO=[9999999](cu-m)
2643 *%-----|-----
2644 ADD HYD              NHYDs um=["S-1-D4S"], NHYDs to add=["S-1-D4J"+"S-1-D4N"]
2645 *%-----|-----
2646 ROUTE RESERVOIR    NHYDout=["S-1-D4R"] ,NHYDin=["S-1-D4S"] ,
2647 *                      RDT=[1](min),
2648 *                      TABLE of ( OUTFLOW STORAGE ) values
2649 *                      (cms) - (ha-m)
2650 *                      [ 0.0      , 0.0 ]
2651 *                      [ 0.0392, 0.1308 ]
2652 *                      [ -1      , -1      ] (max twenty pts)
2653 *                      NHYDovf=["S-1-D4Rovf"]
2654 *%-----|-----
2655 CONTINUOUS STANDHYD NHYD=["S-1-D5"], DT=[1](min), AREA=[12.84](ha), XI MP=[0.65],
TI MP=[0.65], DWF=[0](cms),
2656 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
I Aper=[4.67](mm), SLPP=[2.0](%),
2657 LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
I Ai mp=[1.57](mm), SLPI=[0.75](%),
2658 LGI=[292.57](m), MNI=[0.013], SCI=[0](min),
2659 Continuous simulation parameters:
2660 I aRE Cper=[4](hrs), I aRE Ci mp=[4](hrs),
2661 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2662 Inter Event Ti me=[12](hrs), END=-1
2663 *%-----|-----
2664 *CONTINUOUS NASHYD    NHYD=["S-1-D5"], DT=[1]min, AREA=[12.84](ha),
2665 *                      DWF=[0](cms), CN C=[77], I A=[4.67](mm),
2666 *                      N=[3], TP=[1.10]hrs,
2667 *                      Continuous simulation parameters:
2668 *                      I aRE Cper=[4](hrs),

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2669 * SMN=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
2670 * InterEventTime=[ 12 ] ( hr s )
2671 * Baseflow simulation parameters:
2672 * BaseFlowOption=[ 1 ] ,
2673 * InitGWResVol=[ 50 ] ( mm ) , GWResK=[ 0. 96 ] ( mm / day / mm )
2674 * VHydCond=[ 0. 055 ] ( mm / hr ) , END=- 1
2675 *%-----|
2676 COMPUTE DUALHYD NHYDin=[ " S- 1- D5 " ] , CI NLET=[ 1. 5 ] ( cms ) , NI NLET=[ 1 ] ,
2677 Mj NHYD=[ " S- 1- D5J " ]
2678 MnNHYD=[ " S- 1- D5N " ]
2679 TMSTO=[ 9999999 ] ( cu- m )
2680 *%-----|
2681 ADD HYD NHYDsum=[ " S- 1- D5S " ] , NHYDsto add=[ " S- 1- D5J " + " S- 1- D5N " ]
2682 *%-----|
2683 ROUTE RESERVOIR NHYDout=[ " S- 1- D5R " ] , NHYDin=[ " S- 1- D5S " ] ,
2684 RDT=[ 1 ] ( mi n ) ,
2685 TABLE of ( OUTFLOW STORAGE ) values
2686 ( cms ) - ( ha- m )
2687 [ 0. 0 , 0. 0 ]
2688 [ 0. 1535 , 0. 5120 ]
2689 [ - 1 , - 1 ] ( max twenty pts )
2690 NHYDovf=[ " S- 1- D5Rovf " ]
2691 *%-----|
2692 CONTINUOUS STANDHYD NHYD=[ " S- 1- D6 " ] , DT=[ 1 ] ( mi n ) , AREA=[ 1. 75 ] ( ha ) , XI MP=[ 0. 65 ] ,
TI MP=[ 0. 65 ] , DWF=[ 0 ] ( cms ) ,
2693 LOSS=[ 2 ] , SCS curve number CN=[ 75 ] , Pervious surfaces:
I Aper=[ 4. 67 ] ( mm ) , SLPP=[ 2. 0 ] ( % ) ,
2694 LGP=[ 40 ] ( m ) , MNP=[ 0. 25 ] , SCP=[ 0 ] ( mi n ) , Impervious surfaces:
IAi mp=[ 1. 57 ] ( mm ) , SLPI=[ 0. 75 ] ( % ) ,
2695 LGI=[ 108. 01 ] ( m ) , MNI=[ 0. 013 ] , SCI=[ 0 ] ( mi n ) ,
2696 Continuous simulation parameters:
IaRECper=[ 4 ] ( hr s ) , IaRECI mp=[ 4 ] ( hr s ) ,
2697 SMN=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
2698 InterEventTime=[ 12 ] ( hr s ) , END=- 1
2699 *%-----|
2700 *CONTINUOUS NASHYD NHYD=[ " S- 1- D6 " ] , DT=[ 1 ] mi n , AREA=[ 1. 75 ] ( ha ) ,
2701 DWF=[ 0 ] ( cms ) , CN C=[ 77 ] , IA=[ 4. 67 ] ( mm ) ,
2702 N=[ 3 ] , TP=[ 1. 10 ] hr s ,
2703 Continuous simulation parameters:
2704 IaRECper=[ 4 ] ( hr s ) ,
2705 SMN=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
2706 InterEventTime=[ 12 ] ( hr s )
2707 Baseflow simulation parameters:
2708 BaseFlowOption=[ 1 ] ,
2709 InitGWResVol=[ 50 ] ( mm ) , GWResK=[ 0. 96 ] ( mm / day / mm )
2710 VHydCond=[ 0. 055 ] ( mm / hr ) , END=- 1
2711 *%-----|
2712 COMPUTE DUALHYD NHYDin=[ " S- 1- D6 " ] , CI NLET=[ 0. 232 ] ( cms ) , NI NLET=[ 1 ] ,
2713 Mj NHYD=[ " S- 1- D6J " ]
2714 MnNHYD=[ " S- 1- D6N " ]
2715 TMSTO=[ 9999999 ] ( cu- m )
2716 *%-----|
2717 ADD HYD NHYDsum=[ " S- 1- D6S " ] , NHYDsto add=[ " S- 1- D6J " + " S- 1- D6N " ]
2718 *%-----|
2719 ROUTE RESERVOIR NHYDout=[ " S- 1- D6R " ] , NHYDin=[ " S- 1- D6S " ] ,
2720 RDT=[ 1 ] ( mi n ) ,
2721 TABLE of ( OUTFLOW STORAGE ) values
2722 ( cms ) - ( ha- m )
2723 [ 0. 0 , 0. 0 ]
2724 [ 0. 0209 , 0. 0698 ]
2725 [ - 1 , - 1 ] ( max twenty pts )
2726 NHYDovf=[ " S- 1- D6Rovf " ]
2727 *%-----|
2728 CONTINUOUS STANDHYD NHYD=[ " S- 1- D7 " ] , DT=[ 1 ] ( mi n ) , AREA=[ 2. 03 ] ( ha ) , XI MP=[ 0. 65 ] ,
2729 TI MP=[ 0. 65 ] , DWF=[ 0 ] ( cms ) ,
2730 LOSS=[ 2 ] , SCS curve number CN=[ 75 ] , Pervious surfaces:

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2731 I Ape r=[ 4. 67] ( mm) , SLPP=[ 2. 0] ( % ) ,
LGP=[ 40] ( m) , MNP=[ 0. 25] , SCP=[ 0] ( mi n) , I mperv ious surfaces :
2732 I A i mp=[ 1. 57] ( mm) , SLPI=[ 0. 75] ( % ) ,
2733 LGI=[ 116. 33] ( m) , MNI=[ 0. 013] , SCI=[ 0] ( mi n) ,
2734 C ont i nuous si mul at i on pa ram et ers :
I aRECper=[ 4] ( hr s) , I aRECI mp=[ 4] ( hr s) ,
2735 SM N=[ - 1] ( mm) , SMAX=[ - 1] ( mm) , SK=[ 0. 010] / ( mm) ,
2736 I nt er E vent Ti me=[ 12] ( hr s) , EN D=- 1
2737 *%-----|-----|
2738 *CONTI NUOUS NASHYD NHYD=[ " S- 1- D7" ] , DT=[ 1] mi n , AREA=[ 2. 03] ( ha) ,
2739 * DWF=[ 0] ( cms) , CN C=[ 77] , I A=[ 4. 67] ( mm) ,
2740 * N=[ 3] , TP=[ 1. 10] hr s ,
2741 * C ont i nuous si mul at i on pa ram et ers :
2742 * I aRECper=[ 4] ( hr s) ,
2743 * SM N=[ - 1] ( mm) , SMAX=[ - 1] ( mm) , SK=[ 0. 010] / ( mm) ,
2744 * I nt er E vent Ti me=[ 12] ( hr s)
2745 * B asefl ow si mul at i on pa ram et ers :
2746 * B aseFl owOpt i on=[ 1] ,
2747 * I nt i t GWRes Vol=[ 50] ( mm) , GWRes K=[ 0. 96] ( mm/ day/ mm)
2748 * VHydCond=[ 0. 055] ( mm/ hr) , EN D=- 1
2749 *%-----|-----|
2750 COMPUTE DUALHYD NHYD i n=[ " S- 1- D7" ] , CI NLET=[ 0. 265] ( cms) , NI NLET=[ 1] ,
2751 M a j NHYD=[ " S- 1- D7J" ]
2752 M nNHYD=[ " S- 1- D7N" ]
2753 TM STO=[ 9999999] ( cu- m)
2754 *%-----|-----|
2755 ADD HYD NHYDs um=[ " S- 1- D7S" ] , NHYDs t o add=[ " S- 1- D7J" + " S- 1- D7N" ]
2756 *%-----|-----|
2757 ROUTE RESERVOIR NHYDout=[ " S- 1- D7R" ] , NHYD i n=[ " S- 1- D7S" ] ,
2758 RDT=[ 1] ( mi n) ,
2759 TABLE of ( OUTFLOW STORAGE ) values
2760 ( cms) - ( ha- m)
2761 [ 0. 0 , 0. 0 ]
2762 [ 0. 0243, 0. 0810 ]
2763 [ - 1 , - 1 ] ( max twenty pts)
2764 NHYDovf=[ " S- 1- D7Rovf" ]
2765 *%-----|-----|
2766 * -JFSA 2021-02-26 " S- 1- D8" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2767 *CONTI NUOUS STANDHYD NHYD=[ " S- 1- D8" ] , DT=[ 1] ( mi n) , AREA=[ 5. 27] ( ha) , XI MP=[ 0. 65] ,
TI MP=[ 0. 65] , DWF=[ 0] ( cms) ,
2768 * LOSS=[ 2] , SCS curve number CN=[ 75] , Pervious surfaces:
I Ape r=[ 4. 67] ( mm) , SLPP=[ 2. 0] ( % ) ,
2769 * LGP=[ 40] ( m) , MNP=[ 0. 25] , SCP=[ 0] ( mi n) , I mperv ious surfaces:
I A i mp=[ 1. 57] ( mm) , SLPI=[ 0. 75] ( % ) ,
2770 * LGI=[ 187. 439] ( m) , MNI=[ 0. 013] , SCI=[ 0] ( mi n) ,
2771 * C ont i nuous si mul at i on pa ram et ers :
2772 * I aRECper=[ 4] ( hr s) , I aRECI mp=[ 4] ( hr s) ,
2773 * SM N=[ - 1] ( mm) , SMAX=[ - 1] ( mm) , SK=[ 0. 010] / ( mm) ,
2774 * I nt er E vent Ti me=[ 12] ( hr s) , EN D=- 1
2775 *%-----|-----|
2776 *CONTI NUOUS NASHYD NHYD=[ " S- 1- D8" ] , DT=[ 1] mi n , AREA=[ 5. 27] ( ha) ,
2777 * DWF=[ 0] ( cms) , CN C=[ 77] , I A=[ 4. 67] ( mm) ,
2778 * N=[ 3] , TP=[ 1. 10] hr s ,
2779 * C ont i nuous si mul at i on pa ram et ers :
2780 * I aRECper=[ 4] ( hr s) ,
2781 * SM N=[ - 1] ( mm) , SMAX=[ - 1] ( mm) , SK=[ 0. 010] / ( mm) ,
2782 * I nt er E vent Ti me=[ 12] ( hr s)
2783 * B asefl ow si mul at i on pa ram et ers :
2784 * B aseFl owOpt i on=[ 1] ,
2785 * I nt i t GWRes Vol=[ 50] ( mm) , GWRes K=[ 0. 96] ( mm/ day/ mm)
2786 * VHydCond=[ 0. 055] ( mm/ hr) , EN D=- 1
2787 *%-----|-----|
2788 *COMPUTE DUALHYD NHYD i n=[ " S- 1- D8" ] , CI NLET=[ 2. 279] ( cms) , NI NLET=[ 1] ,
2789 * M a j NHYD=[ " S- 1- D8J" ]
2790 * M nNHYD=[ " S- 1- D8N" ]

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2791 *          TMI STO=[ 9999999 ] ( cu- m)
2792 *%-----|-----|
2793 *ADD HYD          NHYDs um=[ " S- 1- D8S" ], NHYDs to add=[ " S- 1- D8J" +" S- 1- D8N" ]
2794 *%-----|-----|
2795 *ADD HYD          NHYDs um=[ " S- 1- D" ], NHYDs to add=[ " S- 1- Okeefe" +" S- 1" +" S- 1- Fost" ]
2796 *%-----|-----|
2797 *COMPUTE DUALHYD  NHYDi n=[ " S- 1- D" ], CI NLET=[ 11. 616 ] ( cms ), NI NLET=[ 1 ],
2798 *                Mj NHYD=[ " S- 1- D- M" ]
2799 *                MnNHYD=[ " S- 1- D- MN" ]
2800 *          TMI STO=[ 5974 ] ( cu- m)
2801 *%-----|-----|
2802 *ADD HYD          NHYDs um=[ " S- 1- DEV" ], NHYDs to add=[ " S- 1- D- M" +" S- 1- D- MN" ]
2803 *%-----|-----|
2804 *ROUTE RESERVOIR  NHYDout=[ " S- 1- D8R" ] , NHYDi n=[ " S- 1- D8S" ] ,
2805 *                RDT=[ 1 ] ( mi n),
2806 *                TABLE of ( OUTFLOW STORAGE ) values
2807 *                    ( cms ) - ( ha- m)
2808 *                    [ 0. 0      , 0. 0 ]
2809 *                    [ 0. 0630, 0. 2102 ]
2810 *                    [ - 1      , - 1      ] ( max twenty pts)
2811 *                NHYDovf=[ " S- 1- D8Rovf" ]
2812 *%-----|-----|
2813 *%-----|-----|
2814 *          - JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
(W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
2815 *#      Catchment W_CLAR
2816 *#      - To West Clarke Drain (south of the Jock)
2817 *#      - Subdivision with 43% imp. as per Barrhaven South MS
2818 *#      - 2020-11-30 update CLARKE Tributary Drainage Area to = 121 ha based on
P598(04)-11
2819 *#      - 2020-11-30 split CLARKE Drainage Area to MAJOR and ALL
2820 *#*****
2821 CONTINUOUS STANDHYD NHYD=[ " W_CLAR_M" ], DT=[ 1 ] mi n, AREA=[ 1. 772 ] ( ha ),
2822 XI MP=[ 0. 46 ], TI MP=[ 0. 59 ], DWF=[ 0 ] ( cms ), LOSS=[ 2 ],
2823 SCS curve number CN=[ 77 ],
2824 Pervious surfaces: I Aper=[ 4. 67 ] ( mm ), SLPP=[ 1 ] ( % ),
2825 LGP=[ 40 ] ( m ), MNP=[ 0. 25 ], SCP=[ 0 ] ( mi n ),
2826 Impervious surfaces: I Ai mp=[ 1. 57 ] ( mm ), SLPI=[ 1 ] ( % ),
2827 LGI=[ 109 ] ( m ), MNI=[ 0. 013 ], SCI=[ 0 ] ( mi n ),
2828 Continuous simulation parameters:
2829 Ia RECper=[ 4 ] ( hr s ), Ia RECI mp=[ 4 ] ( hr s ),
2830 SM N=[ - 1 ] ( mm ), SMAX=[ - 1 ] ( mm ), SK=[ 0. 010 ] / ( mm ),
2831 Inter Event Time=[ 18 ] ( hr s ), END=- 1
2832 *%-----|-----|
2833 *COMPUTE DUALHYD  NHYDi n=[ " W_CLAR_M" ], CI NLET=[ 0. 213 ] ( cms ), NI NLET=[ 1 ],
2834 *                Mj NHYD=[ " W_CLAR_Mj" ]
2835 *                MnNHYD=[ " W_CLAR_Mn" ]
2836 *                TMI STO=[ 0. 1 ] ( cu- m)
2837 *%-----|-----|
2838 *# 5- Year + 12% Capture
2839 ROUTE RESERVOIR  NHYDout=[ " W_CLAR_Mn" ] , NHYDi n=[ " W_CLAR_M" ] ,
2840 RDT=[ 1 ] ( mi n),
2841 TABLE of ( OUTFLOW STORAGE ) values
2842 ( cms ) - ( ha- m)
2843 [ 0. 0      , 0. 0 ]
2844 [ 0. 213 , 0. 0001 ]
2845 [ - 1      , - 1      ] ( max twenty pts)
2846 NHYDovf=[ " W_CLAR_Mj" ] ,
2847 *%-----|-----|
2848 *          - Clarke_All area from P 598(04)-11 = 120.207 ha, change to 127.298 ha based on
GIS measurements,
2849 *          - JFSA, 2021-01-19 update W_CLAR_ALL to (121.17-1.772=119.398) ha based on GIS
measurements W_CLAR is 121.17 ha and W_CLAR_M is 1.772 ha
2850 CONTINUOUS STANDHYD NHYD=[ " W_CLAR_ALL" ], DT=[ 1 ] mi n, AREA=[ 119. 398 ] ( ha ),
2851 XI MP=[ 0. 60 ], TI MP=[ 0. 65 ], DWF=[ 0 ] ( cms ), LOSS=[ 2 ],
2852 SCS curve number CN=[ 77 ],

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2853          Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
2854                    LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
2855          Impervious surfaces: I A imp=[ 1.57](mm), SLPI=[ 1](%),
2856                    LGI=[ 892.18](m), MNI=[ 0.013], SCI=[ 0](min),
2857          Continuous simulation parameters:
2858          I a REC per=[ 4](hrs), I a REC imp=[ 4](hrs),
2859          SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2860          Inter Event Time=[ 18](hrs), END=- 1
2861  *%-----|-----|
2862  ADD HYD          NHYDsum=[ "W_CLAR" ], NHYDs to add=[ "W_CLAR_ALL"+"W_CLAR_Mj" ]
2863  *%-----|-----|
2864  SAVE HYD        NHYD=[ "W_CLAR" ], # OF PCYCLES=[ -1 ], I CASEs h=[ 1 ]
2865                  HYD_COMMENT=[ "Total Flows to West Clarke" ]
2866  *#*****|
2867  *# West Clarke Pond 2
2868  *# - Rating curve obtained from Barrhaven South MBS modeling
2869  *# - Tributary Drainage Area to MBS Pond 2 = 241 ha
2870  *#*****|
2871  ROUTE RESERVOIR NHYDout=[ "MS_P2" ], NHYDin=[ "W_CLAR" ],
2872                  RDT=[ 1](min),
2873                  TABLE of ( OUTFLOW STORAGE ) values
2874                  (cms) - (ha-m)
2875                  [ 0.0 , 0.0 ]
2876                  [ 0.128 , 0.161 ]
2877                  [ 0.138 , 0.409 ]
2878                  [ 0.148 , 0.68 ]
2879                  [ 0.227 , 0.931 ]
2880                  [ 0.354 , 1.223 ]
2881                  [ 0.505 , 1.52 ]
2882                  [ 0.666 , 1.821 ]
2883                  [ 0.831 , 2.123 ]
2884                  [ 0.995 , 2.434 ]
2885                  [ 1.069 , 2.583 ]
2886                  [ 1.51 , 2.647 ]
2887                  [ 4.904 , 2.861 ]
2888                  [ 13.048 , 3.188 ]
2889                  [ 23.745 , 3.523 ]
2890                  [ 36.474 , 3.871 ]
2891                  [ 45.938 , 4.127 ]
2892                  [ 61.652 , 4.539 ]
2893                  [ -1 , -1 ] (max twenty pts)
2894                  NHYDovf=[ "P2-OVF" ]
2895  *%-----|-----|
2896  *#*****|
2897  * - JFSA, 2021-01-22 "W_CLAR_UNDE" (west of Clarke sub-catchment) discharges
directly to the Jock River through a road side ditch on the west side of Borrisokane
road (station 6016)
2898  *CONTINUOUS NASHYD NHYD=[ "W_CLAR_UNDE" ], DT=[ 1]min, AREA=[ 35.65](ha),
2899  * DWF=[ 0](cms), CNVC=[ 77], IA=[ 4.67](mm),
2900  * N=[ 3], TP=[ 1.10]hrs,
2901  * Continuous simulation parameters:
2902  * I a REC per=[ 4](hrs),
2903  * SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2904  * Inter Event Time=[ 12](hrs)
2905  * Baseflow simulation parameters:
2906  * BaseFlowOption=[ 1 ],
2907  * Init GWRes Vol=[ 50](mm), GWRes K=[ 0.96](mm/day/mm)
2908  * VHydCond=[ 0.055](mm/hr), END=- 1
2909  *%-----|-----|
2910  ADD HYD          NHYDsum=[ "SN_CE" ], NHYDs to
add=[ "N_CE"+"S-1-D4R"+"S-1-D5R"+"S-1-D4Rovf"+"S-1-D5Rovf"+"MS_P2"+"P2-OVF" ]
2911  *%-----|-----|
2912  SAVE HYD        NHYD=[ "SN_CE" ], # OF PCYCLES=[ -1 ], I CASEs h=[ 1 ]
2913                  HYD_COMMENT=[ "Total Flows before Station 5737 on Jock River" ]
2914  *%-----|-----|
2915  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5737

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2916  *# 2021-02-25 add station 5737 before station 5002. Station 5737 was extracted from the
      HEC-RAS model
      T:\PROJ\1474-16\Design\20201026-QuantityControlAnalysis\HEC-RAS\JockLi dar 2005
2917  *# JFSA 2021-03-02 change the slope to 0.0175% instead of 0.02593 to stabilize the model
2918  ROUTE CHANNEL      NHYDout=["5737"] , NHYDin=["SN_CE"] ,
2919                      RDT=[1](min),
2920                      CHLGTH=[270](m),   CHSLOPE=[0.0175](%),
2921                      FPSLOPE=[0.0175](%),
2922                      SECNUM=[1.0],      NSEG=[3]
2923                      ( SEGROUGH, SEGDIST (m))=
2924                      [0.050, -24.04
2925                      -0.035, 23.92
2926                      0.050, 1130.8] NSEG times
2927                      ( DISTANCE (m), ELEVATION (m))=
2928                      [-1060.52, 94 ]
2929                      [-268.6, 91.5 ]
2930                      [-259.43, 91.5 ]
2931                      [-179.48, 91.5 ]
2932                      [-67.9, 91.5 ]
2933                      [-59.21, 91.5 ]
2934                      [-33.19, 91 ]
2935                      [-26.08, 90.5 ]
2936                      [-24.04, 90 ]
2937                      [-13.14, 86.77 ]
2938                      [0, 85 ]
2939                      [14.68, 86.74 ]
2940                      [23.92, 90 ]
2941                      [25.78, 90.5 ]
2942                      [31.91, 91 ]
2943                      [91.95, 91.5 ]
2944                      [772.15, 92 ]
2945                      [961.49, 92.5 ]
2946                      [1044.69, 93 ]
2947                      [1130.8, 95 ]
2948  *%-----|-----|
2949  ADD HYD          NHYDsum=["5002"], NHYDsto
      add=["5737"+"S-1-D1R"+"S-1-D6R"+"S-1-D7R"+"S-1-D1Rovf"+"S-1-D6Rovf"+"S-1-D7Rovf"]
2950  *%-----|-----|
2951  SAVE HYD        NHYD=["5002"], # OF PCYCLES=[-1], ICASEsh=[1]
2952                  HYD_COMMENT=["Total Flows before Station 5002 on Jock River"]
2953  *%-----|-----|
2954  *# Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain
2955  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5002
2956  *# JFSA 2021-02-19 Change the slope from 0.01 % (as per Stantec Report 2007) to 0.0255
      % so the model will be more stable and give reasonable results. It is justifiable as
      ROUTE CHANNELs aren't well suited to really flat slopes.
2957  *# JFSA 2021-02-19 Change to three ROUTE CHANNEL with length 275 m each instead of one
      with 825 m length so the model will be more stable
2958  *# JFSA 2021-02-26 change the length of 5002 route channel from 825 m to 736 m That is
      because of adding station 5737 between station 6016 and station 5002. Then the length
      from station 5737 to station 5002 is 736 m Change the slope from 0.0255 % to 0.09511 %
2959  *
2960  ROUTE CHANNEL    NHYDout=["N_WCa"] , NHYDin=["5002"] ,
2961                  RDT=[1](min),
2962                  CHLGTH=[245.33333](m),   CHSLOPE=[0.09511](%),
2963                  FPSLOPE=[0.09511](%),
2964                  SECNUM=[1.0],      NSEG=[3]
2965                  ( SEGROUGH, SEGDIST (m))=
2966                  [0.050, -37.5
2967                  -0.035, 37.50
2968                  0.050, 157.05] NSEG times
2969                  ( DISTANCE (m), ELEVATION (m))=
2970                  [-601.81, 91.5]
2971                  [-37.50, 90.00]
2972                  [-19.61, 87.04]
2973                  [0.00, 85.70]

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2974 [ 14. 87, 86. 93]
2975 [ 37. 50, 90. 00]
2976 [ 38. 54, 90. 50]
2977 [ 42. 23, 91]
2978 [ 157. 05, 91. 50]
2979 * [ 161. 44, 91. 50]
2980 * [ 236. 48, 93. 00]
2981 * [ 385. 47, 92. 50]
2982 * [ 390. 78, 92. 50]
2983 *%-----|
2984 ROUTE CHANNEL NHYDout =["N_WCb" ] , NHYDin=["N_WCa" ] ,
2985 RDT=[ 1]( mi n) ,
2986 CHLGTH=[ 245. 33333]( m) , CHSLOPE=[ 0. 09511]( % ,
2987 FPSLOPE=[ 0. 09511]( % ,
2988 SECNUM=[ 1. 0] , NSEG=[ 3]
2989 ( SEGROUGH, SEGDI ST ( m) ) =
2990 [ 0. 050, - 37. 5
2991 - 0. 035, 37. 50
2992 0. 050, 157. 05] NSEG t i m e s
2993 ( DI STANCE ( m) , ELEVATI ON ( m) ) =
2994 [- 601. 81, 91. 5]
2995 [- 37. 50, 90. 00]
2996 [- 19. 61, 87. 04]
2997 [ 0. 00, 85. 70]
2998 [ 14. 87, 86. 93]
2999 [ 37. 50, 90. 00]
3000 [ 38. 54, 90. 50]
3001 [ 42. 23, 91]
3002 [ 157. 05, 91. 50]
3003 *%-----|
3004 ROUTE CHANNEL NHYDout =["N_WC" ] , NHYDin=["N_WCb" ] ,
3005 RDT=[ 1]( mi n) ,
3006 CHLGTH=[ 245. 33333]( m) , CHSLOPE=[ 0. 09511]( % ,
3007 FPSLOPE=[ 0. 09511]( % ,
3008 SECNUM=[ 1. 0] , NSEG=[ 3]
3009 ( SEGROUGH, SEGDI ST ( m) ) =
3010 [ 0. 050, - 37. 5
3011 - 0. 035, 37. 50
3012 0. 050, 157. 05] NSEG t i m e s
3013 ( DI STANCE ( m) , ELEVATI ON ( m) ) =
3014 [- 601. 81, 91. 5]
3015 [- 37. 50, 90. 00]
3016 [- 19. 61, 87. 04]
3017 [ 0. 00, 85. 70]
3018 [ 14. 87, 86. 93]
3019 [ 37. 50, 90. 00]
3020 [ 38. 54, 90. 50]
3021 [ 42. 23, 91]
3022 [ 157. 05, 91. 50]
3023 *#*****
3024 * - JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
(W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
3025 *ADD HYD NHYDs um=["SN_WC" ] , NHYDs to
add=["MS_P2"+"P2-OVF"+"N_WC"+"W_CLAR_UNDE" ]
3026 *%-----|
3027 *SAVE HYD NHYD=["SN_WC" ] , # OF PCYCLES=[ - 1] , ICASEsh=[ 1]
3028 * HYD_COMMENT=["Total Flows at West Clarke Pond Outlet" ]
3029 *%-----|
3030 *# Hydrograph from Node West Clarke routed to Node at Kennedy - Burnett Drain
3031 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4534
3032 *#
3033 ROUTE CHANNEL NHYDout =["N_KB" ] , NHYDin=["N_WC" ] ,
3034 RDT=[ 1]( mi n) ,
3035 CHLGTH=[ 1020]( m) , CHSLOPE=[ 0. 0498]( % ,
3036 FPSLOPE=[ 0. 0498]( % ,
3037 SECNUM=[ 1. 0] , NSEG=[ 3]

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3038 ( SEGROUGH, SEGDI ST ( m ) =
3039 [ 0. 050, - 23. 63
3040 - 0. 035, 23. 63
3041 0. 050, 728. 3] NSEG t i m e s
3042 ( DI STANCE ( m ) , ELEVATI ON ( m ) =
3043 [- 1082. 01, 94]
3044 [- 1028. 17, 92. 5]
3045 [- 992. 3, 93. 5]
3046 [- 279. 34, 90]
3047 [- 23. 63, 90]
3048 [- 13. 45, 87. 13]
3049 [- 0. 07, 86. 24]
3050 [ 10. 54, 87. 15]
3051 [ 23. 63, 90]
3052 [ 24. 86, 90. 5]
3053 [ 26. 72, 91]
3054 [ 45. 07, 91. 5]
3055 [ 128. 17, 91. 5]
3056 [ 270. 7, 92. 5]
3057 [ 728. 3, 95]
3058 *%-----|-----|
3059 *#*****|
3060 *# Catchment KEN_BU
3061 *# - To Kennedy-Burnett SWM Facility
3062 *# - Outlets to Fraser-Clarke drain (north of the Jock)
3063 *# - Medium density residential subdivision
3064 * - Add Kennedy Burnett model (Convert PCSWMM from NOVATECH June, 2020 to SWWHYMO)
3065 *#*****|
3066 *CONTINUOUS STANDHYD NHYD=["KEN_BU"], DT=[ 1] mi n, AREA=[ 281]( ha),
3067 * XI MP=[ 0. 55], TI MP=[ 0. 55], DWF=[ 0]( cms), LOSS=[ 2],
3068 * SCS curve number CN=[ 71],
3069 * Per vious surfaces: I A p e r=[ 4. 67]( mm), SLPP=[ 1]( %),
3070 * LGP=[ 40]( m), MNP=[ 0. 25], SCP=[ 0]( mi n),
3071 * I m p e r v i o u s surfaces: I A i m p=[ 1. 57]( mm), SLPI=[ 1]( %),
3072 * LGI=[ 1369]( m), MNI=[ 0. 013], SCI=[ 0]( mi n),
3073 * C o n t i n u o u s simulation parameters:
3074 * I a R E C p e r=[ 4]( hr s), I a R E C i m p=[ 4]( hr s),
3075 * S M N=[ - 1]( mm), S M A X=[ - 1]( mm), S K=[ 0. 010]/( mm),
3076 * I n t e r E v e n t T i m e=[ 18]( hr s), E N D=- 1
3077 *%-----|-----|
3078 *#*****|
3079 *# Existing Kennedy-Burnett SWM Facility
3080 *# - Rating curve obtained from URTKBP
3081 *# - Tributary Drainage Area to Pond = 160 ha
3082 *#*****|
3083 *ROUTE RESERVOIR NHYDout=["KEN_P"], NHYDin=["KEN_BU"],
3084 * RDT=[ 1]( mi n),
3085 * T A B L E of ( O U T F L O W S T O R A G E ) values
3086 * ( cms ) - ( ha - m )
3087 * [ 0. 0 , 0. 0 ]
3088 * [ 0. 13 , 0. 26]
3089 * [ 0. 43 , 0. 56]
3090 * [ 0. 67 , 0. 90]
3091 * [ 0. 86 , 1. 32]
3092 * [ 1. 01 , 1. 79]
3093 * [ 1. 15 , 2. 33]
3094 * [ - 1 , - 1 ] (max twenty pts)
3095 * N H Y D o v f=["KEN-OV"]
3096 *%-----|-----|
3097 * -JFSA, 2021-01-19 update all KEN_BU areas based on GIS measurements
3098 CONTINUOUS STANDHYD NHYD=["KB-01A"], DT=[ 1] mi n, AREA=[ 40. 82]( ha), XI MP=[ 0. 097],
3099 TI MP=[ 0. 4], DWF=[ 0]( cms), LOSS=[ 1]:
3099 Hort on: F o=[ 76. 20]( mm/ hr), F c=[ 13. 20]( mm/ hr), D C A Y=[ 4. 14]( / hr),
3100 F=[ 0. 00]( mm),
3100 P e r v i o u s areas: I A p e r=[ 4. 67]( mm), SLPP=[ 0. 5]( %), LGP=[ 40]( m),
MNP=[ 0. 250], SCP=[ 0]( mi n),

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3101      Impervious areas: I Aimp=[ 0.785](mm), SLPI=[ 0.5](%),
3102      LGI=[ 521.664](m), MNI=[ 0.013], SCI=[ 0](min),
3103      Continuous simulation parameters:
3103      I aRECPer=[ 4](hrs), I aRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3103      END=- 1
3104      *%-----|-----|
3105      COMPUTE DUALHYD      NHYDin=[ "KB-01A"], CINLET=[ 3.6](cms), NINLET=[ 1],
3106      MijNHYD=[ "KB-01A-M"]
3107      MnNHYD=[ "KB-01A-MN"]
3108      TMSSTO=[ 4995](cu-m)
3109      *%-----|-----|
3110      ADD HYD              NHYDsum=[ "KB-01A-S"], NHYDs to add=[ "KB-01A-M"+"KB-01A-MN"]
3111      *%-----|-----|
3112      CONTINUOUS STANDHYD NHYD=[ "KB-01B"], DT=[ 1]min, AREA=[ 31.1](ha), XI MP=[ 0.1875],
3112      TIMP=[ 0.375], DWF=[ 0](cms), LOSS=[ 1]:
3113      Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3113      F=[ 0.00](mm),
3114      Pervious areas: I Aper=[ 4.67](mm), SLPP=[ 0.42](%), LGP=[ 40](m),
3114      MNP=[ 0.250], SCP=[ 0](min),
3115      Impervious areas: I Aimp=[ 0.785](mm), SLPI=[ 0.42](%),
3115      LGI=[ 455.339](m), MNI=[ 0.013], SCI=[ 0](min),
3116      Continuous simulation parameters:
3117      I aRECPer=[ 4](hrs), I aRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3117      END=- 1
3118      *%-----|-----|
3119      COMPUTE DUALHYD      NHYDin=[ "KB-01B"], CINLET=[ 1.585](cms), NINLET=[ 1],
3120      MijNHYD=[ "KB-01B-M"]
3121      MnNHYD=[ "KB-01B-MN"]
3122      TMSSTO=[ 6075](cu-m)
3123      *%-----|-----|
3124      ADD HYD              NHYDsum=[ "KB-01B-S"], NHYDs to add=[ "KB-01B-M"+"KB-01B-MN"]
3125      *%-----|-----|
3126      CONTINUOUS STANDHYD NHYD=[ "KB-01C"], DT=[ 1]min, AREA=[ 13.78](ha), XI MP=[ 0.2045],
3126      TIMP=[ 0.409], DWF=[ 0](cms), LOSS=[ 1]:
3127      Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3127      F=[ 0.00](mm),
3128      Pervious areas: I Aper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3128      MNP=[ 0.250], SCP=[ 0](min),
3129      Impervious areas: I Aimp=[ 0.785](mm), SLPI=[ 0.5](%),
3129      LGI=[ 303.095](m), MNI=[ 0.013], SCI=[ 0](min),
3130      Continuous simulation parameters:
3131      I aRECPer=[ 4](hrs), I aRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3131      END=- 1
3132      *%-----|-----|
3133      COMPUTE DUALHYD      NHYDin=[ "KB-01C"], CINLET=[ 1.35](cms), NINLET=[ 1],
3134      MijNHYD=[ "KB-01C-M"]
3135      MnNHYD=[ "KB-01C-MN"]
3136      TMSSTO=[ 1880](cu-m)
3137      *%-----|-----|
3138      ADD HYD              NHYDsum=[ "KB-01C-S"], NHYDs to add=[ "KB-01C-M"+"KB-01C-MN"]
3139      *%-----|-----|
3140      CONTINUOUS STANDHYD NHYD=[ "KB-03"], DT=[ 1]min, AREA=[ 84.78](ha), XI MP=[ 0.197],
3140      TIMP=[ 0.394], DWF=[ 0](cms), LOSS=[ 1]:
3141      Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3141      F=[ 0.00](mm),
3142      Pervious areas: I Aper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3142      MNP=[ 0.250], SCP=[ 0](min),
3143      Impervious areas: I Aimp=[ 0.785](mm), SLPI=[ 0.63](%),
3143      LGI=[ 751.798](m), MNI=[ 0.013], SCI=[ 0](min),
3144      Continuous simulation parameters:
3145      I aRECPer=[ 4](hrs), I aRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3145      END=- 1
3146      *%-----|-----|
3147      COMPUTE DUALHYD      NHYDin=[ "KB-03"], CINLET=[ 5.27](cms), NINLET=[ 1],
3148      MijNHYD=[ "KB-03-M"]
3149      MnNHYD=[ "KB-03-MN"]

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3150          TMI STO=[ 15500] (cu-m)
3151  *%-----|-----|
3152  ADD HYD      NHYDs um=[ " KB- 03- S" ], NHYDs to add=[ " KB- 03- M" +" KB- 03- MN" ]
3153  *%-----|-----|
3154  CONTI NUOUS STANDHYD NHYD=[ " KB- 04" ], DT=[ 1] mi n, AREA=[ 6.95] (ha), XI MP=[ 0.85],
TI MP=[ 0.85], DWF=[ 0] (cms), LOSS=[ 1]:
3155          Hort on: Fo=[ 76.20] (mm/ hr), Fc=[ 13.20] (mm/ hr), DCAY=[ 4.14] (/ hr),
F=[ 0.00] (mm),
3156          Perv ious areas: I Aper=[ 4.67] (mm), SLPP=[ 2.0] (%), LGP=[ 40] (m),
MNP=[ 0.250], SCP=[ 0] (mi n),
3157          Imperv ious areas: I Ai mp=[ 0.942] (mm), SLPI =[ 0.5] (%),
LGI =[ 215.252] (m), MNI =[ 0.013], SCI =[ 0] (mi n),
3158          Continuous simulation parameters:
3159          IaRECper=[ 4] (hr s), IaRECI mp=[ 4] (hr s), Int er Event Ti me=[ 12] (hr s),
END=- 1
3160  *%-----|-----|
3161  COMPUTE DUALHYD NHYDi n=[ " KB- 04" ], CI NLET=[ 0.503] (cms), NI NLET=[ 1],
3162          Maj NHYD=[ " KB- 04- M" ]
3163          M nNHYD=[ " KB- 04- MN" ]
3164          TMI STO=[ 1972] (cu-m)
3165  *%-----|-----|
3166  ADD HYD      NHYDs um=[ " KB- 04- S" ], NHYDs to add=[ " KB- 04- M" +" KB- 04- MN" ]
3167  *%-----|-----|
3168  CONTI NUOUS STANDHYD NHYD=[ " KB- 05" ], DT=[ 1] mi n, AREA=[ 5.19] (ha), XI MP=[ 0.93],
TI MP=[ 0.93], DWF=[ 0] (cms), LOSS=[ 1]:
3169          Hort on: Fo=[ 76.20] (mm/ hr), Fc=[ 13.20] (mm/ hr), DCAY=[ 4.14] (/ hr),
F=[ 0.00] (mm),
3170          Perv ious areas: I Aper=[ 4.67] (mm), SLPP=[ 2.0] (%), LGP=[ 40] (m),
MNP=[ 0.250], SCP=[ 0] (mi n),
3171          Imperv ious areas: I Ai mp=[ 1.57] (mm), SLPI =[ 0.5] (%),
LGI =[ 186.011] (m), MNI =[ 0.013], SCI =[ 0] (mi n),
3172          Continuous simulation parameters:
3173          IaRECper=[ 4] (hr s), IaRECI mp=[ 4] (hr s), Int er Event Ti me=[ 12] (hr s),
END=- 1
3174  *%-----|-----|
3175  *%-----|-----|
3176  CONTI NUOUS STANDHYD NHYD=[ " KB- 06" ], DT=[ 1] mi n, AREA=[ 12.93] (ha), XI MP=[ 0.873],
TI MP=[ 0.873], DWF=[ 0] (cms), LOSS=[ 1]:
3177          Hort on: Fo=[ 76.20] (mm/ hr), Fc=[ 13.20] (mm/ hr), DCAY=[ 4.14] (/ hr),
F=[ 0.00] (mm),
3178          Perv ious areas: I Aper=[ 4.67] (mm), SLPP=[ 2.0] (%), LGP=[ 40] (m),
MNP=[ 0.250], SCP=[ 0] (mi n),
3179          Imperv ious areas: I Ai mp=[ 0.942] (mm), SLPI =[ 4.75] (%),
LGI =[ 293.598] (m), MNI =[ 0.013], SCI =[ 0] (mi n),
3180          Continuous simulation parameters:
3181          IaRECper=[ 4] (hr s), IaRECI mp=[ 4] (hr s), Int er Event Ti me=[ 12] (hr s),
END=- 1
3182  *%-----|-----|
3183  COMPUTE DUALHYD NHYDi n=[ " KB- 06" ], CI NLET=[ 2.262] (cms), NI NLET=[ 1],
3184          Maj NHYD=[ " KB- 06- M" ]
3185          M nNHYD=[ " KB- 06- MN" ]
3186          TMI STO=[ 1950] (cu-m)
3187  *%-----|-----|
3188  ADD HYD      NHYDs um=[ " KB- 06- S" ], NHYDs to add=[ " KB- 06- M" +" KB- 06- MN" ]
3189  *%-----|-----|
3190  CONTI NUOUS STANDHYD NHYD=[ " KB- 11" ], DT=[ 1] mi n, AREA=[ 4.03] (ha), XI MP=[ 0.675],
TI MP=[ 0.675], DWF=[ 0] (cms), LOSS=[ 1]:
3191          Hort on: Fo=[ 76.20] (mm/ hr), Fc=[ 13.20] (mm/ hr), DCAY=[ 4.14] (/ hr),
F=[ 0.00] (mm),
3192          Perv ious areas: I Aper=[ 4.67] (mm), SLPP=[ 2.0] (%), LGP=[ 40] (m),
MNP=[ 0.250], SCP=[ 0] (mi n),
3193          Imperv ious areas: I Ai mp=[ 0.785] (mm), SLPI =[ 2.0] (%),
LGI =[ 163.911] (m), MNI =[ 0.013], SCI =[ 0] (mi n),
3194          Continuous simulation parameters:
3195          IaRECper=[ 4] (hr s), IaRECI mp=[ 4] (hr s), Int er Event Ti me=[ 12] (hr s),
END=- 1

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3196 *%-----|-----|
3197 COMPUTE DUALHYD NHYDin=["KB-11"], CINLET=[0.5773](cms), NINLET=[1],
3198 MajNHYD=["KB-11-M"]
3199 MnNHYD=["KB-11-MN"]
3200 TMSTO=[597](cu-m)
3201 *%-----|-----|
3202 ADD HYD NHYDsum=["KB-11-S"], NHYDs to add=["KB-11-M"+"KB-11-MN"]
3203 *%-----|-----|
3204 CONTINUOUS STANDHYD NHYD=["S1"], DT=[1]min, AREA=[4.99](ha), XI MP=[0.93], TI MP=[0.93],
DWF=[0](cms), LOSS=[1]:
3205 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3206 Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3207 Impervious areas: I Ai mp=[1.57](mm), SLPI=[2.0](%),
LGI=[182.392](m), MNI=[0.013], SCI=[0](min),
3208 Continuous simulation parameters:
3209 I a RE C per=[4](hrs), I a RE C i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
3210 *%-----|-----|
3211 CONTINUOUS STANDHYD NHYD=["KB-15"], DT=[1]min, AREA=[2.15](ha), XI MP=[0.79],
TI MP=[0.79], DWF=[0](cms), LOSS=[1]:
3212 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3213 Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3214 Impervious areas: I Ai mp=[0.157](mm), SLPI=[0.3](%),
LGI=[119.722](m), MNI=[0.013], SCI=[0](min),
3215 Continuous simulation parameters:
3216 I a RE C per=[4](hrs), I a RE C i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
3217 *%-----|-----|
3218 *%-----|-----|
3219 ADD HYD NHYDsum=["KB-P1"], NHYDs to
add=["KB-01A-S"+"KB-01B-S"+"KB-01C-S"+"KB-03-S"+"KB-04-S"+"KB-05"+"KB-06-S"+"KB-11-S"+"KB
-15"+"S1"]
3220 *%-----|-----|
3221 ROUTE RESERVOIR NHYDout=["KB-P1R"], NHYDin=["KB-P1"],
3222 RDT=[1](min),
3223 TABLE of ( OUTFLOW STORAGE ) values
3224 (cms) - (ha-m)
3225 [ 0.0 , 0.0 ]
3226 [0.076,0.003]
3227 [0.088,0.006]
3228 [0.136,0.011]
3229 [0.301,0.017]
3230 [0.454,0.027]
3231 [0.631,0.041]
3232 [1.173,0.068]
3233 [1.91,0.111]
3234 [4.847,0.231]
3235 [9.813,0.436]
3236 [12.134,0.617]
3237 [12.438,0.732]
3238 [12.424,0.811]
3239 [12.425,0.894]
3240 [ -1 , -1 ] (max twenty pts)
3241 NHYDovf=["KB-P1ovf"]
3242 *%-----|-----|
3243 ADD HYD NHYDsum=["KB-Pond1"], NHYDs to add=["KB-P1R"+"KB-P1ovf"]
3244 *%-----|-----|
3245 SAVE HYD NHYD=["KB-Pond1"], # OF PCYCLES=[-1], I CASEs h=[1]
3246 HYD_COMMENT=["Total Flows at KB first pond"]
3247 *%-----|-----|
3248 CONTINUOUS STANDHYD NHYD=["KB-07"], DT=[1]min, AREA=[10.86](ha), XI MP=[0.86],
TI MP=[0.86], DWF=[0](cms), LOSS=[1]:

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3249      Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
3250      F=[ 0.00](mm),
3251      Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3252      MNP=[ 0.250], SCP=[ 0](min),
3253      Impervious areas: IAimp=[ 0.785](mm), SLPI=[ 2.0](%),
3254      LGI=[ 269.072](m), MNI=[ 0.013], SCI=[ 0](min),
3255      Continuous simulation parameters:
3256      IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3257      END=- 1
3258
3259      *%-----|-----|
3260      COMPUTE DUALHYD NHYDin=[ "KB-07"], CINLET=[ 2.094](cms), NINLET=[ 1],
3261      MajNHYD=[ "KB-07-M"]
3262      MinNHYD=[ "KB-07-MN"]
3263      TMSSTO=[ 1378](cu-m)
3264
3265      *%-----|-----|
3266      ADD HYD NHYDsum=[ "KB-07-S"], NHYDsto add=[ "KB-07-M"+"KB-07-MN"]
3267      *%-----|-----|
3268      CONTINUOUS STANDHYD NHYD=[ "KB-08"], DT=[ 1]min, AREA=[ 6.61](ha), XI MP=[ 0.64],
3269      TITMP=[ 0.64], DWF=[ 0](cms), LOSS=[ 1]:
3270      Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
3271      F=[ 0.00](mm),
3272      Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3273      MNP=[ 0.250], SCP=[ 0](min),
3274      Impervious areas: IAimp=[ 0.785](mm), SLPI=[ 2.0](%),
3275      LGI=[ 209.921](m), MNI=[ 0.013], SCI=[ 0](min),
3276      Continuous simulation parameters:
3277      IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3278      END=- 1
3279
3280      *%-----|-----|
3281      COMPUTE DUALHYD NHYDin=[ "KB-08"], CINLET=[ 1.058](cms), NINLET=[ 1],
3282      MajNHYD=[ "KB-08-M"]
3283      MinNHYD=[ "KB-08-MN"]
3284      TMSSTO=[ 787](cu-m)
3285
3286      *%-----|-----|
3287      ADD HYD NHYDsum=[ "KB-08-S"], NHYDsto add=[ "KB-08-M"+"KB-08-MN"]
3288      *%-----|-----|
3289      CONTINUOUS STANDHYD NHYD=[ "KB-09"], DT=[ 1]min, AREA=[ 2.6](ha), XI MP=[ 0.86],
3290      TITMP=[ 0.86], DWF=[ 0](cms), LOSS=[ 1]:
3291      Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
3292      F=[ 0.00](mm),
3293      Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3294      MNP=[ 0.250], SCP=[ 0](min),
3295      Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 2.0](%),
3296      LGI=[ 131.656](m), MNI=[ 0.013], SCI=[ 0](min),
3297      Continuous simulation parameters:
3298      IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3299      END=- 1
3300
3301      *%-----|-----|
3302      *%-----|-----|
3303      CONTINUOUS STANDHYD NHYD=[ "KB-10_1"], DT=[ 1]min, AREA=[ 2.37](ha), XI MP=[ 0.86],
3304      TITMP=[ 0.86], DWF=[ 0](cms), LOSS=[ 1]:
3305      Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
3306      F=[ 0.00](mm),
3307      Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3308      MNP=[ 0.250], SCP=[ 0](min),
3309      Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 2.0](%),
3310      LGI=[ 125.698](m), MNI=[ 0.013], SCI=[ 0](min),
3311      Continuous simulation parameters:
3312      IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3313      END=- 1
3314
3315      *%-----|-----|
3316      CONTINUOUS STANDHYD NHYD=[ "KB-10_2"], DT=[ 1]min, AREA=[ 1.14](ha), XI MP=[ 0.86],
3317      TITMP=[ 0.86], DWF=[ 0](cms), LOSS=[ 1]:
3318      Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
3319      F=[ 0.00](mm),
3320      Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),

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3294 MNP=[ 0.250], SCP=[ 0](mi n),
Impervious areas: IAi mp=[ 1.57](mm), SLPI=[ 2.0](%), LGI=[ 87.178](m),
MNI=[ 0.013], SCI=[ 0](mi n),
3295 Continuous simulation parameters:
3296 IaREcper=[ 4](hrs), IaRECi mp=[ 4](hrs), InterEventTime=[ 12](hrs),
END=- 1
3297 *%-----|-----|
3298 *%-----|-----|
3299 CONTINUOUS STANDHYD NHYD=["KB-12"], DT=[ 1]mi n, AREA=[ 4.86](ha), XI MP=[ 0.79],
TIMP=[ 0.79], DWF=[ 0](cms), LOSS=[ 1]:
3300 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
F=[ 0.00](mm),
3301 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
MNP=[ 0.250], SCP=[ 0](mi n),
3302 Impervious areas: IAi mp=[ 1.099](mm), SLPI=[ 2.0](%),
LGI=[ 180.000](m), MNI=[ 0.013], SCI=[ 0](mi n),
3303 Continuous simulation parameters:
3304 IaREcper=[ 4](hrs), IaRECi mp=[ 4](hrs), InterEventTime=[ 12](hrs),
END=- 1
3305 *%-----|-----|
3306 COMPUTE DUALHYD NHYDin=["KB-12"], CILET=[ 0.8665](cms), NILET=[ 1],
3307 MajNHYD=["KB-12-M"]
3308 MnNHYD=["KB-12-MN"]
3309 TMS TO=[ 632](cu-m)
3310 *%-----|-----|
3311 ADD HYD NHYDsum=["KB-12-S"], NHYDsto add=["KB-12-M"+"KB-12-MN"]
3312 *%-----|-----|
3313 CONTINUOUS STANDHYD NHYD=["KB-13"], DT=[ 1]mi n, AREA=[ 10.19](ha), XI MP=[ 0.64],
TIMP=[ 0.64], DWF=[ 0](cms), LOSS=[ 1]:
3314 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
F=[ 0.00](mm),
3315 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
MNP=[ 0.250], SCP=[ 0](mi n),
3316 Impervious areas: IAi mp=[ 0.785](mm), SLPI=[ 2.0](%),
LGI=[ 260.640](m), MNI=[ 0.013], SCI=[ 0](mi n),
3317 Continuous simulation parameters:
3318 IaREcper=[ 4](hrs), IaRECi mp=[ 4](hrs), InterEventTime=[ 12](hrs),
END=- 1
3319 *%-----|-----|
3320 COMPUTE DUALHYD NHYDin=["KB-13"], CILET=[ 1.722](cms), NILET=[ 1],
3321 MajNHYD=["KB-13-M"]
3322 MnNHYD=["KB-13-MN"]
3323 TMS TO=[ 1077](cu-m)
3324 *%-----|-----|
3325 ADD HYD NHYDsum=["KB-13-S"], NHYDsto add=["KB-13-M"+"KB-13-MN"]
3326 *%-----|-----|
3327 CONTINUOUS STANDHYD NHYD=["KB-14"], DT=[ 1]mi n, AREA=[ 5.47](ha), XI MP=[ 0.64],
TIMP=[ 0.64], DWF=[ 0](cms), LOSS=[ 1]:
3328 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
F=[ 0.00](mm),
3329 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
MNP=[ 0.250], SCP=[ 0](mi n),
3330 Impervious areas: IAi mp=[ 0.785](mm), SLPI=[ 2.0](%),
LGI=[ 190.962](m), MNI=[ 0.013], SCI=[ 0](mi n),
3331 Continuous simulation parameters:
3332 IaREcper=[ 4](hrs), IaRECi mp=[ 4](hrs), InterEventTime=[ 12](hrs),
END=- 1
3333 *%-----|-----|
3334 COMPUTE DUALHYD NHYDin=["KB-14"], CILET=[ 0.8734](cms), NILET=[ 1],
3335 MajNHYD=["KB-14-M"]
3336 MnNHYD=["KB-14-MN"]
3337 TMS TO=[ 631](cu-m)
3338 *%-----|-----|
3339 ADD HYD NHYDsum=["KB-14-S"], NHYDsto add=["KB-14-M"+"KB-14-MN"]
3340 *%-----|-----|
3341 *%-----|-----|

```



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3342 CONTINUOUS STANDHYD NHYD=["KB-16_2"], DT=[1] min, AREA=[3.42](ha), XI MP=[0.71],
TI MP=[0.71], DWF=[0](cms), LOSS=[1]:
3343 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3344 Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3345 Impervious areas: I A i mp=[0.157](mm), SLPI=[0.3](%),
LGI=[150.997](m), MNI=[0.013], SCI=[0](min),
3346 Continuous simulation parameters:
3347 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=- 1
3348 *%-----|-----|
3349 ADD HYD NHYDsum=["KB-P2"], NHYDs to
add=["KB-Pond1"+"KB-07-S"+"KB-08-S"+"KB-09"+"KB-10_1"+"KB-10_2"+"KB-12-S"+"KB-13-S"+"KB-1
4-S"+"KB-16_2"]
3350 *%-----|-----|
3351 ROUTE RESERVOIR NHYDout=["KB-P2R"], NHYDin=["KB-P2"],
3352 RDT=[1](min),
3353 TABLE of ( OUTFLOW STORAGE ) values
3354 (cms) - (ha-m)
3355 [ 0.0 , 0.0 ]
3356 [ 0.053, 0.005 ]
3357 [ 0.132, 0.009 ]
3358 [ 0.269, 0.014 ]
3359 [ 0.455, 0.023 ]
3360 [ 0.699, 0.037 ]
3361 [ 0.947, 0.056 ]
3362 [ 1.853, 0.09 ]
3363 [ 2.712, 0.146 ]
3364 [ 6.626, 0.287 ]
3365 [ 11.228, 0.515 ]
3366 [ 14.885, 0.738 ]
3367 [ 16.473, 0.893 ]
3368 [ 17.311, 0.998 ]
3369 [ 17.633, 1.063 ]
3370 [ 17.634, 1.112 ]
3371 [ -1 , -1 ] (max twenty pts)
3372 NHYDovf=["KB-P2ovf"]
3373 *%-----|-----|
3374 ADD HYD NHYDsum=["KB-Pond2"], NHYDs to add=["KB-P2R"+"KB-P2ovf"]
3375 *%-----|-----|
3376 SAVE HYD NHYD=["KB-Pond2"], # OF PCYCLES=[-1], I CASEs h=[1]
3377 HYD_COMMENT=["Total Flows at KB second pond"]
3378 *%-----|-----|
3379 CONTINUOUS STANDHYD NHYD=["KB-16_1"], DT=[1] min, AREA=[2.8](ha), XI MP=[0.75],
TI MP=[0.75], DWF=[0](cms), LOSS=[1]:
3380 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3381 Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3382 Impervious areas: I A i mp=[0.157](mm), SLPI=[0.3](%),
LGI=[136.626](m), MNI=[0.013], SCI=[0](min),
3383 Continuous simulation parameters:
3384 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=- 1
3385 *%-----|-----|
3386 ADD HYD NHYDsum=["KB-P3"], NHYDs to add=["KB-Pond2"+"KB-16_1"]
3387 *%-----|-----|
3388 *%-----|-----|
3389 * One inflow node from pond 3 is added to the model (ROUTE RESERVOIR)
3390 * Another inflow node from right side of pond 3 is not added to the model
3391 ROUTE RESERVOIR NHYDout=["KB-P3R"], NHYDin=["KB-P3"],
3392 RDT=[1](min),
3393 TABLE of ( OUTFLOW STORAGE ) values
3394 (cms) - (ha-m)
3395 [ 0.0 , 0.0 ]

```

```

3396 [ 0.051, 0.002]
3397 [ 0.048, 0.003]
3398 [ 0.057, 0.029]
3399 [ 0.089, 0.045]
3400 [ 0.133, 0.069]
3401 [ 0.199, 0.106]
3402 [ 0.321, 0.172]
3403 [ 1.029, 0.306]
3404 [ 4.036, 0.527]
3405 [ 8.332, 0.761]
3406 [ 11.727, 0.941]
3407 [ 14.125, 1.067]
3408 [ 15.675, 1.149]
3409 [ 16.555, 1.196]
3410 [ 16.911, 1.214]
3411 [ -1 , -1 ] (max twenty pts)
3412 NHYDovf=["KB- P3ovf"]
3413 *%-----|-----|
3414 ADD HYD NHYDs um=["KB- Pond3"], NHYDs to add=["KB- P3R"+"KB- P3ovf"]
3415 *%-----|-----|
3416 SAVE HYD NHYD=["KB- Pond3"], # OF PCYCLES=[- 1], ICASEsh=[ 1]
3417 HYD_COMMENT=["Total Flows at KB third pond"]
3418 *%-----|-----|
3419 *#*****|
3420 *# EXISTING / PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118080), SWM
3421 Modeling Approach, NOVATECH Report June, 2020)
3422 *# - TO FRASER- CLARKE DRAIN
3423 *#*****|
3424 CONTINUOUS STANDHYD NHYD=["FC- 01"], DT=[ 1] min, AREA=[ 8.03] (ha), XI MP=[ 0.47],
3425 TI MP=[ 0.47], DWF=[ 0] (cms), LOSS=[ 1]:
3426 Horton: Fo=[ 76.20] (mm/ hr), Fc=[ 13.20] (mm/ hr), DCAY=[ 4.14] (/ hr),
3427 F=[ 0.00] (mm),
3428 Pervious areas: IAper=[ 4.67] (mm), SLPP=[ 2.0] (%), LGP=[ 40] (m),
3429 MNP=[ 0.250], SCP=[ 0] (min),
3430 Impervious areas: IAimp=[ 1.57] (mm), SLPI=[ 1.0] (%),
3431 LGI=[ 231.373] (m), MNI=[ 0.013], SCI=[ 0] (min),
3432 Continuous simulation parameters:
3433 IARECper=[ 4] (hrs), IARECimp=[ 4] (hrs), InterEventTime=[ 12] (hrs),
3434 END=- 1
3435 *%-----|-----|
3436 COMPUTE DUALHYD NHYDin=["FC- 01"], CILET=[ 0.756] (cms), NILET=[ 1],
3437 MajNHYD=["FC- 01- M"]
3438 MnNHYD=["FC- 01- MN"]
3439 TMS TO=[ 714] (cu- m)
3440 *%-----|-----|
3441 ADD HYD NHYDs um=["FC- 01- S"], NHYDs to add=["FC- 01- M"+"FC- 01- MN"]
3442 *%-----|-----|
3443 CONTINUOUS STANDHYD NHYD=["FC- 02"], DT=[ 1] min, AREA=[ 16.05] (ha), XI MP=[ 0.93],
3444 TI MP=[ 0.93], DWF=[ 0] (cms), LOSS=[ 1]:
3445 Horton: Fo=[ 76.20] (mm/ hr), Fc=[ 13.20] (mm/ hr), DCAY=[ 4.14] (/ hr),
3446 F=[ 0.00] (mm),
3447 Pervious areas: IAper=[ 4.67] (mm), SLPP=[ 2.0] (%), LGP=[ 40] (m),
3448 MNP=[ 0.250], SCP=[ 0] (min),
3449 Impervious areas: IAimp=[ 1.57] (mm), SLPI=[ 1.0] (%),
3450 LGI=[ 327.109] (m), MNI=[ 0.013], SCI=[ 0] (min),
3451 Continuous simulation parameters:
3452 IARECper=[ 4] (hrs), IARECimp=[ 4] (hrs), InterEventTime=[ 12] (hrs),
3453 END=- 1
3454 *%-----|-----|
3455 COMPUTE DUALHYD NHYDin=["FC- 02"], CILET=[ 1.159] (cms), NILET=[ 1],
3456 MajNHYD=["FC- 02- M"]
3457 MnNHYD=["FC- 02- MN"]
3458 TMS TO=[ 2385] (cu- m)
3459 *%-----|-----|
3460 ADD HYD NHYDs um=["FC- 02- S"], NHYDs to add=["FC- 02- M"+"FC- 02- MN"]
3461 *%-----|-----|

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3451 CONTINUOUS STANDHYD NHYD=[ "FC- 03" ], DT=[ 1 ] mi n, AREA=[ 7. 37 ] ( ha ), XI MP=[ 0. 64 ],
TI MP=[ 0. 64 ], DWF=[ 0 ] ( cms ), LOSS=[ 1 ] :
3452 Horton: Fo=[ 76. 20 ] ( mm/ hr ), Fc=[ 13. 20 ] ( mm/ hr ), DCAY=[ 4. 14 ] ( / hr ),
F=[ 0. 00 ] ( mm ),
3453 Pervious areas: IAper=[ 4. 67 ] ( mm ), SLPP=[ 2. 0 ] ( % ), LGP=[ 40 ] ( m ),
MNP=[ 0. 250 ], SCP=[ 0 ] ( mi n ),
3454 Impervious areas: IAi mp=[ 1. 57 ] ( mm ), SLPI =[ 1. 0 ] ( % ),
LGI =[ 221. 660 ] ( m ), MNI =[ 0. 013 ], SCI =[ 0 ] ( mi n ),
3455 Continuous simulation parameters:
3456 IaRECper=[ 4 ] ( hrs ), IaRECI mp=[ 4 ] ( hrs ), Inter Event Time=[ 12 ] ( hrs ),
END=- 1
3457 *%-----|
3458 COMPUTE DUALHYD NHYDi n=[ "FC- 03" ], CI NLET=[ 0. 358 ] ( cms ), NI NLET=[ 1 ],
3459 MAj NHYD=[ "FC- 03- M" ]
3460 M nNHYD=[ "FC- 03- MN" ]
3461 TM STO=[ 1131 ] ( cu- m )
3462 *%-----|
3463 ADD HYD NHYDsum=[ "FC- 03- S" ], NHYDs to add=[ "FC- 03- M" +"FC- 03- MN" ]
3464 *%-----|
3465 CONTINUOUS STANDHYD NHYD=[ "FC- 04" ], DT=[ 1 ] mi n, AREA=[ 12. 87 ] ( ha ), XI MP=[ 0. 64 ],
TI MP=[ 0. 64 ], DWF=[ 0 ] ( cms ), LOSS=[ 1 ] :
3466 Horton: Fo=[ 76. 20 ] ( mm/ hr ), Fc=[ 13. 20 ] ( mm/ hr ), DCAY=[ 4. 14 ] ( / hr ),
F=[ 0. 00 ] ( mm ),
3467 Pervious areas: IAper=[ 4. 67 ] ( mm ), SLPP=[ 2. 0 ] ( % ), LGP=[ 40 ] ( m ),
MNP=[ 0. 250 ], SCP=[ 0 ] ( mi n ),
3468 Impervious areas: IAi mp=[ 1. 57 ] ( mm ), SLPI =[ 1. 0 ] ( % ),
LGI =[ 292. 916 ] ( m ), MNI =[ 0. 013 ], SCI =[ 0 ] ( mi n ),
3469 Continuous simulation parameters:
3470 IaRECper=[ 4 ] ( hrs ), IaRECI mp=[ 4 ] ( hrs ), Inter Event Time=[ 12 ] ( hrs ),
END=- 1
3471 *%-----|
3472 COMPUTE DUALHYD NHYDi n=[ "FC- 04" ], CI NLET=[ 0. 741 ] ( cms ), NI NLET=[ 1 ],
3473 MAj NHYD=[ "FC- 04- M" ]
3474 M nNHYD=[ "FC- 04- MN" ]
3475 TM STO=[ 1794 ] ( cu- m )
3476 *%-----|
3477 ADD HYD NHYDsum=[ "FC- 04- S" ], NHYDs to add=[ "FC- 04- M" +"FC- 04- MN" ]
3478 *%-----|
3479 *#*****
3480 *# PROPOSED Subcatchments ( Kennedy- Burnett SWM Facility ( 118080 ), SWM Mdeling
Approach, NOVATECH Report June, 2020)
3481 *# - TO JOCK RI VER
3482 *#*****
3483 CONTINUOUS STANDHYD NHYD=[ "JR- 01" ], DT=[ 1 ] mi n, AREA=[ 8. 24 ] ( ha ), XI MP=[ 0. 64 ],
TI MP=[ 0. 64 ], DWF=[ 0 ] ( cms ), LOSS=[ 1 ] :
3484 Horton: Fo=[ 76. 20 ] ( mm/ hr ), Fc=[ 13. 20 ] ( mm/ hr ), DCAY=[ 4. 14 ] ( / hr ),
F=[ 0. 00 ] ( mm ),
3485 Pervious areas: IAper=[ 4. 67 ] ( mm ), SLPP=[ 2. 0 ] ( % ), LGP=[ 40 ] ( m ),
MNP=[ 0. 250 ], SCP=[ 0 ] ( mi n ),
3486 Impervious areas: IAi mp=[ 1. 57 ] ( mm ), SLPI =[ 1. 0 ] ( % ),
LGI =[ 234. 379 ] ( m ), MNI =[ 0. 013 ], SCI =[ 0 ] ( mi n ),
3487 Continuous simulation parameters:
3488 IaRECper=[ 4 ] ( hrs ), IaRECI mp=[ 4 ] ( hrs ), Inter Event Time=[ 12 ] ( hrs ),
END=- 1
3489 *%-----|
3490 COMPUTE DUALHYD NHYDi n=[ "JR- 01" ], CI NLET=[ 0. 563 ] ( cms ), NI NLET=[ 1 ],
3491 MAj NHYD=[ "JR- 01- M" ]
3492 M nNHYD=[ "JR- 01- MN" ]
3493 TM STO=[ 1040 ] ( cu- m )
3494 *%-----|
3495 ADD HYD NHYDsum=[ "JR- 01- S" ], NHYDs to add=[ "JR- 01- M" +"JR- 01- MN" ]
3496 *%-----|
3497 CONTINUOUS STANDHYD NHYD=[ "JR- 02" ], DT=[ 1 ] mi n, AREA=[ 1. 59 ] ( ha ), XI MP=[ 0. 64 ],
TI MP=[ 0. 64 ], DWF=[ 0 ] ( cms ), LOSS=[ 1 ] :
3498 Horton: Fo=[ 76. 20 ] ( mm/ hr ), Fc=[ 13. 20 ] ( mm/ hr ), DCAY=[ 4. 14 ] ( / hr ),
F=[ 0. 00 ] ( mm ),

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3499          Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3500          MNP=[ 0.250], SCP=[ 0](min),
3501          Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 1.0](%),
3502          LGI=[ 102.956](m), MNI=[ 0.013], SCI=[ 0](min),
3503          Continuous simulation parameters:
3504          IaREcper=[ 4](hrs), IaREcimp=[ 4](hrs), InterEventTime=[ 12](hrs),
3505          END=- 1
3506
3507 *%-----|-----|
3508 COMPUTE DUALHYD NHYDin=["JR-02"], CINLET=[ 0.153](cms), NINLET=[ 1],
3509          MajNHYD=["JR-02-M"],
3510          MnNHYD=["JR-02-MN"],
3511          TMSSTO=[ 153](cu-m)
3512
3513 *%-----|-----|
3514 ADD HYD          NHYDsum=["JR-02-S"], NHYDs to add=["JR-02-M"+"JR-02-MN"]
3515
3516 *%-----|-----|
3517 *******|*****|
3518 ##          Catchment FRASER
3519 ##          - To Fraser-Clarke drain (north of the Jock)
3520 ##          - Developed land with assumed 43% imp.
3521 ##          - 2020-12-17 Change Fraser area to be 35.1 as measured from QGIS
3522 ##          - 2020-12-17 All Fraser is undeveloped (Nashyd)
3523 *******|*****|
3524 CONTINUOUS NASHYD NHYD=["FRASER-DRN"], DT=[ 1]min, AREA=[ 13.65](ha),
3525          DWF=[ 0](cms), CN=C=[ 77], IA=[ 4.67](mm),
3526          N=[ 3], TP=[ 0.4258]hrs,
3527          Continuous simulation parameters:
3528          IaREcper=[ 4](hrs),
3529          SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
3530          InterEventTime=[ 12](hrs)
3531          Baseflow simulation parameters:
3532          BaseFlowOption=[ 1],
3533          InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
3534          VHydCond=[ 0.055](mm/hr), END=- 1
3535
3536 *
3537 CONTINUOUS STANDHYD NHYD=["FRASER-D"], DT=[ 1]min, AREA=[ 21.61](ha),
3538          XI MP=[ 0.585], TI MP=[ 0.585], DWF=[ 0](cms), LOSS=[ 2],
3539          SCS curve number CN=[ 80],
3540          Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
3541          LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
3542          Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
3543          LGI=[ 379.561](m), MNI=[ 0.013], SCI=[ 0](min),
3544          Continuous simulation parameters:
3545          IaREcper=[ 4](hrs), IaREcimp=[ 4](hrs),
3546          SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
3547          InterEventTime=[ 18](hrs), END=- 1
3548
3549 *%-----|-----|
3550 COMPUTE DUALHYD NHYDin=["FRASER-D"], CINLET=[ 2.281](cms), NINLET=[ 1],
3551          MajNHYD=["FRASER-J"],
3552          MnNHYD=["FRASER-N"],
3553          TMSSTO=[ 9999999](cu-m)
3554
3555 *%-----|-----|
3556 ADD HYD          NHYDsum=["FRASER-S"], NHYDs to add=["FRASER-J"+"FRASER-N"]
3557
3558 *%-----|-----|
3559 *ROUTE RESERVOIR NHYDout=["MS_P20"], NHYDin=["FRASER"],
3560          *
3561          RDT=[ 1](min),
3562          *
3563          TABLE of ( OUTFLOW STORAGE ) values
3564          *
3565          ( cms ) - ( ha-m )
3566          *
3567          [ 0.0 , 0.0 ]
3568          *
3569          [ 0.04 , 0.36 ]
3570          *
3571          [ -1 , -1 ] (max twenty pts)
3572          *
3573          NHYDovf=["P20-OVF"]
3574
3575 *%-----|-----|
3576 ADD HYD          NHYDsum=["4241"], NHYDs to
3577          add=["KB-Pond3"+"S-1-B"+"FRASER-DRN"+"FRASER-S"+"N_KB"+"FC-01-S"+"FC-02-S"+"FC-03-S"]
3578
3579 *%-----|-----|
3580 SAVE HYD          NHYD=["4241"], # OF PCYCLES=[ -1], ICASEsh=[ 1]

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3561 HYD_COMMENT=[ "Total Flows at Ken-Burnett Outlet" ]
3562 *%-----|-----|
3563 *# Hydrograph from Node Ken-Burnett to station 3633
3564 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4241
3565 *#
3566 ROUTE CHANNEL NHYDout=[ "4241- out "], NHYDin=[ "4241" ], RDT=[ 1]( min),
3567 CHLGTH=[ 294]( m), CHSLOPE=[ 0.1088]( %), FPSLOPE=[ 0.1088]( %),
3568 SECNUM=[ 1.0], NSEG=[ 3]
3569 ( SEGROUGH, SEGDI ST ( m))=[ 0.05, -20.12
3570 -0.035, 45.26
3571 0.05, 403.84] NSEG times
3572 ( DI STANCE ( m), ELEVATI ON ( m))=[ ]
3573 [-909.72, 95 ]
3574 [-907.09, 94.5 ]
3575 [-904.65, 94 ]
3576 [-902.26, 93.5 ]
3577 [-44.51, 91.5 ]
3578 [-25.1, 91.5 ]
3579 [-20.98, 91 ]
3580 [-20.61, 90.5 ]
3581 [-20.12, 90 ]
3582 [-6.13, 87.26 ]
3583 [17.51, 86.56 ]
3584 [31.37, 87.2 ]
3585 [45.26, 90 ]
3586 [50.41, 90.5 ]
3587 [63.06, 91 ]
3588 [134.5, 91.5 ]
3589 [190.63, 92 ]
3590 [251.98, 92.5 ]
3591 [321.32, 93.5 ]
3592 [403.84, 95 ]
3593 *%-----|-----|
3594 ADD HYD NHYDsum=[ "SN_KB" ], NHYDs to
3595 add=[ "4241- out "+"FC-04- S"+"JR-01- S"+"JR-02- S" ]
3596 *%-----|-----|
3597 SAVE HYD NHYD=[ "SN_KB" ], # OF PCYCLES=[ -1], I CASEs h=[ 1]
3598 HYD_COMMENT=[ "Total Flows before Station 3633" ]
3599 *%-----|-----|
3600 *# Hydrograph from Station 3633 to Node Todd
3601 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 3633
3602 *# JFSA 2021-02-26 change the channel length (at station 3633) from 650m to 608m and
3603 *# change the slope from 0.0498% to 0.24671% That is because of adding station 4241
3604 *# between station 4534 and station 3633
3605 *#
3606 ROUTE CHANNEL NHYDout=[ "N_TO" ], NHYDin=[ "SN_KB" ], RDT=[ 1]( min),
3607 CHLGTH=[ 608]( m), CHSLOPE=[ 0.24671]( %), FPSLOPE=[ 0.24671]( %),
3608 SECNUM=[ 1.0], NSEG=[ 3]
3609 ( SEGROUGH, SEGDI ST ( m))=[ 0.05, -23.74
3610 -0.035, 23.74
3611 0.05, 26.50] NSEG times
3612 ( DI STANCE ( m), ELEVATI ON ( m))=[ ]
3613 [-29.24, 91.0
3614 -27.41, 90.5
3615 -25.64, 90
3616 -23.74, 89.5
3617 -22, 89.26
3618 -20, 88.51
3619 -19, 88.32
3620 -15, 88.1
3621 -10, 88.11
3622 -5, 88.17
3623 0, 88.27
3624 5, 88.19
3625 10, 88.06
3626 15, 88.48

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3624      16, 88.7
3625      23.74, 89.5
3626      24.68, 90
3627      25.57, 90.5
3628      26.50, 91.0
3629      *          [-29.24, 91]
3630      *          [-27.41, 90.5]
3631      *          [-25.64, 90]
3632      *          [-23.74, 89.5]
3633      *          [-22, 89.26]
3634      *          [-20, 88.51]
3635      *          [-19, 88.32]
3636      *          [-15, 88.1]
3637      *          [-10, 88.11]
3638      *          [-5, 88.17]
3639      *          [0, 88.27]
3640      *          [5, 88.19]
3641      *          [10, 88.06]
3642      *          [15, 88.48]
3643      *          [16, 88.7]
3644      *          [23.74, 89.5]
3645      *          [24.68, 90]
3646      *          [25.57, 90.5]
3647      *%-----|-----|
3648      *#*****|*****|
3649      *#      Catchment Greenbank
3650      *#      - To Greenbank Drain (south of the Jock)
3651      *#      - JFSA 2021-01-18 add Greenbank pond as per JFSA, P598(06)-15, June 2016
3652      *#      - JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GIS measurements
3653      *#*****|*****|
3654      CONTINUOUS STANDHYD NHYD=["Greenbank"], DT=[1] min, AREA=[36.6](ha),
3655      XI MP=[0.639], TI MP=[0.682], DWF=[0](cms), LOSS=[2],
3656      SCS curve number CN=[77],
3657      Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
3658      LGP=[40](m), MNP=[0.25], SCP=[0](min),
3659      Impervious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
3660      LGI=[493.96](m), MNI=[0.013], SCI=[0](min),
3661      Continuous simulation parameters:
3662      I a REC per=[4](hrs), I a REC i mp=[4](hrs),
3663      SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3664      I n t e r E v e n t T i m e=[18](hrs), E N D=-1
3665      *%-----|-----|
3666      ROUTE RESERVOIR NHYDout=["GreenB_MN"], NHYDin=["Greenbank"],
3667      RDT=[1](min),
3668      TABLE of ( OUTFLOW STORAGE ) values
3669      ( cms ) - ( ha - m )
3670      [ 0.0 , 0.0 ]
3671      [ 0.033 , 0.084 ]
3672      [ 0.039 , 0.201 ]
3673      [ 0.113 , 0.292 ]
3674      [ 0.237 , 0.386 ]
3675      [ 0.382 , 0.484 ]
3676      [ 0.539 , 0.585 ]
3677      [ 0.7 , 0.692 ]
3678      [ 0.86 , 0.804 ]
3679      [ 4.684 , 0.922 ]
3680      [ 11.539 , 1.052 ]
3681      [ 20.867 , 1.168 ]
3682      [ 103.616 , 1.974 ]
3683      [ -1 , -1 ] (max twenty pts)
3684      NHYDovf=["GreenB_M"],
3685      *%-----|-----|
3686      *%-----|-----|
3687      ADD HYD NHYDsum=["GreenB"], NHYDs to add=["N_TO"+"GreenB_M"+"GreenB_MN"]
3688      *%-----|-----|
3689      SAVE HYD NHYD=["GreenB"], # OF PCYCLES=[-1], I CASES h=[1]

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3690 HYD_COMMENT=["Total Flows at Greenbank Drain"]
3691 *%-----|-----|
3692 *#*****|
3693 *# Catchment TODD
3694 *# - To Todd Drain (south of the Jock)
3695 *# - Subdivision with 43% imp. as per Barrhaven South M&S
3696 *# - 2020-11-30 increase imp. based on P598(04)-11
3697 *# - 2020-11-30 update TODD Tributary Drainage Area to = 146.015 ha based on
P598(04)-11
3698 *# - 2020-11-30 split TODD Drainage Area to MAJOR, MINOR, POND and ALL
3699 *#*****|
3700 *# - JFSA 2021-01-19 add "TODD_MN1" as part of Clarke("W_CLAR_M") and remove it
from Todd
3701 *CONTINUOUS STANDHYD NHYD=["TODD_MN1"], DT=[1] min, AREA=[1.772](ha),
3702 * XI MP=[0.53], TI MP=[0.57], DWF=[0](cms), LOSS=[2],
3703 * SCS curve number CN=[77],
3704 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3705 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3706 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3707 * LGI=[108.689](m), MNI=[0.013], SCI=[0](min),
3708 * Continuous simulation parameters:
3709 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
3710 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3711 * InterEventTime=[18](hrs), END=-1
3712 *%-----|-----|
3713 CONTINUOUS STANDHYD NHYD=["TODD_MN2"], DT=[1] min, AREA=[2.1](ha),
3714 * XI MP=[0.53], TI MP=[0.57], DWF=[0](cms), LOSS=[2],
3715 * SCS curve number CN=[77],
3716 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3717 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3718 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3719 * LGI=[118.322](m), MNI=[0.013], SCI=[0](min),
3720 * Continuous simulation parameters:
3721 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
3722 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3723 * InterEventTime=[18](hrs), END=-1
3724 *%-----|-----|
3725 CONTINUOUS STANDHYD NHYD=["TODD_MN3"], DT=[1] min, AREA=[0.117](ha),
3726 * XI MP=[0.53], TI MP=[0.57], DWF=[0](cms), LOSS=[2],
3727 * SCS curve number CN=[77],
3728 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3729 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3730 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3731 * LGI=[27.928](m), MNI=[0.013], SCI=[0](min),
3732 * Continuous simulation parameters:
3733 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
3734 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3735 * InterEventTime=[18](hrs), END=-1
3736 *%-----|-----|
3737 CONTINUOUS STANDHYD NHYD=["TODD_M"], DT=[1] min, AREA=[30.230](ha),
3738 * XI MP=[0.52], TI MP=[0.64], DWF=[0](cms), LOSS=[2],
3739 * SCS curve number CN=[77],
3740 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3741 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3742 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3743 * LGI=[448.925](m), MNI=[0.013], SCI=[0](min),
3744 * Continuous simulation parameters:
3745 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
3746 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3747 * InterEventTime=[18](hrs), END=-1
3748 *%-----|-----|
3749 * -JFSA, 2021-01-19 update "TODD_ALL" area from 108.741 ha to 112.908 ha based on
GIS measurements (148.41-30.23-0.117-2.1-3.055=112.908 ha)
3750 CONTINUOUS STANDHYD NHYD=["TODD_ALL"], DT=[1] min, AREA=[112.908](ha),
3751 * XI MP=[0.52], TI MP=[0.57], DWF=[0](cms), LOSS=[2],
3752 * SCS curve number CN=[77],

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3753          Pervious surfaces: I A per=[ 4. 67] (mm), SLPP=[ 1] (%),
3754                    LGP=[ 40] (m), MNP=[ 0. 25], SCP=[ 0] (mi n),
3755          Impervious surfaces: I A i mp=[ 1. 57] (mm), SLPI=[ 1] (%),
3756                    LGI=[ 867. 594] (m), MNI=[ 0. 013], SCI=[ 0] (mi n),
3757          Continuous simulation parameters:
3758          I a REC per=[ 4] (hrs), I a REC i mp=[ 4] (hrs),
3759          SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
3760          Inter Event Ti me=[ 18] (hrs), END=- 1
3761          *%-----|-----|
3762          CONTINUOUS STANDHYD NHYD=[ "TODD_P" ], DT=[ 1] mi n, AREA=[ 3. 055] (ha),
3763          XI MP=[ 0. 63], TI MP=[ 0. 63], DWF=[ 0] (cms), LOSS=[ 2],
3764          SCS curve number CN=[ 77],
3765          Pervious surfaces: I A per=[ 4. 67] (mm), SLPP=[ 1] (%),
3766                    LGP=[ 40] (m), MNP=[ 0. 25], SCP=[ 0] (mi n),
3767          Impervious surfaces: I A i mp=[ 1. 57] (mm), SLPI=[ 1] (%),
3768                    LGI=[ 142. 712] (m), MNI=[ 0. 013], SCI=[ 0] (mi n),
3769          Continuous simulation parameters:
3770          I a REC per=[ 4] (hrs), I a REC i mp=[ 4] (hrs),
3771          SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
3772          Inter Event Ti me=[ 18] (hrs), END=- 1
3773          *%-----|-----|
3774          *%-----|-----|
3775          * -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
          drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"
          and its parameters remain the same.
3776          *CONTINUOUS STANDHYD NHYD=[ "TODD_DEVL" ], DT=[ 1] mi n, AREA=[ 15. 87] (ha),
3777          *          XI MP=[ 0. 63], TI MP=[ 0. 63], DWF=[ 0] (cms), LOSS=[ 2],
3778          *          SCS curve number CN=[ 77],
3779          *          Pervious surfaces: I A per=[ 4. 67] (mm), SLPP=[ 1] (%),
3780          *                    LGP=[ 40] (m), MNP=[ 0. 25], SCP=[ 0] (mi n),
3781          *          Impervious surfaces: I A i mp=[ 1. 57] (mm), SLPI=[ 1] (%),
3782          *                    LGI=[ 325. 27] (m), MNI=[ 0. 013], SCI=[ 0] (mi n),
3783          *          Continuous simulation parameters:
3784          *          I a REC per=[ 4] (hrs), I a REC i mp=[ 4] (hrs),
3785          *          SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
3786          *          Inter Event Ti me=[ 18] (hrs), END=- 1
3787          *%-----|-----|
3788          * -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
          is called "corr2" and its parameters remain the same.
3789          *CONTINUOUS NASHYD NHYD=[ "TODD_UnD" ], DT=[ 1] mi n, AREA=[ 12. 47] (ha),
3790          *          DWF=[ 0] (cms), CN C=[ 77], I A=[ 4. 67] (mm),
3791          *          N=[ 3], TP=[ 1. 10] hrs,
3792          *          Continuous simulation parameters:
3793          *          I a REC per=[ 4] (hrs),
3794          *          SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
3795          *          Inter Event Ti me=[ 12] (hrs)
3796          *          Baseflow simulation parameters:
3797          *          BaseFlowOption=[ 1] ,
3798          *          I n i t GWRes Vol =[ 50] (mm), GWRes K=[ 0. 96] (mm/ day/ mm)
3799          *          VHydCond=[ 0. 055] (mm/ hr), END=- 1
3800          *%-----|-----|
3801          *# 5- Year + 12% Capture
3802          *COMPUTE DUALHYD NHYD i n=[ "TODD_M" ], CI NLET=[ 3. 314] (cms), NI NLET=[ 1],
3803          *          M i j NHYD=[ "TODD_M j " ]
3804          *          M nNHYD=[ "TODD_M n" ]
3805          *          TM I STO=[ 0. 1] (cu- m)
3806          ROUTE RESERVOIR NHYDout =[ "TODD_M n" ], NHYD i n=[ "TODD_M" ] ,
3807          RDT=[ 1] (mi n),
3808          TABLE of ( OUTFLOW STORAGE ) values
3809          ( cms ) - ( ha- m)
3810          [ 0. 0 , 0. 0 ]
3811          [ 3. 314 , 0. 0001 ]
3812          [ - 1 , - 1 ] (max twenty pts)
3813          NHYDovf=[ "TODD_M j " ] ,
3814          *%-----|-----|
3815          *# 5- Year + 12% Capture

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3816 *COMPUTE DUALHYD      NHYDi n=[ " TODD_MN1" ], CI NLET=[ 0. 227 ]( c ms ) , NI NLET=[ 1 ] ,
3817 *                      Mij NHYD=[ " TODD_MN1j " ]
3818 *                      MnnNHYD=[ " TODD_MN1n " ]
3819 *                      TMi STO=[ 0. 1 ]( c u - m )
3820 *ROUTE RESERVOIR     NHYDout =[ " TODD_MN1n " ] , NHYDi n=[ " TODD_MN1 " ] ,
3821 *                      RDT=[ 1 ]( m i n ) ,
3822 *                      TABLE of ( OUTFLOW STORAGE ) values
3823 *                      ( c ms ) - ( ha - m )
3824 *                      [ 0. 0 , 0. 0 ]
3825 *                      [ 0. 227 , 0. 0001 ]
3826 *                      [ -1 , -1 ] (max twenty pts)
3827 *                      NHYDovf=[ " TODD_MN1j " ] ,
3828 *%-----|-----|
3829 *COMPUTE DUALHYD      NHYDi n=[ " TODD_MN2" ], CI NLET=[ 0. 268 ]( c ms ) , NI NLET=[ 1 ] ,
3830 *                      Mij NHYD=[ " TODD_MN2j " ]
3831 *                      MnnNHYD=[ " TODD_MN2n " ]
3832 *                      TMi STO=[ 0. 1 ]( c u - m )
3833 ROUTE RESERVOIR     NHYDout =[ " TODD_MN2n " ] , NHYDi n=[ " TODD_MN2 " ] ,
3834 *                      RDT=[ 1 ]( m i n ) ,
3835 *                      TABLE of ( OUTFLOW STORAGE ) values
3836 *                      ( c ms ) - ( ha - m )
3837 *                      [ 0. 0 , 0. 0 ]
3838 *                      [ 0. 268 , 0. 0001 ]
3839 *                      [ -1 , -1 ] (max twenty pts)
3840 *                      NHYDovf=[ " TODD_MN2j " ] ,
3841 *%-----|-----|
3842 *COMPUTE DUALHYD      NHYDi n=[ " TODD_MN3" ], CI NLET=[ 0. 016 ]( c ms ) , NI NLET=[ 1 ] ,
3843 *                      Mij NHYD=[ " TODD_MN3j " ]
3844 *                      MnnNHYD=[ " TODD_MN3n " ]
3845 *                      TMi STO=[ 0. 1 ]( c u - m )
3846 ROUTE RESERVOIR     NHYDout =[ " TODD_MN3n " ] , NHYDi n=[ " TODD_MN3 " ] ,
3847 *                      RDT=[ 1 ]( m i n ) ,
3848 *                      TABLE of ( OUTFLOW STORAGE ) values
3849 *                      ( c ms ) - ( ha - m )
3850 *                      [ 0. 0 , 0. 0 ]
3851 *                      [ 0. 016 , 0. 0001 ]
3852 *                      [ -1 , -1 ] (max twenty pts)
3853 *                      NHYDovf=[ " TODD_MN3j " ] ,
3854 *%-----|-----|
3855 * -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
major system from A2 can be added to Todd
3856 CONTINUOUS STANDHYD NHYD=[ " A2 " ], DT=[ 1 ] m i n , AREA=[ 25. 5 ]( ha ) ,
3857 *                      XI MP=[ 0. 42 ] , TI MP=[ 0. 52 ] , DWF=[ 0 ]( c ms ) , LOSS=[ 2 ] ,
3858 *                      SCS curve number CN=[ 75 ] ,
3859 *                      Pervious surfaces: I A per=[ 4. 67 ]( mm ) , SLPP=[ 1 ]( % ) ,
3860 *                      LGP=[ 40 ]( m ) , MNP=[ 0. 25 ] , SCP=[ 0 ]( m i n ) ,
3861 *                      Impervious surfaces: I A i mp=[ 1. 57 ]( mm ) , SLPI=[ 1 ]( % ) ,
3862 *                      LGI=[ 566 ]( m ) , MNI=[ 0. 013 ] , SCI=[ 0 ]( m i n ) ,
3863 *                      Continuous simulation parameters:
3864 *                      I a REC per=[ 4 ]( hr s ) , I a REC i mp=[ 4 ]( hr s ) ,
3865 *                      SM N=[ - 1 ]( mm ) , SMAX=[ - 1 ]( mm ) , SK=[ 0. 010 ] / ( mm ) ,
3866 *                      Inter Event Ti me=[ 18 ]( hr s ) , END=- 1
3867 *%-----|-----|
3868 COMPUTE DUALHYD      NHYDi n=[ " A2 " ], CI NLET=[ 1. 818 ]( c ms ) , NI NLET=[ 1 ] ,
3869 *                      Mij NHYD=[ " A2 - M " ]
3870 *                      MnnNHYD=[ " A2 - MN " ]
3871 *                      TMi STO=[ 924 ]( c u - m )
3872 *%-----|-----|
3873 ADD HYD              NHYDs um=[ " TODD " ] , NHYDs t o
add=[ " TODD_MN2n " + " TODD_MN3n " + " TODD_Mij " + " TODD_P " + " TODD_ALL " + " Wi CLAR_Min " ]
3874 *%-----|-----|
3875 SAVE HYD             NHYD=[ " TODD " ] , # OF PCYCLES=[ - 1 ] , I CASEs h=[ 1 ]
3876 *                      HYD_COMMENT=[ " Total Flows at Todd Drain " ]
3877 *%-----|-----|
3878 *#*****
3879 *# Todd Pond 3

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3880  *# - Rating curve obtained from Barrhaven South M&S modeling
3881  *# - stantec 2007, Tributary Drainage Area to M&S Pond 3 = 193 ha
3882  *#*****
3883  ROUTE RESERVOIR      NHYDout=["MS_P3"],  NHYDIn=["TODD"],
3884                      RDT=[1](min),
3885                      TABLE of ( OUTFLOW STORAGE ) values
3886                      (cms) - (ha-m)
3887                      [ 0.0 , 0.0 ]
3888                      [ 0.014 , 0.155 ]
3889                      [ 0.048 , 0.394 ]
3890                      [ 0.061 , 0.56 ]
3891                      [ 0.08 , 0.909 ]
3892                      [ 0.088 , 1.089 ]
3893                      [ 0.109 , 1.652 ]
3894                      [ 0.118 , 1.952 ]
3895                      [ 0.122 , 2.099 ]
3896                      [ 1.972 , 2.269 ]
3897                      [ 9.135 , 2.598 ]
3898                      [ 15.608 , 2.826 ]
3899                      [ 19.256 , 2.942 ]
3900                      [ 27.282 , 3.181 ]
3901                      [ 40.957 , 3.55 ]
3902                      [ 56.372 , 3.929 ]
3903                      [ 73.349 , 4.317 ]
3904                      [ 85.469 , 4.579 ]
3905                      [ 104.771 , 4.977 ]
3906                      [ -1 , -1 ] (max twenty pts)
3907                      NHYDovf=["P3-OVF"]
3908  *%-----|-----|
3909  ADD HYD              NHYDsum=["SN_TO"], NHYDs to
add=["GreenB"+"MS_P3"+"P3-OVF"+"TODD_MN2j"+"A2-M"]
3910  *%-----|-----|
3911  SAVE HYD            NHYD=["SN_TO"], # OF PCYCLES=[-1], ICASEsh=[1]
3912                      HYD_COMMENT=["Total Flows at Todd Drain"]
3913  *%-----|-----|
3914  *#
3915  *# Hydrograph from Todd Drain routed to Corrigan Drain
3916  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
3917  *# 2021-02-19 Change the slope from 0.033 % (as per Stantec Report 2007) to 0.05 % so
the model will be more stable and give reasonable results. It is justifiable as ROUTE
CHANNELS aren't well suited to really flat slopes.
3918  *
3919  ROUTE CHANNEL      NHYDout=["N_TO"], NHYDIn=["SN_TO"],
3920                      RDT=[1](min),
3921                      CHLGTH=[280](m),  CHSLOPE=[0.05](%),
3922                      FPSLOPE=[0.05](%),
3923                      SECNUM=[1.0],  NSEG=[3]
3924                      ( SEGROUGH, SEGDIST (m) )=
3925                      [ 0.075, -17.72
3926                      -0.045, 17.72
3927                      0.075, 80.62] NSEG times
3928                      ( DISTANCE (m), ELEVATION (m) )=
3929                      [-83.32, 90.00]
3930                      [-81.36, 89.50]
3931                      [-79.12, 89.00]
3932                      [-76.13, 88.50]
3933                      [-20.46, 88.00]
3934                      [-19.36, 87.50]
3935                      [-18.51, 87.00]
3936                      [-17.72, 86.50]
3937                      [-11.95, 85.24]
3938                      [-0.11, 85.12]
3939                      [11.49, 85.20]
3940                      [17.72, 86.50]
3941                      [19.74, 87.00]
3942                      [21.22, 87.50]

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3943 [ 22. 68, 88. 00]
3944 [ 24. 28, 88. 50]
3945 [ 26. 79, 89. 00]
3946 [ 71. 98, 90. 00]
3947 [ 80. 62, 90. 50]
3948 *%-----|-----|
3949 SAVE HYD NHYD=[ "N_TO" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1]
3950 HYD_COMMENT=[ "Total inflows at Station 2462" ]
3951 *%-----|-----|
3952 *#*****|*****|
3953 *# Catchment CORRIG
3954 *# - To Corrigan Drain (south of the Jock)
3955 *# - Primarily Developed (medium density)
3956 *# - JFSA JAN 2021, add Corrigan subcatchments as per IBI, July 2008
3957 *#*****|*****|
3958 *ROUTE RESERVOIR NHYDout=[ "MS_P1" ], NHYDin=[ "CORRIG" ],
3959 * RDT=[ 1 ] (mi n),
3960 * TABLE of ( OUTFLOW STORAGE ) values
3961 * ( cms ) - ( ha- m)
3962 * [ 0. 0 , 0. 0 ]
3963 * [ 0. 06 , 0. 58]
3964 * [ - 1 , - 1 ] (max twenty pts)
3965 * NHYDovf=[ "P1- OVF" ]
3966 *%-----|-----|
3967 *ADD HYD NHYDs um=[ "SN_CO" ], NHYDs to add=[ "N_TO" + "P1- OVF" + "MS_P1" ]
3968 *%-----|-----|
3969 *SAVE HYD NHYD=[ "SN_CO" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1]
3970 * HYD_COMMENT=[ "Total Flows at Corrigan Drain" ]
3971 *%-----|-----|
3972 * -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"
and its parameters remain the same.
3973 CONTINUOUS STANDHYD NHYD=[ "corr1" ], DT=[ 1 ] mi n, AREA=[ 15. 87 ] (ha),
3974 XI MP=[ 0. 63 ], TI MP=[ 0. 63 ], DWF=[ 0 ] (cms), LOSS=[ 2 ],
3975 SCS curve number CN=[ 77 ],
3976 Pervious surfaces: I A per=[ 4. 67 ] (mm), SLPP=[ 1 ] ( %),
3977 LGP=[ 40 ] (m), MNP=[ 0. 25 ], SCP=[ 0 ] (mi n),
3978 Impervious surfaces: I A i mp=[ 1. 57 ] (mm), SLPI=[ 1 ] ( %),
3979 LGI=[ 325. 27 ] (m), MNI=[ 0. 013 ], SCI=[ 0 ] (mi n),
3980 Continuous simulation parameters:
3981 I a REC per=[ 4 ] (hrs), I a REC i mp=[ 4 ] (hrs),
3982 SM N=[ - 1 ] (mm), SMAX=[ - 1 ] (mm), SK=[ 0. 010 ] / (mm),
3983 Inter Event Ti me=[ 18 ] (hrs), END=- 1
3984 *%-----|-----|
3985 * -JFSA 2021-02-23 add DUALHYD for "corr1". "corr1" DUALHYD Parameters are the
same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to "corr1".
3986 * At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for
Al-Corrig
3987 COMPUTE DUALHYD NHYDin=[ "corr1" ], CI NLET=[ 1. 818 ] (cms), NI NLET=[ 1 ],
3988 M a j NHYD=[ "corr1- M" ]
3989 M n NHYD=[ "corr1- MN" ]
3990 TM STO=[ 924 ] (cu- m)
3991 *%-----|-----|
3992 * -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
is called "corr2" and its parameters remain the same.
3993 CONTINUOUS NASHYD NHYD=[ "corr2" ], DT=[ 1 ] mi n, AREA=[ 12. 47 ] (ha),
3994 DWF=[ 0 ] (cms), CN C=[ 77 ], I A=[ 4. 67 ] (mm),
3995 N=[ 3 ], TP=[ 1. 10 ] hrs,
3996 Continuous simulation parameters:
3997 I a REC per=[ 4 ] (hrs),
3998 SM N=[ - 1 ] (mm), SMAX=[ - 1 ] (mm), SK=[ 0. 010 ] / (mm),
3999 Inter Event Ti me=[ 12 ] (hrs)
4000 Baseflow simulation parameters:
4001 BaseFl owOpt ion=[ 1 ],
4002 I ni t GWR es Vol=[ 50 ] (mm), GWR es K=[ 0. 96 ] (mm/ day/ mm)
4003 VHydCond=[ 0. 055 ] (mm/ hr), END=- 1

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4004 *%-----|-----|
4005 * -JFSA 2021-01-19 change Al-Corrig to be developed as per geottawa website and
apply the parameters of A2, the nearest sub-catchment to Al-Corrig, LGI is calculated
based on Al-Corrig area
4006 * -JFSA 2021-01-19 update all Corrigan areas based on GIS measurements, and keep
LGI as it is from Corrigan Report, IBI Group, 2008 because LGI calculated is less than
LGI from the Corrigan Report
4007 CONTINUOUS STANDHYD NHYD=["Al-Corrig"], DT=[1] min, AREA=[15.75](ha),
4008 XI MP=[0.42], TI MP=[0.52], DWF=[0](cms), LOSS=[2],
4009 SCS curve number CN=[75],
4010 Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4011 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4012 Impervious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
4013 LGI=[324.037](m), MNI=[0.013], SCI=[0](min),
4014 Continuous simulation parameters:
4015 I a REC per=[4](hrs), I a REC i mp=[4](hrs),
4016 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4017 Inter Event Ti me=[18](hrs), END=-1
4018 *
4019 * -JFSA 2021-01-25 add DUALHYD for Al-Corrig. Al-Corrig DUALHYD Parameters are the
same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to Al-Corrig.
4020 * At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for
Al-Corrig
4021 COMPUTE DUALHYD NHYD i n=["Al-Corrig"], CI NLET=[1.818](cms), NI NLET=[1],
4022 M a j NHYD=["Al-M"]
4023 M n NHYD=["Al-MN"]
4024 TM STO=[924](cu-m)
4025 *%-----|-----|
4026 *CONTINUOUS NASHYD NHYD=["Al-Corrig"], DT=[1] min, AREA=[15.75](ha),
4027 * DWF=[0](cms), CN/ C=[66], I A=[2.5](mm),
4028 * N=[3.0], TP=[0.36] hrs,
4029 * Continuous simulation parameters:
4030 * I a REC per=[4](hrs),
4031 * SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4032 * Inter Event Ti me=[12](hrs)
4033 * Baseflow simulation parameters:
4034 * BaseFl owOpt ion=[1],
4035 * I ni t GWRes Vol =[50](mm), GWRes K=[0.96](mm/day/mm)
4036 * VHydCond=[0.055](mm/hr), END=-1
4037 *%-----|-----|
4038 CONTINUOUS NASHYD NHYD=["B1"], DT=[1] min, AREA=[2.77](ha),
4039 DWF=[0](cms), CN/ C=[56], I A=[2.5](mm),
4040 N=[3.0], TP=[0.23] hrs,
4041 Continuous simulation parameters:
4042 I a REC per=[4](hrs),
4043 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4044 Inter Event Ti me=[12](hrs)
4045 Baseflow simulation parameters:
4046 BaseFl owOpt ion=[1],
4047 I ni t GWRes Vol =[50](mm), GWRes K=[0.96](mm/day/mm)
4048 VHydCond=[0.055](mm/hr), END=-1
4049 *%-----|-----|
4050 CONTINUOUS STANDHYD NHYD=["A4"], DT=[1] min, AREA=[1.27](ha),
4051 XI MP=[0.65], TI MP=[0.65], DWF=[0](cms), LOSS=[2],
4052 SCS curve number CN=[75],
4053 Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4054 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4055 Impervious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
4056 LGI=[253](m), MNI=[0.013], SCI=[0](min),
4057 Continuous simulation parameters:
4058 I a REC per=[4](hrs), I a REC i mp=[4](hrs),
4059 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4060 Inter Event Ti me=[18](hrs), END=-1
4061 *%-----|-----|
4062 COMPUTE DUALHYD NHYD i n=["A4"], CI NLET=[0.405](cms), NI NLET=[1],
4063 M a j NHYD=["A4-M"]

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4064 MnNHYP=[ " A4- MN" ]
4065 TMI STO=[ 68] ( cu- m)
4066 *%-----|-----|
4067 ADD HYD NHYDs um=[ " MHI 01" ], NHYDs to
add=[ " A1- M" + " A1- MN" + " corr 1- M" + " corr 1- MN" + " corr 2" + " B1" + " A4- MN" ]
4068 *%-----|-----|
4069 SAVE HYD NHYD=[ " MHI 01" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
4070 HYD_ COMMENT=[ " Tot al Fl ows at MHI 01" ]
4071 *%-----|-----|
4072 ROUTE PI PE PTYPE=[ 1] circ, NHYDout=[ " 101- 102" ], RNUMBER=[ 1. 0 ], PDI AM=[ 1050] ( mm ),
4073 PLNGTH=[ 368] ( m ), PROUGH=[ 0. 013 ], PSLOPE=[ 0. 0054] ( m/ m ),
NHYDn=[ " MHI 01" ], RDT=[ 1 ]
4074 *%-----|-----|
4075 * -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
major system from A2 can be added to Todd
4076 *CONTINUOUS STANDHYD NHYD=[ " A2" ], DT=[ 1] mi n, AREA=[ 25. 5] ( ha ),
4077 * XI MP=[ 0. 42 ], TI MP=[ 0. 52 ], DWF=[ 0] ( cms ), LOSS=[ 2 ],
4078 * SCS curve number CN=[ 75 ],
4079 * Pervious surfaces: IAper=[ 4. 67] ( mm ), SLPP=[ 1] ( % ),
4080 * LGP=[ 40] ( m ), MNP=[ 0. 25 ], SCP=[ 0] ( mi n ),
4081 * ImperVIOUS surfaces: IAi mp=[ 1. 57] ( mm ), SLPI=[ 1] ( % ),
4082 * LGI=[ 566] ( m ), MNI=[ 0. 013 ], SCI=[ 0] ( mi n ),
4083 * Continuous simulation parameters:
4084 * IaRECper=[ 4] ( hrs ), IaRECI mp=[ 4] ( hrs ),
4085 * SMN=[ - 1] ( mm ), SMAX=[ - 1] ( mm ), SK=[ 0. 010] / ( mm ),
4086 * InterEvent Time=[ 18] ( hrs ), END=- 1
4087 *%-----|-----|
4088 *COMPUTE DUALHYD NHYDn=[ " A2" ], CINLET=[ 1. 818] ( cms ), NI NLET=[ 1 ],
4089 * Mj NHYD=[ " A2- M" ]
4090 * MnNHYP=[ " A2- MN" ]
4091 * TMI STO=[ 924] ( cu- m)
4092 *%-----|-----|
4093 ADD HYD NHYDs um=[ " MHI 02" ], NHYDs to add=[ " A2- MN" + " 101- 102" ]
4094 *%-----|-----|
4095 SAVE HYD NHYD=[ " MHI 02" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
4096 HYD_ COMMENT=[ " Tot al Fl ows at MHI 02" ]
4097 *%-----|-----|
4098 CONTINUOUS STANDHYD NHYD=[ " A5" ], DT=[ 1] mi n, AREA=[ 1. 6] ( ha ),
4099 * XI MP=[ 0. 71 ], TI MP=[ 0. 71 ], DWF=[ 0] ( cms ), LOSS=[ 2 ],
4100 * SCS curve number CN=[ 75 ],
4101 * Pervious surfaces: IAper=[ 4. 67] ( mm ), SLPP=[ 1] ( % ),
4102 * LGP=[ 40] ( m ), MNP=[ 0. 25 ], SCP=[ 0] ( mi n ),
4103 * ImperVIOUS surfaces: IAi mp=[ 1. 57] ( mm ), SLPI=[ 1] ( % ),
4104 * LGI=[ 300] ( m ), MNI=[ 0. 013 ], SCI=[ 0] ( mi n ),
4105 * Continuous simulation parameters:
4106 * IaRECper=[ 4] ( hrs ), IaRECI mp=[ 4] ( hrs ),
4107 * SMN=[ - 1] ( mm ), SMAX=[ - 1] ( mm ), SK=[ 0. 010] / ( mm ),
4108 * InterEvent Time=[ 18] ( hrs ), END=- 1
4109 *%-----|-----|
4110 ADD HYD NHYDs um=[ " A5T" ], NHYDs to add=[ " A4- M" + " A5" ]
4111 *%-----|-----|
4112 COMPUTE DUALHYD NHYDn=[ " A5T" ], CINLET=[ 0. 357] ( cms ), NI NLET=[ 1 ],
4113 * Mj NHYD=[ " A5- M" ]
4114 * MnNHYP=[ " A5- MN" ]
4115 * TMI STO=[ 60] ( cu- m)
4116 *%-----|-----|
4117 * -JFSA Jan. 2021, A3 is a part of Todd so it is removed
4118 * -JFSA Jan. 2021, " A2- M" added to " Todd"
4119 *CONTINUOUS STANDHYD NHYD=[ " A3" ], DT=[ 1] mi n, AREA=[ 18. 4] ( ha ),
4120 * XI MP=[ 0. 58 ], TI MP=[ 0. 65 ], DWF=[ 0] ( cms ), LOSS=[ 2 ],
4121 * SCS curve number CN=[ 75 ],
4122 * Pervious surfaces: IAper=[ 4. 67] ( mm ), SLPP=[ 1] ( % ),
4123 * LGP=[ 40] ( m ), MNP=[ 0. 25 ], SCP=[ 0] ( mi n ),
4124 * ImperVIOUS surfaces: IAi mp=[ 1. 57] ( mm ), SLPI=[ 1] ( % ),
4125 * LGI=[ 450] ( m ), MNI=[ 0. 013 ], SCI=[ 0] ( mi n ),
4126 * Continuous simulation parameters:

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4127 * IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4128 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4129 * InterEventTime=[ 18](hrs), END=- 1
4130 *%-----|-----|
4131 *ADD HYD NHYDsum=[ "A3- A2M"], NHYDs to add=[ "A2- M"+"A3"]
4132 *%-----|-----|
4133 *COMPUTE DUALHYD NHYDin=[ "A3- A2M"], CILET=[ 2.208](cms), NILET=[ 1],
4134 * MjNHYD=[ "A3R- M"]
4135 * MnNHYD=[ "A3R- MN"]
4136 * TMSO=[ 908](cu-m)
4137 *%-----|-----|
4138 ROUTE PIPE PTYPE=[ 1]circ, NHYDout=[ "102- 103"], RNUMBER=[ 1.0], PDIAM=[ 1500](mm),
4139 PLNGTH=[ 504](m), PROUGH=[ 0.013], PSLOPE=[ 0.0028](m/m),
NHYDin=[ "MH102"], RDT=[ 1]
4140 *%-----|-----|
4141 ADD HYD NHYDsum=[ "MH103"], NHYDs to add=[ "102- 103"+"A5- MN"]
4142 *%-----|-----|
4143 SAVE HYD NHYD=[ "MH103"], # OF PCYCLES=[ -1], ICASEsh=[ 1]
4144 HYD_COMMENT=[ "Total Flows at MH103"]
4145 *%-----|-----|
4146 ROUTE PIPE PTYPE=[ 1]circ, NHYDout=[ "103- 104"], RNUMBER=[ 1.0], PDIAM=[ 1650](mm),
4147 PLNGTH=[ 438](m), PROUGH=[ 0.013], PSLOPE=[ 0.0046](m/m),
NHYDin=[ "MH103"], RDT=[ 1]
4148 *%-----|-----|
4149 CONTINUOUS STANDHYD NHYD=[ "A6"], DT=[ 1]min, AREA=[ 1.56](ha),
4150 XI MP=[ 0.71], TI MP=[ 0.71], DWF=[ 0](cms), LOSS=[ 2],
4151 SCS curve number CN=[ 75],
4152 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4153 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4154 Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4155 LGI=[ 280](m), MNI=[ 0.013], SCI=[ 0](min),
4156 Continuous simulation parameters:
4157 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4158 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4159 InterEventTime=[ 18](hrs), END=- 1
4160 *%-----|-----|
4161 ADD HYD NHYDsum=[ "A6T"], NHYDs to add=[ "A5- M"+"A6"]
4162 *%-----|-----|
4163 COMPUTE DUALHYD NHYDin=[ "A6T"], CILET=[ 0.357](cms), NILET=[ 1],
4164 MjNHYD=[ "A6- M"]
4165 MnNHYD=[ "A6- MN"]
4166 TMSO=[ 60](cu-m)
4167 *%-----|-----|
4168 * -JFSA Jan. 2021, A7-corrige is a part of Todd so it is removed
4169 *CONTINUOUS STANDHYD NHYD=[ "A7- corrige"], DT=[ 1]min, AREA=[ 11.8](ha),
4170 * XI MP=[ 0.41], TI MP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4171 * SCS curve number CN=[ 75],
4172 * Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4173 * LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4174 * Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4175 * LGI=[ 438](m), MNI=[ 0.013], SCI=[ 0](min),
4176 * Continuous simulation parameters:
4177 * IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4178 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4179 * InterEventTime=[ 18](hrs), END=- 1
4180 *%-----|-----|
4181 *ADD HYD NHYDsum=[ "A7- A3RM"], NHYDs to add=[ "A3R- M"+"A7- corrige"]
4182 *%-----|-----|
4183 *COMPUTE DUALHYD NHYDin=[ "A7- A3RM"], CILET=[ 1.003](cms), NILET=[ 1],
4184 * MjNHYD=[ "A7R- M"]
4185 * MnNHYD=[ "A7R- MN"]
4186 * TMSO=[ 496](cu-m)
4187 *%-----|-----|
4188 ADD HYD NHYDsum=[ "MH104"], NHYDs to add=[ "A6- MN"+"103- 104"+"TODD_Mn"]
4189 *%-----|-----|
4190 SAVE HYD NHYD=[ "MH104"], # OF PCYCLES=[ -1], ICASEsh=[ 1]

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4191 HYD_COMMENT=["Tot al Fl ows at MH104"]
4192 *%-----|-----|
4193 CONTINUOUS STANDHYD NHYD=[" B2"], DT=[ 1] mi n, AREA=[ 12. 31] (ha),
4194 XI MP=[ 0. 41], TI MP=[ 0. 54], DWF=[ 0] (cms), LOSS=[ 2],
4195 SCS curve number CN=[ 75],
4196 Pervious surfaces: I A per=[ 4. 67] (mm), SLPP=[ 1] (%),
4197 LGP=[ 40] (m), MNP=[ 0. 25], SCP=[ 0] (mi n),
4198 Impervious surfaces: I A i mp=[ 1. 57] (mm), SLPI =[ 1] (%),
4199 LGI =[ 417] (m), MNI =[ 0. 013], SCI =[ 0] (mi n),
4200 Continuous simulation parameters:
4201 I a REC per=[ 4] (hr s), I a REC i mp=[ 4] (hr s),
4202 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
4203 I nter Event Ti me=[ 18] (hr s), END=- 1
4204 *%-----|-----|
4205 COMPUTE DUALHYD NHYD i n=[" B2"], CI NLET=[ 1. 029] (cms), NI NLET=[ 1],
4206 M a j NHYD=[" B2- M "]
4207 M n NHYD=[" B2- MN"]
4208 TM STO=[ 508] (cu- m)
4209 *%-----|-----|
4210 ROUTE PIPE PTYPE=[ 1] circ, NHYDout=[" 315- 333"], RNUMBER=[ 1. 0], PDI AM=[ 1200] (mm),
4211 PLNGTH=[ 254] (m), PROUGH=[ 0. 013], PSLOPE=[ 0. 001] (m/ m),
NHYD i n=[" B2- MN"], RDT=[ 1]
4212 *%-----|-----|
4213 CONTINUOUS STANDHYD NHYD=[" B3"], DT=[ 1] mi n, AREA=[ 5. 59] (ha),
4214 XI MP=[ 0. 41], TI MP=[ 0. 54], DWF=[ 0] (cms), LOSS=[ 2],
4215 SCS curve number CN=[ 75],
4216 Pervious surfaces: I A per=[ 4. 67] (mm), SLPP=[ 1] (%),
4217 LGP=[ 40] (m), MNP=[ 0. 25], SCP=[ 0] (mi n),
4218 Impervious surfaces: I A i mp=[ 1. 57] (mm), SLPI =[ 1] (%),
4219 LGI =[ 345] (m), MNI =[ 0. 013], SCI =[ 0] (mi n),
4220 Continuous simulation parameters:
4221 I a REC per=[ 4] (hr s), I a REC i mp=[ 4] (hr s),
4222 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
4223 I nter Event Ti me=[ 18] (hr s), END=- 1
4224 *%-----|-----|
4225 COMPUTE DUALHYD NHYD i n=[" B3"], CI NLET=[ 0. 459] (cms), NI NLET=[ 1],
4226 M a j NHYD=[" B3- M "]
4227 M n NHYD=[" B3- MN"]
4228 TM STO=[ 227] (cu- m)
4229 *%-----|-----|
4230 ADD HYD NHYD s um=[" MH33"], NHYD s to add=[" B3- MN" + " 315- 333"]
4231 *%-----|-----|
4232 SAVE HYD NHYD=[" MH33"], # OF PCYCLES=[ - 1], I CASE s h=[ 1]
4233 HYD_COMMENT=["Tot al Fl ows at MH33"]
4234 *%-----|-----|
4235 ROUTE PIPE PTYPE=[ 1] circ, NHYDout=[" 333- 335"], RNUMBER=[ 1. 0], PDI AM=[ 1200] (mm),
4236 PLNGTH=[ 251] (m), PROUGH=[ 0. 013], PSLOPE=[ 0. 001] (m/ m),
NHYD i n=[" MH33"], RDT=[ 1]
4237 *%-----|-----|
4238 ROUTE PIPE PTYPE=[ 1] circ, NHYDout=[" 335- 338"], RNUMBER=[ 1. 0], PDI AM=[ 1200] (mm),
4239 PLNGTH=[ 185] (m), PROUGH=[ 0. 013], PSLOPE=[ 0. 001] (m/ m),
NHYD i n=[" 333- 335"], RDT=[ 1]
4240 *%-----|-----|
4241 ROUTE PIPE PTYPE=[ 1] circ, NHYDout=[" 338- 340"], RNUMBER=[ 1. 0], PDI AM=[ 1350] (mm),
4242 PLNGTH=[ 233] (m), PROUGH=[ 0. 013], PSLOPE=[ 0. 001] (m/ m),
NHYD i n=[" 335- 338"], RDT=[ 1]
4243 *%-----|-----|
4244 CONTINUOUS STANDHYD NHYD=[" B4"], DT=[ 1] mi n, AREA=[ 7. 6] (ha),
4245 XI MP=[ 0. 41], TI MP=[ 0. 54], DWF=[ 0] (cms), LOSS=[ 2],
4246 SCS curve number CN=[ 75],
4247 Pervious surfaces: I A per=[ 4. 67] (mm), SLPP=[ 1] (%),
4248 LGP=[ 40] (m), MNP=[ 0. 25], SCP=[ 0] (mi n),
4249 Impervious surfaces: I A i mp=[ 1. 57] (mm), SLPI =[ 1] (%),
4250 LGI =[ 388] (m), MNI =[ 0. 013], SCI =[ 0] (mi n),
4251 Continuous simulation parameters:
4252 I a REC per=[ 4] (hr s), I a REC i mp=[ 4] (hr s),

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4253 SM N=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
4254 I n t e r E v e n t T i m e =[ 18 ] ( h r s ) , E N D = - 1
4255 *%-----|-----|
4256 COMPUTE DUALHYD NHYD i n =[ " B4 " ] , C I N L E T =[ 0. 655 ] ( c m s ) , N I N L E T =[ 1 ] ,
4257 M a j N H Y D =[ " B4 - M " ]
4258 M n N H Y D =[ " B4 - M N " ]
4259 T M S T O =[ 323 ] ( c u - m )
4260 *%-----|-----|
4261 ADD HYD NHYD s u m =[ " M H 340 " ] , N H Y D s t o a d d =[ " 338 - 340 " + " B4 - M N " ]
4262 *%-----|-----|
4263 SAVE HYD NHYD =[ " M H 340 " ] , # O F P C Y C L E S =[ - 1 ] , I C A S E s h =[ 1 ]
4264 H Y D _ C O M M E N T =[ " T o t a l F l o w s a t M H 340 " ]
4265 *%-----|-----|
4266 ROUTE P I P E P T Y P E =[ 1 ] c i r c , N H Y D o u t =[ " 340 - 104 " ] , R N U M B E R =[ 1. 0 ] , P D I A M =[ 1650 ] ( mm ) ,
4267 P L N G T H =[ 240 ] ( m ) , P R O U G H =[ 0. 013 ] , P S L O P E =[ 0. 0015 ] ( m / m ) ,
N H Y D i n =[ " M H 340 " ] , R D T =[ 1 ]
4268 *%-----|-----|
4269 ADD HYD NHYD s u m =[ " M H 104T " ] , N H Y D s t o a d d =[ " 340 - 104 " + " M H 104 " ]
4270 *%-----|-----|
4271 ROUTE P I P E P T Y P E =[ 2 ] r e c t , N H Y D o u t =[ " 104 - 105 " ] , R N U M B E R =[ 1. 0 ] ,
P W D T H =[ 2400 ] ( mm ) b y P H E I G H T =[ 2100 ] ( mm ) ,
4272 P L N G T H =[ 380 ] ( m ) , P R O U G H =[ 0. 013 ] , P S L O P E =[ 0. 001 ] ( m / m ) ,
N H Y D i n =[ " M H 104T " ] , R D T =[ 1 ]
4273 *%-----|-----|
4274 CONTINUOUS STANDHYD NHYD =[ " B5 " ] , D T =[ 1 ] m i n , A R E A =[ 2. 2 ] ( ha ) ,
4275 X I M P =[ 0. 57 ] , T I M P =[ 0. 57 ] , D W F =[ 0 ] ( c m s ) , L O S S =[ 2 ] ,
4276 S C S c u r v e n u m b e r C N =[ 75 ] ,
4277 P e r v i o u s s u r f a c e s : I A p e r =[ 4. 67 ] ( mm ) , S L P P =[ 1 ] ( % ) ,
4278 L G P =[ 40 ] ( m ) , M N P =[ 0. 25 ] , S C P =[ 0 ] ( m i n ) ,
4279 I m p e r v i o u s s u r f a c e s : I A i m p =[ 1. 57 ] ( mm ) , S L P I =[ 1 ] ( % ) ,
4280 L G I =[ 187 ] ( m ) , M N I =[ 0. 013 ] , S C I =[ 0 ] ( m i n ) ,
4281 C o n t i n u o u s s i m u l a t i o n p a r a m e t e r s :
4282 I a R E C p e r =[ 4 ] ( h r s ) , I a R E C i m p =[ 4 ] ( h r s ) ,
4283 S M N =[ - 1 ] ( mm ) , S M A X =[ - 1 ] ( mm ) , S K =[ 0. 010 ] / ( mm ) ,
4284 I n t e r E v e n t T i m e =[ 18 ] ( h r s ) , E N D = - 1
4285 *%-----|-----|
4286 COMPUTE DUALHYD NHYD i n =[ " B5 " ] , C I N L E T =[ 0. 260 ] ( c m s ) , N I N L E T =[ 1 ] ,
4287 M a j N H Y D =[ " B5 - M " ]
4288 M n N H Y D =[ " B5 - M N " ]
4289 T M S T O =[ 250 ] ( c u - m )
4290 *%-----|-----|
4291 CONTINUOUS STANDHYD NHYD =[ " A8 " ] , D T =[ 1 ] m i n , A R E A =[ 0. 96 ] ( ha ) ,
4292 X I M P =[ 0. 71 ] , T I M P =[ 0. 71 ] , D W F =[ 0 ] ( c m s ) , L O S S =[ 2 ] ,
4293 S C S c u r v e n u m b e r C N =[ 75 ] ,
4294 P e r v i o u s s u r f a c e s : I A p e r =[ 4. 67 ] ( mm ) , S L P P =[ 1 ] ( % ) ,
4295 L G P =[ 40 ] ( m ) , M N P =[ 0. 25 ] , S C P =[ 0 ] ( m i n ) ,
4296 I m p e r v i o u s s u r f a c e s : I A i m p =[ 1. 57 ] ( mm ) , S L P I =[ 1 ] ( % ) ,
4297 L G I =[ 186 ] ( m ) , M N I =[ 0. 013 ] , S C I =[ 0 ] ( m i n ) ,
4298 C o n t i n u o u s s i m u l a t i o n p a r a m e t e r s :
4299 I a R E C p e r =[ 4 ] ( h r s ) , I a R E C i m p =[ 4 ] ( h r s ) ,
4300 S M N =[ - 1 ] ( mm ) , S M A X =[ - 1 ] ( mm ) , S K =[ 0. 010 ] / ( mm ) ,
4301 I n t e r E v e n t T i m e =[ 18 ] ( h r s ) , E N D = - 1
4302 *%-----|-----|
4303 ADD HYD NHYD s u m =[ " A8T " ] , N H Y D s t o a d d =[ " A6 - M " + " A8 " ]
4304 *%-----|-----|
4305 COMPUTE DUALHYD NHYD i n =[ " A8T " ] , C I N L E T =[ 0. 238 ] ( c m s ) , N I N L E T =[ 1 ] ,
4306 M a j N H Y D =[ " A8 - M " ]
4307 M n N H Y D =[ " A8 - M N " ]
4308 T M S T O =[ 40 ] ( c u - m )
4309 *%-----|-----|
4310 ADD HYD NHYD s u m =[ " M H 105 " ] , N H Y D s t o
a d d =[ " 104 - 105 " + " B5 - M N " + " A8 - M N " + " T O D D _ M N 3 j " ]
4311 *%-----|-----|
4312 SAVE HYD NHYD =[ " M H 105 " ] , # O F P C Y C L E S =[ - 1 ] , I C A S E s h =[ 1 ]
4313 H Y D _ C O M M E N T =[ " T o t a l F l o w s a t M H 105 " ]

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4314 *%-----|
4315 DI VERT HYD      NHYDin=["A8-M"] NIDout=[2]max five,
4316                  outflow hydrographs (NHYDs)=["A8-M-JR" "A8-M-B6"]
4317                  flow distribution table: (modify as necessary)
4318                  Note: all flows are in (cms)
4319                  QIDi + QIDi = QTOTAL
4320                  [ 0 + 0 = 0 ]
4321                  [ 50 + 50 = 100 ] end
4322 *%-----|
4323 DI VERT HYD      NHYDin=["MHI05"] NIDout=[2]max five,
4324                  outflow hydrographs (NHYDs)=["MHI05-JR" "MHI05-B6"]
4325                  flow distribution table: (modify as necessary)
4326                  Note: all flows are in (cms)
4327                  QIDi + QIDi = QTOTAL
4328                  [ 0 + 0 = 0 ]
4329                  [ 0 + 3.0 = 3.0 ]
4330                  [ 96.9+ 3.1 = 100 ] end
4331 *%-----|
4332 CONTINUOUS STANDHYD NHYD=["B7"], DT=[1]min, AREA=[7.19](ha),
4333                  XI MP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4334                  SCS curve number CN=[75],
4335                  Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4336                  LGP=[40](m), MNP=[0.25], SCP=[0](min),
4337                  Impervious surfaces: I A imp=[1.57](mm), SLPI=[1](%),
4338                  LGI=[211](m), MNI=[0.013], SCI=[0](min),
4339                  Continuous simulation parameters:
4340                  I a REC per=[4](hrs), I a REC imp=[4](hrs),
4341                  SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4342                  Inter Event Time=[18](hrs), END=-1
4343 *%-----|
4344 ADD HYD          NHYDs um=["B7-B4M"], NHYDs to add=["B4-M"+"B7"]
4345 *%-----|
4346 COMPUTE DUALHYD NHYDin=["B7-B4M"], CINLET=[0.629](cms), NINLET=[1],
4347                  Maj NHYD=["B7R-M"]
4348                  MinNHYD=["B7R-MN"]
4349                  TMS TO=[311](cu-m)
4350 *%-----|
4351 ROUTE PIPE      PTYPE=[1]circ, NHYDout=["360-106A"], RNUMBER=[1.0], PDI AM=[1050](mm),
4352                  PLNGTH=[167](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
4353                  NHYDin=["B7R-MN"], RDT=[1]
4354 *%-----|
4355 * -JFSA 2021-01-19 change B6 to be developed as per geottawa website and apply the
4356 parameters of A7, the nearest sub-catchment to B6, LGI is calculated based on B6 area
4357 CONTINUOUS STANDHYD NHYD=["B6"], DT=[1]min, AREA=[3.29](ha),
4358                  XI MP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4359                  SCS curve number CN=[75],
4360                  Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4361                  LGP=[40](m), MNP=[0.25], SCP=[0](min),
4362                  Impervious surfaces: I A imp=[1.57](mm), SLPI=[1](%),
4363                  LGI=[148.099](m), MNI=[0.013], SCI=[0](min),
4364                  Continuous simulation parameters:
4365                  I a REC per=[4](hrs), I a REC imp=[4](hrs),
4366                  SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4367                  Inter Event Time=[18](hrs), END=-1
4368 *%-----|
4369 * -JFSA 2021-01-25 add B1 DUALHYD as per Corrigan Report, IBI Group, 2008
4370 COMPUTE DUALHYD NHYDin=["B6"], CINLET=[0.064](cms), NINLET=[1],
4371                  Maj NHYD=["B6-M"]
4372                  MinNHYD=["B6-MN"]
4373                  TMS TO=[5484](cu-m)
4374 *%-----|
4375 *CONTINUOUS NASHYD NHYD=["B6"], DT=[1]min, AREA=[3.29](ha),
4376                  * DWF=[0](cms), CN/C=[75], IA=[2.5](mm),
4377                  * N=[3.0], TP=[0.36]hrs,

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4376 *          Continuous simulation parameters:
4377 *          IaRECper=[ 4](hrs),
4378 *          SMN=[- 1](mm),  SMAX=[- 1](mm),  SK=[ 0.010]/(mm),
4379 *          InterEventTime=[ 12](hrs)
4380 *          Baseflow simulation parameters:
4381 *          BaseFlowOption=[ 1] ,
4382 *          InitGWResVol=[ 50](mm),  GWResK=[ 0.96](mm/day/mm)
4383 *          VHydCond=[ 0.055](mm/hr),  END=- 1
4384 *%-----|-----
4385 *% -EX-LAND is external land. It is a part of JOCKVA sub-catchment as per Corrigan
Report, IBI Group, 2008
4386 CONTINUOUS STANDHYD NHYD=["EX-LAND"], DT=[ 1]min, AREA=[ 32.5](ha),
4387 XI MP=[ 0.50], TI MP=[ 0.50], DWF=[ 0](cms), LOSS=[ 2],
4388 SCS curve number CN=[ 74],
4389 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4390 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4391 Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4392 LGI=[ 465.475](m), MNI=[ 0.013], SCI=[ 0](min),
4393 Continuous simulation parameters:
4394 IaRECper=[ 4](hrs),  IaRECImp=[ 4](hrs),
4395 SMN=[- 1](mm),  SMAX=[- 1](mm),  SK=[ 0.010]/(mm),
4396 InterEventTime=[ 18](hrs),  END=- 1
4397 *%-----|-----
4398 COMPUTE DUALHYD NHYDin=["EX-LAND"], CINLET=[ 2.275](cms), NINLET=[ 1],
4399 MajNHYD=["EX-LAND-M"]
4400 MnNHYD=["EX-LAND-MN"]
4401 TMS TO=[ 1365](cu-m)
4402 *%-----|-----
4403 ADD HYD NHYDsum=["B6-B7ExM"], NHYDsto
add=["B7R-M"+"EX-LAND-M"+"B5-M"+"B6-M"+"B6-MN"+"A8-M-B6"]
4404 *%-----|-----
4405 COMPUTE DUALHYD NHYDin=["B6-B7ExM"], CINLET=[ 0.064](cms), NINLET=[ 1],
4406 MajNHYD=["B6R-M"]
4407 MnNHYD=["B6R-MN"]
4408 TMS TO=[ 5484](cu-m)
4409 *%-----|-----
4410 ROUTE PIPE PTYPE=[ 1]circ, NHYDout=["105-106A"], RNUMBER=[ 1.0], PDIAM=[ 1800](mm),
4411 PLNGTH=[ 208](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
NHYDin=["MH105-B6"], RDT=[ 1]
4412 *%-----|-----
4413 ADD HYD NHYDsum=["MH106A"], NHYDsto
add=["360-106A"+"105-106A"+"B6R-MN"+"B6R-M"]
4414 *%-----|-----
4415 SAVE HYD NHYD=["MH106A"], # OF PCYCLES=[- 1], ICASEsh=[ 1]
4416 HYD_COMMENT=["Total Flows at MH106A"]
4417 *%-----|-----
4418 *% -JFSA 2021-01-12 THE MANHOLE MH106 is called MH17/106 in Corrigan Report, IBI
Group, July 2008
4419 *%
4420 ROUTE PIPE PTYPE=[ 1]circ, NHYDout=["106A-106"], RNUMBER=[ 1.0], PDIAM=[ 1800](mm),
4421 PLNGTH=[ 190](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
NHYDin=["MH106A"], RDT=[ 1]
4422 *%-----|-----
4423 CONTINUOUS STANDHYD NHYD=["A9"], DT=[ 1]min, AREA=[ 2.44](ha),
4424 XI MP=[ 0.71], TI MP=[ 0.71], DWF=[ 0](cms), LOSS=[ 2],
4425 SCS curve number CN=[ 75],
4426 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4427 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4428 Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4429 LGI=[ 262](m), MNI=[ 0.013], SCI=[ 0](min),
4430 Continuous simulation parameters:
4431 IaRECper=[ 4](hrs),  IaRECImp=[ 4](hrs),
4432 SMN=[- 1](mm),  SMAX=[- 1](mm),  SK=[ 0.010]/(mm),
4433 InterEventTime=[ 18](hrs),  END=- 1
4434 *%-----|-----
4435 COMPUTE DUALHYD NHYDin=["A9"], CINLET=[ 0.547](cms), NINLET=[ 1],

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4436      Mj NHYD=[ " A9- M " ]
4437      MnNHYD=[ " A9- MN" ]
4438      TM STO=[ 0 ] ( cu- m)
4439  *%-----|-----|
4440  ADD HYD      NHYDs um=[ " MHI06" ], NHYDs to add=[ " 106A- 106" + " A9- MN" ]
4441  *%-----|-----|
4442  SAVE HYD     NHYD=[ " MHI06" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
4443      HYD_ COMMENT=[ " Tot al Fl ows at MHI06" ]
4444  *%-----|-----|
4445  *%      -JFSA 2021-01-12 THE MANHOLE MHI07 is called MHI18/107 in Corrigan Report, IBI
Group, July 2008
4446  *%
4447  ROUTE PIPE   PTYPER=[ 1 ] circ, NHYDout=[ " 106- 107" ], RNUMBER=[ 1. 0 ], PDI AM=[ 1800 ] ( mm),
4448      PLNGTH=[ 122. 5 ] ( m), PROUGH=[ 0. 013 ], PSLOPE=[ 0. 001 ] ( m/ m),
      NHYDin=[ " MHI06" ], RDT=[ 1 ]
4449  *%-----|-----|
4450  CONTINUOUS STANDHYD NHYD=[ " A10" ], DT=[ 1 ] mi n, AREA=[ 4. 14 ] ( ha),
4451      XI MP=[ 0. 35 ], TI MP=[ 0. 47 ], DWF=[ 0 ] ( cms), LOSS=[ 2 ],
4452      SCS curve number CN=[ 75 ],
4453      Pervious surfaces: IAper=[ 4. 67 ] ( mm), SLPP=[ 1 ] ( %),
4454      LGP=[ 40 ] ( m), MNP=[ 0. 25 ], SCP=[ 0 ] ( mi n),
4455      Impervious surfaces: IAi mp=[ 1. 57 ] ( mm), SLPI=[ 1 ] ( %),
4456      LGI=[ 183 ] ( m), MNI=[ 0. 013 ], SCI=[ 0 ] ( mi n),
4457      Continuous simulation parameters:
4458      IaRECPper=[ 4 ] ( hr s), IaRECI mp=[ 4 ] ( hr s),
4459      SMN=[ - 1 ] ( mm), SMAX=[ - 1 ] ( mm), SK=[ 0. 010 ] / ( mm),
4460      InterEvent Time=[ 18 ] ( hr s), END=- 1
4461  *%-----|-----|
4462  COMPUTE DUALHYD NHYDin=[ " A10" ], CI NLET=[ 0. 310 ] ( cms), NI NLET=[ 1 ],
4463      Mj NHYD=[ " A10- M " ]
4464      MnNHYD=[ " A10- MN" ]
4465      TM STO=[ 228 ] ( cu- m)
4466  *%-----|-----|
4467  CONTINUOUS STANDHYD NHYD=[ " A11" ], DT=[ 1 ] mi n, AREA=[ 10. 61 ] ( ha),
4468      XI MP=[ 0. 53 ], TI MP=[ 0. 62 ], DWF=[ 0 ] ( cms), LOSS=[ 2 ],
4469      SCS curve number CN=[ 75 ],
4470      Pervious surfaces: IAper=[ 4. 67 ] ( mm), SLPP=[ 1 ] ( %),
4471      LGP=[ 40 ] ( m), MNP=[ 0. 25 ], SCP=[ 0 ] ( mi n),
4472      Impervious surfaces: IAi mp=[ 1. 57 ] ( mm), SLPI=[ 1 ] ( %),
4473      LGI=[ 379 ] ( m), MNI=[ 0. 013 ], SCI=[ 0 ] ( mi n),
4474      Continuous simulation parameters:
4475      IaRECPper=[ 4 ] ( hr s), IaRECI mp=[ 4 ] ( hr s),
4476      SMN=[ - 1 ] ( mm), SMAX=[ - 1 ] ( mm), SK=[ 0. 010 ] / ( mm),
4477      InterEvent Time=[ 18 ] ( hr s), END=- 1
4478  *%-----|-----|
4479  COMPUTE DUALHYD NHYDin=[ " A11" ], CI NLET=[ 0. 993 ] ( cms), NI NLET=[ 1 ],
4480      Mj NHYD=[ " A11- M " ]
4481      MnNHYD=[ " A11- MN" ]
4482      TM STO=[ 556 ] ( cu- m)
4483  *%-----|-----|
4484  ADD HYD      NHYDs um=[ " MHI07" ], NHYDs to add=[ " 106- 107" + " A10- MN" + " A11- MN" ]
4485  *%-----|-----|
4486  SAVE HYD     NHYD=[ " MHI07" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
4487      HYD_ COMMENT=[ " Tot al Fl ows at MHI07" ]
4488  *%-----|-----|
4489  ROUTE PIPE   PTYPER=[ 1 ] circ, NHYDout=[ " 107- 119" ], RNUMBER=[ 1. 0 ], PDI AM=[ 1800 ] ( mm),
4490      PLNGTH=[ 114 ] ( m), PROUGH=[ 0. 013 ], PSLOPE=[ 0. 0012 ] ( m/ m),
      NHYDin=[ " MHI07" ], RDT=[ 1 ]
4491  *%-----|-----|
4492  *%      -JFSA 2021-01-12 THE MANHOLE MHI08 is called MHI20/108 in Corrigan Report, IBI
Group, July 2008
4493  *%
4494  ROUTE PIPE   PTYPER=[ 1 ] circ, NHYDout=[ " 119- 108" ], RNUMBER=[ 1. 0 ], PDI AM=[ 1800 ] ( mm),
4495      PLNGTH=[ 65. 8 ] ( m), PROUGH=[ 0. 013 ], PSLOPE=[ 0. 0012 ] ( m/ m),
      NHYDin=[ " 107- 119" ], RDT=[ 1 ]
4496  *%-----|-----|

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4497 CONTINUOUS STANDHYD NHYD=["A12"], DT=[1] min, AREA=[12.29] (ha),
 4498 XI MP=[0.41], TI MP=[0.54], DWF=[0] (cms), LOSS=[2],
 4499 SCS curve number CN=[75],
 4500 Pervious surfaces: I A per=[4.67] (mm), SLPP=[1] (%),
 4501 LGP=[40] (m), MNP=[0.25], SCP=[0] (min),
 4502 Impervious surfaces: I A i mp=[1.57] (mm), SLPI=[1] (%),
 4503 LGI=[183] (m), MNI=[0.013], SCI=[0] (min),
 4504 Continuous simulation parameters:
 4505 I a REC per=[4] (hrs), I a REC i mp=[4] (hrs),
 4506 SM N=[-1] (mm), SMAX=[-1] (mm), SK=[0.010] / (mm),
 4507 Inter Event Time=[18] (hrs), END=- 1
 4508 *%-----|
 4509 COMPUTE DUALHYD NHYD i n=["A12"], CI NLET=[1.029] (cms), NI NLET=[1],
 4510 M a j NHYD=["A12- M"]
 4511 M n NHYD=["A12- MN"]
 4512 TM STO=[672] (cu-m)
 4513 *%-----|
 4514 CONTINUOUS STANDHYD NHYD=["A13"], DT=[1] min, AREA=[2.59] (ha),
 4515 XI MP=[0.71], TI MP=[0.71], DWF=[0] (cms), LOSS=[2],
 4516 SCS curve number CN=[75],
 4517 Pervious surfaces: I A per=[4.67] (mm), SLPP=[1] (%),
 4518 LGP=[40] (m), MNP=[0.25], SCP=[0] (min),
 4519 Impervious surfaces: I A i mp=[1.57] (mm), SLPI=[1] (%),
 4520 LGI=[379] (m), MNI=[0.013], SCI=[0] (min),
 4521 Continuous simulation parameters:
 4522 I a REC per=[4] (hrs), I a REC i mp=[4] (hrs),
 4523 SM N=[-1] (mm), SMAX=[-1] (mm), SK=[0.010] / (mm),
 4524 Inter Event Time=[18] (hrs), END=- 1
 4525 *%-----|
 4526 COMPUTE DUALHYD NHYD i n=["A13"], CI NLET=[0.571] (cms), NI NLET=[1],
 4527 M a j NHYD=["A13- M"]
 4528 M n NHYD=["A13- MN"]
 4529 TM STO=[0] (cu-m)
 4530 *%-----|
 4531 * -JFSA 2021-01-22 add the Corrigan pond area ("Pond-Block")
 4532 CONTINUOUS STANDHYD NHYD=["Pond-Block"], DT=[1] min, AREA=[2.94] (ha),
 4533 XI MP=[0.415], TI MP=[0.415], DWF=[0] (cms), LOSS=[2],
 4534 SCS curve number CN=[75],
 4535 Pervious surfaces: I A per=[4.67] (mm), SLPP=[1] (%),
 4536 LGP=[40] (m), MNP=[0.25], SCP=[0] (min),
 4537 Impervious surfaces: I A i mp=[1.57] (mm), SLPI=[1] (%),
 4538 LGI=[183] (m), MNI=[0.013], SCI=[0] (min),
 4539 Continuous simulation parameters:
 4540 I a REC per=[4] (hrs), I a REC i mp=[4] (hrs),
 4541 SM N=[-1] (mm), SMAX=[-1] (mm), SK=[0.010] / (mm),
 4542 Inter Event Time=[18] (hrs), END=- 1
 4543 *%-----|
 4544 ADD HYD NHYD s um=["MHI08"], NHYD s to add=["119-108"+"A13-MN"+"A12-MN"]
 4545 *%-----|
 4546 SAVE HYD NHYD=["MHI08"], # OF PCYCLES=[-1], I CASE s h=[1]
 4547 HYD_COMMENT=["Total Flows at MHI08"]
 4548 *%-----|
 4549 ROUTE PIPE PTYPE=[1] circ, NHYD out=["108-116"], RNUMBER=[1.0], PDI AM=[1800] (mm),
 4550 PLNGTH=[76.6] (m), PROUGH=[0.013], PSLOPE=[0.0013] (m/m),
 NHYD i n=["MHI08"], RDT=[1]
 4551 *%-----|
 4552 ROUTE PIPE PTYPE=[1] circ, NHYD out=["116-corrigan"], RNUMBER=[1.0],
 4553 PDI AM=[1800] (mm),
 PLNGTH=[79.5] (m), PROUGH=[0.013], PSLOPE=[0.0013] (m/m),
 NHYD i n=["108-116"], RDT=[1]
 4554 *%-----|
 4555 ADD HYD NHYD s um=["Corrigan"], NHYD s to add=["116-corrigan"+"Pond-Block"]
 4556 *%-----|
 4557 SAVE HYD NHYD=["Corrigan"], # OF PCYCLES=[-1], I CASE s h=[1]
 4558 HYD_COMMENT=["Total Flows at Corrigan Pond"]
 4559 *%-----|

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4560 ROUTE RESERVOIR      NHYDout=["Co-P"],  NHYDin=["Corrigan"],
4561 RDT=[1](min),
4562          TABLE of ( OUTFLOW STORAGE ) values
4563                    (cms) - (ha-m)
4564                    [ 0.0 , 0.0 ]
4565                    [ 0.015 , 0.04118]
4566                    [ 0.030 , 0.08297]
4567                    [ 0.045 , 0.12537]
4568                    [ 0.060 , 0.16837]
4569                    [ 0.075 , 0.21199]
4570                    [ 0.090 , 0.27545]
4571                    [ 0.105 , 0.34650]
4572                    [ 0.120 , 0.42049]
4573                    [ 0.135 , 0.50188]
4574                    [ 0.186 , 0.60307]
4575                    [ 2.110 , 0.79083]
4576                    [ 5.874 , 1.00271]
4577                    [ 11.395 , 1.29643]
4578                    [ 18.770 , 1.62054]
4579                    [ 28.143 , 1.97516]
4580                    [ -1 , -1 ] (max twenty pts)
4581          NHYDovf=["Co-P-OVF"]
4582 *%-----|-----|
4583 ADD HYD          NHYDsum=["corrig"], NHYDs to
add=["Co-P-OVF"+"Co-P"+"N_TO"+"MH105-JR"+"A8-M-JR"+"A9-M-JR"+"A10-M-JR"+"A11-M-JR"+"A12-M-JR"+"A13-M-JR"]
4584 *%-----|-----|
4585 SAVE HYD        NHYD=["corrig"], # OF PCYCLES=[-1], ICASEsh=[1]
4586          HYD_COMMENT=["Total Flows at Corrigan Pond"]
4587 *%-----|-----|
4588 *#*****|*****|
4589 *#   Corrigan Pond 1
4590 *#   - Rating curve obtained from Barrhaven South M&S modeling
4591 *#   - Tributary Drainage Area to M&S Pond 1 = 145 ha
4592 *#*****|*****|
4593 *ROUTE RESERVOIR NHYDout=["MS_P1"], NHYDin=["CORRIG"],
4594 *          RDT=[1](min),
4595 *          TABLE of ( OUTFLOW STORAGE ) values
4596 *                    (cms) - (ha-m)
4597 *                    [ 0.0 , 0.0 ]
4598 *                    [ 0.06 , 0.58]
4599 *                    [ -1 , -1 ] (max twenty pts)
4600 *          NHYDovf=["P1-OVF"]
4601 *%-----|-----|
4602 *ADD HYD          NHYDsum=["SN_CO"], NHYDs to add=["N_TO"+"P1-OVF"+"MS_P1"]
4603 *%-----|-----|
4604 *SAVE HYD        NHYD=["SN_CO"], # OF PCYCLES=[-1], ICASEsh=[1]
4605 *          HYD_COMMENT=["Total Flows at Corrigan Drain"]
4606 *%-----|-----|
4607 *#
4608 *# Hydrograph from Corrigan Drain routed to Jockvale Road
4609 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
4610 *#
4611 ROUTE CHANNEL    NHYDout=["N_M"] ,NHYDin=["corrig"] ,
4612 RDT=[1](min),
4613 CHLGTH=[580](m),  CHSLOPE=[0.4448](%),
4614                    FPSLOPE=[0.4448](%),
4615 SECNUM=[1.0],    NSEG=[3]
4616 ( SEGROUGH, SEGDI ST (m))=
4617   [0.075, -17.72
4618   -0.045, 17.72
4619   0.075, 80.62] NSEG times
4620 ( DI STANCE (m), ELEVATI ON (m))=
4621 [-83.32, 90.00]
4622 [-81.36, 89.50]
4623 [-79.12, 89.00]

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4624 [- 76. 13, 88. 50]
4625 [- 20. 46, 88. 00]
4626 [- 19. 36, 87. 50]
4627 [- 18. 51, 87. 00]
4628 [- 17. 72, 86. 50]
4629 [- 11. 95, 85. 24]
4630 [- 0. 11, 85. 12]
4631 [11. 49, 85. 20]
4632 [17. 72, 86. 50]
4633 [19. 74, 87. 00]
4634 [21. 22, 87. 50]
4635 [22. 68, 88. 00]
4636 [24. 28, 88. 50]
4637 [26. 79, 89. 00]
4638 [71. 98, 90. 00]
4639 [80. 62, 90. 50]

4640 *%-----|-----|
4641 *#*****|*****|

4642 *# Catchment MLLS
4643 *# - To SWM Facility north of the Jock
4644 *# - Primarily residential development
4645 *#*****|*****|

4646 CONTINUOUS STANDHYD NHYD=["MLLS"], DT=[1] min, AREA=[175.99] (ha),
4647 XI MP=[0.38], TI MP=[0.38], DWF=[0] (cms), LOSS=[2],
4648 SCS curve number CN=[74],
4649 Pervious surfaces: I A per=[4.67] (mm), SLPP=[1] (%),
4650 LGP=[40] (m), MNP=[0.25], SCP=[0] (min),
4651 Impervious surfaces: I A i mp=[1.57] (mm), SLPI=[1] (%),
4652 LGI=[1118.123] (m), MNI=[0.013], SCI=[0] (min),
4653 Continuous simulation parameters:
4654 I a REC per=[4] (hrs), I a REC i mp=[4] (hrs),
4655 S M N=[-1] (mm), S M A X=[-1] (mm), S K=[0.010] / (mm),
4656 I n t e r E v e n t T i m e=[18] (hrs), E N D=-1

4657 *%-----|-----|
4658 *#*****|*****|

4659 *# Chapman Mills SWM Pond
4660 *# - Rating curve obtained from CCL hydraulic modeling
4661 *#*****|*****|

4662 ROUTE RESERVOIR NHYDout=["MLL_P"], NHYDin=["MLLS"],
4663 RDT=[1] (min),
4664 TABLE of (OUTFLOW STORAGE) values
4665 (cms) - (ha-m)
4666 [0.0 , 0.0]
4667 [0.01 , 0.01]
4668 [0.05 , 0.06]
4669 [0.09 , 0.11]
4670 [0.13 , 0.15]
4671 [0.18 , 0.19]
4672 [0.28 , 0.28]
4673 [0.37 , 0.34]
4674 [0.45 , 0.40]
4675 [0.51 , 0.44]
4676 [0.56 , 0.47]
4677 [0.64 , 0.52]
4678 [0.76 , 0.59]
4679 [0.86 , 0.65]
4680 [1.09 , 0.78]
4681 [1.44 , 0.96]
4682 [3.18 , 1.84]
4683 [4.05 , 2.31]
4684 [-1 , -1] (max twenty pts)
4685 NHYDovf=["ML-OV"]

4686 *%-----|-----|
4687 ADD HYD NHYDsum=["SN_M"], NHYDsto add=["N_M"+"ML-OV"+"MLL_P"]
4688 *%-----|-----|

4689 SAVE HYD NHYD=["SN_M"], # OF PCYCLES=[-1], I CASEs h=[1]

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4690 HYD_COMMENT=["Total Flows at Jockvale Road"]
4691 *%-----|-----|
4692 *#
4693 *# Hydrograph from Jockvale Road routed to Heart's Desire
4694 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 689
4695 *#
4696 ROUTE CHANNEL NHYDout=["N_DE"], NHYDin=["SN_M"],
4697 RDT=[1](min),
4698 CHLGTH=[1962](m), CHSLOPE=[0.2227](%),
4699 FPSLOPE=[0.2227](%),
4700 SECNUM=[1.0], NSEG=[3]
4701 (SEGROUGH, SEGDIST (m))=
4702 [0.075, -17.56
4703 -0.045, 18.27
4704 0.075, 32.51] NSEG times
4705 (DISTANCE (m), ELEVATION (m))=
4706 [-54.07, 85.00]
4707 [-39.43, 84.50]
4708 [-28.30, 84.00]
4709 [-24.12, 83.50]
4710 [-22.30, 83.00]
4711 [-20.55, 82.50]
4712 [-17.56, 82.00]
4713 [-12.63, 81.22]
4714 [-0.11, 80.75]
4715 [11.55, 81.22]
4716 [18.27, 82.00]
4717 [19.82, 82.50]
4718 [22.48, 83.00]
4719 [27.90, 83.50]
4720 [29.31, 84.00]
4721 [30.81, 84.50]
4722 [32.51, 85.00]
4723 *%-----|-----|
4724 *#*****|*****|
4725 *# Catchment DESIRE
4726 *# - To Jock River (north of the Jock)
4727 *# - Rural-estate subdivision (Heart's Desire Community)
4728 *#*****|*****|
4729 CONTINUOUS STANDHYD NHYD=["DESIRE"], DT=[1]min, AREA=[23.78](ha),
4730 XI MP=[0.25], TI MP=[0.25], DWF=[0](cms), LOSS=[2],
4731 SCS curve number CN=[77],
4732 Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4733 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4734 Impervious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
4735 LGI=[400](m), MNI=[0.013], SCI=[0](min),
4736 Continuous simulation parameters:
4737 I a RE C per=[4](hrs), I a RE C i mp=[4](hrs),
4738 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4739 Inter Event Time=[18](hrs), END=-1
4740 *%-----|-----|
4741 *#*****|*****|
4742 *# Catchment JOCKVA
4743 *# - To Jockvale SWM Facility
4744 *# - Residential development & golf course
4745 *# - JFSA 2021-01-11 update JOCKVA after updating CORRIG as per IBI GROUP, July 2008.
4746 *# JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two
4747 *# areas JOCKVA and EX-LAND 32.5 ha as per IBI GROUP, July 2008.
4748 *#*****|*****|
4749 CONTINUOUS STANDHYD NHYD=["JOCKVA"], DT=[1]min, AREA=[225.13](ha),
4750 XI MP=[0.50], TI MP=[0.50], DWF=[0](cms), LOSS=[2],
4751 SCS curve number CN=[74],
4752 Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4753 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4754 Impervious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
4755 LGI=[1310.55](m), MNI=[0.013], SCI=[0](min),

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4755 Continuous simulation parameters:
4756 IaRECPper=[ 4] (hrs), IaRECImp=[ 4] (hrs),
4757 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010]/(mm),
4758 InterEventTime=[ 18] (hrs), END=- 1
4759 *%-----|-----|
4760 ADD HYD NHYDsum=["JOCKVA-TO"], NHYDsto
add=["EX-LAND-MN"+"JOCKVA"+"B2-M"+"B3-M"]
4761 *%-----|-----|
4762 SAVE HYD NHYD=["JOCKVA-TO"], # OF PCYCLES=[ -1], ICASEsh=[ 1]
4763 HYD_COMMENT=["Total Flows at KB first pond"]
4764 *%-----|-----|
4765 *#*****|*****|
4766 *# Jockvale SWM Facility
4767 *# - Rating curve obtained from Jockvale Servicing Study (CCL 1999)
4768 *#*****|*****|
4769 ROUTE RESERVOIR NHYDout=["JOCK_P"], NHYDin=["JOCKVA-TO"],
4770 RDT=[ 1] (min),
4771 TABLE of ( OUTFLOW STORAGE ) values
4772 (cms) - (ha-m)
4773 [ 0.0 , 0.0 ]
4774 [ 0.27 , 0.03]
4775 [ 0.28 , 0.55]
4776 [ 0.29 , 1.14]
4777 [ 0.30 , 1.80]
4778 [ 0.31 , 2.32]
4779 [ 1.12 , 2.87]
4780 [ 2.92 , 3.45]
4781 [ 4.64 , 4.07]
4782 [ 6.69 , 4.72]
4783 [ 9.02 , 5.39]
4784 [ 11.62 , 6.10]
4785 [ 14.42 , 6.85]
4786 [ 17.45 , 7.62]
4787 [ 20.69 , 8.44]
4788 [ 24.08 , 9.28]
4789 [ 27.68 , 10.17]
4790 [ -1 , -1 ] (max twenty pts)
4791 NHYDovf=["JO-OVF"]
4792 *%-----|-----|
4793 ADD HYD NHYDsum=["SN_DE"], NHYDsto add=["N_DE"+"DESIRE"+"JO-OVF"+"JOCK_P"]
4794 *%-----|-----|
4795 SAVE HYD NHYD=["SN_DE"], # OF PCYCLES=[ -1], ICASEsh=[ 1]
4796 HYD_COMMENT=["Total Flows at Heart's Desire"]
4797 *%-----|-----|
4798 *#
4799 *# Hydrograph from Heart's Desire routed to Rideau River
4800 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 0
4801 *#
4802 ROUTE CHANNEL NHYDout=["N1"], NHYDin=["SN_DE"],
4803 RDT=[ 1] (min),
4804 CHLGTH=[ 563] (m), CHSLOPE=[ 0.9668] (%),
4805 FPSLOPE=[ 0.9668] (%),
4806 SECNUM=[ 1.0], NSEG=[ 3]
4807 ( SEGROUGH, SEGDIST (m))=
4808 [ 0.075, -30.20
4809 -0.045, 30.20
4810 0.075, 48.48] NSEG times
4811 ( DISTANCE (m), ELEVATION (m))=
4812 [-98.46, 81.50]
4813 [-92.24, 81.00]
4814 [-86.88, 80.50]
4815 [-81.54, 80.00]
4816 [-74.36, 79.50]
4817 [-63.54, 79.00]
4818 [-39.23, 78.50]
4819 [-34.51, 78.00]

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4820 [- 33. 01, 77. 50]
4821 [- 30. 20, 77. 00]
4822 [- 13. 42, 76. 18]
4823 [- 1. 14, 76. 09]
4824 [17. 06, 76. 18]
4825 [30. 20, 77. 00]
4826 [32. 95, 77. 50]
4827 [34. 06, 78. 00]
4828 [35. 11, 78. 50]
4829 [36. 32, 79. 00]
4830 [37. 74, 79. 50]
4831 [48. 48, 81. 50]
4832 *%-----|-----|
4833 *#*****|*****|
4834 *# Catchment S-2
4835 *# - To Jock River (north and south)
4836 *# - Undeveloped floodplain and river
4837 *#*****|*****|
4838 CONTINUOUS NASHYD NHYD=["S-2"], DT=[1] min, AREA=[102.94] (ha),
4839 DWF=[0] (cms), CN/C=[72], IA=[4.67] (mm),
4840 N=[3], TP=[0.40] hrs,
4841 Continuous simulation parameters:
4842 IaRECper=[4] (hrs),
4843 SMN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
4844 InterEventTime=[12] (hrs)
4845 Baseflow simulation parameters:
4846 BaseFlowOption=[1],
4847 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
4848 VHydCond=[0.055] (mm/hr), END=-1
4849 *%-----|-----|
4850 ADD HYD NHYDs um=["SN_NI"], NHYDs to add=["NI"+"S-2"]
4851 *%-----|-----|
4852 SAVE HYD NHYD=["SN_NI"], # OF PCYCLES=[-1], ICASEsh=[1]
4853 HYD_COMMENT=["Total Flows at Rideau River"]
4854 *%-----|-----|
4855 *#####|#####|
4856 *% 5 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4857 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[5]
4858 *% ["C24SC005.stm"] <--storm filename, one per line for NSTORMtime
4859 *%-----|-----|
4860 *% 10 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4861 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[10]
4862 *% ["C24SC010.stm"] <--storm filename, one per line for NSTORMtime
4863 *%-----|-----|
4864 *% 25 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4865 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[25]
4866 *% ["C24SC025.stm"] <--storm filename, one per line for NSTORMtime
4867 *%-----|-----|
4868 *% 50 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4869 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[50]
4870 *% ["C24SC050.stm"] <--storm filename, one per line for NSTORMtime
4871 *%-----|-----|
4872 *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4873 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4874 *% ["100YC3H.STM"] <--storm filename, one per line for NSTORMtime
4875 *%-----|-----|
4876 *% 100 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4877 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4878 *% ["C24SC100.stm"] <--storm filename, one per line for NSTORMtime
4879 *%-----|-----|
4880 *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4881 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4882 *% ["C24SC100.stm"] <--storm filename, one per line for NSTORMtime
4883 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[101]
4884 *% ["A24SC100.stm"] <--storm filename, one per line for NSTORMtime
4885 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[102]

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4886 *%
4887 FINISH
4888

["A24SCI00_60.stm"] <-- storm filename, one per line for NSTORMtime


```

00375# #
00376# R002:CO039 --- Dfm-n-ID-NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rvmm-R-C --- Dwfcm
00377# ADD HYD + 1.0 02:DM1 9506.00 7.379 No.date 33:12 11.30 n/a 000
00378# ROUTE CHANNEL > 1.0 02:S_ND 1923.00 8.276 No.date 39:46 11.36 n/a 000
00379# + 1.0 02:NC_CK 1917.00 4.042 No.date 34:24 11.98 n/a 000
00380# SIMM 1.0 01:S_N1 11923.00 12.077 No.date 33:14 11.36 n/a 000
00381#
00382# Sum of hydrographs from Node 11 routed to Node 10
00383# Section 7
00384#
00385# R002:CO040 --- Dfm-n-ID-NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rvmm-R-C --- Dwfcm
00386# ROUTE CHANNEL > 1.0 02:S_N1 11923.00 8.276 No.date 39:46 11.36 n/a 000
00387# [RFE:1.00] out_c 1.0 01:N1 11923.00 8.276 No.date 39:46 11.36 n/a 000
00388# [L/S/n=4028./157.040]
00389# [Vmax=.462;Dmax=.886]
00390#
00391# Addition of Subwatershed 10 to Node 10
00392#
00393# R002:CO041 --- Dfm-n-ID-NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rvmm-R-C --- Dwfcm
00394# ADD HYD + 1.0 02:N1 11923.00 8.276 No.date 39:46 11.36 n/a 000
00395# + 1.0 02:SW1 5066.00 11.228 No.date 29:22 11.98 n/a 000
00396# SIMM 1.0 01:S_N0 17589.00 19.451 No.date 38:31 12.19 n/a 000
00397# [L/S/n=3982./051.040]
00398# [Vmax=.577;Dmax=2.212]
00399#
00400# SAVE HYD 1.0 01:S_N0 17589.00 19.451 No.date 38:31 12.19 n/a 000
00401# frame_HLSND
00402# remark:flow at S_N0: N0 + SW10
00403# Addition of Kings Creek to S_N10
00404#
00405# R002:CO043 --- Dfm-n-ID-NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rvmm-R-C --- Dwfcm
00406# ADD HYD + 1.0 02:S_N0 25965.00 30.328 No.date 39:58 12.12 n/a 000
00407# + 1.0 02:NC_CK 8376.00 11.072 No.date 39:59 11.98 n/a 000
00408# SIMM 1.0 01:S_N0A 25965.00 30.328 No.date 39:58 12.12 n/a 000
00409#
00410# Sum of hydrographs from Node 10 routed to Node 9
00411# Section 2
00412#
00413# R002:CO044 --- Dfm-n-ID-NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rvmm-R-C --- Dwfcm
00414# ROUTE CHANNEL > 1.0 02:S_N0A 25965.00 29.579 No.date 39:59 12.12 n/a 000
00415# [RFE:1.00] out_c 1.0 01:N1 25965.00 29.579 No.date 39:59 12.12 n/a 000
00416# [L/S/n=3982./073.040]
00417# [Vmax=.595;Dmax=1.208]
00418#
00419# Addition of Subwatershed 9 and Nichols Creek to Node 9
00420#
00421# R002:CO045 --- Dfm-n-ID-NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rvmm-R-C --- Dwfcm
00422# ADD HYD + 1.0 02:N1 25965.00 29.579 No.date 39:59 12.12 n/a 000
00423# + 1.0 02:SW1 131.00 4.434 No.date 39:56 13.25 n/a 000
00424# + 1.0 02:NC_CK 4464.00 5.504 No.date 39:59 10.98 n/a 000
00425# SIMM 1.0 01:S_N1 31561.00 36.313 No.date 39:59 12.00 n/a 000
00426#
00427# Sum of hydrographs from Node 9 routed to Node 8
00428# Section 3
00429#
00430# R002:CO046 --- Dfm-n-ID-NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rvmm-R-C --- Dwfcm
00431# ROUTE CHANNEL > 1.0 02:S_N1 31561.00 36.313 No.date 39:59 12.00 n/a 000
00432# [RFE:1.00] out_c 1.0 01:N1 31561.00 36.313 No.date 39:59 12.00 n/a 000
00433# [L/S/n=3982./087.040]
00434# [Vmax=.418;Dmax=1.281]
00435#
00436# Addition of Subwatershed 8 and Hibbs' Drain to Node 8
00437#
00438# R002:CO047 --- Dfm-n-ID-NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rvmm-R-C --- Dwfcm
00439# ADD HYD + 1.0 02:N1 31561.00 36.313 No.date 39:59 12.00 n/a 000
00440# + 1.0 02:SW1 131.00 4.434 No.date 39:56 13.25 n/a 000
00441# + 1.0 02:NC_CK 4464.00 5.504 No.date 39:59 10.98 n/a 000
00442# SIMM 1.0 01:S_N1 31561.00 36.313 No.date 39:59 12.00 n/a 000
00443#
00444# Sum of hydrographs from Node 8 routed to Node 7
00445# Section 4
00446#
00447# R002:CO048 --- Dfm-n-ID-NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rvmm-R-C --- Dwfcm
00448# ROUTE CHANNEL > 1.0 02:S_N1 35546.00 40.474 No.date 39:59 12.00 n/a 000
00449# [RFE:1.00] out_c 1.0 01:N1 35546.00 40.474 No.date 39:59 12.00 n/a 000
00450# [L/S/n=3750./053.070]
00451# [Vmax=.208;Dmax=1.651]
00452#
00453# Addition of Subwatershed 7 to Node 7
00454# Section 5
00455#
00456# R002:CO049 --- Dfm-n-ID-NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rvmm-R-C --- Dwfcm
00457# ADD HYD + 1.0 02:SW7 3197.00 4.651 No.date 36:31 9.85 n/a 000
00458# + 1.0 02:SW7 38743.00 35.071 No.date 43:33 11.82 n/a 000
00459# SIMM 1.0 01:S_N1 38743.00 35.071 No.date 43:33 11.82 n/a 000
00460#
00461# SAVE HYD 1.0 01:S_N1 38743.00 35.071 No.date 43:33 11.82 n/a 000
00462# frame_HLSND
00463# remark:flow at S_N7: N0 + SW7
00464# Insertion of a Reservoir to simulate the effects of the Richmond Fen.
00465# Storage area and volumes were estimated from available topography.
00466# Release rate from fen was assumed to be controlled by the downstream
00467# river cross section for various conditions. It is assumed that for up to
00468# 0.75 m of water, the main channel of the river provided the storage. Above
00469# this depth, the wetland starts to significantly store water.
00470#
00471# R002:CO050 --- Dfm-n-ID-NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rvmm-R-C --- Dwfcm
00472# ROUTE RESERVOIR > 1.0 01:RES_RF 38743.00 23.265 No.date 55:09 11.82 n/a 000
00473# [M&S:out_c=7.00]
00474# + 1.0 02:SW7 38743.00 35.071 No.date 43:33 11.82 n/a 000
00475# SIMM 1.0 01:S_N1 38743.00 35.071 No.date 43:33 11.82 n/a 000
00476#
00477# SAVE HYD 1.0 01:RES_RF 38743.00 23.265 No.date 55:09 11.82 n/a 000
00478# frame_HLSRF
00479# remark:outflow of Richmond Fen
00480#
00481# Sum of hydrographs from Node 7 routed to Node 6
00482# Section 5
00483#
00484# R002:CO051 --- Dfm-n-ID-NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rvmm-R-C --- Dwfcm
00485# ROUTE CHANNEL > 1.0 02:RES_RF 38743.00 23.268 No.date 55:09 11.82 n/a 000
00486# [RFE:1.00] out_c 1.0 01:N1 38743.00 23.268 No.date 56:38 11.82 n/a 000
00487# [L/S/n=1067./083.040]
00488# [Vmax=.432;Dmax=.808]
00489#
00490# Addition of Subwatershed 6 and Van Gual Drain to Node 6
00491#
00492# R002:CO054 --- Dfm-n-ID-NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rvmm-R-C --- Dwfcm
00493# ADD HYD + 1.0 02:N1 38743.00 23.268 No.date 55:09 11.82 n/a 000
00494# + 1.0 02:SW2 40240.00 23.318 No.date 39:59 11.89 n/a 000
00495# + 1.0 02:SW2 40240.00 23.318 No.date 39:59 11.89 n/a 000
00496# SIMM 1.0 01:S_N1 40240.00 23.318 No.date 39:59 11.89 n/a 000
00497#
00498# Sum of hydrographs from Node 6 routed to Node 5
00499# Section 6
00500#
00501# R002:CO055 --- Dfm-n-ID-NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rvmm-R-C --- Dwfcm
00502# ROUTE CHANNEL > 1.0 02:S_N1 40240.00 23.318 No.date 39:59 11.89 n/a 000
00503# [RFE:1.00] out_c 1.0 01:N1 40240.00 23.318 No.date 56:09 11.89 n/a 000
00504# [L/S/n=1882./054.040]
00505# [Vmax=.378;Dmax=.917]
00506#
00507# Addition of Subwatershed 5 and Flowing Creek to Node 5
00508# Section 8
00509#
00510# R002:CO056 --- Dfm-n-ID-NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rvmm-R-C --- Dwfcm
00511# ADD HYD + 1.0 02:N1 40240.00 23.285 No.date 56:09 11.89 n/a 000
00512# + 1.0 02:SW2 2597.00 2.597 No.date 37:08 12.20 n/a 000
00513# + 1.0 02:PL_CK 4945.00 14.839 No.date 32:25 14.57 n/a 000
00514# SIMM 1.0 01:S_N1 40240.00 23.166 No.date 37:08 12.20 n/a 000
00515#
00516# Sum of hydrographs from Node 5 routed to Node 5A
00517# Section 7
00518#
00519# R002:CO057 --- Dfm-n-ID-NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rvmm-R-C --- Dwfcm
00520# ROUTE CHANNEL > 1.0 02:S_N1 45409.01 33.166 No.date 37:08 12.20 n/a 000
00521# [RFE:1.00] out_c 1.0 01:N1 45409.01 33.166 No.date 37:20 12.20 n/a 000
00522# [L/S/n=556./090.040]
00523# [Vmax=.443;Dmax=.937]
00524#
00525# Addition of Subwatershed 5A and Subwatershed 5A2 to Node 5A
00526# Section 8
00527#
00528# R002:CO058 --- Dfm-n-ID-NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rvmm-R-C --- Dwfcm
00529# ADD HYD + 1.0 02:NSA 45409.01 33.166 No.date 37:20 12.20 n/a 000
00530# + 1.0 02:SW2A 20.00 .309 No.date 28:36 17.79 n/a 000
00531# + 1.0 02:SW2A 1412.00 3.090 No.date 38:04 15.22 n/a 000
00532# SIMM 1.0 01:S_N1 45409.01 36.216 No.date 37:28 12.30 n/a 000
00533#
00534# Sum of hydrographs from Node 5A routed to Node 4
00535# Section 8
00536#
00537# R002:CO059 --- Dfm-n-ID-NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rvmm-R-C --- Dwfcm
00538# ROUTE CHANNEL > 1.0 02:S_N1A 46841.01 36.216 No.date 37:28 12.30 n/a 000
00539# [RFE:1.00] out_c 1.0 01:N1 46841.01 35.288 No.date 39:22 12.30 n/a 000
00540# [L/S/n=4630./043.035]
00541# [Vmax=.695;Dmax=2.444]
00542#
00543# Addition of Subwatershed 4 and Leary Creek to Node 4
00544# Section 9
00545#
00546# R002:CO060 --- Dfm-n-ID-NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rvmm-R-C --- Dwfcm
00547# ADD HYD + 1.0 02:SW4 585.00 4.325 No.date 29:58 17.79 n/a 000
00548# + 1.0 02:SW4 1021.00 5.747 No.date 30:50 17.79 n/a 000
00549# + 1.0 02:SW4 48447.00 37.581 No.date 38:13 12.47 n/a 000
00550# SIMM 1.0 01:S_N1 48447.00 37.581 No.date 38:13 12.47 n/a 000
00551#
00552# SAVE HYD 1.0 01:S_N1 48447.00 37.581 No.date 38:13 12.47 n/a 000
00553# frame_S.N.002
00554# remark:flow at S_N1
00555#
00556# Sum of hydrographs from Node 4 routed to Node 2
00557# Section 10
00558#
00559# R002:CO062 --- Dfm-n-ID-NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rvmm-R-C --- Dwfcm
00560# ROUTE CHANNEL > 1.0 02:S_N1 48447.00 37.581 No.date 38:13 12.47 n/a 000
00561# [RFE:1.00] out_c 1.0 01:N1 48447.00 37.581 No.date 38:13 12.47 n/a 000
00562# [L/S/n=1667./060.040]
00563# [Vmax=.715;Dmax=2.845]
00564#
00565# Addition of Subwatershed 2 with Mbohan Drain and Smith Drain to Node 2
00566# R002:CO063 --- Dfm-n-ID-NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rvmm-R-C --- Dwfcm
00567# ADD HYD + 1.0 02:N1 48447.00 37.455 No.date 38:49 12.47 n/a 000

```

Table with columns for ID, description, coordinates, and various parameters. Includes entries for ROUTE RESERVOIR, ROUTE CHANNEL, and CONTINUOUS STANDBY. Contains detailed technical specifications and flow data.

```
012128 #  
012129 ROUTE CHANNEL >> 1.0 02:5:1-FO-DNS 53577.82 47.629 N.Date 34:57 12.82 n/a 0.00  
012130 [RFS: 1.0] out <= 1.0 01:8:FO-DI 35577.82 47.599 N.Date 35:11 12.82 n/a 0.00  
012131 [L/S:n= 1183 / 0767 / 035]  
012132 [Vmax = 919:DMax= 2.64]  
012133 *****  
01300 # Catchment FOSTER  
01301 # To West ditch (north of the Jack)  
01302 # Partially defined (medium density); remaining agricultural  
01303 # 2020-12-01 decrease area to 332 ac per Foster SWA Foster area 127.98 HA after increasing Kflecfe Drainage area to 4 (5  
01304 # 2021:02:12 update Foster area to 323.44 ac as measured from QGIS  
01305 #  
01306 #  
013177 R0002:CO0157..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
013178 CONTIUS STANHDID ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
013179 [XMP: 55:TIMP: 65]  
013180 [LRS: 2 - Cn= 74.0]  
013181 [Previous area: I:APER= 4.67:SLP2= 0.0:LEP: 40.:MNP: 250:SCP: 0]  
013182 [Impervious area: I:AMP= 1.57:SLP1= 0.5:LG= 1473.:MNI: 013:SCI= 0]  
013183 [IARECmp= 4.00: IAREJRC= 4.00]  
013184 [SMN= 36.67: SMMX=244.49: SKE= 010]  
013185 *****  
01466 # Foster Pond  
01467 # Rating curve obtained assuming 400m^3/hr in 24 hours for quality control  
01468 # ratio of the catchment area to the West Clarke pond rating curve  
01469 # from the MS for the next coordinates  
01470 #  
015151 R0002:CO0159..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
015152 ROUTE RESERVOIR >> 1.0 02:5:1-FO-DNS 325.44 13.697 N.Date 28:15 28.56 n/a 0.00  
015153 out <= 1.0 01:8:FO-DI 325.44 13.694 N.Date 29:12 28.56 n/a 0.00  
015154 overflow <= 1.0 03:5:1-DBRovf 0.00 0.00 N.Date 0.00 0.00 n/a 0.00  
015155 [MSYSSto: 0.0000E+00, Tot Of Vol.: 0.0000E+00, N Of Cr.: 0, Tot Dur Of: 0 hrs]015156 R0002:CO0160..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
015157 ADD HYD ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
015158 + 1.0 02:5:1-FO-DNS 325.44 13.694 N.Date 29:12 28.56 n/a 0.00  
015159 SIML ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
015160 [Mjor System / 1.0 03:5:1-FO-DNS 325.44 13.694 N.Date 29:12 28.56 n/a 0.00  
015161 [Mjor System / 1.0 03:5:1-FO-DNS 325.44 13.694 N.Date 29:12 28.56 n/a 0.00  
015162 [MSYSSto: 0.0000E+00, Tot Of Vol.: 0.0000E+00, N Of Cr.: 0, Tot Dur Of: 0 hrs]  
015163 CONTIUS STANHDID ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
015164 [XMP: 65:TIMP: 65]  
015165 [LRS: 2 - Cn= 77.0]  
015166 [Previous area: I:APER= 4.67:SLP2= 0.0:LEP: 40.:MNP: 250:SCP: 0]  
015167 [Impervious area: I:AMP= 1.57:SLP1= 0.5:LG= 699.:MNI: 013:SCI= 0]  
015168 [IARECmp= 4.00: IAREJRC= 4.00]  
015169 [SMN= 31.15: SMMX=207.66: SKE= 010]  
015170 ROUTE RESERVOIR >> 1.0 02:5:1-FO-DNS 73.29 4.584 N.Date 28:07 31.34 n/a 0.00  
015171 out <= 1.0 01:8:FO-DI 73.29 4.584 N.Date 28:50 31.34 n/a 0.00  
015172 overflow <= 1.0 03:5:1-DBRovf 0.00 0.00 N.Date 0.00 0.00 n/a 0.00  
015173 [MSSto: 0.0000E+00, Tot Of Vol.: 0.0000E+00, N Of Cr.: 0, Tot Dur Of: 0 hrs]  
015174 R0002:CO0162..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
015175 CONTIUS STANHDID ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
015176 [XMP: 65:TIMP: 65]  
015177 [LRS: 2 - Cn= 74.0]  
015178 [Previous area: I:APER= 4.67:SLP2= 0.0:LEP: 40.:MNP: 250:SCP: 0]  
015179 [Impervious area: I:AMP= 1.57:SLP1= 0.5:LG= 181.:MNI: 013:SCI= 0]  
015180 [IARECmp= 4.00: IAREJRC= 4.00]  
015181 [SMN= 36.67: SMMX=244.49: SKE= 010]  
015182 R0002:CO0164..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
015183 COMPUTE DUALHYD ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
015184 Mjor System / 1.0 02:5:1-FO-DI 4.94 383 N.Date 28:01 28.56 n/a 0.00  
015185 Mjor System / 1.0 02:5:1-FO-DI 4.94 383 N.Date 28:01 28.56 n/a 0.00  
015186 [MSYSSto: 0.0000E+00, Tot Of Vol.: 0.0000E+00, N Of Cr.: 0, Tot Dur Of: 0 hrs]  
015187 R0002:CO0165..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
015188 ADD HYD ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
015189 + 1.0 02:5:1-FO-DNS 4.94 383 N.Date 28:01 28.56 n/a 0.00  
015190 SIML ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
015191 [Mjor System / 1.0 03:5:1-FO-DNS 4.94 383 N.Date 28:01 28.56 n/a 0.00  
015192 ROUTE RESERVOIR >> 1.0 02:5:1-FO-DNS 4.94 383 N.Date 28:01 28.56 n/a 0.00  
015193 out <= 1.0 01:8:FO-DI 4.94 383 N.Date 28:50 28.56 n/a 0.00  
015194 overflow <= 1.0 03:5:1-DBRovf 0.00 0.00 N.Date 0.00 0.00 n/a 0.00  
015195 [MSSto: 0.0000E+00, Tot Of Vol.: 0.0000E+00, N Of Cr.: 0, Tot Dur Of: 0 hrs]  
015196 R0002:CO0167..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
015197 ADD HYD ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
015198 + 1.0 02:5:1-FO-DNS 325.44 13.694 N.Date 29:12 28.56 n/a 0.00  
015199 SIML ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
015200 [Mjor System / 1.0 03:5:1-FO-DNS 325.44 13.694 N.Date 29:12 28.56 n/a 0.00  
015201 [Mjor System / 1.0 03:5:1-FO-DNS 325.44 13.694 N.Date 29:12 28.56 n/a 0.00  
015202 [MSYSSto: 0.0000E+00, Tot Of Vol.: 0.0000E+00, N Of Cr.: 0, Tot Dur Of: 0 hrs]  
015203 SAVE HYD ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
015204 [LRS: 2 - Cn= 75.0]  
015205 #  
015206 # Hydrograph from Node Foster SWM1 Station 98010 Node at station 520  
015207 # Channel X-Section obtained from RCVA Hydraulic Model - Station 980  
015208 #  
015209 R0002:CO0169..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
015210 ROUTE CHANNEL ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
015211 [RFS: 1.0] out <= 1.0 01:8:FO-DI 330.38 3.791 N.Date 29:25 28.56 n/a 0.00  
015212 [L/S:n= 603 / 043 / 035]  
015213 [Vmax = 544:DMax= 1.092]  
015214 CONTIUS STANHDID ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
015215 [XMP: 65:TIMP: 65]  
015216 [LRS: 2 - Cn= 74.0]  
015217 [Previous area: I:APER= 4.67:SLP2= 0.0:LEP: 40.:MNP: 250:SCP: 0]  
015218 [Impervious area: I:AMP= 1.57:SLP1= 0.5:LG= 185.:MNI: 013:SCI= 0]  
015219 [IARECmp= 4.00: IAREJRC= 4.00]  
015220 [SMN= 36.67: SMMX=244.49: SKE= 010]  
015221 *****  
012228 R0002:CO0171..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012229 COMPUTE DUALHYD ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012230 Mjor System / 1.0 03:5:1-FO-DI 5.11 460 N.Date 28:01 31.98 n/a 0.00  
012231 Mjor System / 1.0 03:5:1-FO-DI 5.11 460 N.Date 28:01 31.98 n/a 0.00  
012232 Mjor System / 1.0 03:5:1-FO-DNS 5.11 460 N.Date 28:01 31.98 n/a 0.00  
012233 [MSYSSto: 0.0000E+00, Tot Of Vol.: 0.0000E+00, N Of Cr.: 0, Tot Dur Of: 0 hrs]  
012234 R0002:CO0172..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012235 ADD HYD ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012236 + 1.0 02:5:1-FO-DNS 5.11 460 N.Date 28:01 31.98 n/a 0.00  
012237 SIML ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012238 [Mjor System / 1.0 03:5:1-FO-DNS 5.11 460 N.Date 28:01 31.98 n/a 0.00  
012239 [Mjor System / 1.0 03:5:1-FO-DNS 5.11 460 N.Date 28:01 31.98 n/a 0.00  
012240 [MSYSSto: 0.0000E+00, Tot Of Vol.: 0.0000E+00, N Of Cr.: 0, Tot Dur Of: 0 hrs]  
012241 R0002:CO0173..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012242 CONTIUS STANHDID ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012243 [XMP: 65:TIMP: 65]  
012244 [LRS: 2 - Cn= 74.0]  
012245 [Previous area: I:APER= 4.67:SLP2= 0.0:LEP: 40.:MNP: 250:SCP: 0]  
012246 [Impervious area: I:AMP= 1.57:SLP1= 0.5:LG= 316.:MNI: 013:SCI= 0]  
012247 [IARECmp= 4.00: IAREJRC= 4.00]  
012248 [SMN= 36.67: SMMX=244.49: SKE= 010]  
012249 R0002:CO0178..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012250 COMPUTE DUALHYD ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012251 Mjor System / 1.0 02:5:1-FO-DI 14.96 1.215 N.Date 28:02 31.98 n/a 0.00  
012252 Mjor System / 1.0 02:5:1-FO-DI 14.96 1.215 N.Date 28:02 31.98 n/a 0.00  
012253 Mjor System / 1.0 02:5:1-FO-DNS 14.96 1.215 N.Date 28:02 31.98 n/a 0.00  
012254 [MSYSSto: 0.0000E+00, Tot Of Vol.: 0.0000E+00, N Of Cr.: 0, Tot Dur Of: 0 hrs]  
012255 R0002:CO0179..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012256 ADD HYD ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012257 + 1.0 02:5:1-FO-DNS 14.96 1.215 N.Date 28:02 31.98 n/a 0.00  
012258 SIML ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012259 [Mjor System / 1.0 03:5:1-FO-DNS 14.96 1.215 N.Date 28:02 31.98 n/a 0.00  
012260 [Mjor System / 1.0 03:5:1-FO-DNS 14.96 1.215 N.Date 28:02 31.98 n/a 0.00  
012261 [MSYSSto: 0.0000E+00, Tot Of Vol.: 0.0000E+00, N Of Cr.: 0, Tot Dur Of: 0 hrs]  
012262 R0002:CO0180..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012263 CONTIUS STANHDID ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012264 [XMP: 65:TIMP: 65]  
012265 [LRS: 2 - Cn= 74.0]  
012266 [Previous area: I:APER= 4.67:SLP2= 0.0:LEP: 40.:MNP: 250:SCP: 0]  
012267 [Impervious area: I:AMP= 1.57:SLP1= 0.5:LG= 316.:MNI: 013:SCI= 0]  
012268 [IARECmp= 4.00: IAREJRC= 4.00]  
012269 [SMN= 36.67: SMMX=244.49: SKE= 010]  
012270 R0002:CO0181..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012271 ADD HYD ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012272 + 1.0 02:5:1-FO-DNS 14.96 1.215 N.Date 28:02 31.98 n/a 0.00  
012273 SIML ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012274 [Mjor System / 1.0 03:5:1-FO-DNS 14.96 1.215 N.Date 28:02 31.98 n/a 0.00  
012275 [Mjor System / 1.0 03:5:1-FO-DNS 14.96 1.215 N.Date 28:02 31.98 n/a 0.00  
012276 [MSYSSto: 0.0000E+00, Tot Of Vol.: 0.0000E+00, N Of Cr.: 0, Tot Dur Of: 0 hrs]  
012277 R0002:CO0182..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012278 CONTIUS STANHDID ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012279 [XMP: 32:TIMP: 65]  
012280 [LRS: 2 - Cn= 77.0]  
012281 [Previous area: I:APER= 4.67:SLP2= 0.0:LEP: 40.:MNP: 250:SCP: 0]  
012282 [Impervious area: I:AMP= 1.57:SLP1= 0.5:LG= 181.:MNI: 013:SCI= 0]  
012283 [IARECmp= 4.00: IAREJRC= 4.00]  
012284 [SMN= 36.67: SMMX=244.49: SKE= 010]  
012285 R0002:CO0183..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012286 COMPUTE DUALHYD ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012287 Mjor System / 1.0 02:5:1-DI 5.27 475 N.Date 28:02 23.32 n/a 0.00  
012288 Mjor System / 1.0 02:5:1-DI 5.27 475 N.Date 28:02 23.32 n/a 0.00  
012289 [MSYSSto: 0.0000E+00, Tot Of Vol.: 0.0000E+00, N Of Cr.: 0, Tot Dur Of: 0 hrs]  
012290 R0002:CO0184..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012291 ADD HYD ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012292 + 1.0 02:5:1-DNS 5.27 475 N.Date 28:02 23.32 n/a 0.00  
012293 SIML ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012294 [Mjor System / 1.0 03:5:1-DBRovf 0.00 0.00 N.Date 0.00 0.00 n/a 0.00  
012295 [Mjor System / 1.0 03:5:1-DBRovf 0.00 0.00 N.Date 0.00 0.00 n/a 0.00  
012296 [MSSto: 0.0000E+00, Tot Of Vol.: 0.0000E+00, N Of Cr.: 0, Tot Dur Of: 0 hrs]  
012297 R0002:CO0185..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012298 CONTIUS STANHDID ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012299 [XMP: 65:TIMP: 65]  
012300 [LRS: 2 - Cn= 77.0]  
012301 [Previous area: I:APER= 4.67:SLP2= 0.0:LEP: 40.:MNP: 250:SCP: 0]  
012302 [Impervious area: I:AMP= 1.57:SLP1= 0.5:LG= 181.:MNI: 013:SCI= 0]  
012303 [IARECmp= 4.00: IAREJRC= 4.00]  
012304 [SMN= 36.67: SMMX=244.49: SKE= 010]  
012305 R0002:CO0186..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012306 CONTIUS STANHDID ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012307 [XMP: 32:TIMP: 65]  
012308 [LRS: 2 - Cn= 77.0]  
012309 [Previous area: I:APER= 4.67:SLP2= 0.0:LEP: 40.:MNP: 250:SCP: 0]  
012310 [Impervious area: I:AMP= 1.57:SLP1= 0.5:LG= 181.:MNI: 013:SCI= 0]  
012311 [IARECmp= 4.00: IAREJRC= 4.00]  
012312 [SMN= 36.67: SMMX=244.49: SKE= 010]  
012313 R0002:CO0187..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012314 ADD HYD ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012315 + 1.0 02:5:1-DNS 335.49 3.820 N.Date 29:25 28.61 n/a 0.00  
012316 SIML ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012317 [Mjor System / 1.0 03:5:1-FO-DNS 335.49 3.820 N.Date 29:25 28.61 n/a 0.00  
012318 [Mjor System / 1.0 03:5:1-FO-DNS 335.49 3.820 N.Date 29:25 28.61 n/a 0.00  
012319 [MSYSSto: 0.0000E+00, Tot Of Vol.: 0.0000E+00, N Of Cr.: 0, Tot Dur Of: 0 hrs]  
012320 R0002:CO0188..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012321 CONTIUS STANHDID ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012322 [XMP: 65:TIMP: 65]  
012323 [LRS: 2 - Cn= 77.0]  
012324 [Previous area: I:APER= 4.67:SLP2= 0.0:LEP: 40.:MNP: 250:SCP: 0]  
012325 [Impervious area: I:AMP= 1.57:SLP1= 0.5:LG= 181.:MNI: 013:SCI= 0]  
012326 [IARECmp= 4.00: IAREJRC= 4.00]  
012327 [SMN= 36.67: SMMX=244.49: SKE= 010]  
012328 R0002:CO0189..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012329 COMPUTE DUALHYD ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012330 Mjor System / 1.0 02:5:1-DI 5.27 475 N.Date 28:02 23.32 n/a 0.00  
012331 Mjor System / 1.0 02:5:1-DI 5.27 475 N.Date 28:02 23.32 n/a 0.00  
012332 [MSYSSto: 0.0000E+00, Tot Of Vol.: 0.0000E+00, N Of Cr.: 0, Tot Dur Of: 0 hrs]  
012333 R0002:CO0190..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012334 ADD HYD ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012335 + 1.0 02:5:1-DNS 335.49 3.820 N.Date 29:25 28.61 n/a 0.00  
012336 SIML ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012337 [Mjor System / 1.0 03:5:1-FO-DNS 335.49 3.820 N.Date 29:25 28.61 n/a 0.00  
012338 [Mjor System / 1.0 03:5:1-FO-DNS 335.49 3.820 N.Date 29:25 28.61 n/a 0.00  
012339 [MSYSSto: 0.0000E+00, Tot Of Vol.: 0.0000E+00, N Of Cr.: 0, Tot Dur Of: 0 hrs]  
012340 R0002:CO0191..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012341 CONTIUS STANHDID ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012342 [XMP: 65:TIMP: 65]  
012343 [LRS: 2 - Cn= 77.0]  
012344 [Previous area: I:APER= 4.67:SLP2= 0.0:LEP: 40.:MNP: 250:SCP: 0]  
012345 [Impervious area: I:AMP= 1.57:SLP1= 0.5:LG= 181.:MNI: 013:SCI= 0]  
012346 [IARECmp= 4.00: IAREJRC= 4.00]  
012347 [SMN= 36.67: SMMX=244.49: SKE= 010]  
012348 R0002:CO0192..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012349 COMPUTE DUALHYD ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012350 Mjor System / 1.0 02:5:1-DI 5.27 475 N.Date 28:02 23.32 n/a 0.00  
012351 Mjor System / 1.0 02:5:1-DI 5.27 475 N.Date 28:02 23.32 n/a 0.00  
012352 [MSYSSto: 0.0000E+00, Tot Of Vol.: 0.0000E+00, N Of Cr.: 0, Tot Dur Of: 0 hrs]  
012353 R0002:CO0193..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012354 ADD HYD ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012355 + 1.0 02:5:1-DNS 335.49 3.820 N.Date 29:25 28.61 n/a 0.00  
012356 SIML ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012357 [Mjor System / 1.0 03:5:1-FO-DNS 335.49 3.820 N.Date 29:25 28.61 n/a 0.00  
012358 [Mjor System / 1.0 03:5:1-FO-DNS 335.49 3.820 N.Date 29:25 28.61 n/a 0.00  
012359 [MSYSSto: 0.0000E+00, Tot Of Vol.: 0.0000E+00, N Of Cr.: 0, Tot Dur Of: 0 hrs]  
012360 R0002:CO0194..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012361 CONTIUS STANHDID ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012362 [XMP: 65:TIMP: 65]  
012363 [LRS: 2 - Cn= 77.0]  
012364 [Previous area: I:APER= 4.67:SLP2= 0.0:LEP: 40.:MNP: 250:SCP: 0]  
012365 [Impervious area: I:AMP= 1.57:SLP1= 0.5:LG= 181.:MNI: 013:SCI= 0]  
012366 [IARECmp= 4.00: IAREJRC= 4.00]  
012367 [SMN= 36.67: SMMX=244.49: SKE= 010]  
012368 R0002:CO0195..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012369 COMPUTE DUALHYD ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012370 Mjor System / 1.0 02:5:1-DI 5.27 475 N.Date 28:02 23.32 n/a 0.00  
012371 Mjor System / 1.0 02:5:1-DI 5.27 475 N.Date 28:02 23.32 n/a 0.00  
012372 [MSYSSto: 0.0000E+00, Tot Of Vol.: 0.0000E+00, N Of Cr.: 0, Tot Dur Of: 0 hrs]  
012373 R0002:CO0196..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012374 ADD HYD ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012375 + 1.0 02:5:1-DNS 335.49 3.820 N.Date 29:25 28.61 n/a 0.00  
012376 SIML ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012377 [Mjor System / 1.0 03:5:1-FO-DNS 335.49 3.820 N.Date 29:25 28.61 n/a 0.00  
012378 [Mjor System / 1.0 03:5:1-FO-DNS 335.49 3.820 N.Date 29:25 28.61 n/a 0.00  
012379 [MSYSSto: 0.0000E+00, Tot Of Vol.: 0.0000E+00, N Of Cr.: 0, Tot Dur Of: 0 hrs]  
012380 R0002:CO0197..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012381 CONTIUS STANHDID ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012382 [XMP: 65:TIMP: 65]  
012383 [LRS: 2 - Cn= 77.0]  
012384 [Previous area: I:APER= 4.67:SLP2= 0.0:LEP: 40.:MNP: 250:SCP: 0]  
012385 [Impervious area: I:AMP= 1.57:SLP1= 0.5:LG= 181.:MNI: 013:SCI= 0]  
012386 [IARECmp= 4.00: IAREJRC= 4.00]  
012387 [SMN= 36.67: SMMX=244.49: SKE= 010]  
012388 R0002:CO0198..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012389 COMPUTE DUALHYD ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012390 Mjor System / 1.0 02:5:1-DI 5.27 475 N.Date 28:02 23.32 n/a 0.00  
012391 Mjor System / 1.0 02:5:1-DI 5.27 475 N.Date 28:02 23.32 n/a 0.00  
012392 [MSYSSto: 0.0000E+00, Tot Of Vol.: 0.0000E+00, N Of Cr.: 0, Tot Dur Of: 0 hrs]  
012393 R0002:CO0199..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012394 ADD HYD ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C..... Dwfcm  
012395 + 1.0 02:5:1-DNS 335.49 3.820 N.Date 29:25 28.61 n/a 0.00  
012396 SIML ..... Dfm: 1-D N-D NDD..... AREHA-QPEAKm-TPeakDte-hh:mm..... Rvmm R.C.....
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014975 overflow c 1.0 0:03:DFW ..... 0.00 0.00 N_date 0.00 0.00 n/a ..... 0.00
014985 [M$TotVol=0.0000E+00, TotDirOf=0.00] ..... 0.00 0.00 N_date 0.00 0.00 n/a ..... 0.00
014995 *****
015000 R0002:CO0219 ..... DfIn-ID NND ..... AREA-A ..... QPEAKm-TPeakDte-hh:mm ..... Rvmm-R ..... DWcm
015010 ADD HYD ..... 1.0 0:02:NC ..... 54118.36 49.269 N_date 34:41 12.96 n/a ..... 0.00
015020 + 1.0 0:02:1-DR ..... 3.28 0.09 N_date 29:16 32.20 n/a ..... 0.00
015030 + 1.0 0:02:1-DR ..... 12.84 0.00 N_date 29:23 32.20 n/a ..... 0.00
015040 + 1.0 0:02:1-DR ..... 0.00 0.00 N_date 0.00 0.00 n/a ..... 0.00
015050 + 1.0 0:02:1-DR ..... 0.00 0.00 N_date 0.00 0.00 n/a ..... 0.00
015060 + 1.0 0:02:1-DR ..... 119.40 8.16 N_date 29:25 31.34 n/a ..... 0.00
015070 + 1.0 0:02:1-DR ..... 0.00 0.00 N_date 0.00 0.00 n/a ..... 0.00
015080 SIMM ..... 1.0 0:01:SN ..... 54253.88 49.833 N_date 34:41 13.00 n/a ..... 0.00
015090 R0002:CO0218 ..... DfIn-ID NND ..... AREA-A ..... QPEAKm-TPeakDte-hh:mm ..... Rvmm-R ..... DWcm
015100 SAVE HYD ..... 1.0 0:01:SN ..... 54253.88 49.833 N_date 34:41 13.00 n/a ..... 0.00
015110 *****
015120 *****
015130 Channel X Section obtained from RCVA Hydraulic Model - Station 5737
015140 *****
015150 *****
015160 R0002:CO0219 ..... DfIn-ID NND ..... AREA-A ..... QPEAKm-TPeakDte-hh:mm ..... Rvmm-R ..... DWcm
015175 ROUTE CHANNEL ..... 1.0 0:01:SN ..... 54253.88 49.833 N_date 34:41 13.00 n/a ..... 0.00
015180 + [RFD=1.00] out c ..... 1.0 0:01:SN ..... 54253.88 49.833 N_date 34:41 13.00 n/a ..... 0.00
015190 [L/S=1.270 / 0.0175] ..... 54253.88 49.833 N_date 34:41 13.00 n/a ..... 0.00
015200 [Vmax=611.0Dmax=3.459]
015210 R0002:CO0220 ..... DfIn-ID NND ..... AREA-A ..... QPEAKm-TPeakDte-hh:mm ..... Rvmm-R ..... DWcm
015220 ADD HYD ..... 1.0 0:02:NC ..... 54253.88 49.833 N_date 34:41 13.00 n/a ..... 0.00
015230 + 1.0 0:02:1-DR ..... 21.67 1.26 N_date 29:27 32.20 n/a ..... 0.00
015240 + 1.0 0:02:1-DR ..... 1.75 0.10 N_date 29:14 32.20 n/a ..... 0.00
015250 + 1.0 0:02:1-DR ..... 2.03 0.12 N_date 29:15 32.20 n/a ..... 0.00
015260 + 1.0 0:02:1-DR ..... 0.00 0.00 N_date 0.00 0.00 n/a ..... 0.00
015270 + 1.0 0:02:1-DR ..... 0.00 0.00 N_date 0.00 0.00 n/a ..... 0.00
015280 + 1.0 0:02:1-DR ..... 0.00 0.00 N_date 0.00 0.00 n/a ..... 0.00
015290 SIMM ..... 1.0 0:01:SN ..... 54279.33 48.627 N_date 37:44 13.01 n/a ..... 0.00
015300 R0002:CO0221 ..... DfIn-ID NND ..... AREA-A ..... QPEAKm-TPeakDte-hh:mm ..... Rvmm-R ..... DWcm
015310 SAVE HYD ..... 1.0 0:01:SN ..... 54279.33 48.627 N_date 37:44 13.01 n/a ..... 0.00
015320 *****
015330 *****
015340 *****
015350 *****
015360 *****
015370 *****
015380 *****
015390 R0002:CO0222 ..... DfIn-ID NND ..... AREA-A ..... QPEAKm-TPeakDte-hh:mm ..... Rvmm-R ..... DWcm
015400 ROUTE CHANNEL ..... 1.0 0:02:SN ..... 54279.33 48.627 N_date 37:44 13.01 n/a ..... 0.00
015410 [RFD=1.00] out c ..... 1.0 0:02:SN ..... 54279.33 48.627 N_date 37:44 13.01 n/a ..... 0.00
015420 [L/S=245 / 0.0915] ..... 54279.33 48.627 N_date 37:44 13.01 n/a ..... 0.00
015430 [Vmax=961.0Dmax=4.00]
015440 R0002:CO0223 ..... DfIn-ID NND ..... AREA-A ..... QPEAKm-TPeakDte-hh:mm ..... Rvmm-R ..... DWcm
015450 ROUTE CHANNEL ..... 1.0 0:02:NC ..... 54279.33 48.627 N_date 37:44 13.01 n/a ..... 0.00
015460 [RFD=1.00] out c ..... 1.0 0:02:NC ..... 54279.33 48.627 N_date 37:44 13.01 n/a ..... 0.00
015470 [L/S=245 / 0.0915] ..... 54279.33 48.627 N_date 37:44 13.01 n/a ..... 0.00
015480 *****
015490 R0002:CO0224 ..... DfIn-ID NND ..... AREA-A ..... QPEAKm-TPeakDte-hh:mm ..... Rvmm-R ..... DWcm
015500 ROUTE CHANNEL ..... 1.0 0:02:NC ..... 54279.33 48.627 N_date 37:44 13.01 n/a ..... 0.00
015510 [RFD=1.00] out c ..... 1.0 0:02:NC ..... 54279.33 48.627 N_date 37:44 13.01 n/a ..... 0.00
015520 [L/S=245 / 0.0915] ..... 54279.33 48.627 N_date 37:44 13.01 n/a ..... 0.00
015530 [Vmax=961.0Dmax=4.00]
015540 *****
015550 *****
015560 *****
015570 *****
015580 R0002:CO0225 ..... DfIn-ID NND ..... AREA-A ..... QPEAKm-TPeakDte-hh:mm ..... Rvmm-R ..... DWcm
015590 ROUTE CHANNEL ..... 1.0 0:02:NC ..... 54279.33 48.627 N_date 37:44 13.01 n/a ..... 0.00
015600 [RFD=1.00] out c ..... 1.0 0:02:NC ..... 54279.33 48.627 N_date 37:44 13.01 n/a ..... 0.00
015610 [L/S=1020 / 0.5015] ..... 54279.33 48.627 N_date 37:44 13.01 n/a ..... 0.00
015620 [Vmax=961.0Dmax=4.00]
015630 *****
015640 *****
015650 *****
015660 *****
015670 *****
015680 *****
015690 *****
015700 *****
015710 *****
015720 *****
015730 *****
015740 *****
015750 *****
015760 *****
015770 *****
015780 *****
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016740 *****
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016760 *****
016770 *****
016780 *****
016790 *****
016800 *****
016810 *****
016820 *****
016830 *****

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018713	[AREC mp = 4.00; IAREC mp = 4.00]	ARESHA-QPEAKm-Tpeakdte-hh-mm-Rvmm-R.C.-Dfwm	020585	R0002-CO309	Dfwn-ID-NDD	ARESHA-QPEAKm-Tpeakdte-hh-mm-Rvmm-R.C.-Dfwm	020585	R0002-CO309	Dfwn-ID-NDD	ARESHA-QPEAKm-Tpeakdte-hh-mm-Rvmm-R.C.-Dfwm	
018713	ADD IHD	1.0 0.02:KB-Pond2 254.24 9.930 Ndate 28:12 22.82 n/a 0.00	020585	ROUTE CHANNEL	1.0 0.02:SN:80 54683.13 48.944 Ndate 37:46 13.09 n/a 0.00	020585	ROUTE CHANNEL	1.0 0.02:SN:80 54683.13 48.944 Ndate 37:46 13.09 n/a 0.00	020585	ROUTE CHANNEL	1.0 0.02:SN:80 54683.13 48.944 Ndate 37:46 13.09 n/a 0.00
018713	ROUTE RESEVER	1.0 0.01:KB-PF 257.04 10.049 Ndate 28:11 22.96 n/a 0.00	020600	[RETE 1.00] out	1.0 0.01:N:TO 54683.13 48.905 Ndate 37:53 13.09 n/a 0.00	020600	[RETE 1.00] out	1.0 0.01:N:TO 54683.13 48.905 Ndate 37:53 13.09 n/a 0.00	020600	[RETE 1.00] out	1.0 0.01:N:TO 54683.13 48.905 Ndate 37:53 13.09 n/a 0.00
018713	SUM	1.0 0.01:KB-PF 257.04 10.049 Ndate 28:11 22.96 n/a 0.00	020600	[MSysSto=602.5E+00] Tot.OxVol=0.000E+00 N.Ox=0.0 To.DurOrf=0.0 hrs	020600	[MSysSto=602.5E+00] Tot.OxVol=0.000E+00 N.Ox=0.0 To.DurOrf=0.0 hrs	020600	[MSysSto=602.5E+00] Tot.OxVol=0.000E+00 N.Ox=0.0 To.DurOrf=0.0 hrs	020600	[MSysSto=602.5E+00] Tot.OxVol=0.000E+00 N.Ox=0.0 To.DurOrf=0.0 hrs	
018713	R0002-CO279	Dfwn-ID-NDD	020600	R0002-CO309	Dfwn-ID-NDD	020600	R0002-CO309	Dfwn-ID-NDD	020600	R0002-CO309	Dfwn-ID-NDD
018713	ADD IHD	1.0 0.02:KB-PF 18.54 0.651 Ndate 18:09 22.96 n/a 0.00	020600	ROUTE RESEVER	1.0 0.02:SN:80 54683.13 48.944 Ndate 37:46 13.09 n/a 0.00	020600	ROUTE RESEVER	1.0 0.02:SN:80 54683.13 48.944 Ndate 37:46 13.09 n/a 0.00	020600	ROUTE RESEVER	1.0 0.02:SN:80 54683.13 48.944 Ndate 37:46 13.09 n/a 0.00
018713	overFlow	1.0 0.02:KB-PF 238.50 9.907 Ndate 28:11 22.96 n/a 0.00	020600	Catchment Greenbank	020600	Catchment Greenbank	020600	Catchment Greenbank	020600	Catchment Greenbank	020600
018800	[MSysSto=2001.0E+00] Tot.OxVol=5.477E+00 N.Ox=0.0 To.DurOrf=22.4 hrs	020600	to Greenbank Drain (south of the Jack)	020600	to Greenbank Drain (south of the Jack)	020600	to Greenbank Drain (south of the Jack)	020600	to Greenbank Drain (south of the Jack)	020600	to Greenbank Drain (south of the Jack)
018800	ADD IHD	1.0 0.02:KB-PF 18.54 0.651 Ndate 18:09 22.96 n/a 0.00	020600	JFSA 2021-01-19 update area from 37.47 to 36.6 ha based on GIS measurements	020600	JFSA 2021-01-19 update area from 37.47 to 36.6 ha based on GIS measurements	020600	JFSA 2021-01-19 update area from 37.47 to 36.6 ha based on GIS measurements	020600	JFSA 2021-01-19 update area from 37.47 to 36.6 ha based on GIS measurements	
018800	SUM	1.0 0.02:KB-PF 238.50 9.907 Ndate 28:11 22.96 n/a 0.00	020600	JFSA 2021-01-19 update area from 37.47 to 36.6 ha based on GIS measurements	020600	JFSA 2021-01-19 update area from 37.47 to 36.6 ha based on GIS measurements	020600	JFSA 2021-01-19 update area from 37.47 to 36.6 ha based on GIS measurements	020600	JFSA 2021-01-19 update area from 37.47 to 36.6 ha based on GIS measurements	
018800	R0002-CO281	Dfwn-ID-NDD	020600	R0002-CO310	Dfwn-ID-NDD	020600	R0002-CO310	Dfwn-ID-NDD	020600	R0002-CO310	Dfwn-ID-NDD
018800	SAVE IHD	1.0 0.01:KB-Pond2 257.04 10.048 Ndate 28:11 22.96 n/a 0.00	020600	CONTINUES STANDBY	1.0 0.01:TOOD:MSJ 36.60 2.954 Ndate 28:02 32.54 715 0.00	020600	CONTINUES STANDBY	1.0 0.01:TOOD:MSJ 36.60 2.954 Ndate 28:02 32.54 715 0.00	020600	CONTINUES STANDBY	1.0 0.01:TOOD:MSJ 36.60 2.954 Ndate 28:02 32.54 715 0.00
018800	remark: Total Flow at KH third pond	018800	remark: Total Flow at KH third pond	018800	remark: Total Flow at KH third pond	018800	remark: Total Flow at KH third pond	018800	remark: Total Flow at KH third pond	018800	remark: Total Flow at KH third pond
018800	EDM STING / PROPOSED Subcatchment (Kennedy-Burnett SWM Facility (118080)), SWM Modeling Approach, NOWATECH Report Ju	018800	EDM STING / PROPOSED Subcatchment (Kennedy-Burnett SWM Facility (118080)), SWM Modeling Approach, NOWATECH Report Ju	018800	EDM STING / PROPOSED Subcatchment (Kennedy-Burnett SWM Facility (118080)), SWM Modeling Approach, NOWATECH Report Ju	018800	EDM STING / PROPOSED Subcatchment (Kennedy-Burnett SWM Facility (118080)), SWM Modeling Approach, NOWATECH Report Ju	018800	EDM STING / PROPOSED Subcatchment (Kennedy-Burnett SWM Facility (118080)), SWM Modeling Approach, NOWATECH Report Ju	018800	EDM STING / PROPOSED Subcatchment (Kennedy-Burnett SWM Facility (118080)), SWM Modeling Approach, NOWATECH Report Ju

Table with multiple columns containing technical specifications, codes, and values. The table is organized into two main sections, one on the left and one on the right, each containing a list of entries with various alphanumeric identifiers and numerical data.

026199 [Impervious area: 1Amp=1.57;SLLP=1.00;LGA=183.0;NN=013;SCL=0]

026200 [ARECmp=4.00;IARECmp=4.00]

026201 [SMN=33.81;SMW=225.43;SKE=010]

026202 R0002:CO0404 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026203 COMPUTE DUALIND 1.0 01:AO:M 4.14 246.00 28:01 23.49 n/a 000

026204 Mjor System / 1.0 02:AO:M 0.00 0.00 28:02 0.00 n/a 000

026205 Mjor System \ 1.0 03:AO:M 4.14 246.00 28:01 23.49 n/a 000

026206 [MjorSystem=0.0000E+00;TotOfVol=0.0000E+00;NOf=0;TotDurOf=0.0hrs]

026207 R0002:CO0405 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026208 CONTINUUS STANINH 1.0 01:AI:1 10.61 781.00 28:02 29.20 642.000

026209 [X[M;S;L;T;M] 38.71;TMp=38.71]

026210 [LGA=2.0;CN=75.0]

026211 [Impervious area: 1Amp=4.67;SLLP=1.00;LGA=40.0;MNP=250;SCP=0]

026212 [ARECmp=4.00;IARECmp=4.00]

026213 [SMN=33.81;SMW=225.43;SKE=010]

026214 R0002:CO0406 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026215 COMPUTE DUALIND 1.0 01:AI:1 10.61 781.00 28:02 29.20 n/a 000

026216 Mjor System / 1.0 02:AO:M 12.00 0.00 28:02 0.00 n/a 000

026217 Mjor System \ 1.0 03:AO:M 10.61 781.00 28:02 29.20 n/a 000

026218 [MjorSystem=0.0000E+00;TotOfVol=0.0000E+00;NOf=0;TotDurOf=0.0hrs]

026219 R0002:CO0407 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026220 CONTINUUS STANINH 1.0 01:AI:1 10.61 781.00 28:02 29.20 642.000

026221 [X[M;S;L;T;M] 38.71;TMp=38.71]

026222 [LGA=2.0;CN=75.0]

026223 [Impervious area: 1Amp=4.67;SLLP=1.00;LGA=40.0;MNP=250;SCP=0]

026224 [ARECmp=4.00;IARECmp=4.00]

026225 [SMN=33.81;SMW=225.43;SKE=010]

026226 R0002:CO0408 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026227 ADD HYD + 1.0 02:AO:M 4.14 246.00 28:01 23.49 n/a 000

026228 + 1.0 02:AO:M 0.00 0.00 28:02 0.00 n/a 000

026229 + 1.0 02:AO:M 4.14 246.00 28:01 23.49 n/a 000

026230 + 1.0 02:AO:M 10.61 781.00 28:02 29.20 n/a 000

026231 SIM + 1.0 01:MH:07 146.76 4.589.00 28:02 26.52 000

026232 R0002:CO0409 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026233 SAVE HYD 1.0 01:MH:07 146.76 4.589.00 28:02 26.52 n/a 000

026234 [name:MH07.0002]

026235 remark:Total Flow at MH07

026236 R0002:CO0410 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026237 ROUTE PIPE > 1.0 02:MH:19 146.76 4.589.00 28:02 26.52 n/a 000

026238 [RDE=1.00] out < 1.0 01:19:108 146.76 4.469.00 28:07 26.52 n/a 000

026239 [L/S=114.7/1200.013]

026240 [D=1.80;Dused=1.99]

026241 R0002:CO0411 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026242 CONTINUUS STANINH 1.0 01:AI:1 12.29 834.00 28:01 25.66 564.000

026243 [X[M;S;L;T;M] 38.71;TMp=38.71]

026244 [LGA=2.0;CN=75.0]

026245 [Impervious area: 1Amp=1.57;SLLP=1.00;LGA=183.0;NN=013;SCL=0]

026246 [ARECmp=4.00;IARECmp=4.00]

026247 [SMN=33.81;SMW=225.43;SKE=010]

026248 R0002:CO0412 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026249 COMPUTE DUALIND 1.0 02:AO:M 12.00 0.00 28:02 0.00 n/a 000

026250 Mjor System / 1.0 02:AO:M 0.00 0.00 28:02 0.00 n/a 000

026251 Mjor System \ 1.0 03:AO:M 12.29 834.00 28:01 25.66 n/a 000

026252 [MjorSystem=0.0000E+00;TotOfVol=0.0000E+00;NOf=0;TotDurOf=0.0hrs]

026253 R0002:CO0413 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026254 CONTINUUS STANINH 1.0 01:AI:2 12.29 834.00 28:01 25.66 564.000

026255 [X[M;S;L;T;M] 38.71;TMp=38.71]

026256 [LGA=2.0;CN=75.0]

026257 [Impervious area: 1Amp=4.67;SLLP=1.00;LGA=40.0;MNP=250;SCP=0]

026258 [ARECmp=4.00;IARECmp=4.00]

026259 [SMN=33.81;SMW=225.43;SKE=010]

026260 R0002:CO0414 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026261 COMPUTE DUALIND 1.0 01:AI:1 10.61 781.00 28:02 29.20 n/a 000

026262 Mjor System / 1.0 02:AO:M 12.00 0.00 28:02 0.00 n/a 000

026263 Mjor System \ 1.0 03:AO:M 10.61 781.00 28:02 29.20 n/a 000

026264 [MjorSystem=0.0000E+00;TotOfVol=0.0000E+00;NOf=0;TotDurOf=0.0hrs]

026265 R0002:CO0415 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026266 CONTINUUS STANINH 1.0 01:AI:2 12.29 834.00 28:01 25.66 564.000

026267 [X[M;S;L;T;M] 38.71;TMp=38.71]

026268 [LGA=2.0;CN=75.0]

026269 [Impervious area: 1Amp=1.57;SLLP=1.00;LGA=183.0;NN=013;SCL=0]

026270 [ARECmp=4.00;IARECmp=4.00]

026271 [SMN=33.81;SMW=225.43;SKE=010]

026272 R0002:CO0416 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026273 ROUTE PIPE > 1.0 02:MH:19 146.76 4.589.00 28:02 26.52 n/a 000

026274 [RDE=1.00] out < 1.0 01:19:116 161.64 5.396.00 28:04 26.58 n/a 000

026275 [L/S=71.7/1301.013]

026276 [D=1.80;Dused=1.99]

026277 R0002:CO0417 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026278 CONTINUUS STANINH 1.0 01:AI:1 161.64 5.363.00 28:04 26.58 n/a 000

026279 [X[M;S;L;T;M] 38.71;TMp=38.71]

026280 [LGA=2.0;CN=75.0]

026281 [Impervious area: 1Amp=4.67;SLLP=1.00;LGA=40.0;MNP=250;SCP=0]

026282 [ARECmp=4.00;IARECmp=4.00]

026283 [SMN=33.81;SMW=225.43;SKE=010]

026284 R0002:CO0418 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026285 COMPUTE DUALIND 1.0 01:AI:1 2.59 239.00 28:02 34.21 n/a 000

026286 Mjor System / 1.0 02:AO:M 2.59 239.00 28:02 34.21 n/a 000

026287 Mjor System \ 1.0 03:AO:M 2.59 239.00 28:02 34.21 n/a 000

026288 [MjorSystem=0.0000E+00;TotOfVol=0.0000E+00;NOf=0;TotDurOf=0.0hrs]

026289 R0002:CO0419 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026290 CONTINUUS STANINH 1.0 01:AI:1 2.59 239.00 28:02 34.21 534.000

026291 [X[M;S;L;T;M] 41.71;TMp=41.71]

026292 [LGA=2.0;CN=75.0]

026293 [Impervious area: 1Amp=4.67;SLLP=1.00;LGA=40.0;MNP=250;SCP=0]

026294 [ARECmp=4.00;IARECmp=4.00]

026295 [SMN=33.81;SMW=225.43;SKE=010]

026296 R0002:CO0420 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026297 ADD HYD + 1.0 02:AO:M 4.14 246.00 28:01 23.49 n/a 000

026298 + 1.0 02:AO:M 0.00 0.00 28:02 0.00 n/a 000

026299 + 1.0 02:AO:M 4.14 246.00 28:01 23.49 n/a 000

026300 + 1.0 02:AO:M 10.61 781.00 28:02 29.20 n/a 000

026301 SIM + 1.0 01:MH:08 161.64 5.450.00 28:03 26.58 n/a 000

026302 R0002:CO0421 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026303 SAVE HYD 1.0 01:MH:08 161.64 5.450.00 28:03 26.58 n/a 000

026304 [name:MH08.0002]

026305 remark:Total Flow at MH08

026306 R0002:CO0422 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026307 ROUTE PIPE > 1.0 02:MH:19 161.64 5.450.00 28:03 26.58 n/a 000

026308 [RDE=1.00] out < 1.0 01:19:116 161.64 5.396.00 28:04 26.58 n/a 000

026309 [L/S=71.7/1301.013]

026310 [D=1.80;Dused=1.99]

026311 R0002:CO0423 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026312 CONTINUUS STANINH 1.0 01:AI:2 161.64 5.363.00 28:04 26.58 n/a 000

026313 [X[M;S;L;T;M] 38.71;TMp=38.71]

026314 [LGA=2.0;CN=75.0]

026315 [Impervious area: 1Amp=1.57;SLLP=1.00;LGA=183.0;NN=013;SCL=0]

026316 [ARECmp=4.00;IARECmp=4.00]

026317 [SMN=33.81;SMW=225.43;SKE=010]

026318 R0002:CO0424 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026319 COMPUTE DUALIND 1.0 02:AO:M 16.59 3.620.00 28:02 0.00 n/a 000

026320 Mjor System / 1.0 02:AO:M 0.00 0.00 28:02 0.00 n/a 000

026321 Mjor System \ 1.0 03:AO:M 16.59 3.620.00 28:02 0.00 n/a 000

026322 [MjorSystem=0.0000E+00;TotOfVol=0.0000E+00;NOf=0;TotDurOf=0.0hrs]

026323 R0002:CO0425 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026324 CONTINUUS STANINH 1.0 01:AI:1 161.64 5.363.00 28:04 26.58 n/a 000

026325 [X[M;S;L;T;M] 38.71;TMp=38.71]

026326 [LGA=2.0;CN=75.0]

026327 [Impervious area: 1Amp=1.57;SLLP=1.00;LGA=183.0;NN=013;SCL=0]

026328 [ARECmp=4.00;IARECmp=4.00]

026329 [SMN=33.81;SMW=225.43;SKE=010]

026330 R0002:CO0426 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026331 COMPUTE DUALIND 1.0 02:AO:M 16.59 3.620.00 28:02 0.00 n/a 000

026332 Mjor System / 1.0 02:AO:M 0.00 0.00 28:02 0.00 n/a 000

026333 Mjor System \ 1.0 03:AO:M 16.59 3.620.00 28:02 0.00 n/a 000

026334 [MjorSystem=0.0000E+00;TotOfVol=0.0000E+00;NOf=0;TotDurOf=0.0hrs]

026335 R0002:CO0427 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026336 CONTINUUS STANINH 1.0 01:AI:2 161.64 5.363.00 28:04 26.58 n/a 000

026337 [X[M;S;L;T;M] 38.71;TMp=38.71]

026338 [LGA=2.0;CN=75.0]

026339 [Impervious area: 1Amp=4.67;SLLP=1.00;LGA=40.0;MNP=250;SCP=0]

026340 [ARECmp=4.00;IARECmp=4.00]

026341 [SMN=33.81;SMW=225.43;SKE=010]

026342 R0002:CO0428 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026343 ROUTE PIPE > 1.0 02:MH:19 161.64 5.450.00 28:03 26.58 n/a 000

026344 [RDE=1.00] out < 1.0 01:19:116 161.64 5.396.00 28:04 26.58 n/a 000

026345 [L/S=80.7/1301.013]

026346 [D=1.80;Dused=1.99]

026347 R0002:CO0429 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026348 CONTINUUS STANINH 1.0 01:AI:1 161.64 5.363.00 28:04 26.58 n/a 000

026349 [X[M;S;L;T;M] 38.71;TMp=38.71]

026350 [LGA=2.0;CN=75.0]

026351 [Impervious area: 1Amp=1.57;SLLP=1.00;LGA=183.0;NN=013;SCL=0]

026352 [ARECmp=4.00;IARECmp=4.00]

026353 [SMN=33.81;SMW=225.43;SKE=010]

026354 R0002:CO0430 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026355 ADD HYD + 1.0 02:AO:M 4.14 246.00 28:01 23.49 n/a 000

026356 + 1.0 02:AO:M 0.00 0.00 28:02 0.00 n/a 000

026357 + 1.0 02:AO:M 4.14 246.00 28:01 23.49 n/a 000

026358 + 1.0 02:AO:M 10.61 781.00 28:02 29.20 n/a 000

026359 SIM + 1.0 01:SN:M 55194.88 49.260.00 28:02 39.17 13.21 n/a 000

026360 R0002:CO0431 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026361 SAVE HYD 1.0 01:SN:M 55194.88 49.260.00 28:02 39.17 13.21 n/a 000

026362 [name:SN.M.0002]

026363 remark:Total Flow at JOckvale Road

026364 R0002:CO0432 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026365 ROUTE PIPE > 1.0 02:MH:19 161.64 5.450.00 28:03 26.58 n/a 000

026366 [RDE=1.00] out < 1.0 01:19:116 161.64 5.396.00 28:04 26.58 n/a 000

026367 [L/S=80.7/1301.013]

026368 [D=1.80;Dused=1.99]

026369 R0002:CO0433 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026370 CONTINUUS STANINH 1.0 01:AI:1 161.64 5.363.00 28:04 26.58 n/a 000

026371 [X[M;S;L;T;M] 38.71;TMp=38.71]

026372 [LGA=2.0;CN=75.0]

026373 [Impervious area: 1Amp=1.57;SLLP=1.00;LGA=183.0;NN=013;SCL=0]

026374 [ARECmp=4.00;IARECmp=4.00]

026375 [SMN=33.81;SMW=225.43;SKE=010]

026376 R0002:CO0434 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026377 COMPUTE DUALIND 1.0 01:AI:1 161.64 5.363.00 28:04 26.58 n/a 000

026378 Mjor System / 1.0 02:AO:M 16.59 3.620.00 28:02 0.00 n/a 000

026379 Mjor System \ 1.0 03:AO:M 16.59 3.620.00 28:02 0.00 n/a 000

026380 [MjorSystem=0.0000E+00;TotOfVol=0.0000E+00;NOf=0;TotDurOf=0.0hrs]

026381 R0002:CO0435 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026382 CONTINUUS STANINH 1.0 01:AI:2 161.64 5.363.00 28:04 26.58 n/a 000

026383 [X[M;S;L;T;M] 38.71;TMp=38.71]

026384 [LGA=2.0;CN=75.0]

026385 [Impervious area: 1Amp=1.57;SLLP=1.00;LGA=183.0;NN=013;SCL=0]

026386 [ARECmp=4.00;IARECmp=4.00]

026387 [SMN=33.81;SMW=225.43;SKE=010]

026388 R0002:CO0436 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026389 ADD HYD + 1.0 02:AO:M 4.14 246.00 28:01 23.49 n/a 000

026390 + 1.0 02:AO:M 0.00 0.00 28:02 0.00 n/a 000

026391 + 1.0 02:AO:M 4.14 246.00 28:01 23.49 n/a 000

026392 + 1.0 02:AO:M 10.61 781.00 28:02 29.20 n/a 000

026393 SIM + 1.0 01:SN:M 55194.88 49.260.00 28:02 39.17 13.21 n/a 000

026394 R0002:CO0437 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026395 SAVE HYD 1.0 01:SN:M 55194.88 49.260.00 28:02 39.17 13.21 n/a 000

026396 [name:SN.M.0002]

026397 remark:Total Flow at JOckvale Road

026398 R0002:CO0438 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026399 ROUTE PIPE > 1.0 02:MH:19 161.64 5.450.00 28:03 26.58 n/a 000

026400 [RDE=1.00] out < 1.0 01:19:116 161.64 5.396.00 28:04 26.58 n/a 000

026401 [L/S=192.7/2214.013]

026402 [D=1.80;Dused=1.99]

026403 R0002:CO0439 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026404 CONTINUUS STANINH 1.0 01:AI:1 161.64 5.363.00 28:04 26.58 n/a 000

026405 [X[M;S;L;T;M] 38.71;TMp=38.71]

026406 [LGA=2.0;CN=75.0]

026407 [Impervious area: 1Amp=1.57;SLLP=1.00;LGA=183.0;NN=013;SCL=0]

026408 [ARECmp=4.00;IARECmp=4.00]

026409 [SMN=33.81;SMW=225.43;SKE=010]

026410 R0002:CO0440 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026411 COMPUTE DUALIND 1.0 01:AI:1 161.64 5.363.00 28:04 26.58 n/a 000

026412 Mjor System / 1.0 02:AO:M 16.59 3.620.00 28:02 0.00 n/a 000

026413 Mjor System \ 1.0 03:AO:M 16.59 3.620.00 28:02 0.00 n/a 000

026414 [MjorSystem=0.0000E+00;TotOfVol=0.0000E+00;NOf=0;TotDurOf=0.0hrs]

026415 R0002:CO0441 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026416 CONTINUUS STANINH 1.0 01:AI:2 161.64 5.363.00 28:04 26.58 n/a 000

026417 [X[M;S;L;T;M] 38.71;TMp=38.71]

026418 [LGA=2.0;CN=75.0]

026419 [Impervious area: 1Amp=1.57;SLLP=1.00;LGA=183.0;NN=013;SCL=0]

026420 [ARECmp=4.00;IARECmp=4.00]

026421 [SMN=33.81;SMW=225.43;SKE=010]

026422 R0002:CO0442 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026423 ROUTE PIPE > 1.0 02:MH:19 161.64 5.450.00 28:03 26.58 n/a 000

026424 [RDE=1.00] out < 1.0 01:19:116 161.64 5.396.00 28:04 26.58 n/a 000

026425 [L/S=144.1/1200.013]

026426 [D=1.80;Dused=1.99]

026427 R0002:CO0443 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026428 CONTINUUS STANINH 1.0 01:AI:1 161.64 5.363.00 28:04 26.58 n/a 000

026429 [X[M;S;L;T;M] 38.71;TMp=38.71]

026430 [LGA=2.0;CN=75.0]

026431 [Impervious area: 1Amp=1.57;SLLP=1.00;LGA=183.0;NN=013;SCL=0]

026432 [ARECmp=4.00;IARECmp=4.00]

026433 [SMN=33.81;SMW=225.43;SKE=010]

026434 R0002:CO0444 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026435 ADD HYD + 1.0 02:AO:M 4.14 246.00 28:01 23.49 n/a 000

026436 + 1.0 02:AO:M 0.00 0.00 28:02 0.00 n/a 000

026437 + 1.0 02:AO:M 4.14 246.00 28:01 23.49 n/a 000

026438 + 1.0 02:AO:M 10.61 781.00 28:02 29.20 n/a 000

026439 SIM + 1.0 01:SN:M 55194.88 49.260.00 28:02 39.17 13.21 n/a 000

026440 R0002:CO0445 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026441 SAVE HYD 1.0 01:SN:M 55194.88 49.260.00 28:02 39.17 13.21 n/a 000

026442 [name:SN.M.0002]

026443 remark:Total Flow at JOckvale Road

026444 R0002:CO0446 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026445 ROUTE PIPE > 1.0 02:MH:19 161.64 5.450.00 28:03 26.58 n/a 000

026446 [RDE=1.00] out < 1.0 01:19:116 161.64 5.396.00 28:04 26.58 n/a 000

026447 [L/S=192.7/2214.013]

026448 [D=1.80;Dused=1.99]

026449 R0002:CO0447 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026450 CONTINUUS STANINH 1.0 01:AI:1 161.64 5.363.00 28:04 26.58 n/a 000

026451 [X[M;S;L;T;M] 38.71;TMp=38.71]

026452 [LGA=2.0;CN=75.0]

026453 [Impervious area: 1Amp=1.57;SLLP=1.00;LGA=183.0;NN=013;SCL=0]

026454 [ARECmp=4.00;IARECmp=4.00]

026455 [SMN=33.81;SMW=225.43;SKE=010]

026456 R0002:CO0448 [AREA:QPEAKm;TpeakDte;hh:mm;Rvmm;R.C.;DFWm]

026457 COMPUTE DUALIND 1.0 02:AO:M 16.59 3.620.00 28:02 0.00 n/a 000

026458 Mjor System / 1.0 02:AO:M 0.00 0.00 28:02 0.00 n/a 000</

Table with columns for node ID, description, and various data points. Rows include detailed hydrograph data for various nodes (e.g., 029983, 029984, 029985) and summary statistics for different subwatersheds and reservoirs.

Table containing engineering data with columns for ID, description, coordinates (Easting, Northing, Elevation), and various parameters. The table is split into two columns across the page.

Table with columns for item ID, name/description, type, and various numerical data points. The table is organized into several vertical sections with headers like [SMN 33.81; SWM0225.43; SKG 010] and [Dn 1.80; Daved=1.85]. Each entry includes details such as 'AREA=AREA', 'QPEAK=QPEAK', and 'TPEAK=DATE'. It covers a wide range of infrastructure items from 'CONTINUS STANDBY' to 'ROTE PIPE' and 'HYDRAULIC MODEL'.

059855 # (Approximated cross section - see cross section 258)
059856 # Use method for spring conditions and set out 025 for spring conditions
059857 #
059858 # Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
059859 #
059900 ROUTE010: C00038 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
059901 ROUTE CHANNEL >> 1.0 02:S_N2 9506.00 12.534 No date 22:45 19.65 n/a 0.000
059902 [RDE 1.00] out < 1.0 01:N1 9506.00 12.710 No date 33:02 19.65 n/a 0.000
059903 [L/S in 182.7 / 0547.040]
059904 [Vmax = 680.0; Dmax = 2.98]
059905 #
059906 # Addition of Subwatershed 11 and No Name Creek to Node 11
059907 #
059908 ROUTE010: C00039 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
059909 ADD HYD + 1.0 02: NDD 9506.00 12.710 No date 33:02 19.65 n/a 0.000
060000 + 1.0 02: SW10 500.00 5.639 No date 29:22 21.19 n/a 0.000
060001 + 1.0 02: NC CK 1917.00 7.897 No date 34:28 21.19 n/a 0.000
060002 SIMM + 1.0 01: S_N1 11923.00 21.813 No date 33:05 19.96 n/a 0.000
060003 #
060004 # Sum of hydrographs from Node 11 routed to Node 10
060005 # Section 7
060006 ROUTE010: C00040 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
060007 ROUTE CHANNEL >> 1.0 02: S_N1 11923.00 21.813 No date 33:05 19.96 n/a 0.000
060008 [RDE 1.00] out < 1.0 01: N0 11923.00 14.761 No date 39:58 19.96 n/a 0.000
060009 [L/S in 4028.7 / 1571.040]
060010 [Vmax = 452.0; Dmax = 1.212]
060011 #
060012 # Addition of Subwatershed 10 to Node 10
060013 #
060014 ROUTE010: C00041 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
060015 ADD HYD + 1.0 02: NDD 11923.00 14.761 No date 39:58 19.96 n/a 0.000
060016 + 1.0 02: SW10 3066.00 21.255 No date 37:58 24.81 n/a 0.000
060017 SIMM + 1.0 01: S_N0 17589.00 35.808 No date 38:35 21.52 n/a 0.000
060018 [Vmax = 478.0; Dmax = 2.42]
060019 ROUTE010: C00042 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
060020 SAVE HYD 1.0 01: S_N0 17589.00 35.808 No date 38:35 21.52 n/a 0.000
060021 frame : H_SND0
060022 remark: flow at S_N0: N0 + SW10
060023 # Addition of Kings Creek to S_N10
060024 #
060025 ROUTE010: C00043 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
060026 ADD HYD + 1.0 02: NDD 17589.00 35.808 No date 38:35 21.52 n/a 0.000
060027 + 1.0 02: NC CK 8376.00 20.598 No date 39:59 21.19 n/a 0.000
060028 SIMM + 1.0 01: S_N10 25965.00 55.807 No date 39:58 21.41 n/a 0.000
060029 #
060030 # Sum of hydrographs from Node 10 routed to Node 9
060031 # Section 7
060032 #
060033 ROUTE010: C00044 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
060034 ROUTE CHANNEL >> 1.0 02: S_N0A 25965.00 55.807 No date 39:59 21.41 n/a 0.000
060035 [RDE 1.00] out < 1.0 01: N0 25965.00 54.076 No date 39:59 21.41 n/a 0.000
060036 [L/S in 3082.7 / 0740.400]
060037 [Vmax = 682.0; Dmax = 1.095]
060038 #
060039 # Addition of Subwatershed 9 and Nichols Creek to Node 9
060040 #
060041 ROUTE010: C00045 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
060042 ADD HYD + 1.0 02: NDD 25965.00 54.076 No date 39:59 21.41 n/a 0.000
060043 + 1.0 02: SW10 1132.00 8.921 No date 30:54 23.73 n/a 0.000
060044 + 1.0 02: NC CK 4664.00 10.128 No date 39:59 19.29 n/a 0.000
060045 SIMM + 1.0 01: S_N0 31561.00 66.284 No date 39:59 21.20 n/a 0.000
060046 #
060047 # Sum of hydrographs from Node 9 routed to Node 8
060048 # Section 7
060049 #
060050 ROUTE010: C00046 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
060051 ROUTE CHANNEL >> 1.0 02: S_N 31561.00 66.284 No date 39:59 21.20 n/a 0.000
060052 [RDE 1.00] out < 1.0 01: N0 31561.00 61.483 No date 39:57 21.20 n/a 0.000
060053 [L/S in 2209.0 / 0847.440]
060054 [Vmax = 363.0; Dmax = 1.619]
060055 #
060056 # Addition of Subwatershed 8 and Hobb's Drain to Node 8
060057 #
060058 ROUTE010: C00047 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
060059 ADD HYD + 1.0 02: NDD 31561.00 61.483 No date 39:57 21.20 n/a 0.000
060060 + 1.0 02: SW10 131.00 1.689 No date 30:54 23.73 n/a 0.000
060061 + 1.0 02: NC CK 3854.00 11.813 No date 39:57 21.19 n/a 0.000
060062 SIMM + 1.0 01: S_N0 35546.00 73.344 No date 39:57 21.19 n/a 0.000
060063 #
060064 # Sum of hydrographs from Node 8 routed to Node 7
060065 # Section 4
060066 #
060067 ROUTE010: C00048 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
060068 ROUTE CHANNEL >> 1.0 02: S_N 35546.00 73.344 No date 39:57 21.19 n/a 0.000
060069 [RDE 1.00] out < 1.0 01: N0 35546.00 61.416 No date 45:01 21.19 n/a 0.000
060070 [L/S in 3750.7 / 0517.070]
060071 [Vmax = 218.0; Dmax = 1.987]
060072 #
060073 # Addition of Subwatershed 7 to Node 7
060074 #
060075 ROUTE010: C00049 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
060076 ADD HYD + 1.0 02: NDD 35546.00 61.416 No date 45:01 21.19 n/a 0.000
060077 + 1.0 02: SW7 3197.00 8.899 No date 36:26 17.07 n/a 0.000
060078 SIMM + 1.0 01: S_N 38743.00 65.819 No date 44:06 20.85 n/a 0.000
060079 [Vmax = 405.0; Dmax = 2.09]
060080 ROUTE010: C00050 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
060081 SAVE HYD 1.0 01: S_N 38743.00 65.819 No date 44:06 20.85 n/a 0.000
060082 frame : H_SND0
060083 remark: flow at S_N: N0 + SW7
060084 # Insertion of a reservoir to simulate the effects of the Richmond Fen.
060085 # Storage area and volumes were estimated from available topography.
060086 # Release rate from Fen was assumed to be controlled by the downstream
060087 # river cross section for summer conditions. It is assumed that for up to
060088 # 0.75 m of water, the main channel of the river provided the storage. Above
060089 # this depth, the wetland starts to significantly store water.
060090 #
060091 ROUTE010: C00051 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
060092 ROUTE RESERVOIR >> 1.0 01: RES_RF 38743.00 31.796 No date 60:32 20.85 n/a 0.000
060093 [M&S elev. elev. 259710.0]
060094 ROUTE010: C00052 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
060095 SAVE HYD 1.0 01: RES_RF 38743.00 31.796 No date 60:32 20.85 n/a 0.000
060096 frame : H_ResRF
060097 remark: outflow from Richmond Fen
060098 #
060099 # Sum of hydrographs from Node 7 routed to Node 6
060100 # Section 7
060101 #
060102 ROUTE010: C00053 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
060103 ROUTE CHANNEL >> 1.0 02: RES_RF 38743.00 31.796 No date 60:32 20.85 n/a 0.000
060104 [RDE 1.00] out < 1.0 01: N6 38743.00 31.737 No date 62:00 20.85 n/a 0.000
060105 [L/S in 1852.7 / 0837.040]
060106 [Vmax = 477.0; Dmax = 960]
060107 #
060108 # Addition of Subwatershed 6 and Van Gaal Drain to Node 6
060109 #
060110 ROUTE010: C00054 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
060111 ADD HYD + 1.0 02: N6 38743.00 31.737 No date 62:00 20.85 n/a 0.000
060112 + 1.0 02: SW5 224.00 2.546 No date 28:45 28.24 n/a 0.000
060113 + 1.0 02: ML CK 1332.00 6.069 No date 35:17 24.81 n/a 0.000
060114 SIMM + 1.0 01: S_N 40240.00 31.737 No date 62:00 20.99 n/a 0.000
060115 #
060116 # Sum of hydrographs from Node 6 routed to Node 5
060117 # Section 6
060118 #
060119 ROUTE010: C00055 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
060120 ROUTE CHANNEL >> 1.0 02: S_N 40240.00 31.737 No date 62:00 20.99 n/a 0.000
060121 [RDE 1.00] out < 1.0 01: N5 40240.00 31.713 No date 62:48 20.99 n/a 0.000
060122 [L/S in 1852.7 / 0547.040]
060123 [Vmax = 412.0; Dmax = 1.069]
060124 #
060125 # Addition of Subwatershed 5 and Flowing Creek to Node 5
060126 #
060127 ROUTE010: C00056 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
060128 ADD HYD + 1.0 02: N5 40240.00 31.713 No date 62:48 20.99 n/a 0.000
060129 + 1.0 02: SW4 224.00 2.546 No date 28:45 28.24 n/a 0.000
060130 + 1.0 02: PL CK 4945.00 28.945 No date 33:21 25.91 n/a 0.000
060131 SIMM + 1.0 01: S_N 45409.00 51.448 No date 34:54 21.56 n/a 0.000
060132 #
060133 # Sum of hydrographs from Node 5 routed to Node 5A
060134 # Section 7
060135 #
060136 ROUTE010: C00057 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
060137 ROUTE CHANNEL >> 1.0 02: S_N 45409.00 51.448 No date 34:54 21.56 n/a 0.000
060138 [RDE 1.00] out < 1.0 01: N5A 45409.00 51.312 No date 35:12 21.56 n/a 0.000
060139 [L/S in 556.7 / 0907.040]
060140 [Vmax = 485.0; Dmax = 1.131]
060141 #
060142 # Addition of Subwatershed 5A and Subwatershed 5A2 to Node 5A
060143 #
060144 ROUTE010: C00058 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
060145 ADD HYD + 1.0 02: N5 45409.00 51.312 No date 35:12 21.56 n/a 0.000
060146 + 1.0 02: SW4 585.00 8.458 No date 29:57 31.37 n/a 0.000
060147 + 1.0 02: ML CK 1021.00 11.195 No date 30:48 30.72 n/a 0.000
060148 SIMM + 1.0 02: SW5A 1412.00 5.817 No date 37:54 27.06 n/a 0.000
060149 [Vmax = 484.0; Dmax = 4644.0] 46.788 No date 35:22 21.73 n/a 0.000
060150 #
060151 # Sum of hydrographs from Node 5A routed to Node 4
060152 # Section 8
060153 #
060154 ROUTE010: C00059 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
060155 ROUTE CHANNEL >> 1.0 02: S_NA 46481.00 56.788 No date 35:22 21.73 n/a 0.000
060156 [RDE 1.00] out < 1.0 01: N4 46481.00 54.543 No date 36:56 21.73 n/a 0.000
060157 [L/S in 4630.7 / 0437.050]
060158 [Vmax = 793.0; Dmax = 3.295]
060159 #
060160 # Addition of Subwatershed 4 and Leamy Creek to Node 4
060161 #
060162 ROUTE010: C00060 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
060163 ADD HYD + 1.0 02: N4 46481.00 54.543 No date 36:56 21.73 n/a 0.000
060164 + 1.0 02: SW4 585.00 8.458 No date 29:57 31.37 n/a 0.000
060165 + 1.0 02: ML CK 1021.00 11.195 No date 30:48 30.72 n/a 0.000
060166 SIMM + 1.0 02: SW5A 1412.00 5.817 No date 37:54 27.06 n/a 0.000
060167 [Vmax = 793.0; Dmax = 4648.0] 46.788 No date 35:22 21.73 n/a 0.000
060168 #
060169 # Sum of hydrographs from Node 4 routed to Node 2
060170 #
060171 #
061725 # Section 9
061726 #
061744 ROUTE010: C00062 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
061745 ROUTE CHANNEL >> 1.0 02: S_N2 48447.00 59.934 No date 36:12 22.03 n/a 0.000
061746 [RDE 1.00] out < 1.0 01: N2 48447.00 59.699 No date 36:35 22.03 n/a 0.000
061747 [L/S in 1867.7 / 0607.040]
061748 [Vmax = 824.0; Dmax = 325]
061749 #
061800 # Addition of Subwatershed 2 with Mnohan Drain and Smith Drain to Node 2
061801 #
061802 ROUTE010: C00063 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
061803 ADD HYD + 1.0 02: N2 48447.00 59.699 No date 36:35 22.03 n/a 0.000
061804 + 1.0 02: SW2 177.00 4.146 No date 28:45 28.24 n/a 0.000
061805 + 1.0 02: SM LR 1122.00 10.275 No date 31:46 31.37 n/a 0.000
061806 + 1.0 02: MD LR 2737.00 22.669 No date 31:32 27.64 n/a 0.000
061807 SIMM + 1.0 01: S_N2 52483.00 83.235 No date 33:15 22.55 n/a 0.000
061808 ROUTE010: C00064 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
061809 SAVE HYD 1.0 01: S_N2 52483.00 83.235 No date 33:15 22.55 n/a 0.000
061810 frame : H_SND0
061811 remark: flow at S_N2 Lock River Gauge at Modoc Dr.
061812 #
061925 # Sum of hydrographs from Node 2 routed to Node 1
061926 # Section 10
061927 #
061935 # Hydrograph from Node 2 routed to Node 416
061936 # Channel X Section obtained from RVCA Hydraulic Model - Station 9025
062000 #
062001 ROUTE010: C00065 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
062002 ROUTE CHANNEL >> 1.0 02: S_N2 52483.00 83.235 No date 33:15 22.55 n/a 0.000
062003 [RDE 1.00] out < 1.0 01: N416 52483.00 81.216 No date 34:18 22.55 n/a 0.000
062004 [L/S in 3227.7 / 0507.050]
062005 [Vmax = 705.0; Dmax = 2.943]
062006 #
062070 # Catchment SW1a
062071 # Portion of RVCA catchment SW1 outside of Reach 1 subwatershed
062072 # Under open agricultural land
062073 #
062120 ROUTE010: C00066 >> Dfln-ID NDD >>> AREAA-QPEAKm-TpeakDate-hh:mm-Rvmm R C...DWFCm
062121 CONTINUOUS STANHDID >> 1.0 01: S1a 536.42 3.888 No date 31:17 23.57 364 000
062122 [CN 54.0 No 3.00; Top 60]
062123 [LGRS 2 CN= 61.0]
062124 [Impervious area: LAmp = 1.57; SLPI = 38; LG = 1450; MM = 0.13; SCL = 0]
062125 [Previous area: APerv = 4.67; SLLP = 32; LGR = 440; MM = 0.15; SCP = 0]
062126 [LGRS 2 CN= 75.0]
062127 [LGRS 2 CN= 75.0]
062128 [Impervious area: LAmp = 1.57; SLPI = 38; LG = 1450; MM = 0.13; SCL = 0]
062129 [Previous area: APerv = 4.67; SLLP = 32; LGR = 440; MM = 0.15; SCP = 0]
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062296 [LGRS 2 CN= 75.0]
062297 [LGRS 2 CN= 75.0]
062298 [LGRS 2 CN= 75.0]
062299 [

06359# R010: CO091#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06360# ROUTE RESERVOIR > 1.0 02: AEA 66.75 6.470 N date 28 10 48.24 n/a 000
06361# overFlow < 1.0 01: ST5TRF 59 052 N date 28 05 38.69 n/a 000
06362# [MSStkEds:1835E-02 m, TotOfVol=0.0000E+00 mb, NcOf=0, TotDirOf=0 h.rs]
06363# [InterEvent Time=12.00]
06364# R010: CO111#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06365# CONTI NUOS STANdHD 1.0 01: A7 587.2 N date 29 04 22.40 346 000
06366# [XfM: 68.7fM: 85]
06367# [InterEvent Time=12.00]
06368# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06369# [Impervious area: IApr= 1.57:SLPI= 50:LD= 180:MM= 013:SCI= 0]
06370# [IAREg m= 4.00: IAREgP= 4.00]
06371# ROUTE RESERVOIR > 1.0 02: A7 60.55 852 N date 29 08 22.40 n/a 000
06372# [RDfE: 1.00] out < 1.0 01: BRPIPE 60.55 852 N date 29 08 22.40 n/a 000
06373# [L/SA= 525 / 230] 043]
06374# [IAREg m= 4.00: IAREgP= 4.00]
06375# R010: CO104#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06376# ADD HYD 261.31 2.972 N date 28 31 17.14 n/a 000
06377# + 1.0 02: IRDANI 658.24 N date 28 25 38.69 n/a 000
06378# + 1.0 02: AI STR 2.50 098 N date 28 24 50.29 n/a 000
06379# + 1.0 02: ST6 OF 1.51 039 N date 28 10 20.0 n/a 000
06380# + 1.0 02: ST5TRF 59 052 N date 28 05 38.69 n/a 000
06381# + 1.0 02: ST2TOF 0.0 000 N date 0.00 0.00 n/a 000
06382# + 1.0 02: BRPIPE 60.55 852 N date 29 08 22.40 n/a 000
06383# SLIM 3.76 3.771 N date 28 40 18.45 n/a 000
06384# R010: CO109#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06385# CONTI NUOS STANdHD 1.0 01: A7 3.51 538 N date 28 01 50.29 777 000
06386# [XfM: 68.7fM: 85]
06387# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06388# [Impervious area: IApr= 1.57:SLPI= 50:LD= 180:MM= 013:SCI= 0]
06389# [IAREg m= 4.00: IAREgP= 4.00]
06390# ROUTE RESERVOIR > 1.0 02: A7 3.51 538 N date 28 01 50.29 n/a 000
06391# overFlow < 1.0 01: ST5TRF 3.51 538 N date 28 01 50.29 n/a 000
06392# [MSStkEds:8167E-01 mb, TotOfVol=0.0000E+00 mb, NcOf=0, TotDirOf=0 h.rs]
06393# [InterEvent Time=12.00]
06394# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06395# [Impervious area: IApr= 1.57:SLPI= 50:LD= 119:MM= 013:SCI= 0]
06396# [IAREg m= 4.00: IAREgP= 4.00]
06397# R010: CO109#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06398# CONTI NUOS STANdHD 1.0 01: ST-6 71 089 N date 28 00 38.69 598 000
06399# [XfM: 68.7fM: 85]
06400# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06401# [Impervious area: IApr= 1.57:SLPI= 50:LD= 119:MM= 013:SCI= 0]
06402# [IAREg m= 4.00: IAREgP= 4.00]
06403# R010: CO109#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06404# ROUTE RESERVOIR > 1.0 02: ST-6 71 089 N date 28 00 38.69 n/a 000
06405# overFlow < 1.0 02: ST2TOF 0.0 000 N date 0.00 0.00 n/a 000
06406# [MSStkEds:1988E-02 m, TotOfVol=0.0000E+00 mb, NcOf=0, TotDirOf=0 h.rs]
06407# [InterEvent Time=12.00]
06408# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06409# [Impervious area: IApr= 1.57:SLPI= 50:LD= 491:MM= 013:SCI= 0]
06410# [IAREg m= 4.00: IAREgP= 4.00]
06411# ROUTE RESERVOIR > 1.0 02: A7 326.12 3.771 N date 28 40 18.45 n/a 000
06412# + 1.0 02: AI STR 67.59 539 N date 28 25 50.29 n/a 000
06413# + 1.0 02: ST6 OF 0.0 000 N date 0.00 0.00 n/a 000
06414# + 1.0 02: ST5TRF 71 039 N date 28 10 20.0 n/a 000
06415# + 1.0 02: ST3TOF 0.0 000 N date 0.00 0.00 n/a 000
06416# SLIM 3.30 3.914 N date 28 39 18.83 n/a 000
06417# R010: CO100#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06418# ROUTE CHANNEL > 1.0 02: P1ST5T 330.34 3.914 N date 28 39 18.83 n/a 000
06419# [RDfE: 1.00] out < 1.0 01: BRDND 330.34 3.914 N date 29 01 88.3 n/a 000
06420# [L/SA= 592 / 230] 043]
06421# [IAREg m= 4.00: IAREgP= 4.00]
06422# R010: CO101#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06423# CONTI NUOS STANdHD 1.0 01: D2 2.28 046 N date 29 04 29.30 453 000
06424# [XfM: 68.7fM: 85]
06425# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06426# [Impervious area: IApr= 1.57:SLPI= 50:LD= 162:MM= 013:SCI= 0]
06427# [IAREg m= 4.00: IAREgP= 4.00]
06428# R010: CO102#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06429# CONTI NUOS STANdHD 1.0 01: A7 12.04 1.618 N date 28 04 50.29 777 000
06430# [XfM: 68.7fM: 85]
06431# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06432# [Impervious area: IApr= 1.57:SLPI= 50:LD= 491:MM= 013:SCI= 0]
06433# [IAREg m= 4.00: IAREgP= 4.00]
06434# R010: CO103#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06435# ROUTE RESERVOIR > 1.0 02: A7 12.04 1.618 N date 28 04 50.29 n/a 000
06436# overFlow < 1.0 01: A7OVP 0.0 000 N date 0.00 0.00 n/a 000
06437# [MSStkEds:2771E+00 mb, TotOfVol=0.0000E+00 mb, NcOf=0, TotDirOf=0 h.rs]
06438# [InterEvent Time=12.00]
06439# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06440# [Impervious area: IApr= 1.57:SLPI= 50:LD= 491:MM= 013:SCI= 0]
06441# [IAREg m= 4.00: IAREgP= 4.00]
06442# R010: CO105#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06443# ROUTE RESERVOIR > 1.0 02: A7 35 046 N date 28 00 38.69 n/a 000
06444# overFlow < 1.0 02: ST4TOF 0.0 000 N date 0.00 0.00 n/a 000
06445# [MSStkEds:1432E+00 mb, TotOfVol=0.0000E+00 mb, NcOf=0, TotDirOf=0 h.rs]
06446# [InterEvent Time=12.00]
06447# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06448# [Impervious area: IApr= 1.57:SLPI= 50:LD= 491:MM= 013:SCI= 0]
06449# [IAREg m= 4.00: IAREgP= 4.00]
06450# R010: CO106#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06451# CONTI NUOS STANdHD 1.0 01: A8 5.30 780 N date 28 02 50.29 777 000
06452# [XfM: 68.7fM: 85]
06453# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06454# [Impervious area: IApr= 1.57:SLPI= 50:LD= 326:MM= 013:SCI= 0]
06455# [IAREg m= 4.00: IAREgP= 4.00]
06456# R010: CO107#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06457# ROUTE RESERVOIR > 1.0 02: A8 5.30 780 N date 28 02 50.29 n/a 000
06458# overFlow < 1.0 01: A8OVP 0.0 000 N date 0.00 0.00 n/a 000
06459# [MSStkEds:232E+00 mb, TotOfVol=0.0000E+00 mb, NcOf=0, TotDirOf=0 h.rs]
06460# [InterEvent Time=12.00]
06461# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06462# [Impervious area: IApr= 1.57:SLPI= 50:LD= 491:MM= 013:SCI= 0]
06463# [IAREg m= 4.00: IAREgP= 4.00]
06464# R010: CO108#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06465# ADD HYD 2.28 046 N date 29 04 29.30 n/a 000
06466# + 1.0 02: AI STR 12.04 040 N date 28 31 50.29 n/a 000
06467# + 1.0 02: ST6 OF 0.0 000 N date 0.00 0.00 n/a 000
06468# + 1.0 02: ST5TRF 35 031 N date 28 04 38.69 n/a 000
06469# + 1.0 02: ST4TOF 0.0 000 N date 0.00 0.00 n/a 000
06470# + 1.0 02: AI STR 5.30 206 N date 28 27 50.29 n/a 000
06471# SLIM 3.50 3.413 N date 28 27 50.29 n/a 000
06472# R010: CO109#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06473# ROUTE CHANNEL > 1.0 02: P1ST5T 350.31 3.413 N date 28 27 50.29 n/a 000
06474# [RDfE: 1.00] out < 1.0 01: BRDND 350.31 3.413 N date 29 17 20.48 n/a 000
06475# [L/SA= 525 / 230] 043]
06476# [IAREg m= 4.00: IAREgP= 4.00]
06477# R010: CO110#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06478# CONTI NUOS STANdHD 1.0 01: D2 7.59 759 N date 28 11 49.05 758 000
06479# [XfM: 68.7fM: 85]
06480# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06481# [Impervious area: IApr= 1.57:SLPI= 50:LD= 1230:MM= 013:SCI= 0]
06482# [IAREg m= 4.00: IAREgP= 4.00]
06483# R010: CO111#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06484# ROUTE RESERVOIR > 1.0 02: ST-6 7.59 759 N date 28 11 49.05 n/a 000
06485# overFlow < 1.0 01: ST5TRF 7.59 759 N date 28 11 49.05 n/a 000
06486# [MSStkEds:1525E-02 m, TotOfVol=0.0000E+00 mb, NcOf=0, TotDirOf=0 h.rs]
06487# [InterEvent Time=12.00]
06488# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06489# [Impervious area: IApr= 1.57:SLPI= 50:LD= 95:MM= 013:SCI= 0]
06490# [IAREg m= 4.00: IAREgP= 4.00]
06491# R010: CO112#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06492# ROUTE RESERVOIR > 1.0 02: ST-6 3.41 133 N date 28 25 50.29 n/a 000
06493# overFlow < 1.0 01: CI STR 3.41 133 N date 28 25 50.29 n/a 000
06494# [MSStkEds:7930E-01 mb, TotOfVol=0.0000E+00 mb, NcOf=0, TotDirOf=0 h.rs]
06495# [InterEvent Time=12.00]
06496# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06497# [Impervious area: IApr= 1.57:SLPI= 50:LD= 491:MM= 013:SCI= 0]
06498# [IAREg m= 4.00: IAREgP= 4.00]
06499# R010: CO113#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06500# CONTI NUOS STANdHD 1.0 01: ST-5 45 058 N date 28 00 38.69 598 000
06501# [XfM: 68.7fM: 85]
06502# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06503# [Impervious area: IApr= 1.57:SLPI= 50:LD= 95:MM= 013:SCI= 0]
06504# [IAREg m= 4.00: IAREgP= 4.00]
06505# R010: CO115#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06506# ADD HYD 350.31 4.037 N date 29 17 20.48 n/a 000
06507# + 1.0 02: AI STR 3.41 133 N date 28 25 50.29 n/a 000
06508# + 1.0 02: CI STR 3.41 133 N date 28 25 50.29 n/a 000
06509# + 1.0 02: CI STR 3.41 133 N date 28 25 50.29 n/a 000
06510# + 1.0 02: CL OF 0.0 000 N date 0.00 0.00 n/a 000
06511# + 1.0 02: ST5TRF 45 058 N date 28 00 38.69 n/a 000
06512# SLIM 356.68 4.181 N date 29 15 20.87 n/a 000
06513# R010: CO116#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06514# CONTI NUOS STANdHD 1.0 01: STRAND 7.59 759 N date 28 11 49.05 758 000
06515# [XfM: 68.7fM: 85]
06516# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06517# [Impervious area: IApr= 1.57:SLPI= 50:LD= 1230:MM= 013:SCI= 0]
06518# [IAREg m= 4.00: IAREgP= 4.00]
06519# R010: CO117#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06520# ROUTE RESERVOIR > 1.0 02: STRAND 7.59 759 N date 28 11 49.05 n/a 000
06521# overFlow < 1.0 01: ST2TOF 7.59 759 N date 28 11 49.05 n/a 000
06522# [MSStkEds:5930E+00 mb, TotOfVol=0.0000E+00 mb, NcOf=0, TotDirOf=0 h.rs]
06523# [InterEvent Time=12.00]
06524# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06525# [Impervious area: IApr= 1.57:SLPI= 50:LD= 491:MM= 013:SCI= 0]
06526# [IAREg m= 4.00: IAREgP= 4.00]
06527# R010: CO118#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06528# ADD HYD 356.68 4.181 N date 29 15 20.87 n/a 000
06529# + 1.0 02: ST-6 356.68 4.181 N date 29 15 20.87 n/a 000
06530# + 1.0 02: AI STR 3.41 133 N date 28 25 50.29 n/a 000
06531# SLIM 364.27 4.242 N date 29 15 20.87 n/a 000
06532# R010: CO119#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06533# CONTI NUOS STANdHD 1.0 01: SNAKUT 364.27 4.242 N date 29 15 21.45 n/a 000
06534# [XfM: 68.7fM: 85]
06535# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06536# [Impervious area: IApr= 1.57:SLPI= 50:LD= 145:MM= 013:SCI= 0]
06537# [IAREg m= 4.00: IAREgP= 4.00]
06538# R010: CO120#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06539# CONTI NUOS STANdHD 1.0 01: Aea-A 66.75 6.470 N date 28 10 48.24 746 000
06540# [XfM: 68.7fM: 85]
06541# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06542# [Impervious area: IApr= 1.57:SLPI= 50:LD= 145:MM= 013:SCI= 0]
06543# [IAREg m= 4.00: IAREgP= 4.00]
06544# R010: CO121#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06545# SAVE HYD 66.75 6.470 N date 28 10 48.24 n/a 000
06546# [XfM: 68.7fM: 85]
06547# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06548# [Impervious area: IApr= 1.57:SLPI= 50:LD= 180:MM= 013:SCI= 0]
06549# [IAREg m= 4.00: IAREgP= 4.00]
06550# R010: CO122#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06551# ROUTE RESERVOIR > 1.0 02: AEA-A 66.75 6.470 N date 28 10 48.24 n/a 000
06552# overFlow < 1.0 01: SWMOW 0.0 000 N date 0.00 0.00 n/a 000
06553# [MSStkEds:2350E+00 mb, TotOfVol=0.0000E+00 mb, NcOf=0, TotDirOf=0 h.rs]
06554# [InterEvent Time=12.00]
06555# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06556# [Impervious area: IApr= 1.57:SLPI= 50:LD= 180:MM= 013:SCI= 0]
06557# [IAREg m= 4.00: IAREgP= 4.00]
06558# R010: CO123#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06559# CONTI NUOS STANdHD 1.0 01: C6 1.87 301 N date 28 01 50.29 777 000
06560# [XfM: 68.7fM: 85]
06561# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06562# [Impervious area: IApr= 1.57:SLPI= 50:LD= 180:MM= 013:SCI= 0]
06563# [IAREg m= 4.00: IAREgP= 4.00]
06564# R010: CO125#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06565# ROUTE RESERVOIR > 1.0 02: C6 1.87 301 N date 28 01 50.29 n/a 000
06566# overFlow < 1.0 01: PT5ST 431.02 4.657 N date 29 18 25.00 n/a 000
06567# [MSStkEds:4578E-02 m, TotOfVol=0.0000E+00 mb, NcOf=0, TotDirOf=0 h.rs]
06568# [InterEvent Time=12.00]
06569# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06570# [Impervious area: IApr= 1.57:SLPI= 50:LD= 180:MM= 013:SCI= 0]
06571# [IAREg m= 4.00: IAREgP= 4.00]
06572# R010: CO127#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06573# CONTI NUOS STANdHD 1.0 01: C7 1.62 262 N date 28 01 50.29 777 000
06574# [XfM: 68.7fM: 85]
06575# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06576# [Impervious area: IApr= 1.57:SLPI= 50:LD= 180:MM= 013:SCI= 0]
06577# [IAREg m= 4.00: IAREgP= 4.00]
06578# R010: CO128#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06579# ROUTE RESERVOIR > 1.0 02: C7 1.62 262 N date 28 01 50.29 n/a 000
06580# overFlow < 1.0 02: ST STR 4.1 053 N date 28 00 38.69 n/a 000
06581# [MSStkEds:378E-01 mb, TotOfVol=0.0000E+00 mb, NcOf=0, TotDirOf=0 h.rs]
06582# [InterEvent Time=12.00]
06583# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06584# [Impervious area: IApr= 1.57:SLPI= 50:LD= 91:MM= 013:SCI= 0]
06585# [IAREg m= 4.00: IAREgP= 4.00]
06586# R010: CO130#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06587# CONTI NUOS STANdHD 1.0 01: ST-6 41 053 N date 28 00 38.69 598 000
06588# [XfM: 68.7fM: 85]
06589# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06590# [Impervious area: IApr= 1.57:SLPI= 50:LD= 91:MM= 013:SCI= 0]
06591# [IAREg m= 4.00: IAREgP= 4.00]
06592# R010: CO131#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06593# ROUTE RESERVOIR > 1.0 02: ST-6 41 053 N date 28 00 38.69 n/a 000
06594# overFlow < 1.0 03: ST5TOF 0.0 000 N date 0.00 0.00 n/a 000
06595# [MSStkEds:1544E-02 m, TotOfVol=0.0000E+00 mb, NcOf=0, TotDirOf=0 h.rs]
06596# [InterEvent Time=12.00]
06597# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06598# [Impervious area: IApr= 1.57:SLPI= 50:LD= 91:MM= 013:SCI= 0]
06599# [IAREg m= 4.00: IAREgP= 4.00]
06600# R010: CO132#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06601# ADD HYD 431.02 4.657 N date 29 18 25.00 n/a 000
06602# + 1.0 02: PT4ST 431.02 4.657 N date 29 18 25.00 n/a 000
06603# + 1.0 02: ST6 OF 1.87 301 N date 28 01 50.29 n/a 000
06604# + 1.0 02: ST5TRF 0.0 000 N date 0.00 0.00 n/a 000
06605# + 1.0 02: ST4TOF 0.0 000 N date 0.00 0.00 n/a 000
06606# + 1.0 02: ST3TOF 0.0 000 N date 0.00 0.00 n/a 000
06607# SLIM 4.1 053 N date 28 00 38.69 n/a 000
06608# R010: CO133#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06609# ROUTE CHANNEL > 1.0 02: PT5ST 434.92 4.740 N date 29 18 25.81 n/a 000
06610# [RDfE: 1.00] out < 1.0 01: IRDNI 434.92 4.740 N date 29 31 25.81 n/a 000
06611# [L/SA= 324 / 100] 043]
06612# [IAREg m= 4.00: IAREgP= 4.00]
06613# R010: CO134#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06614# CONTI NUOS STANdHD 1.0 01: Aea-B 24.04 3.287 N date 28 03 47.99 728 000
06615# [XfM: 63.7fM: 85]
06616# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06617# [Impervious area: IApr= 1.57:SLPI= 50:LD= 491:MM= 013:SCI= 0]
06618# [IAREg m= 4.00: IAREgP= 4.00]
06619# R010: CO135#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06620# ROUTE RESERVOIR > 1.0 02: Aea-B 24.04 3.287 N date 28 03 47.99 n/a 000
06621# overFlow < 1.0 03: SWBDF 0.0 000 N date 0.00 0.00 n/a 000
06622# [MSStkEds:714E+00 mb, TotOfVol=0.0000E+00 mb, NcOf=0, TotDirOf=0 h.rs]
06623# [InterEvent Time=12.00]
06624# [Previous area: IApr= 4.67:SLPP= 50:LG= 50:MM= 250:SCP= 0]
06625# [Impervious area: IApr= 1.57:SLPI= 50:LD= 491:MM= 013:SCI= 0]
06626# [IAREg m= 4.00: IAREgP= 4.00]
06627# R010: CO136#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06628# ADD HYD 434.92 4.740 N date 29 31 25.81 n/a 000
06629# + 1.0 02: IRDNI 434.92 4.740 N date 29 31 25.81 n/a 000
06630# + 1.0 02: SWBDF 24.04 3.56 N date 28 50 47.99 n/a 000
06631# + 1.0 02: AI STR 469.69 4.958 N date 29 31 26.95 n/a 000
06632# SLIM 469.69 4.958 N date 29 31 26.95 n/a 000
06633# R010: CO137#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06634# ROUTE CHANNEL > 1.0 01: IRDNI 469.69 4.958 N date 29 31 26.95 n/a 000
06635# [RDfE: 1.00] out < 1.0 01: IRDNI 469.69 4.958 N date 29 31 26.95 n/a 000
06636# [L/SA= 599:DMw= 896]
06637# [IAREg m= 4.00: IAREgP= 4.00]
06638# R010: CO138#-----DfIn n ID NND-----AREhA-QPEAKm-TpkAktehh-hm-m RvM R C-----DfWcm
06

Table with multiple columns containing numerical data and alphanumeric codes (e.g., 067338, 067345, 067355, etc.). The table lists various items, possibly water flow measurements or station data, across several rows. The data includes numerical values and codes in a structured format.

074811	074828	074830	074831	074832	074833	074834	074835	074836	074837	074838	074839	074840	074841	074842	074843	074844	074845	074846	074847	074848	074849	074850	074851	074852	074853	074854	074855	074856	074857	074858	074859	074860	074861	074862	074863	074864	074865	074866	074867	074868	074869	074870	074871	074872	074873	074874	074875	074876	074877	074878	074879	074880	074881	074882	074883	074884	074885	074886	074887	074888	074889	074890	074891	074892	074893	074894	074895	074896	074897	074898	074899	074900	074901	074902	074903	074904	074905	074906	074907	074908	074909	074910	074911	074912	074913	074914	074915	074916	074917	074918	074919	074920	074921	074922	074923	074924	074925	074926	074927	074928	074929	074930	074931	074932	074933	074934	074935	074936	074937	074938	074939	074940	074941	074942	074943	074944	074945	074946	074947	074948	074949	074950	074951	074952	074953	074954	074955	074956	074957	074958	074959	074960	074961	074962	074963	074964	074965	074966	074967	074968	074969	074970	074971	074972	074973	074974	074975	074976	074977	074978	074979	074980	074981	074982	074983	074984	074985	074986	074987	074988	074989	074990	074991	074992	074993	074994	074995	074996	074997	074998	074999	075000
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Table with multiple columns containing alphanumeric codes, system names, and numerical values. The table is organized into two main sections, one on the left and one on the right, separated by a vertical line. Each entry typically includes a unique identifier, a description of the system or component, and several numerical parameters.

082289 remrk: Total Flow at MH108
082290 R0010: CH0417 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
082313 ROUTE PIPE > 1.0 02:MH107 119.82 3.962 NoDate 28:02 41.87 n/a 000
082323 * [RDS=1.00] out <- 1.0 01:ML107 119.82 3.962 NoDate 28:03 41.87 n/a 000
082333 * [L/S= 123.7 / 100.0] 013
082343 * [Vmax=1.666;Dmax=1.530]
082353 ID= 1.80;Dmax=1.34
082375 R0010: CH0417 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
082377 CONTINXUS STANHD 1.0 01:AI1 4.14 416 NoDate 28:01 38.46 595 000
082388 * [X.M= 35;T.M= 47]
082398 * [S.M= Cn 75.0]
082400 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
082413 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 183.;MNP= 013;SCL= 0]
082428 * [IAREC.mps= 4.00; IAREPFC= 4.00]
082438 * [S.M= 33.81; S.MW=225.43; S.K= 010]
082449 R0010: CH0417 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
082455 COMPUTE DIALHD 1.0 01:AI1 4.14 416 NoDate 28:01 38.46 n/a 000
082465 Major System \ 1.0 02:AI2-M 0.00 0.00 NoDate 0:00 0.0 n/a 000
082475 Major System / 1.0 02:AI3-M 10.61 993 NoDate 27:56 38.48 n/a 000
082485 * [M Systm= 4172E03; Tot OfV= 0.0000E+00; N OfV= 0; Tot Dir OfV= 0 hrs]
082498 R0010: CH0417 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
082500 CONTINXUS STANHD 1.0 01:AI1 10.61 1,251 NoDate 28:01 45.36 701 000
082511 * [X.M= 53;T.M= 62]
082523 * [LRS= 2; Cn= 75.0]
082535 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
082548 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 183.;MNP= 013;SCL= 0]
082555 * [IAREC.mps= 4.00; IAREPFC= 4.00]
082565 * [S.M= 33.81; S.MW=225.43; S.K= 010]
082575 R0010: CH0417 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
082582 COMPUTE DIALHD 1.0 01:AI1 10.61 1,251 NoDate 28:01 45.36 n/a 000
082595 Major System / 1.0 02:AI2-M 0.00 0.00 NoDate 0:00 0.0 n/a 000
082600 Major System \ 1.0 02:AI3-M 10.61 993 NoDate 27:56 38.48 n/a 000
082610 * [M Systm= 1016E03; Tot OfV= 0.0000E+00; N OfV= 0; Tot Dir OfV= 0 hrs]
082620 R0010: CH0417 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
082628 CONTINXUS STANHD 1.0 01:AI1 10.61 1,251 NoDate 28:01 45.36 n/a 000
082638 ADD HYD + 1.0 02:AI2-M 4.14 310 NoDate 27:55 38.48 n/a 000
082648 + 1.0 02:AI3-M 10.61 993 NoDate 27:56 38.48 n/a 000
082658 * [S.M= 33.81; S.MW=225.43; S.K= 010]
082668 SIM 1.0 02:AI1 134.57 5,265 NoDate 28:03 42.04 n/a 000
082678 R0010: CH0417 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
082688 SAVE HYD 1.0 01:MH107 134.57 5,265 NoDate 28:03 42.04 n/a 000
082698 remrk: MH107.010
082708 remrk: Total Flow at MH107
082710 R0010: CH0417 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
082725 ROUTE PIPE > 1.0 02:MH107 134.57 5,265 NoDate 28:03 42.04 n/a 000
082735 * [RDS=1.00] out <- 1.0 01:ML107 134.57 5,265 NoDate 28:05 42.04 n/a 000
082745 * [L/S= 114.7 / 120.0] 013
082755 * [Vmax= 1.912;Dmax= 2.00]
082765 R0010: CH0417 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
082773 ROUTE PIPE > 1.0 02:MH108 134.57 5,248 NoDate 28:06 42.04 n/a 000
082783 * [RDS=1.00] out <- 1.0 01:ML108 134.57 5,248 NoDate 28:06 42.04 n/a 000
082793 * [L/S= 66.7 / 120.0] 013
082803 * [Vmax= 1.912;Dmax= 1.639]
082813 R0010: CH0417 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
082823 CONTINXUS STANHD 1.0 01:AI2 12.29 1,385 NoDate 28:01 41.19 637 000
082833 * [X.M= 54;T.M= 54]
082843 * [LRS= 2; Cn= 75.0]
082855 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
082868 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 183.;MNP= 013;SCL= 0]
082878 * [IAREC.mps= 4.00; IAREPFC= 4.00]
082888 * [S.M= 33.81; S.MW=225.43; S.K= 010]
082898 R0010: CH0417 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
082905 COMPUTE DIALHD 1.0 01:AI1 12.29 1,385 NoDate 28:01 41.19 n/a 000
082915 Major System / 1.0 02:AI2-M 0.00 0.00 NoDate 0:00 0.0 n/a 000
082925 Major System \ 1.0 02:AI3-M 12.29 1,029 NoDate 27:54 41.27 n/a 000
082935 * [M Systm= 1401E03; Tot OfV= 0.0000E+00; N OfV= 0; Tot Dir OfV= 0 hrs]
082945 R0010: CH0417 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
082953 CONTINXUS STANHD 1.0 01:AI1 12.29 1,385 NoDate 28:01 41.19 790 000
082963 * [X.M= 71;T.M= 71]
082973 * [LRS= 2; Cn= 75.0]
082985 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
082998 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 183.;MNP= 013;SCL= 0]
083008 * [IAREC.mps= 4.00; IAREPFC= 4.00]
083018 * [S.M= 33.81; S.MW=225.43; S.K= 010]
083028 R0010: CH0417 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
083035 COMPUTE DIALHD 1.0 01:AI1 2.59 368 NoDate 28:01 51.11 n/a 000
083045 Major System / 1.0 02:AI2-M 0.00 0.00 NoDate 0:00 0.0 n/a 000
083055 Major System \ 1.0 02:AI3-M 2.59 368 NoDate 28:01 51.11 n/a 000
083065 * [M Systm= 1401E03; Tot OfV= 0.0000E+00; N OfV= 0; Tot Dir OfV= 0 hrs]
083075 R0010: CH0417 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
083083 CONTINXUS STANHD 1.0 01:AI1 2.59 368 NoDate 28:01 51.11 601 000
083093 * [X.M= 41;T.M= 41]
083103 * [LRS= 2; Cn= 75.0]
083115 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
083125 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 183.;MNP= 013;SCL= 0]
083135 * [IAREC.mps= 4.00; IAREPFC= 4.00]
083145 * [S.M= 33.81; S.MW=225.43; S.K= 010]
083155 R0010: CH0417 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
083163 ADD HYD + 1.0 02:119:108 134.57 5,248 NoDate 28:06 42.04 n/a 000
083173 + 1.0 02:120:108 134.57 5,248 NoDate 28:06 42.04 n/a 000
083183 * [L/S= 114.7 / 120.0] 013
083193 * [Vmax= 1.912;Dmax= 1.639]
083203 R0010: CH0417 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
083211 CONTINXUS STANHD 1.0 01:AI1 12.29 1,029 NoDate 27:54 41.27 n/a 000
083221 * [S.M= 33.81; S.MW=225.43; S.K= 010]
083231 * [LRS= 2; Cn= 75.0]
083241 R0010: CH0417 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
083250 SAVE HYD 1.0 01:MH108 149.45 6,598 NoDate 28:04 42.14 n/a 000
083260 remrk: MH108.010
083270 remrk: Total Flow at MH108
083280 R0010: CH0417 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
083288 ROUTE PIPE > 1.0 02:MH108 149.45 6,598 NoDate 28:04 42.14 n/a 000
083298 * [RDS=1.00] out <- 1.0 01:ML108 149.45 6,598 NoDate 28:05 42.14 n/a 000
083308 * [L/S= 77.7 / 130.0] 013
083318 * [Vmax= 2.085;Dmax= 1.759]
083328 R0010: CH0417 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
083336 ROUTE PIPE > 1.0 02:MH108 149.45 6,577 NoDate 28:06 42.14 n/a 000
083346 * [RDS=1.00] out <- 1.0 01:ML108 149.45 6,577 NoDate 28:06 42.14 n/a 000
083356 * [L/S= 80.0 / 130.0] 013
083366 * [Vmax= 2.084;Dmax= 1.754]
083376 R0010: CH0417 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
083384 ADD HYD + 1.0 02:116:corr 149.45 6,577 NoDate 28:06 42.14 n/a 000
083394 + 1.0 02:117:corr 149.45 6,577 NoDate 28:06 42.14 n/a 000
083404 * [L/S= 116.0 / 130.0] 013
083414 R0010: CH0417 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
083422 SAVE HYD 1.0 01:MH108 152.39 6,779 NoDate 28:05 42.08 n/a 000
083432 remrk: Corrigan.010
083442 remrk: Total Flow at Corrigan Pond
083450 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
083458 ROUTE RESERVOIR > 1.0 02:Corrigan 152.39 6,779 NoDate 28:05 42.08 n/a 000
083468 * [RDS=1.00] out <- 1.0 03:Co- OFF 0.00 0.00 NoDate 0:00 0.0 n/a 000
083478 * [M Systm= 1401E03; Tot OfV= 0.0000E+00; N OfV= 0; Tot Dir OfV= 0 hrs]
083488 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
083496 CONTINXUS STANHD 1.0 01:AI1 152.39 6,779 NoDate 28:05 42.08 n/a 000
083506 * [X.M= 71;T.M= 71]
083516 * [LRS= 2; Cn= 75.0]
083526 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
083536 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 183.;MNP= 013;SCL= 0]
083546 * [IAREC.mps= 4.00; IAREPFC= 4.00]
083556 * [S.M= 33.81; S.MW=225.43; S.K= 010]
083566 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
083574 ADD HYD + 1.0 02:Co- OFF 152.39 6,100 NoDate 28:15 42.07 n/a 000
083584 + 1.0 02:TO 54837.78 85,488 NoDate 37:22 23.06 n/a 000
083594 * [L/S= 116.0 / 130.0] 013
083604 * [Vmax= 2.084;Dmax= 1.754]
083614 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
083622 CONTINXUS STANHD 1.0 01:AI1 152.39 6,779 NoDate 28:05 42.08 n/a 000
083632 * [X.M= 36.67;T.M= 36.67]
083642 * [LRS= 2; Cn= 75.0]
083652 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
083662 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 118.;MNP= 013;SCL= 0]
083672 * [IAREC.mps= 4.00; IAREPFC= 4.00]
083682 * [S.M= 33.81; S.MW=225.43; S.K= 010]
083692 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
083700 CONTINXUS STANHD 1.0 01:AI1 152.39 6,779 NoDate 28:05 42.08 n/a 000
083710 * [X.M= 36.67;T.M= 36.67]
083720 * [LRS= 2; Cn= 74.0]
083730 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
083740 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 118.;MNP= 013;SCL= 0]
083750 * [IAREC.mps= 4.00; IAREPFC= 4.00]
083760 * [S.M= 33.81; S.MW=225.43; S.K= 010]
083770 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
083778 CONTINXUS STANHD 1.0 01:AI1 152.39 6,779 NoDate 28:05 42.08 n/a 000
083788 * [X.M= 36.67;T.M= 36.67]
083798 * [LRS= 2; Cn= 74.0]
083808 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
083818 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 118.;MNP= 013;SCL= 0]
083828 * [IAREC.mps= 4.00; IAREPFC= 4.00]
083838 * [S.M= 33.81; S.MW=225.43; S.K= 010]
083848 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
083856 CONTINXUS STANHD 1.0 01:AI1 152.39 6,779 NoDate 28:05 42.08 n/a 000
083866 * [X.M= 36.67;T.M= 36.67]
083876 * [LRS= 2; Cn= 74.0]
083886 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
083896 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 118.;MNP= 013;SCL= 0]
083906 * [IAREC.mps= 4.00; IAREPFC= 4.00]
083916 * [S.M= 33.81; S.MW=225.43; S.K= 010]
083926 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
083934 CONTINXUS STANHD 1.0 01:AI1 152.39 6,779 NoDate 28:05 42.08 n/a 000
083944 * [X.M= 36.67;T.M= 36.67]
083954 * [LRS= 2; Cn= 74.0]
083964 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
083974 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 118.;MNP= 013;SCL= 0]
083984 * [IAREC.mps= 4.00; IAREPFC= 4.00]
083994 * [S.M= 33.81; S.MW=225.43; S.K= 010]
084004 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
084012 CONTINXUS STANHD 1.0 01:AI1 152.39 6,779 NoDate 28:05 42.08 n/a 000
084022 * [X.M= 36.67;T.M= 36.67]
084032 * [LRS= 2; Cn= 74.0]
084042 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
084052 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 118.;MNP= 013;SCL= 0]
084062 * [IAREC.mps= 4.00; IAREPFC= 4.00]
084072 * [S.M= 33.81; S.MW=225.43; S.K= 010]
084082 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
084090 CONTINXUS STANHD 1.0 01:AI1 152.39 6,779 NoDate 28:05 42.08 n/a 000
084100 * [X.M= 36.67;T.M= 36.67]
084110 * [LRS= 2; Cn= 74.0]
084120 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
084130 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 118.;MNP= 013;SCL= 0]
084140 * [IAREC.mps= 4.00; IAREPFC= 4.00]
084150 * [S.M= 33.81; S.MW=225.43; S.K= 010]
084160 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
084168 CONTINXUS STANHD 1.0 01:AI1 152.39 6,779 NoDate 28:05 42.08 n/a 000
084178 * [X.M= 36.67;T.M= 36.67]
084188 * [LRS= 2; Cn= 74.0]
084198 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
084208 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 118.;MNP= 013;SCL= 0]
084218 * [IAREC.mps= 4.00; IAREPFC= 4.00]
084228 * [S.M= 33.81; S.MW=225.43; S.K= 010]
084238 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
084246 CONTINXUS STANHD 1.0 01:AI1 152.39 6,779 NoDate 28:05 42.08 n/a 000
084256 * [X.M= 36.67;T.M= 36.67]
084266 * [LRS= 2; Cn= 74.0]
084276 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
084286 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 118.;MNP= 013;SCL= 0]
084296 * [IAREC.mps= 4.00; IAREPFC= 4.00]
084306 * [S.M= 33.81; S.MW=225.43; S.K= 010]
084316 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
084324 CONTINXUS STANHD 1.0 01:AI1 152.39 6,779 NoDate 28:05 42.08 n/a 000
084334 * [X.M= 36.67;T.M= 36.67]
084344 * [LRS= 2; Cn= 74.0]
084354 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
084364 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 118.;MNP= 013;SCL= 0]
084374 * [IAREC.mps= 4.00; IAREPFC= 4.00]
084384 * [S.M= 33.81; S.MW=225.43; S.K= 010]
084394 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
084402 CONTINXUS STANHD 1.0 01:AI1 152.39 6,779 NoDate 28:05 42.08 n/a 000
084412 * [X.M= 36.67;T.M= 36.67]
084422 * [LRS= 2; Cn= 74.0]
084432 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
084442 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 118.;MNP= 013;SCL= 0]
084452 * [IAREC.mps= 4.00; IAREPFC= 4.00]
084462 * [S.M= 33.81; S.MW=225.43; S.K= 010]
084472 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
084480 CONTINXUS STANHD 1.0 01:AI1 152.39 6,779 NoDate 28:05 42.08 n/a 000
084490 * [X.M= 36.67;T.M= 36.67]
084500 * [LRS= 2; Cn= 74.0]
084510 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
084520 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 118.;MNP= 013;SCL= 0]
084530 * [IAREC.mps= 4.00; IAREPFC= 4.00]
084540 * [S.M= 33.81; S.MW=225.43; S.K= 010]
084550 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
084558 CONTINXUS STANHD 1.0 01:AI1 152.39 6,779 NoDate 28:05 42.08 n/a 000
084568 * [X.M= 36.67;T.M= 36.67]
084578 * [LRS= 2; Cn= 74.0]
084588 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
084598 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 118.;MNP= 013;SCL= 0]
084608 * [IAREC.mps= 4.00; IAREPFC= 4.00]
084618 * [S.M= 33.81; S.MW=225.43; S.K= 010]
084628 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
084636 CONTINXUS STANHD 1.0 01:AI1 152.39 6,779 NoDate 28:05 42.08 n/a 000
084646 * [X.M= 36.67;T.M= 36.67]
084656 * [LRS= 2; Cn= 74.0]
084666 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
084676 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 118.;MNP= 013;SCL= 0]
084686 * [IAREC.mps= 4.00; IAREPFC= 4.00]
084696 * [S.M= 33.81; S.MW=225.43; S.K= 010]
084706 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
084714 CONTINXUS STANHD 1.0 01:AI1 152.39 6,779 NoDate 28:05 42.08 n/a 000
084724 * [X.M= 36.67;T.M= 36.67]
084734 * [LRS= 2; Cn= 74.0]
084744 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
084754 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 118.;MNP= 013;SCL= 0]
084764 * [IAREC.mps= 4.00; IAREPFC= 4.00]
084774 * [S.M= 33.81; S.MW=225.43; S.K= 010]
084784 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
084792 CONTINXUS STANHD 1.0 01:AI1 152.39 6,779 NoDate 28:05 42.08 n/a 000
084802 * [X.M= 36.67;T.M= 36.67]
084812 * [LRS= 2; Cn= 74.0]
084822 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
084832 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 118.;MNP= 013;SCL= 0]
084842 * [IAREC.mps= 4.00; IAREPFC= 4.00]
084852 * [S.M= 33.81; S.MW=225.43; S.K= 010]
084862 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
084870 CONTINXUS STANHD 1.0 01:AI1 152.39 6,779 NoDate 28:05 42.08 n/a 000
084880 * [X.M= 36.67;T.M= 36.67]
084890 * [LRS= 2; Cn= 74.0]
084900 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
084910 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 118.;MNP= 013;SCL= 0]
084920 * [IAREC.mps= 4.00; IAREPFC= 4.00]
084930 * [S.M= 33.81; S.MW=225.43; S.K= 010]
084940 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
084948 CONTINXUS STANHD 1.0 01:AI1 152.39 6,779 NoDate 28:05 42.08 n/a 000
084958 * [X.M= 36.67;T.M= 36.67]
084968 * [LRS= 2; Cn= 74.0]
084978 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
084988 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 118.;MNP= 013;SCL= 0]
084998 * [IAREC.mps= 4.00; IAREPFC= 4.00]
085008 * [S.M= 33.81; S.MW=225.43; S.K= 010]
085018 R0010: CH0424 ----- DfIn-ID NND ----- AREHA-QPEAKm-TpeakDte,h:mm ----- Rvsm R.C. --- DfWcm
085026 CONTINXUS STANHD 1.0 01:AI1 152.39 6,779 NoDate 28:05 42.08 n/a 000
085036 * [X.M= 36.67;T.M= 36.67]
085046 * [LRS= 2; Cn= 74.0]
085056 * [Pervious area: IApwr= 4.67;SLP=1.00;LCP= 40.;MNP= 250;SCP= 0]
085066 * [Imperious area: IApwr= 1.57;SLP=1.00;LCA= 118.;MNP= 013;SCL= 0]
085076 * [IAREC.mps= 4.00; IAREPFC=

08603#	[Cm 66.0 No. 3.00; Tm= 2.51]	08790#	R0025: C00037.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm
08604#	[IAREC 4.00; SMN= 52.62; SMM=350.79; SKE- 010]	08791#	SAVE HYD + 1.0 01: S_N02 9506.00 16.182 No.date 32:43 25:02 n/a 0000
08605#	[InterEventTime= 12.00]	08792#	fname -H_SMI2
08606#		08793#	remark: flow at S_N02 near Ashton
08607#	The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)	08794#	
08608#	# of 1.80	08795#	Sum of hydrographs from Node 12 routed to Node 11
08609#	R0025: C00011.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm	08796#	(Approximated cross-section - see cross-section 258)
08610#	CNTI NLUK NASIHD 1.0 01: SW1 1917.00 10.351 No.date 34:27 27:01 363 0000	08797#	Use m=0.04 for summer conditions and m=0.025 for spring conditions
08611#	[Cm 66.0 No. 3.00; Tm= 2.51]	08798#	
08612#	[IAREC 4.00; SMN= 52.62; SMM=350.79; SKE- 010]	08799#	Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
08613#	[InterEventTime= 12.00]	08800#	
08614#		08801#	R0025: C00038.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm
08615#	The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)	08802#	ROUTE CHANNEL -> 1.0 02: S_N02 9506.00 16.182 No.date 32:43 25:02 n/a 0000
08616#	# of 1.52	08803#	[RFR= 1.00] out c. 1.0 01: Don1 9506.00 16.007 No.date 33:02 25:02 n/a 0000
08617#	R0025: C00012.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm	08804#	[L/S= n= 972. / 034. 040]
08618#	CNTI NLUK NASIHD 1.0 01: SW1 5666.00 27.457 No.date 37:54 31:50 423 0000	08805#	[Vmax= -721; Dmax= 2.847]
08619#	[Cm 72.0 No. 3.00; Tm= 8.00]	08806#	# Addition of Subwatershed 11 and No Name Creek to Node 11
08620#	[IAREC 4.00; SMN= 39.75; SMM=264.99; SKE- 010]	08807#	
08621#	[InterEventTime= 12.00]	08808#	R0025: C00039.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm
08622#		08809#	ADD HYD + 1.0 02: SW1 500.00 7.521 No.date 29:22 27:01 n/a 0000
08623#	The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)	08810#	+ 1.0 02: SW1 1917.00 10.351 No.date 34:27 27:01 n/a 0000
08624#	# of 1.75	08811#	SUM 1.0 01: S_N1 11923.00 27.908 No.date 33:04 25:42 n/a 0000
08625#	R0025: C00013.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm	08812#	
08626#	CNTI NLUK NASIHD 1.0 01: RL_CK 8376.00 26.276 No.date 39:59 27:01 363 0000	08813#	Sum of hydrographs from Node 11 routed to Node 10
08627#	[Cm 66.0 No. 3.00; Tm= 11.661]	08814#	Section 1
08628#	[IAREC 4.00; SMN= 52.62; SMM=350.79; SKE- 010]	08815#	
08629#	[InterEventTime= 12.00]	08816#	
08630#		08817#	
08631#	The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)	08818#	R0025: C00040.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm
08632#	# of 1.82	08819#	ROUTE CHANNEL -> 1.0 02: S_N1 11923.00 27.908 No.date 33:04 25:42 n/a 0000
08633#	R0025: C00014.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm	08820#	[RFR= 1.00] out c. 1.0 01: N10 11923.00 10.039 No.date 40:01 25:42 n/a 0000
08634#	CNTI NLUK NASIHD 1.0 01: HB_LR 1132.00 11.752 No.date 30:54 30:18 406 0000	08821#	[L/S= n= 1028. / 137. 040]
08635#	[Cm 66.0 No. 3.00; Tm= 2.51]	08822#	[Vmax= -464; Dmax= 1.329]
08636#	[IAREC 4.00; SMN= 43.07; SMM=287.10; SKE- 010]	08823#	
08637#	[InterEventTime= 12.00]	08824#	# Addition of Subwatershed 10 to Node 10
08638#		08825#	
08639#	The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)	08826#	R0025: C00041.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm
08640#	# of 1.82	08827#	ADD HYD + 1.0 02: SW1 1923.00 10.039 No.date 40:01 25:42 n/a 0000
08641#	R0025: C00015.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm	08828#	+ 1.0 02: SW10 5666.00 27.457 No.date 37:54 31:50 n/a 0000
08642#	CNTI NLUK NASIHD 1.0 01: HB_LR 3854.00 15.333 No.date 38:34 27:01 363 0000	08829#	SUM 1.0 01: S_N0 17589.00 45.026 No.date 38:35 27:38 n/a 0000
08643#	[Cm 62.0 No. 3.00; Tm= 1.32]	08830#	R0025: C00042.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm
08644#	[IAREC 4.00; SMN= 52.62; SMM=412.66; SKE- 010]	08831#	SAVE HYD + 1.0 01: S_N10 117589.00 45.026 No.date 38:35 27:38 n/a 0000
08645#	[InterEventTime= 12.00]	08832#	fname -H_SMI0
08646#		08833#	remark: flow at S_N10
08647#	The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)	08834#	# Addition of Subwatershed 10 and SW10
08648#	# of 1.80	08835#	# Addition of Subwatershed 9 and Nchols Creek to Node 9
08649#	R0025: C00016.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm	08836#	
08650#	CNTI NLUK NASIHD 1.0 01: SW1 131.00 2.266 No.date 28:57 25:20 339 0000	08837#	ADD HYD + 1.0 02: S_N10 17589.00 45.026 No.date 38:35 27:38 n/a 0000
08651#	[Cm 63.0 No. 3.00; Tm= -90.8]	08838#	+ 1.0 02: S_N10 17589.00 45.026 No.date 38:35 27:38 n/a 0000
08652#	[IAREC 4.00; SMN= 52.62; SMM=396.11; SKE- 010]	08839#	SUM 1.0 01: S_N10 25965.00 70.812 No.date 39:59 26:26 n/a 0000
08653#	[InterEventTime= 12.00]	08840#	
08654#		08841#	Sum of hydrographs from Node 10 routed to Node 9
08655#	The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)	08842#	Section 2
08656#	# of 1.82	08843#	
08657#	R0025: C00017.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm	08844#	R0025: C00044.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm
08658#	CNTI NLUK NASIHD 1.0 01: HB_LR 3854.00 15.333 No.date 38:34 27:01 363 0000	08845#	ROUTE CHANNEL -> 1.0 02: S_N10 25965.00 70.812 No.date 39:59 27:26 n/a 0000
08659#	[Cm 62.0 No. 3.00; Tm= 1.32]	08846#	[RFR= 1.00] out c. 1.0 01: N10 25965.00 69.023 No.date 39:59 27:26 n/a 0000
08660#	[IAREC 4.00; SMN= 52.62; SMM=350.79; SKE- 010]	08847#	[L/S= n= 3982. / 075. 040]
08661#	[InterEventTime= 12.00]	08848#	[Vmax= 718; Dmax= 1.889]
08662#		08849#	
08663#	The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)	08850#	# Addition of Subwatershed 9 and Nchols Creek to Node 9
08664#	# of 1.82	08851#	
08665#	R0025: C00018.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm	08852#	R0025: C00045.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm
08666#	CNTI NLUK NASIHD 1.0 01: SW1 3197.00 11.663 No.date 36:24 21:75 292 0000	08853#	ADD HYD + 1.0 02: SW9 1132.00 11.752 No.date 30:54 30:18 n/a 0000
08667#	[Cm 57.0 No. 3.00; Tm= 6.51]	08854#	+ 1.0 02: SW9 1132.00 11.752 No.date 30:54 30:18 n/a 0000
08668#	[IAREC 4.00; SMN= 52.62; SMM=508.81; SKE- 010]	08855#	4464.00 13.075 No.date 39:59 24:61 0000
08669#	[InterEventTime= 12.00]	08856#	SUM 1.0 01: S_N9 31561.00 84.884 No.date 39:59 26:99 n/a 0000
08670#		08857#	
08671#	The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)	08858#	Sum of hydrographs from Node 9 routed to Node 8
08672#	# of 1.75	08859#	Section 3
08673#	R0025: C00019.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm	08860#	
08674#	CNTI NLUK NASIHD 1.0 01: SW6 165.00 1.076 No.date 33:03 27:63 371 0000	08861#	R0025: C00046.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm
08675#	[Cm 57.0 No. 3.00; Tm= 6.51]	08862#	ROUTE CHANNEL -> 1.0 02: S_N9 31561.00 84.884 No.date 39:59 26:99 n/a 0000
08676#	[IAREC 4.00; SMN= 50.55; SMM=336.97; SKE- 010]	08863#	[RFR= 1.00] out c. 1.0 01: N8 31561.00 79.245 No.date 39:59 26:99 n/a 0000
08677#	[InterEventTime= 12.00]	08864#	[L/S= n= 2269. / 088. 045]
08678#		08865#	[Vmax= -362; Dmax= 7.451]
08679#	The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)	08866#	
08680#	# of 1.82	08867#	# Addition of Subwatershed 8 and Hbb's Drain to Node 8
08681#	R0025: C00020.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm	08868#	
08682#	CNTI NLUK NASIHD 1.0 01: HB_LR 1332.00 7.882 No.date 35:14 31:50 423 0000	08869#	R0025: C00047.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm
08683#	[Cm 72.0 No. 3.00; Tm= 5.95]	08870#	ADD HYD + 1.0 02: S_N 31561.00 79.245 No.date 39:59 26:99 n/a 0000
08684#	[IAREC 4.00; SMN= 39.75; SMM=264.99; SKE- 010]	08871#	+ 1.0 02: S_N 131.00 2.266 No.date 28:57 25:20 n/a 0000
08685#	[InterEventTime= 12.00]	08872#	+ 1.0 02: S_N 131.00 2.266 No.date 28:57 25:20 n/a 0000
08686#	R0025: C00021.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm	08873#	SUM 1.0 01: S_N8 35546.00 91.812 No.date 39:59 26:99 n/a 0000
08687#	CNTI NLUK NASIHD 1.0 01: SW1 224.00 6.882 No.date 28:45 35:66 479 0000	08874#	
08688#	[Cm 77.0 No. 3.00; Tm= 7.51]	08875#	Sum of hydrographs from Node 8 routed to Node 7
08689#	[IAREC 4.00; SMN= 31.15; SMM=207.66; SKE- 010]	08876#	Section 4
08690#	[InterEventTime= 12.00]	08877#	
08691#		08878#	R0025: C00048.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm
08692#	The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)	08879#	ROUTE CHANNEL -> 1.0 02: S_N 35546.00 94.597 No.date 39:59 26:99 n/a 0000
08693#	# of 1.20	08880#	[RFR= 1.00] out c. 1.0 01: N7 35546.00 80.337 No.date 45:08 26:98 n/a 0000
08694#	R0025: C00022.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm	08881#	[L/S= n= 3760. / 053. 070]
08695#	CNTI NLUK NASIHD 1.0 01: FL_CK 4945.00 37.664 No.date 33:18 32:85 442 0000	08882#	[Vmax= -226; Dmax= 2.161]
08696#	[Cm 74.0 No. 3.00; Tm= 4.45]	08883#	
08697#	[IAREC 4.00; SMN= 34.96; SMM=244.99; SKE- 010]	08884#	# Addition of Subwatershed 7 to Node 7
08698#	[InterEventTime= 12.00]	08885#	
08699#	R0025: C00023.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm	08886#	R0025: C00049.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm
08700#	CNTI NLUK NASIHD 1.0 01: SW2A 20.00 7.98 No.date 28:35 39:36 529 0000	08887#	ADD HYD + 1.0 02: N7 35546.00 80.337 No.date 45:08 26:98 n/a 0000
08701#	[Cm 81.0 No. 3.00; Tm= 6.21]	08888#	+ 1.0 02: N7 3197.00 11.663 No.date 36:24 21:75 n/a 0000
08702#	[IAREC 4.00; SMN= 25.21; SMM=168.09; SKE- 010]	08889#	SUM 1.0 01: S_N7 38743.00 86.331 No.date 44:08 26:55 n/a 0000
08703#	[InterEventTime= 12.00]	08890#	R0025: C00050.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm
08704#		08891#	SAVE HYD + 1.0 01: S_N7 38743.00 86.331 No.date 44:08 26:55 n/a 0000
08705#	The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)	08892#	fname -H_SN7
08706#	# of 1.81	08893#	remark: flow at S_N7; N7 + SW7
08707#	R0025: C00024.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm	08894#	# Insertion of a reservoir to simulate the effects of the Richmond Fen.
08708#	CNTI NLUK NASIHD 1.0 01: SW2AI 1412.00 7.480 No.date 37:50 34:24 1460 0000	08895#	Storage area and volume were estimated from available top maps.
08709#	[Cm 72.0 No. 3.00; Tm= 8.00]	08896#	Release rate from Fen was assumed to be controlled by the downstream
08710#	[IAREC 4.00; SMN= 33.81; SMM=225.43; SKE- 010]	08897#	river cross-section for summer conditions. It was assumed that for up to
08711#	[InterEventTime= 12.00]	08898#	0.75 of water, the river channel, the river and the storage. Above
08712#	R0025: C00025.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm	08899#	this depth, the wetland starts to significantly store water.
08713#	CNTI NLUK NASIHD 1.0 01: SW1 585.00 10.942 No.date 29:56 39:36 529 0000	08900#	
08714#	[Cm 81.0 No. 3.00; Tm= 1.75]	08901#	R0025: C00051.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm
08715#	[IAREC 4.00; SMN= 25.21; SMM=168.09; SKE- 010]	08902#	ROUTE RESERVOIR -> 1.0 02: S_N7 38743.00 86.331 No.date 44:08 26:55 n/a 0000
08716#	[InterEventTime= 12.00]	08903#	[RFR= 1.00] out c. 1.0 01: RES_RF 38743.00 42.032 No.date 60:05 26:55 n/a 0000
08717#	R0025: C00026.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm	08904#	[MStoldev= 367; E= 0.3]
08718#	CNTI NLUK NASIHD 1.0 01: SW2C 1021.00 14.476 No.date 30:46 38:60 519 0000	08905#	R0025: C00052.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm
08719#	[Cm 80.0 No. 3.00; Tm= 2.46]	08906#	SAVE HYD + 1.0 01: RES_RF 38743.00 42.032 No.date 60:05 26:55 n/a 0000
08720#	[IAREC 4.00; SMN= 26.32; SMM=175.50; SKE- 010]	08907#	fname -H_RES_RF
08721#	[InterEventTime= 12.00]	08908#	remark: outflow of Richmond Fen
08722#	R0025: C00027.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm	08909#	
08723#	CNTI NLUK NASIHD 1.0 01: SW1 171.00 5.438 No.date 28:45 35:66 479 0000	08910#	Sum of hydrographs from Node 7 routed to Node 6
08724#	[Cm 76.0 No. 3.00; Tm= 7.51]	08911#	Section 5
08725#	[IAREC 4.00; SMN= 25.21; SMM=168.09; SKE- 010]	08912#	
08726#	[InterEventTime= 12.00]	08913#	R0025: C00053.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm
08727#	R0025: C00028.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C.--DFWcm	08914#	ROUTE CHANNEL -> 1.0 02: RES_RF 38743.00 42.032 No.date 60:05 26:55 n/a 0000
08728#	CNTI NLUK NASIHD 1.0 01: SW1 1122.00 13.229 No.date 31:45 39:36 529 0000	08915#	[RFR= 1.00] out c. 1.0 01: RES_RF 38743.00 42.032 No.date 61:20 26:55 n/a 0000
08729#	[Cm 81.0 No. 3.00; Tm= 1.75]	08916#	[L/S= n= 3056. / 032. 025]
08730#	[IAREC 4.00; SMN= 25.21; SMM=168.09; SKE- 010]	08917#	[Vmax= 514; Dmax= 1.120]
08731#	[InterEventTime= 12.00]	08918#	
08732#	R0025: C00029.....Dfai n-1D NND.....AREHA-QPEAGm-TpeakDte-hh-mm--Rvmm R.C		

08977#	R0025:CO061	Dfmn 1-D NND	AREBA-QPEAKm-TpeakDte.hh:mm	Rvmm R.C.	Dfwmc
08978#	SAVE HYD		1.0 01:5-N	4847.00	73.819 Ndate	35:41	28.02 n/a	0.00	
08979#			fname S_N.0025						
08980#			remark:flow at S_N						
08981#									
08982#			Sum of hydrographs from Node 4 routed to Node 2						
08983#			# Section						
08984#									
08985#	R0025:CO062	Dfmn 1-D NND	AREBA-QPEAKm-TpeakDte.hh:mm	Rvmm R.C.	Dfwmc
08986#	ROUTE CHANNEL	>	1.0 02:5-N	4847.00	73.819 Ndate	35:41	28.02 n/a	0.00	
08987#			[RfW 1.00] out <	1.0 02:5-N	4847.00	73.819 Ndate	35:41	28.02 n/a	0.00
08988#			[L/S/m 1667 / 060/040]						
08989#			[Vmax = 874; Dmax= 3.570]						
08990#			# Addition of Subwatershed 2 with Mhoanah Drain and Smith Drain to Node 2						
08991#									
08992#	R0025:CO063	Dfmn 1-D NND	AREBA-QPEAKm-TpeakDte.hh:mm	Rvmm R.C.	Dfwmc
08993#	ADD HYD		1.0 02:5-N	4847.00	73.819 Ndate	35:42	28.02 n/a	0.00	
08994#			[ARECm 4.00; IARECm 4.00]						
08995#			+ 1.0 02:5-N	1122.00	13.229 Ndate	31:45	39.36 n/a	0.00	
08996#			+ 1.0 02:5-N	2737.00	5.438 Ndate	31:30	34.94 n/a	0.00	
08997#			+ 1.0 02:5-N	52483.00	106.109 Ndate	33:07	28.64 n/a	0.00	
08998#			SUM						
08999#	R0025:CO064	Dfmn 1-D NND	AREBA-QPEAKm-TpeakDte.hh:mm	Rvmm R.C.	Dfwmc
09000#	SAVE HYD		1.0 01:5-N	52483.00	106.109 Ndate	33:07	28.64 n/a	0.00	
09001#			fname H_SND						
09002#			remark:flow at S_N Jock River Gauge at Moeiric Dr.						
09003#			# Sum of hydrographs from Node 2 routed to Node 1						
09004#			# Section 10						
09005#									
09006#									
09007#									
09008#									
09009#			Hydrograph from Node 2 routed to Node 416						
09010#			Channel X-Section obtained from RGA Hydraulic Model - Station 9025						
09011#									
09012#	R0025:CO065	Dfmn 1-D NND	AREBA-QPEAKm-TpeakDte.hh:mm	Rvmm R.C.	Dfwmc
09013#	ROUTE CHANNEL	>	1.0 02:5-N	52483.00	106.109 Ndate	33:07	28.64 n/a	0.00	
09014#			[ARECm 4.00; IARECm 4.00]						
09015#			[RfW 1.00] out <	1.0 01:5-N	52483.00	106.109 Ndate	33:07	28.64 n/a	0.00
09016#			[L/S/m 2327 / 050/055]						
09017#			[Vmax = 754; Dmax = 3.061]						
09018#			# Catchment SW of RGA catchment SW outside of Reach 1 subwatershed						
09019#			# Undeveloped agricultural land						
09020#									
09021#	R0025:CO066	Dfmn 1-D NND	AREBA-QPEAKm-TpeakDte.hh:mm	Rvmm R.C.	Dfwmc
09022#	CNTINUES STANNHD		1.0 01:1-C	536.42	5.154 Ndate	31:16	30.13 405	0.00	
09023#			[Cm 72.0; Nc 3.00; Tm 2.79]						
09024#			[AREC 4.00; SMN 39.75; SMM 264.99; SKE 010]						
09025#			[InterEvent Time 12.00]						
09026#	R0025:CO067	Dfmn 1-D NND	AREBA-QPEAKm-TpeakDte.hh:mm	Rvmm R.C.	Dfwmc
09027#	CNTINUES STANNHD		1.0 01:5-N	44.93	6.507 Ndate	28:03	57.38 771	0.00	
09028#			[XMP: 65; TIMP: 65]						
09029#			[LBS: 2; CNE 61.0]						
09030#			[Pervious area: IPer= 4.67; SLP= 2.00; LQP= 4.00; MNP: 250; SCP= 0]						
09031#			[Imperious area: IImper= 1.57; SLP= 1.32; LQ= 547; MN: 013; SCL= 0]						
09032#			[ARECm 4.00; IARECm 4.00]						
09033#			[RfW 1.00] out <	1.0 01:5-N	44.93	6.507 Ndate	28:03	57.38 n/a	0.00
09034#			[L/S/m 33.81; SMM 225.45; SKE 010]						
09035#	R0025:CO068	Dfmn 1-D NND	AREBA-QPEAKm-TpeakDte.hh:mm	Rvmm R.C.	Dfwmc
09036#	COMPUTE DUALHD		1.0 01:5-N	44.93	6.507 Ndate	28:03	57.38 n/a	0.00	
09037#			[Mf System / 0.00]						
09038#			[Mf System / 0.00]						
09039#			[Mf System / 0.00]						
09040#			[Mf System / 0.00]						
09041#			[Mf System / 0.00]						
09042#			[Mf System / 0.00]						
09043#			[Mf System / 0.00]						
09044#			[Mf System / 0.00]						
09045#			[Mf System / 0.00]						
09046#			[Mf System / 0.00]						
09047#			[Mf System / 0.00]						
09048#			[Mf System / 0.00]						
09049#			[Mf System / 0.00]						
09050#			[Mf System / 0.00]						
09051#			[Mf System / 0.00]						
09052#			[Mf System / 0.00]						
09053#			[Mf System / 0.00]						
09054#			[Mf System / 0.00]						
09055#			[Mf System / 0.00]						
09056#			[Mf System / 0.00]						
09057#			[Mf System / 0.00]						
09058#			[Mf System / 0.00]						
09059#			[Mf System / 0.00]						
09060#			[Mf System / 0.00]						
09061#			[Mf System / 0.00]						
09062#			[Mf System / 0.00]						
09063#	R0025:CO073	Dfmn 1-D NND	AREBA-QPEAKm-TpeakDte.hh:mm	Rvmm R.C.	Dfwmc
09064#	ROUTE CHANNEL	>	1.0 01:5-N	536.42	5.154 Ndate	31:16	30.13 405	0.00	
09065#			[ARECm 4.00; IARECm 4.00]						
09066#			[RfW 1.00] out <	1.0 01:5-N	536.42	5.154 Ndate	31:16	30.13 405	0.00
09067#			[L/S/m 4.99; SMM 3.00]						
09068#			[Vmax = 569; Dmax = 2.314]						
09069#			# Catchment OKEEFE						
09070#			# To O'Keefe drain (north of the Jock)						
09071#			# Developed with area added per the NODATA HYDRO model (Citi-Gate 2014)						
09072#			# -2020-12-01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area 513.02 HA)						
09073#			# -2020-12-01 add Okeefe model per the NODATA HYDRO model (Citi-Gate 2014)						
09074#									
09075#	R0025:CO074	Dfmn 1-D NND	AREBA-QPEAKm-TpeakDte.hh:mm	Rvmm R.C.	Dfwmc
09076#	CNTINUES STANNHD		1.0 01:5-N	63.72	9.917 Ndate	28:58	22.21 299	0.00	
09077#			[AREC 4.00; SMN 430.01; SKE 010]						
09078#			[InterEvent Time 12.00]						
09079#									
09080#	R0025:CO075	Dfmn 1-D NND	AREBA-QPEAKm-TpeakDte.hh:mm	Rvmm R.C.	Dfwmc
09081#	ROUTE CHANNEL	>	1.0 02:0-1	63.72	9.917 Ndate	28:58	22.21 n/a	0.00	
09082#			[RfW 1.00] out <	1.0 01:0-1	63.72	9.917 Ndate	29:15	22.21 n/a	0.00
09083#			[L/S/m 960 / 630/043]						
09084#			[Vmax = 829; Dmax = 3.981]						
09085#	R0025:CO076	Dfmn 1-D NND	AREBA-QPEAKm-TpeakDte.hh:mm	Rvmm R.C.	Dfwmc
09086#	CNTINUES STANNHD		1.0 01:0-2	28.61	3.310 Ndate	29:13	20.55 276	0.00	
09087#			[Cm 54.0; Nc 3.00; Tm 6.01]						
09088#			[AREC 4.00; SMN 76.32; SMM 508.81; SKE 010]						
09089#			[InterEvent Time 12.00]						
09090#	R0025:CO077	Dfmn 1-D NND	AREBA-QPEAKm-TpeakDte.hh:mm	Rvmm R.C.	Dfwmc
09091#	CNTINUES STANNHD		1.0 01:0-4	46.94	4.226 Ndate	29:00	15.62 210	0.00	
09092#			[Cm 61.0; Nc 3.00; Tm 9.01]						
09093#			[AREC 4.00; SMN 104.59; SMM 697.25; SKE 010]						
09094#			[InterEvent Time 12.00]						
09095#	R0025:CO078	Dfmn 1-D NND	AREBA-QPEAKm-TpeakDte.hh:mm	Rvmm R.C.	Dfwmc
09096#	ADD HYD		1.0 02:0-1	63.72	9.917 Ndate	29:15	22.21 n/a	0.00	
09097#			+ 1.0 02:0-1	39.67	1.013 Ndate	28:23	24.45 n/a	0.00	
09098#			+ 1.0 02:0-1	46.94	4.226 Ndate	29:00	15.62 n/a	0.00	
09099#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09100#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09101#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09102#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09103#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09104#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09105#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09106#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09107#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09108#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09109#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09110#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09111#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09112#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09113#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09114#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09115#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09116#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09117#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09118#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09119#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09120#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09121#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09122#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09123#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09124#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09125#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09126#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09127#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09128#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09129#			+ 1.0 02:0-1	139.27	1.623 Ndate	29:11	19.65 n/a	0.00	
09130#		</							

Table with multiple columns containing technical data, including area names, dimensions, coordinates, and various system identifiers. The table is organized into sections by area name, such as ROUTE RESERVOIR, COMPUTE DUAL/D, and CONTINUOUS STANDIPD.


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12221      remark Total Flow at Jockvale Road
12222 #
12223 # Hydrograph from Jockvale Road routed to Heart's Desire
12224 # Channel X-Section obtained from RMA Hydraulic Model - Station 689
12225 #
12226 R0025: CH0428 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
12227 ROUTE CHANNEL 2 1.0 02:SN.D 55194.86 104.129 No.date 39:29 50.23 n/a 0.000
12228 [RDE 1.00] out< 1.0 01:N.DE 55194.86 104.140 No.date 39:45 29.33 n/a 0.000
12229 [L/S= 1962 / 222] (Vmax= 4.48; Dmax= 2.264)
12230 #
12231 #####
12232 # Catchment DESIRE
12233 # - To Jock River (north of the Jock)
12234 # Rural-estate subdivision, Heart's Desire Community)
12235 #
12236 R0025: CH0429 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
12237 CONTI NUS NASHHD 1.0 01: DESIRE 23.78 2.161 No.date 28:03 40.77 548 0.000
12238 [SM= 25; TM= 25]
12239 [RDE 1.00] out< 1.0 02:SN.D 55194.86 104.129 No.date 39:29 50.23 n/a 0.000
12240 [L/S= 1962 / 222] (Vmax= 4.48; Dmax= 2.264)
12241 #####
12242 # Catchment JOCKVA
12243 # - Residential development & golf course
12244 # JFSA 2021-01-11 update JOCKVA after updating CORP GA per IIR GROUP, July 2008.
12245 # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX.LAND 32.5 ha as
12246 #
12247 R0025: CH0430 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
12248 CONTI NUS NASHHD 1.0 01: JOCKVA 225.13 21.797 No.date 28:07 50.08 673 0.000
12249 [SM= 25; TM= 25]
12250 #
12251 #####
12252 # Catchment JOCKVA
12253 # - Residential development & golf course
12254 # JFSA 2021-01-11 update JOCKVA after updating CORP GA per IIR GROUP, July 2008.
12255 # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX.LAND 32.5 ha as
12256 #
12257 R0025: CH0431 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
12258 CONTI NUS NASHHD 1.0 01: JOCKVA 225.13 21.797 No.date 28:07 50.08 673 0.000
12259 [SM= 25; TM= 25]
12260 #
12261 #####
12262 # Catchment JOCKVA
12263 # - Residential development & golf course
12264 # JFSA 2021-01-11 update JOCKVA after updating CORP GA per IIR GROUP, July 2008.
12265 # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX.LAND 32.5 ha as
12266 #
12267 R0025: CH0432 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
12268 CONTI NUS NASHHD 1.0 01: JOCKVA 225.13 21.797 No.date 28:07 50.08 673 0.000
12269 [SM= 25; TM= 25]
12270 #
12271 #####
12272 # Catchment JOCKVA
12273 # - Residential development & golf course
12274 # JFSA 2021-01-11 update JOCKVA after updating CORP GA per IIR GROUP, July 2008.
12275 # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX.LAND 32.5 ha as
12276 #
12277 R0025: CH0433 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
12278 CONTI NUS NASHHD 1.0 01: JOCKVA 225.13 21.797 No.date 28:07 50.08 673 0.000
12279 [SM= 25; TM= 25]
12280 #
12281 #####
12282 # Catchment JOCKVA
12283 # - Residential development & golf course
12284 # JFSA 2021-01-11 update JOCKVA after updating CORP GA per IIR GROUP, July 2008.
12285 # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX.LAND 32.5 ha as
12286 #
12287 R0025: CH0434 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
12288 CONTI NUS NASHHD 1.0 01: JOCKVA 225.13 21.797 No.date 28:07 50.08 673 0.000
12289 [SM= 25; TM= 25]
12290 #
12291 #####
12292 # Catchment JOCKVA
12293 # - Residential development & golf course
12294 # JFSA 2021-01-11 update JOCKVA after updating CORP GA per IIR GROUP, July 2008.
12295 # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX.LAND 32.5 ha as
12296 #
12297 R0025: CH0435 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
12298 CONTI NUS NASHHD 1.0 01: JOCKVA 225.13 21.797 No.date 28:07 50.08 673 0.000
12299 [SM= 25; TM= 25]
12300 #
12301 #####
12302 # Catchment JOCKVA
12303 # - Residential development & golf course
12304 # JFSA 2021-01-11 update JOCKVA after updating CORP GA per IIR GROUP, July 2008.
12305 # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX.LAND 32.5 ha as
12306 #
12307 R0025: CH0436 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
12308 CONTI NUS NASHHD 1.0 01: JOCKVA 225.13 21.797 No.date 28:07 50.08 673 0.000
12309 [SM= 25; TM= 25]
12310 #
12311 #####
12312 # Catchment JOCKVA
12313 # - Residential development & golf course
12314 # JFSA 2021-01-11 update JOCKVA after updating CORP GA per IIR GROUP, July 2008.
12315 # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX.LAND 32.5 ha as
12316 #
12317 R0025: CH0437 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
12318 CONTI NUS NASHHD 1.0 01: JOCKVA 225.13 21.797 No.date 28:07 50.08 673 0.000
12319 [SM= 25; TM= 25]
12320 #
12321 #####
12322 # Catchment JOCKVA
12323 # - Residential development & golf course
12324 # JFSA 2021-01-11 update JOCKVA after updating CORP GA per IIR GROUP, July 2008.
12325 # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX.LAND 32.5 ha as
12326 #
12327 R0025: CH0438 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
12328 CONTI NUS NASHHD 1.0 01: JOCKVA 225.13 21.797 No.date 28:07 50.08 673 0.000
12329 [SM= 25; TM= 25]
12330 #
12331 #####
12332 # Catchment JOCKVA
12333 # - Residential development & golf course
12334 # JFSA 2021-01-11 update JOCKVA after updating CORP GA per IIR GROUP, July 2008.
12335 # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX.LAND 32.5 ha as
12336 #
12337 R0025: CH0439 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
12338 CONTI NUS NASHHD 1.0 01: JOCKVA 225.13 21.797 No.date 28:07 50.08 673 0.000
12339 [SM= 25; TM= 25]
12340 #
12341 #####
12342 # Catchment JOCKVA
12343 # - Residential development & golf course
12344 # JFSA 2021-01-11 update JOCKVA after updating CORP GA per IIR GROUP, July 2008.
12345 # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX.LAND 32.5 ha as
12346 #
12347 R0025: CH0440 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
12348 CONTI NUS NASHHD 1.0 01: JOCKVA 225.13 21.797 No.date 28:07 50.08 673 0.000
12349 [SM= 25; TM= 25]
12350 #
12351 #####
12352 # Catchment JOCKVA
12353 # - Residential development & golf course
12354 # JFSA 2021-01-11 update JOCKVA after updating CORP GA per IIR GROUP, July 2008.
12355 # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX.LAND 32.5 ha as
12356 #
12357 R0025: CH0441 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
12358 CONTI NUS NASHHD 1.0 01: JOCKVA 225.13 21.797 No.date 28:07 50.08 673 0.000
12359 [SM= 25; TM= 25]
12360 #
12361 #####
12362 # Catchment JOCKVA
12363 # - Residential development & golf course
12364 # JFSA 2021-01-11 update JOCKVA after updating CORP GA per IIR GROUP, July 2008.
12365 # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX.LAND 32.5 ha as
12366 #
12367 R0025: CH0442 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
12368 CONTI NUS NASHHD 1.0 01: JOCKVA 225.13 21.797 No.date 28:07 50.08 673 0.000
12369 [SM= 25; TM= 25]
12370 #
12371 #####
12372 # Catchment JOCKVA
12373 # - Residential development & golf course
12374 # JFSA 2021-01-11 update JOCKVA after updating CORP GA per IIR GROUP, July 2008.
12375 # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX.LAND 32.5 ha as
12376 #
12377 R0025: CH0443 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
12378 CONTI NUS NASHHD 1.0 01: JOCKVA 225.13 21.797 No.date 28:07 50.08 673 0.000
12379 [SM= 25; TM= 25]
12380 #
12381 #####
12382 # Catchment JOCKVA
12383 # - Residential development & golf course
12384 # JFSA 2021-01-11 update JOCKVA after updating CORP GA per IIR GROUP, July 2008.
12385 # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX.LAND 32.5 ha as
12386 #
12387 R0025: CH0444 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
12388 CONTI NUS NASHHD 1.0 01: JOCKVA 225.13 21.797 No.date 28:07 50.08 673 0.000
12389 [SM= 25; TM= 25]
12390 #
12391 #####
12392 # Catchment JOCKVA
12393 # - Residential development & golf course
12394 # JFSA 2021-01-11 update JOCKVA after updating CORP GA per IIR GROUP, July 2008.
12395 # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX.LAND 32.5 ha as
12396 #
12397 R0025: CH0445 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
12398 CONTI NUS NASHHD 1.0 01: JOCKVA 225.13 21.797 No.date 28:07 50.08 673 0.000
12399 [SM= 25; TM= 25]
12400 #
12401 #####
12402 # Catchment JOCKVA
12403 # - Residential development & golf course
12404 # JFSA 2021-01-11 update JOCKVA after updating CORP GA per IIR GROUP, July 2008.
12405 # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX.LAND 32.5 ha as
12406 #
12407 R0025: CH0446 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
12408 CONTI NUS NASHHD 1.0 01: JOCKVA 225.13 21.797 No.date 28:07 50.08 673 0.000
12409 [SM= 25; TM= 25]

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14408# CONTI NUS NASHHD 1.0 01:JR.ASH 1781.00 16.834 No.date 32:39 36.85 452 0.000
14409# [CN= 72.0; No 3.00; Tm= 3.11]
14410# [IAR=C 4.00; SM= 39.75; SMX=264.99; SK= 0.010]
14411# [InterEventTime= 12.000]
14412# R0050: CH0010 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14413# CONTI NUS NASHHD 1.0 01:SW.I1 500.00 9.061 No.date 29:21 31.73 389 0.000
14414# [CN= 66.0; No 3.00; Tm= 5.29]
14415# [IAR=C 4.00; SM= 32.62; SMX=350.79; SK= 0.010]
14416# [InterEventTime= 12.000]
14417# #
14418# The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
14419# # of 1.80
14420# R0050: CH0011 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14421# CONTI NUS NASHHD 1.0 01:SW.IK 4876.00 31.024 No.date 39:59 31.73 389 0.000
14422# [CN= 66.0; No 3.00; Tm= 5.29]
14423# [IAR=C 4.00; SM= 32.62; SMX=350.79; SK= 0.010]
14424# [InterEventTime= 12.000]
14425# #
14426# The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
14427# # of 1.52
14428# R0050: CH0012 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14429# CONTI NUS NASHHD 1.0 01:SW.L0 5666.00 32.402 No.date 37:52 36.85 452 0.000
14430# [CN= 72.0; No 3.00; Tm= 8.00]
14431# [IAR=C 4.00; SM= 39.75; SMX=264.99; SK= 0.010]
14432# [InterEventTime= 12.000]
14433# #
14434# The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
14435# # of 1.25
14436# R0050: CH0013 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14437# CONTI NUS NASHHD 1.0 01:RL.KC 4376.00 31.024 No.date 39:59 31.73 389 0.000
14438# [CN= 66.0; No 3.00; Tm= 1.00]
14439# [IAR=C 4.00; SM= 32.62; SMX=350.79; SK= 0.010]
14440# [InterEventTime= 12.000]
14441# #
14442# The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
14443# # of 1.68
14444# R0050: CH0014 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14445# CONTI NUS NASHHD 1.0 01:SN.CK 1132.00 14.039 No.date 30:53 35.35 424 0.000
14446# [CN= 70.0; No 3.00; Tm= 2.51]
14447# [IAR=C 4.00; SM= 36.75; SMX=287.10; SK= 0.010]
14448# [InterEventTime= 12.000]
14449# #
14450# The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
14451# # of 1.82
14452# R0050: CH0015 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14453# CONTI NUS NASHHD 1.0 01:NC.CK 4464.00 15.472 No.date 39:59 28.95 355 0.000
14454# [CN= 72.0; No 3.00; Tm= 8.00]
14455# [IAR=C 4.00; SM= 61.90; SMX=412.66; SK= 0.010]
14456# [InterEventTime= 12.000]
14457# #
14458# The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
14459# # of 1.50
14460# R0050: CH0016 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14461# CONTI NUS NASHHD 1.0 01:SW.L8 131.00 1.740 No.date 28:57 29.64 364 0.000
14462# [CN= 63.0; No 3.00; Tm= 5.90]
14463# [IAR=C 4.00; SM= 32.62; SMX=396.11; SK= 0.010]
14464# [InterEventTime= 12.000]
14465# #
14466# The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
14467# # of 1.65
14468# R0050: CH0017 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14469# CONTI NUS NASHHD 1.0 01:HL.RL 3854.00 18.180 No.date 38:32 31.73 389 0.000
14470# [CN= 66.0; No 3.00; Tm= 8.42]
14471# [IAR=C 4.00; SM= 32.62; SMX=350.79; SK= 0.010]
14472# [InterEventTime= 12.000]
14473# #
14474# The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
14475# # of 1.32
14476# R0050: CH0018 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14477# CONTI NUS NASHHD 1.0 01:SW.7 3197.00 19.937 No.date 36:23 25.61 314 0.000
14478# [CN= 57.0; No 3.00; Tm= 6.65]
14479# [IAR=C 4.00; SM= 36.32; SMX=508.81; SK= 0.010]
14480# [InterEventTime= 12.000]
14481# #
14482# The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
14483# # of 1.57
14484# R0050: CH0019 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14485# CONTI NUS NASHHD 1.0 01:SW.6 165.00 1.285 No.date 35:02 32.44 398 0.000
14486# [CN= 67.0; No 3.00; Tm= 4.18]
14487# [IAR=C 4.00; SM= 30.55; SMX=336.97; SK= 0.010]
14488# [InterEventTime= 12.000]
14489# #
14490# The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
14491# # of 1.67
14492# R0050: CH0020 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14493# CONTI NUS NASHHD 1.0 01:VGL.RL 1332.00 9.332 No.date 35:12 36.85 452 0.000
14494# [CN= 72.0; No 3.00; Tm= 5.91]
14495# [IAR=C 4.00; SM= 39.75; SMX=264.99; SK= 0.010]
14496# [InterEventTime= 12.000]
14497# R0050: CH0021 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14498# CONTI NUS NASHHD 1.0 01:SW.5 224.00 8.187 No.date 28:45 41.51 509 0.000
14499# [CN= 70.0; No 3.00; Tm= 7.51]
14500# [IAR=C 4.00; SM= 31.15; SMX=207.66; SK= 0.010]
14501# [InterEventTime= 12.000]
14502# #
14503# The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
14504# # of 1.20
14505# R0050: CH0022 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14506# CONTI NUS NASHHD 1.0 01:HL.CK 4945.00 44.623 No.date 33:18 38.37 471 0.000
14507# [CN= 74.0; No 3.00; Tm= 4.45]
14508# [IAR=C 4.00; SM= 36.67; SMX=244.49; SK= 0.010]
14509# [InterEventTime= 12.000]
14510# R0050: CH0023 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14511# CONTI NUS NASHHD 1.0 01:SW.S2 20.00 0.943 No.date 28:35 45.60 560 0.000
14512# [CN= 81.0; No 3.00; Tm= 6.21]
14513# [IAR=C 4.00; SM= 25.21; SMX=168.09; SK= 0.010]
14514# [InterEventTime= 12.000]
14515# #
14516# The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
14517# # of 1.64
14518# R0050: CH0024 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14519# CONTI NUS NASHHD 1.0 01:SW.S1 1412.00 8.794 No.date 37:48 39.93 490 0.000
14520# [CN= 75.0; No 3.00; Tm= 8.00]
14521# [IAR=C 4.00; SM= 33.81; SMX=225.43; SK= 0.010]
14522# [InterEventTime= 12.000]
14523# R0050: CH0025 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14524# CONTI NUS NASHHD 1.0 01:SW.4 585.00 12.896 No.date 29:55 45.60 560 0.000
14525# [CN= 70.0; No 3.00; Tm= 3.25]
14526# [IAR=C 4.00; SM= 25.21; SMX=168.09; SK= 0.010]
14527# [InterEventTime= 12.000]
14528# R0050: CH0026 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14529# CONTI NUS NASHHD 1.0 01:LM.LCK 1021.00 17.059 No.date 30:46 44.77 549 0.000
14530# [CN= 80.0; No 3.00; Tm= 2.46]
14531# [IAR=C 4.00; SM= 26.32; SMX=175.50; SK= 0.010]
14532# [InterEventTime= 12.000]
14533# R0050: CH0027 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14534# CONTI NUS NASHHD 1.0 01:SW.2 177.00 6.469 No.date 28:45 41.51 509 0.000
14535# [CN= 70.0; No 3.00; Tm= 6.65]
14536# [IAR=C 4.00; SM= 31.15; SMX=207.66; SK= 0.010]
14537# [InterEventTime= 12.000]
14538# R0050: CH0028 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14539# CONTI NUS NASHHD 1.0 01:SM.LR 1122.00 15.544 No.date 31:43 45.60 560 0.000
14540# [CN= 81.0; No 3.00; Tm= 3.25]
14541# [IAR=C 4.00; SM= 25.21; SMX=168.09; SK= 0.010]
14542# [InterEventTime= 12.000]
14543# R0050: CH0029 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14544# CONTI NUS NASHHD 1.0 01:ML.RL 2737.00 34.946 No.date 31:29 40.72 500 0.000
14545# [CN= 76.0; No 3.00; Tm= 3.63]
14546# [IAR=C 4.00; SM= 32.46; SMX=216.39; SK= 0.010]
14547# [InterEventTime= 12.000]
14548# #
14549# Routing hydrographs
14550# #
14551# Starting with the addition of Jock River Headwater and Subwatershed 13
14552# #
14553# R0050: CH0030 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14554# ADD RHD 3680.00 18.440 No.date 36:55 30.33 372 0.000
14555# [IAR=C 4.00; SM= 32.46; SMX=216.39; SK= 0.010]
14556# [CN= 76.0; No 3.00; Tm= 3.63]
14557# #
14558# Sum of hydrographs from Node 13 routed to Node 13A
14559# # (Approximate cross-section - see cross-section 258)
14560# Use n=0.04 for summer conditions and n=0.025 for spring conditions
14561# #
14562# R0050: CH0031 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14563# ROUTE CHANNEL 1 1.0 02:SN.L3 4651.00 23.559 No.date 35:24 29.90 n/a 0.000
14564# [RDE 1.00] out< 1.0 01:SN.A 4651.00 19.136 No.date 39:54 27.68 n/a 0.000
14565# [L/S= 9074.7 / 022/040]
14566# [Vmax= 574.0; Dmax= 9.920]
14567# #
14568# Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
14569# #
14570# R0050: CH0032 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14571# ADD RHD 3074.00 19.136 No.date 39:09 29.90 n/a 0.000
14572# [CN= 85.0; No 3.00; Tm= 1.31]
14573# [IAR=C 4.00; SM= 11.00; SNIA 7725.00 27.939 No.date 39:54 27.68 n/a 0.000]
14574# #
14575# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
14576# #
14577# R0050: CH0033 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14578# ROUTE RESERVOIR 1 1.0 02:SN.LA 4651.00 3.808 No.date 61:35 27.67 n/a 0.000
14579# [RDE 1.00] out< 1.0 01:RES_GM 7725.00 3.808 No.date 61:35 27.67 n/a 0.000
14580# [IAR=C 4.00; SM= 32.46; SMX=216.39; SK= 0.010]
14581# [IAR=C 4.00; SM= 32.46; SMX=216.39; SK= 0.010]
14582# #
14583# R0050: CH0034 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14584# SAVE RHD 7725.00 3.808 No.date 61:35 27.67 n/a 0.000
14585# #
14586# Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
14587# # (Approximate cross-section 258)
14588# Use n=0.04 for summer conditions and n=0.025 for spring conditions
14589# #
14590# R0050: CH0035 ..... Dfma 1-D N DND ..... AREA/A.....PEAK/Dte/hh:mm ..... Rvmm R.C. .... Dfwm
14591# ROUTE CHANNEL 1 1.0 02:RES_GM 7725.00 3.808 No.date 61:35 27.67 n/a 0.000
14592# [L/S= 9926.0 / 076/040]
14593# [Vmax= 556; Dmax= 1.541]
14594# #

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115955 # Addition of Subwatershed Lock River at Ashton to Node 12

115956 #

115957 ROUTE05: C00036..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

115958 ADD HYD + 1.0 02:SN 9506.0 18.687 Ndate 32:42 29.39 n/a .000

115959 + 1.0 02:JRA_ASH 1781.0 16.834 Ndate 32:39 36.85 n/a .000

116000 ROUTE CHANNEL + 1.0 02:SN 9506.0 18.687 Ndate 32:42 29.39 n/a .000

116001 ROUTE CHANNEL + 1.0 02:SN 9506.0 18.687 Ndate 32:42 29.39 n/a .000

116002 SAVE HYD 1.0 01:SN_N12 9506.0 18.687 Ndate 32:42 29.39 n/a .000

116003 Frame :H_S_N12

116004 remark:flow at S_N12 near Ashton

116005 #

116006 # Sum of hydrographs from Node 12 routed to Node 11

116007 # (Approximated cross section - see cross.section 258)

116008 # Use out.04 for storm conditions and out.025 for spring conditions

116009 #

116010 # Sum of hydrographs from Node 12 routed to Node 11 with Damsy section 248

116011 #

116012 ROUTE05: C00038..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116013 ROUTE CHANNEL + 1.0 02:SN 9506.0 18.687 Ndate 32:42 29.39 n/a .000

116014 [RfE= 1.00] out.c 1.0 01:DM1 9506.0 18.687 Ndate 32:59 29.39 n/a .000

116015 [L/S= 972 / 0.54] 051

116016 [Vmax = 751;Dmax= 3.029]

116017 #

116018 # Addition of Subwatershed 11 and No Name Creek to Node 11

116019 #

116020 ROUTE05: C00039..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116021 ADD HYD + 1.0 02:SN 9506.0 18.687 Ndate 32:59 29.39 n/a .000

116022 + 1.0 02:SW2 590.0 9.063 Ndate 29:21 31.73 n/a .000

116023 + 1.0 02:NC_CK 1917.0 12.342 Ndate 34:26 31.73 n/a .000

116024 SIMM 1.0 01:SN_N10 11923.0 32.851 Ndate 33:00 29.87 n/a .000

116025 #

116026 # Sum of hydrographs from Node 11 routed to Node 10

116027 # Section 1

116028 #

116029 ROUTE05: C00040..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116030 ROUTE CHANNEL + 1.0 02:SN_N1 11923.0 32.851 Ndate 33:00 29.87 n/a .000

116031 [RfE= 1.00] out.c 1.0 01:N0 11923.0 20.490 Ndate 40:02 29.87 n/a .000

116032 [L/S= 14028 / 157] 040

116033 [Vmax = 474;Dmax= 1.423]

116034 #

116035 # Addition of Subwatershed 10 to Node 10

116036 #

116037 ROUTE05: C00041..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116038 ADD HYD + 1.0 02:SN 11923.0 20.490 Ndate 40:02 29.87 n/a .000

116039 + 1.0 02:SW10 8966.0 32.402 Ndate 37:52 36.85 n/a .000

116040 SIMM 1.0 01:SN_N10 17589.0 52.600 Ndate 38:19 32.12 n/a .000

116041 ROUTE05: C00042..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116042 SAVE HYD 1.0 01:SN_N10 17589.0 52.600 Ndate 38:19 32.12 n/a .000

116043 Frame :H_S_N10

116044 remark:flow at S_N10: N10 +SW10

116045 # Addition of Kings Creek to S_N10

116046 #

116047 ROUTE05: C00043..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116048 ADD HYD + 1.0 02:SN 17589.0 52.600 Ndate 38:19 32.12 n/a .000

116049 + 1.0 02:KE_CK 8376.0 31.024 Ndate 39:59 31.73 n/a .000

116050 SIMM 1.0 01:SN_N10A 25965.0 82.746 Ndate 39:45 31.99 n/a .000

116051 #

116052 # Sum of hydrographs from Node 10 routed to Node 9

116053 # Section 2

116054 #

116055 ROUTE05: C00044..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116056 ROUTE CHANNEL + 1.0 02:SN_N10A 25965.0 82.746 Ndate 39:45 31.99 n/a .000

116057 [RfE= 1.00] out.c 1.0 01:N0 25965.0 80.980 Ndate 39:59 31.99 n/a .000

116058 [L/S= 3082 / 0.74] 040

116059 [Vmax = 744;Dmax= 2.015]

116060 #

116061 # Addition of Subwatershed 9 and Nichols Creek to Node 9

116062 #

116063 ROUTE05: C00045..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116064 ADD HYD + 1.0 02:SN 25965.0 80.980 Ndate 39:59 31.99 n/a .000

116065 + 1.0 02:SW10 14018.0 44.019 Ndate 30:53 35.35 n/a .000

116066 + 1.0 02:NC_CK 4164.0 15.472 Ndate 39:59 28.95 n/a .000

116067 SIMM 1.0 01:SN_N10 34864.0 54.224 Ndate 39:59 31.68 n/a .000

116068 #

116069 # Sum of hydrographs from Node 9 routed to Node 8

116070 # Section 3

116071 #

116072 ROUTE05: C00046..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116073 ROUTE CHANNEL + 1.0 02:SN_N9 31561.0 99.244 Ndate 39:59 31.68 n/a .000

116074 [RfE= 1.00] out.c 1.0 01:N8 31561.0 93.665 Ndate 39:59 31.68 n/a .000

116075 [L/S= 2269 / 0.89] 045

116076 [Vmax = 367;Dmax= 1.834]

116077 #

116078 # Addition of Subwatershed 8 and Webb's Drain to Node 8

116079 #

116080 ROUTE05: C00047..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116081 ADD HYD + 1.0 02:SN 31561.0 93.665 Ndate 39:59 31.68 n/a .000

116082 + 1.0 02:WB 2740.0 6.251 Ndate 30:53 35.35 n/a .000

116083 + 1.0 02:WB_DR 3854.0 18.180 Ndate 38:32 31.73 n/a .000

116084 SIMM 1.0 01:SN_N8 35546.0 111.843 Ndate 39:59 31.68 n/a .000

116085 #

116086 # Sum of hydrographs from Node 8 routed to Node 7

116087 # Section 4

116088 #

116089 ROUTE05: C00048..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116090 ROUTE CHANNEL + 1.0 02:SN_N8 35546.0 111.843 Ndate 39:59 31.68 n/a .000

116091 [RfE= 1.00] out.c 1.0 01:N8 35546.0 95.475 Ndate 44:55 31.68 n/a .000

116092 [L/S= 3750 / 0.53] 070

116093 [Vmax = 231;Dmax= 2.290]

116094 #

116095 # Addition of Subwatershed 7 to Node 7

116096 #

116097 ROUTE05: C00049..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116098 ADD HYD + 1.0 02:SN 35546.0 95.475 Ndate 44:55 31.68 n/a .000

116099 + 1.0 02:SW7 3197.0 13.937 Ndate 36:23 25.61 n/a .000

116100 SIMM 1.0 01:SN_N7 38743.0 102.892 Ndate 43:46 31.18 n/a .000

116101 ROUTE05: C00050..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116102 SAVE HYD 1.0 01:SN_N7 38743.0 102.892 Ndate 43:46 31.18 n/a .000

116103 Frame :H_S_N7

116104 remark:flow at S_N7: N0 + SW7

116105 # Insertion of a reservoir to simulate the effects of the Richmond Fen

116106 # Storage area and volumes were estimated from available top maps

116107 # Release rate from Fen was assumed to be controlled by the downstream

116108 # river cross-section for storm conditions. It is assumed that for up to

116109 # 0.75 m of water, the main channel of the river provided the storage. Above

116110 # this depth, the wetland starts to significantly store water.

116111 #

116112 ROUTE05: C00051..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116113 ROUTE RESERVOIR + 1.0 02:SN_N7 38743.0 102.892 Ndate 43:46 31.18 n/a .000

116114 [RfE= 1.00] out.c 1.0 01:RES_RF 38743.0 52.029 Ndate 59:07 31.18 n/a .000

116115 [MS=0.64; 4384]044

116116 ROUTE05: C00052..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116117 SAVE HYD 1.0 01:RES_RF 38743.0 52.029 Ndate 59:07 31.18 n/a .000

116118 Frame :H_RES_RF

116119 remark:outflow of Richmond Fen

116120 #

116121 # Sum of hydrographs from Node 7 routed to Node 6

116122 # Section 5

116123 #

116124 ROUTE05: C00053..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116125 ROUTE CHANNEL + 1.0 02:RES_RF 38743.0 52.029 Ndate 59:07 31.18 n/a .000

116126 [RfE= 1.00] out.c 1.0 01:N6 38743.0 51.784 Ndate 60:27 31.18 n/a .000

116127 [L/S= 827 / 0.8] 041

116128 [Vmax = 538;Dmax= 1.253]

116129 #

116130 # Addition of Subwatershed 6 and Van Gaal Drain to Node 6

116131 #

116132 ROUTE05: C00054..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116133 ADD HYD + 1.0 02:SN 38743.0 51.784 Ndate 60:27 31.18 n/a .000

116134 + 1.0 02:SW6 165.0 1.285 Ndate 33:02 32.44 n/a .000

116135 + 1.0 02:VGLDR 1332.0 9.332 Ndate 35:12 36.85 n/a .000

116136 SIMM 1.0 01:SN_N6 40420.0 51.810 Ndate 60:20 31.37 n/a .000

116137 #

116138 # Sum of hydrographs from Node 6 routed to Node 5

116139 # Section 6

116140 #

116141 ROUTE05: C00055..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116142 ROUTE CHANNEL + 1.0 02:SN_N6 40420.0 51.810 Ndate 60:20 31.37 n/a .000

116143 [RfE= 1.00] out.c 1.0 01:N5 40420.0 51.693 Ndate 61:06 31.37 n/a .000

116144 [L/S= 1852 / 0.5] 045

116145 [Vmax = 469;Dmax= 1.351]

116146 #

116147 # Addition of Subwatershed 5 and Flowing Creek to Node 5

116148 #

116149 ROUTE05: C00056..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116150 ADD HYD + 1.0 02:SN 40420.0 51.693 Ndate 61:06 31.37 n/a .000

116151 + 1.0 02:SW5 224.0 8.187 Ndate 28:45 41.51 n/a .000

116152 + 1.0 02:FJ_CK 4945.0 44.623 Ndate 33:18 38.37 n/a .000

116153 SIMM 1.0 01:SN_N5 45499.0 71.514 Ndate 34:20 32.18 n/a .000

116154 #

116155 # Sum of hydrographs from Node 5 routed to Node 5A

116156 # Section 7

116157 #

116158 ROUTE05: C00057..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116159 ROUTE CHANNEL + 1.0 02:SN_N5A 45499.0 71.514 Ndate 34:20 32.18 n/a .000

116160 [RfE= 1.00] out.c 1.0 01:NSA 45499.0 71.514 Ndate 34:15 32.18 n/a .000

116161 [L/S= 556 / 0.90] 040

116162 [Vmax = 530;Dmax= 1.290]

116163 #

116164 # Addition of Subwatershed 5A and Subwatershed 5A2 to Node 5A

116165 #

116166 ROUTE05: C00058..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116167 ADD HYD + 1.0 02:SN 45499.0 71.514 Ndate 34:15 32.18 n/a .000

116168 + 1.0 02:SW5A2 20.0 94.3 Ndate 28:35 45.60 n/a .000

116169 + 1.0 02:SW5A1 1412.0 8.794 Ndate 37:48 39.93 n/a .000

116170 SIMM 1.0 01:SN_N5A 46841.0 71.514 Ndate 34:46 32.42 n/a .000

116171 #

116172 # Sum of hydrographs from Node 5A routed to 4

116173 # Section 8

116174 #

116175 ROUTE05: C00059..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116176 ROUTE CHANNEL + 1.0 02:SN_N5A 46841.0 79.247 Ndate 34:46 32.42 n/a .000

116177 [RfE= 1.00] out.c 1.0 01:NSA 46841.0 75.833 Ndate 36:02 32.42 n/a .000

116178 [L/S= 4630 / 0.43] 035

116179 [Vmax = 874;Dmax= 3.702]

116180 #

116181 # Addition of Subwatershed 4 and Leang Creek to Node 4

116182 #

116183 ROUTE05: C00060..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116184 ADD HYD + 1.0 02:SN 46841.0 75.833 Ndate 36:02 32.42 n/a .000

116185 + 1.0 02:SW4 545.0 12.898 Ndate 29:45 45.00 n/a .000

116186 + 1.0 02:LMCK 1021.0 17.059 Ndate 30:46 47.77 n/a .000

116187 SIMM 1.0 01:SN_N4 48447.0 84.908 Ndate 35:20 32.84 n/a .000

116188 ROUTE05: C00061..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116189 SAVE HYD 1.0 01:SN_N4 48447.0 84.908 Ndate 35:20 32.84 n/a .000

116190 Frame :S_N4_0050

116191 remark:flow at S_N4

116192 #

116193 # Sum of hydrographs from Node 4 routed to Node 2

116194 # Section 9

116195 #

116196 ROUTE05: C00062..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116197 ROUTE CHANNEL + 1.0 01:SN_N4 48447.0 84.908 Ndate 35:20 32.84 n/a .000

116198 [RfE= 1.00] out.c 1.0 01:N2 48447.0 84.882 Ndate 35:30 32.84 n/a .000

116199 [L/S= 1667 / 0.60] 040

116200 [Vmax = 909;Dmax= 3.749]

116201 #

116202 # Addition of Subwatershed 2 with Mnohan Drain and Smith Drain to Node 2

116203 #

116204 ROUTE05: C00063..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116205 ADD HYD + 1.0 02:SN 48447.0 84.882 Ndate 35:30 32.84 n/a .000

116206 + 1.0 02:SW2 177.0 6.469 Ndate 28:45 41.51 n/a .000

116207 + 1.0 02:MLDR 1122.0 15.844 Ndate 29:45 45.00 n/a .000

116208 + 1.0 02:MLDR 2737.0 34.946 Ndate 31:29 40.72 n/a .000

116209 SIMM 1.0 01:SN_N2 52483.0 124.249 Ndate 35:52 33.56 n/a .000

116210 ROUTE05: C00064..... Dfma-ID NDD.....AREHA-QPEAGm-TPeakDte-bh:mm--Rvmm R.C--DfWcm

116211 SAVE HYD 1.0 01:SN_N2 52483.0 124.249 Ndate 35:52 33.56 n/a .000

116212 Frame :H_S_N2

116213 remark:flow at S_N2 Jock River Gauge at Modoc Dr.

116214 #

116215 # Sum of hydrographs from Node 2 routed to Node 1

116216 # Section 10

116217 #

116218 #

116219 #

116220 #

116221 #

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116223 #

116224 #

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116297 #

116298 #

116299 #

116300 #

Table with columns for ID, description, and various parameters (e.g., flow rate, velocity, coordinates). The table lists numerous entries, each with a unique identifier and a detailed description of a specific flow or system component. The descriptions often include flow direction, flow rate, and velocity. The table is organized into sections, with some entries having sub-headers or titles.

127175 R0505:CO0213.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

127188 CONTINUES STANDBY 1.0 01:KB:ALL 119.40 17.558 No.date 28.04 63.49 779 0000

127189 [X.M.P. 60:TIMP=63]

127200 [IBREC= 4.00: IAREBER= 4.00]

127201 [Pervious area: IAPER= 4.67:SLP=2.00:LG= 40:MN= 250:SCP= 0]

127202 [Impervious area: IAIM= 1.57:SLP=2.00:LG= 892:MN= 013:SCI= 0]

127210 [IBREC= 4.00: IAREBER= 4.00]

127211 [X.M.P. 31.15: SMM=207.66: SKE= 010]

127225 R0505:CO0214.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

127226 ADD IHD 1.0 01:KB:01A 49.40 17.358 No.date 28.04 63.49 n/a 0000

127227 MJOR SYSTEM 1.0 02:KB:01M 49.40 17.358 No.date 28.04 63.49 n/a 0000

127228 MNR SYSTEM 1.0 03:KB:01N 49.40 17.358 No.date 28.04 63.49 n/a 0000

127229 R0505:CO0215.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

127230 SAVE IHD 1.0 01:KB:ALL 119.47 17.371 No.date 28.04 63.49 n/a 0000

127231 [X.M.P. WCLAR.0050]

127232 remark: Total Flow at West Clark

127233 West Clark Pond

127235 Rating curve obtained from Barbavren South SMS modeling

127236 Tributary Drainage Area to MS Pond 2 = 241 ha

127237

127288 R0505:CO0216.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

127289 ROUTE CHANNEL 1.0 02:KB:ALL 119.47 17.371 No.date 28.04 63.49 n/a 0000

127290 overflow sw 1.0 01:MB:P2 119.47 10.246 No.date 28.16 63.49 n/a 0000

127291 [MKSollected=00:0760E3] Tot Of Vol= 0.000E+00, N Of Cr= 0, Tot DirOfV= 0.0 r/s

127292

127293 R0505:CO0217.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

127294 ADD IHD 1.0 02:KB:CE 54118.36 133.007 No.date 33.45 33.87 n/a 0000

127295 + 1.0 02:KB:1-DIR 3.28 .018 No.date 29.14 63.98 n/a 0000

127296 + 1.0 02:KB:1-DR 12.84 .018 No.date 29.18 64.12 n/a 0000

127297 + 1.0 02:KB:1-DR 12.84 .018 No.date 29.18 64.12 n/a 0000

127298 + 1.0 02:KB:1-DR 2.03 .024 No.date 29.12 64.19 n/a 0000

127299 + 1.0 02:KB:1-DR 0.00 0.000 No.date 0.00 0.00 n/a 0000

127300 + 1.0 02:MB:P2 119.47 10.246 No.date 28.16 63.49 n/a 0000

127301 + 1.0 01:SN:CE 54253.95 134.004 No.date 33.44 33.95 n/a 0000

127302 R0505:CO0218.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

127303 SAVE IHD 1.0 01:KB:ALL 134.004 No.date 33.44 33.95 n/a 0000

127304 [X.M.P. SN CE.0050]

127305 remark: Total Flow before Station 5737 on Jack River

127306 Channel X-Section obtained from RVCA Hydraulic Model - Station 5737

127307 # 2021-02-23 add station 5737 before station 5002. Station 5737 was extracted from the HEC-RAS model T:\PROJ\1474-10\De

127308 # JFSA 2021-02-19 Change to 375 ft water surface elevation at station 5737 because of adding station 5737 be

127309 R0505:CO0219.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

127310 ROUTE CHANNEL 1.0 02:KB:ALL 54279.41 126.128 No.date 35.58 33.96 n/a 0000

127311 [RDR= 1.00] out s 1.0 01:5737 54253.95 125.921 No.date 35.58 33.95 n/a 0000

127312 [L/S= 245 / 0957 / 051]

127313 [X.M.P. Dmax= 827: Dmax= 5.276]

127368 R0505:CO0220.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

127369 ADD IHD 1.0 02:KB:DIR 54253.95 134.004 No.date 35.58 33.95 n/a 0000

127370 + 1.0 02:KB:1-DR 21.67 .250 No.date 29.21 64.14 n/a 0000

127371 + 1.0 02:KB:1-DR 7.75 .148 No.date 29.11 64.45 n/a 0000

127372 + 1.0 02:KB:1-DR 2.03 .024 No.date 29.12 64.19 n/a 0000

127373 + 1.0 02:KB:1-DR 0.00 0.000 No.date 0.00 0.00 n/a 0000

127374 + 1.0 02:KB:1-DR 0.00 0.000 No.date 0.00 0.00 n/a 0000

127375 + 1.0 02:KB:1-DR 0.00 0.000 No.date 0.00 0.00 n/a 0000

127376 + 1.0 02:KB:1-DR 0.00 0.000 No.date 0.00 0.00 n/a 0000

127377 R0505:CO0221.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

127378 SAVE IHD 1.0 01:KB:ALL 126.128 No.date 35.58 33.96 n/a 0000

127379 [X.M.P. 5002.0050]

127380 remark: Total Flow before Station 5002 on Jack River

127381 Channel X-Section obtained from RVCA Hydraulic Model - Station 5002

127382 # Hydrograph from Node West Clark Drain routed to Node at West Clark Drain

127383 # Hydrograph from Node West Clark Drain routed to Node at West Clark Drain

127384 # Hydrograph from Node West Clark Drain routed to Node at West Clark Drain

127385 # Hydrograph from Node West Clark Drain routed to Node at West Clark Drain

127386 # Hydrograph from Node West Clark Drain routed to Node at West Clark Drain

127387 # Hydrograph from Node West Clark Drain routed to Node at West Clark Drain

127388 # Hydrograph from Node West Clark Drain routed to Node at West Clark Drain

127389 # Hydrograph from Node West Clark Drain routed to Node at West Clark Drain

127390 # Hydrograph from Node West Clark Drain routed to Node at West Clark Drain

127391 # Hydrograph from Node West Clark Drain routed to Node at West Clark Drain

127392 # Hydrograph from Node West Clark Drain routed to Node at West Clark Drain

127393 R0505:CO0222.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

127394 ROUTE CHANNEL 1.0 02:KB:ALL 54279.41 126.128 No.date 35.58 33.96 n/a 0000

127395 + RDR= 1.00] out s 1.0 01:5737 54279.41 126.128 No.date 35.58 33.96 n/a 0000

127396 [L/S= 245 / 0957 / 051]

127397 [X.M.P. 245: Dmax= 2.907]

127398

127399 # Hydrograph from Node West Clark Drain routed to Node at West Clark Drain

127400 # Channel X-Section obtained from RVCA Hydraulic Model - Station 4534

128001

128002 R0505:CO0223.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

128003 ROUTE CHANNEL 1.0 02:KB:ALL 54279.41 126.128 No.date 36.27 33.96 n/a 0000

128004 + RDR= 1.00] out s 1.0 01:5737 54279.41 126.128 No.date 36.27 33.96 n/a 0000

128005 [L/S= 1020 / 0501 / 051]

128006

128007 # Catchment Run In

128008 To Kennedy-Burnett SWM Facility

128009 Outlets to Frasier-Creek drain (north of the Jock)

128010 Median velocity retained from statistical analysis

128011

128012 Rating curve obtained from URPR

128013 Tributary Drainage Area to MS Pond 160 ha

128014 Existing Kennedy-Burnett SWM Facility

128015

128016

128017

128018 R0505:CO0224.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

128019 CONTINUES STANDBY 1.0 01:KB:01A 40.82 4.812 No.date 28.10 33.07 406 0000

128020 [X.M.P. TIMP= 10]

128021 [IBREC= 4.00: IAREBER= 4.00]

128022 [Pervious area: IAPER= 4.67:SLP=2.00:LG= 40:MN= 250:SCP= 0]

128023 [Impervious area: IAIM= 1.57:SLP=2.00:LG= 252:MN= 013:SCI= 0]

128024 [IBREC= 4.00: IAREBER= 4.00]

128025 R0505:CO0225.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

128026 COMPUTE DUAL IHD 1.0 01:KB:01A 40.82 4.812 No.date 28.10 33.07 n/a 0000

128027 MJOR SYSTEM 1.0 02:KB:01M 40.82 4.812 No.date 28.10 33.07 n/a 0000

128028 MNR SYSTEM 1.0 03:KB:01N 40.82 4.812 No.date 28.10 33.14 n/a 0000

128029 [MYSys= 1.01:01:01A] Tot Of Vol= 0.000E+00, N Of Cr= 0, Tot DirOfV= 0.0 r/s

128030 R0505:CO0226.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

128031 ADD IHD 1.0 02:KB:01M 40.82 4.812 No.date 28.10 33.14 n/a 0000

128032 + 1.0 02:KB:01M 40.82 4.812 No.date 28.10 33.14 n/a 0000

128033 SIM 1.0 01:KB:01A 40.82 4.812 No.date 28.10 33.14 n/a 0000

128034 CONTINUES STANDBY 1.0 01:KB:01A 40.82 4.812 No.date 28.10 33.14 n/a 0000

128035 [X.M.P. 19-TIMP= 38]

128036 [IBREC= 4.00: IAREBER= 4.00]

128037 [Pervious area: IAPER= 4.67:SLP=2.00:LG= 40:MN= 250:SCP= 0]

128038 [Impervious area: IAIM= 1.57:SLP=2.00:LG= 421:MN= 013:SCI= 0]

128039 [IBREC= 4.00: IAREBER= 4.00]

128040 R0505:CO0227.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

128041 COMPUTE DUAL IHD 1.0 01:KB:01M 31.10 3.541 No.date 28.07 36.47 n/a 0000

128042 MJOR SYSTEM 1.0 02:KB:01M 31.10 3.541 No.date 28.07 36.47 n/a 0000

128043 MNR SYSTEM 1.0 03:KB:01N 31.10 3.541 No.date 28.07 36.47 n/a 0000

128044 [MYSys= 1.01:01:01M] Tot Of Vol= 0.000E+00, N Of Cr= 0, Tot DirOfV= 0.0 r/s

128045 R0505:CO0228.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

128046 ADD IHD 1.0 02:KB:01M 31.10 3.541 No.date 28.07 36.47 n/a 0000

128047 + 1.0 02:KB:01M 31.10 3.541 No.date 28.07 36.47 n/a 0000

128048 SIM 1.0 01:KB:01M 31.10 3.541 No.date 28.07 36.47 n/a 0000

128049 CONTINUES STANDBY 1.0 01:KB:01M 31.10 3.541 No.date 28.07 36.47 n/a 0000

128050 [X.M.P. 20-TIMP= 41]

128051 [IBREC= 4.00: IAREBER= 4.00]

128052 [Pervious area: IAPER= 4.67:SLP=2.00:LG= 40:MN= 250:SCP= 0]

128053 [Impervious area: IAIM= 79:SLP= 2.00:LG= 303:MN= 013:SCI= 0]

128054 [IBREC= 4.00: IAREBER= 4.00]

128055 R0505:CO0229.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

128056 COMPUTE DUAL IHD 1.0 01:KB:01C 13.78 1.263 No.date 28.04 37.72 n/a 0000

128057 MJOR SYSTEM 1.0 02:KB:01C 13.78 1.263 No.date 28.04 37.72 n/a 0000

128058 MNR SYSTEM 1.0 03:KB:01N 13.78 1.263 No.date 28.04 37.72 n/a 0000

128059 [MYSys= 1.01:01:01C] Tot Of Vol= 0.000E+00, N Of Cr= 0, Tot DirOfV= 0.0 r/s

128060 R0505:CO0230.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

128061 ADD IHD 1.0 02:KB:01C 13.78 1.263 No.date 28.04 37.72 n/a 0000

128062 + 1.0 02:KB:01C 13.78 1.263 No.date 28.04 37.72 n/a 0000

128063 SIM 1.0 01:KB:01C 13.78 1.263 No.date 28.04 37.72 n/a 0000

128064 CONTINUES STANDBY 1.0 01:KB:01C 13.78 1.263 No.date 28.04 37.72 n/a 0000

128065 [X.M.P. 20-TIMP= 39]

128066 [IBREC= 4.00: IAREBER= 4.00]

128067 [Pervious area: IAPER= 4.67:SLP=2.00:LG= 40:MN= 250:SCP= 0]

128068 [Impervious area: IAIM= 79:SLP= 2.00:LG= 303:MN= 013:SCI= 0]

128069 [IBREC= 4.00: IAREBER= 4.00]

128070 R0505:CO0231.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

128071 COMPUTE DUAL IHD 1.0 01:KB:03 84.78 11.833 No.date 28.07 37.17 456 0000

128072 MJOR SYSTEM 1.0 02:KB:03 84.78 11.833 No.date 28.07 37.17 n/a 0000

128073 MNR SYSTEM 1.0 03:KB:03N 84.78 11.833 No.date 28.07 37.17 n/a 0000

128074 [MYSys= 1.01:01:03] Tot Of Vol= 0.000E+00, N Of Cr= 0, Tot DirOfV= 0.0 r/s

128075 R0505:CO0232.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

128076 ADD IHD 1.0 02:KB:03 84.78 11.833 No.date 28.07 37.17 n/a 0000

128077 + 1.0 02:KB:03 84.78 11.833 No.date 28.07 37.17 n/a 0000

128078 SIM 1.0 01:KB:03 84.78 11.833 No.date 28.07 37.17 n/a 0000

128079 CONTINUES STANDBY 1.0 01:KB:03 84.78 11.833 No.date 28.07 37.17 456 0000

128080 [X.M.P. 85-TIMP= 85]

128081 [IBREC= 4.00: IAREBER= 4.00]

128082 [Pervious area: IAPER= 4.67:SLP=2.00:LG= 40:MN= 250:SCP= 0]

128083 [Impervious area: IAIM= 84:SLP= 2.00:LG= 215:MN= 013:SCI= 0]

128084 [IBREC= 4.00: IAREBER= 4.00]

128085 R0505:CO0233.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

128086 COMPUTE DUAL IHD 1.0 01:KB:04 6.95 1.592 No.date 28.00 71.86 882 0000

128087 MJOR SYSTEM 1.0 02:KB:04 6.95 1.592 No.date 28.00 71.86 n/a 0000

128088 MNR SYSTEM 1.0 03:KB:04N 6.95 1.592 No.date 28.00 71.86 n/a 0000

128089 [MYSys= 1.01:01:04] Tot Of Vol= 0.000E+00, N Of Cr= 0, Tot DirOfV= 0.0 r/s

128090 R0505:CO0234.....Dfn=I-D N DND.....AREAs-QPEAKm-TPeakTdt,h:m:m.....RvmR.K.C.....DfwmC

128091 ADD IHD 1.0 02:KB:04 6.95 1.592 No.date 28.00 71.86 n/a 0000

128092 + 1.0 02:KB:04 6.95 1.592 No.date 28.00 71.86 n/a 0000

128093 SIM 1.0 01:KB:04 6.95 1.592 No.date 28.00 71.86 882 0000

128094 CONTINUES STANDBY 1.0 01:KB:04 6.95 1.592 No.date 28.00 71.86 882 0000

128095 [X.M.P. 93-TIMP= 93]

128096 [IBREC= 4.00: IAREBER= 4.00]

128097 [Pervious area: IAPER= 4.67:SLP=2.00:LG= 40:MN= 250:SCP= 0]

128098 [Impervious area: IAIM= 1.57:SLP= 2.00:LG= 186:MN= 013:SCI= 0]

128099 [IBREC= 4.00: IAREBER= 4.00]

129001 [IBREC= 4.00: IAREBER= 4.00]

129002 [Pervious area: IAPER= 4.67:SLP=2.00:LG= 40:MN= 250:SCP= 0]

129003 [Impervious area: IAIM= 1.57:SLP= 2.00:LG= 186:MN= 013:SCI= 0]

129004

129005 [IBREC= 4.00: IAREBER= 4.00]

129006 [Pervious area: IAPER= 4.67:SLP=2.00:LG= 40:MN= 250:SCP= 0]

129007 [Impervious area: IAIM= 1.57:SLP= 2.00:LG= 186:MN= 013:SCI= 0]

129008

129009 [IBREC= 4.00: IAREBER= 4.00]

129010 [Pervious area: IAPER= 4.67:SLP=2.00:LG= 40:MN= 250:SCP= 0]

129011 [Impervious area: IAIM= 1.57:SLP= 2.00:LG= 186:MN= 013:SCI= 0]

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Table with columns for ID, description, and numerical values. Includes sub-sections like 'CONTINUOUS STANDBY', 'COMPUTE DRAINAGE', and 'CONTINUOUS STANDBY'. The table contains a large volume of data rows, each representing a specific engineering or planning item with associated parameters and values.

134655	R0505:CO0331	Dfwn-1D-NDD	ARE/AH-A/QE/AK/M-TPeak/Dte,h-hm-..	Rvsm-R-C-...Dfwm	17.88	1.478	Nt.Date	28.19	56.46	n/a	0000
134656	CNTLNXSR STANDBY	1.0 01:COR1	15.87	2.851	Nt.Date	28:01	63.61	7.80	0000				
134657	[XMP:63-TiPM:63]												
134658	[LRS:2-CN:77.0]												
134700	[Pervious area: IApgr 4.67:SLPP4.0:LPQ:4.0:MPN:250:SCP:0]												
134701	[Impervious area: IApmp 1.57:SLP41.0:LG:324:MM:013:SCI:0]												
134702	[IARCCmp 4.00: IARCCpgr 4.00]												
134703	[SMN:33.81:SMW:225.43:SK:010]												
134740	R0505:CO0332	Dfwn-1D-NDD	ARE/AH-A/QE/AK/M-TPeak/Dte,h-hm-..	Rvsm-R-C-...Dfwm	17.88	1.478	Nt.Date	28.19	56.46	n/a	0000
134741	CNTLNXSR STANDBY	1.0 01:COR1	15.87	2.851	Nt.Date	28:01	63.61	7.80	0000				
134742	[XMP:63-TiPM:63]												
134743	[LRS:2-CN:77.0]												
134780	[Pervious area: IApgr 4.67:SLPP4.0:LPQ:4.0:MPN:250:SCP:0]												
134781	[Impervious area: IApmp 1.57:SLP41.0:LG:324:MM:013:SCI:0]												
134782	[IARCCmp 4.00: IARCCpgr 4.00]												
134783	[SMN:33.81:SMW:225.43:SK:010]												
134820	R0505:CO0333	Dfwn-1D-NDD	ARE/AH-A/QE/AK/M-TPeak/Dte,h-hm-..	Rvsm-R-C-...Dfwm	17.88	1.478	Nt.Date	28.19	56.46	n/a	0000
134821	CNTLNXSR STANDBY	1.0 01:COR1	15.87	2.851	Nt.Date	28:01	63.61	7.80	0000				
134822	[XMP:63-TiPM:63]												
134823	[LRS:2-CN:77.0]												
134860	[Pervious area: IApgr 4.67:SLPP4.0:LPQ:4.0:MPN:250:SCP:0]												
134861	[Impervious area: IApmp 1.57:SLP41.0:LG:324:MM:013:SCI:0]												
134862	[IARCCmp 4.00: IARCCpgr 4.00]												
134863	[SMN:33.81:SMW:225.43:SK:010]												
134900	R0505:CO0334	Dfwn-1D-NDD	ARE/AH-A/QE/AK/M-TPeak/Dte,h-hm-..	Rvsm-R-C-...Dfwm	17.88	1.478	Nt.Date	28.19	56.46	n/a	0000
134901	CNTLNXSR STANDBY	1.0 01:COR1	15.87	2.851	Nt.Date	28:01	63.61	7.80	0000				
134902	[XMP:63-TiPM:63]												
134903	[LRS:2-CN:77.0]												
134940	[Pervious area: IApgr 4.67:SLPP4.0:LPQ:4.0:MPN:250:SCP:0]												
134941	[Impervious area: IApmp 1.57:SLP41.0:LG:324:MM:013:SCI:0]												
134942	[IARCCmp 4.00: IARCCpgr 4.00]												
134943	[SMN:33.81:SMW:225.43:SK:010]												
134980	R0505:CO0335	Dfwn-1D-NDD	ARE/AH-A/QE/AK/M-TPeak/Dte,h-hm-..	Rvsm-R-C-...Dfwm	17.88	1.478	Nt.Date	28.19	56.46	n/a	0000
134981	CNTLNXSR STANDBY	1.0 01:COR1	15.87	2.851	Nt.Date	28:01	63.61	7.80	0000				
134982	[XMP:63-TiPM:63]												
134983	[LRS:2-CN:77.0]												
135020	[Pervious area: IApgr 4.67:SLPP4.0:LPQ:4.0:MPN:250:SCP:0]												
135021	[Impervious area: IApmp 1.57:SLP41.0:LG:324:MM:013:SCI:0]												
135022	[IARCCmp 4.00: IARCCpgr 4.00]												
135023	[SMN:33.81:SMW:225.43:SK:010]												
135060	R0505:CO0336	Dfwn-1D-NDD	ARE/AH-A/QE/AK/M-TPeak/Dte,h-hm-..	Rvsm-R-C-...Dfwm	17.88	1.478	Nt.Date	28.19	56.46	n/a	0000
135061	CNTLNXSR STANDBY	1.0 01:COR1	15.87	2.851	Nt.Date	28:01	63.61	7.80	0000				
135062	[XMP:63-TiPM:63]												
135063	[LRS:2-CN:77.0]												
135100	[Pervious area: IApgr 4.67:SLPP4.0:LPQ:4.0:MPN:250:SCP:0]												
135101	[Impervious area: IApmp 1.57:SLP41.0:LG:324:MM:013:SCI:0]												
135102	[IARCCmp 4.00: IARCCpgr 4.00]												
135103	[SMN:33.81:SMW:225.43:SK:010]												

Table of hydrograph routing parameters for nodes 14213-14399. Columns include node ID, flow control type, reduction factor, peak date, peak flow, and routing time. Includes sub-headers for 'The Tp was modified according to a Peak Reduction factor'.

Table of hydrograph routing parameters for nodes 14400-14586. Columns include node ID, flow control type, reduction factor, peak date, peak flow, and routing time. Includes sub-headers for 'Addition of Subwatershed', 'Remark: flow at S_N2 near Ashton', and 'Output of Reservoir Goodwood Marsh'.

145877 ROUTE CHANNEL -> 1.0 02: S_NSA 48447.01 89.756 N_date 34:38 37.51 n/a .000
145878 [RIDE 1.00] out -> 1.0 01: IR 48447.01 85.943 N_date 36:10 37.51 n/a .000
145879 [L/S na= 4630. / 043/ 055]
145880 [Vmax = 904.Dmax= 3.866]
145901 #
145902 # Addition of Subwatershed 4 with Leam Creek to Node 4
145903 #
145904 R0100: C00060 -> Dfm= 1-D NDD -> AREHA-QPEAKm-TPeakDte-hh:mm -> Rvmm R.C. -> Dfwm
145905 ADD HYD + 1.0 02: SW2 4641.01 85.943 N_date 36:10 37.51 n/a .000
145906 + 1.0 02: SW4 585.00 14.953 N_date 29:55 52.06 n/a .000
145907 + 1.0 02: LACK 1021.00 19.782 N_date 30:45 51.16 n/a .000
145908 + 1.0 01: S_N 48447.00 96.618 N_date 35:12 37.97 n/a .000
145909 SIMM 1.0 01: S_N 48447.00 96.618 N_date 35:12 37.97 n/a .000
145910 R0100: C00061 -> Dfm= 1-D NDD -> AREHA-QPEAKm-TPeakDte-hh:mm -> Rvmm R.C. -> Dfwm
146000 SAVE HYD 1.0 01: S_N 48447.00 96.618 N_date 35:12 37.97 n/a .000
146001 #name: S_N.0100
146002 remark: flow at S_N
146003 #
146004 # Sum of hydrographs from Node 4 routed to Node 2
146005 # Section 9
146006 #
146007 R0100: C00062 -> Dfm= 1-D NDD -> AREHA-QPEAKm-TPeakDte-hh:mm -> Rvmm R.C. -> Dfwm
146008 ROUTE CHANNEL -> 1.0 02: S_N 48447.00 96.618 N_date 35:12 37.97 n/a .000
146009 [RIDE 1.00] out -> 1.0 01: IR 48447.00 96.222 N_date 35:13 37.97 n/a .000
146100 [L/S na= 1667. / 060/ 040]
146101 [Vmax = 944.Dmax= 3.929]
146102 #
146103 # Addition of Subwatershed 2 with Mhoanah Drain and Smith Drain to Node 2
146104 #
146105 R0100: C00063 -> Dfm= 1-D NDD -> AREHA-QPEAKm-TPeakDte-hh:mm -> Rvmm R.C. -> Dfwm
146106 ADD HYD + 1.0 02: SW2 48447.00 96.722 N_date 35:13 37.97 n/a .000
146107 + 1.0 02: SW4 177.00 17.000 N_date 28:44 47.62 n/a .000
146108 + 1.0 02: SMDR 1122.00 17.981 N_date 31:42 52.06 n/a .000
146109 + 1.0 02: MD IR 48447.00 40.710 N_date 31:28 46.75 n/a .000
146200 SIMM 1.0 01: S_N 52483.00 143.580 N_date 32:59 38.76 n/a .000
146201 R0100: C00064 -> Dfm= 1-D NDD -> AREHA-QPEAKm-TPeakDte-hh:mm -> Rvmm R.C. -> Dfwm
146202 SAVE HYD 1.0 01: S_N 52483.00 143.580 N_date 32:59 38.76 n/a .000
146203 #name: H_NSD
146204 remark: flow at S_N Jock River Gauge at Moele Dr.
146205 #
146206 # Sum of hydrographs from Node 2 routed to Node 1
146207 # Section 10
146208 #
146209 #
146210 #
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149610 #      + 1.0 02: S:OPF              4.00   0.00 Ndate 0:00   0.00 n/a   0.000
149620 # SIMM                          364.79  7.924 Ndate 28:07  35.79 n/a   0.000
149630 # 149630 R1001:COU19.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
149640 # SAVE HYD                          564.27  7.924 Ndate 29:06  35.79 n/a   0.000
149650 # fname :SSAOKT.0100
149660 # remark :SSAOKT
149670 # CONT NEXUS STANDHID 1.0 01: S:Area-A 66.75  9.945 Ndate 28:08  67.64  764.000
149680 # [X MPa: 64.7 Tmp: 80]
149700 # [Horizon parameters: Fow 76.20; Fcn 13.20; DCAVd: 14; Fw: 00]
149710 # [Impervious area: IArea: 4.67; SLLPp: 50; LQp: 50; MNPp: 250; SCPw: 0]
149720 # [IARCG mp: 4.00; IARCGPerc: 4.00]
149730 # [IARCG mp: 4.00; IARCGPerc: 4.00]
149740 # [MSi:ob:ed:2700E:01] mb, TotOfVol: 0.0000E+00 mb, N:Of: 0, TotDurOf: 0 hrs.]
149750 # 149750 R1001:COU121.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
149760 # SAVE HYD                          66.75  9.945 Ndate 28:08  67.64  764.000
149770 # fname :Area-A.0100
149780 # remark :SMF-A Inflow
149790 # 149790 R1001:COU122.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
149800 # ROUTE RESERVOIR > 1.0 02: Area-A 66.75  9.945 Ndate 28:08  67.64  764.000
149810 # out <= 1.0 01: SMF-A 66.75  1.357 Ndate 29:10  67.64  n/a   0.000
149820 # overflow <= 1.0 03: S:IDRF 0.00  0.00 Ndate 0:00  0.00 n/a   0.000
149830 # [MSi:ob:ed:3051E:01] mb, TotOfVol: 0.0000E+00 mb, N:Of: 0, TotDurOf: 0 hrs.]
149840 # 149840 R1001:COU123.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
149850 # SAVE HYD                          66.75  1.357 Ndate 29:10  67.64  n/a   0.000
149860 # fname :SMF-A.0100
149870 # 149870 R1001:COU124.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
149880 # ADD HYD                          364.99  7.924 Ndate 29:00  35.79 n/a   0.000
149890 # + 1.0 02: SMF-A 66.75  1.357 Ndate 29:10  67.64  n/a   0.000
149900 # + 1.0 02: SMF:RV 0.00  0.00 Ndate 0:00  0.00 n/a   0.000
149910 # SIMM                          431.02  9.279 Ndate 29:07  40.72  n/a   0.000
149920 # [MSi:ob:ed:3051E:01] mb, TotOfVol: 0.0000E+00 mb, N:Of: 0, TotDurOf: 0 hrs.]
149930 # 149930 R1001:COU125.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
149940 # CONT NEXUS STANDHID 1.0 01: S:ID 18.67  3.580 Ndate 28:01  70.58  797.000
149950 # [X MPa: 68.7 Tmp: 85]
149960 # [Horizon parameters: Fow 76.20; Fcn 13.20; DCAVd: 14; Fw: 00]
149970 # [Impervious area: IArea: 4.67; SLLPp: 50; LQp: 50; MNPp: 250; SCPw: 0]
149980 # [IARCG mp: 4.00; IARCGPerc: 4.00]
149990 # [IARCG mp: 4.00; IARCGPerc: 4.00]
150000 # [MSi:ob:ed:3051E:01] mb, TotOfVol: 0.0000E+00 mb, N:Of: 0, TotDurOf: 0 hrs.]
150010 # 150010 R1001:COU126.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
150020 # ROUTE RESERVOIR > 1.0 02: FoF 1.87  1.129 Ndate 28:16  70.42  n/a   0.000
150030 # out <= 1.0 01: Co:STR 1.87  1.129 Ndate 28:16  70.42  n/a   0.000
150040 # overflow <= 1.0 03: S:IDRF 0.00  0.00 Ndate 0:00  0.00 n/a   0.000
150050 # [MSi:ob:ed:3051E:01] mb, TotOfVol: 0.0000E+00 mb, N:Of: 0, TotDurOf: 0 hrs.]
150060 # 150060 R1001:COU127.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
150070 # CONT NEXUS STANDHID 1.0 01: S:ID 18.67  3.580 Ndate 28:00  70.58  797.000
150080 # [X MPa: 68.7 Tmp: 85]
150090 # [Horizon parameters: Fow 76.20; Fcn 13.20; DCAVd: 14; Fw: 00]
150100 # [Impervious area: IArea: 4.67; SLLPp: 50; LQp: 50; MNPp: 250; SCPw: 0]
150110 # [IARCG mp: 4.00; IARCGPerc: 4.00]
150120 # [IARCG mp: 4.00; IARCGPerc: 4.00]
150130 # 150130 R1001:COU128.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
150140 # out <= 1.0 01: Co:STR 1.87  1.129 Ndate 28:16  70.42  n/a   0.000
150150 # overflow <= 1.0 03: S:IDRF 1.87  1.129 Ndate 28:16  70.42  n/a   0.000
150160 # [MSi:ob:ed:3056E:01] mb, TotOfVol: 0.0000E+00 mb, N:Of: 0, TotDurOf: 0 hrs.]
150170 # 150170 R1001:COU129.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
150180 # CONT NEXUS STANDHID 1.0 01: S:ID 18.67  3.580 Ndate 28:00  55.78  790.000
150190 # [X MPa: 64.7 Tmp: 57]
150200 # [Horizon parameters: Fow 76.20; Fcn 13.20; DCAVd: 14; Fw: 00]
150210 # [Impervious area: IArea: 4.67; SLLPp: 50; LQp: 50; MNPp: 250; SCPw: 0]
150220 # [IARCG mp: 4.00; IARCGPerc: 4.00]
150230 # [IARCG mp: 4.00; IARCGPerc: 4.00]
150240 # 150240 R1001:COU130.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
150250 # ROUTE RESERVOIR > 1.0 02: FoF 1.87  1.129 Ndate 28:16  70.42  n/a   0.000
150260 # out <= 1.0 01: S:STSR 1.87  1.129 Ndate 28:13  55.78  n/a   0.000
150270 # overflow <= 1.0 03: S:IDRF 4.00  0.00 Ndate 0:00  0.00 n/a   0.000
150280 # [MSi:ob:ed:3877E:02] mb, TotOfVol: 0.0000E+00 mb, N:Of: 0, TotDurOf: 0 hrs.]
150290 # 150290 R1001:COU131.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
150300 # ADD HYD                          431.02  9.279 Ndate 29:07  40.72  n/a   0.000
150310 # + 1.0 02: Co:STR 1.87  1.129 Ndate 28:16  70.42  n/a   0.000
150320 # + 1.0 02: Co:STR 1.87  1.129 Ndate 28:16  70.42  n/a   0.000
150330 # + 1.0 02: S:IDRF 1.87  1.129 Ndate 28:16  70.42  n/a   0.000
150340 # + 1.0 02: S:STSR 4.00  0.00 Ndate 0:00  0.00 n/a   0.000
150350 # + 1.0 02: S:IDRF 4.00  0.00 Ndate 0:00  0.00 n/a   0.000
150360 # SIMM                          434.92  9.426 Ndate 29:06  40.97  n/a   0.000
150370 # 150370 R1001:COU132.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
150380 # ROUTE CHANNEL > 1.0 02: Bx:EN 434.92  9.426 Ndate 29:06  40.97  n/a   0.000
150390 # [RF: 1.00] out <= 1.0 01: BR:NLI 434.92  9.061 Ndate 29:16  40.97  n/a   0.000
150400 # [L/S: 524 / 100]
150410 # [Vmax: 507; Dmax: 1.619]
150420 # 150420 R1001:COU133.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
150430 # CONT NEXUS STANDHID 1.0 01: S:ID 18.67  3.580 Ndate 28:00  57.07  644.000
150440 # [Cns: 8.0; Nc: 3.00; Tpa: 60]
150450 # [IARCG: 4.00; SMN: 17.42; SMW: 116.21; SKE: 010]
150460 # [InterEvent Time: 12.00]
150470 # 150470 R1001:COU134.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
150480 # CONT NEXUS STANDHID 1.0 01: S:ID 18.67  3.580 Ndate 28:00  66.17  747.000
150490 # [X MPa: 62.7 Tmp: 77]
150500 # [Horizon parameters: Fow 76.20; Fcn 13.20; DCAVd: 14; Fw: 00]
150510 # [Impervious area: IArea: 4.67; SLLPp: 50; LQp: 50; MNPp: 250; SCPw: 0]
150520 # [IARCG mp: 4.00; IARCGPerc: 4.00]
150530 # [IARCG mp: 4.00; IARCGPerc: 4.00]
150540 # 150540 R1001:COU135.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
150550 # ROUTE RESERVOIR > 1.0 02: FoF 24.04  4.931 Ndate 28:01  66.17  n/a   0.000
150560 # out <= 1.0 01: SMF:V 24.04  6.641 Ndate 28:41  66.17  n/a   0.000
150570 # overflow <= 1.0 03: S:IDRF 0.00  0.00 Ndate 0:00  0.00 n/a   0.000
150580 # [MSi:ob:ed:9727E:00] mb, TotOfVol: 0.0000E+00 mb, N:Of: 0, TotDurOf: 0 hrs.]
150590 # 150590 R1001:COU136.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
150600 # ADD HYD                          434.92  9.061 Ndate 29:16  40.97  n/a   0.000
150610 # + 1.0 02: Bx:EN 1.73  1.129 Ndate 28:33  57.07  n/a   0.000
150620 # + 1.0 02: SMF:V 24.04  6.641 Ndate 28:41  66.17  n/a   0.000
150630 # + 1.0 02: SMF:RV 0.00  0.00 Ndate 0:00  0.00 n/a   0.000
150640 # SIMM                          440.69  9.722 Ndate 29:15  42.35  n/a   0.000
150650 # 150650 R1001:COU137.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
150660 # ROUTE CHANNEL > 1.0 02: Bx:EN 440.69  9.722 Ndate 29:15  42.35  n/a   0.000
150670 # [RF: 1.00] out <= 1.0 01: BR:NLI 440.69  9.426 Ndate 29:06  40.97  n/a   0.000
150680 # [L/S: 413 / 160] 0.03]
150690 # [Vmax: 703; Dmax: 1.0]
150700 # 150700 R1001:COU138.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
150710 # CONT NEXUS STANDHID 1.0 01: S:ID 1.90  1.104 Ndate 28:40  54.04  610.000
150720 # [Cns: 8.0; Nc: 3.00; Tpa: 60]
150730 # [IARCG: 4.00; SMN: 17.42; SMW: 116.21; SKE: 010]
150740 # [InterEvent Time: 12.00]
150750 # 150750 R1001:COU139.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
150760 # CONT NEXUS STANDHID 1.0 01: S:IDRF 9.74  6.75 Ndate 28:21  50.83  574.000
150770 # [Cns: 8.0; Nc: 3.00; Tpa: 43]
150780 # [InterEvent Time: 12.00]
150790 # 150790 R1001:COU140.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
150800 # ROUTE RESERVOIR > 1.0 02: S:IDRF 9.74  6.75 Ndate 28:21  50.83  574.000
150810 # out <= 1.0 01: S:IDRF 9.74  0.070 Ndate 30:50  50.83  n/a   0.000
150820 # overflow <= 1.0 03: S:IDRF 0.00  0.00 Ndate 0:00  0.00 n/a   0.000
150830 # [MSi:ob:ed:2813E:00] mb, TotOfVol: 0.0000E+00 mb, N:Of: 0, TotDurOf: 0 hrs.]
150840 # 150840 R1001:COU141.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
150850 # ADD HYD                          440.69  9.664 Ndate 29:16  42.35  n/a   0.000
150860 # + 1.0 02: Bx:EN 1.90  1.104 Ndate 28:40  54.04  n/a   0.000
150870 # + 1.0 02: SMF:V 24.04  6.641 Ndate 28:41  66.17  n/a   0.000
150880 # + 1.0 02: SMF:RV 0.00  0.00 Ndate 0:00  0.00 n/a   0.000
150890 # SIMM                          440.69  9.722 Ndate 29:15  42.35  n/a   0.000
150900 # 150900 R1001:COU142.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
150910 # CONT NEXUS STANDHID 1.0 01: S:ID 10.67  3.094 Ndate 28:13  49.72  561.000
150920 # [Cns: 8.2; 0; Nc: 3.00; Tpa: 30]
150930 # [IARCG: 4.00; SMN: 25.09; SMW: 168.09; SKE: 010]
150940 # [InterEvent Time: 12.00]
150950 # 150950 R1001:COU143.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
150960 # ADD HYD                          472.33  6.694 Ndate 29:26  42.35  n/a   0.000
150970 # + 1.0 02: S:IDRF 10.67  9.840 Ndate 28:13  49.72  n/a   0.000
150980 # SIMM                          488.00  9.844 Ndate 29:26  42.35  n/a   0.000
150990 # 150990 R1001:COU144.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
151000 # ROUTE CHANNEL > 1.0 02: Bx:EN 488.00  9.844 Ndate 29:26  42.35  n/a   0.000
151010 # [RF: 1.00] out <= 1.0 01: S:IDRF 488.00  8.880 Ndate 29:52  42.35  n/a   0.000
151020 # [L/S: 845 / 100] 0.03]
151030 # [Vmax: 556; Dmax: 1.861]
151040 # 151040 R1001:COU145.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
151050 # CONT NEXUS STANDHID 1.0 01: S:ID 5.00  7.22 Ndate 28:04  49.72  561.000
151060 # [Cns: 8.2; 0; Nc: 3.00; Tpa: 13]
151070 # [IARCG: 4.00; SMN: 25.09; SMW: 168.09; SKE: 010]
151080 # [InterEvent Time: 12.00]
151090 # 151090 R1001:COU146.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
151100 # ADD HYD                          483.00  8.880 Ndate 29:52  42.35  n/a   0.000
151110 # + 1.0 02: S:IDRF 5.00  7.22 Ndate 28:04  49.72  n/a   0.000
151120 # SIMM                          488.00  8.825 Ndate 29:52  40.72  n/a   0.000
151130 # *****
151140 # Creefe Pond
151150 # Raising curve obtained assuming 40mb/ha in 24 hours for quality control
151160 # and a ratio of the catchment area to the West Clarke pond rating curve
151170 # from the MS for the next coordinates
151180 # 151180 R1001:COU147.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
151190 # CONT NEXUS STANDHID 1.0 01: S:1-ID 18.67  3.580 Ndate 28:01  70.58  797.000
151200 # [X MPa: 65.7 Tmp: 65]
151210 # [LGS: 2; Cns: 75.0]
151220 # [Previous area: IArea: 4.67; SLLPp: 0; LQp: 40; MNPp: 250; SCPw: 0]
151230 # [Impervious area: IArea: 4.67; SLLPp: 50; LQp: 50; MNPp: 250; SCPw: 0]
151240 # [IARCG mp: 4.00; IARCGPerc: 4.00]
151250 # [IARCG mp: 4.00; IARCGPerc: 4.00]
151260 # 151260 R1001:COU148.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
151270 # COMPUTE DRAIN/DIAD 1.0 01: S:1-FO-D 18.67  3.580 Ndate 28:01  70.58  n/a   0.000
151280 # Major System / 1.0 03: S:1-FO-D 18.67  2.097 Ndate 27:52  70.87  n/a   0.000
151290 # Minor System / 1.0 03: S:1-FO-D 18.67  2.097 Ndate 27:52  70.87  n/a   0.000
151300 # [MSi:ob:ed:7940E:00] mb, TotOfVol: 0.0000E+00 mb, N:Of: 0, TotDurOf: 0 hrs.]
151310 # 151310 R1001:COU149.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
151320 # ADD HYD                          18.67  2.097 Ndate 27:52  70.87  n/a   0.000
151330 # + 1.0 02: S:1-IDN 18.67  2.097 Ndate 27:52  70.87  n/a   0.000
151340 # + 1.0 02: S:1-IDN 18.67  2.097 Ndate 27:52  70.87  n/a   0.000
151350 # SIMM                          18.67  2.097 Ndate 27:52  70.87  n/a   0.000
151360 # 151360 R1001:COU150.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
151370 # ROUTE RESERVOIR > 1.0 02: S:1-IDN 18.67  2.097 Ndate 27:52  70.87  n/a   0.000
151380 # out <= 1.0 02: S:1-IDRF 18.67  2.097 Ndate 27:52  70.87  n/a   0.000
151390 # overflow <= 1.0 03: S:1-IDRF 18.67  2.097 Ndate 27:52  70.87  n/a   0.000
151400 # [MSi:ob:ed:7445E:00] mb, TotOfVol: 0.0000E+00 mb, N:Of: 0, TotDurOf: 0 hrs.]
151410 # 151410 R1001:COU151.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
151420 # CONT NEXUS STANDHID 1.0 01: S:1-ID 6.79  1.405 Ndate 28:00  70.58  797.000
151430 # [X MPa: 65.7 Tmp: 65]
151440 # [LGS: 2; Cns: 75.0]
151450 # [Previous area: IArea: 4.67; SLLPp: 0; LQp: 40; MNPp: 250; SCPw: 0]
151460 # [Impervious area: IArea: 4.67; SLLPp: 50; LQp: 50; MNPp: 250; SCPw: 0]
151470 # [IARCG mp: 4.00; IARCGPerc: 4.00]
151480 # *****
151490 # [SMN: 33.81; SMW: 225.43; SKE: 010]
151500 # 151500 R1001:COU152.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
151510 # COMPUTE DRAIN/DIAD 1.0 01: S:1-ID 6.79  1.405 Ndate 28:00  70.58  n/a   0.000
151520 # Major System / 1.0 03: S:1-FO-D 6.79  0.831 Ndate 28:00  70.58  n/a   0.000
151530 # Minor System / 1.0 03: S:1-FO-D 6.79  0.831 Ndate 28:00  70.58  n/a   0.000
151540 # [MSi:ob:ed:3005E:00] mb, TotOfVol: 0.0000E+00 mb, N:Of: 0, TotDurOf: 0 hrs.]
151550 # 151550 R1001:COU153.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
151560 # ADD HYD                          6.79  0.831 Ndate 27:51  70.87  n/a   0.000
151570 # + 1.0 02: S:1-IDN 6.79  0.831 Ndate 27:51  70.87  n/a   0.000
151580 # + 1.0 01: S:1-IDN 6.79  0.831 Ndate 27:51  70.87  n/a   0.000
151590 # 151590 R1001:COU154.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
151600 # ROUTE RESERVOIR > 1.0 02: S:1-IDN 6.79  0.831 Ndate 27:51  70.87  n/a   0.000
151610 # out <= 1.0 01: S:1-IDR 6.51  0.81 Ndate 28:27  70.87  n/a   0.000
151620 # overflow <= 1.0 03: S:1-IDRF 6.79  0.831 Ndate 28:27  70.87  n/a   0.000
151630 # [MSi:ob:ed:2700E:00] mb, TotOfVol: 0.0000E+00 mb, N:Of: 0, TotDurOf: 0 hrs.]
151640 # 151640 R1001:COU155.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
151650 # ADD HYD                          35377.81  148.295 Ndate 33:05  38.86  n/a   0.000
151660 # + 1.0 02: CR:EEFE 488.00  8.825 Ndate 29:52  42.35  n/a   0.000
151670 # + 1.0 02: S:1-IDR 17.89  2.23 Ndate 28:10  70.87  n/a   0.000
151680 # + 1.0 02: S:1-IDR 6.51  0.81 Ndate 28:27  70.87  n/a   0.000
151690 # + 1.0 02: S:1-IDRF 6.79  0.831 Ndate 28:27  70.87  n/a   0.000
151700 # SIMM                          35377.81  148.295 Ndate 33:05  38.86  n/a   0.000
151710 # 151710 R1001:COU156.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
151720 # SAVE HYD                          35377.81  148.295 Ndate 33:05  38.86  n/a   0.000
151730 # fname :SN.OK.0100
151740 # remark :Total Flows at Keeffe Drain
151750 # *****
151760 # Hydrograph from Node Keeffe routed to Node at Foster Drain
151770 # Channel X Section obtained from RVCA Hydraulic Model - Station 6215
151780 # *****
151790 # 151790 R1001:COU157.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
151800 # ROUTE CHANNEL > 1.0 02: SN:OK 35377.81  148.295 Ndate 33:05  38.86  n/a   0.000
151810 # [RF: 1.00] out <= 1.0 01: S:FO 35377.81  147.939 Ndate 33:45  38.86  n/a   0.000
151820 # [L/S: 118.00 / 100] 0.76] 0.05]
151830 # [Vmax: 1.293; Dmax: 3.590]
151840 # *****
151850 # Catchment FOSTER
151860 # To Foster ditch (north of the Jack)
151870 # Elevation developed (medium density): remaining agricultural
151880 # 2020-12-01 JFSA Foster area is 332 as per Foster SWF Environmental Study Report, CH2MHILL Aug. 2014
151890 # 2020-12-01 decrease Foster area from 373 to 332 as per Foster SWF Environmental Study Report, CH2MHILL Aug. 2014
151900 # 2021-02-12 update Foster area to 325.44 ha as measured from QGS
151910 # 151910 R1001:COU158.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
151920 # CONT NEXUS STANDHID 1.0 01: S:FO-D 325.44  36.526 Ndate 28:10  65.13  735.000
151930 # [X MPa: 65.7 Tmp: 65]
151940 # [LGS: 2; Cns: 74.0]
151950 # [Previous area: IArea: 4.67; SLLPp: 50; LQp: 40; MNPp: 250; SCPw: 0]
151960 # [Impervious area: IArea: 1.57; SLLP: 50; LQ: 4173; MNP: 013; SCl: 0]
151970 # [IARCG mp: 4.00; IARCGPerc: 4.00]
151980 # [IARCG mp: 4.00; IARCGPerc: 4.00]
151990 # *****
152000 # Raising curve obtained assuming 40mb/ha in 24 hours for quality control
152010 # and a ratio of the catchment area to the West Clarke pond rating curve
152020 # from the MS for the next coordinates
152030 # 152030 R1001:COU159.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
152040 # CONT NEXUS STANDHID 1.0 01: S:FO-D 325.44  36.526 Ndate 28:10  65.13  n/a   0.000
152050 # [X MPa: 65.7 Tmp: 65]
152060 # [LGS: 2; Cns: 74.0]
152070 # [Previous area: IArea: 1.57; SLLP: 50; LQp: 40; MNPp: 250; SCPw: 0]
152080 # [Impervious area: IArea: 1.57; SLLP: 50; LQ: 4173; MNP: 013; SCl: 0]
152090 # [IARCG mp: 4.00; IARCGPerc: 4.00]
152100 # [IARCG mp: 4.00; IARCGPerc: 4.00]
152110 # 152110 R1001:COU160.....DfM n-ID NDD.....AREQA-QPEAQm-TeprkDtie,h-hmm-.....Rvmm R.C...DfWcm
152120 # ADD HYD                          325.44  36.526 Ndate 28:10  65.13  n/a   0.000
152130 # + 1.0 02: FoF:FCF 325.44  9.091 Ndate 29:01  65.13  n/a   0.000
152140 # overflow <= 1.0 03: FoF:FO 0.00  0.00 Ndate 0:00  0.00 n/a   0.000
152150 # [MSi:ob:
```

Table with columns for ID, Description, Parameters, and Values. Rows include detailed hydrograph data for various stations (e.g., 153535, 153536, 153537) and include notes on data sources and modeling assumptions.


```

168313 ROUTE RESERVOIR -> 1.0 02: MLLS 175.99 20.390 No_date 28:06 56.87 n/a .000
168328 out <= 1.0 01: MLLP 146.22 4.050 No_date 28:08 56.87 n/a .000
168333 overflow <= 1.0 03: MLLC 20.77 16.228 No_date 28:08 56.87 n/a .000
168349 [MKS]obled_23101601 ob_ N 0.041 2. TotDurOfa 1. hrs]
168355 R0100: CO0426 ----- Dfm n- LD NMD ----- AREba- QPEAGcm- TpeakDtte_bh- mm- Rvmm R. C. ----- Dfwm
168360 ADD HYD + 1.0 02: N.M 5520.07 145.768 No_date 36:59 39.46 n/a .000
168375 + 1.0 02: MLLC 29.77 16.228 No_date 28:08 56.87 n/a .000
168388 + 1.0 02: MLLP 146.22 4.050 No_date 28:08 56.87 n/a .000
168399 SLM 55196.05 146.399 No_date 36:58 39.51 n/a .000
168400 R0100: CO0427 ----- Dfm n- LD NMD ----- AREba- QPEAGcm- TpeakDtte_bh- mm- Rvmm R. C. ----- Dfwm
168414 SAVE HYD 1.0 01: SN,DE 55196.05 146.399 No_date 36:58 39.51 n/a .000
168425 #name: SN,M 0100
168430 #remark: Total Flow at Jockvale Road
168445 #
168455 # Hydrograph from Jockvale Road routed to Heart's Desire
168460 # Channel X-Section obtained from RCV4 Hydraulic Model - Station 689
168475 #
168480 R0100: CO0428 ----- Dfm n- LD NMD ----- AREba- QPEAGcm- TpeakDtte_bh- mm- Rvmm R. C. ----- Dfwm
168490 ROUTE CHANNEL -> 1.0 02: SN,M 55196.05 146.399 No_date 36:58 39.51 n/a .000
168500 [RDF= 1.00] out <= 1.0 01: N,DE 55196.05 146.071 No_date 37:13 39.51 n/a .000
168510 [L/S= 1962 / 221.045]
168520 [Vmax= 1.642; Dmax= 2.661]
168530 #
168540 # Catchment DESIRE
168555 # - To Jock River (north of the Jock)
168560 # - Rural estate subdivision (Heart's Desire Community)
168575 #
168580 R0100: CO0429 ----- Dfm n- LD NMD ----- AREba- QPEAGcm- TpeakDtte_bh- mm- Rvmm R. C. ----- Dfwm
168590 CONTINUOUS STANDPFD 1.0 01: DESIRE 23.78 3.004 No_date 28:03 53.11 6.00 .000
168600 [X MPa= 25; TPA= 25]
168610 [LRS= 2; C/N= 77.0]
168620 [Pervious area: IArea 4.67; SLP1= 0.0; LCA= 40; MPa= 250; SCW= .0]
168630 [Impervious area: IArea 1.57; SLP1= 0.0; LCA= 400; MN= 013; SCL= .0]
168640 [IARECm= 4.00; IARECPer= 4.00]
168650 [SM N= 31.15; SMLM= 45.0; SK= 010]
168660 #
168670 # Catchment JOCKVA
168680 # - To Jockvale SVM Facility
168690 # - Residential development & golf course
168700 # - JESA C201-01-11 update JOCKVA after updating CORP G as per HR GROUP July 2008.
168710 # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX LAND 32.5 ha as
168720 #
168730 R0100: CO0430 ----- Dfm n- LD NMD ----- AREba- QPEAGcm- TpeakDtte_bh- mm- Rvmm R. C. ----- Dfwm
168740 CONTINUOUS STANDPFD 1.0 01: JOCKVA 225.13 28.623 No_date 28:07 62.70 .708 .000
168750 [X MPa= 50]
168760 [LRS= 2; C/N= 74.0]
168770 [Pervious area: IArea 4.67; SLP1= 0.0; LCA= 40; MPa= 250; SCW= .0]
168780 [Impervious area: IArea 1.57; SLP1= 0.0; LCA= 400; MN= 013; SCL= .0]
168790 [IARECm= 4.00; IARECPer= 4.00]
168800 [SM N= 36.67; SMLM= 45.0; SK= 010]
168810 R0100: CO0431 ----- Dfm n- LD NMD ----- AREba- QPEAGcm- TpeakDtte_bh- mm- Rvmm R. C. ----- Dfwm
168820 ADD HYD + 1.0 02: SN,DE 55196.05 146.399 No_date 36:58 39.51 n/a .000
168830 + 1.0 02: JOCKVA 225.13 28.623 No_date 28:07 62.70 n/a .000
168840 + 1.0 02: MML 36.82 820 No_date 28:05 62.88 n/a .000
168850 + 1.0 02: R0,M 19.402 No_date 28:04 62.88 n/a .000
168860 SLM 31.850 No_date 28:06 62.71 n/a .000
168870 R0100: CO0432 ----- Dfm n- LD NMD ----- AREba- QPEAGcm- TpeakDtte_bh- mm- Rvmm R. C. ----- Dfwm
168880 SAVE HYD 1.0 01: JOCKVA,TO 256.41 31.850 No_date 28:06 62.71 n/a .000
168890 #name: JOCKVA,TO 0100
168900 #remark: Total Flow at KB first pond
168910 #
168920 # Jockvale SVM Facility
168930 # - Rating curve obtained from Jockvale Servicing Study (CC, 1999)
168940 #
168950 R0100: CO0433 ----- Dfm n- LD NMD ----- AREba- QPEAGcm- TpeakDtte_bh- mm- Rvmm R. C. ----- Dfwm
168960 ROUTE RESERVOIR -> 1.0 02: SN,DE 55196.05 146.399 No_date 36:58 39.51 n/a .000
168970 out <= 1.0 01: JOCK P 256.41 12.850 No_date 28:35 62.71 n/a .000
168980 overflow <= 1.0 03: JO,DF 0.00 0.00 No_date 0:00 60 n/a .000
168990 [MKS]obled_64301010 ob_ N 0.041 0. TotDurOfa 0. hrs]
169000 R0100: CO0434 ----- Dfm n- LD NMD ----- AREba- QPEAGcm- TpeakDtte_bh- mm- Rvmm R. C. ----- Dfwm
169010 ADD HYD + 1.0 02: N,DE 55196.05 146.071 No_date 37:13 39.51 n/a .000
169020 + 1.0 02: DESIRE 23.78 3.004 No_date 28:03 53.11 n/a .000
169030 + 1.0 02: JO,DF 0.00 0.00 No_date 0:00 60 n/a .000
169040 + 1.0 02: JOCK P 256.41 12.850 No_date 28:35 62.71 n/a .000
169050 SLM 31.850 No_date 28:06 62.71 n/a .000
169060 R0100: CO0435 ----- Dfm n- LD NMD ----- AREba- QPEAGcm- TpeakDtte_bh- mm- Rvmm R. C. ----- Dfwm
169070 SAVE HYD 1.0 01: SN,DE 55476.25 147.027 No_date 37:12 39.63 n/a .000
169080 #name: SN,DE 0100
169090 #remark: Total Flow at Heart's Desire
169100 #
169110 # Hydrograph from Heart's Desire routed to Rideau River
169120 # Channel X-Section obtained from RCV4 Hydraulic Model - Station 0
169130 #
169140 R0100: CO0436 ----- Dfm n- LD NMD ----- AREba- QPEAGcm- TpeakDtte_bh- mm- Rvmm R. C. ----- Dfwm
169150 ROUTE CHANNEL -> 1.0 02: SN,DE 55476.25 147.027 No_date 37:12 39.63 n/a .000
169160 [RDF= 1.00] out <= 1.0 01: N,DE 55476.25 147.014 No_date 37:15 39.63 n/a .000
169170 [L/S= 563 / 967.045]
169180 [Vmax= 2.19; Dmax= 1.24]
169190 #
169200 # Catchment S
169210 # - To Jock River (north and south)
169220 # - Underlapped floodplain and river
169230 #
169240 R0100: CO0437 ----- Dfm n- LD NMD ----- AREba- QPEAGcm- TpeakDtte_bh- mm- Rvmm R. C. ----- Dfwm
169250 CONTINUOUS STANDPFD 1.0 01: S,2 1.02 94.2 5.685 No_date 28:20 40.95 4.62 .000
169260 [C/N= 72.0; N= 3.00; TPA= 40]
169270 [IAREC= 4.00; SLM N= 39.75; SMLM= 264.99; SK= 010]
169280 [InterEventTime= 12.00]
169290 R0100: CO0438 ----- Dfm n- LD NMD ----- AREba- QPEAGcm- TpeakDtte_bh- mm- Rvmm R. C. ----- Dfwm
169300 ADD HYD + 1.0 02: N,DE 55476.25 147.014 No_date 37:15 39.63 n/a .000
169310 + 1.0 02: S,2 102.94 5.685 No_date 28:20 40.95 n/a .000
169320 SLM 55579.19 147.276 No_date 37:15 39.63 n/a .000
169330 R0100: CO0439 ----- Dfm n- LD NMD ----- AREba- QPEAGcm- TpeakDtte_bh- mm- Rvmm R. C. ----- Dfwm
169340 SAVE HYD 1.0 01: SN,DE 55579.19 147.276 No_date 37:15 39.63 n/a .000
169350 #name: SN,NI 0100
169360 #remark: Total Flow at Rideau River
169370 #
169380 R0100: CO0440 ----- Dfm n- LD NMD ----- AREba- QPEAGcm- TpeakDtte_bh- mm- Rvmm R. C. ----- Dfwm
169390 FIN SH
169400 #
169410 #
169420 #
169430 #
169440 R0002: CO0319 ROUTE RESERVOIR ->
169450 *** WARNING: Inflow peak was not reduced! Check OUTFLOW STORAGE table or reduce DT.
169460 R0002: CO0341 ROUTE PIPE ->
169470 *** WARNING: New pipe size used for routing.
169480 R0002: CO0347 ROUTE PIPE ->
169490 *** WARNING: New pipe size used for routing.
169500 R0002: CO0380 DI VERT HYD ->
169510 *** NOTE: Inflow hyd. is dry and cannot be diverted.
169520 R0002: CO0400 ROUTE PIPE ->
169530 *** WARNING: New pipe size used for routing.
169540 R0002: CO0407 ROUTE PIPE ->
169550 *** WARNING: New pipe size used for routing.
169560 R0002: CO0408 ROUTE PIPE ->
169570 *** WARNING: New pipe size used for routing.
169580 R0002: CO0416 ROUTE PIPE ->
169590 *** WARNING: New pipe size used for routing.
169600 R0002: CO0417 ROUTE PIPE ->
169610 *** WARNING: New pipe size used for routing.
169620 R0005: CO0319 ROUTE RESERVOIR ->
169630 *** WARNING: Inflow peak was not reduced! Check OUTFLOW STORAGE table or reduce DT.
169640 R0005: CO0341 ROUTE PIPE ->
169650 *** WARNING: New pipe size used for routing.
169660 R0005: CO0347 ROUTE PIPE ->
169670 *** WARNING: New pipe size used for routing.
169680 R0005: CO0363 ROUTE PIPE ->
169690 *** WARNING: New pipe size used for routing.
169700 R0005: CO0364 ROUTE PIPE ->
169710 *** WARNING: New pipe size used for routing.
169720 R0005: CO0372 ROUTE PIPE ->
169730 *** WARNING: New pipe size used for routing.
169740 R0005: CO0380 DI VERT HYD ->
169750 *** NOTE: Inflow hyd. is dry and cannot be diverted.
169760 R0005: CO0395 ROUTE PIPE ->
169770 *** WARNING: New pipe size used for routing.
169780 R0005: CO0400 ROUTE PIPE ->
169790 *** WARNING: New pipe size used for routing.
169800 R0005: CO0407 ROUTE PIPE ->
169810 *** WARNING: New pipe size used for routing.
169820 R0005: CO0408 ROUTE PIPE ->
169830 *** WARNING: New pipe size used for routing.
169840 R0005: CO0416 ROUTE PIPE ->
169850 *** WARNING: New pipe size used for routing.
169860 R0005: CO0417 ROUTE PIPE ->
169870 *** WARNING: New pipe size used for routing.
169880 R0010: CO0341 ROUTE PIPE ->
169890 *** WARNING: New pipe size used for routing.
169900 R0010: CO0347 ROUTE PIPE ->
169910 *** WARNING: New pipe size used for routing.
169920 R0010: CO0363 ROUTE PIPE ->
169930 *** WARNING: New pipe size used for routing.
169940 R0010: CO0364 ROUTE PIPE ->
169950 *** WARNING: New pipe size used for routing.
169960 R0010: CO0372 ROUTE PIPE ->
169970 *** WARNING: New pipe size used for routing.
169980 R0010: CO0380 DI VERT HYD ->
169990 *** NOTE: Inflow hyd. is dry and cannot be diverted.
170000 R0010: CO0395 ROUTE PIPE ->
170010 *** WARNING: New pipe size used for routing.
170020 R0010: CO0400 ROUTE PIPE ->
170030 *** WARNING: New pipe size used for routing.
170040 R0010: CO0407 ROUTE PIPE ->
170050 *** WARNING: New pipe size used for routing.
170060 R0010: CO0408 ROUTE PIPE ->
170070 *** WARNING: New pipe size used for routing.
170080 R0010: CO0416 ROUTE PIPE ->
170090 *** WARNING: New pipe size used for routing.
170100 R0010: CO0417 ROUTE PIPE ->
170110 *** WARNING: New pipe size used for routing.
170120 R0025: CO0341 ROUTE PIPE ->
170130 *** WARNING: New pipe size used for routing.
170140 R0025: CO0347 ROUTE PIPE ->
170150 *** WARNING: New pipe size used for routing.
170160 R0025: CO0363 ROUTE PIPE ->
170170 *** WARNING: New pipe size used for routing.

```

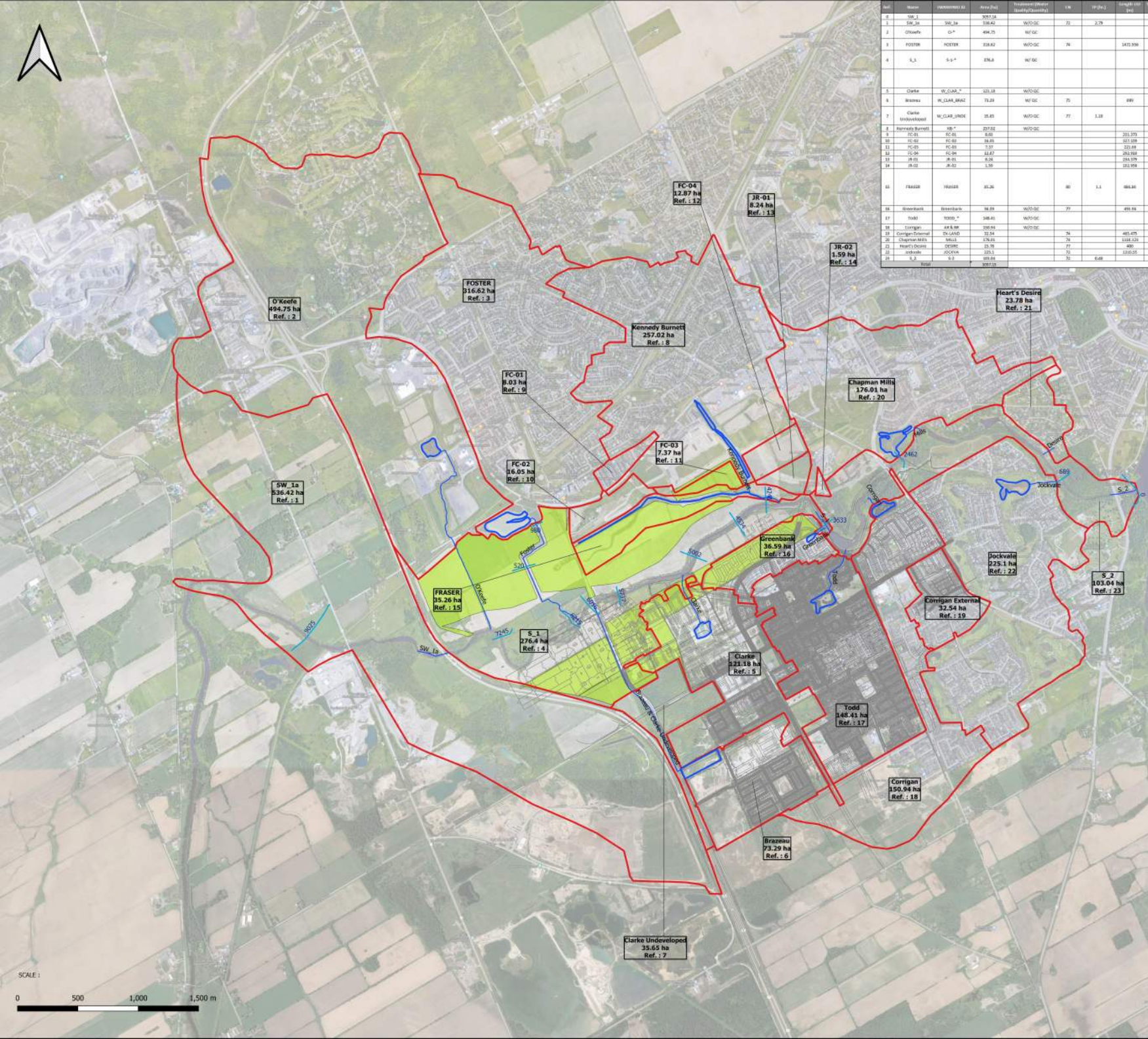
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170180 R0025: CO0364 ROUTE PIPE ->
170190 *** WARNING: New pipe size used for routing.
170200 R0025: CO0372 ROUTE PIPE ->
170210 *** WARNING: New pipe size used for routing.
170220 R0025: CO0380 DI VERT HYD ->
170230 *** NOTE: Inflow hyd. is dry and cannot be diverted.
170240 R0025: CO0385 ROUTE PIPE ->
170250 *** WARNING: New pipe size used for routing.
170260 R0025: CO0400 ROUTE PIPE ->
170270 *** WARNING: New pipe size used for routing.
170280 R0025: CO0407 ROUTE PIPE ->
170290 *** WARNING: New pipe size used for routing.
170300 R0025: CO0408 ROUTE PIPE ->
170310 *** WARNING: New pipe size used for routing.
170320 R0025: CO0416 ROUTE PIPE ->
170330 *** WARNING: New pipe size used for routing.
170340 R0025: CO0417 ROUTE PIPE ->
170350 *** WARNING: New pipe size used for routing.
170360 R0050: CO0341 ROUTE PIPE ->
170370 *** WARNING: New pipe size used for routing.
170380 R0050: CO0347 ROUTE PIPE ->
170390 *** WARNING: New pipe size used for routing.
170400 R0050: CO0363 ROUTE PIPE ->
170410 *** WARNING: New pipe size used for routing.
170420 R0050: CO0364 ROUTE PIPE ->
170430 *** WARNING: New pipe size used for routing.
170440 R0050: CO0372 ROUTE PIPE ->
170450 *** WARNING: New pipe size used for routing.
170460 R0050: CO0380 DI VERT HYD ->
170470 *** NOTE: Inflow hyd. is dry and cannot be diverted.
170480 R0050: CO0385 ROUTE PIPE ->
170490 *** WARNING: New pipe size used for routing.
170500 R0050: CO0400 ROUTE PIPE ->
170510 *** WARNING: New pipe size used for routing.
170520 R0050: CO0407 ROUTE PIPE ->
170530 *** WARNING: New pipe size used for routing.
170540 R0050: CO0408 ROUTE PIPE ->
170550 *** WARNING: New pipe size used for routing.
170560 R0050: CO0416 ROUTE PIPE ->
170570 *** WARNING: New pipe size used for routing.
170580 R0050: CO0417 ROUTE PIPE ->
170590 *** WARNING: New pipe size used for routing.
170600 R0100: CO0341 ROUTE PIPE ->
170610 *** WARNING: New pipe size used for routing.
170620 R0100: CO0347 ROUTE PIPE ->
170630 *** WARNING: New pipe size used for routing.
170640 R0100: CO0363 ROUTE PIPE ->
170650 *** WARNING: New pipe size used for routing.
170660 R0100: CO0364 ROUTE PIPE ->
170670 *** WARNING: New pipe size used for routing.
170680 R0100: CO0372 ROUTE PIPE ->
170690 *** WARNING: New pipe size used for routing.
170700 R0100: CO0380 DI VERT HYD ->
170710 *** NOTE: Inflow hyd. is dry and cannot be diverted.
170720 R0100: CO0385 ROUTE PIPE ->
170730 *** WARNING: New pipe size used for routing.
170740 R0100: CO0400 ROUTE PIPE ->
170750 *** WARNING: New pipe size used for routing.
170760 R0100: CO0407 ROUTE PIPE ->
170770 *** WARNING: New pipe size used for routing.
170780 R0100: CO0408 ROUTE PIPE ->
170790 *** WARNING: New pipe size used for routing.
170800 R0100: CO0416 ROUTE PIPE ->
170810 *** WARNING: New pipe size used for routing.
170820 R0100: CO0417 ROUTE PIPE ->
170830 *** WARNING: New pipe size used for routing.
170840 Simulation ended on 2021-03-04 at 12:01:23
170850 #
170860 #
170870 #

```


Attachment F

Updated Subcatchment Schematics & Tables



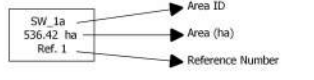
Sub-Catchment	Area (ha)	Reference
O'Keefe	494.75	Ref: 2
SW_1a	536.42	Ref: 1
FOSTER	316.62	Ref: 3
Kennedy Burnett	257.02	Ref: 8
FC-01	9.03	Ref: 9
FC-02	16.05	Ref: 10
FC-03	7.37	Ref: 11
Fraser	35.26	Ref: 15
S_1	276.4	Ref: 4
Greenbank	36.59	Ref: 16
FC-04	12.87	Ref: 12
JR-01	8.24	Ref: 13
JR-02	1.59	Ref: 14
Heart's Desire	23.78	Ref: 21
Chagman Mills	176.01	Ref: 20
Jockvale	225.1	Ref: 22
S_2	103.04	Ref: 23
Corrigan External	32.54	Ref: 19
Todd	148.41	Ref: 17
Clarke	121.18	Ref: 5
Corrigan	150.04	Ref: 18
Brazens	73.29	Ref: 6
Clarke Undeveloped	35.65	Ref: 7

Legend

- Sub-catchments
- SW_1
- Channel Cross Section
- SWM Drains
- SWM ponds
- Approved Developments
- Additional Future Developments
- Google Hybrid

File name: Figure 3 - Overall Jock River Lower Reach one Sub-catchments.pdf

XS 4534 Cross Section at station 4534



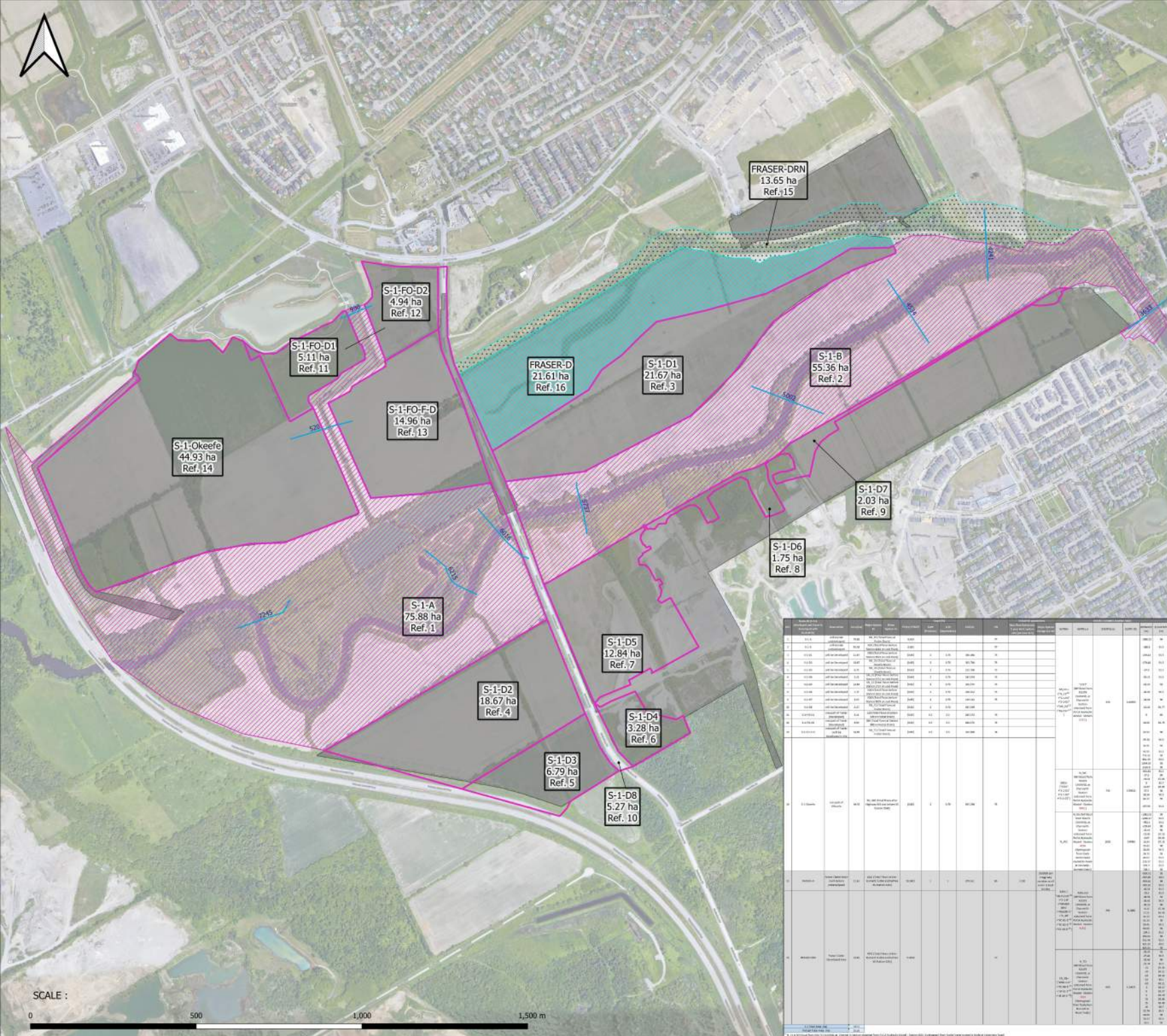
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DSEL
 david schaeffer engineering ltd

PROJECT : BCDC - Quantity Control Study

TITLE : Figure 3 - Overall Jock River Lower Reach one Sub-catchments
 Table 3 - Overall Jock River Lower Reach one Sub-catchments

PROJECT NO.	1474-16
DRAWN:	MM
DATE:	Mar. 2021



Legend

- Channel Cross Sections
- S-1 Sub-catchments and Fraser Sub-catchments
- S-1 Sub-catchments
- FRASER-DRN
- FRASER-D

Google Hybrid

File name:
Figure 4A - S-1 & Fraser Clarke Sub-catchments.pdf

XS 3633 Cross Section at station 3633

S-1-A 90.84 ha Area ID
Ref. 1 Area (ha)
Reference Number

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PROJECT :
BCDC - Quantity Control Study

TITLE :
Figure 4A - S-1 & Fraser Clarke Sub-catchments
Table 4A - S-1 & Fraser Clarke Sub-catchments

PROJECT NO. 1474-16

DRAWN: MM

DATE: Mar. 2021

Station	Channel	Area (ha)	Reference	Channel	Area (ha)	Reference	Channel	Area (ha)	Reference	Channel	Area (ha)	Reference	Channel	Area (ha)	Reference	Channel	Area (ha)	Reference	Channel	Area (ha)	Reference																											
31	S-1-A	75.88	Ref. 1	S-1-D1	21.67	Ref. 3	S-1-D2	18.67	Ref. 4	S-1-D3	6.79	Ref. 5	S-1-D4	3.28	Ref. 6	S-1-D5	12.84	Ref. 7	S-1-D6	1.75	Ref. 8	S-1-D7	2.03	Ref. 9	S-1-D8	5.27	Ref. 10	S-1-D9	1.75	Ref. 11	S-1-F0-D1	5.11	Ref. 12	S-1-F0-D2	4.94	Ref. 13	S-1-F0-F-D	14.96	Ref. 14	S-1-Okeefe	44.93	Ref. 15	FRASER-D	21.61	Ref. 16	FRASER-DRN	13.65	Ref. 17



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- Legend**
- Channel Cross Sections
 - S-1 Sub-catchments and Fraser Sub-catchments
 - ▨ S-1 Sub-catchments
 - ▨ FRASER-DRN
 - ▨ FRASER-D
 - Google Hybrid

File name: Figure 4B - S-1 & Fraser Clarke Sub-catchments.pdf

XS 3633 Cross Section at station 3633

S-1-A	▼ Area ID
90.84 ha	▶ Area (ha)
Ref. 1	▶ Reference Number

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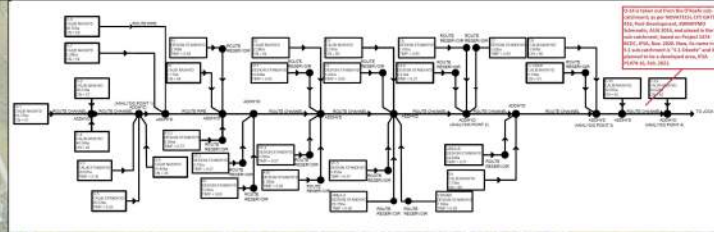
PROJECT : BCDC - Quantity Control Study

TITLE : Figure 4B - S-1 & Fraser Clarke Sub-catchments
 Table 4B - S-1 & Fraser Clarke Sub-catchments

PROJECT NO.	1474-16
DRAWN:	MM
DATE:	Mar. 2021

Station	Channel Name	Channel Type	Channel Material	Channel Slope	Channel Width	Channel Depth	Channel Velocity	Channel Discharge	Channel Capacity	Channel Status
3633	Fraser	Open Channel	Gravel	0.000	10.0	1.0	0.5	10.0	10.0	Active
3634	Fraser	Open Channel	Gravel	0.000	10.0	1.0	0.5	10.0	10.0	Active
3635	Fraser	Open Channel	Gravel	0.000	10.0	1.0	0.5	10.0	10.0	Active
3636	Fraser	Open Channel	Gravel	0.000	10.0	1.0	0.5	10.0	10.0	Active
3637	Fraser	Open Channel	Gravel	0.000	10.0	1.0	0.5	10.0	10.0	Active
3638	Fraser	Open Channel	Gravel	0.000	10.0	1.0	0.5	10.0	10.0	Active
3639	Fraser	Open Channel	Gravel	0.000	10.0	1.0	0.5	10.0	10.0	Active
3640	Fraser	Open Channel	Gravel	0.000	10.0	1.0	0.5	10.0	10.0	Active
3641	Fraser	Open Channel	Gravel	0.000	10.0	1.0	0.5	10.0	10.0	Active
3642	Fraser	Open Channel	Gravel	0.000	10.0	1.0	0.5	10.0	10.0	Active
3643	Fraser	Open Channel	Gravel	0.000	10.0	1.0	0.5	10.0	10.0	Active
3644	Fraser	Open Channel	Gravel	0.000	10.0	1.0	0.5	10.0	10.0	Active
3645	Fraser	Open Channel	Gravel	0.000	10.0	1.0	0.5	10.0	10.0	Active
3646	Fraser	Open Channel	Gravel	0.000	10.0	1.0	0.5	10.0	10.0	Active
3647	Fraser	Open Channel	Gravel	0.000	10.0	1.0	0.5	10.0	10.0	Active
3648	Fraser	Open Channel	Gravel	0.000	10.0	1.0	0.5	10.0	10.0	Active
3649	Fraser	Open Channel	Gravel	0.000	10.0	1.0	0.5	10.0	10.0	Active
3650	Fraser	Open Channel	Gravel	0.000	10.0	1.0	0.5	10.0	10.0	Active





Area ID	Area (ha)	Reference Number	Area ID	Area (ha)	Reference Number
O-1	47.34	1	O-14	5	31
O-2	26.61	2	O-15	11.76	30
O-3	43.68	5	O-17	11.99	15
O-4	43	3	A 1	2.6	9
O-5	64.2	6	A 7	3.51	12
O-6	16.14	4	A 8	5.36	17
O-7	3.67	7	A 9	5.36	18
O-8	48.69	11	D 1	1.21	8
O-13	8.68	29	D 2	2.35	14
O-14	5	31	D 3	2.36	18
O-15	11.76	30	D 4	1.56	26
O-17	11.99	15	D 5	1.94	28
A 1	2.6	9	AREA-A	68.04	22
A 7	3.51	12	AREA-B	23.18	27
A 8	5.36	17	STRAND	5.69	21
A 9	5.36	18	ST-1	0.72	10
D 1	1.21	8	ST-2	0.99	13
D 2	2.35	14	ST-3	0.44	16
D 3	2.36	18	ST-4	0.59	20
D 4	1.56	26	ST-5	1.98	23
D 5	1.94	28	ST-6	3.42	19
AREA-A	68.04	22	C 1	1.78	24
AREA-B	23.18	27	C 6	1.98	23
STRAND	5.69	21	C 7	1.78	24
ST-1	0.72	10			
ST-2	0.99	13			
ST-3	0.44	16			
ST-4	0.59	20			
ST-5	1.98	23			
ST-6	3.42	19			
C 1	3.42	19			
C 6	1.98	23			
C 7	1.78	24			



File name: Figure F1 - O'Keefe Sub-catchments.pdf

Legend
 20210129-O'Keefe Sub-catchment Boundaries
 O'Keefe Sub-catchment Boundaries
 Google Hybrid

HYDROLOGIC MODELING (SWHYMO) ANALYSIS POINT ENVIRONMENTAL MANAGEMENT (EMP) ANALYSIS POINT

S1 - E1

O-1 47.34 ha Ref. : 1

Area ID
Area (ha)
Reference Number

STA. 1840.6 CROSS SECTION AND STATION

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PROJECT :
BCDC - Quantity Control Study

TITLE :
Figure F1 - O'Keefe Sub-catchments
Table F1 - O'Keefe Sub-catchments
Schematic F1 - O'Keefe Sub-catchments

PROJECT NO.	1474
DRAWN:	MM
DATE:	Mar. 2021

Ref.	Name ID	Area (ha)	Major System To	Minor System To	T. Imperv.	XIMP	CN	LGI: Length (m) =SQRT (Area*10000/1.5)	Slope (%)		ROUTE RESERVOIR					ROUTE CHANNEL (Station 6016)					
									SLPP (Pervious)	SLPI (Impervious)	NHYDin	NHYDout	NHYDovf (OVERFLOW)	Outflow (cms)	Storage (ha-m)	NHYDin	NHYDout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)
1	FOSTER	325.44	FOSTER-OUT = ["P_FOS"+"FO-OVF"]		0.55	0.55	74	1472.956211	0.5	0.5	FOSTER	P_FOS	FO-OVF	10.34	10	SN_FO (Total Flows at Foster Drain)	N_CE	159	0.0818	-645.23	91.5
																				-391.2	91.5
																				-91	91.5
																				-85.52	91.5
																				-15.46	89.4
																				-9.79	89.31
																				-3.22	86.24
																				3.22	85.07
																				10.96	85.79
																				16.44	86.49
																				26.55	89.45
																				29.03	90.27
																				35.76	90.67
																				36.67	91
																				108.08	91
																				109.82	90.5
																				112.04	90.5
																				114.62	91
																				116.76	91.5



Ref.	Route ID (Linker Sub-catchment)	Area (ha)	Major System To	Minor System To	T. Imperv. FIP (%)	XIMP	C.R.	Slope (%)	ROUTE RESERVOIR			ROUTE CHANNEL (Station #348)																		
									WYDIn	WYDOut	WYDDef (OVERFLOW)	WYDIn	WYDOut	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)													
1	W_CLAR_MJ	1,772	Clarke	Todd	0.50	0.80	77	109		W_CLAR_MJ	W_CLAR_MIn	W_CLAR_MJ	0.213	0.0001*																
2	W_CLAR_ALL	119,338	Clarke		0.05	0.4	77	892.38	1	W_CLAR = W_CLAR_MJ	MS_P2	P2-DIVF	0.128	0.351																
													0.138	0.409																
													0.149	0.448																
													0.177	0.561																
													0.234	1.223																
													0.305	1.32																
													0.486	1.821																
													0.881	2.125																
													0.995	2.434																
													1.089	2.383																
													1.31	2.647																
4.884	2.861																													
13.048	3.188																													
23.745	3.523																													
36.476	3.871																													
45.989	4.227																													
61.652	4.589																													
3	W_CLAR_UNDE	35.65	Jock River (Station 4534)		1.30		77																							
		156.83																												

* Small storage was assumed to allow overflow and direct the flow towards minor and major systems
 ** N_WC is AFFDOut from ROUTE CHANNEL at Channel X-Section obtained from RIVICA Hydraulic Model - Station 5062 (Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain)

Legend

- Channel Cross Sections
- SWMF Drains
 - Brazeau & Clarke Undeveloped
 - Clarke
- SWMF ponds
 - West Clarke
 - Brazeau
- Clarke Sub-catchment & Brazeau Sub-catchment
 - W_CLAR_MJ
 - W_CLAR_MJ (Major Only to Clarke SWM Pond)
 - W_CLAR_ALL
 - W_CLAR_BRAZ
 - W_CLAR_UNDE
 - Clarke-Brazeau-CAD
- Google Hybrid

File name: Figure F3 - Clarke & Brazeau Sub-catchments.pdf

XS 4534 Cross Section at station 4534 Minor System

W_CLAR_MJ (Major Only to Clarke SWM Pond) 1,772 ha & Ref. 1

- Area ID
- Reference Number
- Area (ha)

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PROJECT : BCDC - Quantity Control Study

TITLE : Figure F3 - Clarke & Brazeau Sub-catchments
 Table F3-1 - Clarke Sub-catchments
 Figure F3-2 - Brazeau Sub-catchment

PROJECT NO.	1474-16
DRAWN:	MM
DATE:	Mar. 2021

Ref.	Route ID (Linker Sub-catchment)	Area (ha)	Major System To	Minor System To	T. Imperv. FIP (%)	XIMP	C.R.	Slope (%)	ROUTE RESERVOIR			ROUTE CHANNEL (Station #348)																	
									WYDIn	WYDOut	WYDDef (OVERFLOW)	WYDIn	WYDOut	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)												
4	W_CLAR_BRAZ	73.29	Clarke	Jock River	0.05	0.8	77	889		W_CLAR_BRAZ	MS_P2	P2-DIVF	0.213	0.0001*															
													0.088	0.301															
													0.271	0.583															
													0.576	0.911															
													0.88	0.984															
													0.891	0.943															
													1.288	0.93															
													1.538	1.243															
													1.533	1.267															
													1.194	1.476															
													1.1	1.851															
													1.283	1.389															
1.1	1.885																												
1.388	2.833																												



* Small storage was assumed to allow overflow and direct the flow towards minor and major systems

Ref.	Name ID (Clarke Sub-catchment)	Area (ha)	Major System To	Minor System To	T. Imperv. [TP (hr)]	XIMP	CN	LGI: Length (m) =SQRT (Area*10000/1.5)	Slope (%)	ROUTE RESERVOIR					ROUTE CHANNEL (Station 4534)																			
										NHYDin	NHYDout	NHYDovf (OVERFLOW)	Outflow (cms)	Storage (ha-m)	NHYDin	NHYDout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)														
1	W_CLAR_MJ	1.772	Clarke	Todd	0.59	0.46	77	109	1	W_CLAR_MJ	W_CLAR_MJn	W_CLAR_MJj	0.213	0.0001*																				
2	W_CLAR_ALL	119.398	Clarke		0.65	0.6	77	892.18	1	W_CLAR = W_CLAR_ALL + W_CLAR_MJj	MS_P2	P2-OVF	0.128	0.161																				
													0.138	0.409																				
													0.148	0.68																				
													0.227	0.931																				
													0.354	1.223																				
													0.505	1.52																				
													0.666	1.821																				
													0.831	2.123																				
													0.995	2.434																				
													1.069	2.583																				
													1.51	2.647																				
													4.904	2.861																				
													13.048	3.188																				
													23.745	3.523																				
36.474	3.871																																	
45.938	4.127																																	
61.652	4.539																																	
3	W_CLAR_UNDE	35.65	Jock River (Station		[1.10]		77																											
Total		156.82																																

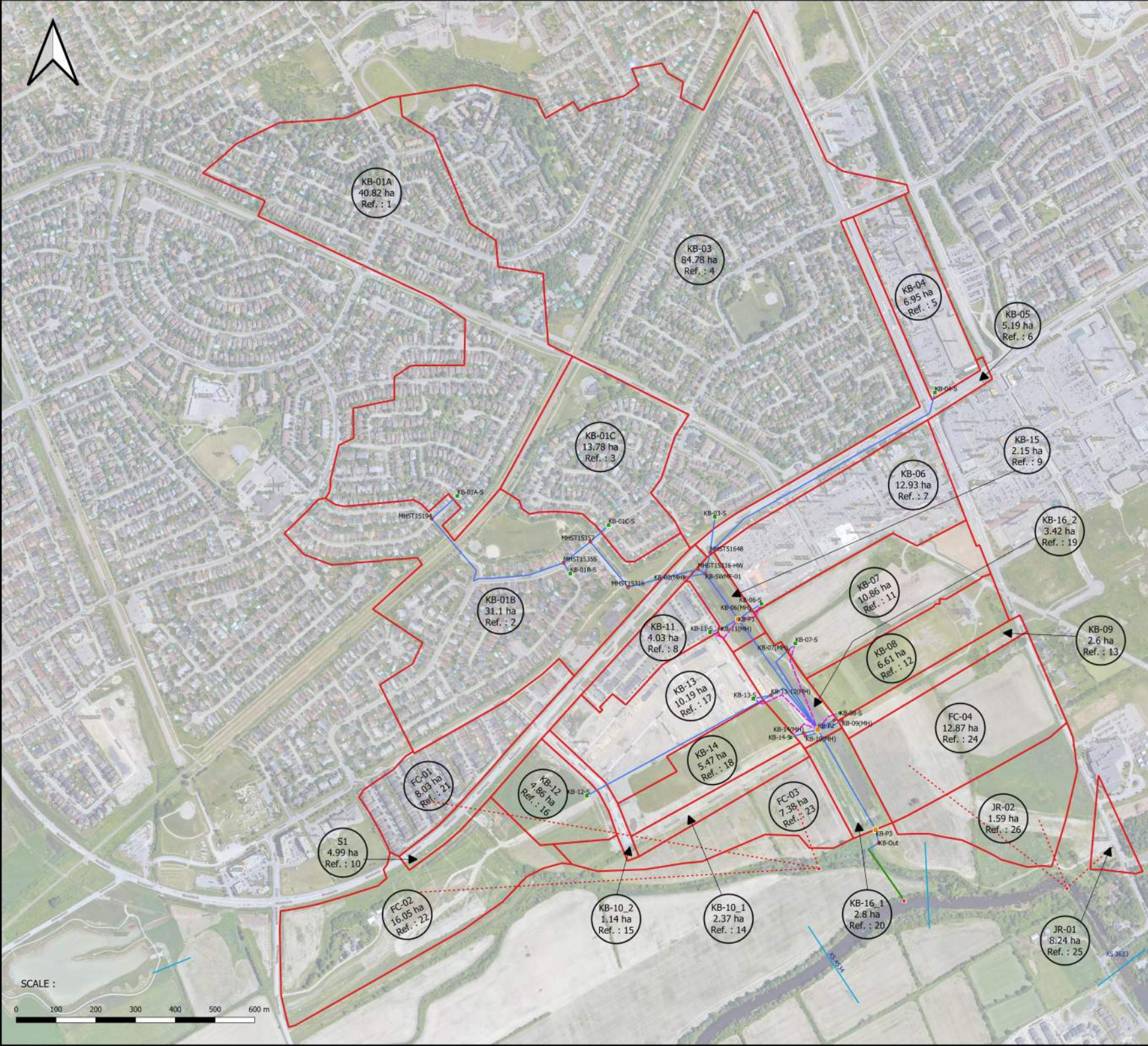
* Small storage was assumed to allow overflow and direct the flow towards minor and major systems

** N_WC is NHYDout from ROUTE CHANNEL at Channel X-Section obtained from RVCA Hydraulic Model - Station 5002 (Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain)

Ref.	ID (Brazeau Sub-catchment)	Area (ha)	Major System To	Minor System To	T. Imperv. [TP (hr)]	XIMP	CN	LGI: Length (m) =SQRT (Area*10000/1.5)	Slope (%)		ROUTE RESERVOIR					ROUTE CHANNEL (Station 6016)					
									SLPP (Pervious)	SLPI (Impervious)	NHYDin	NHYDout	NHYDovf (OVERFLOW)	Outflow (cms)	Storage (ha-m)	NHYDin	NHYDout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)
4	W_CLAR_BRAZ	73.29	Pond in Brazeau which drains to Jock River (station 6016)*		0.65	0.6	77	699	1	0.5	W_CLAR_BRAZ	MS_P10	P10-OVF	0.068	0.001	SN_FO (Total Flows at Foster Drain)	N_CE**	159	0.0818	-645.23	91.5
														0.271	0.022					-391.2	91.5
														0.379	0.051					-91	91.5
														0.48	0.091					-85.52	91.5
														0.853	0.341					-15.46	89.4
														1.005	0.61					-9.79	89.31
														1.128	1.231					-3.22	86.24
														1.155	1.592					3.22	85.07
														1.194	1.876					10.96	85.79
														1.2	1.921					16.44	86.49
														1.259	2.369					26.55	89.45
														1.3	2.665					29.03	90.27
														1.349	2.813					35.76	90.67
																				36.67	91
																				108.08	91
		109.82	90.5																		
		112.04	90.5																		
		114.62	91																		
		116.76	91.5																		
Total		73.29																			

* Brazeau pond discharges directly to the jock river through a road side ditch on the west side of Borrissokane road (station 6016)

** N_CE is NHYDout from ROUTE CHANNEL at Channel X-Section obtained from RVCA Hydraulic Model - Station 6016 (Hydrograph from Node Foster routed to Node at Cedarview Road)



Area ID	Area (ha)	Reference Number
KB-01A	40.82	1
KB-01B	31.1	2
KB-01C	13.78	3
KB-03	84.78	4
KB-04	6.95	5
KB-05	5.19	6
KB-06	12.93	7
KB-07	10.86	11
KB-08	6.61	12
KB-09	2.6	13
KB-10_1	2.37	14
KB-10_2	1.14	15
KB-11	4.03	8
KB-12	4.86	16
KB-13	10.19	17
KB-14	5.47	18
KB-15	2.15	9
KB-16_1	2.8	20
KB-16_2	3.42	19
FC-01	8.03	21
FC-02	16.05	22
FC-03	7.36	23
FC-04	12.87	24
JR-01	8.24	25
JR-02	1.59	26
S1	4.99	10

- Legend**
- Ken-BU storage
 - Ken-BU MH
 - ▲ Ken-BU Pond
 - ▲ Ken-BU Outfalls
 - Ken-BU Pipe
 - Ken-BU Major System
 - Ken-BU Channel
 - Ken-BU to FC (Fraser Clarke) and JR (Jock River)
 - Kennedy Burnett Sub-catchment
 - Kennedy Burnett (Ken-BU)
 - Google Hybrid

File name: Figure F4 - Kennedy Burnett Sub-catchments.pdf



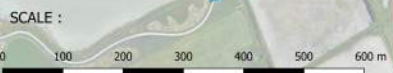
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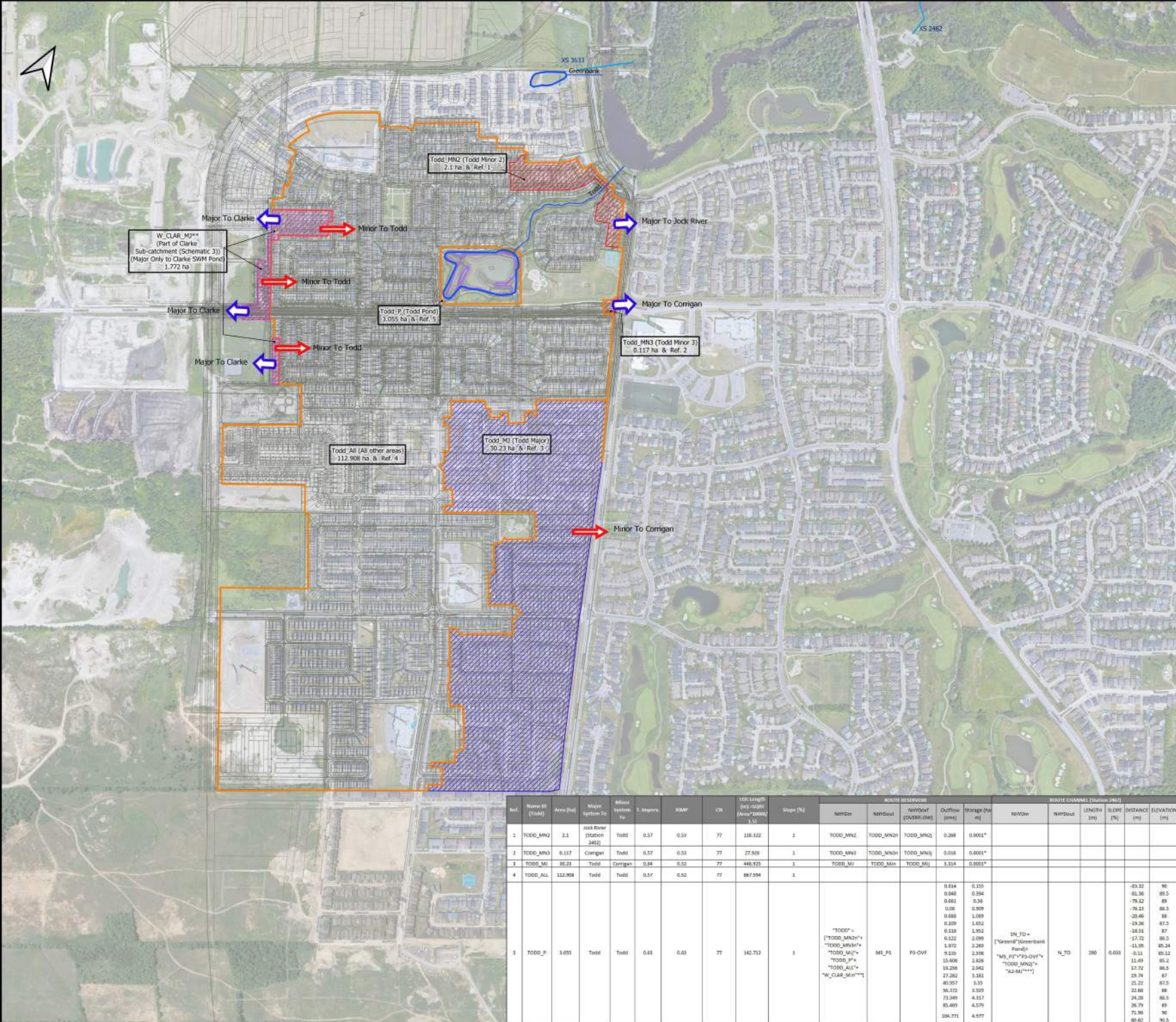
DSEI
 david schaeffer engineering ltd

PROJECT :
 BCDC - Quantity Control Study

TITLE :
 Figure F4 - Kennedy Burnett Sub-catchments
 Table F4 - Kennedy Burnett Sub-catchments

PROJECT NO.	1474
DRAWN:	MM
DATE:	Mar. 2021





- Legend**
- Channel Cross Sections
 - SWMF Drains
 - SWMF ponds
 - Sub-catchments
 - ▨ Todd
 - ▨ Todd Minor
 - ▨ Todd Major
 - ▨ Todd Pond Boundary
 - ▨ W_CLAR_Major
 - Todd-Greenbank-CAD
 - Google Hybrid

File name: Figure F5 -Todd Sub-catchments.pdf

➡ Major System ➡ Minor System

XS 2462 Cross Section at station 2462
 Area ID
 Reference Number
 Area (ha)

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SCALE : 0 250 500 m

PROJECT : BCDC - Quantity Control Study

TITLE : Figure F5 -Todd Sub-catchments
 Table F5 -Todd Sub-catchments

PROJECT NO. 1474-16

DRAWN: MM

DATE: Mar. 2021

Ref.	Name ID (Code)	Area (ha)	Major System To	Minor System To	T. Ingress	XMP	CH	MFC Length (m) (4015 Area/10000 L/S)	Slope (%)	ROUTER RESERVOIR			ROUTE CHANNEL (Sewer/RAZ)					
										NIPIDin	NIPIDout	NIPIDin	NIPIDout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)	
1	TODD_MN2	2.1	Jock River (Station 2462)	Todd	0.57	0.55	77	138.322	1	TODD_MN2	TODD_MN2	TODD_MN2	0.268	0.0001*				
2	TODD_MN3	0.117	Corrigan	Todd	0.57	0.53	77	27.928	1	TODD_MN3	TODD_MN3	TODD_MN3	0.016	0.0001*				
3	TODD_M4	30.23	Todd	Corrigan	0.64	0.52	77	448.925	1	TODD_M4	TODD_Min	TODD_Min	3.314	0.0001*				
4	TODD_All	112.908	Todd	Todd	0.57	0.52	77	667.294	1									
5	TODD_P	3.055	Todd	Todd	0.63	0.63	77	142.713	1	ROUTER RESERVOIR			ROUTE CHANNEL (Sewer/RAZ)					
										MIPin	MIPout	MIPin	MIPout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)	
Total																		

* Small storage was assumed to allow overflow and direct the flow towards minor and major systems
 ** "W_CLAR_Min" is the minor system from the major system: area/Area = 1.772 ha & TRMP = 0.55 & XMP = 0.46 & CH = 75 & Slope = 1% & Outflow = 0.223 c/m in Clarke sub-catchment (Schematic 3) to Jock River (Station 2462)
 *** "AD_Min" is the major system from A2 area (Area = 25.1 ha & TRMP = 0.52 & XMP = 0.42 & CH = 75 & Slope = 1% & Storage = 934 cum & Flow rate = 3.838 c/m) in Corrigan sub-catchment (Schematic 1) to Todd sub-catchments

Ref.	Name ID (Todd)	Area (ha)	Major System To	Minor System To	T. Imperv.	XIMP	CN	LGI: Length (m) =SQRT (Area*10000/1.5)	Slope (%)	ROUTE RESERVOIR					ROUTE CHANNEL (Station 2462)					
										NHYDin	NHYDout	NHYDovf (OVERFLOW)	Outflow (cms)	Storage (ha-m)	NHYDin	NHYDout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)
1	TODD_MN2	2.1	Jock River (Station 2462)	Todd	0.57	0.53	77	118.322	1	TODD_MN2	TODD_MN2n	TODD_MN2j	0.268	0.0001*						
2	TODD_MN3	0.117	Corrigan	Todd	0.57	0.53	77	27.928	1	TODD_MN3	TODD_MN3n	TODD_MN3j	0.016	0.0001*						
3	TODD_MJ	30.23	Todd	Corrigan	0.64	0.52	77	448.925	1	TODD_MJ	TODD_MJn	TODD_MJj	3.314	0.0001*						
4	TODD_ALL	112.908	Todd	Todd	0.57	0.52	77	867.594	1											
5	TODD_P	3.055	Todd	Todd	0.63	0.63	77	142.712	1	"TODD" = ["TODD_MN2n"+ "TODD_MN3n"+ "TODD_MJj"+ "TODD_P"+ "TODD_ALL"+ "W_CLAR_MJn"***]	MS_P3	P3-OVF	0.014 0.048 0.061 0.08 0.088 0.109 0.118 0.122 1.972 9.135 15.608 19.256 27.282 40.957 56.372 73.349 85.469 104.771	0.155 0.394 0.56 0.909 1.089 1.652 1.952 2.099 2.269 2.598 2.826 2.942 3.181 3.55 3.929 4.317 4.579 4.977	SN_TO = ["GreenB" (Greenbank Pond)+ "MS_P3"+"P3-OVF"+ "TODD_MN2j"+ "A2-MJ"***]	N_TO	280	0.033	-83.32 -81.36 -79.12 -76.13 -20.46 -19.36 -18.51 -17.72 -11.95 -0.11 11.49 17.72 19.74 21.22 22.68 24.28 26.79 71.98 80.62	90 89.5 89 88.5 88 87.5 87 86.5 85.24 85.12 85.2 86.5 87 87.5 88 88.5 89 90 90.5
Total		148.41																		

* Small storage was assumed to allow overflow and direct the flow towards minor and major systems

** "W_CLAR_MJn" is the minor system from the major system area(Area = 1.772 ha & TIMP = 0.59 & XIMP = 0.46 & CN = 75 & Slope = 1% & Outflow = 0.213 cms)in Clarke sub-catchment (Schematic 3) to Jock River (Station 2462)

*** "A2-MJ" is the major system from A2 area (Area = 25.5 ha & TIMP = 0.52 & XIMP = 0.42 & CN = 75 & Slope = 1% & Storage = 924 cu-m & Flow rate = 1.818 cms) in Corrigan sub-catchment (Schematic 1) to Todd sub-catchment



Station	Flow	Velocity	Depth	Area	Perimeter	Roughness	Capacity	Notes
XS 2462	10.0	1.5	0.8	1.2	4.5	0.015	1.5	
XS 2633	15.0	1.8	1.0	1.5	5.0	0.015	2.0	
XS 2902	20.0	2.0	1.2	2.0	6.0	0.015	2.5	
XS 3524	30.0	2.5	1.5	3.0	7.5	0.015	3.5	



File name:
Figure F6 - Corrigan Sub-catchments.pdf

Major System
 Overflow

Legend

- Channel Cross Section
- Corrigan-Pipe Line
- Corrigan-MH
- Corrigan Drainage Boundaries
- Corrigan Drainage Boundaries

Area ID
 Area (ha)
 Reference Number
 Cross Section at station 0

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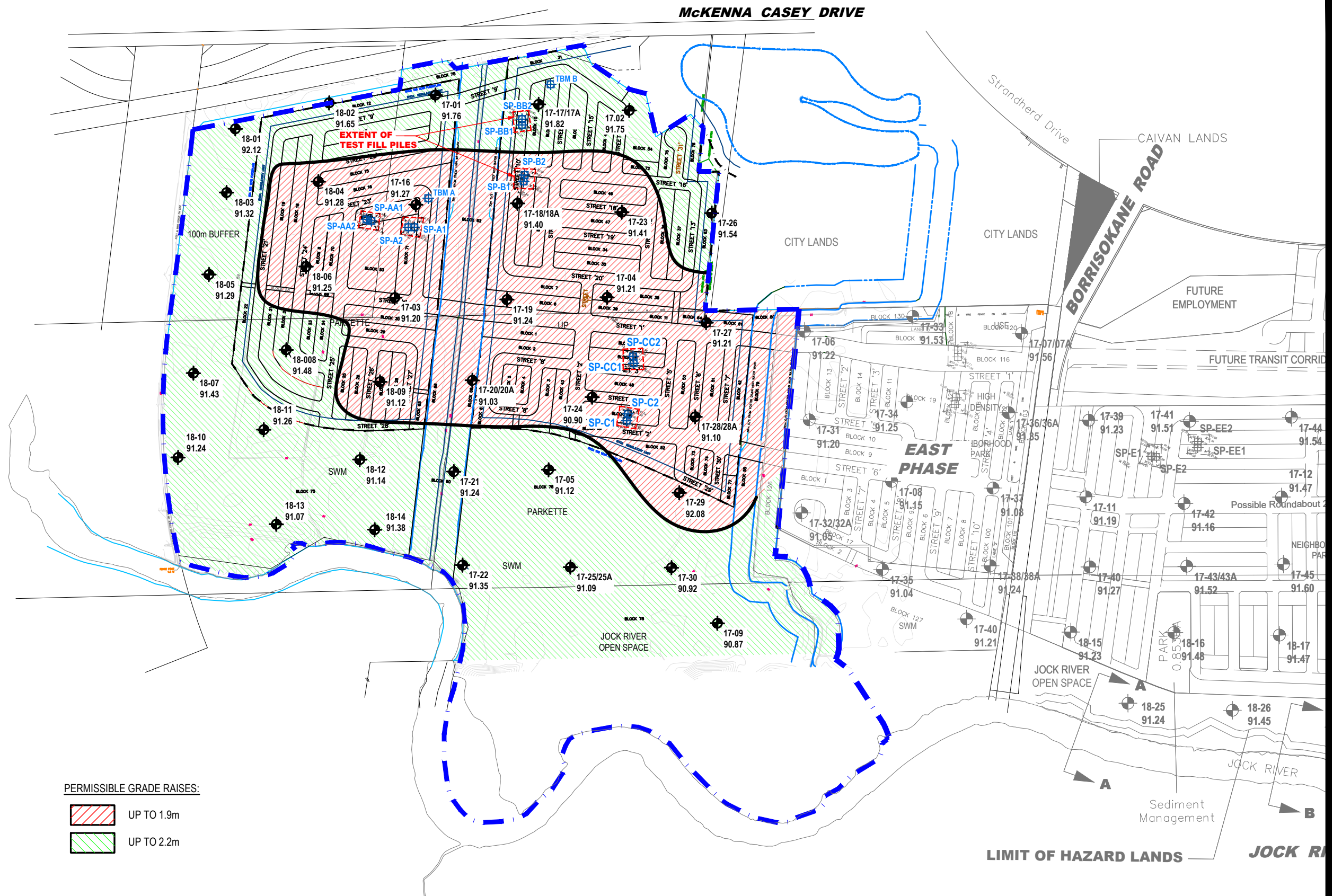
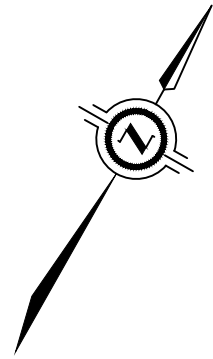
TITLE :
Figure F6 - Corrigan Sub-catchments
Table F6 - Corrigan Sub-catchments

PROJECT NO.	1474
DRAWN:	MM
DATE:	Mar. 2021


SCALE :
0 500 1,000 1,500 m

APPENDIX E

GEO TECHNICAL



LEGEND:

-  APPROXIMATE BOREHOLE LOCATION (GOLDER ASSOCIATES, 04/2019)
- 91.07 GROUND SURFACE ELEVATION (m)
- BOREHOLE LOCATIONS WERE SURVEYED BY OTHERS AND ARE REFERENCED TO A GEODETIC DATUM.

PERMISSIBLE GRADE RAISES:

-  UP TO 1.9m
-  UP TO 2.2m



9 AURIGA DRIVE
OTTAWA, ON
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TEL: (613) 226-7381

NO.	REVISIONS	DATE	INITIAL
3	UPDATED TO LATEST CONCEPTUAL PLAN	08/12/2022	KP
2	GRADE RAISE RESTRICTIONS UPDATED	30/11/2021	KP
1	UPDATED TO LATEST CONCEPTUAL PLAN	19/10/2021	OC

CAIVAN COMMUNITIES
GEOTECHNICAL INVESTIGATION
PROP. RESIDENTIAL DEVELOPMENT - CONSERVANCY LANDS WEST
OTTAWA, ONTARIO

Title:
PERMISSIBLE GRADE RAISE PLAN

Scale:	1:5000	Date:	09/2019
Drawn by:	MPG	Report No.:	PG5036-2
Checked by:	SD	Dwg. No.:	PG5036-5
Approved by:	SD	Revision No.:	3