

# **ADEQUACY OF SERVICES REPORT**

*FOR*

## **BARRHAVEN CONSERVANCY DEVELOPMENT CORPORATION**

## **BARRHAVEN CONSERVANCY WEST**

CITY OF OTTAWA

**PROJECT NO.: 21-1226**

**OCTOBER 2021  
1<sup>ST</sup> SUBMISSION  
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## **1.0 INTRODUCTION**

David Schaeffer Engineering Limited (DSEL) has been retained to prepare an Adequacy of Services Report (AES) in support of the Barrhaven **Conservancy West** development area on behalf of Barrhaven Conservancy Development Corporation (BCDC).

The overall Conservancy land area is approximately 139.7 ha (all land use components) and is located within the City of Ottawa urban boundary in the Barrhaven ward. As illustrated in **Figure 1**, the subject site is located north of the Jock River, east of Highway 416, west of Borrisokane Road and south of McKenna Casey Drive.

The focus of this report is for the **Conservancy West** land area that is located west of the existing Foster Ditch which bisects the overall BCDC landholdings and consists of vacant land. The subject lands are approximately 35.6ha in area (including all right-of-ways, residential area and park areas) and the proposed development draft plan **Figure 2** is provided for reference. The development area is currently zoned Development Reserve (DR) and is planned to be developed with a mix of detached single homes, townhomes, park blocks, open spaces and a road network.

A previous draft plan application has been submitted for the BCDC landholdings to the east of this development area with draft approval anticipated in October 2021.

The Conservancy West development area is outside of the Jock River 100-year limit as confirmed by the Rideau Valley Conservation Authority (RVCA). Refer to the RVCA confirmation letter in **Appendix D**. The 100-year regulatory flood line is demonstrated in Drawing 1 (Grading) and Drawing 3 (Stormwater) in the **Appendix**.

The objective of this report is to provide sufficient detail to demonstrate that the proposed development area can be supported by municipal services.

## 1.1 Existing Conditions

The initial **Conservancy West** property topography is relatively flat with the existing ground elevations varying between 91 m and 92 m. All existing flows are either overland to the Jock River or conveyed to the Jock River by way of the O'Keefe Municipal Drain or the Foster Ditch (and their tributaries) which run through the subject property. The property is within the Jock River watershed and is under the jurisdiction of the RVCA.

## 1.2 Summary of Pre-Consultation

The following provides a summary of the pre-consultation:

### 1.2.1 Ministry of the Environment, Conservation and Parks (MECP)

Prior consultations associated with the Conservancy Phase 1 development were previously undertaken for the approval of that phase of the development area.

A pre-consultation with the local MECP office has not yet been completed for the Conservancy West development area until the functional design details and requirements have been established with the City of Ottawa.

### 1.2.2 Rideau Valley Conservation Authority (RVCA)

Multiple consultations, analysis and submissions were coordinated with the RVCA to establish that the development area is outside of the Jock River 100-year limit. See the RVCA documentation in **Appendix D** for reference.

## 1.3 Existing Permits / Approvals

Key approvals associated with the advancement of development of the Barrhaven Conservancy area, are presented in the following table. The most relevant approval is the Environmental Compliance Approval (ECA) for the South Nepean Collector sanitary trunk sewer that future phases will be connecting to. The document is provided in **Appendix A** for reference.

**Table 1A: Existing Permits / Approvals**

Agency	Approval Type	Approval Number	Remarks
Ministry of the Environment, Conservation and Parks (MECP)	Environmental Compliance Approval	# 8129-AB7LDF (June 23, 2016)	South Nepean Collector existing approval (sanitary outlet for development area)
Rideau Valley Conservation Authority (RVCA)	RVCA Letter of Permission under O.Reg. 174/06	RV5-4419	Letter of permission related to placement of fill within a regulated area.

#### 1.4 Required Permits / Approvals

The City of Ottawa must approve detailed engineering design drawings and reports prior to future construction of the municipal infrastructure identified in this report. This will occur as part of the Plan of Subdivision application process and detailed design.

Based on pre-consultation with City staff, the additional approvals and permits listed in the following table are expected to be required prior to construction of the municipal infrastructure detailed herein. Please note that other permits and approvals may be required, as detailed in the other studies to be submitted as part of the Plan of Subdivision application (e.g. *Tree Conservation Report, Environmental Impact Statement, Phase 1 Environmental Site Assessment, Headwater Drainage Feature Assessment, etc.*)

**Table 1B: Required Permits/Approvals**

Agency	Permit/Approval Required	Trigger	Remarks
MECP	Environmental Compliance Approval	Construction of new sanitary and storm sewers throughout the subdivision.	The MECP will review the sanitary and storm sewer design through the City of Ottawa transfer of review process.
MECP	Environmental Compliance Approval	Implementation of oil-grit separator units for quality control.	The MECP will review the stormwater management appurtenance design through the City of Ottawa transfer of review process.
MECP	Permit to Take Water	Construction of proposed land uses (e.g. basements for residential homes) and services.	Pumping of groundwater may be required during construction, given groundwater conditions and proposed land uses and on-site/off-site municipal infrastructure.

City of Ottawa	MECP Form 1 – Record of Watermains Authorized as a Future Alteration.	Construction of watermains throughout the subdivision	The City of Ottawa will review the watermains on behalf of the MECP through the Form 1 – Record of Watermains Authorized as a Future Alteration.
RVCA	Permit under Ontario Regulation 174/06, RVCA's Development, Interference with Wetlands and Alterations to Shorelines and Watercourses Regulation	Grading (proposed development & potential temporary access roads) within the subject lands (i.e. crossing of Foster Ditch)	Supporting applications and documentation as required through consultation with the RVCA.
RVCA	Outlets to Jock River	In conjunction with issuance of MECP applications	Supporting applications and documentation as required through consultation with the RVCA.
RVCA	Alteration to Watercourses (O'Keefe Drain)	As necessary through consultation with the RVCA	Supporting applications and documentation as required through consultation with the RVCA.
City of Ottawa	Commence Work Notification (CWN)	Construction of new sanitary and storm sewers throughout the subdivision	The City of Ottawa will issue a commence work notification for construction of the sanitary and storm sewers once an approval is issued by the MECP.

## 2.0 GUIDELINES, PREVIOUS STUDIES, AND REPORTS

### 2.1 Existing Studies, Guidelines, and Reports

The following studies were utilized in the preparation of this report.

- Ottawa Sewer Design Guidelines, City of Ottawa, *SDG002*, October 2012 (*City Standards*)
  - Technical Bulletin ISDTB-2014-01  
City of Ottawa, February 5, 2014 (ITSB-2014-01)
  - Technical Bulletin PIEDTB-2016-01  
City of Ottawa, September 6, 2016 (PIEDTB-2016-01)



- Technical Bulletin ISTB-2018-01  
City of Ottawa, March 21, 2018  
(*ISTB-2018-01*)
- Technical Bulletin ISTB-2018-04  
City of Ottawa, June 27, 2018  
(*ISTB-2018-04*)
- Ottawa Design Guidelines – Water Distribution  
City of Ottawa, July 2010.  
(*Water Supply Guidelines*)
  - Technical Bulletin ISD-2010-2  
City of Ottawa, December 15, 2010.  
(*ISD-2010-2*)
  - Technical Bulletin ISDTB-2014-2  
City of Ottawa, May 27, 2014.  
(*ISDTB-2014-2*)
  - Technical Bulletin ISTB-2018-02 / ISTB-2019-02  
City of Ottawa, March 21, 2018 / July 08, 2019  
(*ISTB-2018-02 / ISTB-2019-02*)
  - Technical Bulletin ISDTB-2021-03  
City of Ottawa, August 18, 2021  
(*ISTB-2021-03*)
- Design Guidelines for Sewage Works,  
Ministry of the Environment, Conservation and Parks, 2008. (formerly MOECC)  
(*MECP Design Guidelines*)
- Stormwater Planning and Design Manual,  
Ministry of the Environment, March 2003.  
(*SWMP Design Manual*)
- City of Ottawa Official Plan,  
adopted by Council 2003.  
(*Official Plan*)
- City of Ottawa Secondary Plan – Former Nepean – South Nepean Urban Area –  
Areas 9 and 10,  
Adopted by Council 2003.  
(*Secondary Plan*)
- South Nepean Collector: Phase 2 Hydraulics Review / Assessment Technical  
Memorandum  
Novatech, August 2015  
(*Novatech SNC Memo*)

- South Nepean Collector: Phase 2 Preliminary Design Report,  
Novatech, March 2016  
*(Novatech SNC Design Report)*
- Strandherd Drive Widening Project, South Nepean Collector: Phase 3 Sanitary  
Flow Calculations  
Novatech, May 2019  
*(2019 Novatech SNC Design Report)*
- Hydraulic Potable Water Assessment for Barrhaven Conservancy Development  
Corporation, March 2021  
*(Stantec Hydraulic Analysis)*
- Jock River Reach One Subwatershed Study  
Stantec, 2007  
*(Jock River SWS)*
- Geotechnical Investigation, Proposed Residential Development, Conservancy  
Lands West, Ottawa, Ontario  
Paterson Group, September 27, 2019 (Project No. PG5036-1)  
*(Geotechnical Report)*
- Environmental Impact Statement for Barrhaven Conservancy East  
Kilgour & Associates Ltd., July 29, 2020  
*(Kilgour EIS)*

### 3.0 WATER SUPPLY SERVICING

#### 3.1 Existing Water Supply Services

The subject property is located adjacent to the City of Ottawa's Pressure Zone (PZ) 3SW (previously known as PZ BARR). PZ SUC services the lands that are east of the subject property, as well as south of the Jock River.

The City of Ottawa has recently reconfigured the pressure zones servicing Barrhaven and the South Urban Community (SUC) in order to improve reliability and efficiency and to increase pumping capacity to accommodate for future growth in the area. There are three pumping stations servicing Zone 3SW and Zone SUC as follows: the Fallowfield Road Pumping Station (FRPS), the Barrhaven Pumping Station (BPS) and the Ottawa South Pumping Station (OSPS).

The future water mains to be implemented through the detailed design process for the adjacent Conservancy East lands will facilitate water service to the West area. There are future trunk water mains proposed in the vicinity of Conservancy East area which will provide water service to the development lands. These services will be further extended to provide the requisite water supply to this development area.

#### 3.2 Water Supply Servicing Design

Stantec Consulting Limited was previously retained to perform a hydraulic assessment for the Barrhaven Conservancy Lands. The ***Hydraulic Potable Water Assessment for Barrhaven Conservancy Development Corporation (Stantec Hydraulic Analysis)*** prepared by Stantec (March 2021) is enclosed in ***Appendix B*** for reference. The analysis reviewed the adjacent pressure zones and various servicing alternatives. The subject property was deemed serviceable and the analysis offered a number of servicing alternatives that could adequately service the subject property conforming to all relevant City and Ministry of the Environment, Conservation and Parks (MECP) Guidelines and Policies.

The proposed water servicing layout is presented in ***Figure 3*** and shows the anticipated water extension from the Conservancy East area. The ***Stantec Hydraulic Analysis*** indicates that there are several options to provide water servicing to support the development of the site, extending from existing or planned infrastructure. Prior coordination with City staff (and further discussion at a February 11, 2021 meeting) has indicated that an acceptable approach would be for service to be provided from the recently reconfigured South Urban Community (SUC) pressure zone (identified as Alternative '2C' in the ***Stantec Hydraulic Analysis***). This new zone was established in order to improve reliability and allow for accommodation of future growth. As such, the water supply network will be expanded through neighboring properties within the PZ SUC Nepean Town Centre (NTC) development area (i.e. Claridge's "Burnett Lands")

development at 3370 Greenbank Road – a current General Plan of services is provided in **Appendix B** for reference) with ultimate watermain concepts in line with the prior Stantec study completed titled “*Kennedy-Burnett Potable Water Master Servicing Study (April 2014)*” (excerpt provided in **Appendix B**). Coordination with Claridge and City staff has been undertaken in order to facilitate an appropriate watermain stub location from that development area (see emails and supporting information in **Appendix B**). The **Stantec Hydraulic Analysis** assessed the feeds as being a 200mm connection at Claridge’s development (expanding to a 300mm) and a 300mm extension from Chapman Mills Drive to feed into the Barrhaven Conservancy development areas. Once extended to service the Conservancy East area the watermain network will be further extended to the West area. At the time of detailed design, detailed hydraulic modelling will be undertaken to verify that the proposed on-site and off-site watermains are in conformance with all relevant criteria. Other external watermain expansions, with the potential of providing additional system redundancies to the overall Conservancy development area from south of the Jock River, will be further discussed with City staff through the draft plan approval process.

The following table summarizes the relevant Water Supply Design Criteria which will be employed in the design of the subject property.

**Table 2A: Water Supply Design Criteria**

Design Parameter	Value
<b><i>Extracted from Section 4: Ottawa Design Guidelines, Water Distribution (July 2010)</i></b>	
Residential – Detached Single	3.4 p/unit
Residential – Townhome/ Semi	2.7 p/unit
Residential – Apartment	1.8 p/unit
Minimum Watermain Size	150 mm diameter
Minimum Depth of Cover	2.4 m from top of watermain to finished grade
During normal operating conditions desired operating pressure is within	350 kPa and 480kPa
During fire flow operating pressure must not drop below	140 kPa
<b><i>Stantec Hydraulic Analysis, Stantec, July 20, 2017 for Population Exceeding 3000 Persons</i></b>	
Residential – Detached Single	180 L/cap/day
Residential – Rear Lane Town	198 L/cap/day
Residential – Back-to-Back	198 L/cap/day
Outdoor Water Demand	1049 L/unit/day (single detached)
Basic Day	Population x Demand
Max Day	Basic Day + Outdoor Water Demand

### 3.2.1 Fire Flow Demand

Fire Flow requirements are to be confirmed in accordance with Local Guidelines (Fire Underwriters Survey), City of Ottawa Water Supply Guidelines, and the Ontario Building Code, upon development of detailed concepts for the detached single homes, townhouses, and the park. For planning purposes, fire flow estimates are provided in the preliminary water demand estimate (**Appendix B** and the following table) based on the information available in the preliminary concept plan and comparable recent developments in the City of Ottawa.

### 3.2.2 Boundary Conditions

To support the future development of a hydraulic analysis for the subdivision, boundary conditions are expected to be provided by the City of Ottawa for the preliminary water demands.

### 3.2.3 Water Demand Calculations

A summary of water demands for the subject site is presented in the following table as derived from the criteria above and the Stantec Hydraulic Analysis found in **Appendix B**. The draft plan approval process for the Conservancy East area has advanced since the preparation of the March 2021 **Stantec Hydraulic Analysis** and is currently yielding a unit count of ~1,380 units. As well, the proposed unit yield for the current application for Conservancy West is 1,036 units. The demand estimates in the table below from the March 2021 reporting are higher than the newly noted unit counts therefore the prior analysis findings are conservative and still relevant.

**Table 2B: Water Demand Estimate <sup>(1)</sup>**

	Unit Count			Pop	L/c/d	BSDY (MLD)	MXDY (MLD)
	Conservancy East	Conservancy West	Total				
Single Family	730	775	1,505	5,117	180	0.92	2.50
Townhouse	445	525	970	2,619	198	0.52	0.52
Rear-Lane Townhouse	165	-	165	446	198	0.09	0.09
High Density	100	-	100	210	219	0.05	0.05
<b>Total</b>	<b>1,440</b>	<b>1,300</b>	<b>2,740</b>	<b>8,392</b>		<b>1.58</b>	<b>3.16</b>

**Notes:** (1) Water demand details derived from Stantec Hydraulic Analysis. See Appendix D for report details.

### **3.3 Water Supply Conclusion**

The subject lands are have been reviewed by Stantec to confirm that servicing is feasible from the SUC pressure zone. Future watermain extensions from Nepean Town Centre development areas will facilitate servicing to the Conservancy East lands via watermain extension along the future Chapman Mills Drive extension and through the Claridge “Burnett Lands” development area and extended to the Conservancy West development area in future. Future modelling at the detailed design stage will confirm phasing of the extensions of trunk watermains and sizing of the local watermain network. The proposed water supply design will conform to all relevant City and MECP Guidelines and Policies.

## 4.0 WASTEWATER SERVICING

### 4.1 Existing Wastewater Services

Per the **South Nepean Collector (SNC) Wastewater Servicing Study and Functional Design Report** by Dillon in October 2003 (**Dillon SNC Report**), the subject property is tributary to the South Nepean Collector (SNC) sewer as urban development land.

The SNC (previously called the Jock River Collector) sewer operates north of the subject property within Strandherd Drive prior to travelling south down a Chapman Mills Drive (CMD) and then turns eastward within the future CMD right-of-way (ROW).

The **South Nepean Collector Phase 2: Hydraulics Review / Assessment** memo was prepared by Novatech Engineering Consultants on August 20, 2015 (**Novatech SNC Memo**) to provide an update to the sanitary design flows for Phase 2 of the South Nepean Collector, as previously documented in the **South Nepean Collector (SNC) – Functional Design Report and Update** by Dillon in 2012 (**Dillon SNC Report and Update**). In addition, Novatech is also currently the engineer of record for the design and implementation of the Phase 3 extension of the SNC.

### 4.2 South Nepean Collector Phase 3 – Preliminary Design

The 2015 **Novatech SNC Memo** contemplated that the Conservancy Phase 1 development area (north of the Fraser-Clarke Watercourse) would be serviced by the 900 mm diameter SNC sewer running adjacent to the property within the future extension of CMD. This is represented by area “A6-E” within the “**Sanitary Drainage Areas and Land Use – Fig.1**” plan within the 2015 Novatech memo (note that the actual tributary area and population varied slightly).

For the Phase 3 extension of the SNC, Novatech has prepared another review of sanitary flows within their technical memorandum titled “**Strandherd Drive Widening Project, South Nepean Collector Phase 3: Sanitary Flow Calculations**” May 30, 2019 (**2019 Novatech SNC Memo**). The memorandum, along with the design sheet calculations from the Novatech memo, are provided in **Appendix C** for reference along with DSEL annotations on key items in the figure and design sheets. The updated “**Sanitary Drainage Areas and Land Use – Fig.1**” (May 2019) plan is essentially reflective of the same tributary information that was provided in the 2015 study (the plan has been marked up to reflect the Conservancy areas as a frame of reference). The associated design sheet also reflects updated City wastewater design criteria that was not accounted for in the 2015 study and is discussed further in the following section.

Report excerpts are provided in **Appendix C** for the SNC Phase 2 analysis as well as draft information associated with the Phase 3 extension. The location of the SNC sewer is shown in **Figure 4**.

### 4.3 Wastewater Design

The subject property is planned to be serviced by an internal gravity sanitary sewer system that is to generally follow the local road network with select servicing easements as required to achieve efficiencies in servicing and grading designs. The wastewater servicing plan can be seen in **Drawing 4**.

Similar to the proposed Conservancy East development, this report proposes that the drainage area of the SNC sanitary sewer be expanded to include the entirety of the Conservancy property. The sewer network will connect to the off-site SNC sanitary sewer within the future CMD at existing manhole 'SANMH8' as identified in the Novatech SNC Phase 2 design Drawing No. 20 provided in **Appendix C** for reference (City contract number ISD14-2033). As noted in the prior section, the 2015 **Novatech SNC Memo** was derived flows based on the City guideline parameters of the time (namely 350 L/capita/day, infiltration allowance of 0.28 L/s/ha and commercial properties at 50,000 L/ha/d). The following table summarizes the new City design guidelines and criteria to be applied to the **Conservancy East** sewer design as well for the determination of the projected flows to be tributary to the SNC along the frontage of the Conservancy Phase 1 development area.

**Table 3: Wastewater Design Criteria**

Design Parameter	Value
<b>Current Design Guidelines</b>	
Residential - Single Family	3.4 p/unit
Residential – Townhome/ Semi	2.7 p/unit
Residential – Apartment	1.8 p/unit
Average Daily Demand	280 L/d/person
Peaking Factor	Harmon's Peaking Factor. Max 4.0, Min 2.0
Commercial / Institutional Flows	28,000 L/ha/day
Commercial / Institutional Peak Factor	1.5
Infiltration and Inflow Allowance	0.33 L/s/ha
Park Flows	28,000 L/ha/d
Park Peaking Factor	1.0
Sanitary sewers are to be sized employing the Manning's Equation	$Q = \frac{1}{n} AR^{2/3} S^{1/2}$
Minimum Sewer Size	200mm diameter
Minimum Manning's 'n'	0.013
Minimum Depth of Cover	2.5m from crown of sewer to grade
Minimum Full Flowing Velocity	0.6m/s
Maximum Full Flowing Velocity	3.0m/s
<i>Extracted from Sections 4 and 6 of the City of Ottawa Sewer Design Guidelines, October 2012, and associated Technical Bulletins.</i>	

The **Conservancy West** development area will contribute approximately 35.7 ha of drainage area (includes lots, ROWs, blocks and parks) to the downstream sewer systems. This is in addition to the ~57.9 ha contributed by the Conservancy East lands.



The sanitary drainage area information is shown in **Figure 4** and the design sheet is enclosed in **Appendix C** for reference.

Applying the City of Ottawa’s wastewater design criteria to the overall development concept, the estimated peak sanitary flow from the subject property is ~48.81 L/s per the provided design sheet. This is in line with the design sheet from the July 2021 *Master Infrastructure Review* (MIR) which demonstrated a flow of 48.93 L/s (provided in **Appendix C** for reference). As noted above, the downstream Conservancy East lands add an additional ~56 L/s of flow. The proposed internal gravity sanitary trunk sewer adequately services the subject property and does not exceed 72% capacity throughout the network.

The proposed peak sanitary flow from the subject property (including Conservancy East and external areas) to the existing SNC sanitary sewer (SANMH 8 in Novatech Drawing No. 20) is ~105 L/s. The addition of the Conservancy Land’s peak flow to the peak design flows from the **2019 Novatech SNC Memo** results in an updated peak flow of 401.05 L/s to the existing SNC sewer installations downstream of existing SANMH 8. With the inclusion of the subject property, the SNC sanitary sewer along the Conservancy Phase 1 frontage would be at approximately 95% capacity and downstream sections (based on SNC as-built information which had a minimum slope of 0.05%) and can adequately handle the entirety of the Conservancy property’s proposed sanitary flows.

When reviewing the projected flows to the SNC, as derived from the *Novatech Phase 2 and Phase 3* SNC data, along with Conservancy Lands design flows, the following is summarized:

**Table 4: South Nepean Collector – Projected Flow Updates**

Report Reference	Projected Flows at Strandherd/CMD intersection (L/s)	Flow at Conservancy Lands Connection Point (L/s)	Difference From Original 2015 SNC Capacity Design (L/s)
2015 Novatech SNC Memo	384.7 <sup>(1)</sup>	423.6	0
2019 Novatech Preliminary Phase 3 Design	282.5 <sup>(2)</sup>	308.6 <sup>(3)</sup>	-115.0
DSEL inclusion of Conservancy Lands (including Ph1) tributary of ~105.99 ha	282.5	401.05 <sup>(4)</sup>	-22.55

- (1) See annotated Novatech design sheet "South Nepean Collector – Phase 2 & 3" (August 2015) in Appendix C and associated "Sanitary Drainage Areas and Land Use" Figure 1 dated August 2015.
- (2) See annotated Novatech design sheet "South Nepean Collection Phase 3" (September 2019) in Appendix C and associated "Sanitary Drainage Areas and Land Use" Figure 1 dated May 2019
- (3) Incorporating the new Phase 3 flows into the 2015 Novatech analysis
- (4) See DSEL sanitary flow spreadsheet review of Novatech's SNC Phase 2 & 3 design sheet data in Appendix C.

The above table demonstrates that with the updates to the SNC design parameters and incorporation of the Conservancy Lands sanitary flows there is a net reduction of 22.55 L/s (from the original design) to the SNC sewer at this location. As such, this translates into no negative impacts to the SNC sewer network downstream of the connection point into the system.

#### **4.4 Wastewater Servicing Conclusion**

The subject property will be serviced by local sanitary sewers, an on-site trunk sanitary sewer, and the off-site SNC sanitary sewer as defined in previous reports. This AES proposes the expansion of the drainage areas from the **2019 Novatech SNC Memo** to include the entirety of the subject property. There is residual capacity in the downstream SNC providing sufficient capacity for the peak sanitary flows for the subject property, including external commercial and community park flows.

## 5.0 STORMWATER CONVEYANCE

### 5.1 Existing Stormwater Drainage

The subject property is within the Jock River watershed. Per the existing topography characterized in available City of Ottawa base mapping, as well as site specific survey, all flows from the subject property are ultimately conveyed to the Jock River by a series of watercourses, sheet flow and minor ditches. The Foster Ditch and the O'Keefe Municipal Drain are the main stormwater conveyances within the Conservancy West property that convey stormwater to the Jock River.

### 5.2 Proposed Stormwater Management Strategy

Various stormwater strategies were discussed within the Master Infrastructure Review (MIR) prepared previously. Alternatives reviewed were:

**Alternative 1 – Oil and Grit Separators & Treatment Train to Naturalized Wetlands\***

Alternative 2 – Stormwater Management Wetland Facilities in the Floodplain

Alternative 3 – Stormwater Management Wetland Facilities out of the Floodplain

Alternative 4 – Modified Etobicoke filtration System (MEFS)

For the purposes of this AES Alternative 1 is being advanced as per the evaluation provided in the MIR and per discussions with the City of Ottawa on July 20, 2021. This alternative:

- Provides for the most efficient use of land that would otherwise be occupied by multiple stormwater management ponds (i.e. potentially four ponds, with up to ten forebays based on prior analysis, as well as sediment management areas) for water quality control. The alternative also mitigates against site constraints imposed due to the proximity of the development to the Jock River, and grade raise restrictions along with relatively flat topography;
- Proposes OGS units as part of a treatment train approach that, overall, will provide the required Enhanced Level of Protection (80% total suspended solids (TSS) removal) and have outlets that are above the 2-year event summer water levels on the Jock River;
- As part of a treatment train approach, deep sump catchbasins equipped with catchbasin inserts such the CB Shield™ (certified with third party testing (i.e ETV verified)) to further reduce catchbasin sump sediment re-suspension and optimize TSS removal;
- Proposal is to also incorporate an infiltration-type LID within the right-of-way extending out from catchbasin locations (see **Figure 5 in Figures & Drawings**). The detailed design process, when detailed grading is available, will define suitable locations in order to yield optimal benefit from this LID. See Section 5.7 for additional LID discussion;

- Has an added benefit of providing hydration with treated stormwater to naturalized channels in the natural heritage corridor connecting to the Jock River, and;
- Has straightforward system maintenance requirements via mobile vacuum trucks that are more readily achieved as part of the City's typical maintenance programs as opposed to the additional efforts required to maintain wet pond forebays (heavy equipment for sediment removal and relocation).

The design for the site proposes to have stormwater flows conveyed through the development area of the subject property via an underground sewer network. The stormwater runoff will be treated before ultimately being released into the natural heritage features and the Jock River as per the ***Jock River Reach One Subwatershed Study*** prepared by Stantec in 2007 (***Jock River SWS***).

The proposed stormwater design layout is shown on ***Drawing 3*** with the stormwater management design consisting of:

- A storm sewer system designed to capture at least the minimum design capture events in accordance with the amendment to the storm sewer and stormwater management elements of the Ottawa Design Guidelines – Sewer (Technical Bulletin PIEDTB-2016-01);
- Multiple oil and grit separators (OGS) designed to assist with achieving the required Enhanced Level of Protection per MECP guidelines, along with additional treatment train elements, via treatment of the stormwater captured by the storm sewer network;
- The storm systems will discharge the treated stormwater at multiple outlets located along the natural heritage corridor, connecting via naturalized channels outletting to the Jock River. Discharge locations are demonstrated in ***Drawing 3***;
- Inverts of storm outlets are set at the 2-year summer water levels of the Jock River;
- An on-site road network designed to maximize the available storage within right-of-ways for the 100-year design event, where possible, with controlled release of stormwater to the minor storm system; and
- An overland flow route designed to safely convey stormwater runoff flows in excess of the on-site road storage.

Although quantity control has not typically been required for this reach of the Jock River, as per the ***Jock River SWS***, the quantity of stormwater runoff exiting from the subject property will be minimized by optimizing on-site storage in the sags of the proposed road network, which in turn minimizes the size of downstream storm sewer infrastructure. It is noted that the RVCA is currently reviewing the SWM requirements within the Jock River Reach 1 area. In consideration of this, J.F. Sabourin and

Associates (JFSA) has undertaken a review of the existing quantity control recommendations and the existing, and proposed, development conditions for this area. The findings are presented in the JFSA memorandum *Review of Quantity Control Requirement for Jock River Reach 1 (March 2021)* provided in **Appendix D** which concludes that quantity controls will still not be required for this reach of the Jock River.

### 5.2.1 Post-Development Stormwater Management Targets

Stormwater management requirements for the proposed alternative Stormwater management scheme have been adopted from the **Jock River SWS, City Standards**, and the **MECP SWMP Manual**.

Given the general criteria mentioned above, the following specific standards are anticipated for stormwater management within the subject property:

- Enhanced quality treatment will be provided for stormwater runoff from the subject property, corresponding to a long-term average TSS removal efficiency of 80%, as defined by the MECP prescribed treatment levels;
- Downstream receiving watercourses will be assessed for responses to planned stormwater management outflows, and stabilization mitigation measures will be planned as required;
- Storm sewers on local roads are to be designed to provide at least a 2-year level of service without any ponding per the City's latest Technical Bulletin PIEDTB-2016-01;
- Storm sewers on collector roads are to be designed to provide at least a 5-year level of service without any ponding per the City's latest Technical Bulletin PIEDTB-2016-01;
- For less frequent storms (i.e. larger than 2-year or 5-year), the minor system sewer capture will be restricted with the use of inlet control devices to prevent excessive hydraulic surcharges;
- Under full flow conditions, the allowable velocity in storm sewers is to be no less than 0.80 m/s and no greater than 6.0 m/s;
- For the 100-year storm and for all roads, the maximum depth of water (static and/or dynamic) on streets, rear yards, public space and parking areas shall not exceed 0.35 m at the gutter;
- The major system shall be designed with sufficient capacity to allow the excess runoff of a 100-year storm to be conveyed within the public ROW, or adjacent to the ROW, provided the water level does not touch any part of the building envelope; must remain below all building openings during the stress test event

- (100-year + 20%); and must maintain 15 cm vertical clearance between spill elevation on the street and the ground elevation at the nearest building envelope;
- Flow across road intersections shall not be permitted for minor storms (generally 5-year or less);
  - When catchbasins are installed in rear yards, safe overland flow routes are to be provided to allow the release of excess flows from such areas. A minimum of 30 cm of vertical clearance is required between the rear yard spill elevation and the ground elevation at the adjacent building envelope; and
  - The product of the maximum flow depths on streets and maximum flow velocity must be less than 0.60 m<sup>2</sup>/s on all roads.

### 5.2.2 Quality Control

Per the **Jock River SWS**, Enhanced quality treatment will be provided for stormwater runoff from the subject property, corresponding to a long-term average TSS removal efficiency of 80%, as described by the MECP prescribed treatment levels. See Section 5.3 for quality control approach and discussion.

### 5.2.3 Quantity Control

As noted in the **Jock River SWS**, quantity control is not anticipated to be required for outlets to the Jock River, however, some quantity control may be provided by erosion storage, as erosion thresholds for any watercourses/outlets will be respected where required. As noted in Section 5.2, JFSA has reviewed the current/future development conditions contributing to this reach of the Jock River and concludes that quantity control will still not be required. See “*Review of Quantity Control Requirement for Jock River Reach 1 (JFSA March 2021)*” provided in **Appendix D**.

## 5.3 Stormwater Management Design

As shown on **Drawing 3**, there will be multiple OGS units at various locations along the southern boundary of the property, discharging to the Jock River via naturalized channels. By way of an MECP Certificate of Technology Assessment and manufacturer’s design report, the OGS units will demonstrate compliance with Enhanced Level of Protection requirements, with specific drainage area parameters for each area.

The manufacturer’s reported efficiency of TSS removal of the OGS units is expected to be based on a ‘fine distribution’ particle size distribution in conformance with the following table, unless otherwise approved by the City of Ottawa, RVCA, and MECP. The particle size distribution is the generic particle size distribution accepted by the City of Toronto per the *Wet Weather Flow Management Guidelines* (City of Toronto, 2006) as a typical average stormwater particle size distribution, and is an excerpt from Table

3.3 of the *Stormwater Management Practices Planning and Design Manual* (MOECC, 1994).

**Table 5: Typical Stormwater Particle Size Distribution & Settling Velocities  
(Source: *Stormwater Management Practices Planning and Design Manual*,  
MOECC, 1994)**

Particle Size (microns) (NURP 1983)	% of Particle Mass	Average Settling Velocities (m/s)
< 20	0 - 20	0.00000254
20 - 40	20 - 30	0.00001300
40 - 60	30 - 40	0.00002540
60 - 130	40 - 60	0.00012700
130 - 400	60 - 80	0.00059267
400 - 4000	80 - 100	0.00550333

To allow for flexibility as detailed design advances, it is proposed that any OGS unit can be selected, given that it:

- Meets the requirements set out in the preceding sections;
- Ensures no significant negative impact on the upstream storm sewer system – to be determined via hydraulic modelling at detailed design; and
- Demonstrates suitability for meeting Enhanced water quality targets via a MECP Certificate of Technology Assessment.

The preliminary OGS units proposed in the following table have been sized to treat the stormwater runoff for the tributary areas noted in order to meet MECP Enhanced Level of Protection criteria as part of a treatment train approach prior to discharge to the Jock River via naturalized channels as shown on ***Drawing 3***. The OGS total suspended removal rates and preliminary OGS unit details have been attached for reference in ***Appendix D***.

**Table 6: OGS Unit ID and Design Characteristics**

Area and Unit ID <sup>(1)(2)</sup>	Drainage Area Target (ha)	Estimated Weighted C Value	Unit Treatment Capacity (L/s)	Unit Model <sup>(1)</sup>
Area 1 – OGS W1	8.92	0.65	255	CDS Model 5640-10
Area 2 – OGS W2	8.22	0.65	212	CDS Model 4045-8
Area 3 – OGS W3	9.90	0.65	255	CDS Model 5640-10
Area 4 – OGS W4	8.60	0.65	255	CDS Model 5640-10
(1) Providing at minimum 80% TSS removal (until such time that criteria for the MECP’s Consolidated Linear Infrastructure approach is in force at which time only 50% is attributed to OGS units). (2) See <b>Drawing 3</b> for OGS unit locations. The “W” prefix in the numbering indicates ‘West’ development area.				

The above preliminary OGS unit sizing will achieve required quality controls and, along with other treatment train elements, will have additional beneficial TSS mitigation.

### 5.3.1 Groundwater

Paterson Group has reviewed the anticipated long term groundwater condition for the development area. Paterson drawing PG5036-10B in **Appendix D** demonstrates the long term groundwater elevation across the Conservancy West development area. The elevations range from ~88.5 m in the southern areas up to ~90 m in the northern areas. The lowest storm outlet at the southern boundary is 89.35 m (OGS W1) and all storm sewers, and any infiltration-type LIDs proposed within the development area, are above the anticipated long term groundwater elevation. Profiles for the storm sewers can be seen in **Drawing 5**.

### 5.4 Proposed Minor System

The subject property will be serviced by an internal gravity storm sewer system that is to generally follow the local road network and proposed servicing easements as required. The drainage will be conveyed within the underground piped sewer system to headwall outlets located along the natural heritage corridor, providing hydration to naturalized outlet channels.

Street catchbasins will collect drainage from the streets and front yards, while rear yard catchbasins will capture drainage from backyards. Perforated catch basin leads will be provided in rear yards, except the last segment where they connect to the right-of-way which will be solid pipe, per City standards.

The preliminary rational method design of the minor system captures drainage for storm events up to and including the 2-year (local) and 5-year (collector) event assuming the



use of inlet control devices (ICD) for all catchbasins within the subject property. The following table summarizes the standards that will be employed in the detailed design of the storm sewer network. The preliminary drainage area information can be found in **Drawing 3** and rational method design sheets are provided in **Appendix D**.

**Table 7: Storm Sewer Design Criteria**

Design Parameter	Value
Minor System Design Return Period	1:2 year (PIEDTB-2016-01) for local roads, without ponding 1:5 year (PIEDTB-2016-01) for collector roads, without ponding 1:100 year (PIEDTB-2016-01) for arterial road, without ponding
Major System Design Return Period	1:100 year
Intensity Duration Frequency Curve (IDF) 2-year storm event: A=732.951   B=6.199   C=0.810 5-year storm event: A = 998.071   B = 6.053   C = 0.814	$i = \frac{A}{(t_c + B)^C}$
Minimum Time of Concentration	10 minutes
Rational Method	$Q = CiA$
Storm sewers are to be sized employing the Manning's Equation	$Q = \frac{1}{n} AR^{2/3} S^{1/2}$
Runoff coefficient for paved and roof areas	0.9
Runoff coefficient for landscaped areas	0.2
Minimum Sewer Size	250 mm diameter
Minimum Manning's 'n' for pipe flow	0.013
Minimum Depth of Cover	1.5 m from crown of sewer to grade
Minimum Full Flowing Velocity	0.8 m/s
Maximum Full Flowing Velocity	6.0 m/s
Clearance from 100-Year Hydraulic Grade Line to Building Opening	0.30 m
Design Parameter	Value
Max. Allowable Flow Depth on Municipal Roads	35 cm above gutter (PIEDTB-2016-01)
Extent of Major System	To be contained within the municipal ROW or adjacent to the ROW provided that the water level must not touch any part of the building envelope and must remain below the lowest building opening during the stress test event (100-year + 20%) and 15cm vertical clearance is maintained between spill elevation on the street and the ground elevation at the nearest building envelope (PIEDTB-2016-01)

Stormwater Management Model	DDSWMM (release 2.1), SWMHYMO (v. 5.02) and XPSWMM (v. 10)
Model Parameters	Fo = 76.2 mm/hr, Fc = 13.2 mm/hr, DCAY = 4.14/hr, D.Stor.Imp. = 1.57 mm, D.Stor.Per. = 4.67 mm
Imperviousness	Based on runoff coefficient (C) where Percent Imperviousness = $(C - 0.2) / 0.7 \times 100\%$ .
Design Storms	Chicago 3-hour Design Storms and 24-hour SCS Type II Design Storms. Maximum intensity averaged over 10 minutes.
Historical Events	July 1st, 1979, August 4th, 1988 and August 8th, 1996
Climate Change Street Test	20% increase in the 100-year, 3-hour Chicago storm
<i>Extracted from City of Ottawa Sewer Design Guidelines, October 2012, and ISSU, and based on recent residential subdivisions in City of Ottawa.</i>	

The peak design flows are calculated based on an average predicted runoff coefficient (C-value) of 0.65 for the development area in keeping with the MIR and will require updating, 0.40 for park areas and 0.25 for grassed areas. As detailed design progresses, the runoff coefficients will be refined to reflect the proposed building envelopes, driveways and other details.

There are several trunk sewers proposed and the peak flows are described for the trunk sewers which correspond to the stormwater management design areas as summarized in the following table:

**Table 8: Minor System Trunk Sewer Outlets**

Area/Outlet # (from east to west)	Trunk Sewer Outlet Headwall	Peak Flow (L/s)
1 (HW1)	1050 mm diameter @ 0.19%	938
2 (HW2)	975 mm diameter @ 0.20%	744
3 (HW3)	1050 mm diameter @ 0.15%	823
4 (HW4)	825 mm diameter @ 0.55%	823
Note: See rational design sheet in Appendix D for details.		

The storm sewers tributary to the various outlets, and associated peak flows, are detailed in the rational method design sheet, enclosed in **Appendix D**.

The conceptual servicing layout is shown on **Drawing 2** in **Drawings**. As detailed design progresses, alignment and sizing of local storm sewers will be confirmed and additional servicing easements may be required, potentially triggering minor

amendments to the proposed lot fabric in the concept plan. The preliminary sanitary and storm trunk plan and profiles are shown on **Drawing 5 and 6** in **Drawings**.

#### 5.4.1 Hydraulic Grade Line Analysis

A preliminary hydraulic grade line (HGL) modelling analysis has been completed by JFSA to demonstrate that the HGL will be maintained below the ground surface. See the JFSA memo entitled *BCDC Phase 3 – Preliminary HGL Analysis (October 2021)* in **Appendix D** for details/results. The analysis has been evaluated for various scenarios for the Jock River in order to assess the appropriate HGL boundary condition:

- 5-year water level in Jock River + 100yr rain event; or
- 100-year water level in Jock River + 5yr rain event (deemed to be the critical event).

The HGL results in JFSA's Table 1 (**Appendix D**) demonstrate that the freeboard to the ground surface ranges from 0.07 m to 1.08 m (with an average of 0.62 m) for the critical event noted above.

An updated HGL analysis will be completed for the proposed system at the detailed design stage, based on the above noted events, including historical design storms and climate change stress test as required. Detailed grading design and storm sewer design will be modified as required to achieve the freeboard requirements set out per PIEDTB-2016-01.

#### 5.5 Proposed Major System

Major system conveyance, or overland flow, will be provided to accommodate flows in excess of the minor system capacity. Overland flow is accommodated by generally storing stormwater up to the 100-year design event in road sags then routing additional surface flow along the road network and service easements towards the proposed stormwater outlets, discharging to the Jock River through the natural heritage corridors, as shown on **Drawing 1**. The grading design includes a saw-toothed-road design with 0.10% minimum grade from high point to high point in order to maximize available surface storage for management of flows up to the 100-year design event where possible.

#### 5.6 Foundation Drainage (Sump Pumps)

Due to the grade raise restrictions and the proposed storm and sanitary drainage schemes, the road centerlines do not allow for standard basements with a gravity connection to the storm sewer system. As such, because of the constraints on the subject property, sump pumps are proposed to be installed for all residential blocks and residential lots.

The City of Ottawa issued Technical Bulletin *ISTB-2018-04* and *2019-02* for the amendment of the *Ottawa Design Guidelines – Sewer, Second Edition*, October 2012 with respect to the screening criteria for the use of sump pump systems for foundation drainage in Greenfield developments on sites with clay soils. Similar to the development of Conservancy Phase 1 and the Conservancy East (Phase 2) site, **Conservancy West** has also been assessed as meeting the required criteria for the use of sump pumps.

One of the screening criterion is with respect to the hydraulic grade line (HGL) for the development wherein the system should be reviewed to demonstrate that the HGL cannot reasonably be lowered any further due to outlet restrictions. The site grading is constrained by the close proximity of the Jock River, which is the receiver of stormwater outflows, and is also constrained by grade raise restrictions for the property.

For the Barrhaven **Conservancy West** Lands the grade raise restriction varies between 1.2 m and 1.8 m. Paterson's permissible grade raise plan is contained in **Appendix E** for reference (See Section 6 for discussion). Further investigations on the property and potential surcharging or lightweight fill (LWF) underneath garages could increase the permissible grade raise and will be investigated further as part of the detailed design.

The functional grading plan for the subdivision has been prepared with the grade raise restrictions in mind with grades being kept as low as possible.

The proposed centerline of road grades, and subsequently the house grades, do not allow for standard basements with a gravity connection to the storm sewer system. As such, the subdivision will be serviced entirely by sump pumps due to site constraints imposed by grade raise restrictions, HGL elevations and the proximity to the Jock River stormwater outlet.

## 5.7 Low Impact Development (LID) - Infiltration

The following general Low Impact Development (LID) techniques could be considered for implementation, where possible, as part of detailed design (noting that they have to be weighed against the objectives of the City's sump pump technical bulletins):

- Rear-yard swales should be designed with minimum grades where possible, to promote infiltration;
- Rear-yard catchbasin leads should be perforated (except for the last segment connecting to the storm sewer within the ROW), to promote infiltration; and,
- Where eavestroughs are provided on residential units, they are to be directed to landscaped surfaces, to promote infiltration.
- Furthermore, the following techniques can be examined as part of detailed landscaping design of the park block; and,
- Micro-grading can be considered to promote infiltration.

Generally, the development area is not as strong a candidate for LID techniques beyond those proposed above due to the existing clay soils and high groundwater levels. The long term groundwater anticipated is demonstrated on Paterson Drawing *PG5036-10B* in **Appendix D** as previously noted. The infiltration measure noted in Section 5.2 will contribute some infiltration and quality benefits as first flush stormwater is conveyed into the filtration trench. The amount of infiltration is dependent upon the surrounding soils, but the proposed design will optimize the potential on the site. JFSA has completed a high level water budget review of the site which is provided in **Appendix D** for reference.

To assess the water budget for the site under both pre- and post-development conditions, a SWMHYMO model was developed. This model was run using 36 years of hourly rainfall data from the Ottawa International Airport from 1967 to 2003 (excluding missing 2001 rainfall data), the average annual runoff volumes from the subject site were computed and compared. The conceptual LIDs have been included in the model through the use of ROUTE RESERVOIR commands, which represent the storage volume and infiltration rates of each of these proposed LID features. After running each of the models for the 36 years, the annual runoff and infiltration results were extracted and the annual average water budget for each scenario calculated. Full summary tables for each year and scenario have been provided in Table A1 in **Appendix D**.

The analysis concludes that with the proposed LID the existing annual water infiltration volume can be met and exceeded. The extents of the LID system can be refined at detailed design to optimize LID locations and to minimize the extent of infrastructure to be maintained.

### **5.7.1 Water Quality Benefits**

In terms of quality benefits, if it is required that the LID were to achieve a TSS removal of 60% (for the overall treatment train to achieve the 80% TSS removal), the Table 3.2 of the MOECC (now MECP) publication entitled "*Stormwater Management Planning and Design Manual, March 2003*" sets the storage volume requirements for infiltration measures to achieve certain TSS removal rates as follows:

Table 3.2 Water Quality Storage Requirements based on Receiving Waters<sup>1, 2</sup>

Protection Level	SWMP Type	Storage Volume (m <sup>3</sup> /ha) for Impervious Level			
		35%	55%	70%	85%
Enhanced 80% long-term S.S. removal	Infiltration	25	30	35	40
	Wetlands	80	105	120	140
	Hybrid Wet Pond/Wetland	110	150	175	195
	Wet Pond	140	190	225	250
Normal 70% long-term S.S. removal	Infiltration	20	20	25	30
	Wetlands	60	70	80	90
	Hybrid Wet Pond/Wetland	75	90	105	120
	Wet Pond	90	110	130	150
Basic X 60% long-term S.S. removal	Infiltration	20	20	20	20
	Wetlands	60	60	60	60
	Hybrid Wet Pond/Wetland	60	70	75	80
	Wet Pond	60	75	85	95
	Dry Pond (Continuous Flow)	90	150	200	240

<sup>1</sup>Table 3.2 does not include every available SWMP type. Any SWMP type that can be demonstrated to the approval agencies to meet the required long-term suspended solids removal for the selected protection levels under the conditions of the site is acceptable for water quality objectives. The sizing for these SWMP types is to be determined based on performance results that have been peer-reviewed. The designer and those who review the design should be fully aware of the assumptions and sampling methodologies used in formulating performance predictions and their implications for the design.

<sup>2</sup>Hybrid Wet Pond/Wetland systems have 50-60% of their permanent pool volume in deeper portions of the facility (e.g., forebay, wet pond).

The required storage volume of 20 m<sup>3</sup>/ha for the site is not dependent upon the average imperviousness anticipated for the site based on the above table. The site area for Conservancy West (not including parks) is ~32.1 ha. This equates to a storage volume requirement of ~640 m<sup>3</sup> to achieve the required 60% TSS removal.

With the infiltration LID concept at catchbasins (see Figure 5) a configuration of 15m long, 250mm diameter perforated storage pipes off each side of catchbasin locations with a clear stone surround will provide the required storage for the development area.

This is estimated based on the following rationale:

- (i) The proposed draft plan has approximately 7,200 lineal meters of roadway;
- (ii) Assuming a set of catchbasins approximately every 80m = 7,200/80 = ~90 sets of catchbasins;
- (iii) Each set of catchbasins equates to 2 CBs x 30m (perforated 250mm pipe at each CB) x 0.05 m<sup>3</sup>/m = 3.0m<sup>3</sup> per set of catchbasins;
- (iv) Total volume is approximately 90 CB sets x 3.0m<sup>3</sup>/set = ~270 m<sup>3</sup> of provided storage in pipes;
- (v) Storage in the granular trench is based on a 1.25m x 0.4m clear stone trench (void ratio of 0.4). Accounting for the exclusion of the pipe this equates to [(1.25x0.4)-(0.05)] x (90x2x30) x 0.4 = ~970 m<sup>3</sup>
- (vi) Provided storage of ~1,240m<sup>3</sup> > required storage of 640m<sup>3</sup>. At detailed design the system will be fine-tuned to optimize the extent of infrastructure to be installed to meet the required storage targets.

## 5.8 Existing Watercourses

### 5.8.1 Foster Ditch

The Foster Ditch borders the eastern boundary of the **Conservancy West** development area. It originates south of Fallowfield Road, west of Cedarview Road and flows south until it converges with the Jock River south of McKenna Casey Drive. The ditch is approximately 3,200 m long and has been artificially straightened. This non-municipal drain is a fish bearing tributary of the Jock River with approximately 335 ha of catchment area. The surrounding land use is urban and vacant lands. Riparian vegetation is very sparse consisting of mostly grasses with a few shrubs.

As noted in the **Jock River SWS**, to ensure protection of the aquatic habitat north of the Jock River, a development setback should be provided for all of the tributaries. Further studies will determine the development setback, which will be the greater of: 1) regulatory floodplain; 2) meander belt width; and 3) aquatic setback, whichever is greater.

### 5.8.2 O'Keefe Municipal Drain

The O'Keefe Drain is located east of and runs parallel to Highway 416. The drain extends from south of Fallowfield Road and enters the Jock River south of McKenna Casey Drive. The drain is approximately 3,100 m in length and has been artificially straightened through development areas to the north and to follow the depression between agricultural lands through the subject property. The predominant land use is agricultural. The riparian vegetation consists mainly of grasses and some shrubs with thicker forested patches as the reach approaches the Jock River.

As a component of this development application, a process has been initiated with the City's Municipal Drain Group wherein the O'Keefe Drain is proposed to be realigned around the western perimeter of the subject lands so it does not bisect the development area. A staff report recommending the appointment of Robinson Consultants as the engineer of record for the proposed alteration under Section 78 of the *Drainage Act* was carried by the Agriculture and Rural Affairs Committee (ARAC) on June 3, 2021 and subsequently carried by Council on June 9, 2021 (see recommendation in **Appendix D** for reference).

The proposed realignment will see the drain directed westward immediately south of McKenna Casey Drive, then southward along the site boundary to a new outlet connection point to the Jock River. A preliminary meeting has taken place with Robinson Consultants on June 29, 2021 to review the proposal and consultation with the RVCA has taken place on September 22, 2021 as the design work progresses. Once approval of the realignment is advanced there will be an associated application to the RVCA to remove the floodplain designation that exists over the current drain alignment.

## 5.9 Floodplain

On November 8th 2019 the RCVA gave permission to Barrhaven Conservancy Development Corporation to cut and fill on the subject property under permit RV5 44/19 pursuant to review under Section 28 of the Conservation Authorities Act, regulation 174/06. The application and approval by the RVCA was supported by a 2D HEC-RAS model prepared by JFSA. The JFSA model identified the existing and proposed 100-year water levels and permissible extent of fill placement.

The works pursuant to the above-mentioned permit were completed and accepted by the RVCA on May 31st 2020. Options to complete the fill area boundary as set by JFSA included building a structural face of fill (retaining wall) to the limits of the 100-year floodplain boundary, or, building a berm with the toe of slope at the 100-year floodplain boundary. As-builts for the fill placement were subsequently provided and approved by the RVCA, resulting in the May 31st approval noted above and the current 100-year floodplain boundary delineation. The toe of any material placed corresponds to the approved 100-year floodplain line. As noted in the prior report section an application to remove the floodplain from the existing O'Keefe Drain will be a condition of approval associated with that drain realignment.

## 5.10 Stormwater Servicing Conclusions

The stormwater runoff is designed to be captured by an internal gravity sewer system that will convey flows to multiple outlet locations equipped with end of line OGS units. A proposed treatment train arrangement of 1.0 m deep sump catchbasins and a catchbasin insert such as CB Shields™ to optimize catchbasin sump retention of solids, as well as select catchbasin locations with connected infiltration-type subdrains will provide the required quality control treatment to achieve the Enhanced Level of protection. Downstream of the storm outlets along the southern development boundary will be naturalized channels where hydration with treated stormwater will occur in the natural heritage corridor prior to discharge to the Jock River. It is anticipated that quantity control is not required for the Jock River. Notwithstanding, some quantity control by means of erosion storage will be included.

A preliminary Hydraulic Grade Line (HGL) modelling analysis has been completed for the **Conservancy West** development area at this time and demonstrates that the HGL is maintained below the ground surface with freeboards ranging from 0.07 m to 1.08 m for critical event conditions. Further detailed HGL review will be completed for the proposed system at the detailed design stage. Due to the grade raise restrictions, and the proposed storm and sanitary drainage schemes, the road centerlines do not allow for standard basements with a gravity connection to the storm sewer system. As such, because of the constraints on the subject property, sump pumps are proposed to be installed for all residential blocks and residential lots.



The **Conservancy West** development area will be outside of the Jock River's regulatory floodplain area.

Appropriate setbacks from existing watercourse are incorporated into the draft plan based on advancement/finalizing of studies to assess the various determining criteria.

## 6.0 GRADING

A site grading arrangement has been developed to optimize earthworks and provide major system conveyance to the receiving outlets, and naturalized channels, which ultimately outlet to the existing Jock River drainage network. The proposed grading can be found in **Drawing 1** in **Drawings**.

The development area is outside of the Jock River regulatory flood plain limits. The site grading will be a minimum of 0.50m above the 100-year regulatory limit event of the Jock River.

### 6.1 Geotechnical Conditions

Paterson completed a geotechnical investigation for the Conservancy West lands as follows:

- Geotechnical Investigation – Proposed Residential Development, Conservancy Lands West (Paterson Group, October 19, 2021);

The existing ground surface across the site is relatively level with approximate ground surface elevation varying between 91 m and 92 m. The subsurface profile generally consists of an approximate 50 mm to 360 mm thick layer of topsoil underlain by a silty clay deposit.

Due to the presence of a silty clay deposit, permissible grade raise restrictions are recommended for this site. The recommended permissible grade raise varies between 1.2 m in the northwest and 1.8 m. Figure PG5036-5 '*Permissible Grade Raise Plan*' by Paterson is enclosed in **Appendix E** for reference. At the time of detailed design, efforts will be made to mitigate any exceedances and detailed review and signoff by a licensed Geotechnical Engineer will be required. Where grade raises exceed the permissible levels the Engineer will recommend appropriate measures to mitigate where required (i.e. light weight fill or pre-consolidation etc).

The following additional grading criteria and guidelines will be applied to detailed design, per **City of Ottawa Guidelines**:

- Driveway slopes will have a maximum slope of 6%;
- Grading in grassed/landscaped areas to range from 2% to 3:1, with terracing required for slopes larger than 7%;
- Swales are to be 0.15m deep with 3:1 side slopes unless otherwise indicated on the drawings; and,
- Perforated pipe will be required for drainage swales if they are less than 1.5% in slope.

The geotechnical analysis of the site, published under separate cover in support of the development applications, provides additional information about the suitability of the site for the proposed services and grading scheme. At the time of detailed design, detailed review and signoff by a licensed Geotechnical Engineer will be required.

## **7.0 EROSION AND SEDIMENT CONTROL**

Soil erosion occurs naturally and is a function of soil type, climate and topography. The extent of erosion losses is exaggerated during construction where vegetation has been removed and the top layer of soil becomes agitated.

Prior to topsoil stripping, earthworks or underground construction, erosion and sediment controls are implemented and will be maintained throughout any construction phase.

The following specific recommendations to the Contractor will be included in contract documents.

- Limit extent of exposed soils at any given time.
- Re-vegetate exposed areas as soon as possible.
- Minimize the area to be cleared and grubbed.
- Protect exposed slopes with plastic or synthetic mulches.
- Install silt fence to prevent sediment from leaving the site and entering existing watercourses, and clean and maintain throughout construction.
- Install catchbasin inserts during construction to protect from silt entering the storm sewer system.
- Install mud mats in order to prevent mud tracking onto adjacent roadways.
- No refueling or cleaning of equipment near existing watercourses.
- No material stockpiles within 30m of existing watercourses, unless otherwise permitted by RVCA and City of Ottawa.
- Provide sediment traps and basins during dewatering.
- Plan construction at proper time to avoid flooding.
- The Contractor will, at every rainfall, complete inspections to ensure proper performance.
- Erosion and sediment controls will remain in place until the working areas have been stabilized and re-vegetated.

## 8.0 UTILITIES

Utility services extending to the site may require connections to multiple existing infrastructure points: consultation with Enbridge gas, Hydro Ottawa, Rogers, and Bell is required as part of the development process to confirm the servicing plan for the subject lands.

## 9.0 CONCLUSION AND RECOMMENDATIONS

This AES provides details on the planned on-site municipal services for the subject property and demonstrates that adequate municipal infrastructure capacity is expected to be available for the planned development of the subject property.

- The subject lands have been reviewed by Stantec to confirm that servicing is feasible by City of Ottawa PZ SUC. Several alternatives were presented to confirm that servicing is feasible. The water supply network will be expanded through neighboring properties to meet the water demands of the proposed concept plan, via the trunk watermain network and local watermains identified. Detailed modelling will confirm phasing of the extensions of trunk watermains and sizing of the local watermain network.
- Sanitary service is to be provided to the subject property via the off-site South Nepean Collector (SNC) trunk sanitary sewer. With the inclusion of the subject property, the SNC sanitary sewer will have projected flows that are lower than the previous Phase 2 SNC estimated flows (423.6 L/s at Novatech's Area ID A6-E which was based on old City design criteria) but higher than the flows assessed for the current SNC trunk Phase 3 extension of the SNC sanitary trunk (flow of 313.8 L/s at Area ID A6-E). Since Phase 2 was designed with a higher capacity the SNC can adequately handle the entirety of the subject property's proposed sanitary flows.
- Stormwater service is to be provided by capturing stormwater runoff by an internal gravity sewer system that will convey flows to various outlets along the southern boundary to proposed naturalized channels. Prior to discharge from the development, any first flush stormwater will have passed through an end of line OGS unit for quality control. The OGS units will provide an Enhanced Level of Protection quality control treatment for stormwater in combination with an upstream treatment train of measures such as 1.0 m deep catchbasin sumps CB Shield™ inserts and LID system prior to discharge from the development. It is anticipated that quantity control will not be required for discharges to the Jock River.
- A preliminary Hydraulic Grade Line (HGL) modelling analysis has been completed at this time and demonstrates that the HGL is maintained below the

ground surface. Another detailed HGL review will be completed for the proposed system at the detailed design level.

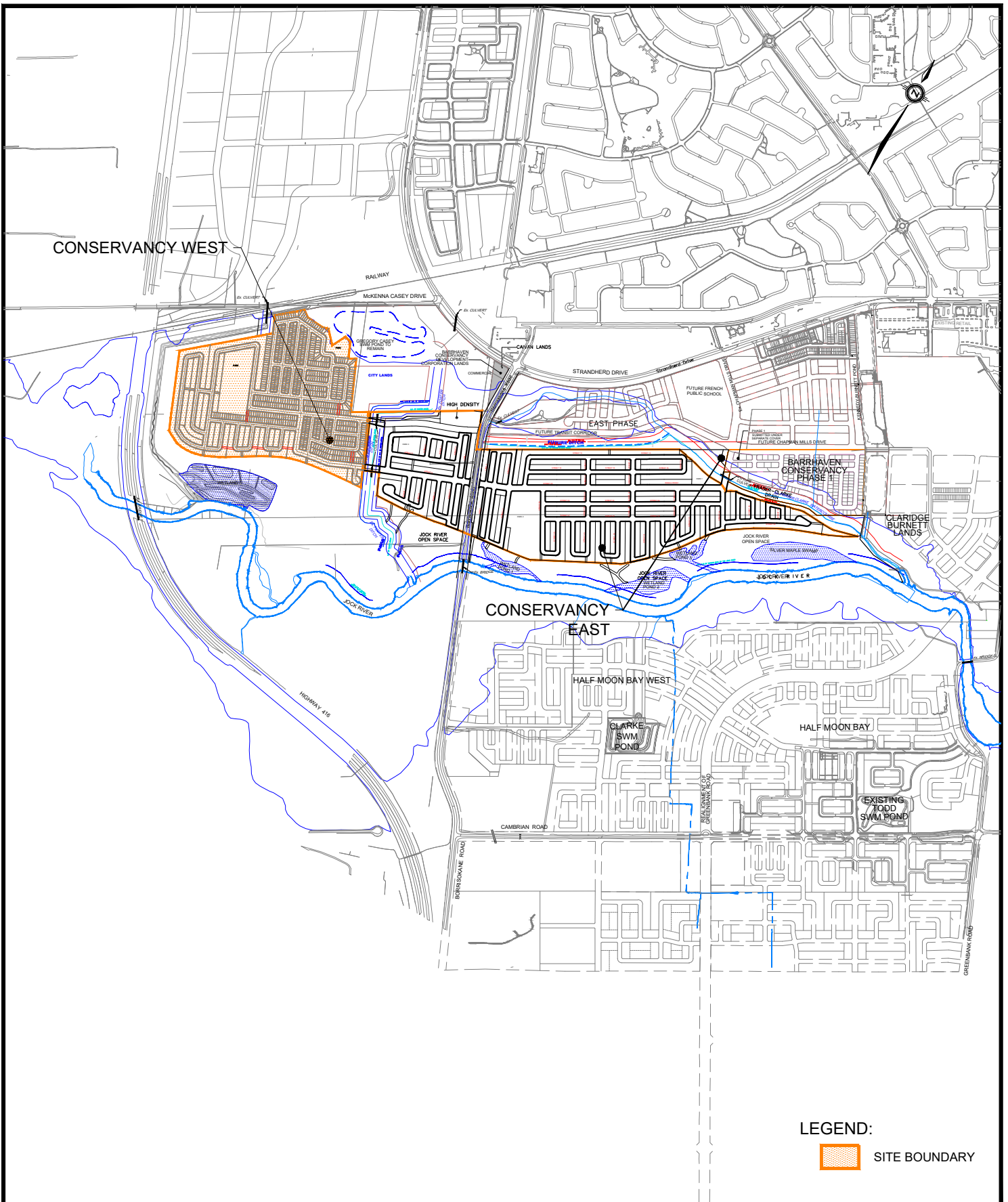
- A preliminary water budget analysis has been completed by JFSA at this time and indicates that pre-development infiltration levels can be met.
- Sump pumps are proposed to be installed for all units within residential blocks and lots;
- The proposed servicing and grading plans are expected to meet all City, RVCA, and MECP requirements as set out in background studies and current standards.
- Prior to detailed design of the infrastructure presented in this report, this AES will require approval under the Planning Act as supporting information for the Plan of Subdivision application. Project-specific approvals are also expected to be required for the infrastructure presented in this report from the City of Ottawa, MECP, and Rideau Valley Conservation Authority, among other agencies.

Prepared by,  
**David Schaeffer Engineering Ltd.**

Per:



## **FIGURES & DRAWINGS**



120 Iber Road, Unit 103  
 Stittsville, ON K2S 1E9  
 TEL: (613) 836-0856  
 FAX: (613) 836-7183  
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## BARRHAVEN CONSERVANCY

# KEY PLAN

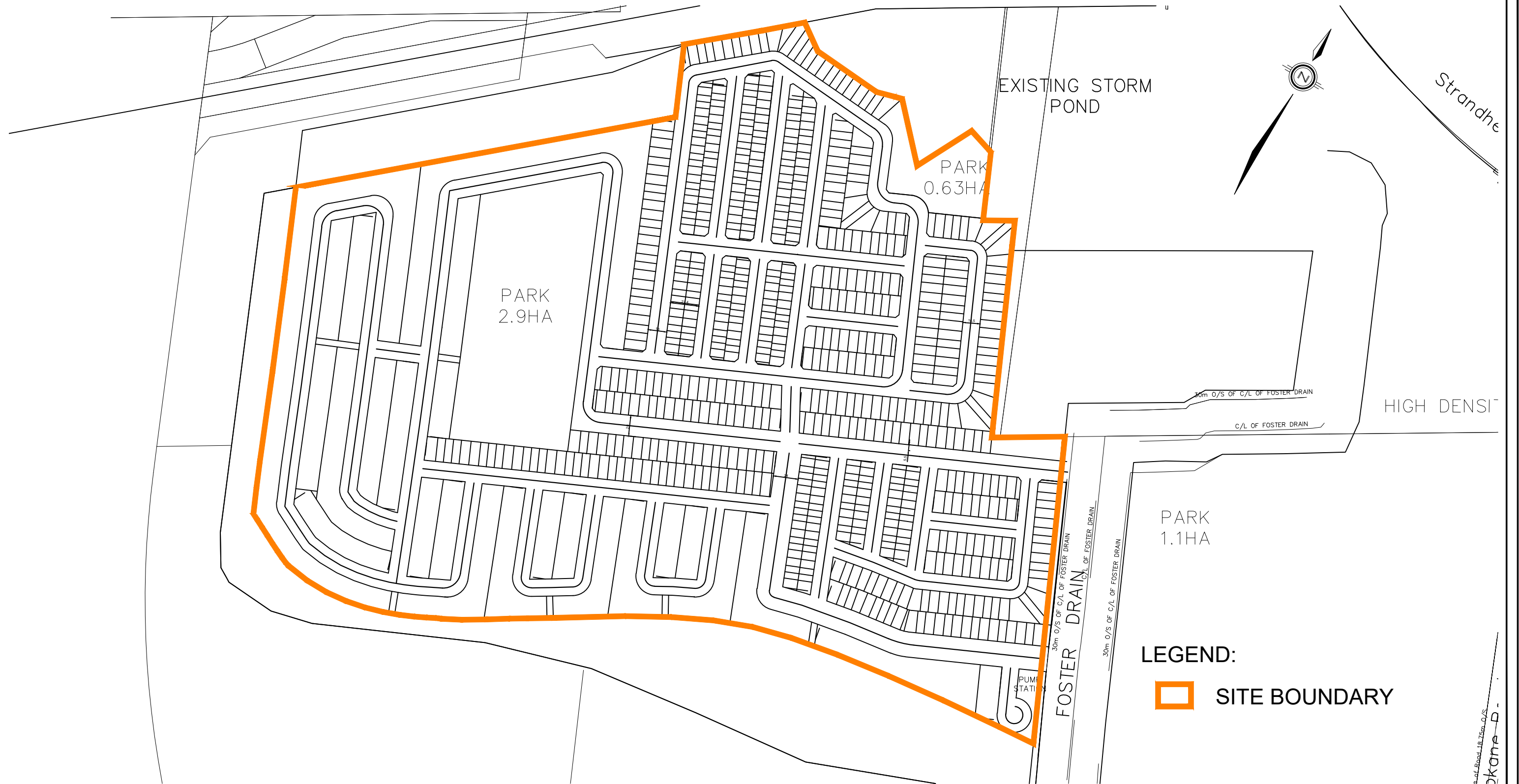
CITY OF OTTAWA


DATE: OCTOBER 2021

SCALE: 1:20000

PROJECT No.: 20-1226

FIGURE: 1



**LEGEND:**  
 **SITE BOUNDARY**



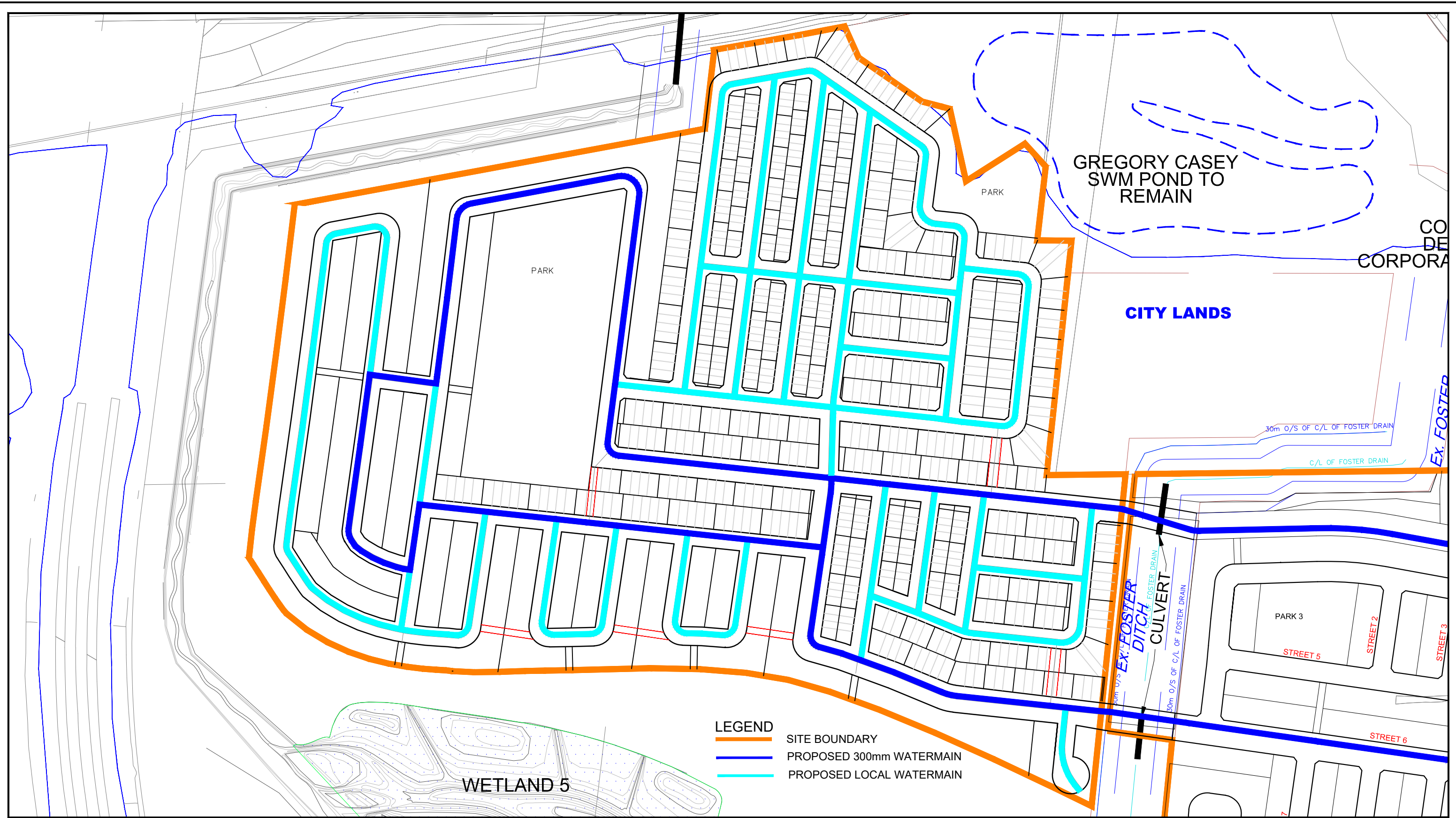
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**BARRHAVEN CONSERVANCY  
 SUBDIVISION PLAN  
 CITY OF OTTAWA**

PROJECT No.:	20-1226
SCALE:	NTS
DATE:	OCTOBER 2021
FIGURE:	2

30m O/S of Road 18.25m O/S  
 Skane-D.





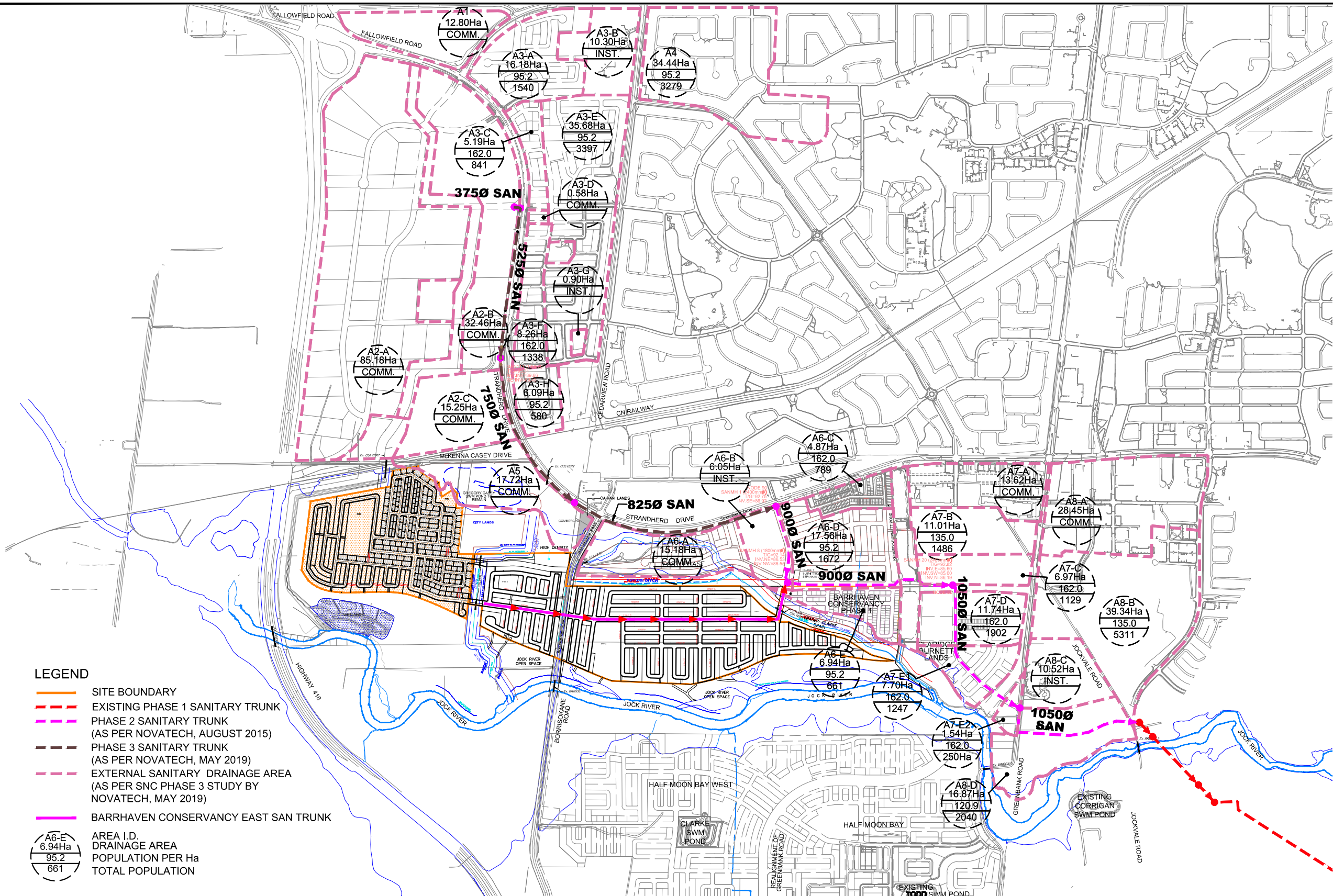
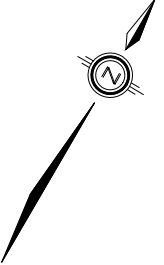
- LEGEND**
- SITE BOUNDARY
  - PROPOSED 300mm WATERMAIN
  - PROPOSED LOCAL WATERMAIN



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**BARRHAVEN CONSERVANCY  
 WATERMAIN SERVICING PLAN  
 CITY OF OTTAWA**

PROJECT No.:	20-1226
SCALE:	1:3000
DATE:	OCTOBER 2021
FIGURE:	3



- LEGEND**
- SITE BOUNDARY
  - - - EXISTING PHASE 1 SANITARY TRUNK
  - - - PHASE 2 SANITARY TRUNK (AS PER NOVATECH, AUGUST 2015)
  - - - PHASE 3 SANITARY TRUNK (AS PER NOVATECH, MAY 2019)
  - - - EXTERNAL SANITARY DRAINAGE AREA (AS PER SNC PHASE 3 STUDY BY NOVATECH, MAY 2019)
  - BARRHAVEN CONSERVANCY EAST SAN TRUNK
- A6-E  
6.94Ha  
95.2  
661 AREA I.D.  
 DRAINAGE AREA  
 POPULATION PER Ha  
 TOTAL POPULATION

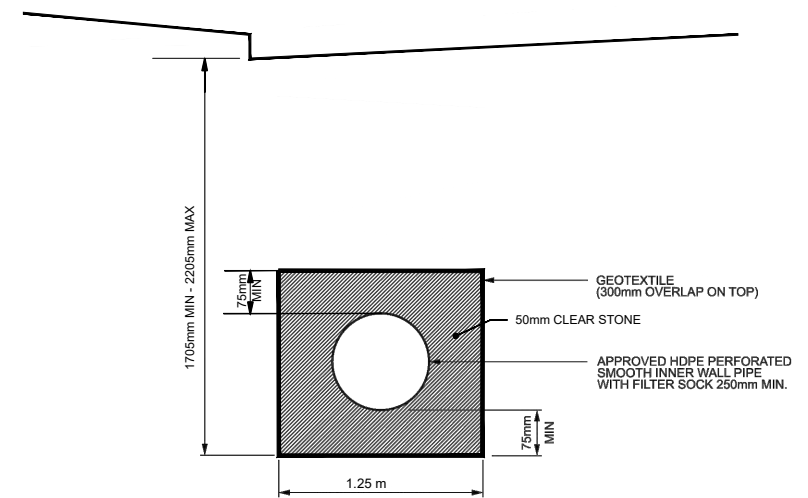
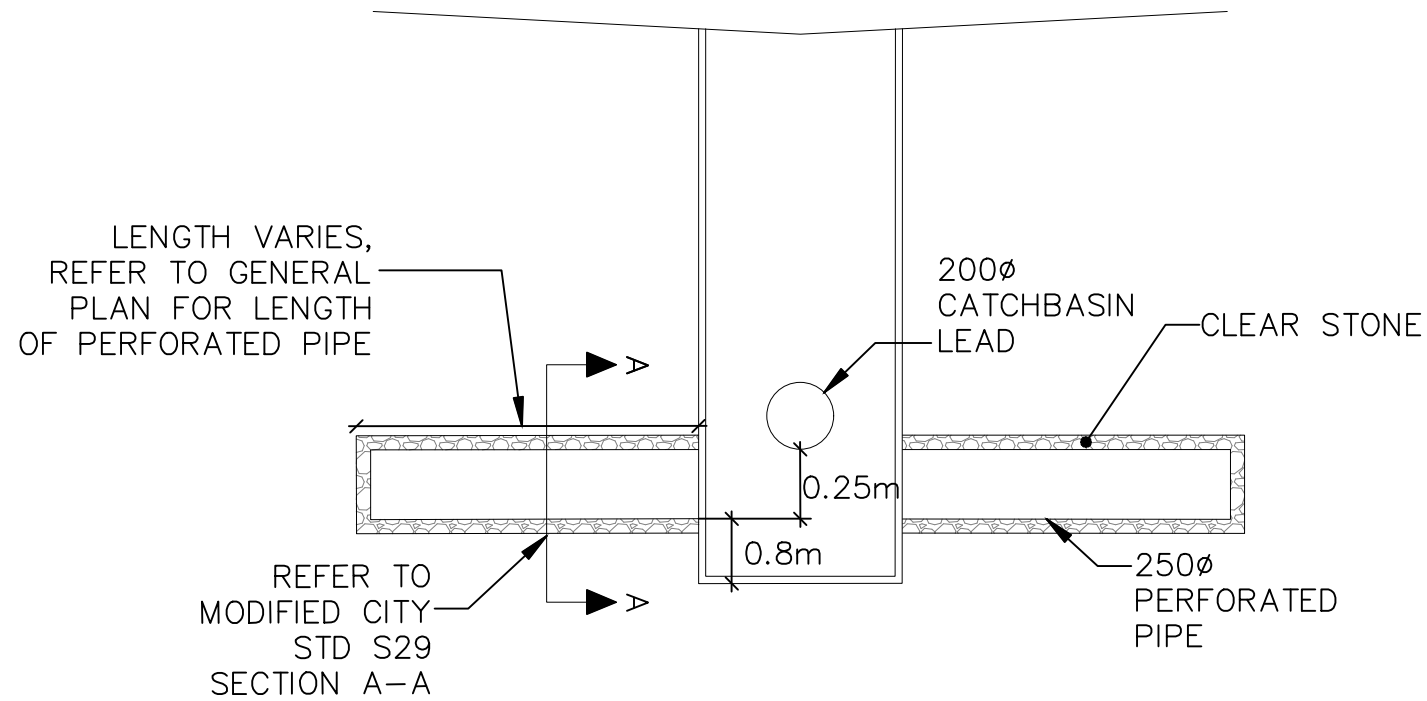


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**BARRHAVEN CONSERVANCY  
 EXTERNAL SANITARY SERVICING  
 CITY OF OTTAWA**

PROJECT No.:	20-1226
SCALE:	1:18000
DATE:	OCTOBER 2021
FIGURE:	4





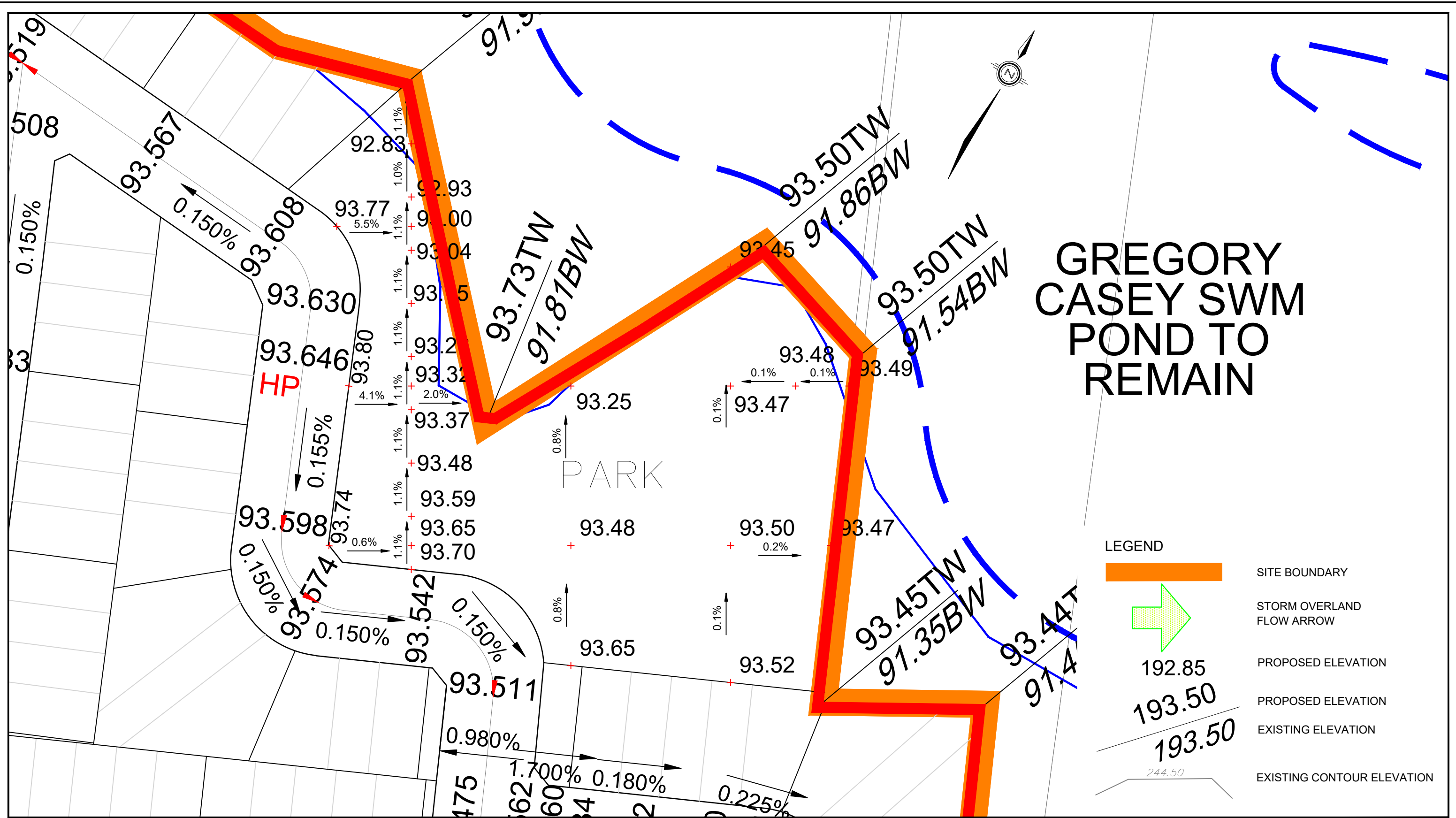
SECTION A-A: MODIFIED CITY STD S29  
SCALE: N.T.S.



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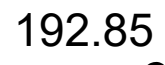
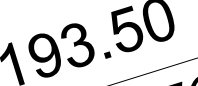
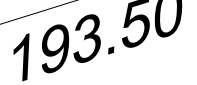

BARRHAVEN CONSERVANCY  
FILTRATION SYSTEM DETAILS  
CITY OF OTTAWA

PROJECT No.:	20-1226
SCALE:	NTS
DATE:	OCTOBER 2021
FIGURE:	5



**GREGORY  
CASEY SWM  
POND TO  
REMAIN**

**LEGEND**

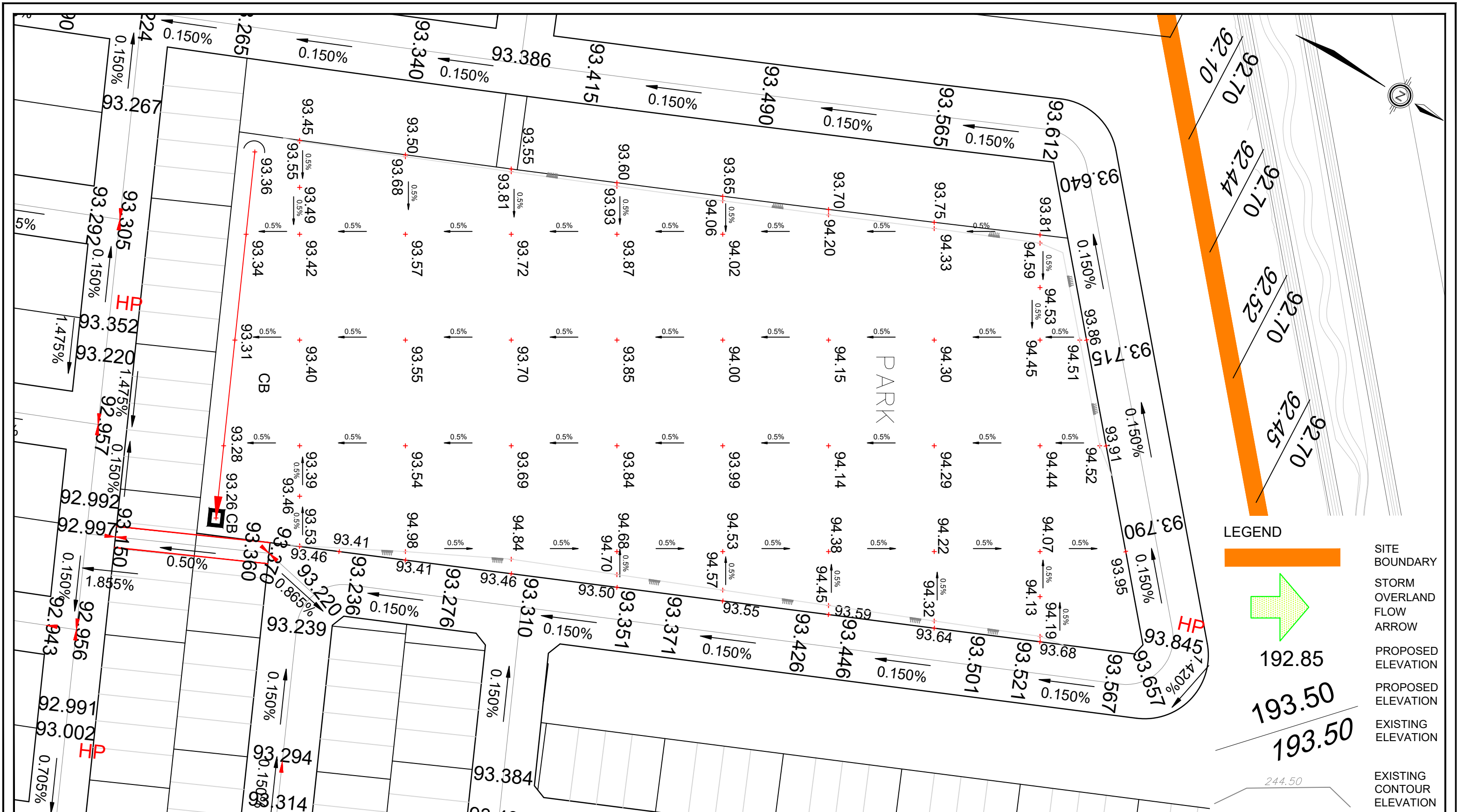
-  SITE BOUNDARY
-  STORM OVERLAND FLOW ARROW
-  PROPOSED ELEVATION
-  PROPOSED ELEVATION
-  EXISTING ELEVATION
-  EXISTING CONTOUR ELEVATION



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**BARRHAVEN CONSERVANCY  
CONCEPTUAL PARK 1 GRADING PLAN  
CITY OF OTTAWA**

PROJECT No.:	20-1226
SCALE:	1:1500
DATE:	OCTOBER 2021
FIGURE:	6

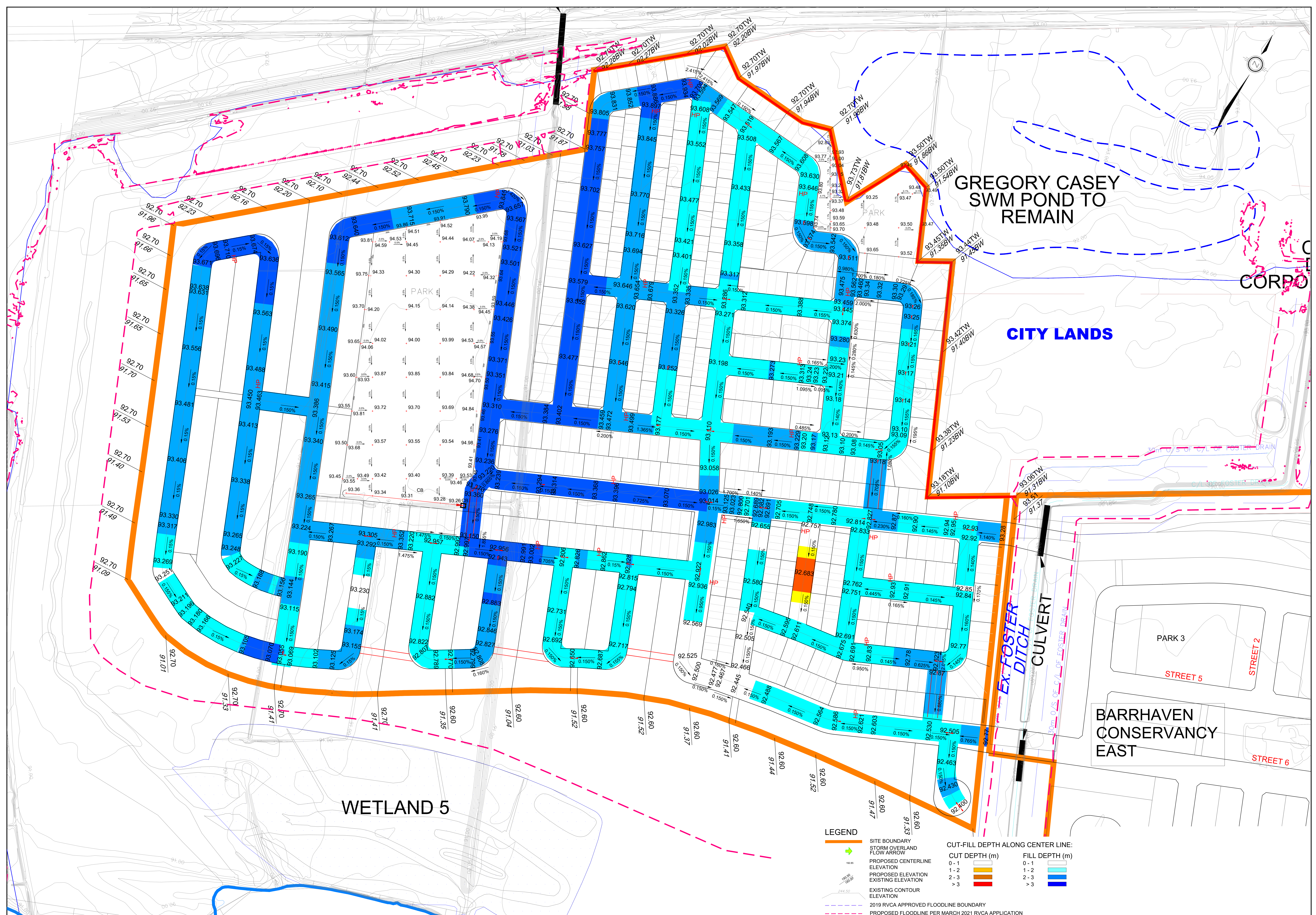


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BARRHAVEN CONSERVANCY EAST  
 CONCEPTUAL PARK 2 GRADING PLAN  
 CITY OF OTTAWA

PROJECT No.:	20-1226
SCALE:	1:1000
DATE:	OCTOBER 2021
FIGURE:	7





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BARRHAVEN CONSERVANCY  
 CONCEPTUAL GRADING PLAN  
 CITY OF OTTAWA

PROJECT No. : 20-1226  
 SCALE: 1:1000  
 DATE: OCTOBER 2021  
 DRAWING No. 1



Ex. CULVERT

McKENNA CASEY DRIVE

GREGORY CASEY SWM POND TO REMAIN

CORPO

CITY LANDS

BARRHAVEN CONSERVANCY EAST

EX-FOSTER DITCH CULVERT

WETLAND 5

SANITARY PUMPING STATION

- LEGEND**
- SITE BOUNDARY
  - STORM LOCAL SEWER
  - SANITARY TRUNK SEWER
  - SANITARY LOCAL SEWER
  - PROPOSED WATERMAIN
  - EXTERNAL SANITARY TRUNK SEWER
  - EXISTING WATERMAIN
  - FUTURE WATERMAIN
  - - - PROPOSED FLOODLINE PER MARCH 2021 RVCA APPLICATION
  - STORM MANHOLE
  - SANITARY MANHOLE



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BARRHAVEN CONSERVANCY  
CONCEPTUAL SERVICING PLAN  
CITY OF OTTAWA

PROJECT No. : 20-1226  
SCALE: 1:1000  
DATE: OCTOBER 2021  
DRAWING No. 2



Ex. CULVERT

# McKENNA CASEY DRIVE

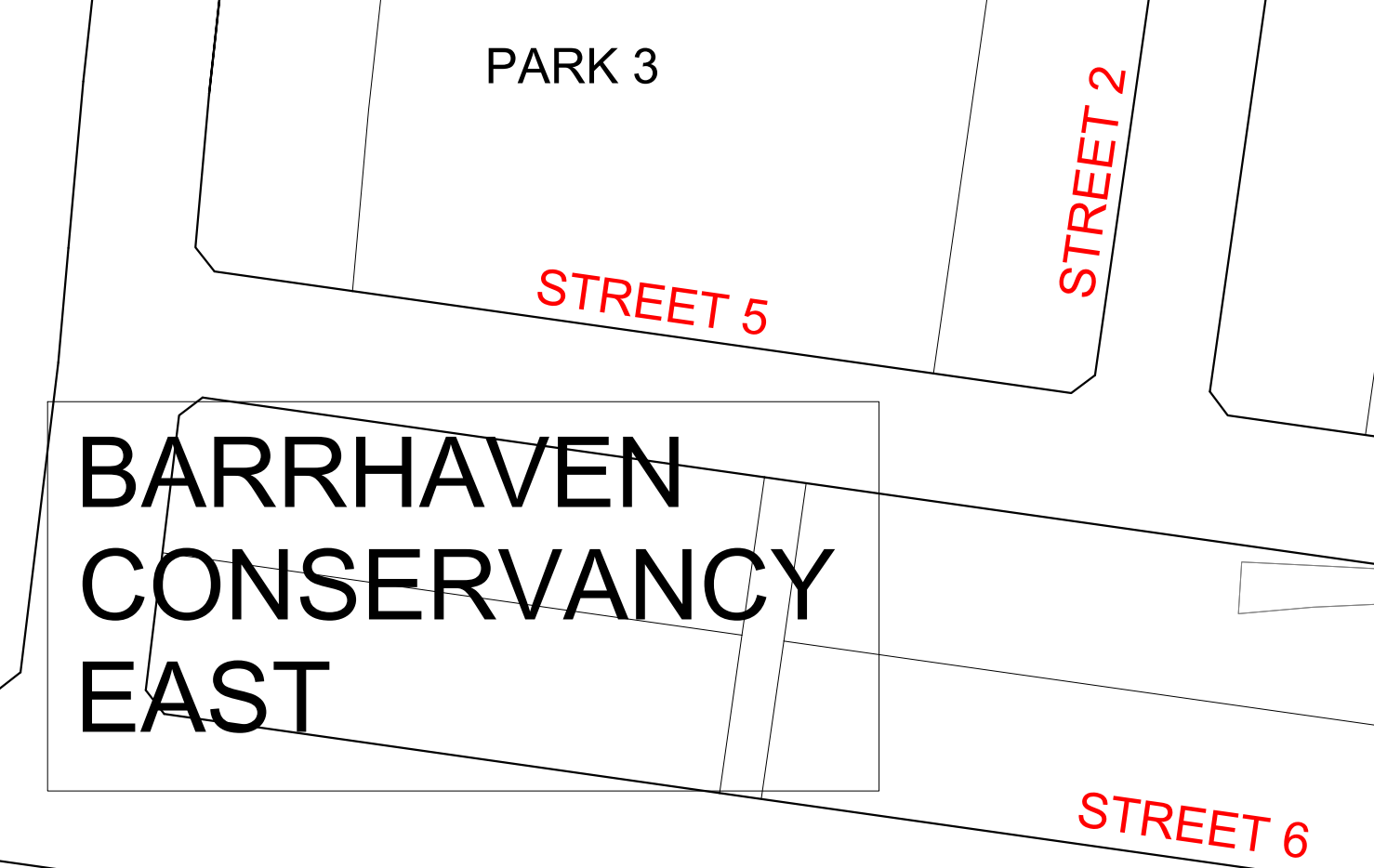
GREGORY CASEY SWM POND TO REMAIN

CITY LANDS

CITY LANDS

30m O/S OF C/L OF FOSTER DRAIN  
C/L OF FOSTER DRAIN

Ex-FOSTER DITCH  
CULVERT



### STM DRAWING LEGEND

- |  |                            |  |                    |
|--|----------------------------|--|--------------------|
|  | SITE BOUNDARY              |  | AREA IN HECTARES   |
|  | STORM TRUNK SEWER          |  | RUNOFF COEFFICIENT |
|  | STORM LOCAL SEWER          |  | STORM MAHOLE       |
|  | STORM TRUNK TRIBUTARY AREA |  |                    |



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BARRHAVEN CONSERVANCY  
STORM TRIBUTARY AREA  
CITY OF OTTAWA

PROJECT No. : 20-1226  
SCALE: 1:1000  
DATE: OCTOBER 2021  
DRAWING No. 3



EX. COLVERT

MICKENNA CASEY DRIVE

CORP

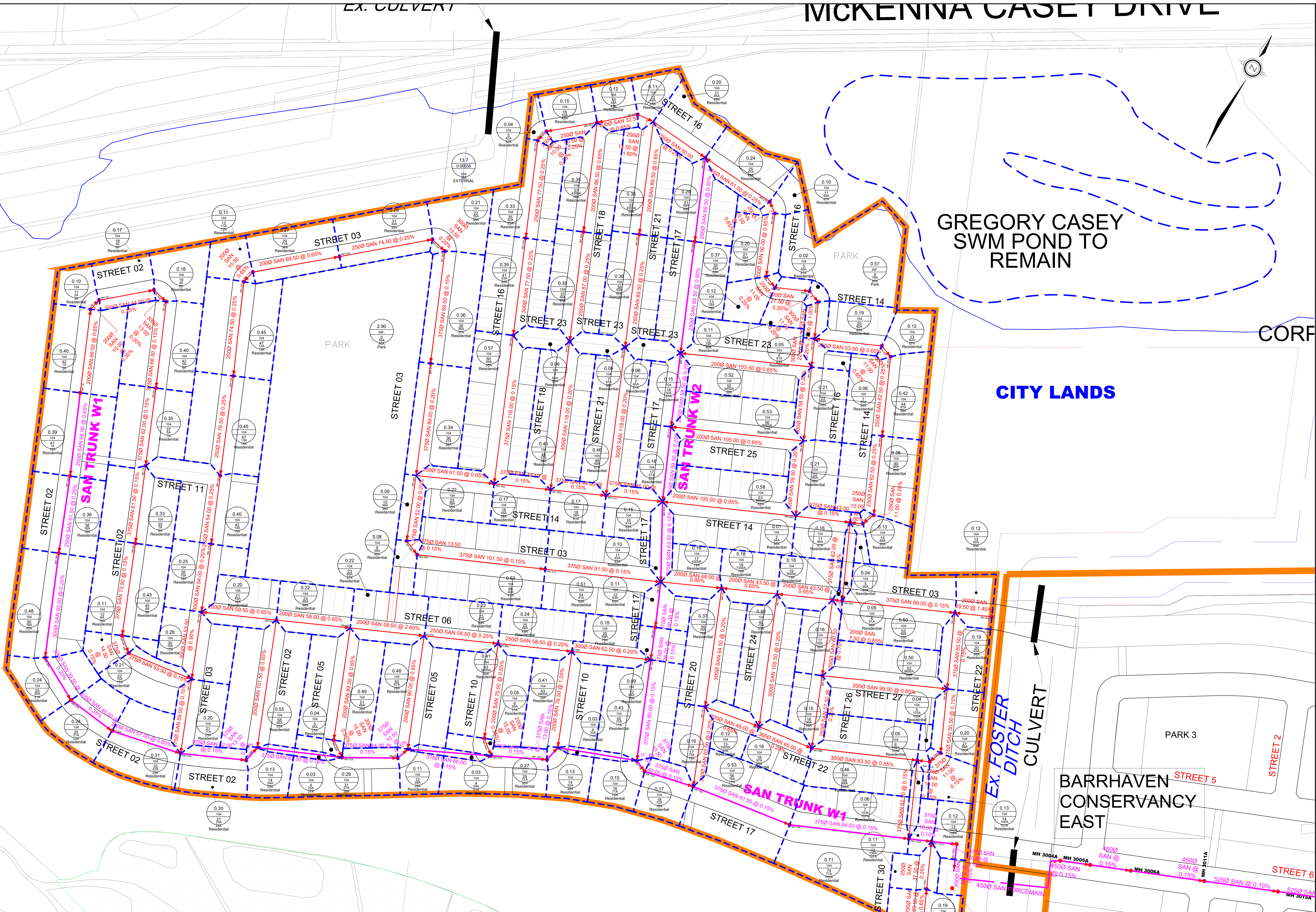
GREGORY CASEY SWM POND TO REMAIN

CITY LANDS

BARRHAVEN CONSERVANCY EAST

WETLAND 5

- LEGEND**
- SITE BOUNDARY
  - SANITARY TRUNK SEWER
  - SANITARY LOCAL SEWER
  - EXTERNAL SANITARY TRUNK SEWER
  - SANITARY MANHOLE
  - - - SANITARY TRIBUTARY AREA
- AREA IN HECTARES  
POPULATION PER HECTARE  
POPULATION



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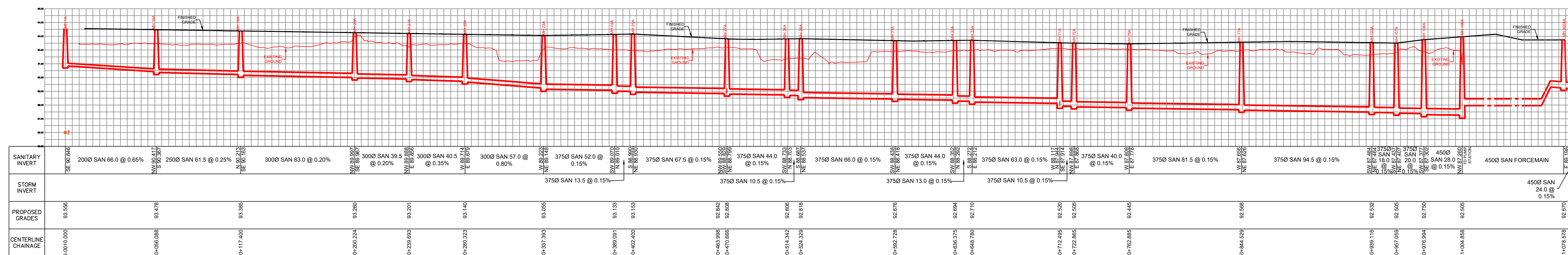
BARRHAVEN CONSERVANCY  
SANITARY TRIBUTARY AREA  
CITY OF OTTAWA

PROJECT No. : 20-1226  
SCALE: 1:1000  
DATE: OCTOBER 2021  
DRAWING No. 4

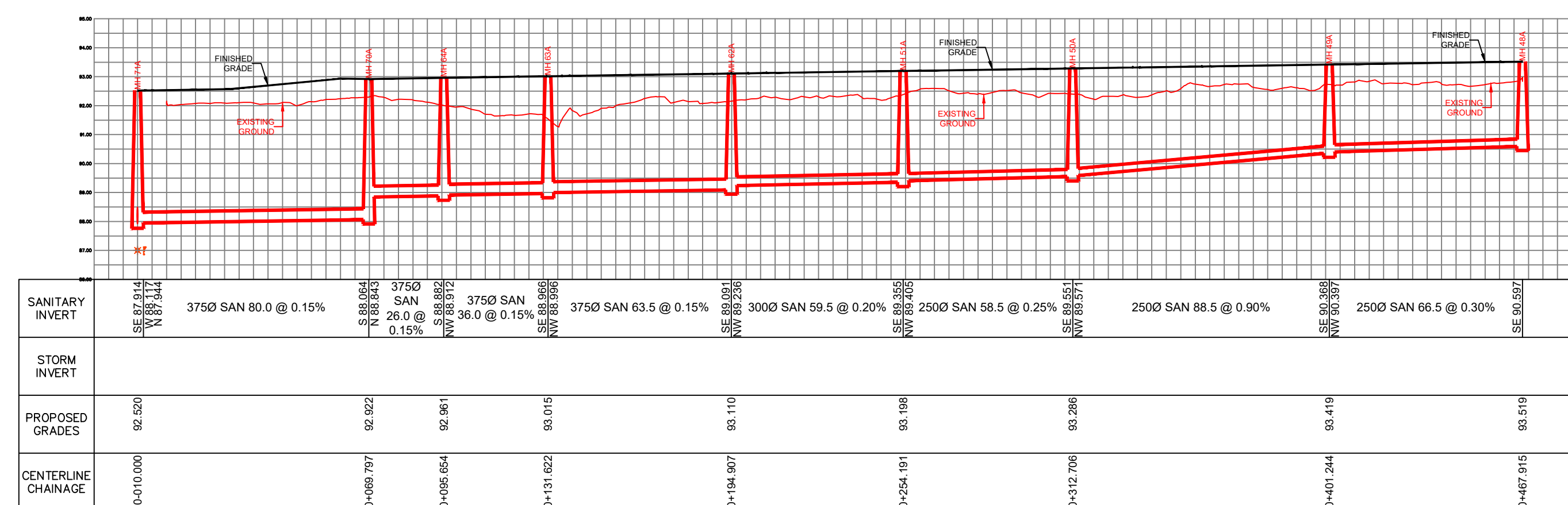




### SAN TRUNK W1



### SAN TRUNK W2



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BARRHAVEN CONSERVANCY  
SANITARY TRUNK PROFILES  
CITY OF OTTAWA

PROJECT No. : 20-1226  
SCALE: 1:1500  
DATE: OCTOBER 2021  
DRAWING No. 6

# **APPENDIX A**

## **GENERAL**

Content Copy Of Original



Ministry of the Environment and Climate Change  
Ministère de l'Environnement et de l'Action en matière de changement  
climatique

**ENVIRONMENTAL COMPLIANCE APPROVAL**

NUMBER 8129-AB7LDF

Issue Date: June 23, 2016

City of Ottawa  
100 Constellation Crescent West, 6th Floor  
Ottawa, Ontario  
K2G 6J8

Site Location: Jockvale Road and Strandherd Drive  
City of Ottawa, Ontario

*You have applied under section 20.2 of Part II.1 of the Environmental Protection Act, R.S.O. 1990, c. E. 19 (Environmental Protection Act) for approval of:*

sanitary sewers to be constructed in the City of Ottawa, on various vacant development lands (from Station 0+003 to Station 2+517), Greenbank Road (from Station 1+846 to Station 1+947), and Jockvale Road (from Station 2+430 to Station 2+517);

all in accordance with the application form from the City of Ottawa, dated June 22, 2016, including final plans and specifications prepared by Novatech Engineers, Planners and Landscape Architects.

*In accordance with Section 139 of the Environmental Protection Act, you may by written Notice served upon me and the Environmental Review Tribunal within 15 days after receipt of this Notice, require a hearing by the Tribunal. Section 142 of the Environmental Protection Act provides that the Notice requiring the hearing shall state:*

1. The portions of the environmental compliance approval or each term or condition in the environmental compliance approval in respect of which the hearing is required, and;
2. The grounds on which you intend to rely at the hearing in relation to each portion appealed.

*The Notice should also include:*

3. The name of the appellant;
4. The address of the appellant;
5. The environmental compliance approval number;
6. The date of the environmental compliance approval;
7. The name of the Director, and;
8. The municipality or municipalities within which the project is to be engaged in.

*And the Notice should be signed and dated by the appellant.*

*This Notice must be served upon:*

The Secretary\*  
Environmental Review Tribunal  
655 Bay Street, Suite 1500

AND

The Director appointed for the  
purposes of Part II.1 of the  
Environmental Protection Act

Toronto, Ontario  
M5G 1E5

Ministry of the Environment and  
Climate Change  
135 St. Clair Avenue West, 1st  
Floor  
Toronto, Ontario  
M4V 1P5

**\* Further information on the Environmental Review Tribunal's requirements for an appeal can be obtained directly from the Tribunal at: Tel: (416) 212-6349, Fax: (416) 326-5370 or [www.ert.gov.on.ca](http://www.ert.gov.on.ca)**

*The above noted activity is approved under s.20.3 of Part II.1 of the Environmental Protection Act.*

DATED AT TORONTO this 23rd day of June, 2016

Gregory Zimmer, P.Eng.  
Director  
appointed for the purposes of Part II.1 of  
the *Environmental Protection Act*

AF/  
c: District Manager, MOECC Ottawa  
Water Supervisor, MOECC, Ottawa  
M. Rick O'Connor, City Clerk, City of Ottawa  
Luc Marineau, City of Ottawa  
Jonathan Knoyle, City of Ottawa  
Bob Dowdall, Novatech Engineers, Planners and Landscape Architects  
Edson Donnelly, Novatech Engineers, Planners and Landscape Architects

**APPENDIX B**  
**WATER SUPPLY**

---

To:	Kevin Murphy David Schaeffer Engineering Ltd.	From:	Jasmin Sidhu / Kevin Alemany Stantec Consulting Ltd.
File:	163401437 / 163401660	Date:	March 5, 2021

---

**Reference: Hydraulic Potable Water Assessment for Barrhaven Conservancy Development Corporation**

## OVERVIEW

Stantec Consulting Ltd. (Stantec) was retained by Barrhaven Conservancy Development Corporation to perform a hydraulic assessment for a land parcel located adjacent to Pressure Zone (PZ) 3SW (previously known as PZ BARR). This technical memo reviews and assesses the limitations/opportunities associated with servicing the parcel in question as it is located near the Jock River. The parcel in question, which is divided into east (Conservancy East) and west (Conservancy West) portions, is herein referred to as the Barrhaven Conservancy Lands.

## BACKGROUND REVIEW

As part of the assessment, the following reports were reviewed:

- City of Ottawa 2013 Water Master Plan, Stantec Consulting Ltd., September 2013;
- Kennedy-Burnett Potable Water Master Servicing Study, Stantec Consulting Ltd., April 2014;
- SUC Water Infrastructures Upgrades – Hydraulic Assessment, Stantec Consulting Ltd., July 2015; and,
- Barrhaven Master Servicing Study Addendum – Revised Potable Water and Sanitary Servicing Analysis for the Barrhaven South Urban Expansion Area, Stantec Consulting Ltd., March 2017.

## ZONE 3SW AND ZONE SUC

### ZONAL WATER DEMANDS & POPULATION PROJECTIONS

Zone 3SW services the lands adjacent to the proposed Barrhaven Conservancy Lands development. In 2015, the City embarked on a large initiative to reconfigure the pressure zones servicing Barrhaven and the southern reaches of Ottawa, and area called the South Urban Community (SUC). The purpose of the zone reconfiguration was to improve reliability, to improve efficiencies and to provide increased pumping capacity for future growth.

**Table 1** shows the projected water demands and **Table 2** shows the projected populations of Zone 3SW and Zone SUC before and after the pressure zone reconfiguration. These values were adapted from the City of Ottawa 2013 Water Master Plan (Stantec, 2013) and the SUC Water Infrastructure Upgrades – Hydraulic Assessment (Stantec, 2015) reports.



Reference: Hydraulic Potable Water Assessment for Barrhaven Conservancy Development Corporation

**Table 1: Water Demand Projections**

Zone	Existing Pre-Zone Reconfiguration (MLD)			2018 Post-Zone Reconfiguration (MLD)			2031 Post-Zone Reconfiguration (MLD)			2060 Post-Zone Reconfiguration (MLD)		
	BSDY	MXDY	PKHR	BSDY	MXDY	PKHR	BSDY	MXDY	PKHR	BSDY	MXDY	PKHR
<b>3SW</b>	12.0	26.2	52.3	5.7	11.7	27.0	6.3	12.8	29.5	6.4	12.9	29.8
<b>SUC</b>	3.4	7.3	14.6	24.7	47.6	90.8	44.4	78.7	148.9	63.3	107.6	207.1

**Table 2: Population Projections**

Zone	Existing Pre-Zone Reconfiguration	2018 Post-Zone Reconfiguration	2031 Post-Zone Reconfiguration	2060 Post-Zone Reconfiguration
<b>3SW</b>	48,917	29,995	30,363	31,183
<b>SUC</b>	5,737	137,909	175,073	234,538

**PUMPING CAPACITY**

The newly installed pumps for Zone 3SW are sized based on population/demand projections for lands within current approved growth areas. They do not include demands attributed to the Barrhaven Conservancy Lands. As such, the current pumping capacity into Zone 3SW is not sufficient to supply these additional lands along with the growth already planned for in Zone 3SW up to 2060 projections.

The Fallowfield Road Pumping Station (FRPS) (previously known as Barrhaven Reservoir Pumping Station) and Barrhaven Pumping Station (BPS) will continue to service Zone 3SW post pressure zone reconfiguration; however, both pump stations are being equipped with new pumps that were sized for the post pressure zone reconfiguration water demands in Zone 3SW.

The new FRPS is already commissioned and in operation while the BPS is currently undergoing pumping tests on the newly installed pumps as part of its commissioning process.

The BPS is changing from a single zone station to a dual zone pump station and will operate in conjunction with Ottawa South Pumping Station (OSPS) to service the newly expanded Zone SUC. It will also continue to service the smaller/reduced Zone 3SW with one of its pumps.

The Ottawa South Pumping Station is the second pumping station that will feed Zone SUC. It is currently undergoing a detailed design for its upgrade. It may be possible to make some provisions to account for the additional demands in SUC however it is recommended that this be considered as soon as possible through discussions with the City.

**Table 3** provides the pumping capacities into each pressure zone post zone reconfiguration upgrades.

Reference: Hydraulic Potable Water Assessment for Barrhaven Conservancy Development Corporation

**Table 3: Pumping Capacity Post-Zone Reconfiguration**

Zone	Firm Pumping Capacity (MLD)	Total Pumping Capacity (MLD)
3SW	14	21
SUC	113	173

Due to the elevated balancing storage provided by Moodie Tank, the firm capacity of the 3SW pumps must be able to supply the future 2060 maximum day demand of 12.9 MLD as shown in **Table 1**. The 3SW pumps were sized based on 2060 demands as they do not increase significantly compared to 2018 post zone reconfiguration demands.

In Zone SUC, without elevated storage, the firm capacity of the pumps must be able to supply the greater demand of peak hour (90.8 MLD) or maximum day plus fire flow (66.3 MLD; FF = 18.7 MLD) for post zone reconfiguration demands. It should be noted that pumping capacity at the SUC pump stations will be further increased in the future to meet 2031 and 2060 projected demands.

The above shows that both the 3SW and SUC pumps have been sized to meet the existing and future demands within the previously established growth areas. For the purpose of this assessment, it is assumed that the demand for the Barrhaven Conservancy Lands is not accounted for in the current capacity of the Zone 3SW pumps but can be accommodated by the SUC pumps. The impact on district-level distribution pumping and needs will be further reviewed as part of the City's 2021 Water Master Plan.

## HYDRAULIC ASSESSMENT

### WATER DEMANDS

Following the 2013 Water Master Plan "Design Criteria and Levels of Service", when projected population exceeds 3,000 persons, basic unit demands for Zone/System Levels are to be used. For residential land-uses, single family and semi-detached homes were considered to have similar demands, with both types of residential home categorized under "single family home" or SFH. All townhomes were categorized under "multi-level townhomes" or MLT and all apartments or high-density units were categorized under APT. Consumption rates for SFH, MLT and APT are presented in **Table 4**.

To determine the MXDY demand, an outdoor water demand (OWD) of 1,049 L/SFH/d is allocated to all SFH units. This is a fixed value and does not change with zone demand. This outdoor water demand is added to the basic day (BSDY) demand to obtain the MXDY demand.

The unit counts were provided by David Schaeffer Engineering Ltd. (DSEL) via email on March 1, 2021. The estimated water demands are presented in **Table 4**. This additional demand is not within the current capacity of the new pumps within Zone 3SW.

Reference: Hydraulic Potable Water Assessment for Barrhaven Conservancy Development Corporation

**Table 4: Estimated Water Demands of the Barrhaven Conservancy Lands**

Unit Types	Unit Count			PPU	Pop.	L/c/d	BSDY (MLD)	MXDY (MLD)
	Conservancy East	Conservancy West	Total					
Single Family	730	775	1,505	3.4	5,117	180	0.92	2.50
Townhouse	445	525	970	2.7	2,619	198	0.52	0.52
Rear-Lane Townhouse	165	-	165	2.7	446	198	0.09	0.09
High Density	100	-	100	2.1	210	219	0.05	0.05
<b>Total</b>	<b>1,440</b>	<b>1,300</b>	<b>2,740</b>		<b>8,392</b>		<b>1.57</b>	<b>3.15</b>

### POTABLE WATER SERVICING ALTERNATIVES

Figures 1 to 6 and Table 5 present alternatives to service the Barrhaven Conservancy Lands with potable water and discusses limitations of each alternative. For system reliability purposes, primary and secondary feeds have been identified for each alternative. It should be noted that the alignments shown in Figures 1 to 6 are approximate with the intent to show general locations for possible connections.

Based on hydraulic modelling of trunk main looping through the Conservancy Lands and review of previously completed servicing studies for adjacent lands, all alternatives are anticipated to satisfy the City’s objective minimum pressure of 40 psi during peak hour demand and achieve a typical planning level fire flow value 13,000 L/min or greater. These results are discussed further in the following sections. Detailed modelling results are provided in the **Hydraulic Modelling Results** attachment.

#### Alternative 1 – Servicing from 3SW

Figure 1 shows the connection points to the Kennedy-Burnett watermains that are fed by the future Strandherd Drive watermain.

Based on the Kennedy-Burnett Potable Water Master Servicing Study (Stantec, 2014), which is a subdivision adjacent to the Barrhaven Conservancy Lands, it is likely the Barrhaven Conservancy Lands will experience pressures greater than the City of Ottawa’s objective pressure of 80 psi during basic day demands if operating at Zone 3SW pressure. This is corroborated by hydraulic modelling results which show the maximum pressure along the trunk main looping through the Conservancy Lands under basic day demands to be approximately 88 psi. Therefore, pressure mitigation measures would need to be considered (i.e., pressure reducing valves (PRVs) at individual service connections) for this servicing alternative.

Pumping capacity upgrades at FRPS and/or BPS would be required to service the Barrhaven Conservancy Lands from Zone 3SW on a permanent basis. As an example of costs, recent upgrades to the FRPS totaled approximately \$1.5 million. Additional works at FRPS and BPS to service the Conservancy Lands could include retrofitting the pump(s), piping, valving and supporting infrastructures as well as instrumentation, electrical and mechanical aspects. A more in-depth assessment would be required to determine the potential costs.

Another alternative to service the Barrhaven Conservancy Lands from Zone 3SW would be on a temporary basis. As shown in Figure 1, the initial phase of development (estimated boundary shown) could be serviced at 3SW pressure and switched over to SUC pressure at a later time as development takes place. While this

**Reference:** Hydraulic Potable Water Assessment for Barrhaven Conservancy Development Corporation

alternative is likely to be technically feasible, the extent of development within the Barrhaven Conservancy Lands that can operate at 3SW pressure in the interim will depend on the City's planning and approvals currently in place. This alternative essentially borrows capacity from existing approved areas within Zone 3SW until such time that the borrowed capacity is replaced through system upgrades. Through discussions with City staff, the City has indicated that this is not a desirable option.

### **Alternative 2 – Servicing from SUC**

**Figures 2 to 5** show the Barrhaven Conservancy Lands being serviced by new SUC watermains and include various options for a secondary feed.

Both Alternatives 2a and 2b propose a new SUC watermain running parallel to the future 3SW Strandherd watermain as the primary feed. This feed would then run south, parallel to the existing watermains that currently service the existing subdivisions north of the Conservancy Lands (including Phase 1 lands) that operate at 3SW pressures. Alternative 2a proposes a secondary feed from Nepean Town Centre (NTC) whereas Alternative 2b proposes a secondary feed from Barrhaven South. Based on findings from the Barrhaven South Urban Expansion Area Master Servicing Study (Stantec, 2017), the Barrhaven Conservancy Lands can anticipate maximum pressures greater than 75 psi and potentially greater than 80 psi during basic day demands if operating at Zone SUC pressure. Hydraulic modelling results indicate that the maximum pressure along the trunk main looping through the Conservancy Lands under basic day demands is estimated to be approximately 76 psi and available fire flow to be in excess of 13,000 L/min for both Alternatives 2a and 2b. Therefore, PRVs would not be required. As these two options would require the installation of a second separate watermain along Strandherd Drive (which will be undergoing widening as part of a separate recently awarded project) and through the existing north subdivision, the City has indicated that these alternatives are not preferred.

Alternative 2c proposes both primary and secondary feeds from the NTC (one along future Chapman Mills Drive and one through the future Claridge development from southeast of the KB pond) to service the first stages of development in the Conservancy Lands. As per currently proposed, site servicing through the Claridge lands, Alternative 2c would connect to a 300 mm diameter watermain along Chapman Mills Drive and a 200 mm watermain southeast of the KB pond. Similar to Alternatives 2a and 2b, hydraulic modelling results show that the maximum pressure along the trunk main looping through the Conservancy Lands under basic day demands is estimated to be approximately 76 psi and available fire flow to be in excess of 13,000 L/min.

Alternative 2d proposes a primary feed through the future Claridge development from southeast of the KB pond and a secondary feed from Barrhaven South. Pressures and available fire flows along the trunk main looping through the Conservancy Lands are similar to those for Alternatives 2a, 2b and 2c.

All four alternatives (2a to 2d) present challenges due to limited land access, crossings of a body of water, and/or requiring a new watermain to be installed along recently or soon to be (re)constructed right-of-ways.

### **Alternative 3 – Servicing from SUC with an Automated Valve from 3SW**

**Figure 6** shows the Barrhaven Conservancy Lands being serviced by a new SUC watermain running parallel to the Strandherd Drive watermain and a secondary feed from 3SW for emergency conditions.

This alternative proposes a secondary feed from 3SW via an automated valve off the future Strandherd Drive watermain. Water would flow from the high pressure Zone 3SW into the low pressure Zone SUC if there is a pressure drop on the SUC side of the valve. This alternative requires an interzonal valve connection that is not typically used/accepted in the City of Ottawa and would present both operational challenges and costs to operate and maintain. Similar to Alternatives 2a and 2b, this option would require the installation of a second separate watermain along Strandherd Drive (which will be undergoing widening as part of a separate recently

**Reference:** Hydraulic Potable Water Assessment for Barrhaven Conservancy Development Corporation

awarded project) and through the existing north subdivision; therefore, the City has indicated that this alternative is not preferred.

**Table 5: Potable Water Servicing Alternatives & Limitations**

Alternative		Zone	Max Pressures	Min Pressures	Available Fire Flow at 20 psi	Limitations
1	Connect to the future 3SW 406 mm dia. WM along Strandherd Drive at two locations	3SW	88 psi	52 psi	> 13,000 L/min	Requires additional pumping capacity in Zone 3SW. Will require individual PRVs at each service connection. <b>Therefore, the City has indicated that this is not a preferred option.</b>
2a	Connect to a future SUC WM that will run parallel to the future Strandherd WM and connect to a 2nd future SUC WM from the NTC (north of the Jock River)	SUC	76 psi	64 psi	≥ 13,000 L/min	Requires crossing water way east of the Barrhaven Conservancy Lands. Land around ponds may not be accessible. Requires installation of a second separate WM along Strandherd Drive and through the existing north subdivision. <b>Therefore, the City has indicated that this is not a preferred option.</b>
2b	Connect to a future SUC WM that will run parallel to the future Strandherd WM and connect to a 2nd future SUC WM from Barrhaven South (south of the Jock River – crossing river)	SUC	76 psi	61 psi	> 13,000 L/min	Requires crossing the Jock River. Requires installation of a second separate WM along Strandherd Drive and through the existing north subdivision. <b>Therefore, the City has indicated that this is not a preferred option.</b>
2c	Connect to future SUC WMs in the NTC (north of the Jock River) at two locations	SUC	76 psi	64 psi	> 13,000 L/min	Requires crossing water way east of the Barrhaven Conservancy Lands. Land around ponds may not be accessible. Requires installation of a second separate WM through the existing north subdivision that is currently operated at 3SW pressures.

Reference: Hydraulic Potable Water Assessment for Barrhaven Conservancy Development Corporation

Alternative		Zone	Max Pressures	Min Pressures	Available Fire Flow at 20 psi	Limitations
2d	Connect to a future SUC WM through the Claridge lands (north of the Jock River) and connect to a 2nd future SUC WM from Barrhaven South (south of the Jock River – crossing river)	SUC	76 psi	61 psi	> 13,000 L/min	Requires crossing the Jock River. Requires crossing water way east of the Barrhaven Conservancy Lands. Land around ponds may not be accessible.
3	Connect to a future SUC WM that will run parallel to the future Strandherd WM and connect to the Strandherd 3SW WM using an automated valve to feed from 3SW under emergency conditions	SUC	76 psi (could potentially be > 80 psi depending on valve operation)	67 psi	> 13,000 L/min	Requires crossing water way east of the Barrhaven Conservancy Lands. Land around ponds may not be accessible. May possibly require PRVs at each service connection. An automated 3SW/SUC valve presents operational challenges and costs. Requires installation of a second separate WM along Strandherd Drive and through the existing north subdivision. <b>Therefore, the City has indicated that this is not a preferred option.</b>

## SUMMARY & RECOMMENDATIONS

The recent pump station upgrades at the Zone 3SW pump stations are nearing completion. For the purpose of this assessment, it is assumed that the demand for the Barrhaven Conservancy Lands is not accounted for in the current capacity of the Zone 3SW pumps but can be accommodated by the SUC pumps.

Alternative 1 for servicing the Conservancy Lands would eventually require changing the recently commissioned pumps at the Fallowfield Road Pumping and Station and one of the new pumps at the Barrhaven Pump Station and potentially some of the associated piping, valving, instrumentation, electrical and mechanical appurtenances for higher capacity pumps and appurtenances. Due to the anticipated maximum pressures exceeding 80 psi during basic day demands, individual PRVs will be required at each service connection if the lands operate at Zone 3SW pressure. It is understood from discussions with the City staff that this is not a preferred option.

Servicing the Conservancy Lands from Zone SUC requires the installation of a second separate watermain along Strandherd Drive and through the existing north subdivision and/or a crossing of a stormwater pond and/or the Jock River to complete a looping network. All four alternatives present their own challenges with either limited land access, crossings of a body of water, and/or requiring a new watermain to be installed along recently or soon to be (re)constructed right-of-ways. City staff have indicated that options requiring a separate

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**Reference: Hydraulic Potable Water Assessment for Barrhaven Conservancy Development Corporation**

watermain along Strandherd (2a, 2b and 3) are not preferred since this portion of Strandherd Drive is undergoing widening as part of a separate recently awarded project and the timing for modifications does not work. As such, the City has identified Alternative 2c as the preferred servicing alternative, with 2d also being a viable option. Based on hydraulic modelling results along the trunk main looping through the Conservancy Lands, servicing of these lands with two 300 mm diameter watermains from the future 300 mm and 200 mm Claridge lands watermains (i.e., Alternative 2c) is possible, however ultimate optimization of sizing would have to be completed at a later phase.

An automated 3SW/SUC valve could potentially be considered for interim conditions, as discussed in Alternative 3, however inter-zonal automated valve connections are not typically used/accepted in the City of Ottawa and would present both operational challenges and costs to operate and maintain.

In addition to the secondary feeds proposed for each alternative, other system reliability measures may be considered as development continues to progress in adjacent lands. Measures may include providing additional looping between subdivisions and/or potential use of automated valves between the 3SW and SUC networks in this area for use under emergency conditions.

Sincerely,

**Stantec Consulting Ltd.**

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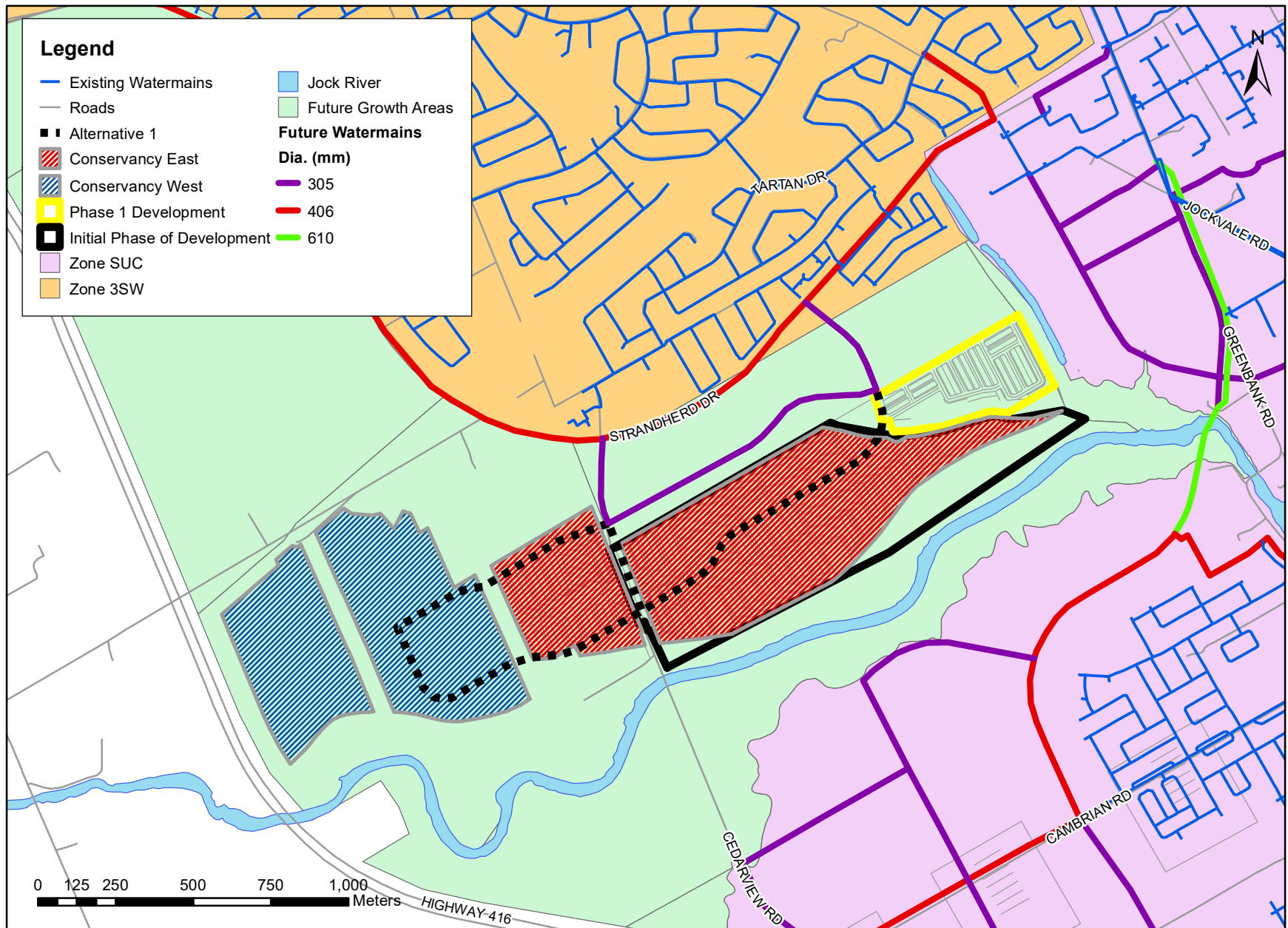
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Attachments: Figure 1: Alternative 1 – Servicing from Zone 3SW  
Figure 2: Alternative 2a – Servicing from Zone SUC (from Strandherd) w/ Secondary Feed from NTC  
Figure 3: Alternative 2b – Servicing from Zone SUC (from Strandherd) w/ Secondary Feed from Barrhaven South  
Figure 4: Alternative 2c – Servicing from Zone SUC (from NTC) w/ Secondary Feed from NTC  
Figure 5: Alternative 2d – Servicing from Zone SUC (from Claridge Lands) w/ Secondary Feed from Barrhaven South  
Figure 6: Alternative 3 – Servicing from Zone SUC w/ Automated Valve from 3SW for Emergency Conditions  
Figure 7: Conservancy Lands System Node ID Map  
Hydraulic Modelling Results

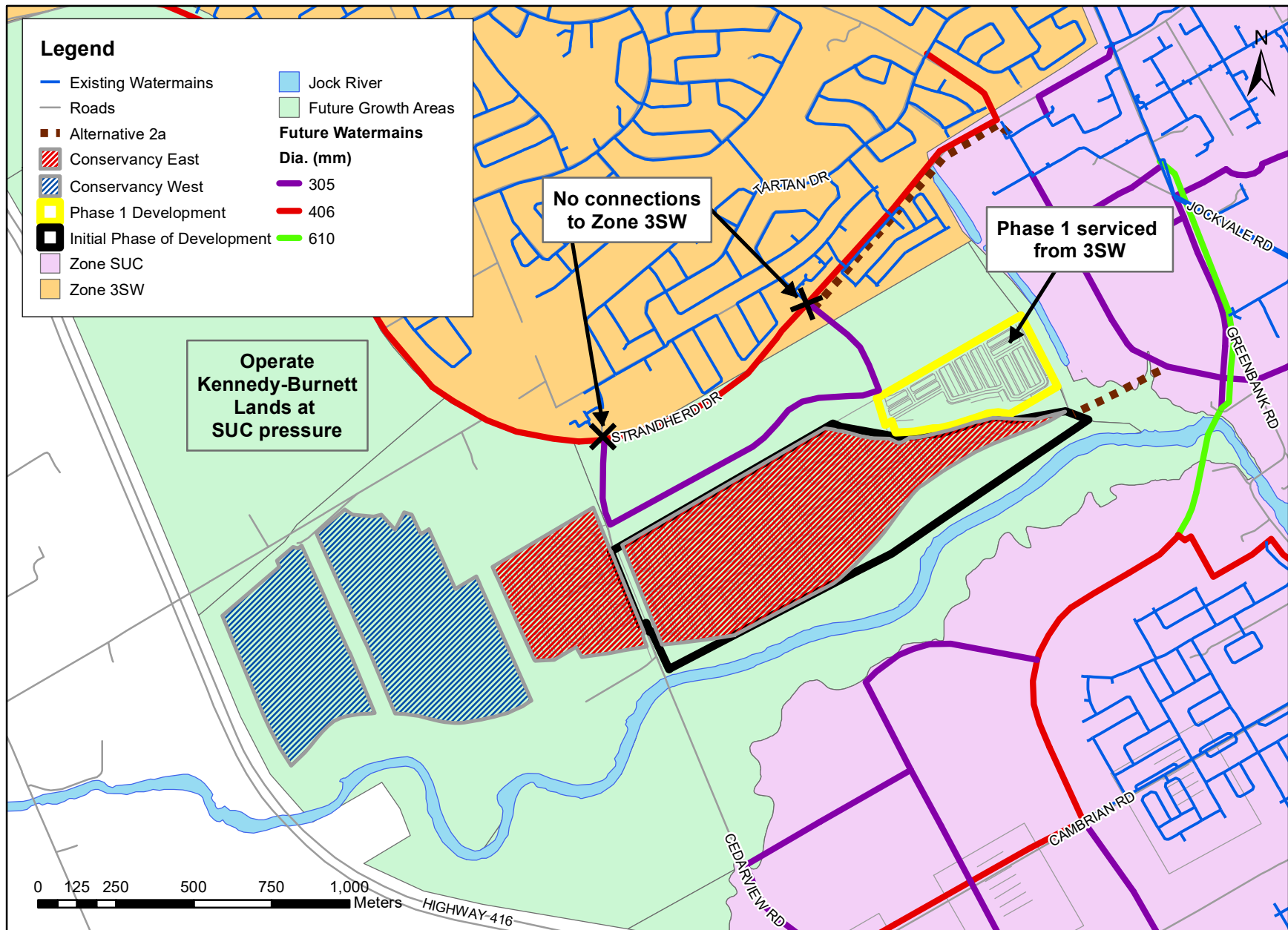


**Figure 1: Alternative 1 - Servicing from Zone 3SW**

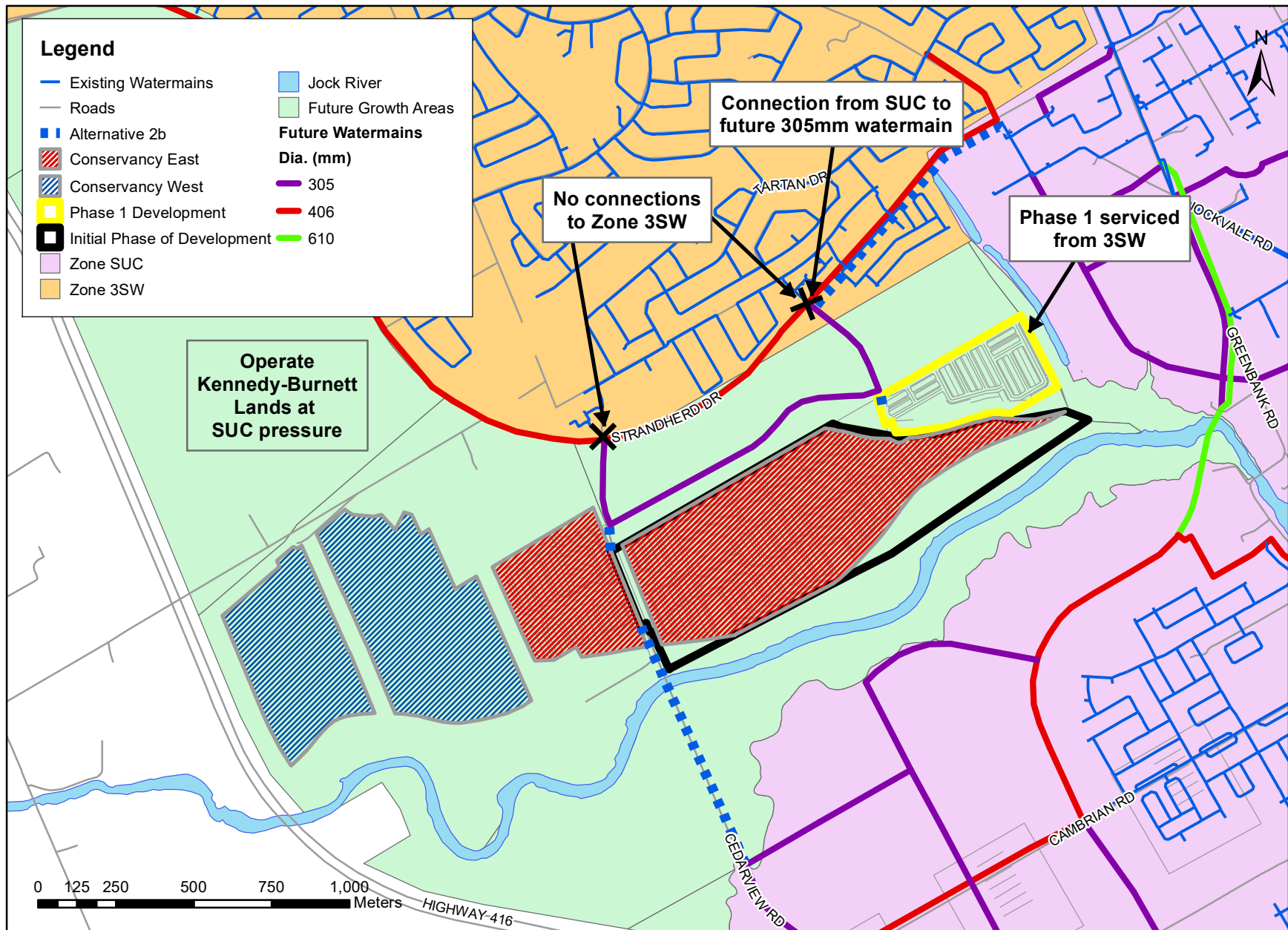




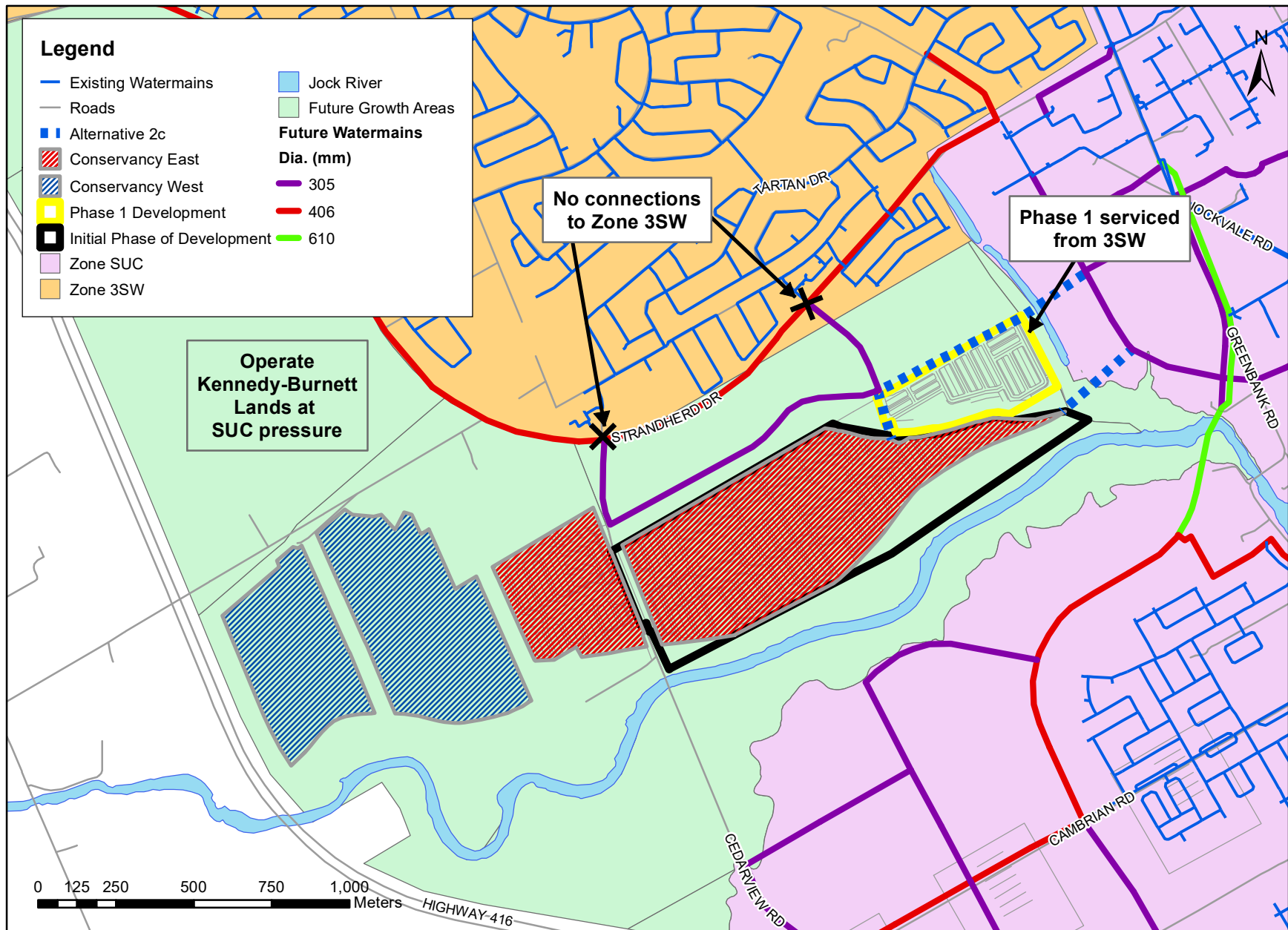
**Figure 2: Alternative 2a - Servicing from Zone SUC (from Strandherd) w/ Secondary Feed from NTC**



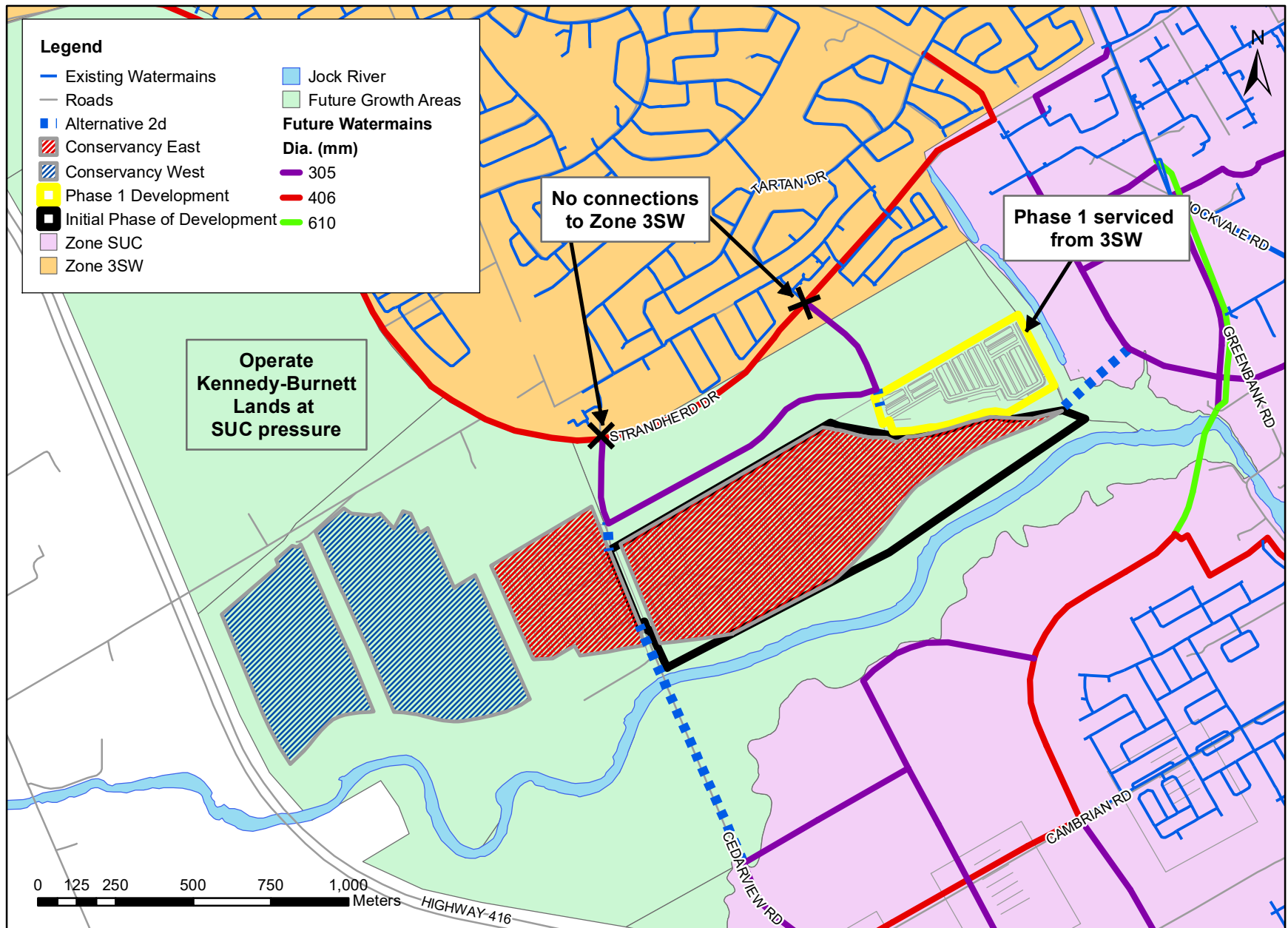
**Figure 3: Alternative 2b - Servicing from Zone SUC (from Strandherd) w/ Secondary Feed from Barrhaven South**



**Figure 4: Alternative 2c - Servicing from Zone SUC (from NTC) w/ Secondary Feed from NTC**

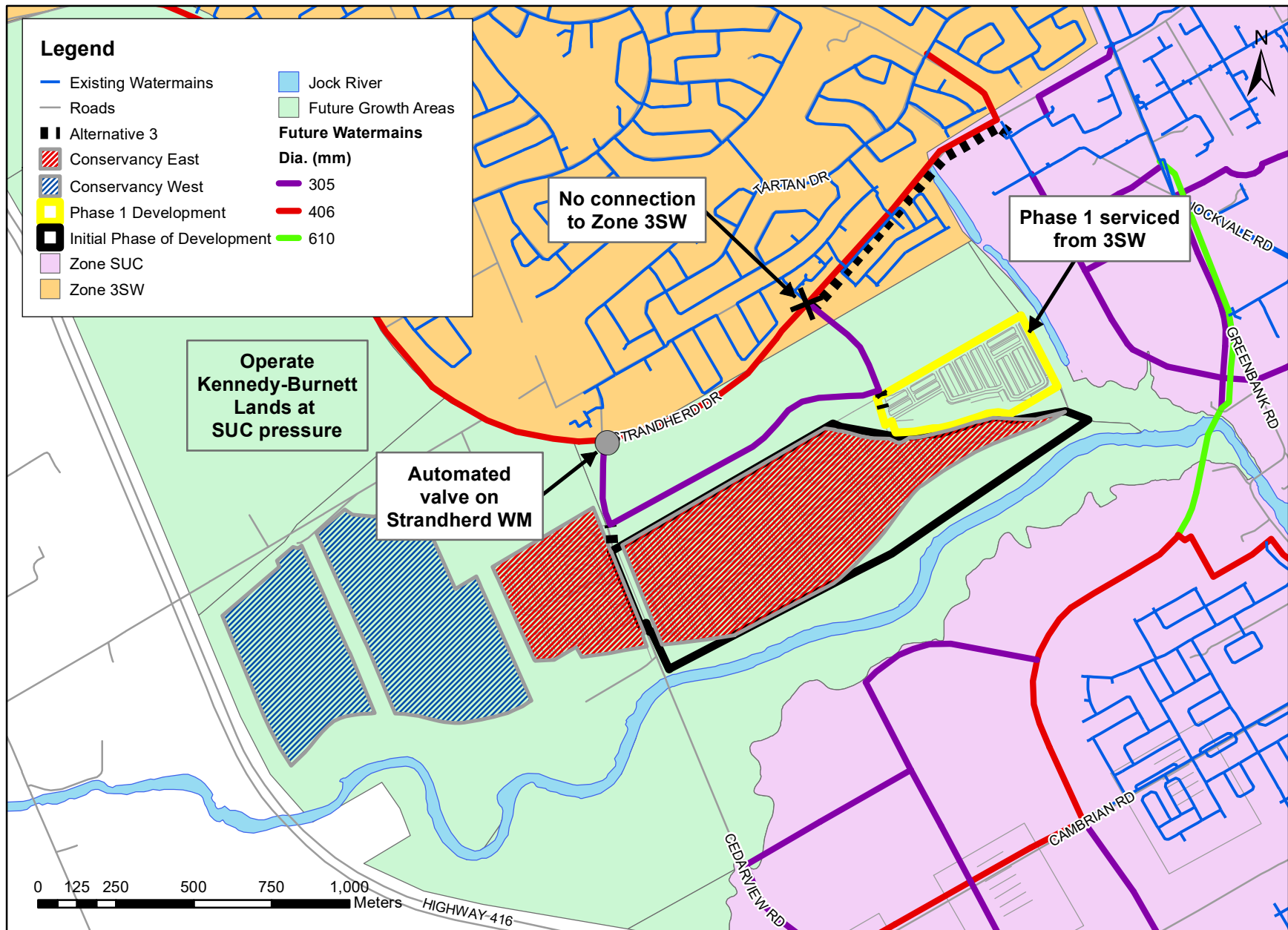


**Figure 5: Alternative 2d - Servicing from Zone SUC (from Claridge Lands) w/ Secondary Feed from Barrhaven South**

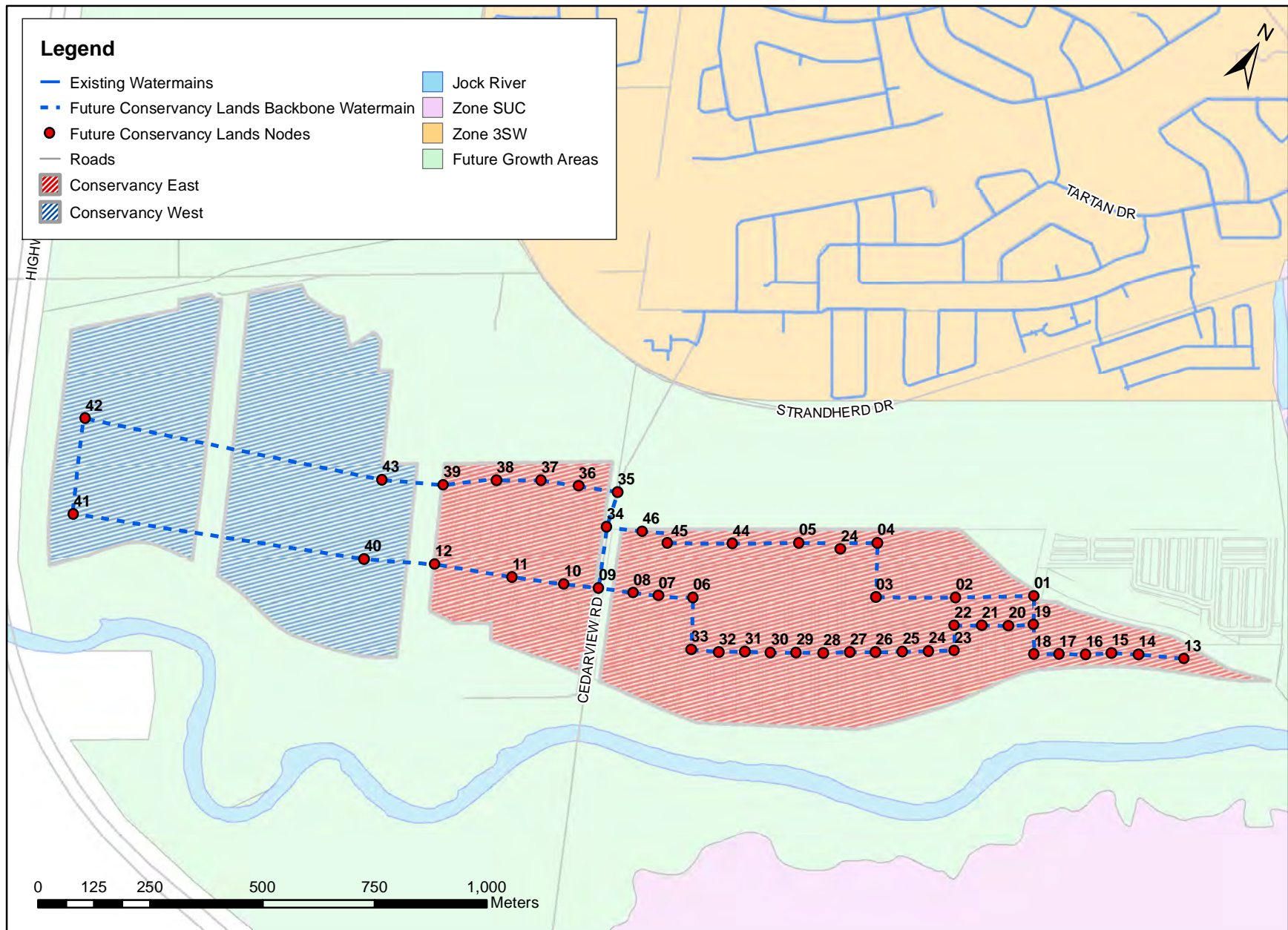




**Figure 6: Alternative 3 - Servicing from Zone SUC w/ Automated Valve from 3SW for Emergency Conditions**



**Figure 7: Conservancy Lands System Node ID Map**



**BSDY Model Results**

MIN		87.5						75.7							75.6					
MAX		87.5						75.7							75.6					
Model Node ID	Figure Node ID	Servicing Alternative 1							Servicing Alternative 2a						Servicing Alternative 2b					
		Max Value (psi)	Max Time (hrs.)	Min Value (psi)	Min Time (hrs.)	Avg (psi)	Diff (psi)	Max Value (psi)	Max Time (hrs.)	Min Value (psi)	Min Time (hrs.)	Avg (psi)	Diff (psi)	Max Value (psi)	Max Time (hrs.)	Min Value (psi)	Min Time (hrs.)	Avg (psi)	Diff (psi)	
F_BARRCONS_01	01	87.47	2:00	82.62	7:00	85.36	4.85	75.66	3:00	73.69	7:00	74.86	1.98	75.58	3:00	73.30	7:00	74.66	2.28	
F_BARRCONS_02	02	87.47	2:00	82.62	7:00	85.36	4.85	75.66	3:00	73.66	7:00	74.85	2.01	75.58	3:00	73.28	7:00	74.66	2.29	
F_BARRCONS_03	03	87.47	2:00	82.62	7:00	85.36	4.85	75.66	3:00	73.63	7:00	74.84	2.03	75.57	3:00	73.27	7:00	74.65	2.30	
F_BARRCONS_04	04	87.47	2:00	82.62	7:00	85.36	4.85	75.66	3:00	73.61	7:00	74.83	2.05	75.57	3:00	73.27	7:00	74.65	2.30	
F_BARRCONS_05	05	87.47	2:00	82.62	7:00	85.36	4.85	75.66	3:00	73.59	7:00	74.83	2.07	75.57	3:00	73.26	7:00	74.65	2.31	
F_BARRCONS_06	06	87.47	2:00	82.60	7:00	85.35	4.87	75.66	3:00	73.56	7:00	74.81	2.10	75.57	3:00	73.25	7:00	74.64	2.31	
F_BARRCONS_07	07	87.47	2:00	82.61	7:00	85.35	4.87	75.66	3:00	73.55	7:00	74.81	2.10	75.57	3:00	73.25	7:00	74.64	2.31	
F_BARRCONS_08	08	87.47	2:00	82.61	7:00	85.35	4.86	75.66	3:00	73.55	7:00	74.81	2.10	75.57	3:00	73.25	7:00	74.64	2.31	
F_BARRCONS_09	09	87.47	2:00	82.61	7:00	85.36	4.86	75.66	3:00	73.55	7:00	74.81	2.11	75.57	3:00	73.26	7:00	74.64	2.31	
F_BARRCONS_10	10	87.47	2:00	82.61	7:00	85.36	4.86	75.66	3:00	73.55	7:00	74.81	2.11	75.57	3:00	73.25	7:00	74.64	2.31	
F_BARRCONS_11	11	87.47	2:00	82.61	7:00	85.36	4.86	75.66	3:00	73.55	7:00	74.81	2.11	75.57	3:00	73.25	7:00	74.64	2.31	
F_BARRCONS_12	12	87.47	2:00	82.61	7:00	85.36	4.86	75.66	3:00	73.55	7:00	74.81	2.11	75.57	3:00	73.25	7:00	74.64	2.32	
F_BARRCONS_13	13	87.47	2:00	82.60	7:00	85.36	4.87	75.66	3:00	73.78	7:00	74.90	1.89	75.58	3:00	73.28	7:00	74.65	2.30	
F_BARRCONS_14	14	87.47	2:00	82.60	7:00	85.36	4.87	75.66	3:00	73.75	7:00	74.89	1.91	75.58	3:00	73.28	7:00	74.65	2.30	
F_BARRCONS_15	15	87.47	2:00	82.60	7:00	85.36	4.87	75.66	3:00	73.73	7:00	74.88	1.93	75.58	3:00	73.28	7:00	74.65	2.30	
F_BARRCONS_16	16	87.47	2:00	82.60	7:00	85.36	4.87	75.66	3:00	73.72	7:00	74.88	1.94	75.58	3:00	73.28	7:00	74.65	2.30	
F_BARRCONS_17	17	87.47	2:00	82.61	7:00	85.36	4.87	75.66	3:00	73.71	7:00	74.87	1.96	75.58	3:00	73.28	7:00	74.66	2.30	
F_BARRCONS_18	18	87.47	2:00	82.61	7:00	85.36	4.87	75.66	3:00	73.70	7:00	74.87	1.97	75.58	3:00	73.28	7:00	74.66	2.30	
F_BARRCONS_19	19	87.47	2:00	82.61	7:00	85.36	4.86	75.66	3:00	73.68	7:00	74.86	1.98	75.58	3:00	73.28	7:00	74.66	2.30	
F_BARRCONS_20	20	87.47	2:00	82.61	7:00	85.36	4.87	75.66	3:00	73.67	7:00	74.86	1.99	75.57	3:00	73.28	7:00	74.65	2.30	
F_BARRCONS_21	21	87.47	2:00	82.60	7:00	85.35	4.87	75.66	3:00	73.65	7:00	74.85	2.01	75.57	3:00	73.27	7:00	74.65	2.30	
F_BARRCONS_22	22	87.47	2:00	82.60	7:00	85.35	4.87	75.66	3:00	73.64	7:00	74.85	2.02	75.57	3:00	73.27	7:00	74.65	2.31	
F_BARRCONS_23	23	87.47	2:00	82.60	7:00	85.35	4.87	75.66	3:00	73.63	7:00	74.84	2.03	75.57	3:00	73.26	7:00	74.65	2.31	
F_BARRCONS_25	25	87.47	2:00	82.60	7:00	85.35	4.87	75.66	3:00	73.61	7:00	74.83	2.05	75.57	3:00	73.26	7:00	74.64	2.31	
F_BARRCONS_24	24	87.47	2:00	82.60	7:00	85.35	4.87	75.66	3:00	73.62	7:00	74.84	2.04	75.57	3:00	73.26	7:00	74.65	2.31	
F_BARRCONS_26	26	87.47	2:00	82.60	7:00	85.35	4.87	75.66	3:00	73.60	7:00	74.83	2.06	75.57	3:00	73.26	7:00	74.64	2.31	
F_BARRCONS_27	27	87.47	2:00	82.60	7:00	85.35	4.87	75.66	3:00	73.59	7:00	74.83	2.07	75.57	3:00	73.25	7:00	74.64	2.31	
F_BARRCONS_28	28	87.47	2:00	82.60	7:00	85.35	4.87	75.66	3:00	73.58	7:00	74.82	2.08	75.57	3:00	73.25	7:00	74.64	2.32	
F_BARRCONS_29	29	87.47	2:00	82.60	7:00	85.35	4.87	75.66	3:00	73.58	7:00	74.82	2.08	75.57	3:00	73.25	7:00	74.64	2.32	
F_BARRCONS_30	30	87.47	2:00	82.60	7:00	85.35	4.87	75.66	3:00	73.57	7:00	74.82	2.09	75.57	3:00	73.25	7:00	74.64	2.31	
F_BARRCONS_31	31	87.47	2:00	82.60	7:00	85.35	4.87	75.66	3:00	73.57	7:00	74.82	2.09	75.57	3:00	73.25	7:00	74.64	2.31	
F_BARRCONS_32	32	87.47	2:00	82.60	7:00	85.35	4.87	75.66	3:00	73.56	7:00	74.82	2.09	75.57	3:00	73.25	7:00	74.64	2.31	
F_BARRCONS_33	33	87.47	2:00	82.60	7:00	85.35	4.87	75.66	3:00	73.56	7:00	74.81	2.10	75.57	3:00	73.25	7:00	74.64	2.31	
F_BARRCONS_34	34	87.47	2:00	82.62	7:00	85.36	4.85	75.66	3:00	73.55	7:00	74.81	2.11	75.57	3:00	73.25	7:00	74.64	2.31	
F_BARRCONS_35	35	87.47	2:00	82.64	7:00	85.36	4.83	75.66	3:00	73.55	7:00	74.81	2.11	75.57	3:00	73.25	7:00	74.64	2.31	
F_BARRCONS_36	36	87.47	2:00	82.63	7:00	85.36	4.84	75.66	3:00	73.55	7:00	74.81	2.11	75.57	3:00	73.25	7:00	74.64	2.32	
F_BARRCONS_37	37	87.47	2:00	82.63	7:00	85.36	4.84	75.66	3:00	73.55	7:00	74.81	2.11	75.57	3:00	73.25	7:00	74.64	2.32	
F_BARRCONS_38	38	87.47	2:00	82.63	7:00	85.36	4.85	75.66	3:00	73.55	7:00	74.81	2.11	75.57	3:00	73.25	7:00	74.64	2.32	
F_BARRCONS_39	39	87.47	2:00	82.62	7:00	85.36	4.85	75.66	3:00	73.54	7:00	74.81	2.11	75.57	3:00	73.25	7:00	74.64	2.32	
F_BARRCONS_40	40	87.47	2:00	82.61	7:00	85.36	4.86	75.66	3:00	73.54	7:00	74.81	2.11	75.57	3:00	73.25	7:00	74.64	2.32	
F_BARRCONS_41	41	87.47	2:00	82.61	7:00	85.36	4.86	75.66	3:00	73.54	7:00	74.81	2.11	75.57	3:00	73.25	7:00	74.64	2.32	
F_BARRCONS_42	42	87.47	2:00	82.61	7:00	85.36	4.86	75.66	3:00	73.54	7:00	74.81	2.11	75.57	3:00	73.25	7:00	74.64	2.32	
F_BARRCONS_43	43	87.47	2:00	82.62	7:00	85.36	4.85	75.66	3:00	73.54	7:00	74.81	2.11	75.57	3:00	73.25	7:00	74.64	2.32	
F_BARRCONS_44	44	87.47	2:00	82.62	7:00	85.36	4.85	75.66	3:00	73.58	7:00	74.82	2.08	75.57	3:00	73.26	7:00	74.64	2.31	
F_BARRCONS_45	45	87.47	2:00	82.62	7:00	85.36	4.85	75.66	3:00	73.56	7:00	74.82	2.10	75.57	3:00	73.26	7:00	74.64	2.31	
F_BARRCONS_46	46	87.47	2:00	82.62	7:00	85.36	4.85	75.66	3:00	73.56	7:00	74.81	2.10	75.57	3:00	73.25	7:00	74.64	2.31	

**BSDY Model Results (cont'd)**

MIN		75.7						75.6							75.6				
MAX		75.7						75.6							75.6				
Model Node ID	Figure Node ID	Servicing Alternative 2c						Servicing Alternative 2d						Servicing Alternative 3					
		Max Value (psi)	Max Time (hrs.)	Min Value (psi)	Min Time (hrs.)	Avg (psi)	Diff (psi)	Max Value (psi)	Max Time (hrs.)	Min Value (psi)	Min Time (hrs.)	Avg (psi)	Diff (psi)	Max Value (psi)	Max Time (hrs.)	Min Value (psi)	Min Time (hrs.)	Avg (psi)	Diff (psi)
F_BARRCONS_01	01	75.66	3:00	73.73	7:00	74.87	1.93	75.57	3:00	73.32	7:00	74.66	2.25	75.63	3:00	72.17	7:00	74.29	3.45
F_BARRCONS_02	02	75.66	3:00	73.70	7:00	74.86	1.95	75.57	3:00	73.31	7:00	74.66	2.26	75.63	3:00	72.14	7:00	74.28	3.49
F_BARRCONS_03	03	75.65	3:00	73.67	7:00	74.85	1.98	75.56	3:00	73.30	7:00	74.65	2.27	75.63	3:00	72.11	7:00	74.27	3.51
F_BARRCONS_04	04	75.65	3:00	73.66	7:00	74.84	2.00	75.56	3:00	73.29	7:00	74.65	2.27	75.62	3:00	72.09	7:00	74.26	3.53
F_BARRCONS_05	05	75.65	3:00	73.64	7:00	74.84	2.02	75.56	3:00	73.29	7:00	74.65	2.27	75.62	3:00	72.07	7:00	74.25	3.55
F_BARRCONS_06	06	75.65	3:00	73.60	7:00	74.82	2.05	75.56	3:00	73.28	7:00	74.64	2.28	75.62	3:00	72.03	7:00	74.23	3.59
F_BARRCONS_07	07	75.65	3:00	73.60	7:00	74.82	2.05	75.56	3:00	73.28	7:00	74.64	2.28	75.62	3:00	72.03	7:00	74.23	3.59
F_BARRCONS_08	08	75.65	3:00	73.60	7:00	74.82	2.05	75.56	3:00	73.28	7:00	74.64	2.28	75.62	3:00	72.03	7:00	74.23	3.60
F_BARRCONS_09	09	75.65	3:00	73.60	7:00	74.82	2.05	75.56	3:00	73.28	7:00	74.64	2.28	75.62	3:00	72.03	7:00	74.23	3.60
F_BARRCONS_10	10	75.65	3:00	73.60	7:00	74.82	2.06	75.56	3:00	73.28	7:00	74.64	2.28	75.62	3:00	72.02	7:00	74.23	3.60
F_BARRCONS_11	11	75.65	3:00	73.59	7:00	74.82	2.06	75.56	3:00	73.28	7:00	74.64	2.28	75.62	3:00	72.02	7:00	74.23	3.60
F_BARRCONS_12	12	75.65	3:00	73.59	7:00	74.82	2.06	75.56	3:00	73.27	7:00	74.64	2.28	75.62	3:00	72.02	7:00	74.23	3.60
F_BARRCONS_13	13	75.66	3:00	73.80	7:00	74.90	1.85	75.60	3:00	73.53	7:00	74.76	2.07	75.63	3:00	72.14	7:00	74.28	3.49
F_BARRCONS_14	14	75.66	3:00	73.78	7:00	74.89	1.88	75.59	3:00	73.47	7:00	74.73	2.12	75.63	3:00	72.14	7:00	74.28	3.49
F_BARRCONS_15	15	75.66	3:00	73.77	7:00	74.89	1.89	75.59	3:00	73.44	7:00	74.72	2.15	75.63	3:00	72.14	7:00	74.28	3.49
F_BARRCONS_16	16	75.66	3:00	73.76	7:00	74.88	1.90	75.58	3:00	73.41	7:00	74.70	2.17	75.63	3:00	72.14	7:00	74.28	3.49
F_BARRCONS_17	17	75.66	3:00	73.75	7:00	74.88	1.91	75.58	3:00	73.38	7:00	74.69	2.20	75.63	3:00	72.14	7:00	74.28	3.48
F_BARRCONS_18	18	75.66	3:00	73.74	7:00	74.87	1.92	75.57	3:00	73.35	7:00	74.68	2.22	75.63	3:00	72.14	7:00	74.28	3.48
F_BARRCONS_19	19	75.66	3:00	73.73	7:00	74.87	1.93	75.57	3:00	73.33	7:00	74.66	2.24	75.63	3:00	72.15	7:00	74.28	3.48
F_BARRCONS_20	20	75.66	3:00	73.71	7:00	74.87	1.94	75.57	3:00	73.32	7:00	74.66	2.25	75.63	3:00	72.13	7:00	74.27	3.50
F_BARRCONS_21	21	75.66	3:00	73.70	7:00	74.86	1.96	75.57	3:00	73.31	7:00	74.66	2.26	75.63	3:00	72.12	7:00	74.27	3.51
F_BARRCONS_22	22	75.66	3:00	73.68	7:00	74.85	1.97	75.57	3:00	73.30	7:00	74.65	2.26	75.62	3:00	72.10	7:00	74.26	3.52
F_BARRCONS_23	23	75.65	3:00	73.67	7:00	74.85	1.98	75.57	3:00	73.30	7:00	74.65	2.27	75.62	3:00	72.09	7:00	74.26	3.53
F_BARRCONS_25	25	75.65	3:00	73.65	7:00	74.84	2.00	75.56	3:00	73.29	7:00	74.65	2.27	75.62	3:00	72.07	7:00	74.25	3.55
F_BARRCONS_24	24	75.65	3:00	73.66	7:00	74.85	1.99	75.56	3:00	73.30	7:00	74.65	2.27	75.62	3:00	72.08	7:00	74.25	3.54
F_BARRCONS_26	26	75.65	3:00	73.64	7:00	74.84	2.01	75.56	3:00	73.29	7:00	74.65	2.27	75.62	3:00	72.06	7:00	74.25	3.56
F_BARRCONS_27	27	75.65	3:00	73.64	7:00	74.83	2.02	75.56	3:00	73.29	7:00	74.65	2.28	75.62	3:00	72.06	7:00	74.25	3.57
F_BARRCONS_28	28	75.65	3:00	73.63	7:00	74.83	2.02	75.56	3:00	73.28	7:00	74.64	2.28	75.62	3:00	72.05	7:00	74.24	3.57
F_BARRCONS_29	29	75.65	3:00	73.62	7:00	74.83	2.03	75.56	3:00	73.28	7:00	74.64	2.28	75.62	3:00	72.05	7:00	74.24	3.58
F_BARRCONS_30	30	75.65	3:00	73.62	7:00	74.83	2.04	75.56	3:00	73.28	7:00	74.64	2.28	75.62	3:00	72.04	7:00	74.24	3.58
F_BARRCONS_31	31	75.65	3:00	73.61	7:00	74.83	2.04	75.56	3:00	73.28	7:00	74.64	2.28	75.62	3:00	72.04	7:00	74.24	3.58
F_BARRCONS_32	32	75.65	3:00	73.61	7:00	74.82	2.04	75.56	3:00	73.28	7:00	74.64	2.28	75.62	3:00	72.04	7:00	74.24	3.59
F_BARRCONS_33	33	75.65	3:00	73.61	7:00	74.82	2.05	75.56	3:00	73.28	7:00	74.64	2.28	75.62	3:00	72.03	7:00	74.24	3.59
F_BARRCONS_34	34	75.65	3:00	73.60	7:00	74.82	2.05	75.56	3:00	73.28	7:00	74.64	2.28	75.62	3:00	72.03	7:00	74.23	3.60
F_BARRCONS_35	35	75.65	3:00	73.60	7:00	74.82	2.06	75.56	3:00	73.28	7:00	74.64	2.28	75.62	3:00	72.02	7:00	74.23	3.60
F_BARRCONS_36	36	75.65	3:00	73.59	7:00	74.82	2.06	75.56	3:00	73.28	7:00	74.64	2.28	75.62	3:00	72.02	7:00	74.23	3.60
F_BARRCONS_37	37	75.65	3:00	73.59	7:00	74.82	2.06	75.56	3:00	73.27	7:00	74.64	2.28	75.62	3:00	72.02	7:00	74.23	3.60
F_BARRCONS_38	38	75.65	3:00	73.59	7:00	74.82	2.06	75.56	3:00	73.27	7:00	74.64	2.28	75.62	3:00	72.02	7:00	74.23	3.60
F_BARRCONS_39	39	75.65	3:00	73.59	7:00	74.82	2.06	75.56	3:00	73.27	7:00	74.64	2.29	75.62	3:00	72.02	7:00	74.23	3.60
F_BARRCONS_40	40	75.65	3:00	73.59	7:00	74.82	2.06	75.56	3:00	73.27	7:00	74.64	2.28	75.62	3:00	72.02	7:00	74.23	3.60
F_BARRCONS_41	41	75.65	3:00	73.59	7:00	74.82	2.06	75.56	3:00	73.27	7:00	74.64	2.29	75.62	3:00	72.02	7:00	74.23	3.60
F_BARRCONS_42	42	75.65	3:00	73.59	7:00	74.82	2.06	75.56	3:00	73.27	7:00	74.64	2.29	75.62	3:00	72.02	7:00	74.23	3.60
F_BARRCONS_43	43	75.65	3:00	73.59	7:00	74.82	2.06	75.56	3:00	73.27	7:00	74.64	2.29	75.62	3:00	72.02	7:00	74.23	3.60
F_BARRCONS_44	44	75.65	3:00	73.62	7:00	74.83	2.03	75.56	3:00	73.28	7:00	74.64	2.28	75.62	3:00	72.05	7:00	74.24	3.57
F_BARRCONS_45	45	75.65	3:00	73.61	7:00	74.82	2.04	75.56	3:00	73.28	7:00	74.64	2.28	75.62	3:00	72.04	7:00	74.24	3.58
F_BARRCONS_46	46	75.65	3:00	73.60	7:00	74.82	2.05	75.56	3:00	73.28	7:00	74.64	2.28	75.62	3:00	72.03	7:00	74.24	3.59



**PKHR Model Results**

				51.9						63.6						61.3			
				51.9						64.0						61.6			
Model Node ID	Figure Node ID	Servicing Alternative 1						Servicing Alternative 2a						Servicing Alternative 2b					
		Max Value (psi)	Max Time (hrs.)	Min Value (psi)	Min Time (hrs.)	Avg (psi)	Diff (psi)	Max Value (psi)	Max Time (hrs.)	Min Value (psi)	Min Time (hrs.)	Avg (psi)	Diff (psi)	Max Value (psi)	Max Time (hrs.)	Min Value (psi)	Min Time (hrs.)	Avg (psi)	Diff (psi)
F_BARRCONS_01	01	86.63	0:00	51.91	22:00	75.81	34.73	75.56	3:00	63.93	20:00	72.35	11.63	75.47	3:00	61.59	20:00	71.64	13.88
F_BARRCONS_02	02	86.63	0:00	51.90	22:00	75.81	34.73	75.55	3:00	63.87	20:00	72.31	11.69	75.47	3:00	61.53	20:00	71.62	13.94
F_BARRCONS_03	03	86.63	0:00	51.90	22:00	75.80	34.74	75.55	3:00	63.81	20:00	72.27	11.74	75.46	3:00	61.47	20:00	71.60	13.99
F_BARRCONS_04	04	86.63	0:00	51.90	22:00	75.80	34.74	75.55	3:00	63.78	20:00	72.24	11.77	75.46	3:00	61.44	20:00	71.59	14.02
F_BARRCONS_05	05	86.63	0:00	51.89	22:00	75.80	34.74	75.54	3:00	63.73	20:00	72.21	11.81	75.46	3:00	61.40	20:00	71.58	14.06
F_BARRCONS_06	06	86.63	0:00	51.87	22:00	75.78	34.76	75.54	3:00	63.66	20:00	72.16	11.88	75.46	3:00	61.33	20:00	71.56	14.13
F_BARRCONS_07	07	86.63	0:00	51.87	22:00	75.78	34.76	75.54	3:00	63.65	20:00	72.16	11.88	75.46	3:00	61.32	20:00	71.57	14.14
F_BARRCONS_08	08	86.63	0:00	51.87	22:00	75.78	34.76	75.54	3:00	63.65	20:00	72.16	11.88	75.46	3:00	61.32	20:00	71.57	14.14
F_BARRCONS_09	09	86.63	0:00	51.88	22:00	75.79	34.75	75.54	3:00	63.65	20:00	72.15	11.89	75.46	3:00	61.32	20:00	71.57	14.14
F_BARRCONS_10	10	86.63	0:00	51.88	22:00	75.79	34.75	75.53	3:00	63.65	20:00	72.15	11.89	75.46	3:00	61.32	20:00	71.56	14.14
F_BARRCONS_11	11	86.63	0:00	51.88	22:00	75.79	34.75	75.53	3:00	63.64	20:00	72.15	11.89	75.46	3:00	61.31	20:00	71.56	14.15
F_BARRCONS_12	12	86.63	0:00	51.88	22:00	75.79	34.75	75.53	3:00	63.64	20:00	72.15	11.90	75.46	3:00	61.31	20:00	71.56	14.15
F_BARRCONS_13	13	86.63	0:00	51.88	22:00	75.79	34.75	75.57	3:00	64.04	20:00	72.48	11.54	75.47	3:00	61.52	20:00	71.61	13.94
F_BARRCONS_14	14	86.63	0:00	51.88	22:00	75.79	34.75	75.57	3:00	64.00	20:00	72.44	11.57	75.47	3:00	61.52	20:00	71.61	13.94
F_BARRCONS_15	15	86.63	0:00	51.88	22:00	75.79	34.75	75.57	3:00	63.98	20:00	72.42	11.59	75.47	3:00	61.52	20:00	71.61	13.94
F_BARRCONS_16	16	86.63	0:00	51.88	22:00	75.79	34.75	75.56	3:00	63.96	20:00	72.40	11.60	75.47	3:00	61.53	20:00	71.61	13.94
F_BARRCONS_17	17	86.63	0:00	51.88	22:00	75.79	34.75	75.56	3:00	63.95	20:00	72.38	11.62	75.47	3:00	61.53	20:00	71.61	13.94
F_BARRCONS_18	18	86.63	0:00	51.89	22:00	75.79	34.74	75.56	3:00	63.93	20:00	72.36	11.63	75.47	3:00	61.53	20:00	71.62	13.94
F_BARRCONS_19	19	86.63	0:00	51.89	22:00	75.80	34.74	75.56	3:00	63.92	20:00	72.35	11.64	75.47	3:00	61.53	20:00	71.62	13.93
F_BARRCONS_20	20	86.63	0:00	51.88	22:00	75.79	34.75	75.56	3:00	63.89	20:00	72.32	11.67	75.47	3:00	61.51	20:00	71.61	13.96
F_BARRCONS_21	21	86.63	0:00	51.88	22:00	75.79	34.75	75.55	3:00	63.86	20:00	72.30	11.70	75.46	3:00	61.48	20:00	71.60	13.98
F_BARRCONS_22	22	86.63	0:00	51.87	22:00	75.78	34.75	75.55	3:00	63.83	20:00	72.28	11.72	75.46	3:00	61.46	20:00	71.59	14.01
F_BARRCONS_23	23	86.63	0:00	51.87	22:00	75.78	34.76	75.55	3:00	63.80	20:00	72.26	11.75	75.46	3:00	61.44	20:00	71.59	14.03
F_BARRCONS_25	25	86.63	0:00	51.87	22:00	75.78	34.76	75.54	3:00	63.76	20:00	72.23	11.78	75.46	3:00	61.40	20:00	71.58	14.06
F_BARRCONS_24	24	86.63	0:00	51.87	22:00	75.78	34.76	75.55	3:00	63.78	20:00	72.25	11.77	75.46	3:00	61.42	20:00	71.58	14.04
F_BARRCONS_26	26	86.63	0:00	51.87	22:00	75.78	34.76	75.54	3:00	63.74	20:00	72.22	11.80	75.46	3:00	61.39	20:00	71.57	14.07
F_BARRCONS_27	27	86.63	0:00	51.87	22:00	75.78	34.76	75.54	3:00	63.73	20:00	72.21	11.82	75.46	3:00	61.37	20:00	71.57	14.09
F_BARRCONS_28	28	86.63	0:00	51.87	22:00	75.78	34.76	75.54	3:00	63.71	20:00	72.20	11.83	75.46	3:00	61.36	20:00	71.57	14.10
F_BARRCONS_29	29	86.63	0:00	51.87	22:00	75.78	34.76	75.54	3:00	63.70	20:00	72.19	11.84	75.46	3:00	61.35	20:00	71.57	14.11
F_BARRCONS_30	30	86.63	0:00	51.87	22:00	75.78	34.76	75.54	3:00	63.69	20:00	72.18	11.85	75.46	3:00	61.35	20:00	71.57	14.11
F_BARRCONS_31	31	86.63	0:00	51.87	22:00	75.78	34.76	75.54	3:00	63.68	20:00	72.18	11.86	75.46	3:00	61.34	20:00	71.56	14.12
F_BARRCONS_32	32	86.63	0:00	51.87	22:00	75.78	34.76	75.54	3:00	63.67	20:00	72.17	11.86	75.46	3:00	61.34	20:00	71.56	14.12
F_BARRCONS_33	33	86.63	0:00	51.87	22:00	75.78	34.76	75.54	3:00	63.67	20:00	72.17	11.87	75.46	3:00	61.33	20:00	71.56	14.13
F_BARRCONS_34	34	86.63	0:00	51.90	22:00	75.80	34.74	75.54	3:00	63.65	20:00	72.15	11.88	75.46	3:00	61.32	20:00	71.57	14.14
F_BARRCONS_35	35	86.64	0:00	51.91	22:00	75.82	34.73	75.53	3:00	63.65	20:00	72.15	11.89	75.46	3:00	61.32	20:00	71.56	14.14
F_BARRCONS_36	36	86.64	0:00	51.90	22:00	75.81	34.73	75.53	3:00	63.64	20:00	72.15	11.89	75.46	3:00	61.31	20:00	71.56	14.15
F_BARRCONS_37	37	86.64	0:00	51.90	22:00	75.81	34.74	75.53	3:00	63.64	20:00	72.15	11.89	75.46	3:00	61.31	20:00	71.56	14.15
F_BARRCONS_38	38	86.64	0:00	51.89	22:00	75.80	34.74	75.53	3:00	63.64	20:00	72.15	11.90	75.46	3:00	61.31	20:00	71.56	14.15
F_BARRCONS_39	39	86.63	0:00	51.89	22:00	75.80	34.75	75.53	3:00	63.64	20:00	72.14	11.90	75.46	3:00	61.31	20:00	71.56	14.15
F_BARRCONS_40	40	86.63	0:00	51.88	22:00	75.79	34.75	75.53	3:00	63.64	20:00	72.15	11.90	75.46	3:00	61.31	20:00	71.56	14.15
F_BARRCONS_41	41	86.63	0:00	51.88	22:00	75.79	34.75	75.53	3:00	63.64	20:00	72.14	11.90	75.46	3:00	61.31	20:00	71.56	14.15
F_BARRCONS_42	42	86.63	0:00	51.88	22:00	75.79	34.75	75.53	3:00	63.64	20:00	72.14	11.90	75.46	3:00	61.31	20:00	71.56	14.15
F_BARRCONS_43	43	86.63	0:00	51.89	22:00	75.80	34.75	75.53	3:00	63.64	20:00	72.14	11.90	75.46	3:00	61.31	20:00	71.56	14.15
F_BARRCONS_44	44	86.63	0:00	51.89	22:00	75.80	34.74	75.54	3:00	63.70	20:00	72.19	11.84	75.46	3:00	61.37	20:00	71.58	14.09
F_BARRCONS_45	45	86.63	0:00	51.89	22:00	75.80	34.74	75.54	3:00	63.67	20:00	72.17	11.86	75.46	3:00	61.34	20:00	71.57	14.12
F_BARRCONS_46	46	86.63	0:00	51.89	22:00	75.80	34.74	75.54	3:00	63.66	20:00	72.16	11.87	75.46	3:00	61.33	20:00	71.57	14.13

**PKHR Model Results (cont'd)**

		MIN		63.6				61.2						66.7					
		MAX		64.0				62.4						66.9					
Model Node ID	Figure Node ID	Servicing Alternative 2c						Servicing Alternative 2d						Servicing Alternative 3					
		Max Value (psi)	Max Time (hrs.)	Min Value (psi)	Min Time (hrs.)	Avg (psi)	Diff (psi)	Max Value (psi)	Max Time (hrs.)	Min Value (psi)	Min Time (hrs.)	Avg (psi)	Diff (psi)	Max Value (psi)	Max Time (hrs.)	Min Value (psi)	Min Time (hrs.)	Avg (psi)	Diff (psi)
F_BARRCONS_01	01	75.56	3:00	63.93	20:00	72.41	11.63	75.47	3:00	61.52	20:00	71.67	13.95	75.30	3:00	66.72	20:00	70.77	8.58
F_BARRCONS_02	02	75.56	3:00	63.87	20:00	72.37	11.69	75.46	3:00	61.46	20:00	71.65	14.01	75.29	3:00	66.73	20:00	70.73	8.57
F_BARRCONS_03	03	75.55	3:00	63.81	20:00	72.33	11.74	75.46	3:00	61.40	20:00	71.63	14.06	75.29	3:00	66.74	20:00	70.70	8.55
F_BARRCONS_04	04	75.55	3:00	63.78	20:00	72.31	11.77	75.46	3:00	61.37	20:00	71.62	14.09	75.28	3:00	66.74	20:00	70.68	8.54
F_BARRCONS_05	05	75.54	3:00	63.73	20:00	72.28	11.81	75.46	3:00	61.33	20:00	71.61	14.13	75.28	3:00	66.76	20:00	70.65	8.52
F_BARRCONS_06	06	75.54	3:00	63.66	20:00	72.22	11.88	75.46	3:00	61.26	20:00	71.60	14.20	75.27	3:00	66.74	20:00	70.60	8.53
F_BARRCONS_07	07	75.54	3:00	63.66	20:00	72.22	11.88	75.46	3:00	61.25	20:00	71.60	14.20	75.27	3:00	66.75	20:00	70.60	8.52
F_BARRCONS_08	08	75.54	3:00	63.65	20:00	72.22	11.88	75.46	3:00	61.25	20:00	71.60	14.21	75.27	3:00	66.76	20:00	70.60	8.51
F_BARRCONS_09	09	75.54	3:00	63.65	20:00	72.22	11.89	75.46	3:00	61.25	20:00	71.60	14.21	75.27	3:00	66.78	20:00	70.60	8.49
F_BARRCONS_10	10	75.54	3:00	63.65	20:00	72.22	11.89	75.46	3:00	61.24	20:00	71.59	14.21	75.27	3:00	66.78	20:00	70.60	8.49
F_BARRCONS_11	11	75.54	3:00	63.64	20:00	72.21	11.89	75.46	3:00	61.24	20:00	71.59	14.22	75.27	3:00	66.78	20:00	70.60	8.49
F_BARRCONS_12	12	75.54	3:00	63.64	20:00	72.21	11.90	75.46	3:00	61.24	20:00	71.59	14.22	75.27	3:00	66.78	20:00	70.60	8.49
F_BARRCONS_13	13	75.57	3:00	64.02	20:00	72.52	11.55	75.51	3:00	62.39	20:00	72.01	13.12	75.29	3:00	66.70	20:00	70.73	8.59
F_BARRCONS_14	14	75.57	3:00	63.99	20:00	72.48	11.58	75.50	3:00	62.16	20:00	71.92	13.34	75.29	3:00	66.70	20:00	70.73	8.59
F_BARRCONS_15	15	75.57	3:00	63.97	20:00	72.46	11.60	75.49	3:00	62.02	20:00	71.86	13.47	75.29	3:00	66.70	20:00	70.73	8.59
F_BARRCONS_16	16	75.57	3:00	63.95	20:00	72.45	11.61	75.48	3:00	61.90	20:00	71.82	13.59	75.29	3:00	66.70	20:00	70.73	8.59
F_BARRCONS_17	17	75.56	3:00	63.94	20:00	72.43	11.62	75.48	3:00	61.78	20:00	71.77	13.70	75.29	3:00	66.71	20:00	70.73	8.59
F_BARRCONS_18	18	75.56	3:00	63.93	20:00	72.42	11.63	75.47	3:00	61.67	20:00	71.73	13.81	75.29	3:00	66.71	20:00	70.73	8.59
F_BARRCONS_19	19	75.56	3:00	63.92	20:00	72.41	11.64	75.47	3:00	61.55	20:00	71.68	13.92	75.29	3:00	66.71	20:00	70.73	8.58
F_BARRCONS_20	20	75.56	3:00	63.89	20:00	72.39	11.67	75.47	3:00	61.51	20:00	71.67	13.96	75.29	3:00	66.71	20:00	70.72	8.58
F_BARRCONS_21	21	75.56	3:00	63.86	20:00	72.37	11.70	75.46	3:00	61.48	20:00	71.66	13.99	75.29	3:00	66.71	20:00	70.70	8.58
F_BARRCONS_22	22	75.55	3:00	63.83	20:00	72.34	11.73	75.46	3:00	61.45	20:00	71.64	14.02	75.29	3:00	66.71	20:00	70.68	8.58
F_BARRCONS_23	23	75.55	3:00	63.80	20:00	72.33	11.75	75.46	3:00	61.42	20:00	71.64	14.04	75.28	3:00	66.71	20:00	70.67	8.58
F_BARRCONS_25	25	75.55	3:00	63.76	20:00	72.30	11.79	75.46	3:00	61.37	20:00	71.62	14.09	75.28	3:00	66.71	20:00	70.65	8.57
F_BARRCONS_24	24	75.55	3:00	63.78	20:00	72.31	11.77	75.46	3:00	61.40	20:00	71.63	14.06	75.28	3:00	66.71	20:00	70.66	8.58
F_BARRCONS_26	26	75.55	3:00	63.74	20:00	72.28	11.80	75.46	3:00	61.35	20:00	71.62	14.11	75.28	3:00	66.71	20:00	70.64	8.57
F_BARRCONS_27	27	75.54	3:00	63.73	20:00	72.27	11.82	75.46	3:00	61.34	20:00	71.61	14.12	75.28	3:00	66.71	20:00	70.63	8.57
F_BARRCONS_28	28	75.54	3:00	63.71	20:00	72.26	11.83	75.46	3:00	61.32	20:00	71.61	14.14	75.28	3:00	66.71	20:00	70.63	8.57
F_BARRCONS_29	29	75.54	3:00	63.70	20:00	72.25	11.84	75.46	3:00	61.31	20:00	71.60	14.15	75.28	3:00	66.71	20:00	70.62	8.57
F_BARRCONS_30	30	75.54	3:00	63.69	20:00	72.25	11.85	75.46	3:00	61.30	20:00	71.60	14.16	75.27	3:00	66.71	20:00	70.62	8.56
F_BARRCONS_31	31	75.54	3:00	63.68	20:00	72.24	11.86	75.46	3:00	61.29	20:00	71.60	14.17	75.27	3:00	66.72	20:00	70.61	8.56
F_BARRCONS_32	32	75.54	3:00	63.68	20:00	72.24	11.86	75.46	3:00	61.28	20:00	71.60	14.18	75.27	3:00	66.72	20:00	70.61	8.55
F_BARRCONS_33	33	75.54	3:00	63.67	20:00	72.23	11.87	75.46	3:00	61.27	20:00	71.60	14.19	75.27	3:00	66.73	20:00	70.61	8.55
F_BARRCONS_34	34	75.54	3:00	63.65	20:00	72.22	11.89	75.46	3:00	61.25	20:00	71.59	14.21	75.27	3:00	66.81	20:00	70.61	8.46
F_BARRCONS_35	35	75.54	3:00	63.65	20:00	72.22	11.89	75.46	3:00	61.24	20:00	71.59	14.21	75.27	3:00	66.88	20:00	70.61	8.39
F_BARRCONS_36	36	75.54	3:00	63.64	20:00	72.21	11.89	75.46	3:00	61.24	20:00	71.59	14.22	75.27	3:00	66.86	20:00	70.60	8.41
F_BARRCONS_37	37	75.54	3:00	63.64	20:00	72.21	11.90	75.46	3:00	61.24	20:00	71.59	14.22	75.27	3:00	66.85	20:00	70.60	8.42
F_BARRCONS_38	38	75.54	3:00	63.64	20:00	72.21	11.90	75.46	3:00	61.23	20:00	71.59	14.22	75.27	3:00	66.84	20:00	70.60	8.43
F_BARRCONS_39	39	75.54	3:00	63.64	20:00	72.21	11.90	75.46	3:00	61.23	20:00	71.58	14.22	75.27	3:00	66.83	20:00	70.60	8.44
F_BARRCONS_40	40	75.54	3:00	63.64	20:00	72.21	11.90	75.46	3:00	61.23	20:00	71.59	14.22	75.27	3:00	66.78	20:00	70.60	8.49
F_BARRCONS_41	41	75.54	3:00	63.64	20:00	72.21	11.90	75.46	3:00	61.23	20:00	71.58	14.22	75.27	3:00	66.79	20:00	70.59	8.48
F_BARRCONS_42	42	75.54	3:00	63.64	20:00	72.21	11.90	75.46	3:00	61.23	20:00	71.58	14.22	75.27	3:00	66.80	20:00	70.59	8.47
F_BARRCONS_43	43	75.54	3:00	63.64	20:00	72.21	11.90	75.46	3:00	61.23	20:00	71.58	14.22	75.27	3:00	66.82	20:00	70.60	8.45
F_BARRCONS_44	44	75.54	3:00	63.70	20:00	72.25	11.84	75.46	3:00	61.30	20:00	71.60	14.16	75.28	3:00	66.77	20:00	70.63	8.51
F_BARRCONS_45	45	75.54	3:00	63.67	20:00	72.23	11.87	75.46	3:00	61.27	20:00	71.60	14.19	75.27	3:00	66.79	20:00	70.62	8.49
F_BARRCONS_46	46	75.54	3:00	63.66	20:00	72.23	11.88	75.46	3:00	61.26	20:00	71.60	14.20	75.27	3:00	66.80	20:00	70.61	8.47

MXDY+FF Model Results

		303.0																		218.8		236.1	
		492.7																		396.5		333.3	
		Servicing Alternative 1									Servicing Alternative 2a						Servicing Alternative 2b						
Model Node ID	Figure Node ID	Static Demand @ 6:00 (L/s)	Static Pressure @ 6:00 (psi)	Static Head @ 6:00 (m)	Fire-Flow Demand (L/s)	Residual Pressure (psi)	Available Flow at Hydrant (L/s)	Available Flow Pressure (psi)	Static Demand @ 6:00 (L/s)	Static Pressure @ 6:00 (psi)	Static Head @ 6:00 (m)	Fire-Flow Demand (L/s)	Residual Pressure (psi)	Available Flow at Hydrant (L/s)	Available Flow Pressure (psi)	Static Demand @ 6:00 (L/s)	Static Pressure @ 6:00 (psi)	Static Head @ 6:00 (m)	Fire-Flow Demand (L/s)	Residual Pressure (psi)	Available Flow at Hydrant (L/s)	Available Flow Pressure (psi)	
F BARRCONS 01	01	1.23	82.45	151.40	217.00	65.22	492.66	20.00	1.23	73.02	144.77	217.00	47.82	348.72	20.00	1.23	72.61	144.48	217.00	44.71	324.95	20.00	
F BARRCONS 02	02	1.23	82.44	151.39	217.00	62.16	438.32	20.00	1.23	72.93	144.70	217.00	42.43	307.95	20.00	1.23	72.60	144.47	217.00	42.21	307.03	20.00	
F BARRCONS 03	03	1.23	82.43	151.39	217.00	60.42	414.21	20.00	1.23	72.85	144.65	217.00	38.66	286.14	20.00	1.23	72.58	144.46	217.00	40.63	297.16	20.00	
F BARRCONS 04	04	1.23	82.43	151.39	217.00	59.86	407.27	20.00	1.23	72.80	144.61	217.00	36.67	276.21	20.00	1.23	72.58	144.45	217.00	40.05	293.76	20.00	
F BARRCONS 05	05	1.23	82.43	151.39	217.00	59.87	407.38	20.00	1.23	72.74	144.57	217.00	34.42	266.07	20.00	1.23	72.57	144.45	217.00	39.91	292.95	20.00	
F BARRCONS 06	06	1.23	82.38	151.35	217.00	59.74	408.68	20.00	1.23	72.64	144.50	217.00	31.89	255.93	20.00	1.23	72.56	144.44	217.00	41.94	305.86	20.00	
F BARRCONS 07	07	1.23	82.39	151.35	217.00	60.61	419.49	20.00	1.23	72.63	144.49	217.00	31.56	254.65	20.00	1.23	72.56	144.44	217.00	43.06	313.45	20.00	
F BARRCONS 08	08	1.23	82.39	151.36	217.00	61.37	429.79	20.00	1.23	72.63	144.49	217.00	31.38	253.98	20.00	1.23	72.57	144.45	217.00	44.04	320.51	20.00	
F BARRCONS 09	09	1.23	82.40	151.36	217.00	62.66	448.88	20.00	1.23	72.62	144.49	217.00	31.22	253.41	20.00	1.23	72.58	144.45	217.00	45.68	333.33	20.00	
F BARRCONS 10	10	1.23	82.40	151.36	217.00	60.88	422.35	20.00	1.23	72.62	144.48	217.00	29.02	245.21	20.00	1.23	72.57	144.45	217.00	43.22	314.36	20.00	
F BARRCONS 11	11	1.23	82.40	151.36	217.00	58.77	396.01	20.00	1.23	72.61	144.48	217.00	26.50	236.73	20.00	1.23	72.56	144.44	217.00	40.57	296.97	20.00	
F BARRCONS 12	12	1.23	82.40	151.36	217.00	56.46	372.06	20.00	1.23	72.61	144.48	217.00	23.77	228.42	20.00	1.23	72.56	144.44	217.00	37.75	281.20	20.00	
F BARRCONS 13	13	1.23	82.40	151.37	217.00	46.56	303.01	20.00	1.23	73.36	145.01	217.00	52.91	396.48	20.00	1.23	72.57	144.45	217.00	26.45	236.07	20.00	
F BARRCONS 14	14	1.23	82.40	151.37	217.00	50.78	327.64	20.00	1.23	73.26	144.93	217.00	51.39	380.54	20.00	1.23	72.57	144.45	217.00	30.67	250.32	20.00	
F BARRCONS 15	15	1.23	82.40	151.37	217.00	53.30	345.49	20.00	1.23	73.20	144.89	217.00	50.58	372.69	20.00	1.23	72.57	144.45	217.00	33.19	260.19	20.00	
F BARRCONS 16	16	1.23	82.40	151.37	217.00	55.74	365.66	20.00	1.23	73.15	144.86	217.00	49.87	366.14	20.00	1.23	72.57	144.45	217.00	35.63	270.88	20.00	
F BARRCONS 17	17	1.23	82.41	151.37	217.00	58.28	390.68	20.00	1.23	73.10	144.82	217.00	49.19	360.24	20.00	1.23	72.57	144.45	217.00	38.17	283.45	20.00	
F BARRCONS 18	18	1.23	82.41	151.37	217.00	60.70	419.58	20.00	1.23	73.06	144.79	217.00	48.61	355.39	20.00	1.23	72.58	144.45	217.00	40.59	297.10	20.00	
F BARRCONS 19	19	1.23	82.42	151.37	217.00	63.56	463.19	20.00	1.23	73.02	144.76	217.00	48.00	350.45	20.00	1.23	72.58	144.46	217.00	43.45	315.98	20.00	
F BARRCONS 20	20	1.23	82.40	151.37	217.00	62.44	445.23	20.00	1.23	72.97	144.73	217.00	45.79	332.15	20.00	1.23	72.57	144.45	217.00	42.59	310.07	20.00	
F BARRCONS 21	21	1.23	82.40	151.36	217.00	61.45	430.76	20.00	1.23	72.93	144.70	217.00	43.90	318.24	20.00	1.23	72.56	144.44	217.00	41.81	304.98	20.00	
F BARRCONS 22	22	1.23	82.39	151.36	217.00	60.57	419.04	20.00	1.23	72.88	144.67	217.00	42.20	306.94	20.00	1.23	72.56	144.44	217.00	41.12	300.66	20.00	
F BARRCONS 23	23	1.23	82.38	151.35	217.00	59.90	410.67	20.00	1.23	72.85	144.65	217.00	40.83	298.60	20.00	1.23	72.55	144.44	217.00	40.59	297.50	20.00	
F BARRCONS 24	24	1.23	82.38	151.35	217.00	59.33	403.87	20.00	1.23	72.82	144.62	217.00	39.57	291.43	20.00	1.23	72.55	144.43	217.00	40.16	294.91	20.00	
F BARRCONS 25	25	1.23	82.38	151.35	217.00	58.86	398.54	20.00	1.23	72.79	144.60	217.00	38.43	285.31	20.00	1.23	72.55	144.43	217.00	39.81	292.91	20.00	
F BARRCONS 26	26	1.23	82.38	151.35	217.00	58.48	394.41	20.00	1.23	72.76	144.58	217.00	37.35	279.87	20.00	1.23	72.55	144.43	217.00	39.55	291.44	20.00	
F BARRCONS 27	27	1.23	82.37	151.35	217.00	58.23	391.67	20.00	1.23	72.74	144.57	217.00	36.43	275.40	20.00	1.23	72.55	144.43	217.00	39.40	290.58	20.00	
F BARRCONS 28	28	1.23	82.37	151.35	217.00	58.08	390.07	20.00	1.23	72.72	144.55	217.00	35.59	271.50	20.00	1.23	72.55	144.43	217.00	39.34	290.25	20.00	
F BARRCONS 29	29	1.23	82.37	151.35	217.00	58.03	389.50	20.00	1.23	72.70	144.54	217.00	34.82	268.03	20.00	1.23	72.55	144.43	217.00	39.39	290.50	20.00	
F BARRCONS 30	30	1.23	82.37	151.35	217.00	58.07	389.96	20.00	1.23	72.68	144.53	217.00	34.17	265.20	20.00	1.23	72.55	144.43	217.00	39.53	291.29	20.00	
F BARRCONS 31	31	1.23	82.37	151.35	217.00	58.21	391.38	20.00	1.23	72.67	144.52	217.00	33.59	262.75	20.00	1.23	72.55	144.43	217.00	39.78	292.70	20.00	
F BARRCONS 32	32	1.23	82.38	151.35	217.00	58.45	393.89	20.00	1.23	72.66	144.51	217.00	33.06	260.58	20.00	1.23	72.55	144.43	217.00	40.14	294.83	20.00	
F BARRCONS 33	33	1.23	82.38	151.35	217.00	58.79	397.66	20.00	1.23	72.65	144.51	217.00	32.60	258.70	20.00	1.23	72.55	144.43	217.00	40.64	297.78	20.00	
F BARRCONS 34	34	1.23	82.43	151.39	217.00	64.31	475.90	20.00	1.23	72.63	144.49	217.00	31.29	253.65	20.00	1.23	72.56	144.44	217.00	43.76	318.55	20.00	
F BARRCONS 35	35	1.23	82.46	151.41	217.00	64.94	486.74	20.00	1.23	72.62	144.48	217.00	28.93	244.89	20.00	1.23	72.56	144.44	217.00	41.72	304.38	20.00	
F BARRCONS 36	36	1.23	82.45	151.40	217.00	62.29	440.70	20.00	1.23	72.61	144.48	217.00	26.94	238.15	20.00	1.23	72.55	144.44	217.00	39.94	293.44	20.00	
F BARRCONS 37	37	1.23	82.44	151.39	217.00	60.38	414.33	20.00	1.23	72.61	144.48	217.00	25.40	233.27	20.00	1.23	72.55	144.44	217.00	38.54	285.60	20.00	
F BARRCONS 38	38	1.23	82.43	151.38	217.00	58.60	393.27	20.00	1.23	72.61	144.47	217.00	23.92	228.85	20.00	1.23	72.55	144.43	217.00	37.20	278.57	20.00	
F BARRCONS 39	39	1.23	82.42	151.38	217.00	56.93	376.14	20.00	1.23	72.60	144.47	217.00	22.53	224.91	20.00	1.23	72.55	144.43	217.00	35.94	272.42	20.00	
F BARRCONS 40	40	1.23	82.40	151.36	217.00	55.06	359.46	20.00	1.23	72.61	144.47	217.00	22.09	223.70	20.00	1.23	72.55	144.44	217.00	36.00	272.60	20.00	
F BARRCONS 41	41	1.23	82.40	151.36	217.00	53.85	349.45	20.00	1.23	72.60	144.47	217.00	20.44	219.35	20.00	1.23	72.55	144.43	217.00	34.25	264.73	20.00	
F BARRCONS 42	42	1.23	82.41	151.37	217.00	53.93	350.01	20.00	1.23	72.60	144.47	217.00	20.23	218.80	20.00	1.23	72.55	144.43	217.00	33.95	263.41	20.00	
F BARRCONS 43	43	1.23	82.42	151.37	217.00	55.54	363.30	20.00	1.23	72.60	144.47	217.00	21.38	221.81	20.00	1.23	72.55	144.43	217.00	34.91	267.68	20.00	
F BARRCONS 44	44	1.23	82.43	151.39	217.00	60.56	416.31	20.00	1.23	72.70	144.54	217.00	32.99	260.16	20.00	1.23	72.57	144.45	217.00	40.46	296.30	20.00	
F BARRCONS 45	45	1.23	82.43	151.39	217.00	61.91	435.13	20.00	1.23	72.66	144.51	217.00	31.98	256.22	20.00	1.23	72.56	144.45	217.00	41.65	303.81	20.00	
F BARRCONS 46	46	1.23	82.43	151.39	217.00	62.94	451.40	20.00	1.23	72.64	144.50	217.00	31.59	254.74	20.00	1.23	72.56	144.44	217.00	42.57	309.97	20.00	

MXDY+FF Model Results (cont'd)

		235.1																	281.2																	274.7																
		438.9																	411.4																	539.8																
Model Node ID	Figure Node ID	Servicing Alternative 2c							Servicing Alternative 2d							Servicing Alternative 3																																				
		Static Demand @ 6:00 (L/s)	Static Pressure @ 6:00 (psi)	Static Head @ 6:00 (m)	Fire-Flow Demand (L/s)	Residual Pressure (psi)	Available Flow at Hydrant (L/s)	Available Flow Pressure (psi)	Static Demand @ 6:00 (L/s)	Static Pressure @ 6:00 (psi)	Static Head @ 6:00 (m)	Fire-Flow Demand (L/s)	Residual Pressure (psi)	Available Flow at Hydrant (L/s)	Available Flow Pressure (psi)	Static Demand @ 6:00 (L/s)	Static Pressure @ 6:00 (psi)	Static Head @ 6:00 (m)	Fire-Flow Demand (L/s)	Residual Pressure (psi)	Available Flow at Hydrant (L/s)	Available Flow Pressure (psi)																														
F BARRCONS 01	01	1.23	73.27	144.94	217.00	53.88	411.59	20.00	1.23	72.83	144.63	217.00	48.89	357.13	20.00	1.23	68.30	141.44	217.00	54.20	443.36	20.00																														
F BARRCONS 02	02	1.23	73.19	144.88	217.00	48.40	350.55	20.00	1.23	72.81	144.62	217.00	46.37	334.36	20.00	1.23	68.20	141.38	217.00	52.58	417.07	20.00																														
F BARRCONS 03	03	1.23	73.10	144.82	217.00	44.60	320.45	20.00	1.23	72.79	144.60	217.00	44.81	322.29	20.00	1.23	68.11	141.31	217.00	51.74	404.95	20.00																														
F BARRCONS 04	04	1.23	73.06	144.79	217.00	42.59	307.23	20.00	1.23	72.78	144.60	217.00	44.28	318.41	20.00	1.23	68.06	141.28	217.00	51.61	403.52	20.00																														
F BARRCONS 05	05	1.23	72.99	144.75	217.00	40.33	294.01	20.00	1.23	72.78	144.59	217.00	44.23	318.14	20.00	1.23	67.99	141.23	217.00	52.07	408.90	20.00																														
F BARRCONS 06	06	1.23	72.89	144.67	217.00	37.78	281.12	20.00	1.23	72.77	144.59	217.00	46.53	336.61	20.00	1.23	67.87	141.14	217.00	52.49	416.19	20.00																														
F BARRCONS 07	07	1.23	72.88	144.67	217.00	37.45	279.52	20.00	1.23	72.77	144.59	217.00	47.49	344.99	20.00	1.23	67.87	141.14	217.00	53.53	430.30	20.00																														
F BARRCONS 08	08	1.23	72.88	144.67	217.00	37.27	278.69	20.00	1.23	72.78	144.59	217.00	48.33	352.86	20.00	1.23	67.86	141.14	217.00	54.47	444.31	20.00																														
F BARRCONS 09	09	1.23	72.88	144.66	217.00	37.11	277.99	20.00	1.23	72.78	144.60	217.00	49.74	367.17	20.00	1.23	67.86	141.14	217.00	56.10	471.46	20.00																														
F BARRCONS 10	10	1.23	72.87	144.66	217.00	34.91	267.61	20.00	1.23	72.77	144.59	217.00	47.29	343.07	20.00	1.23	67.86	141.13	217.00	54.47	442.40	20.00																														
F BARRCONS 11	11	1.23	72.87	144.66	217.00	32.39	257.01	20.00	1.23	72.77	144.59	217.00	44.64	321.43	20.00	1.23	67.85	141.13	217.00	52.50	413.56	20.00																														
F BARRCONS 12	12	1.23	72.86	144.65	217.00	29.66	246.78	20.00	1.23	72.76	144.58	217.00	41.82	302.25	20.00	1.23	67.84	141.12	217.00	50.35	387.47	20.00																														
F BARRCONS 13	13	1.23	73.53	145.12	217.00	56.33	438.89	20.00	1.23	73.23	144.91	217.00	54.17	411.41	20.00	1.23	68.20	141.38	217.00	36.17	274.69	20.00																														
F BARRCONS 14	14	1.23	73.45	145.07	217.00	55.37	426.51	20.00	1.23	73.11	144.83	217.00	52.87	396.55	20.00	1.23	68.20	141.38	217.00	40.39	297.87	20.00																														
F BARRCONS 15	15	1.23	73.40	145.03	217.00	54.90	420.96	20.00	1.23	73.05	144.78	217.00	52.19	389.38	20.00	1.23	68.20	141.38	217.00	42.91	314.77	20.00																														
F BARRCONS 16	16	1.23	73.37	145.01	217.00	54.52	416.78	20.00	1.23	72.99	144.74	217.00	51.60	383.50	20.00	1.23	68.20	141.38	217.00	45.35	333.95	20.00																														
F BARRCONS 17	17	1.23	73.33	144.98	217.00	54.19	413.50	20.00	1.23	72.93	144.71	217.00	51.06	378.34	20.00	1.23	68.21	141.38	217.00	47.89	357.86	20.00																														
F BARRCONS 18	18	1.23	73.30	144.96	217.00	53.94	411.33	20.00	1.23	72.89	144.67	217.00	50.61	374.21	20.00	1.23	68.21	141.38	217.00	50.31	385.71	20.00																														
F BARRCONS 19	19	1.23	73.27	144.94	217.00	53.72	409.85	20.00	1.23	72.84	144.64	217.00	50.14	370.18	20.00	1.23	68.21	141.39	217.00	53.17	428.11	20.00																														
F BARRCONS 20	20	1.23	73.22	144.91	217.00	51.57	383.38	20.00	1.23	72.82	144.63	217.00	49.02	358.69	20.00	1.23	68.17	141.35	217.00	52.47	417.33	20.00																														
F BARRCONS 21	21	1.23	73.18	144.88	217.00	49.70	363.70	20.00	1.23	72.81	144.62	217.00	48.01	349.14	20.00	1.23	68.13	141.33	217.00	51.84	408.28	20.00																														
F BARRCONS 22	22	1.23	73.14	144.85	217.00	48.02	348.06	20.00	1.23	72.80	144.61	217.00	47.11	341.21	20.00	1.23	68.09	141.30	217.00	51.30	400.80	20.00																														
F BARRCONS 23	23	1.23	73.10	144.82	217.00	46.66	336.71	20.00	1.23	72.79	144.60	217.00	46.42	335.46	20.00	1.23	68.06	141.28	217.00	50.89	395.50	20.00																														
F BARRCONS 24	24	1.23	73.07	144.80	217.00	45.41	327.09	20.00	1.23	72.78	144.60	217.00	45.83	330.74	20.00	1.23	68.03	141.25	217.00	50.55	391.30	20.00																														
F BARRCONS 25	25	1.23	73.04	144.78	217.00	44.28	318.97	20.00	1.23	72.78	144.60	217.00	45.35	327.01	20.00	1.23	68.00	141.24	217.00	50.29	388.25	20.00																														
F BARRCONS 26	26	1.23	73.01	144.76	217.00	43.21	311.81	20.00	1.23	72.77	144.59	217.00	44.97	324.11	20.00	1.23	67.98	141.22	217.00	50.12	386.22	20.00																														
F BARRCONS 27	27	1.23	72.99	144.74	217.00	42.30	306.00	20.00	1.23	72.77	144.59	217.00	44.71	322.21	20.00	1.23	67.96	141.20	217.00	50.03	385.34	20.00																														
F BARRCONS 28	28	1.23	72.97	144.73	217.00	41.46	300.94	20.00	1.23	72.77	144.59	217.00	44.56	321.11	20.00	1.23	67.94	141.19	217.00	50.02	385.47	20.00																														
F BARRCONS 29	29	1.23	72.95	144.72	217.00	40.69	296.47	20.00	1.23	72.77	144.59	217.00	44.52	320.85	20.00	1.23	67.92	141.18	217.00	50.11	386.70	20.00																														
F BARRCONS 30	30	1.23	72.94	144.71	217.00	40.05	292.86	20.00	1.23	72.77	144.59	217.00	44.60	321.38	20.00	1.23	67.91	141.17	217.00	50.27	388.93	20.00																														
F BARRCONS 31	31	1.23	72.92	144.70	217.00	39.47	289.73	20.00	1.23	72.77	144.59	217.00	44.77	322.66	20.00	1.23	67.90	141.16	217.00	50.51	392.30	20.00																														
F BARRCONS 32	32	1.23	72.91	144.69	217.00	38.95	286.98	20.00	1.23	72.77	144.59	217.00	45.05	324.78	20.00	1.23	67.89	141.16	217.00	50.86	396.88	20.00																														
F BARRCONS 33	33	1.23	72.90	144.68	217.00	38.48	284.60	20.00	1.23	72.77	144.59	217.00	45.45	327.87	20.00	1.23	67.88	141.15	217.00	51.31	401.96	20.00																														
F BARRCONS 34	34	1.23	72.88	144.67	217.00	37.18	278.30	20.00	1.23	72.77	144.59	217.00	47.96	349.54	20.00	1.23	67.86	141.14	217.00	58.19	511.76	20.00																														
F BARRCONS 35	35	1.23	72.87	144.66	217.00	34.82	267.20	20.00	1.23	72.76	144.58	217.00	45.89	331.47	20.00	1.23	67.86	141.13	217.00	59.57	539.78	20.00																														
F BARRCONS 36	36	1.23	72.87	144.66	217.00	32.83	258.79	20.00	1.23	72.76	144.58	217.00	44.10	317.79	20.00	1.23	67.85	141.13	217.00	56.82	477.17	20.00																														
F BARRCONS 37	37	1.23	72.86	144.65	217.00	31.29	252.75	20.00	1.23	72.76	144.58	217.00	42.70	308.11	20.00	1.23	67.85	141.13	217.00	54.88	443.50	20.00																														
F BARRCONS 38	38	1.23	72.86	144.65	217.00	29.81	247.32	20.00	1.23	72.75	144.58	217.00	41.34	299.52	20.00	1.23	67.84	141.12	217.00	53.06	417.44	20.00																														
F BARRCONS 39	39	1.23	72.86	144.65	217.00	28.42	242.51	20.00	1.23	72.75	144.58	217.00	40.07	292.05	20.00	1.23	67.84	141.12	217.00	51.36	396.64	20.00																														
F BARRCONS 40	40	1.23	72.86	144.65	217.00	27.98	241.02	20.00	1.23	72.76	144.58	217.00	40.08	291.95	20.00	1.23	67.84	141.12	217.00	49.07	372.57	20.00																														
F BARRCONS 41	41	1.23	72.86	144.65	217.00	26.33	235.76	20.00	1.23	72.75	144.58	217.00	38.35	282.65	20.00	1.23	67.84	141.12	217.00	48.02	360.62	20.00																														
F BARRCONS 42	42	1.23	72.86	144.65	217.00	26.12	235.09	20.00	1.23	72.75	144.58	217.00	38.05	281.16	20.00	1.23	67.84	141.12	217.00	48.19	362.40	20.00																														
F BARRCONS 43	43	1.23	72.86	144.65	217.00	27.27	238.74	20.00	1.23	72.75	144.58	217.00	39.04	286.32	20.00	1.23	67.84	141.12	217.00	49.92	381.16	20.00																														
F BARRCONS 44	44	1.23	72.95	144.72	217.00	38.89	286.46	20.00	1.23	72.77	144.59	217.00	44.83	322.66	20.00	1.23	67.94	141.19	217.00	53.10	422.12	20.00																														
F BARRCONS 45	45	1.23	72.91	144.69	217.00	37.88	281.48	20.00	1.23	72.77	144.59	217.00	45.98	331.85	20.00	1.23	67.90	141.16	217.00	54.89	448.52	20.00																														
F BARRCONS 46	46	1.23	72.89	144.68	217.00	37.48	279.64	20.00	1.23	72.77	144.59	217.00	46.84	339.26	20.00	1.23	67.88	141.15	217.00	56.28	472.74	20.00																														



**Kennedy-Burnett Potable  
Water Master Servicing Study**



Prepared for:  
City of Ottawa  
100 Constellation Crescent  
Ottawa, ON K2G 6G8

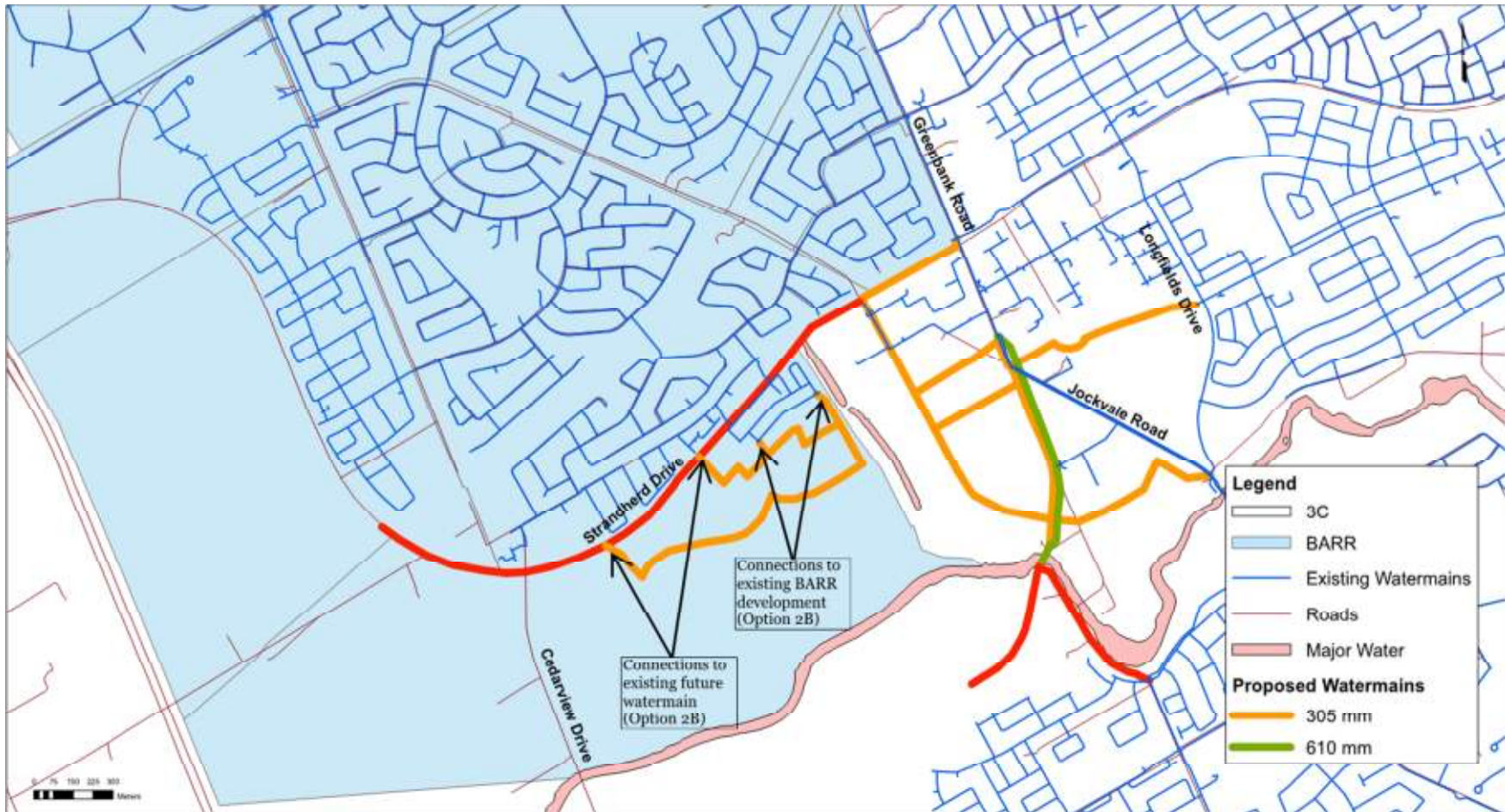
Prepared by:  
Stantec Consulting Ltd.  
400-1331 Clyde Avenue  
Ottawa, ON K2C 3G4

File No. 1634-01221

April 29, 2014

# KENNEDY-BURNETT POTABLE WATER MASTER SERVICING STUDY

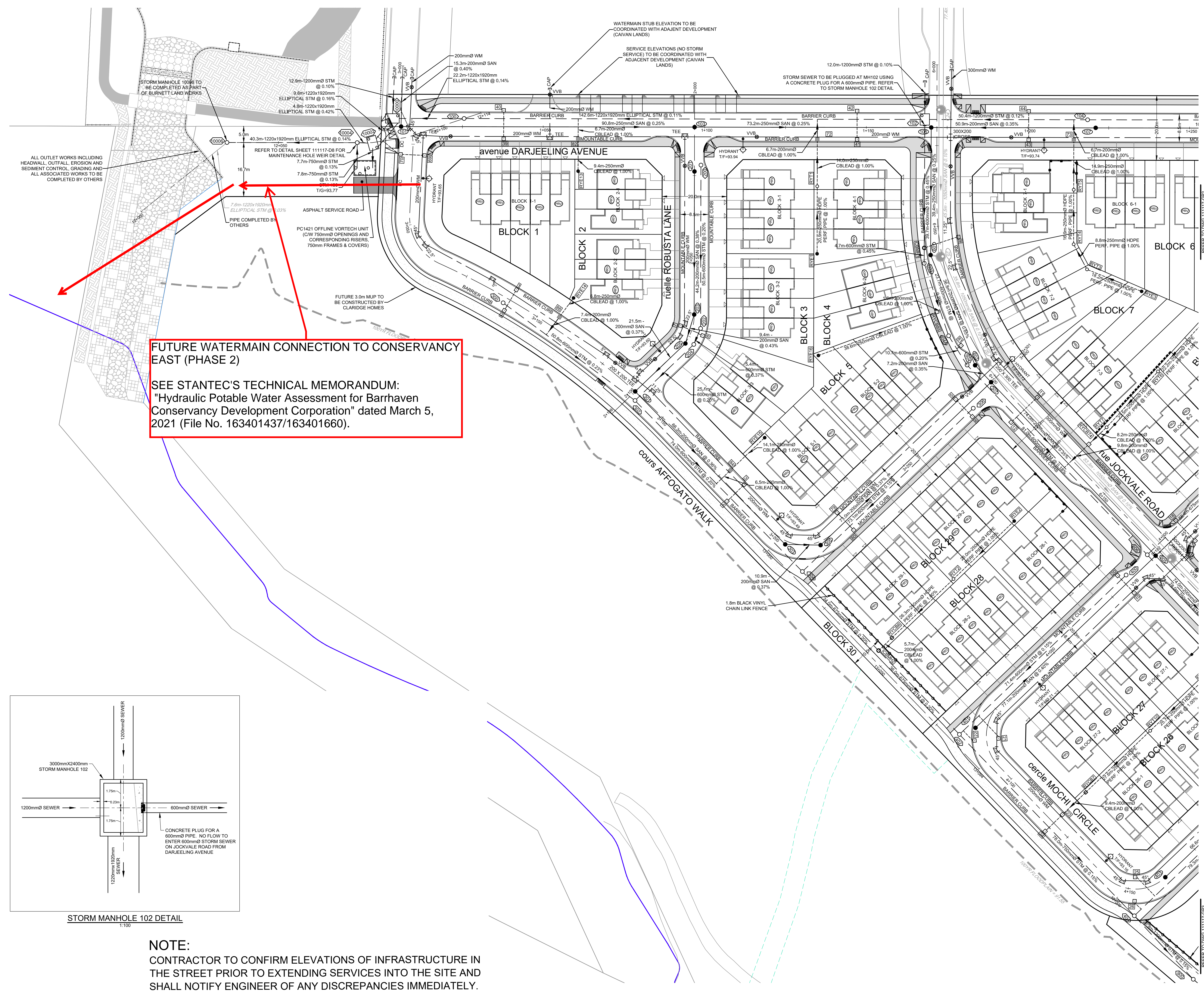
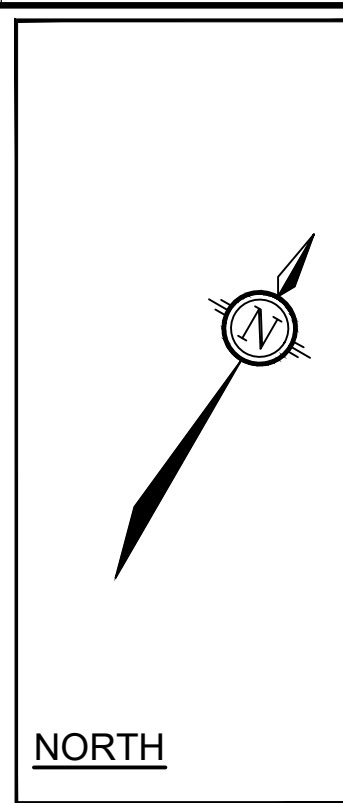
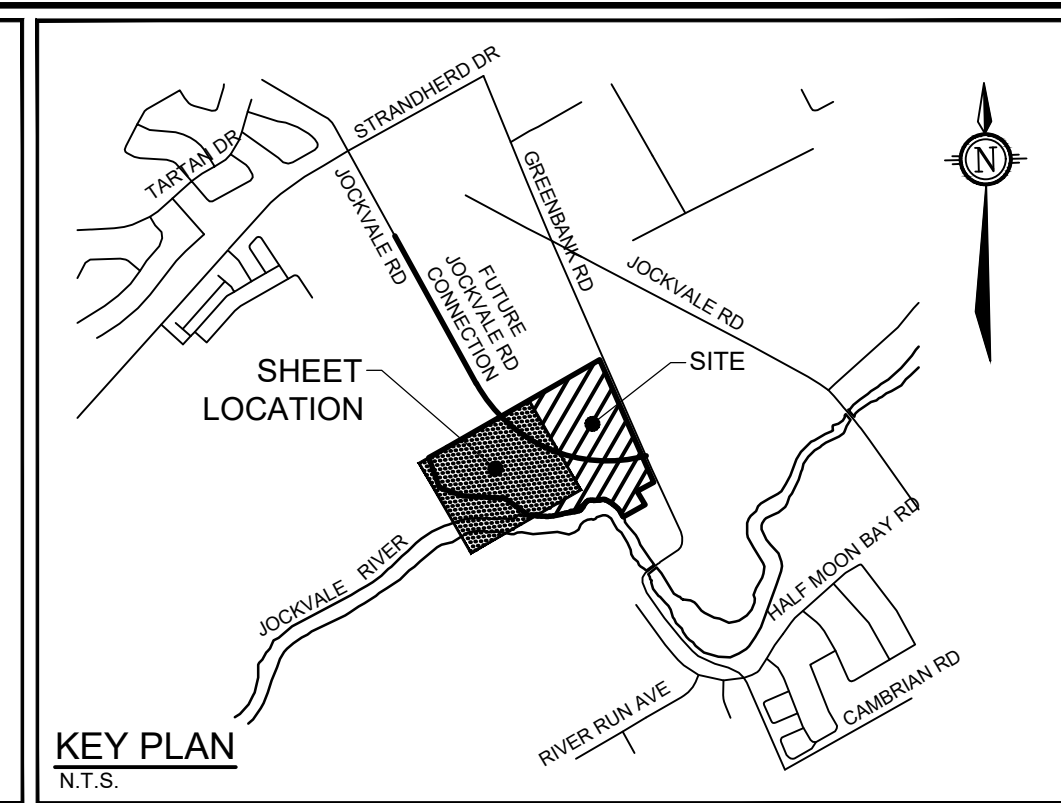
Hydraulic Assessment  
April 29, 2014



**Figure 2-6: Proposed Pipe Layout Post Zone Reconfiguration – Scenario 2B**







**FUTURE WATERMAIN CONNECTION TO CONSERVANCY EAST (PHASE 2)**

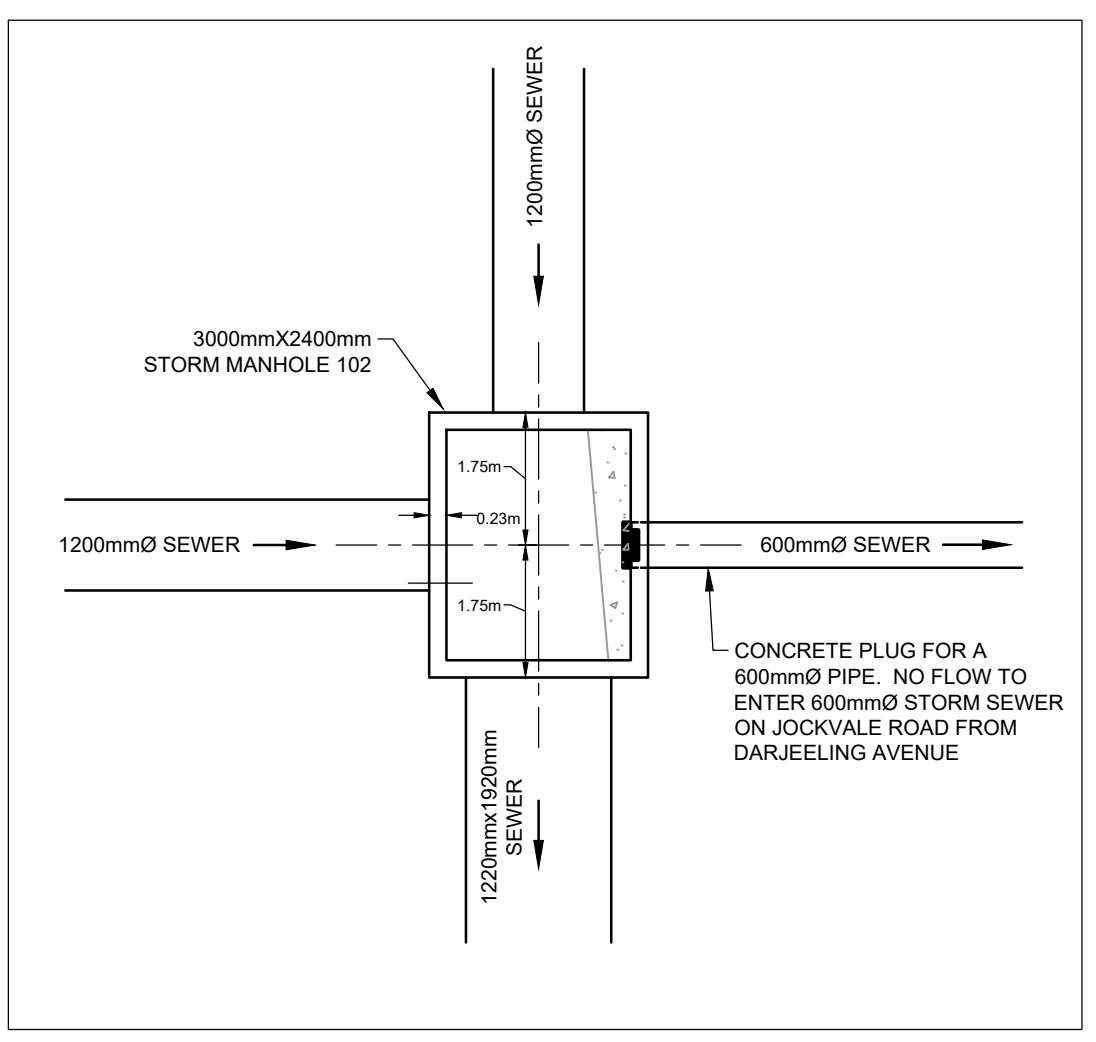
SEE STANTEC'S TECHNICAL MEMORANDUM: "Hydraulic Potable Water Assessment for Barrhaven Conservancy Development Corporation" dated March 5, 2021 (File No. 163401437/163401660).

CATCHBASIN TABLE						
CB No.	STATION	T/G ELEVATION	INVERT	ICD DIA.	FLOW RATE (L/s)	HEAD (m)
CBM1	6+055.96	93.55	90.37			
1	3+090.33	93.10	91.50	83mm ORIFICE SLIDE TYPE	38	1.56
2	3+090.33	93.10	91.50	83mm ORIFICE SLIDE TYPE	38	1.56
3	3+182.44	93.10	91.50	83mm ORIFICE SLIDE TYPE	38	1.56
4	3+182.43	93.10	91.50	83mm ORIFICE SLIDE TYPE	38	1.56
5	3+275.78	93.16	91.57	94mm ORIFICE SLIDE TYPE	50	1.65
6	3+275.78	93.18	91.57	94mm ORIFICE SLIDE TYPE	50	1.65
7	2+072.65	93.17	91.57	102mm ORIFICE SLIDE TYPE	58	1.55
8	2+073.33	93.21	91.61	102mm ORIFICE SLIDE TYPE	58	1.55
9	6+054.11	93.49	91.66	94mm ORIFICE SLIDE TYPE	25	1.63
11	6+114.05	93.41	91.53	102mm ORIFICE SLIDE TYPE	50	1.68
12	6+114.05	93.43	91.53	83mm ORIFICE SLIDE TYPE	50	1.68
19	4+019.25	92.92	91.24	83mm ORIFICE SLIDE TYPE	39	1.64
20	4+019.25	92.92	91.24	83mm ORIFICE SLIDE TYPE	39	1.64
21	4+085.15	92.72	91.13	83mm ORIFICE SLIDE TYPE	39	1.63
22	4+085.15	92.72	91.05	83mm ORIFICE SLIDE TYPE	39	1.63
23	4+118.88	92.69	91.20	83mm ORIFICE SLIDE TYPE	39	1.54
24	4+118.88	92.69	91.20	83mm ORIFICE SLIDE TYPE	39	1.54
25	4+152.04	92.73	91.13	83mm ORIFICE SLIDE TYPE	40	1.65
26	4+152.04	92.73	91.04	83mm ORIFICE SLIDE TYPE	40	1.65
39	1+037.78	93.28	91.47	102mm ORIFICE SLIDE TYPE	56	1.75
40	1+037.78	93.42	91.47	94mm ORIFICE SLIDE TYPE	56	1.75
41	1+147.13	93.44	91.75	83mm ORIFICE SLIDE TYPE	39	1.65
42	1+147.13	93.59	91.75	83mm ORIFICE SLIDE TYPE	39	1.65
43	1+200.23	93.40	91.72	94mm ORIFICE SLIDE TYPE	50	1.63
44	1+200.24	93.55	91.72	94mm ORIFICE SLIDE TYPE	50	1.63
69	3+028.31	93.33	91.61	83mm ORIFICE SLIDE TYPE	41	1.76
70	3+028.31	93.32	91.52	83mm ORIFICE SLIDE TYPE	41	1.76
79	3+225	93.15	91.55	83mm ORIFICE SLIDE TYPE	38	1.56
80	3+225	93.15	91.55	83mm ORIFICE SLIDE TYPE	38	1.56
81	6+087.01	93.51	91.91	83mm ORIFICE SLIDE TYPE	6	1.56

**NOTE:**  
TOP OF GRADE ELEVATIONS ARE EDGE OF PAVEMENT  
GRADES FOR ROADSIDE CATCHBASINS AND TOP OF FRAME  
AND COVER FOR CURB INLET CATCHBASINS.

REAR YARD CATCHBASIN TABLE						
RYCB No.	T/G ELEVATION	INVERT	ICD DIA.	FLOW RATE (L/s)	HEAD (m)	
RYE16	93.44	91.76		0	0.00	
RYE1	93.56	91.75		0	0.00	
RYT11	93.72	91.55		0	0.00	
RYE14	93.59	92.03		0	0.00	
RYE13	93.65	92.00		0	0.00	
RYT5	93.70	91.92		0	0.00	
RYT4	93.76	92.09		0	0.00	
RYE3	93.55	92.35		0	0.00	
RYCB6	93.22	91.11	83mm ORIFICE SLIDE TYPE	23	2.37	
RYT2	93.23	91.37				
RYE2	93.28	91.63				
RYE15	93.43	91.96				
RYCB7	93.19	91.29				
RYT10	93.21	91.57				
RYT6	93.45	91.55				
RYT7	93.44	91.32				
RYT3	93.72	92.17				
RYCB74	93.55	91.24	127mm ORIFICE SLIDE TYPE			
RYCB85	93.70	91.07	152mm ORIFICE SLIDE TYPE			
72	93.53	91.41	102mm ORIFICE SLIDE TYPE			
73	93.51	91.77	127mm ORIFICE SLIDE TYPE			
82	93.48	91.61	83mm ORIFICE SLIDE TYPE			
84	93.14	91.52	94mm ORIFICE SLIDE TYPE			
88	93.19	91.66	94mm ORIFICE SLIDE TYPE			

**NOTE:**  
SERVICE LATERALS UNDER GARAGE SHALL BE INSTALLED WITH SLEEVE.



**NOTE:**  
CONTRACTOR TO CONFIRM ELEVATIONS OF INFRASTRUCTURE IN THE STREET PRIOR TO EXTENDING SERVICES INTO THE SITE AND SHALL NOTIFY ENGINEER OF ANY DISCREPANCIES IMMEDIATELY.

No.	REVISION	mm/dd/yy	BY	No.	REVISION	mm/dd/yy	BY
16	ISSUED FOR SERVICING CONSTRUCTION	FEB 1/21	SAZ	8	ISSUED FOR TENDER	OCT 16/20	SAZ
15	ISSUED FOR COMMENCE WORK NOTICE	JAN 29/21	SAZ	7	REVISED AS PER CITY OF OTTAWA COMMENTS	OCT 9/20	SAZ
14	ISSUED FOR ORDERING PIPE MATERIALS	DEC 4/20	SAZ	6	REVISED AS PER CITY OF OTTAWA COMMENTS	AUG 24/20	SAZ
13	REVISED SIZES FOR MANHOLES 102,10000,10002,10004	DEC 4/20	SAZ	5	ISSUED FOR CITY OF OTTAWA REVIEW	JUNE 22/20	SAZ
12	ISSUED FOR ECA APPROVAL	NOV 19/20	SAZ	4	ISSUED FOR DISCUSSION PURPOSES ONLY	JULY 12/19	SAZ
11	ISSUED TO GEOTECHNICAL CONSULTANT FOR REVIEW	NOV 4/20	SAZ	3	ISSUED WITH DRAFT PLAN OF SUBDIVISION	MAY 29/19	MSP
10	ISSUED FOR ADDENDUM NO.3	OCT 30/20	SAZ	2	REISSUED WITH DRAFT PLAN OF SUBDIVISION	MAY 23/18	MSP
9	ISSUED WITH SITE INSTRUMENT NO.3	FEB 11/21	SAZ	1	REISSUED WITH DRAFT PLAN OF SUBDIVISION	JAN 26/18	MSP

**SCALE**

1:500

0 5 10 15 20

REVISION

SAZ

DOB

RBG

DOB

MSP

**NOVATECH**  
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Facsimile: (613) 254-5867  
Website: www.novatech-eng.com

**CITY OF OTTAWA**  
BURNETT LANDS  
3370 GREENBANK ROAD

DRAWING NAME  
**GENERAL PLAN OF SERVICES**

PROJECT No. 111117  
REV #18  
DRAWING No. 111117-GP1

NOVATECH 111117-GP1.dwg, GP1, Feb 22, 2021, 2:29pm, gpran

D07-16-17-0001

#18179



## Kevin Murphy

---

**From:** Shillington, Jeffrey <jeff.shillington@ottawa.ca>  
**Sent:** Friday, March 12, 2021 9:54 AM  
**To:** Kevin Murphy  
**Cc:** Steve Pichette; Marc Pichette; Hugo Lalonde (hugo.lalonde@caivan.com); Sevigny, John; vincent.denomme@claridgehomes.com; Marc St.Pierre; Julio DaSilva (Julio.DaSilva@caivan.com); Varghese, Renjit  
**Subject:** RE: Barrhaven Conservancy - future water connection to Claridge development

**EXTERNAL E-MAIL - Do not click links or open attachments unless you recognize the sender.**

Kevin,

As per my voicemail, I spoke to Renjit in Water Distribution this morning and he has no concerns with the proposal given that the anticipated timing of construction for Caivan is the fall of this year. We would be looking for the T coming off Claridge's 200 mm dia. watermain with a valve on the property line, with one length of pipe after the valve then capped.

I did speak to John Sevigny about this as well and he had no concerns.

It is assumed that this additional work will be at Caivan's expense.

Let me know if you require any additional information.

Regards,

Jeff Shillington, P.Eng.  
Senior Project Manager, Development Review, South Branch  
Planning, Infrastructure and Economic Development  
City of Ottawa  
tel: 580-2424 x 16960  
email: jeff.shillington@ottawa.ca

---

**From:** Kevin Murphy <KMurphy@dsel.ca>  
**Sent:** March 11, 2021 11:54 AM  
**To:** Shillington, Jeffrey <jeff.shillington@ottawa.ca>  
**Cc:** Steve Pichette <spichette@dsel.ca>; Marc Pichette <MPichette@dsel.ca>; Hugo Lalonde (hugo.lalonde@caivan.com) <hugo.lalonde@caivan.com>; Sevigny, John <John.Sevigny@ottawa.ca>; vincent.denomme@claridgehomes.com; Marc St.Pierre <m.stpierre@novatech-eng.com>; Julio DaSilva (Julio.DaSilva@caivan.com) <Julio.DaSilva@caivan.com>  
**Subject:** RE: Barrhaven Conservancy - future water connection to Claridge development  
**Importance:** High

**CAUTION: This email originated from an External Sender. Please do not click links or open attachments unless you recognize the source.**

Hi Jeff,

**ATTENTION : Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.**

Just

following up with the email chain below.

Firstly, I would like to apologize for not including John Seigny on the coordination below. I presume that you have but I should have kept him apprised of the proposal (I had reached out to him in the past about this).

**By way of this email I would ask for you to confirm for Vincent at Claridge that the City is ok with moving forward with this proposed future connection point to the 200mm watermain within the Claridge development (screenshot below).**

Time is of the essence given the construction progress being made on site by the contractor and the desire to facilitate this prior to commissioning of the watermain.

Hugo will continue to reach out to Vincent to coordinate any logistics between their teams to facilitate this work.

Kevin

## **DSEL**

**david schaeffer engineering ltd.**

**phone:** (613) 836-0856 ext.563

**cell:** (613) 324-8361

**email:** kmurphy@DSEL.ca

---

**From:** Kevin Murphy

**Sent:** Wednesday, March 10, 2021 10:14 AM

**To:** 'Shillington, Jeffrey' <[jeff.shillington@ottawa.ca](mailto:jeff.shillington@ottawa.ca)>

**Cc:** Steve Pichette <[SPichette@dsel.ca](mailto:SPichette@dsel.ca)>; Marc Pichette <[MPichette@dsel.ca](mailto:MPichette@dsel.ca)>

**Subject:** RE: Barrhaven Conservancy - future water connection to Claridge development

**Importance:** High

Hi Jeff,

The timing to install the tee would be as soon as possible while the contractor is active on site and hopefully before the watermain is chlorinated etc.

Timing for Conservancy's first phase of construction would also be as soon as possible depending on draft plan approval and servicing design/approval timelines.

The desire would be to start servicing construction in autumn of this year.

Agreed that a tee with a valve (close to the tee given there are no other services in the roadway – minimizes extent of water in the line) and extended/capped to just out of the ROW.

How best do you want this update/revision facilitated?

**CONTEMPLATED CHANGE NOTICE (CCN) NO. 4**

**TO:** Thomas Cavanagh Construction Limited

**DISTRIBUTION:** Nigel Madden, Cavanagh  
Jonathon Blake, Cavanagh  
Vincent Denomme, Claridge  
Steve Zorgel, Novatech

**PROJECT:** Burnett Lands

**CONTRACT NO.:** 111117-01

**ISSUED BY:** Marc St. Pierre

**DATE:** March 18, 2021

---

The purpose of this contemplated change notice is to give notice of a considered change in the work for which a price must be established and approved by Change Order before the work involved is undertaken. Please respond within 7 working days of the date of this notice.

---

The following work is proposed as a change of scope to the contract:

**SCOPE OF WORK:**

1. To accommodate future development to the west of the Burnett Lands, a 200mm dia. watermain stub is to be installed within the north storm sewer servicing block. The attached figure illustrates the location and elevation of the watermain stub. The service shall be installed 2.0m past the proposed service road.

**QUOTATION:**

1. Contractor shall complete the work on a time and material basis.

**ATTACHMENTS:**

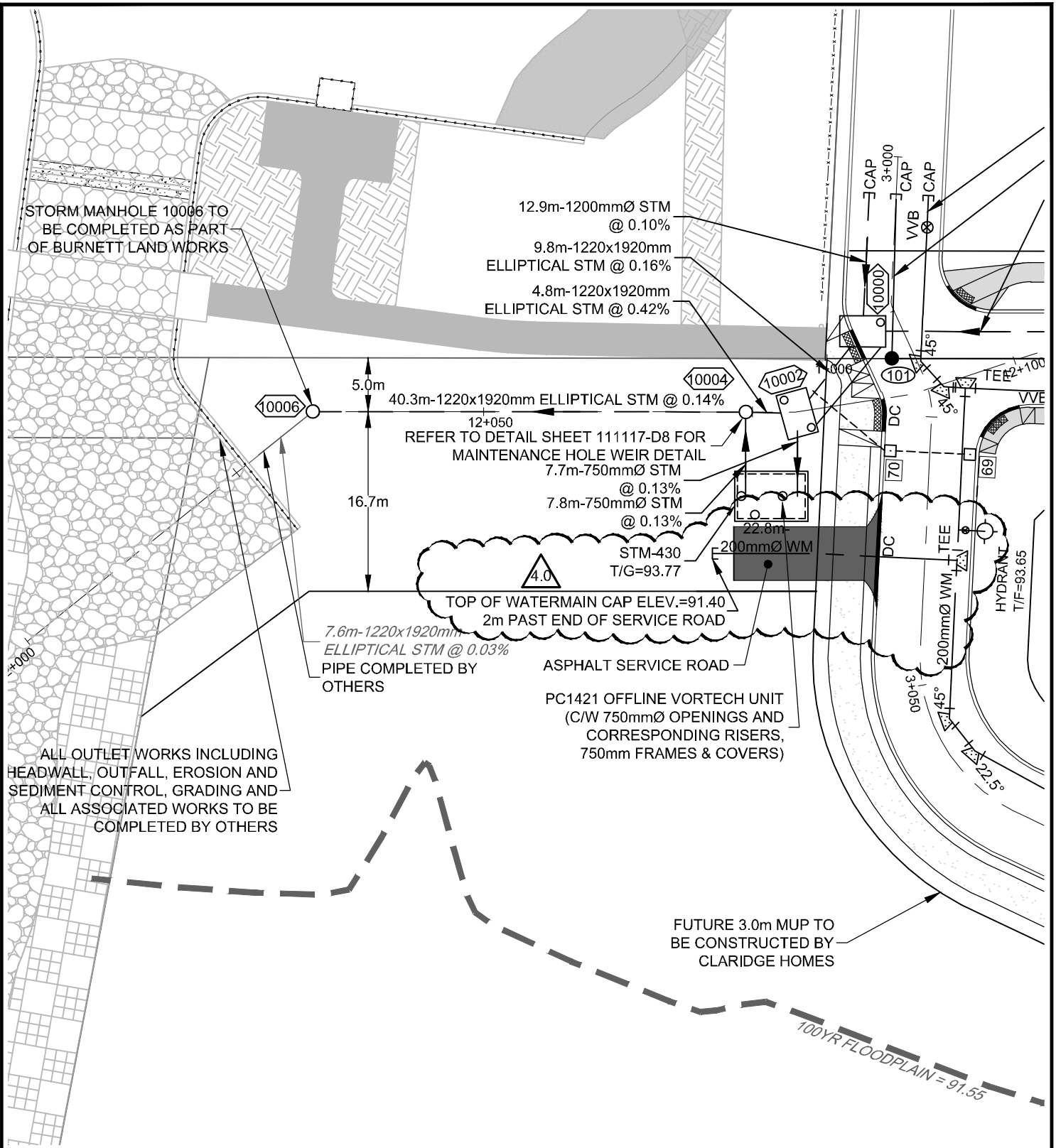
- Figure CCN 4, Watermain Stub Under Service Road, dated March 2021

**NOVATECH**



per \_\_\_\_\_

M:\2011\1117\CAD\Design\Figures\CCN4\FIG-CCN4.dwg, CCN4, Mar 18, 2021 - 10:59am, rgrayton



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Website www.novatech-eng.com

**BURNETT LANDS**  
3370 GREENBANK ROAD

**WATERMAIN STUB UNDER SERVICE ROAD**



DATE MAR 2021 JOB 111117 FIGURE CCN4

# **APPENDIX C**

## **SANITARY**

# MEMORANDUM

**DATE:** MAY 30, 2019

**TO:** JOSÉE VALLEE – CITY OF OTTAWA

**FROM:** CONRAD STANG – NOVATECH

**RE:** STRANDHERD DRIVE WIDENING PROJECT  
SOUTH NEPEAN COLLECTOR PHASE 3: SANITARY FLOW CALCULATIONS

**CC:** EDSON DONNELLY – NOVATECH

See markups on:  
- Figure 1  
- "Sanitary Sewer Design Sheet, South Nepean Collector - Phase 2 & 3" (Dec 5, 2018 version)  
- "Sanitary Sewer Design Sheet, South Nepean Collector - Phase 2 & 3" (August 20, 2015 version)

## 1.0 PURPOSE

This memorandum provides the sanitary sewer flow calculations and design sheet for Phase 3 of the proposed South Nepean Collector (SNC), as part of the Strandherd Drive Widening Project. Sanitary design flows have been estimated for both current-day operational flows and future development peak design flows. They are based on the latest available planning information for the vacant lands within the SNC sewershed.

## 2.0 BACKGROUND

In January 1998, the Master Servicing Study for the South Nepean Urban Area provided a conceptual plan for water, wastewater and stormwater infrastructure. The preferred alternative for wastewater servicing was an east/west trunk sewer alignment that was to be completed in several phases. The proposed sanitary trunk sewer was initially called the Jock River Collector, but was renamed the South Nepean Collector during the original functional design study completed in 2003.

Phase 1 of the South Nepean Collector was completed in 2005 and currently terminates at a 2400mm maintenance hole located east of Longfields Drive, north of Bren-Maur Road. Phase 2 was completed in 2016 and currently terminates at a 2400mm maintenance hole located at the intersection of Strandherd Drive and Fraser Fields Way.

Phase 3 will extend the trunk sewer along Strandherd Drive to the intersection of Kennevale Drive. Here it will connect with the existing sanitary trunk sewer that was constructed as part of the 2014 works to improve Strandherd Drive and develop the CitiGate Lands.

The sanitary sewer flows were previously documented in the *South Nepean Collector – Functional Design Report and Update* (Dillon, 2012). Novatech (2016) completed a *Hydraulics Review / Assessment* of the sanitary flows presented in the Dillon Report (attached). This was based on the latest planning information for the vacant lands within the SNC sewershed. The results of the *Hydraulics Review / Assessment* (Novatech, 2016) were similar to the results from the Dillon (2012) analysis.

### 3.0 DESIGN PARAMETERS AND POPULATION ESTIMATES

#### 3.1 Design Parameters

The sanitary design flow were calculated using the parameters from the City of Ottawa Sewer Design Guidelines (October 2012), revised per Technical Bulletin ISTB-2018-01 (March 2018). These parameters are summarized in **Table 1** and **Table 2**.

**Table 1: Peak Design Flow Parameters**

Land Use	Average Daily Flow	Peaking Factor	Peak Extraneous Flows
Residential	280 L/cap/day	Harmon Equation, K=0.8 (1.6 min – 3.2 max)	0.33 L/s/ha
Commercial	28,000 L/ha/day	1.0 – 1.5*	
Institutional	28,000 L/ha/day	1.0 – 1.5*	
Other†	0 L/ha/day	N/A	

\*Peak Factor = 1.5 if contributing area is >20%; Peak Factor = 1.0 if contributing area is <20%

†Open Space, Arterial ROW, SWM Blocks, etc. with no sanitary flow contribution (extraneous flow only)

**Table 2: Operational Design Flow Parameters**

Land Use	Average Daily Flow	Peaking Factor	Peak Extraneous Flows
Residential	200 L/cap/day	Harmon Equation, K=0.6 (1.2 min – 2.4 max)	0.30 L/s/ha
Commercial	17,000 L/ha/day	1.0 (non-coincident peak)	
Institutional	17,000 L/ha/day	1.0 (non-coincident peak)	

\*There are no industrial areas identified within the tributary area.

$$\text{Harmon Equation} = 1 + \frac{14}{4 + \left(\frac{P}{1000}\right)^{\frac{1}{2}}} \times K$$

Where:

P = Population

K = Correction Factor:

- Peak Flow = 0.8
- Operational = 0.6

#### 3.2 Land Use Designations & Population Estimates

Population densities and unit counts for future residential development are based on the Novatech (2016) Hydraulics Review / Assessment; refer to **Table 3**. They are based on the concept plans provided by the developers of the future residential areas.



**Table 3: Residential Land Use Population Densities**

Residential Land Use	Units per ha	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

The land use designations shown in **Table 4** have been applied for the areas within Phases 2 & 3 of the SNC (Node 70 to 130). The Hydraulics Analysis / Review delineated the sewershed areas and land use designations using aerial photos (existing development) and conceptual site plans (future development).

**Table 4: Land Use Designations**

Land Use Designation	
Secondary Plan	SNC Design
Residential	Residential (Low / Medium / High Density)
Institutional / Office	Institutional
Commercial	Commercial
Recreational	
Business Park	
Prestige Business Park	
Park/Open Space Area	Other*
Ex. Snow Disposal Facility (future commercial)	
Stormwater Management Facility	
Conservation Lands	
Arterial Right-of-Ways	

\* No sanitary flow contribution - extraneous flows (inflow/infiltration) only.

The overall residential population estimate and sewershed area for Phases 2 and 3 of the SNC is provided in **Table 5** below. It is assumed that the snow dump facility at the Stranderd Drive and McKenna Casey Drive will ultimately be re-zoned for commercial development.

**Table 5: Population Estimates and Areas**

Existing / Future	Estimated Population / Area	Novatech (2015)
Existing	Estimated Population	6,944 persons
	Gross Residential Area	60.09 ha
	Gross Commercial / Institutional Area	64.37 ha
	<i>Total Sewershed Area</i>	124.5 ha
Future (full service)	Estimated Population	27,312 persons
	Gross Residential Area	248.48 ha
	Gross Commercial / Institutional Area	228.82 ha
	<i>Total Sewershed Area</i>	477.3 ha

#### 4.0 SANITARY DESIGN FLOWS

The sanitary flow allocations for Phases 2 and 3 of the SNC are provided in **Table 6**. The corresponding sanitary drainage area plan is provided as **Figure 1**. Sanitary sewer flow calculations for Phases 2 and 3 and detailed sanitary sewer design sheets for Phase 3 are attached to this memorandum.

The estimated sanitary design flows from Phase 3 of the SNC (entering Node 90) are as follows:

- Present-Day Operational Design Flows (Theoretical) = 55.1 L/s
- Future Peak Design Flows = 282.5 L/s

The outlet for Phase 3 of the SNC is the existing 900mm outlet pipe at the 2400mm maintenance hole (Node 90) located at the intersection of Strandherd Drive and Fraser Fields Way. Given a minimum design slope of 0.10%, this 900mm sanitary trunk sewer would have a full flow capacity of 597.2 L/s. Therefore, the downstream sanitary trunk sewer would be at 64% capacity, based on the future peak design flow being 282.5 L/s.

#### ATTACHMENTS:

- Figure 1: Sanitary Drainage Areas and Land Use
- Sanitary Sewer Flow Calculations
- Sanitary Sewer Design Sheets (Phase 3)
- South Nepean Collector Phase 2: Hydraulics Review / Assessment (Novatech, 2016)
- Excerpts from Dillion (2012)

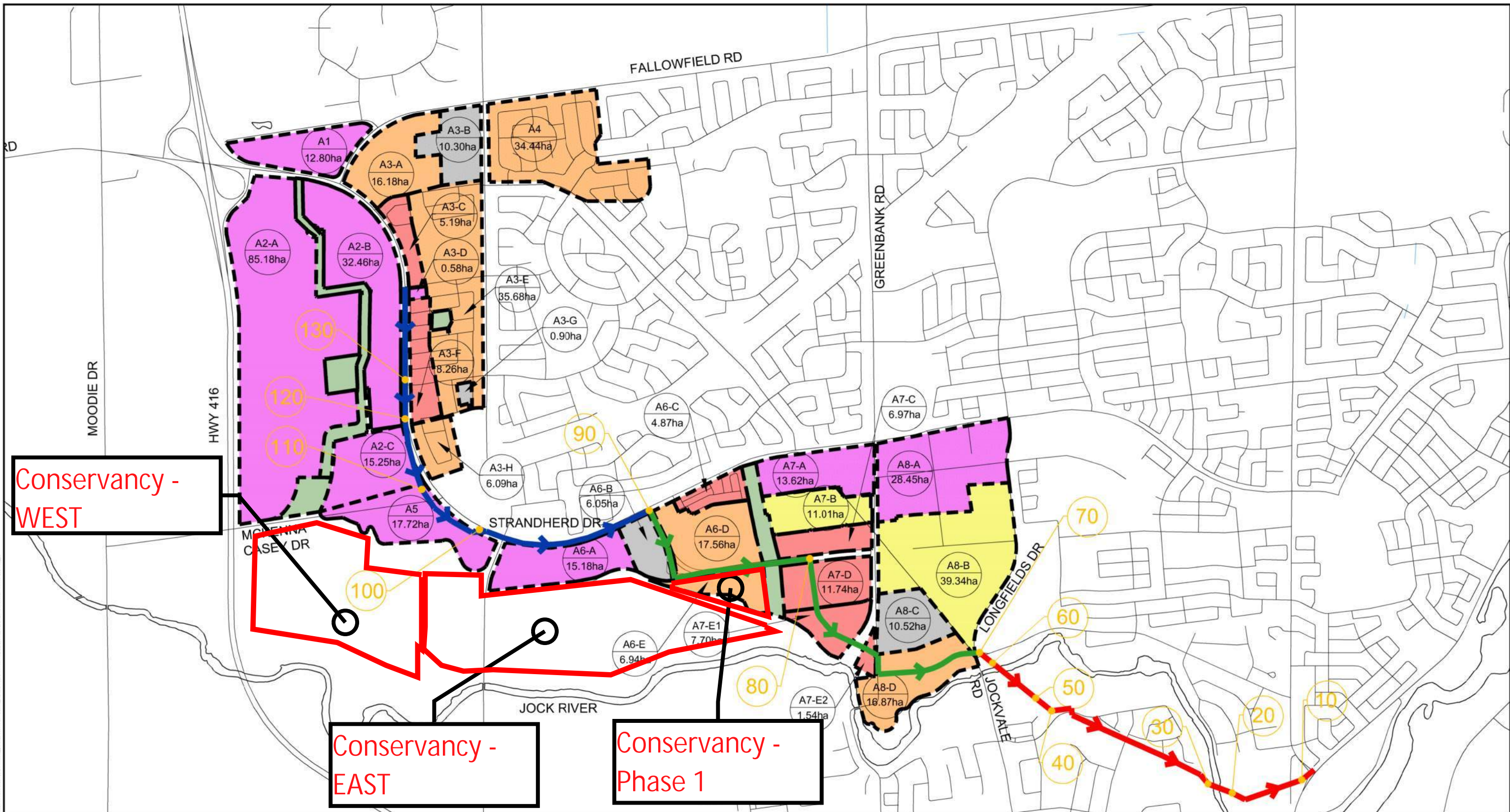


**Table 6: Updated Allocation of Commercial, Institutional and Residential Demands to Phases 2 & 3 (Nodes 70 – 130) of the SNC by Collection Area**

Collection Area	Upstream Node	Existing / Proposed Development	Existing / Proposed Land Use	Area (ha)	Estimated Number of Residential Units	Population Density (persons / ha)	Comment	Reference
A1	130	Proposed	Commercial	12.80	-	-	O'Keefe Court – Conceptual site plan shows proposed commercial.	Conceptual Plans for O'Keefe Court
A2-A	130	Proposed	Commercial	85.18	-	-	CitiGate – Analysis uses same approach as the design for CitiGate.	Detailed Servicing and SWM Report (Phase 1) (Novatech, 2014)
A2-B	130	Proposed	Commercial	32.46	-	-		
A2-C	120	Proposed	Commercial (ex. Snow dump)	15.25	-	-	Existing snow dump facility assumed to be future commercial.	Functional Design Report and Update – SNC Phase 2 and 3 (Dillon, 2012)
A3-A	130	Proposed	Low Density Residential	16.18	461	95.2	Havencrest – Existing single family units.	Havencrest Design Report (IBI, 2013)
A3-B	130	Existing	Institutional	10.30	-	-	Cedarview Middle School and Cedarview Alliance Church.	Aerial Photos / Site Visits
A3-C	130	Existing	Medium Density Residential	5.19	311	162	Existing townhouse units.	
A3-D	130	Existing	Commercial	0.58	-	-	Existing commercial buildings.	
A3-E	130	Existing	Low Density Residential	35.68	999	95.2	Existing single family units.	
A3-F	130	Existing	Medium Density Residential	8.26	496	162.0	Existing townhouse units.	
A3-G	130	Existing	Institutional	0.90	-	-	Ottawa Torah Centre Chibad.	
A3-H	120	Existing	Low Density Residential	6.09	171	95.2	Existing single family units.	
A4	130	Existing	Low Density Residential	34.44	964	95.2	Existing single family units currently serviced by Jockvale pump station; to be redirected to SNC.	
A5	110	Proposed	Commercial	17.72	-	-	Proposed commercial south of McKenna Casey Drive.	Site Visits
A6-A	100	Proposed	Commercial	15.18	-	-	Proposed commercial south of Srandherd Drive; east of Borrisokane Road.	Conceptual Plan for Lands Adjacent the Kennedy-Burnett SWMF provided by Minto (2015)
A6-B	100	Proposed	Institutional	6.05	-	-	Proposed school site on Minto property.	
A6-C	90	Existing	Medium Density Residential	4.87	292	162.0	Existing townhouse units.	Aerial Photos / Site Visits
A6-D	90	Proposed	Low Density Residential	17.56	492	95.2	Proposed single family units on lands owned by Minto / Mion.	Conceptual Plans for Lands Adjacent the Kennedy-Burnett SWMF provided by land owners.
A6-E	90	Proposed	Low Density Residential	6.94	203	95.2	Proposed single family units on lands owned by Pavic / Braovac.	
A7-A	80	Existing	Commercial	13.62	-	-	Existing large retail stores (commercial).	Aerial Photos
A7-B	80	Proposed	High Density Residential	11.01	826	135.0	Proposed high density units on lands owned by Richcraft / Trinity.	Conceptual Plans for Lands Adjacent the Kennedy-Burnett SWMF provided by land owners.
A7-C	80	Proposed	Medium Density Residential	6.97	418	162.0	Proposed Medium density units on lands owned by Mion.	
A7-D	80	Proposed	Medium Density Residential	11.74	704	162.0	Proposed Medium density units on lands owned by Caivan.	
A7-E1/E2	80	Proposed	Medium Density Residential	9.24	554	162.0	Proposed Medium density units on lands owned by Claridge.	
A8-A	80	Existing	Commercial	28.45	-	-	Existing Barrhaven Market Place (commercial).	Aerial Photos / Site Visits
A8-B	80	Proposed	High Density Residential	39.34	2951	135.0	Future development similar to Ampersands development.	Site Visits
A8-C	80	Existing	Institutional	10.52	-	-	Existing St. Joseph High School.	Aerial Photos / Site Visits
A8-D	80	Proposed	Low Density Residential	16.87	1012	162.0	Proposed 600 low density residential units.	Functional Design Report and Update – SNC Phase 2 and 3 (Dillon, 2012)



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**LEGEND**

	EXISTING / PROPOSED HIGH DENSITY RESIDENTIAL		OTHER LANDS (OPEN SPACE, PARKS, AND SWMFS)
	EXISTING / PROPOSED MEDIUM DENSITY RESIDENTIAL		SOUTH NEPEAN COLLECTOR PHASE 1
	EXISTING / PROPOSED LOW DENSITY RESIDENTIAL		SOUTH NEPEAN COLLECTOR PHASE 2
	EXISTING / PROPOSED COMMERCIAL		SOUTH NEPEAN COLLECTOR PHASE 3
	EXISTING / PROPOSED INSTITUTIONAL		SOUTH NEPEAN COLLECTOR NODE ID



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 Telephone (613) 254-9643  
 Facsimile (613) 254-5867  
 Website www.novatech-eng.com

<b>SOUTH NEPEAN COLLECTOR SEWER</b>		
<b>SANITARY DRAINAGE AREAS AND LAND USE</b>		
SCALE	1:20 000	
DATE	JOB	FIGURE
MAY 2019	117190	FIG. 1



PROJECT #: 117190  
 DESIGNED BY: CMS  
 CHECKED BY: RJD  
 DATE: December 5, 2018

**SANITARY SEWER DESIGN SHEET**

**South Nepean Collector - Phase 2 & 3**

Theoretical Current Operational Peak Wastewater Flow



Location			Areas				Population				Individual Design Flows			Cumulative Design Flows				
Area I.D.	Existing Land Use	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Total Gross Area (ha)	Residential Population Density (people / ha)	Individual Residential Population	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn <sup>1</sup> )	Commercial Peak Flow Rate <sup>2</sup> (17,000 L/ha/d) (L/s)	Institutional Peak Flow Rate <sup>2</sup> (17,000 L/ha/d) (L/s)	Infiltration / Inflow Rate (0.3 L/s/ha) (L/s)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (200 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)
A1	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A2-A	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A2-B	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A3-A	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A3-B	Institutional	130		10.30		10.30					0.0	2.0	3.1	0.0	2.0	3.1	0.0	5.1
A3-C	Medium Density Residential	130			5.19	5.19	162.0	841	841	2.40	0.0	0.0	1.6	0.0	2.0	4.6	4.7	11.3
A3-D	Commercial	130	0.58			0.58		841	841	2.40	0.1	0.0	0.2	0.1	2.0	4.8	4.7	11.6
A3-E	Low Density Residential	130			35.68	35.68	95.2	3397	4238	2.39	0.0	0.0	10.7	0.1	2.0	15.5	23.4	41.1
A3-F	Medium Density Residential	130			8.26	8.26	162	1338	5576	2.32	0.0	0.0	2.5	0.1	2.0	18.0	29.9	50.1
A3-G	Institutional	130		0.90		0.90			5576	2.32	0.0	0.2	0.3	0.1	2.2	18.3	29.9	50.5
A4	Low Density Residential*	130				0.00			5576	2.32	0.0	0.0	0.0	0.1	2.2	18.3	29.9	50.5
A2-C	Snow Dump Facility	120				0.00			5576	2.32	0.0	0.0	0.0	0.1	2.2	18.3	29.9	50.5
A3-H	Low Density Residential	120			6.09	6.09	95.2	580	6155	2.30	0.0	0.0	1.8	0.1	2.2	20.1	32.7	55.1
A5	Open Space	110				0.00			6155	2.30	0.0	0.0	0.0	0.1	2.2	20.1	32.7	55.1
A6-A	Open Space	100				0.00			6155	2.30	0.0	0.0	0.0	0.1	2.2	20.1	32.7	55.1
A6-B	Open Space	100				0.00			6155	2.30	0.0	0.0	0.0	0.1	2.2	20.1	32.7	55.1
A6-C	Medium Density Residential	90			4.87	4.87	162.0	789	6944	2.27	0.0	0.0	1.5	0.1	2.2	21.6	36.4	60.3
A6-D	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	0.1	2.2	21.6	36.4	60.3
A6-E	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	0.1	2.2	21.6	36.4	60.3
A7-A	Commercial	90	13.62			13.62			6944	2.27	2.7	0.0	4.1	2.8	2.2	25.6	36.4	67.1
A7-B	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	2.2	25.6	36.4	67.1
A7-C	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	2.2	25.6	36.4	67.1
A7-D	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	2.2	25.6	36.4	67.1
A7-E1/E2	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	2.2	25.6	36.4	67.1
A8-A	Commercial	80	28.45			28.45			6944	2.27	5.6	0.0	8.5	8.4	2.2	34.2	36.4	81.2
A8-B	Open Space	80				0.00			6944	2.27	0.0	0.0	0.0	8.4	2.2	34.2	36.4	81.2
A8-C	Institutional	80		10.52		10.52			6944	2.27	0.0	2.1	3.2	8.4	4.3	37.3	36.4	86.4
A8-D	Open Space	80				0.00			6944	2.27	0.0	0.0	0.0	8.4	4.3	37.3	36.4	86.4
ROW Along SNC Sewer Alignment	-	80				14.34			6944	2.27	0.0	0.0	4.3	8.4	4.3	41.6	36.4	90.7
<b>TOTAL</b>		<b>80</b>	<b>42.65</b>	<b>21.72</b>	<b>60.09</b>	<b>138.80</b>	<b>-</b>	<b>6944</b>	<b>6944</b>	<b>2.27</b>	<b>8.4</b>	<b>4.3</b>	<b>41.6</b>	<b>8.4</b>	<b>4.3</b>	<b>41.6</b>	<b>36.4</b>	<b>90.7</b>

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

Notes:

- Harmon Equation =  $1 + [14 / (4 + (P/1000)^{1/2})] \times K$   
 Where: P = population; K = correction factor = 0.6
- Institutional / Commercial Peaking Factor = 1.0

Reported Design Flows / Assumptions:

- Area A4: Existing single family units currently serviced by Jockvale pump station; currently not directed to SNC

PROJECT #: 117190  
 DESIGNED BY: CMS  
 CHECKED BY: RJD  
 DATE: December 5, 2018

**SANITARY SEWER DESIGN SHEET**

**South Nepean Collector - Phase 2 & 3**

Theoretical Future Full Service Peak Wastewater Flow



Location			Areas				Population				Individual Design Flows			Cumulative Design Flows				
Area I.D.	Existing / Proposed Land Use	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Total Gross Area (ha)	Residential Population Density (people / ha)	Individual Residential Population	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn <sup>1</sup> )	Commercial Peak Flow Rate <sup>2</sup> (28,000 L/ha/d) (L/s)	Institutional Peak Flow Rate <sup>2</sup> (28,000 L/ha/d) (L/s)	Infiltration / Inflow Rate (0.33 L/s/ha) (L/s)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (280 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)
A1	Commercial	130	12.80			12.80					6.2	0.0	4.2	6.2	0.0	4.2	0.0	10.4
A2-A	Commercial	130	85.18			85.18					41.4	0.0	28.1	47.6	0.0	32.3	0.0	80.0
A2-B	Commercial	130	32.46			32.46					15.8	0.0	10.7	63.4	0.0	43.0	0.0	106.5
A3-A	Low Density Residential	130			16.18	16.18	95.2	1540	1540	3.14	0.0	0.0	5.3	63.4	0.0	48.4	15.7	127.5
A3-B	Institutional	130		10.30		10.30		1540	1540	3.14	0.0	3.3	3.4	63.4	3.3	51.8	15.7	134.2
A3-C	Medium Density Residential	130			5.19	5.19	162.0	841	2381	3.02	0.0	0.0	1.7	63.4	3.3	53.5	23.3	143.6
A3-D	Commercial	130	0.58			0.58		2381	2381	3.02	0.3	0.0	0.2	63.7	3.3	53.7	23.3	144.0
A3-E	Low Density Residential	130			35.68	35.68	95.2	3397	5778	2.75	0.0	0.0	11.8	63.7	3.3	65.5	51.5	184.0
A3-F	Medium Density Residential	130			8.26	8.26	162	1338	7116	2.68	0.0	0.0	2.7	63.7	3.3	68.2	61.8	197.0
A3-G	Institutional	130		0.90		0.90		7116	7116	2.68	0.0	0.3	0.3	63.7	3.6	68.5	61.8	197.6
A4	Low Density Residential	130			34.44	34.44	95.2	3279	10395	2.55	0.0	0.0	11.4	63.7	3.6	79.9	85.9	233.1
A2-C	Commercial (ex. snow dump)	120	15.25			15.25		10395	10395	2.55	7.4	0.0	5.0	71.1	3.6	84.9	85.9	245.5
A3-H	Low Density Residential	120			6.09	6.09	95.2	580	10974	2.53	0.0	0.0	2.0	71.1	3.6	86.9	90.0	251.7
A5	Commercial	110	17.72			17.72		10974	10974	2.53	8.6	0.0	5.8	79.7	3.6	92.7	90.0	266.1
A6-A	Commercial	100	15.18			15.18		10974	10974	2.53	7.4	0.0	5.0	87.1	3.6	97.7	90.0	278.5
A6-B	Institutional	100		6.05		6.05		10974	10974	2.53	0.0	2.0	2.0	87.1	5.6	99.7	90.0	282.5
A6-C	Medium Density Residential	90			4.87	4.87	162.0	789	11763	2.51	0.0	0.0	1.6	87.1	5.6	101.4	95.6	289.6
A6-D	Low Density Residential	90			17.56	17.56	95.2	1672	13435	2.46	0.0	0.0	5.8	87.1	5.6	107.1	107.2	307.0
A6-E	Low Density Residential	90			6.94	6.94	95.2	661	14096	2.44	0.0	0.0	2.3	87.1	5.6	109.4	111.7	313.8
A7-A	Commercial	90	13.62			13.62		14096	14096	2.44	6.6	0.0	4.5	93.7	5.6	113.9	111.7	324.9
A7-B	High Density Residential	90			11.01	11.01	135.0	1486	15582	2.41	0.0	0.0	3.6	93.7	5.6	117.6	121.7	338.5
A7-C	Medium Density Residential	90			6.97	6.97	162.0	1129	16711	2.38	0.0	0.0	2.3	93.7	5.6	119.9	129.2	348.3
A7-D	Medium Density Residential	90			11.74	11.74	162.0	1902	18613	2.35	0.0	0.0	3.9	93.7	5.6	123.7	141.6	364.6
A7-E1/E2	Medium Density Residential	90			9.24	9.24	162.0	1497	20110	2.32	0.0	0.0	3.0	93.7	5.6	126.8	151.2	377.3
A8-A	Commercial	80	28.45			28.45		20110	20110	2.32	13.8	0.0	9.4	107.5	5.6	136.2	151.2	400.5
A8-B	High Density Residential	80			39.34	39.34	135.0	5311	25421	2.24	0.0	0.0	13.0	107.5	5.6	149.2	184.4	446.7
A8-C	Institutional	80		10.52		10.52		25421	25421	2.24	0.0	3.4	3.5	107.5	9.0	152.6	184.4	453.6
A8-D	Low Density Residential	80			16.87	16.87	120.9	2040	27461	2.21	0.0	0.0	5.6	107.5	9.0	168.2	196.9	471.6
ROW Along SNC Sewer Alignment	-	80				14.34			27461	2.21	0.0	0.0	4.7	107.5	9.0	162.9	196.9	476.3
<b>TOTAL</b>		<b>80</b>	<b>221.24</b>	<b>27.77</b>	<b>230.38</b>	<b>493.73</b>	<b>-</b>	<b>27461</b>	<b>27461</b>	<b>2.21</b>	<b>107.5</b>	<b>9.0</b>	<b>162.9</b>	<b>107.5</b>	<b>9.0</b>	<b>162.9</b>	<b>196.9</b>	<b>476.3</b>

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 - 28 (28 used)	2.7 - 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 - 60 (60 used)	2.7	162.0
High Density (apartments)	60 - 75 (75 used)	1.8	135.0

Notes:

- Harmon Equation =  $1 + [14 / (4 + (P/1000)^{1/2})] \times K$   
 Where: P = population; K = correction factor = 0.8
- Commercial Peaking Factor = 1.5; Institutional Peaking Factor = 1.0

Reported Design Flows / Assumptions:

- Area A4: Existing single family units currently serviced by Jockvale pump station to be redirected to SNC
- Area A8-D: proposed 600 medium density residential units

See Note (2) in the DSEL "Barrhaven Conservancy - Evaluation of SNC Flows" design sheet

THE PRIOR NOVATECH SNC DESIGN SHEET HAD FLOWS AT 423.6 L/s AFTER AREA ID "A6-E".  
 THIS UPDATED NOVATECH 'PHASE 3' EVALUATION HAS A FLOW OF 313.8 L/s.  
 THE DSEL EVALUATION OF SANITARY FLOWS WITH THE NEW CITY DESIGN PARAMETERS AT THIS SAME NODE (WITH CONSERVANCY WEST AND EAST INCLUDED) IS ~401.05 L/s (WHICH IS LESS THAN THE PRIOR 423.6 L/s NOTED ABOVE)

SOUTH NEPEAN COLLECTOR (PHASE 3)  
SANITARY SEWER DESIGN SHEET

DECEMBER 5 2018  
JOB# 117190



LOCATION			Area				Population		Cumulative Design Flows					PROPOSED SEWER						
From MH	To MH	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Total Gross Area (ha)	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn <sup>1</sup> )	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (280 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)	Length (m)	Pipe Size (mm)	Type	Slope %	Capacity (L/s)	Full Flow Velocity (m/s)	Ratio (Q/Qfull)
SA 22	SA 21	120	146.27	11.20	105.84	263.31	10974	2.53	71.1	3.6	86.9	90.0	251.7	131.9	750	CONC	0.10	367.3	0.81	69%
SA 21	SA 20	120											251.7	90.6	750	CONC	0.10	367.3	0.81	69%
SA 20	SA 19	120											251.7	90.0	750	CONC	0.10	367.3	0.81	69%
SA 19	SA 18	120											251.7	72.1	750	CONC	0.10	367.3	0.81	69%
SA 18	SA 17	120											251.7	71.9	750	CONC	0.10	367.3	0.81	69%
SA 17	SA 16	120											251.7	71.4	750	CONC	0.10	367.3	0.81	69%
SA 16	SA 15	110	163.99	11.20	105.84	281.03	10974	2.53	79.7	3.6	92.7	90.0	266.1	73.2	750	CONC	0.10	367.3	0.81	72%
SA 15	SA 14	110											266.1	67.5	750	CONC	0.10	367.3	0.81	72%
SA 14	SA 13	110											266.1	56.6	750	CONC	0.10	367.3	0.81	72%
SA 13	SA 12	110											266.1	133.5	750	CONC	0.10	367.3	0.81	72%
SA 12	SA 11	110											266.1	150.0	750	CONC	0.10	367.3	0.81	72%
SA 11	SA 10	100	179.17	17.25	105.84	302.26	10974	2.53	87.1	5.6	99.7	90.0	282.5	97.8	750	CONC	0.10	367.3	0.81	77%
SA 10	SA 9	100											282.5	76.7	750	CONC	0.10	367.3	0.81	77%
SA 9	SA 8	100											282.5	79.7	750	CONC	0.10	367.3	0.81	77%
SA 8	SA 7	100											282.5	75.3	750	CONC	0.10	367.3	0.81	77%
SA 7	SA 6	100											282.5	84.9	750	CONC	0.10	367.3	0.81	77%
SA 6	SA 5	100											282.5	77.1	750	CONC	0.10	367.3	0.81	77%
SA 5	SA 4	100											282.5	78.9	750	CONC	0.10	367.3	0.81	77%
SA 4	SA 3	100											282.5	80.5	750	CONC	0.10	367.3	0.81	77%
SA 3	SA 2	100											282.5	150.0	750	CONC	0.10	367.3	0.81	77%
SA 2	SA 1	100											282.5	114.6	750	CONC	0.10	367.3	0.81	77%
SA 1	EX 80	100											282.5	12.4	750	CONC	0.10	367.3	0.81	77%

Design Parameters:

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles / semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row / townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

Notes:

- Harmon Equation =  $1 + [14 / (4 + (P/1000)^{1/2})] \times K$   
Where: P = population; K = correction factor = 0.8
- Commercial Peaking Factor = 1.5; Institutional Peaking Factor = 1.0

Reported Design Flows / Assumptions:

- Area A4: Existing single family units currently serviced by Jockvale pump station to be redirected to SNC
- Area A8-D: proposed 600 medium density residential units



# MEMORANDUM

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**DATE:** MAY 26, 2016  
**TO:** JONATHAN KNOYLE – CITY OF OTTAWA  
**FROM:** CONRAD STANG – NOVATECH  
**RE:** SOUTH NEPEAN COLLECTOR PHASE 2: SANITARY FLOW CALCULATIONS  
**CC:** EDSON DONNELLY – NOVATECH

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## 1.0 PURPOSE

This memorandum provides the sanitary sewer flow calculations and design sheet for Phase 2 of the proposed South Nepean Collector (SNC). Sanitary design flows have been estimated for both current-day operational flows and future development peak design flows, based on the latest available planning information for the vacant lands within the SNC sewershed.

## 2.0 BACKGROUND

In January 1998, the Master Servicing Study for the South Nepean Urban Area provided a conceptual plan for water, wastewater and stormwater infrastructure. The preferred alternative for wastewater servicing was an east/west trunk sewer alignment that was to be completed in several phases. The proposed sanitary trunk sewer was initially called the Jock River Collector, but was renamed the South Nepean Collector during the original functional design study completed in 2003.

Phase 1 of the South Nepean Collector was completed in 2005 and currently terminates at a 2400mm maintenance hole located east of Longfields Drive, north of Bren-Maur Road. Phase 2 will extend the trunk sewer to Strandherd Drive at the intersection of the proposed transitway along the proposed extension to Chapman Mills Drive. Phase 3 will extend the trunk sewer along Strandherd Drive to the intersection of Maravista Drive.

The sanitary sewer flows were previously documented in the *South Nepean Collector – Functional Design Report and Update* (Dillon, 2012). A review of the sanitary flows provided in the Dillon Report based on the latest planning information for the vacant lands within the SNC sewershed was documented in the technical memorandum titled *South Nepean Collector Phase 2: Hydraulics Review / Assessment* (Novatech, 2015), which is attached to this memorandum. The results of the *Hydraulics Review / Assessment* (Novatech, 2015) were very similar to the results from the Dillon (2012) analysis.



### 3.0 DESIGN PARAMETERS AND POPULATION ESTIMATES

#### 3.1 Design Parameters

The sanitary design flow were calculated using the parameters from the City of Ottawa Sewer Design Guidelines (October 2012), and are summarized in **Table 1** and **Table 2**.

**Table 1: Peak Design Flow Parameters**

Land Use	Average Daily Flow	Peaking Factor	Peak Extraneous Flows
Residential	350 L/cap/day	Harmon Equation, K=1 (2.0 min – 4.0 max)	0.28 L/s/ha
Commercial	50,000 L/ha/day	1.5	
Institutional	50,000 L/ha/day	1.5	
Other*	0 L/ha/day	N/A	

\*Open Space, Arterial ROW, SWM Blocks, etc. with no sanitary flow contribution (extraneous flow only)

**Table 2: Operational Design Flow Parameters**

Land Use	Average Daily Flow	Peaking Factor	Peak Extraneous Flows
Residential	300 L/cap/day	Harmon Equation, K=0.6 (1.2 min – 2.4 max)	<u>Dry weather</u> 0.05-0.08 L/s/ha
Commercial	17,000 L/ha/day	1.0 (non-coincident peak)	<u>Wet Weather</u> 0.15 - 0.20 L/s/ha (typical events) 0.28 L/s/ha (large/annual events) 0.30 - 0.50 L/s/ha (extreme events)
Institutional	10,000 L/ha/day	1.0 (non-coincident peak)	

\*There are no industrial areas identified within the tributary area.

$$\text{Harmon Equation} = 1 + \frac{14}{4 + \left(\frac{P}{1000}\right)^{\frac{1}{2}}} \times K$$

Where:

P = Population

K = Correction Factor:

- Peak Flow = 1
- Operational = between 0.4 to 0.6 (0.6 used)

#### 3.2 Land Use Designations & Population Estimates

Population densities and unit counts for future residential development are based on the current concept plans for these areas, and are presented in **Table 3**.

**Table 3: Residential Land Use Population Densities**

Residential Land Use	Units per ha	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

The land use designations shown in **Table 4** have been applied for the areas within Phases 2 and 3 of the SNC (Node 70 to 130). The sewershed areas and land use designations were delineated using aerial photos (existing development) and conceptual site plans (future development).

**Table 4: Land Use Designations**

Land Use Designation	
Secondary Plan	SNC Design
Residential	Residential (Low / Medium / High Density)
Institutional / Office	Institutional
Commercial	Commercial
Recreational	
Business Park	
Prestige Business Park	
Park/Open Space Area	Other*
Ex. Snow Disposal Facility (future commercial)	
Stormwater Management Facility	
Conservation Lands	
Arterial Right-of-Ways	

\* No sanitary flow contribution - extraneous flows (inflow/infiltration) only.

The overall residential population estimate and sewershed area for Phases 2 and 3 of the SNC is provided in **Table 5** below. It is assumed that the snow dump facility at the Stranderd Drive and McKenna Casey Drive will ultimately be re-zoned for commercial development.

**Table 5: Population Estimates and Areas**

Existing / Future	Estimated Population / Area	Novatech (2015)
Existing	Estimated Population	6,944 persons
	Gross Residential Area	60.09 ha
	Gross Commercial / Institutional Area	64.37 ha
	<i>Total Sewershed Area</i>	124.5 ha
Future (full service)	Estimated Population	27,312 persons
	Gross Residential Area	248.48 ha
	Gross Commercial / Institutional Area	228.82 ha
	<i>Total Sewershed Area</i>	477.3 ha

#### 4.0 SANITARY DESIGN FLOWS

The sanitary flow allocations for Phases 2 and 3 of the SNC are provided in **Table 6**. The corresponding sanitary drainage area plan is provided as **Figure 1**. Sanitary sewer flow calculations for Phases 2 and 3 and detailed sanitary sewer design sheets for Phase 2 are attached to this memorandum.

The estimated sanitary design flows from Phases 2 and 3 of the SNC (entering Node 70) are as follows:

- Present-Day Operational Design Flows (Theoretical) = 72.5 L/s
- Future Peak Design Flows = 634.2 L/s

The outlet for Phase 2 of the SNC is the existing 1050mm outlet pipe at the 2400mm maintenance hole (Node 70) located east of Longfields Drive, north of Bren-Maur Road. Given a minimum design slope of 0.10%, this sanitary trunk sewer would have a full flow capacity of 900.5 L/s. Therefore, the downstream sanitary trunk sewer would be at 70% capacity, based on the future peak design flow being 634.2 L/s.

#### **ATTACHMENTS:**

- Figure 1: Sanitary Drainage Areas and Land Use
- Sanitary Sewer Flow Calculations
- Sanitary Sewer Design Sheets (Phase 2)
- South Nepean Collector Phase 2: Hydraulics Review / Assessment (Novatech, 2015)



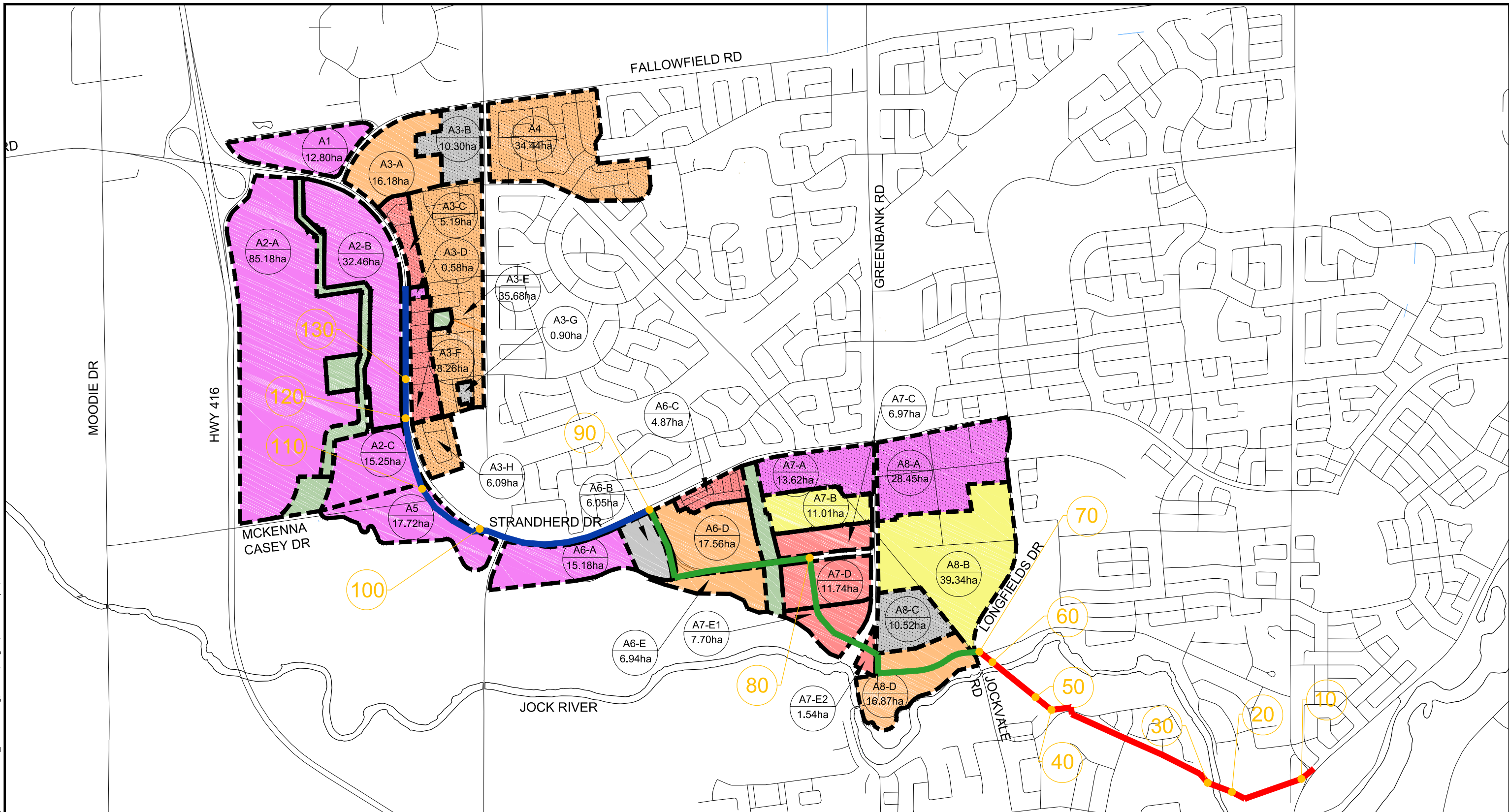
**Table 6: Updated Allocation of Commercial, Institutional and Residential Demands to Phases 2 & 3 (Nodes 70 – 130) of the SNC by Collection Area**

Collection Area	Upstream Node	Existing / Proposed Development	Existing / Proposed Land Use	Area (ha)	Estimated Number of Residential Units	Population Density (persons / ha)	Comment	Reference
A1	130	Proposed	Commercial	12.80	-	-	O'Keefe Court – Conceptual site plan shows proposed commercial.	Conceptual Plans for O'Keefe Court
A2-A	130	Proposed	Commercial	85.18	-	-	CitiGate – Analysis uses same approach as the design for CitiGate.	Detailed Servicing and SWM Report (Phase 1) (Novatech, 2014)
A2-B	130	Proposed	Commercial	32.46	-	-		
A2-C	120	Proposed	Commercial (ex. Snow dump)	15.25	-	-	Existing snow dump facility assumed to be future commercial.	Functional Design Report and Update – SNC Phase 2 and 3 (Dillon, 2012)
A3-A	130	Proposed	Low Density Residential	16.48	461	95.2	Havencrest – Existing single family units.	Havencrest Design Report (IBI, 2013)
A3-B	130	Existing	Institutional	10.30	-	-	Cedarview Middle School and Cedarview Alliance Church.	Aerial Photos / Site Visits
A3-C	130	Existing	Medium Density Residential	5.19	311	162	Existing townhouse units.	
A3-D	130	Existing	Commercial	0.58	-	-	Existing commercial buildings.	
A3-E	130	Existing	Low Density Residential	35.68	999	95.2	Existing single family units.	
A3-F	130	Existing	Medium Density Residential	8.26	496	162.0	Existing townhouse units.	
A3-G	130	Existing	Institutional	0.90	-	-	Ottawa Torah Centre Chibad.	
A3-H	120	Existing	Low Density Residential	6.09	171	95.2	Existing single family units.	
A4	130	Existing	Low Density Residential	34.44	964	95.2	Existing single family units currently serviced by Jockvale pump station; to be redirected to SNC.	
A5	110	Proposed	Commercial	17.72	-	-	Proposed commercial south of McKenna Casey Drive.	Site Visits
A6-A	100	Proposed	Institutional	20.70	-	-	Proposed school site on Minto property.	Conceptual Plan for Lands Adjacent the Kennedy-Burnett SWMF provided by Minto (2015)
A6-B	90	Existing	Medium Density Residential	4.87	292	162.0	Existing townhouse units.	Aerial Photos / Site Visits
A6-C	90	Proposed	Low Density Residential	10.11	283	95.2	Proposed single family units on lands owned by Minto.	Conceptual Plans for Lands Adjacent the Kennedy-Burnett SWMF provided by land owners.
A6-D	90	Proposed	Low Density Residential	5.59	157	95.2	Proposed single family units on lands owned by Mion.	
A6-E	90	Proposed	Low Density Residential	7.24	203	95.2	Proposed single family units on lands owned by Pavic / Braovac.	
A7-A	80	Existing	Commercial	13.62	-	-	Existing large retail stores (commercial).	Aerial Photos
A7-B	80	Proposed	High Density Residential	11.01	826	135.0	Proposed high density units on lands owned by Richcraft / Trinity.	Conceptual Plans for Lands Adjacent the Kennedy-Burnett SWMF provided by land owners.
A7-C	80	Proposed	Medium Density Residential	6.97	418	162.0	Proposed Medium density units on lands owned by Mion.	
A7-D	80	Proposed	Medium Density Residential	11.74	704	162.0	Proposed Medium density units on lands owned by Caivan.	
A7-E1/E2	80	Proposed	Medium Density Residential	9.24	554	162.0	Proposed Medium density units on lands owned by Claridge.	
A8-A	80	Existing	Commercial	28.45	-	-	Existing Barrhaven Market Place (commercial).	Aerial Photos / Site Visits
A8-B	80	Proposed	High Density Residential	39.34	2951	135.0	Future development similar to Ampersands development.	Site Visits
A8-C	80	Existing	Institutional	10.52	-	-	Existing St. Joseph High School.	Aerial Photos / Site Visits
A8-D	80	Proposed	Low Density Residential	16.87	1012	162.0	Proposed 600 low density residential units.	Functional Design Report and Update – SNC Phase 2 and 3 (Dillon, 2012)

Attachment 1  
Sanitary Drainage Areas and Land Use

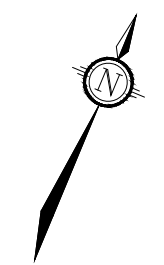


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**LEGEND**

- EXISTING / PROPOSED HIGH DENSITY RESIDENTIAL
- EXISTING / PROPOSED MEDIUM DENSITY RESIDENTIAL
- EXISTING / PROPOSED LOW DENSITY RESIDENTIAL
- EXISTING / PROPOSED COMMERCIAL
- EXISTING / PROPOSED INSTITUTIONAL
- OTHER LANDS (OPEN SPACE, PARKS, AND SWMFS)
- SOUTH NEPEAN COLLECTOR PHASE 1
- SOUTH NEPEAN COLLECTOR PHASE 2
- SOUTH NEPEAN COLLECTOR PHASE 3
- SOUTH NEPEAN COLLECTOR NODE ID



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**SOUTH NEPEAN COLLECTOR SEWER**  
**SANITARY DRAINAGE AREAS AND LAND USE**

SCALE 1:20 000

DATE MAY 2016 JOB 115075 FIGURE FIG. 1

Attachment 2  
Sewer Flow Calculations



PROJECT #: 115075  
DESIGNED BY: CMS  
CHECKED BY: MJP  
DATE: August 20, 2015

**SANITARY SEWER DESIGN SHEET**

**South Nepean Collector - Phase 2 & 3**

Theoretical Current Operational Peak Wastewater Flow



Location			Areas				Population				Individual Design Flows			Cumulative Design Flows				
Area I.D.	Existing Land Use	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Total Gross Area (ha)	Residential Population Density (people / ha)	Individual Residential Population	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn <sup>1</sup> )	Commercial Peak Flow Rate <sup>2</sup> (17,000 L/ha/d) (L/s)	Institutional Peak Flow Rate <sup>2</sup> (10,000 L/ha/d) (L/s)	Infiltration / Inflow Rate (0.05 L/s/ha) (L/s)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (300 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)
A1	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A2-A	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A2-B	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A3-A	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A3-B	Institutional	130		10.30		10.30					0.0	1.2	0.5	0.0	1.2	0.5	0.0	1.7
A3-C	Medium Density Residential	130			5.19	5.19	162.0	841	841	2.71	0.0	0.0	0.3	0.0	1.2	0.8	7.9	9.9
A3-D	Commercial	130	0.58			0.58		841	841	2.71	0.1	0.0	0.0	0.1	1.2	0.8	7.9	10.0
A3-E	Low Density Residential	130			35.68	35.68	95.2	3397	4238	2.39	0.0	0.0	1.8	0.1	1.2	2.6	35.1	39.0
A3-F	Medium Density Residential	130			8.26	8.26	162	1338	5576	2.32	0.0	0.0	0.4	0.1	1.2	3.0	44.9	49.2
A3-G	Institutional	130		0.90		0.90			5576	2.32	0.0	0.1	0.0	0.1	1.3	3.0	44.9	49.4
A4	Low Density Residential*	130				0.00			5576	2.32	0.0	0.0	0.0	0.1	1.3	3.0	44.9	49.4
A2-C	Snow Dump Facility	120				0.00			5576	2.32	0.0	0.0	0.0	0.1	1.3	3.0	44.9	49.4
A3-H	Low Density Residential	120			6.09	6.09	95.2	580	6155	2.30	0.0	0.0	0.3	0.1	1.3	3.4	49.1	53.8
A5	Open Space	110				0.00			6155	2.30	0.0	0.0	0.0	0.1	1.3	3.4	49.1	53.8
A6-A	Open Space	100				0.00			6155	2.30	0.0	0.0	0.0	0.1	1.3	3.4	49.1	53.8
A6-B	Open Space	100				0.00			6155	2.30	0.0	0.0	0.0	0.1	1.3	3.4	49.1	53.8
A6-C	Medium Density Residential	90			4.87	4.87	162.0	789	6944	2.27	0.0	0.0	0.2	0.1	1.3	3.6	54.6	59.6
A6-D	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	0.1	1.3	3.6	54.6	59.6
A6-E	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	0.1	1.3	3.6	54.6	59.6
A7-A	Commercial	90	13.62			13.62			6944	2.27	2.7	0.0	0.7	2.8	1.3	4.3	54.6	63.0
A7-B	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	1.3	4.3	54.6	63.0
A7-C	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	1.3	4.3	54.6	63.0
A7-D	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	1.3	4.3	54.6	63.0
A7-E1/E2	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	1.3	4.3	54.6	63.0
A8-A	Commercial	80	28.45			28.45			6944	2.27	5.6	0.0	1.4	8.4	1.3	5.7	54.6	70.0
A8-B	Open Space	80				0.00			6944	2.27	0.0	0.0	0.0	8.4	1.3	5.7	54.6	70.0
A8-C	Institutional	80		10.52		10.52			6944	2.27	0.0	1.2	0.5	8.4	2.5	6.2	54.6	71.8
A8-D	Open Space	80				0.00			6944	2.27	0.0	0.0	0.0	8.4	2.5	6.2	54.6	71.8
ROW Along SNC Sewer Alignment	-	80				14.34			6944	2.27	0.0	0.0	0.7	8.4	2.5	6.9	54.6	72.5
<b>TOTAL</b>		<b>80</b>	<b>42.65</b>	<b>21.72</b>	<b>60.09</b>	<b>138.80</b>	<b>-</b>	<b>6944</b>	<b>6944</b>	<b>2.27</b>	<b>8.4</b>	<b>2.5</b>	<b>6.9</b>	<b>8.4</b>	<b>2.5</b>	<b>6.9</b>	<b>54.6</b>	<b>72.5</b>

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

Notes:

- Harmon Equation =  $1 + [14 / (4 + (P/1000)^{1/2})] \times K$   
Where: P = population; K = correction factor = 0.6
- Institutional / Commercial Peaking Factor = 1.0

Reported Design Flows / Assumptions:

- Area A4: Existing single family units currently serviced by Jockvale pump station; currently not directed to SNC

PROJECT #: 115075  
 DESIGNED BY: CMS  
 CHECKED BY: MJP  
 DATE: August 20, 2015

**SANITARY SEWER DESIGN SHEET**

**South Nepean Collector - Phase 2 & 3**

Theoretical Future Full Service Peak Wastewater Flow



Location			Areas				Population				Individual Design Flows			Cumulative Design Flows				
Area I.D.	Existing / Proposed Land Use	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Total Gross Area (ha)	Residential Population Density (people / ha)	Individual Residential Population	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn <sup>1</sup> )	Commercial Peak Flow Rate <sup>2</sup> (50,000 L/ha/d) (L/s)	Institutional Peak Flow Rate <sup>2</sup> (50,000 L/ha/d) (L/s)	Infiltration / Inflow Rate (0.28 L/s/ha) (L/s)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (350 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)
A1	Commercial	130	12.80			12.80					11.1	0.0	3.6	11.1	0.0	3.6	0.0	14.7
A2-A	Commercial	130	85.18			85.18					73.9	0.0	23.9	85.1	0.0	27.4	0.0	112.5
A2-B	Commercial	130	32.46			32.46					28.2	0.0	9.1	113.2	0.0	36.5	0.0	149.8
A3-A	Low Density Residential	130			16.18	16.18	95.2	1540	1540	3.67	0.0	0.0	4.5	113.2	0.0	41.1	22.9	177.2
A3-B	Institutional	130		10.30		10.30		1540	1540	3.67	0.0	8.9	2.9	113.2	8.9	43.9	22.9	189.0
A3-C	Medium Density Residential	130			5.19	5.19	162.0	841	2381	3.53	0.0	0.0	1.5	113.2	8.9	45.4	34.0	201.6
A3-D	Commercial	130	0.58			0.58		2381	2381	3.53	0.5	0.0	0.2	113.7	8.9	45.6	34.0	202.2
A3-E	Low Density Residential	130			35.68	35.68	95.2	3397	5778	3.19	0.0	0.0	10.0	113.7	8.9	55.5	74.6	252.8
A3-F	Medium Density Residential	130			8.26	8.26	162	1338	7116	3.10	0.0	0.0	2.3	113.7	8.9	57.9	89.4	269.9
A3-G	Institutional	130		0.90		0.90		7116	7116	3.10	0.0	0.8	0.3	113.7	9.7	58.1	89.4	270.9
A4	Low Density Residential	130			34.44	34.44	95.2	3279	10395	2.94	0.0	0.0	9.6	113.7	9.7	67.8	123.7	314.9
A2-C	Commercial (ex. snow dump)	120	15.25			15.25		10395	10395	2.94	13.2	0.0	4.3	127.0	9.7	72.0	123.7	332.4
A3-H	Low Density Residential	120			6.09	6.09	95.2	580	10974	2.91	0.0	0.0	1.7	127.0	9.7	73.7	129.6	340.0
A5	Commercial	110	17.72			17.72		10974	10974	2.91	15.4	0.0	5.0	142.4	9.7	78.7	129.6	360.3
A6-A	Commercial	100	15.18			15.18		10974	10974	2.91	13.2	0.0	4.3	155.5	9.7	82.9	129.6	377.8
A6-B	Institutional	100		6.05		6.05		10974	10974	2.91	0.0	5.3	1.7	155.5	15.0	84.6	129.6	384.7
A6-C	Medium Density Residential	90			4.87	4.87	162.0	789	11763	2.88	0.0	0.0	1.4	155.5	15.0	86.0	137.4	393.9
A6-D	Low Density Residential	90			17.56	17.56	95.2	1672	13435	2.83	0.0	0.0	4.9	155.5	15.0	90.9	153.8	415.2
A6-E	Low Density Residential	90			6.94	6.94	95.2	661	14096	2.81	0.0	0.0	1.9	155.5	15.0	92.9	160.2	423.6
A7-A	Commercial	90	13.62			13.62		14096	14096	2.81	11.8	0.0	3.8	167.4	15.0	96.7	160.2	439.2
A7-B	High Density Residential	90			11.01	11.01	135.0	1486	15582	2.76	0.0	0.0	3.1	167.4	15.0	99.8	174.3	456.4
A7-C	Medium Density Residential	90			6.97	6.97	162.0	1129	16711	2.73	0.0	0.0	2.0	167.4	15.0	101.7	184.9	468.9
A7-D	Medium Density Residential	90			11.74	11.74	162.0	1902	18613	2.68	0.0	0.0	3.3	167.4	15.0	105.0	202.4	489.7
A7-E1/E2	Medium Density Residential	90			9.24	9.24	162.0	1497	20110	2.65	0.0	0.0	2.6	167.4	15.0	107.6	215.9	505.8
A8-A	Commercial	80	28.45			28.45		20110	20110	2.65	24.7	0.0	8.0	192.0	15.0	115.5	215.9	538.5
A8-B	High Density Residential	80			39.34	39.34	135.0	5311	25421	2.55	0.0	0.0	11.0	192.0	15.0	126.6	262.4	596.0
A8-C	Institutional	80		10.52		10.52		25421	25421	2.55	0.0	9.1	2.9	192.0	24.1	129.5	262.4	608.1
A8-D	Low Density Residential	80			16.87	16.87	120.9	2040	27461	2.52	0.0	0.0	4.7	192.0	24.1	134.2	279.8	630.2
ROW Along SNC Sewer Alignment	-	80				14.34			27461	2.52	0.0	0.0	4.0	192.0	24.1	138.2	279.8	634.2
<b>TOTAL</b>		<b>80</b>	<b>221.24</b>	<b>27.77</b>	<b>230.38</b>	<b>493.73</b>	<b>-</b>	<b>27461</b>	<b>27461</b>	<b>2.52</b>	<b>192.0</b>	<b>24.1</b>	<b>134.2</b>	<b>192.0</b>	<b>24.1</b>	<b>138.2</b>	<b>279.8</b>	<b>634.2</b>

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

Notes:

- Harmon Equation =  $1 + [14 / (4 + (P/1000)^{1/2})] \times K$   
 Where: P = population; K = correction factor = 1.0
- Institutional / Commercial Peaking Factor = 1.5

Reported Design Flows / Assumptions:

- Area A4: Existing single family units currently serviced by Jockvale pump station to be redirected to SNC
- Area A8-D: proposed 600 medium density residential units

**THIS PRIOR NOVATECH SNC DESIGN SHEET HAD DESIGN FLOWS AT 423.6 L/S AFTER AREA ID "A6-E".**

**THE DSEL EVALUATION WITH NEW PARAMETERS AT THIS SAME NODE WITH CONSERVANCY WEST AND EAST INCLUDED IS ~401.05 < 423.6 L/S**

Attachment 3  
Sanitary Sewer Design Sheets (Phase 2)

SOUTH NEPEAN COLLECTOR (PHASE 2)  
SANITARY SEWER DESIGN SHEET

MAY 26, 2016  
JOB# 115075



LOCATION			Area					Population				Individual Design Flows			Cumulative Design Flows				PROPOSED SEWER							
From MH	To MH	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Right-of-Way (ha)	Total Gross Area (ha)	Residential Population Density (people / ha)	Individual Residential Population	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn <sup>1</sup> )	Commercial Peak Flow Rate <sup>2</sup> (50,000 L/ha/d) (L/s)	Institutional Peak Flow Rate <sup>2</sup> (50,000 L/ha/d) (L/s)	Infiltration / Inflow Rate (0.28 L/s/ha) (L/s)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (350 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)	Length (m)	Pipe Size (mm)	Type	Slope %	Capacity (L/s)	Full Flow Velocity (m/s)	Ratio (Q/Qfull)
MHSA 1	MHSA 2	90	192.79	17.25	174.17	0.00	384.21	1678	20110	20110	2.65	167.352	14.97	107.58	167.4	15.0	107.6	215.9	505.8	57.3	900	CONC	0.10	597.2	0.91	85%
MHSA 2	MHSA 3	90																	505.8	57.3	900	CONC	0.10	597.2	0.91	85%
MHSA 3	MHSA 4	90																	505.8	73.9	900	CONC	0.10	597.2	0.91	85%
MHSA 4	MHSA 5	90																	505.8	34.6	900	CONC	0.10	597.2	0.91	85%
MHSA 5	MHSA 6	90																	505.8	42.8	900	CONC	0.10	597.2	0.91	85%
MHSA 6	MHSA 7	90																	505.8	84.4	900	CONC	0.10	597.2	0.91	85%
MHSA 7	MHSA 8	90																	505.8	16.5	900	CONC	0.10	597.2	0.91	85%
MHSA 8	MHSA 9	90																	505.8	85.4	900	CONC	0.10	597.2	0.91	85%
MHSA 9	MHSA 10	90																	505.8	70.6	900	CONC	0.10	597.2	0.91	85%
MHSA 10	MHSA 11	90																	505.8	70.6	900	CONC	0.10	597.2	0.91	85%
MHSA 11	MHSA 12	90																	505.8	77.8	900	CONC	0.10	597.2	0.91	85%
MHSA 12	MHSA 13	90																	505.8	77.8	900	CONC	0.10	597.2	0.91	85%
MHSA 13	MHSA 14	90																	505.8	77.8	900	CONC	0.10	597.2	0.91	85%
MHSA 14	MHSA 15	90																	505.8	25.4	900	CONC	0.10	597.2	0.91	85%
MHSA 15	MHSA 16	90																	505.8	34.2	900	CONC	0.10	597.2	0.91	85%
MHSA 16	MHSA 17	90																	505.8	86.7	900	CONC	0.10	597.2	0.91	85%
MHSA 17	MHSA 18	90																	505.8	34.3	900	CONC	0.10	597.2	0.91	85%
MHSA 18	MHSA 19	90																	505.8	68.6	900	CONC	0.10	597.2	0.91	85%
MHSA 19	MHSA 20	90																	505.8	65.5	900	CONC	0.10	597.2	0.91	85%
MHSA 20	MHSA 21	80	221.24	27.77	230.38	14.34	493.73	256	7351	27461	2.52	192.049	24.11	138.24	192.0	24.1	138.2	279.8	634.2	18.2	1050	CONC	0.10	900.9	1.01	70%
MHSA 21	MHSA 22	80																	634.2	81.9	1050	CONC	0.10	900.9	1.01	70%
MHSA 22	MHSA 23	80																	634.2	84.7	1050	CONC	0.10	900.9	1.01	70%
MHSA 23	MHSA 24	80																	634.2	77.4	1050	CONC	0.10	900.9	1.01	70%
MHSA 24	MHSA 25	80																	634.2	45.5	1050	CONC	0.10	900.9	1.01	70%
MHSA 25	MHSA 26	80																	634.2	35.8	1050	CONC	0.10	900.9	1.01	70%
MHSA 26	MHSA 27	80																	634.2	83.3	1050	CONC	0.10	900.9	1.01	70%
MHSA 27	MHSA 28	80																	634.2	74.4	1050	CONC	0.10	900.9	1.01	70%
MHSA 28	MHSA 29	80																	634.2	77.3	1050	CONC	0.10	900.9	1.01	70%
MHSA 29	MHSA 30	80																	634.2	83.8	1050	CONC	0.10	900.9	1.01	70%
MHSA 30	MHSA 31	80																	634.2	42.3	1050	CONC	0.10	900.9	1.01	70%
MHSA 31	MHSA 32	80																	634.2	100.6	1050	CONC	0.10	900.9	1.01	70%
MHSA 32	MHSA 33	80																	634.2	13.9	1050	CONC	0.10	900.9	1.01	70%
MHSA 33	MHSA 34	80																	634.2	99.9	1050	CONC	0.10	900.9	1.01	70%
MHSA 34	MHSA 35	80																	634.2	99.9	1050	CONC	0.10	900.9	1.01	70%
MHSA 35	MHSA 36	80																	634.2	88.7	1050	CONC	0.10	900.9	1.01	70%
MHSA 36	MHSA 37	80																	634.2	88.8	1050	CONC	0.10	900.9	1.01	70%
MHSA 37	MHSA 38	80																	634.2	90.3	1050	CONC	0.10	900.9	1.01	70%
MHSA 38	MHSA 39	80																	634.2	87.5	1050	CONC	0.10	900.9	1.01	70%

Design Parameters:

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles / semis)	26 - 28 (28 used)	2.7 - 3.4 (3.4 used)	95.2
Medium Density (row / townhouse)	50 - 60 (60 used)	2.7	162.0
High Density (apartments)	60 - 75 (75 used)	1.8	135.0

Notes:

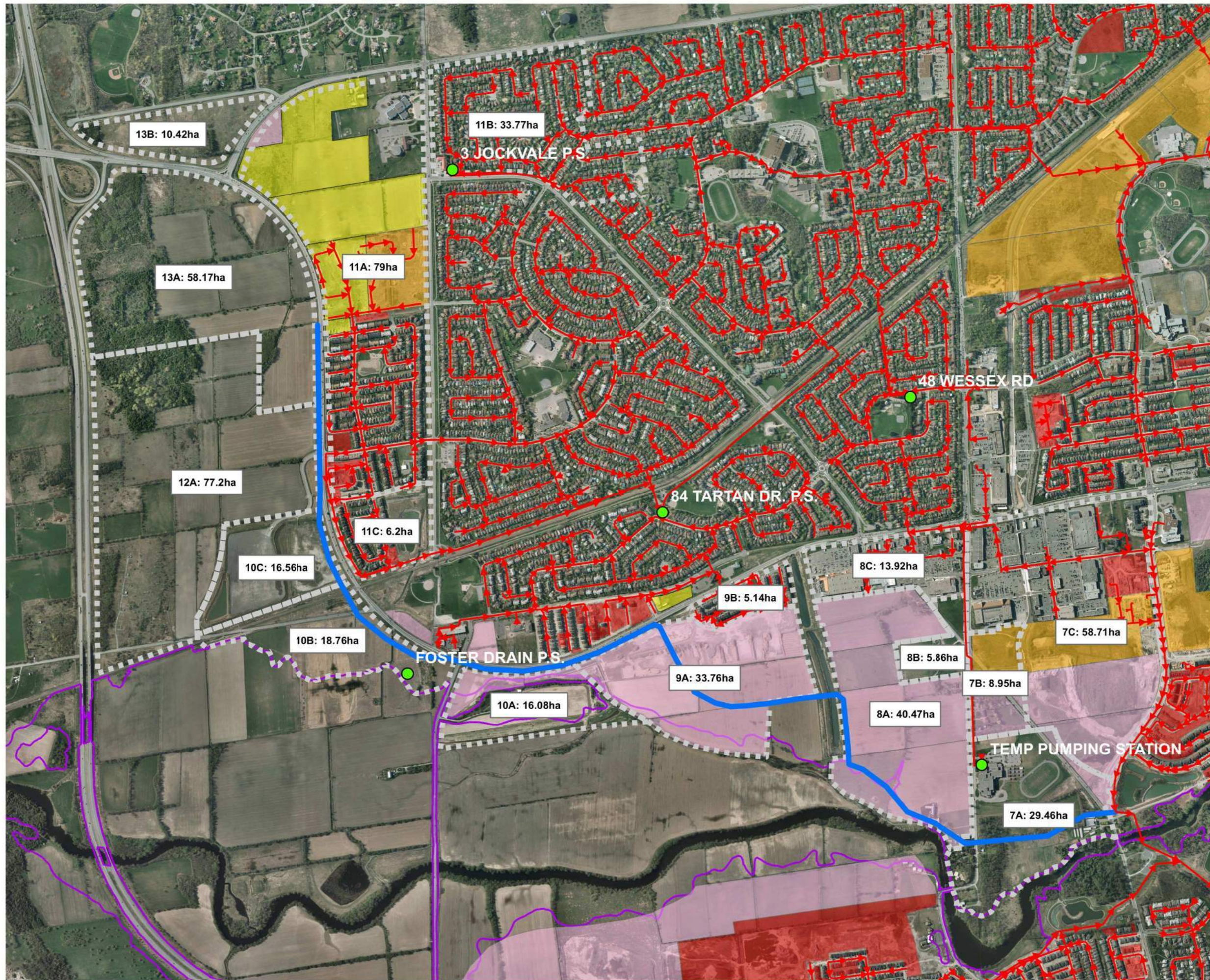
- Harmon Equation =  $1 + [14 / (4 + (P/1000)^{1/2})] \times K$   
Where: P = population; K = correction factor = 1.0
- Institutional / Commercial Peaking Factor = 1.5

Reported Design Flows / Assumptions:

- Area A4: Existing single family units currently serviced by Jockvale pump station to be redirected to SNC
- Area A8-D: proposed 600 medium density residential units



**Figure 01**  
Existing Sanitary Network and Collection Areas



- Pump Station
  - Existing Sanitary Main (With Flow Direction)
  - Proposed Alignment for South Nepean Collector
  - Collection Area
- DEVELOPMENT STATUS**
- Registered
  - Draft Approved
  - Pending
  - No Plan
  - Floodplain

NOT TO SCALE



MAP DRAWING INFORMATION:  
DATA PROVIDED BY THE CITY OF OTTAWA

MAP CREATED BY: BC  
MAP CHECKED BY: MBM  
MAP PROJECTION: NO PROJECTION

FILE LOCATION: \\Dillon.ca\dillon\_dfs\Ottawa\Ottawa\_CA\CAD\2011\115681\Design\_GIS\MXD\Figure01c\_ExistingSanitaryNetwork.mxd



**Table 5.1: Allocation of Commercial/Institutional and Residential Demands to SNC by Collection Area**

Collection Area	Discharging Node	Estimated from GIS			City of Ottawa VURL Data			Other Space <sup>1</sup> (ha)	Population (PE)	Residential Density (PE/net ha)	Comments	Additional Source(s)
		Gross Institutional/Commercial (ha)	Gross Residential (ha)	Gross Area (ha)	Net Residential (ha)	Units (#)	Unit Density (#/ha)					
7A	70	13.5	7.4	29.5	4.0	605	0.3	9.1	1637	4.25	Flow calculations include St Joseph H.S. Pump Station firm capacity of 7.0 L/s Additional 600 units (TAC)	3.4ppu (TAC)
7B		0.0	9.24	9.24	6.23	1474	136.7	3.0	3321	638.8	Population from split VURL allocated by area. VURL parcel id 323 - inconsistency between net and gross reported area.	2.7ppu (TAC)
8A		0.0	40.0	40.0	24.1	4462	185.1	15.9	12047.4	499.9		2.7ppu (TAC)
8B		5.9	0.0	5.9	0.0	0	0	0.0			Future Commercial area	
8C		13.9	0.0	13.9	0.0	0	0	0.0			Commercial area includes Home Depot	
9A	80	0.0	33.8	33.8	18.6	635	34.1	15.2	2210	116.2		3.4ppu (TAC)
10A	90	0.0	16.1	16.1	9.7	451	28.0	6.4	1533.4	158.0	Assume net population = 60% gross.	3.4ppu (TAC)
10B	100	18.8	0.0	35.3	0.0	0	0	16.5			Allocated as potential future I/C use as directed by TAC	
10C	110	16.6	0.0	35.3	0.0	0	0	18.7			Area includes current Municipal Snow Dump. Flow allowance is made for potential future I/C use	
11C		0.0	6.2	6.2	Note 2			2.5	306	82.7	This area is south of '11 block' in the existing development	From IBI Apr 2010 Report Figure 1
11A	120	12.5	66.5	79.0				26.6	3923	98.3	Institutional includes 4.38ha church site and 6.89 ha institution at northeast corner, as well and Claridge Commercial (0.56ha) and DCR/Phoenix Commercial (0.64ha)	From IBI Apr2010 Report Figure 1
11B		0.0	37.0	37.0				14.8	1550	69.8	Presently serviced by Jockvale pump station; to be redirected to SNC.	Estimated from 2011 Census Block data
12A		77.2	0.0	77.2				0.0			Allow sanitary peak flow 79.0 L/s	Novatech, Employment Lands Report, Revised Jan 2012
13A	130	58.5	0.0	58.5				0.0			Allow sanitary peak flow 62.8 L/s plus Collection Area 13B, total 82.2 L/s	
13B		12.5	0.0	12.5	0.0			Allow sanitary peak flow 19.4 L/s; gravity discharge to Collection Area 13A	IBI/Novatech			

Notes:

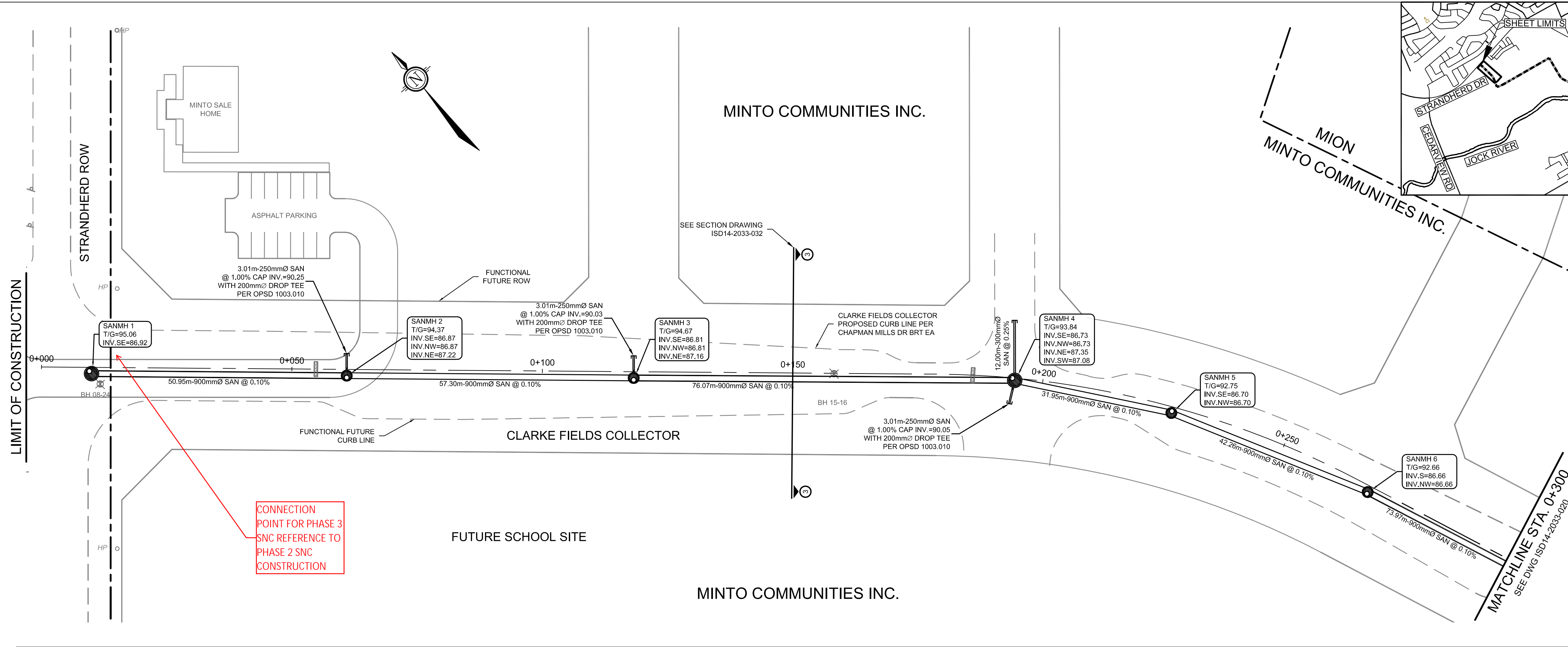
1. Other space includes other residential space accounting for the difference between gross area (measured with GIS) and net area (provided in VURL data), such as sidewalks, roads, greenspace, etc.
2. Collection Area 11A and 11B population and land use as identified under Additional Source(s). Other space reported as 60% of gross residential area, consistent with VURL average.











**CITY OF OTTAWA**  
**SOUTH NEPEAN COLLECTOR (SNC)**  
**SEWER PHASE 2 - STRANDHERD DRIVE**  
**TO JOCKVALE ROAD**

**PLAN AND PROFILE**  
**STA. 0+000 TO 0+300**

Contract No. **ISD14-2033** Dwg. No. **019**  
 Sheet **19** of **51**

Asset No. \_\_\_\_\_  
 Asset Group **ISD**

Wayne Newell, P. Eng. General Manager  
 Jonathan Knoyle, P. Eng. Senior Engineer

**NOVATECH**  
 Engineers, Planners & Landscape Architects  
 Suite 202, 240 Michael Coopers Drive  
 Kanata, Ontario, Canada, K2M 1P6  
 Telephone: (613) 254-9643  
 Facsimile: (613) 254-5867  
 Email: novatech@novatech-eng.com

**PROFESSIONAL ENGINEER**  
**M.A. BISSETT**  
 PROVINCE OF ONTARIO

Des. **RJD** Chk'd. **ERD**  
 Dwn. **NCS** Chk'd. **RJD**  
 Utility Circ. No. \_\_\_\_\_ Index No. \_\_\_\_\_  
 Const. Inspector \_\_\_\_\_

Scale: HORIZONTAL 1:500  
 VERTICAL 1:100

**NOTE:** The location of utilities is approximate only, the exact location should be determined by consulting the municipal authorities and utility companies concerned. The contractor shall prove the location of utilities and shall be responsible for adequate protection from damage.

No.	Description	By	Date (dd/mm/yyyy)
1.	ISSUED FOR PRELIMINARY DESIGN CIRCULATION	ERD	21/12/15
2.	CHANGES TO ORIENTATION ACROSS KB SWM FACILITY	ERD	16/02/16
3.	ISSUED FOR PRELIMINARY DESIGN REPORT	ERD	02/03/16
4.	ISSUED FOR FINAL DESIGN CIRCULATION	ERD	29/04/16
5.	ISSUED FOR MOECC ECA APPLICATION	ERD	26/05/16
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7.	ISSUED FOR CONSTRUCTION	ERD	30/08/16
8.	SEWER ALIGNMENT SHIFT ON GREENBANK	ERD	16/09/16
9.	REVISED PER MION SERVICING	ERD	08/12/16

**LEGEND**

**EXISTING ITEMS**

- WATERMAIN
- WATERMAIN VALVE
- STORM SEWER
- STORM MH
- CATCH BASIN & LEAD
- CULVERT
- STORM STRUCTURE
- SANITARY SEWER
- SANITARY MH

**PROPOSED ITEMS**

- SANITARY SEWER
- SANITARY MH & LID
- CULVERT
- FUTURE STRUCTURE T/G ADJUSTMENT

- NOTES:**
- CONCRETE PRESSURE PIPE SHALL BE AWWA C301 (L) CL-16. FITTING SHALL BE DESIGNED TO THE SAME CRITERIA AS THE ADJACENT PIPE.
  - CONTRACTOR TO PROVIDE PIPE CLASS CALCULATIONS, AS PER AWWA C304 (DESIGN OF PRESTRESSED CONCRETE CYLINDER PIPE), BY THE PIPE MANUFACTURER, SIGNED AND SEALED BY A PROFESSIONAL ENGINEER LICENSED IN THE PROVINCE OF ONTARIO.
  - PIPE EMBEDMENT SHALL BE AS PER CITY OF OTTAWA DETAIL S6. SAND MAY BE USED AS PIPE COVER MATERIAL ABOVE THE SPRINGLINE.
  - A CLOTH DIAPER APPROVED BY THE PIPE MANUFACTURE SHALL BE PLACED AROUND EACH EXTERIOR JOINT RECESS AND FASTENED IN PLACE WITH EITHER WIRE OR STEEL STRAPPING STITCHED INTO ITS EDGES.
  - THE JOINT SHALL BE FILLED WITH MORTAR IN ONCE CONTINUOUS OPERATION AND PATTED OR MANIPULATED TO SETTLE THE MORTAR AND EXPEL AND ENTRAPPED AIR.
  - INTERIOR JOINTS SHALL BE FILLED WITH MORTAR AFTER BACKFILLING AND FINISHED SMOOTH WITH A TROWEL. CEMENT USED SHALL MEET THE REQUIREMENTS OF TYPE HS CEMENT (HIGH-SULPHATE-RESISTANCE), OR APPROVED EQUIVALENT.
  - THE INTERIOR OF THE JOINTS SHALL BE PROTECTED FROM CORROSION WITH EPOXY AND ZINC COATING APPLIED DURING FABRICATION.
  - THE INTERIOR STRUCTURAL CONCRETE CORE SHALL BE MANUFACTURED WITH TYPE HS CEMENT (HIGH-SULPHATE-RESISTANCE), OR APPROVED EQUIVALENT.
  - SEE MANHOLE DETAIL DRAWINGS ISD14-2033-36 TO ISD14-2033-45 FOR ADDITIONAL DETAILS

**MAINTENANCE HOLE DATA**

MH ID	STATION	OFFSET	STRUCTURE	COVER	T/G ELEV.	LOW. INV.
1	0+010.00	1.25R	OPSD 701.013	S24/S25	95.06	86.92
2	0+060.95	1.25R	OPSD 701.012	S24/S25	94.37	86.87
3	0+118.25	1.25R	OPSD 701.012	S24/S25	94.67	86.81
4	0+194.38	0.46R	OPSD 701.013	S24/S25	93.84	86.73
5	0+226.51	1.25R	OPSD 701.012	S24/S25	92.75	86.70
6	0+269.14	1.25R	OPSD 701.012	S24/S25	92.66	86.66

**SANITARY SEWER PIPE DATA**

CONNECTED STRUCTURES & INVERTS	DIA (mm)	LENGTH (m)	MATERIAL
SANMH 1 = 86.92 SANMH 2 = 86.87	900	50.95	AWWA C-301 (L)
SANMH 2 = 86.87 SANMH 3 = 86.81	900	57.30	AWWA C-301 (L)
SANMH 3 = 86.81 SANMH 4 = 86.73	900	76.07	AWWA C-301 (L)
SANMH 4 = 86.73 SANMH 5 = 86.70	900	31.95	AWWA C-301 (L)
SANMH 5 = 86.70 SANMH 6 = 86.66	900	42.26	AWWA C-301 (L)
SANMH 6 = 86.66 SANMH 7 = 86.59	900	73.97	AWWA C-301 (L)

STATION	EXISTING ELEVATION	PROPOSED ELEVATION	PROPOSED INVERT
0+000	83.47	82.76	86.92
0+010	82.75	82.75	86.92
0+020	82.75	82.75	86.92
0+030	82.75	82.75	86.92
0+040	82.75	82.75	86.92
0+050	82.75	82.75	86.92
0+060	82.75	82.75	86.87
0+070	82.75	82.75	86.87
0+080	82.74	82.74	86.87
0+090	82.74	82.74	86.87
0+100	82.74	82.74	86.87
0+110	82.72	82.72	86.81
0+120	82.67	82.67	86.81
0+130	82.62	82.62	86.81
0+140	82.59	82.59	86.81
0+150	82.59	82.59	86.81
0+160	82.55	82.55	86.81
0+170	82.51	82.51	86.81
0+180	82.50	82.50	86.81
0+190	82.49	82.49	86.73
0+200	82.46	82.46	86.73
0+210	82.48	82.48	86.73
0+220	82.47	82.47	86.70
0+230	82.45	82.45	86.70
0+240	82.42	82.42	86.70
0+250	82.40	82.40	86.70
0+260	82.38	82.38	86.66
0+270	82.36	82.36	86.66
0+280	82.34	82.34	86.66
0+290	82.32	82.32	86.66
0+300	82.29	82.29	86.59



**AS-BUILT**

THESE AS-BUILT PLANS HAVE BEEN PREPARED BASED ON INFORMATION PROVIDED BY OTHERS. THE DESIGN PROFESSIONAL HAS NOT VERIFIED THE ACCURACY AND/OR THE COMPLETENESS OF THIS INFORMATION AND SHALL NOT BE RESPONSIBLE FOR ANY ERRORS OR OMISSIONS WHICH MAY BE INCORPORATED HEREIN AS A RESULT.



**CITY OF OTTAWA**  
SOUTH NEPEAN COLLECTOR (SNC)  
SEWER PHASE 2 - STRANDHERD DRIVE  
TO JOCKVALE ROAD

**PLAN AND PROFILE**  
STA. 0+300 TO 0+600

Wayne Newell, P.Eng. (General Manager) / Jonathan Knoyle, P.Eng. (Senior Engineer)

**NOVATECH**

Scale: HORIZONTAL 1:500, VERTICAL 1:100

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No.	Description	By	Date (dd/mm/yyyy)
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3	ISSUED FOR PRELIMINARY DESIGN REPORT	ERC	02/03/16
4	ISSUED FOR FINAL DESIGN CIRCULATION	ERD	29/04/16
5	ISSUED FOR MOECC ECA APPLICATION	ERD	26/05/16
6	ISSUED FOR TENDER	ERD	20/06/16
7	ISSUED FOR CONSTRUCTION	ERD	30/08/16
8	SEWER ALIGNMENT SHIFT ON GREENBANK	ERD	16/09/16
9	REVISED PER MION SERVICING	ERD	08/12/16
10	MINTO LANDS MANHOLE UPDATE	ERD	24/04/17
11	ISSUED FOR AS-BUILT	ERD	28/09/17

**LEGEND**

<b>EXISTING ITEMS</b>	<b>PROPOSED ITEMS</b>
WATERMAIN	SANITARY SEWER
WATERMAIN VALVE	SANITARY MH & LID
STORM SEWER	CULVERT
STORM MH	FUTURE STRUCTURE T/G
CATCH BASIN & LEAD	ADJUSTMENT
CULVERT	
STORM STRUCTURE	
SANITARY SEWER	
SANITARY MH	

**NOTES:**

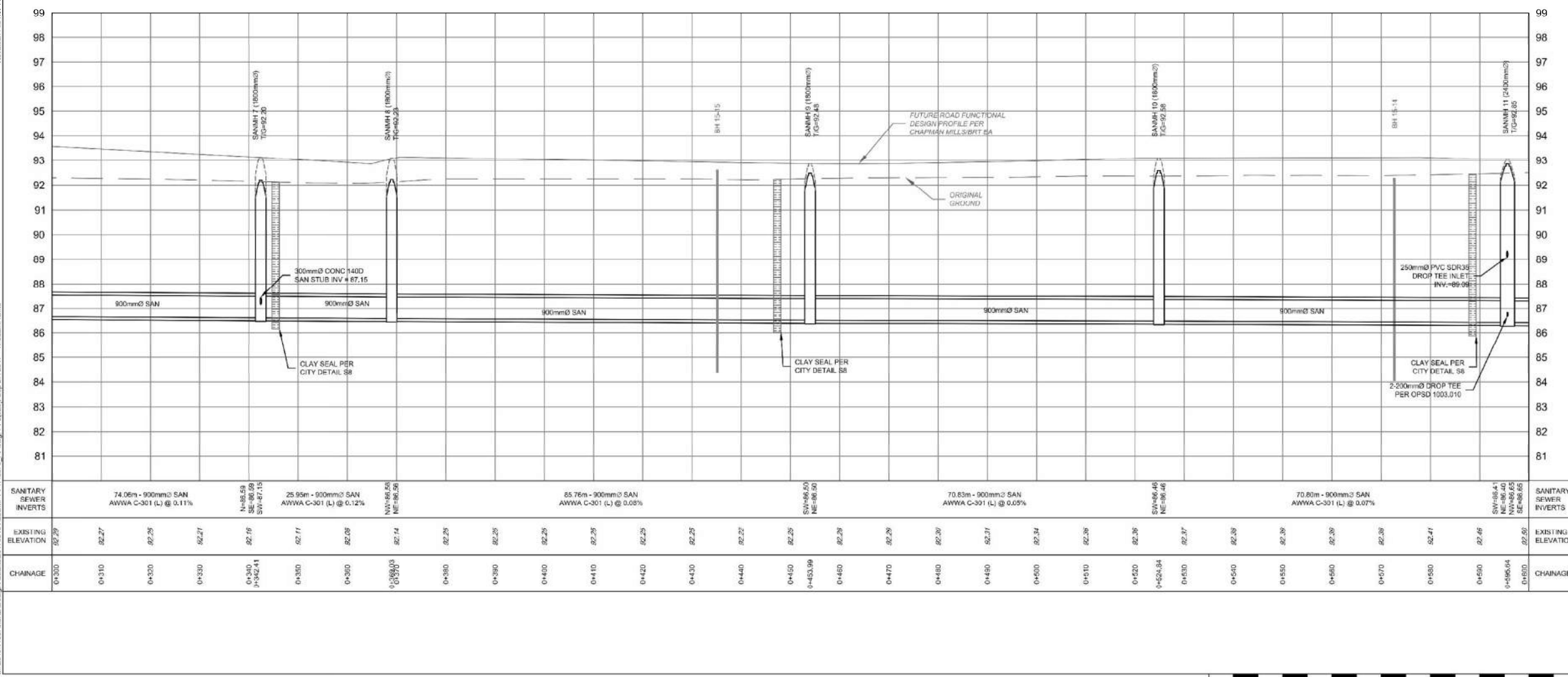
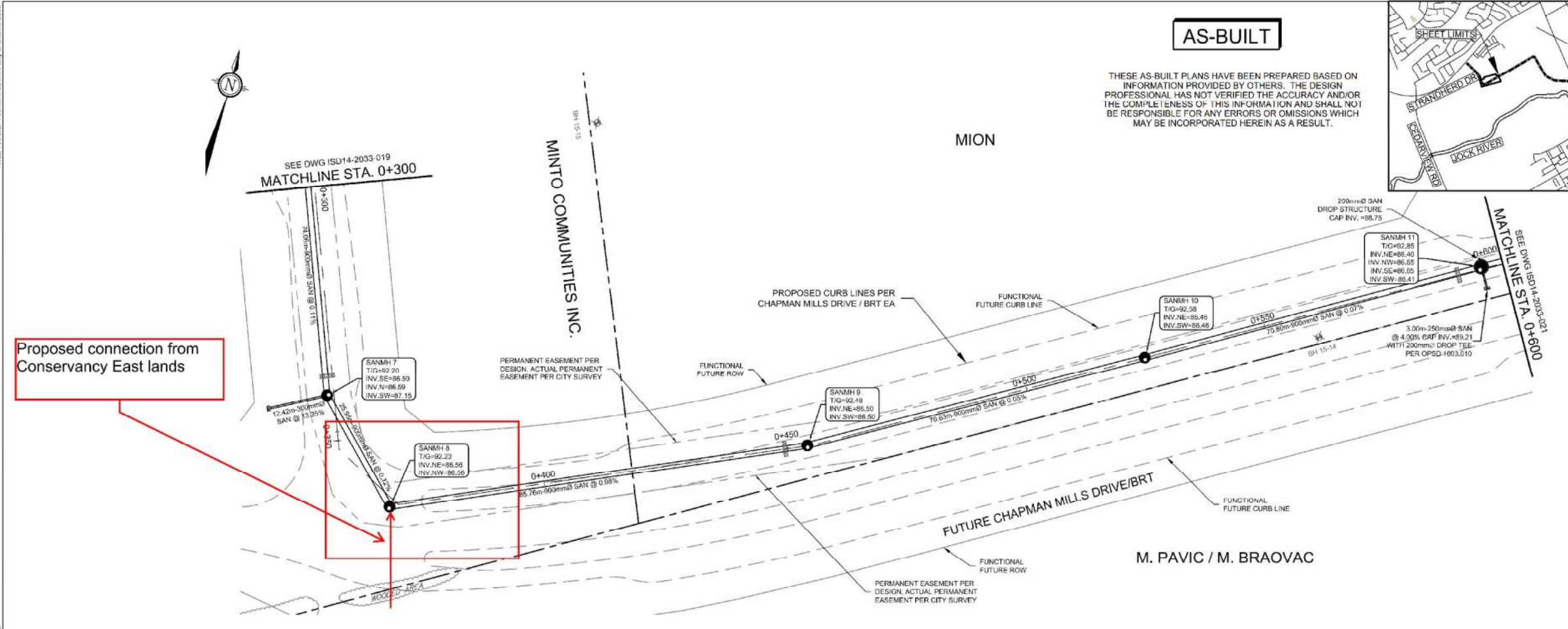
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**MAINTENANCE HOLE DATA**

MH ID	STATION	OFFSET	STRUCTURE	COVER	T/G ELEV	LOW. INV.
7	0+342.41	1.41R	OPSD 701 012	S24/S25	92.20	86.59
8	0+369.03	1.50R	OPSD 701 012	S24/S25	92.23	86.56
9	0+453.99	0.07L	OPSD 701 012	S24/S25	92.48	86.50
10	0+524.84	0.04L	OPSD 701 012	S24/S25	92.58	86.46
11	0+595.64	0.41L	OPSD 701 013	S24/S25	92.85	86.40

**SANITARY SEWER PIPE DATA**

CONNECTED STRUCTURES & INVERTS	DIA (mm)	LENGTH (m)	MATERIAL
SANMH 7 = 86.59 SANMH 8 = 86.56	900	74.06	AWWA C-301 (L)
SANMH 9 = 86.56 SANMH 9 = 86.50	900	25.95	AWWA C-301 (L)
SANMH 10 = 86.48 SANMH 9 = 86.50	900	85.76	AWWA C-301 (L)
SANMH 10 = 86.48 SANMH 10 = 86.40	900	70.83	AWWA C 301 (L)
SANMH 10 = 86.40 SANMH 11 = 86.41	900	70.60	AWWA C-301 (L)
SANMH 11 = 86.40 SANMH 12 = 86.52	900	78.15	AWWA C-301 (L)



TITLE FRAME: 706mm x 634mm, City of Ottawa 2008  
Novatech File No. 115075  
M:\2019\115075\CADD\Design\Submittal\20170813\_Asbuilt\20170813\_Asbuilt.dwg, Sep 27, 2017, 11:08am, nmm





# SANITARY SEWER CALCULATION SHEET

Manning's n=0.013

LOCATION			RESIDENTIAL AREA AND POPULATION						CUMULATIVE		C+H+I		ARK		C+H		INFILTRATION			PIPE							
STREET	FROM M.H.	TO M.H.	AREA (ha)	UNITS	POP.	AREA (ha)	POP.	PEAK FACT.	PEAK FLOW (l/s)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	PEAK FLOW (l/s)	TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	DIST (m)	DIA (mm)	SLOPE (%)	CAP. (FULL) (l/s)	RATIO Q act/Q cap	VEL. (FULL) (m/s)	VEL. (ACT.) (m/s)
<b>Street 30</b>																											
	105A	106A	0.19		20	0.19	20	3.7	0.24		0.00		0.00		0.00	0.00	0.19	0.19	0.06	0.30	23.0	200	0.65	26.44	0.01	0.84	0.28
	106A	107A	0.11		12	0.30	32	3.7	0.38		0.00		0.00		0.00	0.11	0.30	0.10	0.48	37.5	250	0.25	29.73	0.02	0.61	0.22	
To Street 17, Pipe 107A - 108A						0.30	32				0.00		0.00		0.00		0.30										
<b>Street 26</b>																											
Contribution From Street 3, Pipe 9400A - 95A						0.01	2				0.00		0.00		0.00	0.01	0.01										
	95A	96A	0.16		17	0.17	19	3.7	0.23		0.00		0.00		0.00	0.16	0.17	0.06	0.28	60.5	200	0.70	27.44	0.01	0.87	0.28	
	96A	98A	0.15		16	0.32	35	3.7	0.42		0.00		0.00		0.00	0.15	0.32	0.11	0.52	57.5	250	0.25	29.73	0.02	0.61	0.23	
To Street 22, Pipe 98A - 102A						0.32	35				0.00		0.00		0.00		0.32										
<b>Street 24</b>																											
Contribution From Street 3, Pipe 9500A - 73A						0.18	19				0.00		0.00		0.00	0.18	0.18										
	73A	97A	0.40		42	0.58	61	3.6	0.72		0.00		0.00		0.00	0.40	0.58	0.19	0.91	105.5	300	0.20	43.25	0.02	0.61	0.25	
To Street 22, Pipe 97A - 98A						0.58	61				0.00		0.00		0.00		0.58										
<b>Street 27</b>																											
	96A	99A	0.50		52	0.50	52	3.6	0.61		0.00		0.00		0.00	0.50	0.50	0.17	0.78	99.0	200	0.85	30.24	0.03	0.96	0.41	
To Street 22, Pipe 99A - 100A						0.50	52				0.00		0.00		0.00		0.50										
<b>Street 28</b>																											
Contribution From Street 14, Pipe 86A - 91A						1.33	143				0.00		0.00		0.57	1.90	1.90										
Contribution From Street 14, Pipe 90A - 91A						1.09	116				0.00		0.00		0.00	1.09	2.99										
	91A	94A	0.05		6	2.47	265	3.5	2.99		0.00		0.00		0.57	0.06	0.05	3.04	1.00	4.05	62.0	375	0.15	67.91	0.06	0.61	0.34
To Street 3, Pipe 94A - 93A						2.47	265				0.00		0.00		0.57		3.04										
<b>Street 22</b>																											
	75A	97A	0.12		13	0.12	13	3.7	0.16		0.00		0.00		0.00	0.12	0.12	0.04	0.20	45.0	200	0.65	26.44	0.01	0.84	0.24	
Contribution From Street 24, Pipe 73A - 97A						0.58	61				0.00		0.00		0.00	0.58	0.70										
	97A	98A	0.18		19	0.88	93	3.6	1.09		0.00		0.00		0.00	0.18	0.88	0.29	1.38	45.0	300	0.20	43.25	0.03	0.61	0.28	
Contribution From Street 26, Pipe 96A - 98A						0.32	35				0.00		0.00		0.00	0.32	1.20										
	98A	102A	0.46		48	1.66	176	3.5	2.02		0.00		0.00		0.00	0.46	1.66	0.55	2.56	83.5	300	0.55	71.72	0.04	1.01	0.47	
To Street 29, Pipe 102A - 103A						1.66	176				0.00		0.00		0.00		1.66										
Contribution From Street 3, Pipe 92A - 93A						0.12	13				0.00		0.00		0.00	0.12	0.12										
Contribution From Street 3, Pipe 94A - 93A						2.97	317				0.00		0.00		0.57	3.54	3.66										
	93A	99A	0.19		20	3.28	350	3.4	3.90		0.00		0.00		0.57	0.06	0.19	3.85	1.27	5.23	60.5	375	0.15	67.91	0.08	0.61	0.36
Contribution From Street 27, Pipe 9600A - 99A						0.50	52				0.00		0.00		0.00	0.50	4.35										
	99A	100A	0.20		21	3.98	423	3.4	4.67		0.00		0.00		0.57	0.06	0.20	4.55	1.50	6.24	50.5	375	0.15	67.91	0.09	0.61	0.38
	100A	101A	0.13		14	4.11	437	3.4	4.82		0.00		0.00		0.57	0.06	0.13	4.68	1.54	6.42	11.0	375	0.15	67.91	0.09	0.61	0.38
	101A	102A	0.04		5	4.15	442	3.4	4.87		0.00		0.00		0.57	0.06	0.04	4.72	1.56	6.49	10.0	375	0.15	67.91	0.10	0.61	0.38
To Street 29, Pipe 102A - 103A						4.15	442				0.00		0.00		0.57		4.72										
<b>Street 29</b>																											
Contribution From Street 22, Pipe 101A - 102A						4.15	442				0.00		0.00		0.57	4.72	4.72										
Contribution From Street 22, Pipe 98A - 102A						1.66	176				0.00		0.00		0.00	1.66	6.38										
	102A	103A	0.05		6	5.86	624	3.3	6.75		0.00		0.00		0.57	0.06	0.05	6.43	2.12	8.93	62.0	375	0.15	67.91	0.13	0.61	0.42
To Street 17, Pipe 103A - 107A						5.86	624				0.00		0.00		0.57		6.43										

**DESIGN PARAMETERS**

Park Flow =	9300	L/ha/da	0.10764	l/s/ha																								
Average Daily Flow =	280	l/p/day																										
Comm/Inst Flow =	28000	L/ha/da	0.3241	l/s/ha																								
Industrial Flow =	35000	L/ha/da	0.40509	l/s/ha																								
Max Res. Peak Factor =	4.00																											
Commercial/Inst./Park Peak Factor =	1.00																											
Institutional =	0.32	l/s/ha																										

Designed:	A.K.	PROJECT:	<b>BARRHAVEN CONSERVANCY WEST</b>			
Checked:	W.L.	LOCATION:	<b>City of Ottawa</b>			
Dwg. Reference:	Sanitary Drainage Plan, Dwgs. No.	File Ref:	Date:	Oct 2021	Sheet No. of	1 6



# SANITARY SEWER CALCULATION SHEET

Manning's n=0.013

LOCATION			RESIDENTIAL AREA AND POPULATION						CUMULATIVE		PEAK		PARK		C+H		INFILTRATION			PIPE								
STREET	FROM M.H.	TO M.H.	AREA (ha)	UNITS	POP.	AREA (ha)	POP.	PEAK FACT.	PEAK FLOW (l/s)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	PEAK FLOW (l/s)	TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	DIST (m)	DIA (mm)	SLOPE (%)	CAP. (FULL) (l/s)	RATIO Q act/Q cap	VEL. (FULL) (m/s)	VEL. (ACT.) (m/s)	
<b>Street 20</b>																												
Contribution From Street 3, Pipe 6300A - 74A						0.16	17				0.00	0.00		0.00		0.16	0.16											
Contribution From Street 3, Pipe 7300A - 74A						0.18	19				0.00	0.00		0.00		0.18	0.34											
	74A	75A	0.37		39	0.71	75	3.6	0.88		0.00	0.00		0.00	0.00	0.37	0.71	0.23	1.11	94.5	300	0.20	43.25	0.03	0.61	0.26		
	75A	76A	0.16		17	0.87	92	3.6	1.07		0.00	0.00		0.00	0.00	0.16	0.87	0.29	1.36	63.5	300	0.20	43.25	0.03	0.61	0.28		
To Street 17, Pipe 76A - 77A						0.87	92				0.00	0.00		0.00		0.87												
<b>Street 2</b>																												
	65A	25A	0.55		58	0.55	58	3.6	0.68		0.00	0.00		0.00	0.00	0.55	0.55	0.18	0.87	101.5	200	0.65	26.44	0.03	0.84	0.38		
To Street 4, Pipe 25A - 27A						0.55	58				0.00	0.00		0.00		0.55												
	1A	2A	0.40		42	0.40	42	3.7	0.50		0.00	0.00		0.00	0.00	0.40	0.40	0.13	0.63	66.5	200	0.65	26.44	0.02	0.84	0.35		
	2A	3A	0.10		11	0.50	53	3.6	0.63		0.00	0.00		0.00	0.00	0.10	0.50	0.17	0.79	10.0	200	0.35	19.40	0.04	0.62	0.30		
	3A	4A	0.17		18	0.67	71	3.6	0.83		0.00	0.00		0.00	0.00	0.17	0.67	0.22	1.06	44.0	250	0.25	29.73	0.04	0.61	0.28		
	4A	5A	0.18		19	0.85	90	3.6	1.05		0.00	0.00		0.00	0.00	0.18	0.85	0.28	1.33	13.5	300	0.20	43.25	0.03	0.61	0.28		
	5A	6A	0.40		42	1.25	132	3.6	1.53		0.00	0.00		0.00	0.00	0.40	1.25	0.41	1.94	68.5	375	0.15	67.91	0.03	0.61	0.27		
	6A	7A	0.35		37	1.60	169	3.5	1.94		0.00	0.00		0.00	0.00	0.35	1.60	0.53	2.47	62.0	375	0.15	67.91	0.04	0.61	0.29		
	7A	8A	0.33		35	1.93	204	3.5	2.32		0.00	0.00		0.00	0.00	0.33	1.93	0.64	2.96	61.5	375	0.15	67.91	0.04	0.61	0.30		
	8A	9A	0.43		45	2.36	249	3.5	2.82		0.00	0.00		0.00	0.00	0.43	2.36	0.78	3.59	73.5	375	0.15	67.91	0.05	0.61	0.32		
	9A	10A	0.11		12	2.47	261	3.5	2.95		0.00	0.00		0.00	0.00	0.11	2.47	0.82	3.76	14.5	375	0.15	67.91	0.06	0.61	0.32		
	10A	17A	0.21		22	2.68	283	3.5	3.18		0.00	0.00		0.00	0.00	0.21	2.68	0.88	4.07	53.5	375	0.15	67.91	0.06	0.61	0.34		
To Street 3, Pipe 17A - 23A						2.68	283				0.00	0.00		0.00		2.68												
	1A	18A	0.39		41	0.39	41	3.7	0.49		0.00	0.00		0.00	0.00	0.39	0.39	0.13	0.62	66.0	200	0.65	26.44	0.02	0.84	0.35		
	18A	19A	0.36		38	0.75	79	3.6	0.93		0.00	0.00		0.00	0.00	0.36	0.75	0.25	1.17	61.5	250	0.25	29.73	0.04	0.61	0.29		
	19A	20A	0.48		50	1.23	129	3.6	1.49		0.00	0.00		0.00	0.00	0.48	1.23	0.41	1.90	83.0	300	0.20	43.25	0.04	0.61	0.30		
	20A	21A	0.24		25	1.47	154	3.5	1.77		0.00	0.00		0.00	0.00	0.24	1.47	0.49	2.26	39.5	300	0.20	43.25	0.05	0.61	0.32		
	21A	22A	0.24		25	1.71	179	3.5	2.05		0.00	0.00		0.00	0.00	0.24	1.71	0.56	2.61	40.5	300	0.35	57.21	0.05	0.81	0.41		
	22A	23A	0.31		33	2.02	212	3.5	2.41		0.00	0.00		0.00	0.00	0.31	2.02	0.67	3.08	57.0	300	0.80	86.49	0.04	1.22	0.56		
Contribution From Street 3, Pipe 17A - 23A						5.02	529				0.00	0.00		0.00		5.02	7.04											
	23A	24A	0.20		21	7.24	762	3.3	8.15		0.00	0.00		0.00	0.00	0.20	7.24	2.39	10.53	52.0	375	0.15	67.91	0.16	0.61	0.45		
	24A	25A	0.13		14	7.37	776	3.3	8.29		0.00	0.00		0.00	0.00	0.13	7.37	2.43	10.72	13.5	375	0.15	67.91	0.16	0.61	0.45		
To Street 4, Pipe 25A - 27A						7.37	776				0.00	0.00		0.00		7.37												
<b>Street 4</b>																												
Contribution From Street 2, Pipe 24A - 25A						7.37	776				0.00	0.00		0.00		7.37	7.37											
Contribution From Street 2, Pipe 6500A - 25A						0.55	58				0.00	0.00		0.00		0.55	7.92											
	25A	27A	0.03		4	7.95	838	3.3	8.90		0.00	0.00		0.00	0.00	0.03	7.95	2.62	11.53	67.5	375	0.15	67.91	0.17	0.61	0.45		
To Street 5, Pipe 27A - 28A						7.95	838				0.00	0.00		0.00		7.95												
<b>Street 5</b>																												
	67A	29A	0.48		50	0.48	50	3.7	0.59		0.00	0.00		0.00	0.00	0.48	0.48	0.16	0.75	90.0	200	0.65	26.44	0.03	0.84	0.37		
To Street 8, Pipe 29A - 31A						0.48	50				0.00	0.00		0.00		0.48												
	66A	26A	0.49		51	0.49	51	3.7	0.60		0.00	0.00		0.00	0.00	0.49	0.49	0.16	0.77	89.0	200	0.65	26.44	0.03	0.84	0.37		
	26A	27A	0.04		5	0.53	56	3.6	0.66		0.00	0.00		0.00	0.00	0.04	0.53	0.17	0.84	15.0	200	0.35	19.40	0.04	0.62	0.31		
Contribution From Street 4, Pipe 25A - 27A						7.95	838				0.00	0.00		0.00		7.95	8.48											
	27A	28A	0.29		31	8.77	925	3.3	9.76		0.00	0.00		0.00	0.00	0.29	8.77	2.89	12.66	44.0	375	0.15	67.91	0.19	0.61	0.47		

<b>DESIGN PARAMETERS</b> Park Flow = 9300 L/ha/day Average Daily Flow = 280 l/p/day Comm/Inst Flow = 28000 L/ha/day Industrial Flow = 35000 L/ha/day Max Res. Peak Factor = 4.00 Commercial/Inst./Park Peak Factor = 1.00 Institutional = 0.32 l/s/ha Industrial Peak Factor = as per MOE Graph Extraneous Flow = 0.330 L/s/ha Minimum Velocity = 0.600 m/s Manning's n = (Conc) 0.013 (Pvc) 0.013 Townhouse coeff= 2.7 Single house coeff= 3.4										Designed: A.K. Checked: W.L. Dwg. Reference: Sanitary Drainage Plan, Dwg. No.					PROJECT: <b>BARRHAVEN CONSERVANCY WEST</b> LOCATION: <b>City of Ottawa</b> File Ref: _____ Date: <b>Oct 2021</b> Sheet No. <b>2</b>												
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# SANITARY SEWER CALCULATION SHEET

Manning's n=0.013

LOCATION			RESIDENTIAL AREA AND POPULATION						COMM		C+H				INFILTRATION				PIPE								
STREET	FROM M.H.	TO M.H.	AREA (ha)	UNITS	POP.	CUMULATIVE		PEAK FACT.	PEAK FLOW (l/s)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	PEAK FLOW (l/s)	TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	DIST (m)	DIA (mm)	SLOPE (%)	CAP. (FULL) (l/s)	RATIO Q act/Q cap	VEL.	
						AREA (ha)	POP.																			(FULL) (m/s)	(ACT.) (m/s)
	94A	95A	0.01		2	0.01	2	3.8	0.02		0.00		0.00		0.00	0.01	0.01	0.00	0.03	7.5	200	0.65	26.44	0.00	0.84	0.12	
To Street 26, Pipe 95A - 96A						0.01	2				0.00		0.00		0.00		0.01										
	95A	73A	0.18		19	0.18	19	3.7	0.23		0.00		0.00		0.00	0.18	0.18	0.06	0.29	43.5	200	0.65	26.44	0.01	0.84	0.27	
To Street 24, Pipe 73A - 97A						0.18	19				0.00		0.00		0.00		0.18										
	11A	34A	0.27		29	0.27	29	3.7	0.35		0.00		0.00		0.00	0.27	0.27	0.09	0.44	69.5	200	0.65	26.44	0.02	0.84	0.30	
	34A	35A	0.29		31	0.56	60	3.6	0.71		0.00		0.00		0.00	0.29	0.56	0.18	0.89	74.5	250	0.25	29.73	0.03	0.61	0.27	
			13.70		0	14.26	60				0.00		0.00		0.00	13.70	14.26		0.00058								
	35A	36A	0.21		22	14.47	82	3.6	0.96		0.00		0.00		0.00	0.21	14.47	4.78	5.74	13.5	300	0.20	43.25	0.13	0.61	0.42	
	36A	37A	0.36		38	14.83	120	3.6	1.39		0.00		0.00		0.00	0.36	14.83	4.89	6.29	89.0	375	0.15	67.91	0.09	0.61	0.38	
	37A	38A	0.34		36	15.17	156	3.5	1.79		0.00		0.00		0.00	0.34	15.17	5.01	6.80	89.0	375	0.20	78.41	0.09	0.71	0.43	
	38A	39A	0.09		10	15.26	166	3.5	1.91		0.00		0.00		0.00	0.09	15.26	5.04	6.94	52.0	375	0.20	78.41	0.09	0.71	0.44	
	39A	40A	0.08		9	15.34	175	3.5	2.00		0.00		0.00	2.90	2.90	0.31	2.98	18.24	6.02	8.34	13.5	375	0.15	67.91	0.12	0.61	0.42
	40A	41A	0.63		66	15.97	241	3.5	2.73		0.00		0.00	2.90	0.31	0.63	18.87	6.23	9.27	101.5	375	0.15	67.91	0.14	0.61	0.43	
	41A	63A	0.51		54	16.48	295	3.5	3.31		0.00		0.00	2.90	0.31	0.51	19.38	6.40	10.02	91.5	375	0.15	67.91	0.15	0.61	0.44	
To Street 17, Pipe 63A - 64A						16.48	295				0.00		0.00	2.90			19.38		0.00								
	11A	12A	0.11		12	0.11	12	3.7	0.14		0.00		0.00		0.00	0.11	0.11	0.04	0.18	10.5	200	0.65	26.44	0.01	0.84	0.23	
	12A	13A	0.45		47	0.56	59	3.6	0.70		0.00		0.00		0.00	0.45	0.56	0.18	0.88	74.5	250	0.25	29.73	0.03	0.61	0.27	
	13A	14A	0.45		47	1.01	106	3.6	1.23		0.00		0.00		0.00	0.45	1.01	0.33	1.57	79.5	250	0.25	29.73	0.05	0.61	0.32	
	14A	15A	0.40		42	1.41	148	3.6	1.70		0.00		0.00		0.00	0.40	1.41	0.47	2.17	54.0	250	0.25	29.73	0.07	0.61	0.35	
	15A	16A	0.25		26	1.66	174	3.5	1.99		0.00		0.00		0.00	0.25	1.66	0.55	2.54	54.0	300	0.20	43.25	0.06	0.61	0.33	
Contribution From Street 6, Pipe 65A - 16A						0.20	21				0.00		0.00		0.00	0.20	1.86										
	16A	17A	0.28		30	2.14	225	3.5	2.55		0.00		0.00	0.00	0.00	0.28	2.14	0.71	3.26	53.5	300	0.90	91.74	0.04	1.30	0.60	
Contribution From Street 2, Pipe 10A - 17A						2.68	283				0.00		0.00		0.00	2.68	4.82										
	17A	23A	0.20		21	5.02	529	3.4	5.78		0.00		0.00	0.00	0.00	0.20	5.02	1.66	7.43	59.0	375	0.15	67.91	0.11	0.61	0.40	
To Street 2, Pipe 23A - 24A						5.02	529				0.00		0.00		0.00		5.02										
Contribution From Street 28, Pipe 91A - 94A						2.47	265				0.00		0.00	0.57		3.04	3.04										
	94A	93A	0.50		52	2.97	317	3.5	3.55		0.00		0.00	0.57	0.06	0.50	3.54	1.17	4.78	89.0	375	0.15	67.91	0.07	0.61	0.35	
To Street 22, Pipe 93A - 99A						2.97	317				0.00		0.00	0.57			3.54										
<b>Street 21</b>																											
	45A	59A	0.35		37	0.35	37	3.7	0.44		0.00		0.00		0.00	0.35	0.35	0.12	0.56	89.5	200	0.65	26.44	0.02	0.84	0.34	
	59A	60A	0.36		38	0.71	75	3.6	0.88		0.00		0.00		0.00	0.36	0.71	0.23	1.11	89.5	250	0.25	29.73	0.04	0.61	0.29	
			0.06		7	0.77	82				0.00		0.00		0.06	0.77											
	60A	61A	0.46		48	1.23	130	3.6	1.50		0.00		0.00		0.00	0.46	1.23	0.41	1.91	118.0	300	0.20	43.25	0.04	0.61	0.30	
To Street 14, Pipe 61A - 62A						1.23	130				0.00		0.00				1.23										
<b>Street 18</b>																											
	43A	56A	0.35		37	0.35	37	3.7	0.44		0.00		0.00		0.00	0.35	0.35	0.12	0.56	86.5	200	0.65	26.44	0.02	0.84	0.34	
	56A	57A	0.35		37	0.70	74	3.6	0.87		0.00		0.00		0.00	0.35	0.70	0.23	1.10	87.0	250	0.25	29.73	0.04	0.61	0.29	
			0.06		7	0.76	81				0.00		0.00		0.06	0.76											
	57A	58A	0.46		48	1.22	129	3.6	1.49		0.00		0.00		0.00	0.46	1.22	0.40	1.89	118.0	300	0.20	43.25	0.04	0.61	0.30	
To Street 14, Pipe 58A - 61A						1.22	129				0.00		0.00				1.22										

DESIGN PARAMETERS										Designed: A.K.					PROJECT: BARRHAVEN CONSERVANCY WEST									
Average Daily Flow = 280 l/p/day										Checked: W.L.					LOCATION: City of Ottawa									
Comm/Inst Flow = 28000 l/ha/day										Dwg. Reference: Sanitary Drainage Plan, Dwg. No.					File Ref:					Date: Oct 2021				
Industrial Flow = 35000 l/ha/day															Sheet No. 4 of 6									
Max Res. Peak Factor = 4.00																								
Commercial/Inst./Park Peak Factor = 1.00																								
Institutional = 0.32 l/s/ha																								



# SANITARY SEWER CALCULATION SHEET

Manning's n=0.013

LOCATION			RESIDENTIAL AREA AND POPULATION						COMM		INFILTRATION				PIPE											
STREET	FROM M.H.	TO M.H.	AREA (ha)	UNITS	POP.	CUMULATIVE		PEAK FACT.	PEAK FLOW (l/s)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	C+H PEAK FLOW (l/s)	TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	DIST (m)	DIA (mm)	SLOPE (%)	CAP. (FULL) (l/s)	RATIO Q act/Q cap	VEL.		
						AREA (ha)	POP.																	(FULL) (m/s)	(ACT.) (m/s)	
<b>Street 14</b>																										
	82A	83A	0.19		20	0.19	20	3.7	0.24		0.00		0.00	0.00	0.19	0.19	0.06	0.30	53.5	200	0.65	26.44	0.01	0.84	0.28	
To Street 16, Pipe 83A - 84A						0.19	20				0.00		0.00		0.19											
	86A	62A	0.58		61	0.58	61	3.6	0.72		0.00		0.00	0.00	0.58	0.58	0.19	0.91	105.0	200	0.95	31.97	0.03	1.02	0.45	
To Street 17, Pipe 62A - 63A						0.58	61				0.00		0.00		0.58											
	82A	87A	0.12		13	0.12	13	3.7	0.16		0.00		0.00	0.00	0.12	0.12	0.04	0.20	11.0	200	0.65	26.44	0.01	0.84	0.24	
	87A	88A	0.42		44	0.54	57	3.6	0.67		0.00		0.00	0.42	0.54	0.18	0.85	62.5	250	0.25	29.73	0.03	0.61	0.27		
	88A	89A	0.38		40	0.92	97	3.6	1.13		0.00		0.00	0.38	0.92	0.30	1.43	62.5	250	0.25	29.73	0.05	0.61	0.31		
	89A	90A	0.13		14	1.05	111	3.6	1.29		0.00		0.00	0.13	1.05	0.35	1.64	11.0	250	0.25	29.73	0.06	0.61	0.32		
	90A	91A	0.04		5	1.09	116	3.6	1.35		0.00		0.00	0.04	1.09	0.36	1.71	10.0	250	3.00	103.00	0.02	2.10	0.76		
To Street 28, Pipe 91A - 94A						1.09	116				0.00		0.00		1.09											
	38A	55A	0.22		23	0.22	23	3.7	0.28		0.00		0.00	0.22	0.22	0.07	0.35	61.5	200	0.65	26.44	0.01	0.84	0.29		
Contribution From Street 16, Pipe 54A - 55A						1.66	177				0.00		0.00		1.66	1.88										
	55A	58A	0.17		18	2.05	218	3.5	2.48		0.00		0.00	0.17	2.05	0.68	3.15	44.5	375	0.15	67.91	0.05	0.61	0.31		
Contribution From Street 18, Pipe 57A - 58A						1.22	129				0.00		0.00		1.22	3.27										
	58A	61A	0.17		18	3.44	365	3.4	4.06		0.00		0.00	0.17	3.44	1.14	5.20	44.0	375	0.15	67.91	0.08	0.61	0.36		
Contribution From Street 21, Pipe 60A - 61A						1.23	130				0.00		0.00		1.23	4.67										
	61A	62A	0.15		16	4.82	511	3.4	5.59		0.00		0.00	0.15	4.82	1.59	7.18	45.0	375	0.15	67.91	0.11	0.61	0.39		
To Street 17, Pipe 62A - 63A						4.82	511				0.00		0.00		4.82											
Contribution From Street 16, Pipe 85A - 86A						1.17	126				0.00		0.00	0.57	1.74	1.74										
	86A	91A	0.16		17	1.33	143	3.6	1.65		0.00		0.00	0.16	1.90	0.63	2.34	43.0	375	0.15	67.91	0.03	0.61	0.28		
To Street 28, Pipe 91A - 94A						1.33	143				0.00		0.00	0.57	1.90											
<b>Street 25</b>																										
	85A	51A	0.53		56	0.53	56	3.6	0.66		0.00		0.00	0.53	0.53	0.17	0.84	105.0	200	0.65	26.44	0.03	0.84	0.38		
To Street 17, Pipe 51A - 62A						0.53	56				0.00		0.00		0.53											
<b>Street 23</b>																										
	84A	50A	0.52		55	0.52	55	3.6	0.65		0.00		0.00	0.52	0.52	0.17	0.82	103.5	200	0.65	26.44	0.03	0.84	0.38		
To Street 17, Pipe 50A - 51A						0.52	55				0.00		0.00		0.52											
<b>Street 16</b>																										
	44A	45A	0.11		12	0.11	12	3.7	0.14		0.00		0.00	0.11	0.11	0.04	0.18	13.5	200	1.60	41.49	0.00	1.32	0.32		
	45A	48A	0.20		21	0.31	33	3.7	0.39		0.00		0.00	0.20	0.31	0.10	0.50	50.0	250	0.25	29.73	0.02	0.61	0.22		
To Street 17, Pipe 48A - 49A						0.31	33				0.00		0.00		0.31											
	46A	47A	0.10		11	0.10	11	3.7	0.13		0.00		0.00	0.10	0.10	0.03	0.17	10.0	200	0.65	26.44	0.01	0.84	0.23		
	47A	48A	0.24		25	0.34	36	3.7	0.43		0.00		0.00	0.24	0.34	0.11	0.54	61.5	250	0.25	29.73	0.02	0.61	0.23		
To Street 17, Pipe 48A - 49A						0.34	36				0.00		0.00		0.34											
	44A	43A	0.12		13	0.12	13	3.7	0.16		0.00		0.00	0.12	0.12	0.04	0.20	32.5	200	0.65	26.44	0.01	0.84	0.24		
	43A	42A	0.15		16	0.27	29	3.7	0.35		0.00		0.00	0.15	0.27	0.09	0.44	40.5	250	0.25	29.73	0.01	0.61	0.21		
	42A	52A	0.04		5	0.31	34	3.7	0.41		0.00		0.00	0.04	0.31	0.10	0.51	10.0	250	0.25	29.73	0.02	0.61	0.23		
	52A	53A	0.33		35	0.64	69	3.6	0.81		0.00		0.00	0.33	0.64	0.21	1.02	77.5	250	0.25	29.73	0.03	0.61	0.28		
	53A	54A	0.39		41	1.03	110	3.6	1.28		0.00		0.00	0.39	1.03	0.34	1.62	77.5	300	0.20	43.25	0.04	0.61	0.29		

DESIGN PARAMETERS				Designed:		PROJECT:	
Park Flow =	9300	L/ha/da	0.10764	I/s/ha	A.K.	BARRHAVEN CONSERVANCY WEST	
Average Daily Flow =	280	I/p/day					
Comm/Inst Flow =	28000	L/ha/da	0.3241	I/s/ha	Checked:	LOCATION: City of Ottawa	
Industrial Flow =	35000	L/ha/da	0.40509	I/s/ha	W.L.		
Max Res. Peak Factor =	4.00				Dwg. Reference:	File Ref:	Date: Oct 2021
Commercial/Inst./Park Peak Factor =	1.00				Sanitary Drainage Plan, Dwg. No.		Sheet No. of 5 of 6
Institutional =	0.32	I/s/ha					1296_CAD_DesignSheet1.xlsx







# SANITARY SEWER CALCULATION SHEET

Excerpted from Master Infrastructure Review (MIR) prepared by DSEL dated July 27, 2021



Manning's n=0.013

LOCATION			RESIDENTIAL AREA AND POPULATION						COMM		INSTIT		PARK		C+H			INFILTRATION			PIPE						
STREET	FROM M.H.	TO M.H.	AREA (ha)	PPHA*	POP.	CUMULATIVE		PEAK FACT.	PEAK FLOW (l/s)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	PEAK FLOW (l/s)	TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	DIST (m)	DIA (mm)	SLOPE (%)	CAP. (FULL) (l/s)	RATIO Q act/Q cap	VEL.	
						AREA (ha)	POP.																			(FULL) (m/s)	(ACT.) (m/s)
<b>SANITARY TRUNK 2</b>																											
	2002A	2004A	0.56	104	58	0.56	58	3.6	0.69		0.00		0.00		0.00	0.00	0.56	0.56	0.18	0.87	58.5	200	0.35	19.40	0.04	0.62	0.31
	2004A	2006A	0.22	104	23	0.78	81	3.6	0.95		0.00		0.00		0.00	0.22	0.78	0.26	1.21	58.5	200	0.35	19.40	0.06	0.62	0.34	
	2006A	2008A	0.21	104	22	0.99	103	3.6	1.20		0.00		0.00		0.00	0.21	0.99	0.33	1.53	58.5	200	0.35	19.40	0.08	0.62	0.36	
	2008A	2010A	0.22	104	23	1.21	126	3.6	1.46		0.00		0.00		0.00	0.22	1.21	0.40	1.86	58.5	200	0.35	19.40	0.10	0.62	0.39	
	2010A	2012A	0.12	104	12	1.33	138	3.6	1.60		0.00		0.00		0.00	0.12	1.33	0.44	2.04	29.5	200	0.35	19.40	0.10	0.62	0.40	
	2012A	2013A	0.17	104	18	1.50	156	3.5	1.79		0.00		0.00		0.00	0.17	1.50	0.50	2.29	39.5	200	0.35	19.40	0.12	0.62	0.41	
	2013A	2014A	0.15	104	16	1.65	172	3.5	1.97		0.00		0.00		0.00	0.15	1.65	0.54	2.51	35.0	200	0.35	19.40	0.13	0.62	0.42	
	2014A	2015A	0.11	104	11	1.76	183	3.5	2.09		0.00		0.00		0.00	0.11	1.76	0.58	2.67	28.0	200	0.35	19.40	0.14	0.62	0.43	
	2015A	2036A	0.14	104	15	1.90	198	3.5	2.25		0.00		0.00		0.00	0.14	1.90	0.63	2.88	36.0	200	0.35	19.40	0.15	0.62	0.44	
	2036A	2037A	7.40	104	770	9.30	967	3.2	10.18		0.00		0.00		0.00	7.40	9.30	3.07	13.25	53.5	250	0.25	29.73	0.45	0.61	0.59	
	2037A	2038A	0.23	104	24	9.53	991	3.2	10.41		0.00		0.00		0.00	0.23	9.53	3.14	13.56	61.0	250	0.25	29.73	0.46	0.61	0.59	
	2038A	2058A	4.24	104	441	13.77	1432	3.2	14.64		0.00		0.00		0.00	4.24	13.77	4.54	19.19	61.0	300	0.20	43.25	0.44	0.61	0.59	
	2058A	1061A	0.16	104	17	13.93	1449	3.2	14.80		0.00		0.00		0.00	0.16	13.93	4.60	19.40	59.0	300	0.20	43.25	0.45	0.61	0.59	
	1061A	1063A	6.64	104	691	20.57	2139	3.1	21.15		0.00		0.00		0.00	6.64	20.57	6.79	27.94	62.0	375	0.15	67.91	0.41	0.61	0.58	
	1063A	1064A	0.22	104	23	20.79	2162	3.0	21.35		0.00		0.00		0.00	0.22	20.79	6.86	28.21	60.5	375	0.15	67.91	0.42	0.61	0.58	
	1064A	1096A	0.22	104	23	21.01	2185	3.0	21.56		0.00		0.00		0.00	0.22	21.01	6.93	28.49	59.5	375	0.15	67.91	0.42	0.61	0.59	
	1096A	1105A	9.80	104	1019	30.81	3204	2.9	30.47		0.00		0.00		0.00	9.80	30.81	10.17	40.64	67.0	375	0.15	67.91	0.60	0.61	0.64	
	1105A	1111A	0.22	104	23	31.03	3227	2.9	30.67		0.00		0.00		0.00	0.22	31.03	10.24	40.91	56.5	375	0.15	67.91	0.60	0.61	0.64	
	1111A	1120A				31.03	3227	2.9	30.67		0.00		0.00		0.00	0.00	31.03	10.24	40.91	58.5	375	0.15	67.91	0.60	0.61	0.64	
			4.32	85	367	35.35	3594	2.0	23.30		0.00		0.00		0.00	4.32	35.35										
	1120A	5004A	2.56	104	266	37.91	3861	2.9	36.00		0.00		0.00		0.00	2.56	37.91	12.51	48.51	100.0	450	0.15	110.42	0.44	0.69	0.67	
	5004A	PS	0.35	104	36	38.26	3897	2.9	36.31		0.00		0.00		0.00	0.35	38.26	12.63	48.93	100.0	450	0.15	110.42	0.44	0.69	0.67	
To Barrhaven Conservancy East:																											

\* PPHA calculated based on a weighted average across the site, using the single house and townhouse coefficients of 3.4 and 2.7 people per unit respectively

DESIGN PARAMETERS										Designed:		PROJECT:			
Park Flow =	9300	L/ha/da	0.10764	I/s/ha							R.B.	<b>BARRHAVEN CONSERVANCY WEST</b>			
Average Daily Flow =	280	I/p/day			Industrial Peak Factor = as per MOE Graph							LOCATION: <b>City of Ottawa</b>			
Comm/Inst Flow =	28000	L/ha/da	0.3241	I/s/ha	Extraneous Flow =	0.330	L/s/ha				D.A.	Date: July 2021			
Industrial Flow =	35000	L/ha/da	0.40509	I/s/ha	Minimum Velocity =	0.600	m/s					File Ref: 16-891		Sheet No. 1	
Max Res. Peak Factor =	4.00				Manning's n = (Conc)	0.013	(Pvc)	0.013				Date: July 2021		of 1	
Commercial/Inst./Park Peak Factor =	1.00				Townhouse coeff=	2.7						Date: July 2021		of 1	
Institutional =	0.32	I/s/ha			Single house coeff=	3.4						Date: July 2021		of 1	







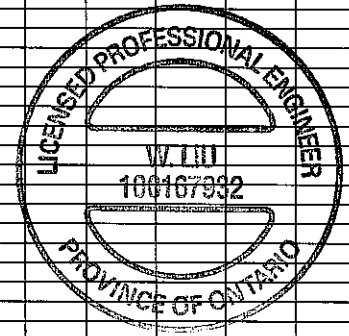
# SANITARY SEWER CALCULATION SHEET



Manning's n=0.013

LOCATION			RESIDENTIAL AREA AND POPULATION					COMM		INSTIT		PARK		I-C+I-P		INFILTRATION				PIPE												
STREET	FROM M.H.	TO M.H.	AREA (ha)	UNITS	UNITS		POP.	CUMULATIVE		PEAK FACT.	PEAK FLOW (l/s)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	ICI Ratio	ICI Peaking Factor	PEAK FLOW (l/s)	TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	DIST (m)	DIA (mm)	SLOPE (%)	CAP. (FULL) (l/s)	RATIO Q act/Q cap	VEL.		
					Single	Townhouse		AREA (ha)	POP.																					(FULL) (m/s)	(ACT.) (m/s)	
	21A	22A	0.04					2.56	198	3.52	2.26										0.04	2.56	0.84	3.10	21.0	200	0.35	19.40	0.16	0.62	0.45	
	22A	23A	0.01					2.57	198	3.52	2.26										0.01	2.57	0.85	3.11	8.0	200	0.35	19.40	0.16	0.62	0.45	
	23A	24A	0.26	6	6		21	2.83	219	3.51	2.49										0.26	2.83	0.93	3.42	42.0	200	0.80	29.34	0.12	0.93	0.62	
Contribution From promenade Albion Falls Drive, Pipe 12A - 24A								3.62	260						0.67						4.29	7.12										
	24A	25A	0.49	12	12		41	6.94	520	3.37	5.68									0.11	0.49	7.61	2.51	8.30	91.5	200	0.35	19.40	0.43	0.62	0.59	
Contribution From voie Horseshoe Falls Way, Pipe 18A - 25A								0.22	19												0.22	7.83										
	Upper Pipe 26A	25A	0.30	5	5		17													0.30	0.30	0.10	0.10	66.5	200	0.65	26.44	0.00	0.84	0.19		
	Lower Pipe 25A	26A						7.46	556	3.36	6.05									0.11	0.00	8.13	2.68	8.85	66.5	200	0.35	19.40	0.46	0.62	0.60	
To promenade Chapman Mills Drive, Pipe 26A - Ex. MH 13								7.46	556													8.13										
promenade Chapman Mills Drive																																
	28A	29A	0.41	7		7	19	0.41	19	3.71	0.23										0.41	0.41	0.14	0.36	42.0	200	0.65	26.44	0.01	0.84	0.29	
	29A	30A	0.28	6		6	17	0.69	36	3.67	0.43										0.28	0.69	0.23	0.66	60.0	200	0.35	19.40	0.03	0.62	0.29	
	30A	31A	0.44	9		9	25	1.13	61	3.64	0.72										0.44	1.13	0.37	1.09	120.0	200	0.35	19.40	0.06	0.62	0.33	
	31A	Ex. MH 11						1.13	61	3.64	0.72										0.00	1.13	0.37	1.09	18.5	200	3.40	60.48	0.02	1.93	0.72	
To Existing Sanitary Trunk, Ex. Pipe 11 - 12								1.13	61													1.13										
	27A	26A	0.50	14		14	38	0.50	38	3.67	0.45									0.00	0.50	0.50	0.17	0.62	98.0	200	0.65	26.44	0.02	0.84	0.35	
Contribution From croissant Point Prim Crescent, Pipe 25A - 26A								7.46	556													8.13	8.13									
	26A	Ex. MH 13						7.96	594	3.35	6.44									0.11	0.00	8.63	2.85	9.40	23.5	200	0.35	19.40	0.48	0.62	0.61	
To Existing Sanitary Trunk, Ex. Pipe 13 - 14								7.96	594														8.63									

Conservancy Phase 1 - Flows and population tributary to South Nepean Collector



<b>DESIGN PARAMETERS</b> Park Flow = 9300 L/ha/da Average Daily Flow = 280 l/p/day Comm/Inst Flow = 28000 L/ha/da Industrial Flow = 35000 L/ha/da Max Res. Peak Factor = 4.00 Park Peak Factor = 1.50			Industrial Peak Factor = as per MOE Graph Extraneous Flow = 0.330 L/s/ha Minimum Velocity = 0.600 m/s Manning's n = (Conc) 0.013 (Pvc) 0.013 Townhouse coeff= 2.7 Single house coeff= 3.4			Designed: P.P. Checked: W.L.		PROJECT: BARRHAVEN CONSERVANCY PHASE 1 LOCATION: City of Ottawa	
Dwg. Reference: Sanitary Drainage Plan, Dwg. No: 33				File Ref: 16-891		Date: January, 2019		Sheet No. 2 of 2	



**SANITARY SEWER CALCULATION SHEET**

104 people/Ha	Population Density (Conservancy West)
83 people/Ha	Population Density (Conservancy East)



Manning's n=0.013

LOCATION			RESIDENTIAL AREA AND POPULATION				COMM		INSTIT		PARK		C+H	INFILTRATION			PIPE									
STREET	FROM M.H.	TO M.H.	AREA (ha)	POP.	CUMULATIVE		PEAK FACT.	PEAK FLOW (l/s)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	PEAK FLOW (l/s)	TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	DIST (m)	DIA (mm)	SLOPE (%)	CAP. (FULL) (l/s)	RATIO Q act/Q cap	VEL.			
					AREA (ha)	POP.																	(FULL) (m/s)	(ACT.) (m/s)		
									0.00				0.00	0.00	0.00	0.00	0.00									
Extracted from SNC Novatech Ph3 design		EX SANMH1 <sup>(1)</sup>	105.8	10974	105.8	10974.0	2.53	89.98	179.17	179.17	17.25	17.25		0.00	92.69	302.22	302.22	99.73	282.40	165.0	914.4	0.10	597.22	0.47	0.91	0.89
at Strandherd & CMD intersection		See Note <sup>(2)</sup>	31.5	3116	137.3	14090	2.44	111.42		179.17				0.00	87.10	31.50	333.7	110.12	308.64	50.0	914.4	0.10	597.22	0.52	0.91	0.91
CONSERVANCY WEST <sup>(3)</sup>		EX SANMH8	45.83	3404	183.1	17494	2.37	134.36		179.17		3.5	3.50	87.66	49.33	383.03	126.40	348.42	125.0	914.4	0.10	597.22	0.58	0.91	0.94	
CONSERVANCY EAST <sup>(3)</sup>		EX SANMH8	53.67	4568	236.8	22062	2.29	163.73	4.21	183.38		4.30	7.80	90.40	62.18	445.21	146.92	401.05	260.0	914.4	0.08	534.17	0.75	0.81	0.89	
					236.8	22062	2.29	163.73		183.38			7.80	90.40	0.00	445.21	146.92	401.05		914.4	0.05	422.30	0.95	0.64	0.73	

**NOTES:**  
 (1) Refer to Novatech Drawing No. 19 - South Nepean Collector (SNC) Sewer Phase 2 - Strandherd Rive to Jockvale Road (ISD14-2033) in Appendix C  
 (2) Derived from Tributary areas "A6-C" and "A6-D" from Novatech's "Sanitary Drainage Areas and Land Use - Fig. 1" plan dated August 2015 (See Appendix C of DSEL report) = 4.87ha and 17.56ha and derived from Barrhaven Conservancy Phase 1 design sheet (see Appendix C of DSEL report) = 1.13ha + 7.96ha  
 (3) Based on population densities of 104 people/ha for WEST and 83 people/ha for EAST. See Conservancy East sanitary design sheet

DESIGN PARAMETERS				Designed:		PROJECT:						
Park Flow =	9300	L/ha/da			KLM	<b>Barrhaven Conservancy - Evaluation of SNC Flows</b>						
Average Daily Flow =	280	l/p/day	Industrial Peak Factor = as per MOE Graph									
Comm/Inst Flow =	28000	L/ha/da	Extraneous Flow =	0.330 L/s/ha	Checked:	KLM	LOCATION: <b>City of Ottawa</b>					
Industrial Flow =	35000	L/ha/da	Minimum Velocity =	0.600 m/s	Dwg. Reference:		File Ref:	1226.000	Date:	October 2021	Sheet No.	1 of 1
Max Res. Peak Factor =	4.00		Manning's n =	0.000								
Commercial/Inst./Park Peak Factor =	1.50		Townhouse coeff=	2.7								
Institutional	0.32	l/s/ha	Single house coeff=	3.4								

Total flow including Conservancy Lands is 401.05 L/s which is LESS than the prior 423.6 L/s determined in the 2015 Novatech assessment of flows at the same location in the South Nepean Collector (SNC) sewer.

Based on Novatech's SNC as-builts, the minimum as-built slope is 0.05% downstream of the existing SANMH8 connection point. Other as-built slopes range from 0.07 to 0.15.

**APPENDIX D**

**STORMWATER**



# Conservation Partners Partenaires en conservation



May 31, 2020

City of Ottawa  
110 Laurier Avenue,  
Ottawa, ON K1P 1J1

Attention: Doug James

Subject: **Barrhaven Conservancy Development Corporation  
Status of As-Built Grading  
Related: RVCA Permit # RV5-4419 and RV5-1718)  
Vacant land on the north side of the Jock River generally bounded by  
Highway 416 and the Fraser Clarke Creek, City of Ottawa**

Dear Mr. James:

The RVCA has reviewed information recently submitted by David Schaeffer Engineering Ltd. including as-built grades in support of works approved by the Rideau Valley Conservation Authority under Section 28 of the Conservation Authorities Act (Permit File Number: RV5-4419 and RV5-1718). The RVCA offers the following comments related to future development proposed for the area within the scope of approved the permits.

The subject lands as identified as part of Lots 11, 12, 13, 14, 15 former geographic Township of Nepean, Concessions 3 & 4, now in the City of Ottawa have been addressed through the general placement of fill and the formal construction of a berm around the perimeter of four blocks within the subject lands. The site specific elevations of the berm have been reviewed by the RVCA and are generally accepted as being appropriate as removing these lands from the floodplain in accordance with the aforementioned approved permits.

The detailed grading plans submitted by David Schaeffer Engineering Ltd. titled "As Constructed plan of Berms and Cut Areas – Barrhaven Conservancy", dated May 27, 2020, prepared by Adam Fobert, P.Eng. of DSEL, DSEL File Number 16891 using the following resources:

- Orthoimagery Survey, dated April 20, 2020, acquired and processed by First Base Solutions a division of JD Barnes Ltd and certified by Chris Fox, O.L.S., A.L.S., P. Eng. of JD Barnes Ltd, file reference number 2037OTTA0001; -
- Topographic Detail of Part of Lot 13, 14, & 15 Concession 3&4, dated May 6, 2020, certified by Chris Fox, O.L.S., A.L.S., P. Eng. of JD Barnes Ltd, file reference number 16-10-127-00; -

- Contractor as-built collected by the Tomlinson Group of Companies of Phase 1 dated May 15, 2020, reviewed by Jeremy Chouindard, EIT and certified by Stephen Pichette, P.Eng. of DSEL

The above information indicates that land within the berm have generally been raised to exceed the flood elevation cross sections throughout the project area. However, it is noted that as this is considered an active construction site the presence of lower areas to manage construction, on-site erosion and sediment control show lower elevations. These areas will be addressed through the construction process, as sufficient material is presently stockpiled for this purpose to ensure. For the purposes of the floodplain, these areas are considered removed by virtue of the berm.

### **Conclusion:**

The grade modifications, including construction of the berm and filling behind the berm, as documented in the above noted "as constructed" plans, have been completed in accordance with the plans approved by the RVCA under permits RV5-4419 and RV5-1718.

Please feel free to contact our office with any questions or comments you may have.

Respectfully,



**Terry Davidson, P.Eng**  
Director of Engineering and Regulations  
Rideau Valley Conservation Authority  
613-692-3571 x1107  
[terry.davidson@rvca.ca](mailto:terry.davidson@rvca.ca)

attach:            Technical memorandum by Evelyn Liu, M.Asc., P.Eng. Water Resources  
Engineer, RVCA dated May 29, 2020







**STORM SEWER CALCULATION SHEET (RATIONAL METHOD)**

Local Roads Return Frequency = 2 years  
 Collector Roads Return Frequency = 5 years  
 Arterial Roads Return Frequency = 10 years



Manning 0.013

LOCATION			AREA (Ha)																FLOW										SEWER DATA							
			2 YEAR				5 YEAR				10 YEAR				100 YEAR				Time of	Intensity	Intensity	Intensity	Intensity	Peak Flow	DIA. (mm)	DIA. (mm)	TYPE	SLOPE	LENGTH	CAPACITY	VELOCITY	TIME OF	RATIO			
Location	From Node	To Node	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	Conc. (min)	2 Year (mm/h)	5 Year (mm/h)	10 Year (mm/h)	100 Year (mm/h)	Q (l/s)	(actual)	(nominal)	(%)	(m)	(l/s)	(m/s)	LOW (min)	Q/Q full				
	59	60	0.15	0.65	0.27	1.59			0.00	0.00			0.00	0.00			0.00	0.00	12.61	68.05	92.16	107.97	157.75	108	450	450	CONC	0.25	12.5	142.5531	0.8963	0.2324	0.759			
	60	61	0.07	0.65	0.13	1.72			0.00	0.00			0.00	0.00			0.00	0.00	12.84	67.37	91.24	106.89	156.16	116	450	450	CONC	0.30	19.0	156.1591	0.9819	0.3225	0.741			
To Street 7, Pipe 61 - 62						1.72				0.00				0.00				0.00	13.17																	
Contribution From Street 6, Pipe 52 - 54						9.41				3.24				0.00				0.00	20.68																	
Contribution From Street 6, Pipe 53 - 54						0.22				0.00				0.00				0.00	10.57																	
	54	55	0.50	0.65	0.90	10.53			0.00	3.24			0.00	0.00			0.00	0.00	20.68	50.96	68.79	80.49	117.43	759	1050	1050	CONC	0.15	90.0	1057.6053	1.2214	1.2281	0.718			
	55	56	0.10	0.65	0.18	10.72			0.00	3.24			0.00	0.00			0.00	0.00	21.91	49.15	66.32	77.59	113.18	741	1050	1050	CONC	0.15	11.0	1057.6053	1.2214	0.1501	0.701			
	56	61	0.09	0.65	0.16	10.88			0.00	3.24			0.00	0.00			0.00	0.00	22.06	48.94	66.03	77.25	112.68	746	1050	1050	CONC	0.15	25.5	1057.6053	1.2214	0.3480	0.705			
To Street 7, Pipe 61 - 62						10.88				3.24				0.00				0.00	22.41																	
<b>Street 7</b>																																				
Contribution From Street 5, Pipe 56 - 61						10.88				3.24				0.00				0.00	22.41																	
Contribution From Street 5, Pipe 60 - 61						1.72				0.00				0.00				0.00	13.17																	
	61	OGS W3	0.01	0.65	0.02	12.61			0.00	3.24			0.00	0.00			0.00	0.00	22.41	48.45	65.37	76.48	111.55	823	1050	1050	CONC	0.15	26.5	1057.6053	1.2214	0.3616	0.778			
<b>Street 8</b>																																				
Contribution From Street 10, Pipe 81 - 82						1.66				0.00				0.00				0.00	13.23																	
	82	83	0.05	0.65	0.09	1.75			0.00	0.00			0.00	0.00			0.00	0.00	13.23	66.28	89.75	105.13	153.58	116	450	450	CONC	0.30	13.5	156.1591	0.9819	0.2292	0.744			
To Street 12, Pipe 83 - 84						1.75				0.00				0.00				0.00	13.46																	
<b>Street 21</b>																																				
	64	69	0.34	0.65	0.61	0.61			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	47	300	300	PVC	0.40	90.5	61.1589	0.8652	1.7433	0.772			
	69	70	0.38	0.65	0.69	1.30			0.00	0.00			0.00	0.00			0.00	0.00	11.74	70.70	95.81	112.27	164.05	92	450	450	CONC	0.20	90.5	127.5033	0.8017	1.8814	0.721			
Contribution From Street 23, Pipe 39 - 70						0.04				0.00				0.00				0.00	10.24																	
	70	71	0.23	0.65	0.42	1.75			0.00	0.00			0.00	0.00			0.00	0.00	13.62	65.22	88.28	103.41	151.05	114	525	525	CONC	0.20	61.5	192.3297	0.8885	1.1537	0.594			
	71	72	0.23	0.65	0.42	2.17			0.00	0.00			0.00	0.00			0.00	0.00	14.78	62.30	84.28	98.70	144.14	135	525	525	CONC	0.20	61.5	192.3297	0.8885	1.1537	0.702			
To Street 14, Pipe 72 - 73						2.17				0.00				0.00				0.00	15.93																	
<b>Street 23</b>																																				
	39	70	0.02	0.65	0.04	0.04			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	3	300	300	PVC	0.95	19.5	94.2522	1.3334	0.2437	0.029			
To Street 21, Pipe 70 - 71						0.04				0.00				0.00				0.00	10.24																	
	39	40	0.03	0.65	0.05	0.05			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	4	300	300	PVC	0.35	24.5	57.2089	0.8093	0.5045	0.073			
To Street 18, Pipe 40 - 41						0.05				0.00				0.00				0.00	10.50																	
	40	36	0.06	0.65	0.11	0.11			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	8	300	300	PVC	0.35	44.5	57.2089	0.8093	0.9164	0.146			
To Street 16, Pipe 36 - 37						0.11				0.00				0.00				0.00	10.92																	
	70	67	0.06	0.65	0.11	0.11			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	8	300	300	PVC	0.35	43.5	57.2089	0.8093	0.8958	0.146			
To Street 17, Pipe 67 - 68						0.11				0.00				0.00				0.00	10.90																	
Contribution From Street 16, Pipe 89 - 90						1.01				0.70				0.00				0.00	12.90																	
	90	67	0.53	0.65	0.96	1.97			0.00	0.70			0.00	0.00			0.00	0.00	12.90	67.23	91.04	106.65	155.81	196	675	675	CONC	0.15	108.5	325.5584	0.9098	1.9877	0.603			
To Street 17, Pipe 67 - 68						1.97				0.70				0.00				0.00	14.88																	
<b>Street 6</b>																																				
	52	57	0.12	0.65	0.22	0.22			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	17	300	300	PVC	0.35	34.0	57.2089	0.8093	0.7002	0.291			
To Street 5, Pipe 57 - 58						0.22				0.00				0.00				0.00	10.70																	
	53	80	0.09	0.65	0.16	0.16			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	12	300	300	PVC	0.70	25.5	80.9057	1.1446	0.3713	0.154			
To Street 10, Pipe 80 - 81						0.16				0.00				0.00				0.00	10.37																	
	53	54	0.12	0.65	0.22	0.22			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	17	300	300	PVC	0.35	27.5	57.2089	0.8093	0.5663	0.291			
To Street 5, Pipe 54 - 55						0.22				0.00				0.00				0.00	10.57																	
	77	80	0.25	0.65	0.45	0.45			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	35	300	300	PVC	0.35	64.0	57.2089	0.8093	1.3179	0.606			
To Street 10, Pipe 80 - 81																																				

**STORM SEWER CALCULATION SHEET (RATIONAL METHOD)**

Local Roads Return Frequency = 2 years  
 Collector Roads Return Frequency = 5 years  
 Arterial Roads Return Frequency = 10 years



Manning 0.013

LOCATION			AREA (Ha)																FLOW							SEWER DATA										
			2 YEAR				5 YEAR				10 YEAR				100 YEAR				Time of	Intensity	Intensity	Intensity	Intensity	Peak Flow	DIA. (mm)	DIA. (mm)	TYPE	SLOPE	LENGTH	CAPACITY	VELOCITY	TIME OF	RATIO			
Location	From Node	To Node	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	Conc. (min)	2 Year (mm/h)	5 Year (mm/h)	10 Year (mm/h)	100 Year (mm/h)	Q (l/s)	(actual)	(nominal)	(%)	(m)	(l/s)	(m/s)	LOW (min)	Q/Q full				
	8	57	0.09	0.65	0.16	0.16													10.00	76.81	104.19	122.14	178.56	12	300	300	PVC	1.40	25.0	114.4179	1.6187	0.2574	0.109			
To Street 5, Pipe 57 - 58						0.16				0.00	0.00								10.26																	
	8	9	0.12	0.65	0.22	0.22													10.00	76.81	104.19	122.14	178.56	17	300	300	PVC	0.35	28.5	57.2089	0.8093	0.5869	0.291			
	9	10	0.21	0.65	0.38	0.60													10.59	74.62	101.19	118.61	173.37	44	300	300	PVC	0.40	59.0	61.1589	0.8652	1.1365	0.728			
To Street 3, Pipe 10 - 19						0.60				0.00	0.00								11.72																	
Contribution From Street 17, Pipe 75 - 76						9.92				1.19	0.00								18.71																	
	76	77	0.20	0.65	0.36	10.28													18.71	54.21	73.22	85.70	125.07	644	975	975	CONC	0.15	57.0	867.9562	1.1625	0.8172	0.742			
To Street 10, Pipe 77 - 78						10.28				1.19	0.00								19.52																	
Contribution From Street 9, Pipe 51 - 52						9.23				3.24	0.00								20.27																	
	52	54	0.10	0.65	0.18	9.41													20.27	51.60	69.66	81.51	118.93	711	1050	1050	CONC	0.15	30.0	1057.6053	1.2214	0.4094	0.672			
To Street 5, Pipe 54 - 55						9.41				3.24	0.00								20.68																	
<b>Street 10</b>																																				
Contribution From Street 6, Pipe 53 - 80						0.16				0.00	0.00								10.37																	
Contribution From Street 6, Pipe 7700 - 80						0.45				0.00	0.00								11.32																	
	80	81	0.43	0.65	0.78	1.39													11.32	72.09	97.71	114.51	167.35	100	450	450	CONC	0.20	79.5	127.5033	0.8017	1.6528	0.787			
	81	82	0.15	0.65	0.27	1.66													12.97	67.01	90.74	106.31	155.30	111	450	450	CONC	0.25	14.0	142.5531	0.8963	0.2603	0.781			
To Street 8, Pipe 82 - 83						1.66				0.00	0.00								13.23																	
Contribution From Street 6, Pipe 76 - 77						10.28				1.19	0.00								19.52																	
	77	78	0.43	0.65	0.78	11.06													19.52	52.81	71.31	83.46	121.78	669	975	975	CONC	0.15	78.0	867.9562	1.1625	1.1183	0.770			
	78	79	0.12	0.65	0.22	11.28													20.64	51.02	68.87	80.59	117.57	657	975	975	CONC	0.15	12.5	867.9562	1.1625	0.1792	0.757			
	79	83	0.11	0.65	0.20	11.47													20.82	50.75	68.50	80.15	118.93	664	975	975	CONC	0.15	31.0	867.9562	1.1625	0.4444	0.765			
To Street 12, Pipe 83 - 84						11.47				1.19	0.00								21.27																	
<b>Street 12</b>																																				
Contribution From Street 10, Pipe 79 - 83						11.47				1.19	0.00								21.27																	
Contribution From Street 8, Pipe 82 - 83						1.75				0.00	0.00								13.46																	
	83	OGS W2	0.01	0.65	0.02	13.25													21.27	50.08	67.59	79.08	115.36	744	975	975	CONC	0.20	26.5	1002.2295	1.3424	0.3290	0.742			
<b>Street 26</b>																																				
Contribution From Street 3, Pipe 10200 - 111						0.00				0.02	0.00								10.28																	
	111	112	0.15	0.65	0.27	0.27													10.28	75.75	102.75	120.44	176.06	22	300	300	PVC	0.35	55.0	57.2089	0.8093	1.1326	0.391			
	112	115	0.15	0.65	0.27	0.54													11.41	71.78	97.29	114.01	166.62	41	375	375	PVC	0.30	57.0	96.0323	0.8695	1.0926	0.424			
To Street 22, Pipe 115 - 116						0.54				0.02	0.00								12.50																	
<b>Street 24</b>																																				
Contribution From Street 3, Pipe 11100 - 110						0.00				0.34	0.00								10.90																	
	110	114	0.39	0.65	0.70	0.70													10.90	73.53	99.69	116.84	170.76	86	450	450	CONC	0.20	99.5	127.5033	0.8017	2.0685	0.675			
To Street 22, Pipe 114 - 115						0.70				0.34	0.00								12.96																	
<b>Street 27</b>																																				
	112	105	0.50	0.65	0.90	0.90													10.00	76.81	104.19	122.14	178.56	69	450	450	CONC	0.20	98.5	127.5033	0.8017	2.0478	0.544			
To Street 22, Pipe 105 - 106						0.90				0.00	0.00								12.05																	
<b>Street 25</b>																																				
	91	68	0.41	0.65	0.74	0.74													10.00	76.81	104.19	122.14	178.56	57	375	375	PVC	0.30	79.5	96.0323	0.8695	1.5239	0.593			
To Street 17, Pipe 68 - 73						0.74				0.00	0.00								11.52																	
	91	92	0.12	0.65	0.22	0.22													10.00	76.81	104.19	122.14	178.56	17	300	300	PVC	0.35	30.5	57.2089	0.8093	0.6281	0.291			
To Street 16, Pipe 92 - 94						0.22				0.00	0.00								10.63																	
<b>Street 16</b>																																				
	31	64	0.06	0.65	0.11	0.11													10.00	76.81	104.19	122.14	178.56	8	300	300	PVC	1.35	9.0	112.3561	1.5895	0.0944	0.074			
	64	65	0.19	0.65	0.34	0.45													10.09	76.44	103.70	121.56	177.70	35	300	300	PVC	0.35	50.0	57.2089	0.8093	1.0296	0.604			
To Street 17, Pipe 65 - 66						0.45				0.00	0.00								11.12																	

Definitions:  
 Q = 2.78 AIR, where  
 Q = Peak Flow in Litres per second (L/s)  
 A = Areas in hectares (ha)  
 I = Rainfall Intensity (mm/h)  
 R = Runoff Coefficient

Notes:  
 1) Ottawa Rainfall-Intensity Curve  
 2) Min. Velocity = 0.80 m/s</







# STORM SEWER CALCULATION SHEET (RATIONAL METHOD)

Local Roads Return Frequency = 2 years  
 Collector Roads Return Frequency = 5 years  
 Arterial Roads Return Frequency = 10 years



Manning 0.013

LOCATION			AREA (Ha)																FLOW						SEWER DATA									
			2 YEAR				5 YEAR				10 YEAR				100 YEAR				Time of	Intensity	Intensity	Intensity	Intensity	Peak Flow	DIA. (mm)	DIA. (mm)	TYPE	SLOPE	LENGTH	CAPACITY	VELOCITY	TIME OF	RATIO	
Location	From Node	To Node	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	Conc. (min)	2 Year (mm/h)	5 Year (mm/h)	10 Year (mm/h)	100 Year (mm/h)	Q (l/s)	(actual)	(nominal)	(%)	(m)	(l/s)	(m/s)	LOW (min)	Q/Q full		
	1	2	0.30	0.65	0.54	0.54			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	42	300	300	PVC	0.35	73.0	57.2089	0.8093	1.5033	0.728	
	2	3	0.26	0.65	0.47	1.01			0.00	0.00			0.00	0.00			0.00	0.00	11.50	71.48	96.87	113.52	165.89	72	375	375	PVC	0.30	67.0	96.0323	0.8695	1.2843	0.753	
	3	4	0.12	0.65	0.22	1.23			0.00	0.00			0.00	0.00			0.00	0.00	12.79	67.54	91.46	107.15	156.54	83	375	375	PVC	0.40	10.0	110.8885	1.0040	0.1660	0.748	
	4	5	0.44	0.65	0.80	2.02			0.00	0.00			0.00	0.00			0.00	0.00	12.95	67.06	90.81	106.38	155.42	136	525	525	CONC	0.20	73.0	192.3297	0.8885	1.3694	0.706	
	5	6	0.46	0.65	0.83	2.86			0.00	0.00			0.00	0.00			0.00	0.00	14.32	63.41	85.81	100.50	146.78	181	600	600	CONC	0.15	82.0	237.8056	0.8411	1.6249	0.761	
Contribution From Street 11, Pipe 1500 - 6						0.14			0.00	0.00			0.00	0.00			0.00	0.00	11.23															
	6	7	0.30	0.65	0.54	3.54			0.00	0.00			0.00	0.00			0.00	0.00	15.95	59.62	80.61	94.39	137.82	211	600	600	CONC	0.20	54.0	274.5943	0.9712	0.9267	0.769	
	7	10	0.25	0.65	0.45	3.99			0.00	0.00			0.00	0.00			0.00	0.00	16.87	57.67	77.95	91.26	133.22	230	675	675	CONC	0.15	54.5	325.5584	0.9098	0.9984	0.707	
Contribution From Street 6, Pipe 9 - 10						0.60			0.00	0.00			0.00	0.00			0.00	0.00	11.72															
	10	19	0.26	0.65	0.47	5.06			0.00	0.00			0.00	0.00			0.00	0.00	17.87	55.72	75.29	88.14	128.64	282	675	675	CONC	0.20	48.0	375.9224	1.0505	0.7615	0.750	
Contribution From Street 2, Pipe 18 - 19						3.96			0.00	0.00			0.00	0.00			0.00	0.00	17.40															
	19	29	0.21	0.65	0.38	9.40			0.00	0.00			0.00	0.00			0.00	0.00	18.63	54.34	73.40	85.91	125.37	511	750	750	CONC	0.35	64.0	658.6236	1.4908	0.7155	0.775	
To Street 1, Pipe 30						9.40			0.00	0.00			0.00	0.00			0.00	0.00	19.35															
	1	45	0.22	0.65	0.40	0.40			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	31	300	300	PVC	0.35	13.0	57.2089	0.8093	0.2677	0.534	
	45	46	0.36	0.65	0.65	1.05			0.00	0.00			0.00	0.00			0.00	0.00	10.27	75.79	102.80	120.50	176.15	79	450	450	CONC	0.20	88.0	127.5033	0.8017	1.8295	0.623	
	46	47	0.32	0.65	0.58	1.63			0.00	0.00			0.00	0.00			0.00	0.00	12.10	69.59	94.28	110.47	161.42	113	525	525	CONC	0.20	88.0	192.3297	0.8885	1.6508	0.588	
Contribution From Street 14, Pipe 44 - 47						6.04			0.00	0.00			0.00	0.00			0.00	0.00	18.42															
	47	48	0.08	0.65	0.14	7.81			0.00	0.00			0.00	0.00			0.00	0.00	18.42	54.71	73.91	86.51	126.25	427	825	825	CONC	0.15	48.0	555.9418	1.0400	0.7692	0.768	
	48	50	0.02	0.65	0.04	7.84			0.00	0.00			0.00	0.00			0.00	0.00	19.19	53.37	72.07	84.35	123.09	419	825	825	CONC	0.15	12.5	555.9418	1.0400	0.2003	0.753	
To Street 9, Pipe 50 - 51						7.84			0.00	0.00			0.00	0.00			0.00	0.00	19.39															
Street 20																																		
Contribution From Street 3, Pipe 108 - 109						0.00			0.00	0.00			0.00	0.00			0.00	0.00	10.55															
Contribution From Street 3, Pipe 11000 - 109						0.00			0.00	0.31			0.00	0.00			0.00	0.00	10.83															
	109	113	0.36	0.65	0.65	0.65			0.00	0.51			0.00	0.00			0.00	0.00	10.83	73.75	99.99	117.19	171.28	99	450	450	CONC	0.20	88.5	127.5033	0.8017	1.8399	0.773	
	113	120	0.17	0.65	0.31	0.96			0.00	0.51			0.00	0.00			0.00	0.00	12.67	67.87	91.91	107.68	157.32	112	600	600	CONC	0.15	68.5	237.8056	0.8411	1.3574	0.469	
To Street 17, Pipe 120 - 121						0.96			0.00	0.51			0.00	0.00			0.00	0.00	14.03															
Street 17																																		
	123	124			0.00	0.00	0.12	0.65	0.22	0.22			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	23	300	300	PVC	1.25	27.0	108.1147	1.5295	0.2942	0.209	
To Street 30, Pipe 124 - 125						0.00			0.00	0.22			0.00	0.00			0.00	0.00	10.29															
Contribution From Street 16, Pipe 63 - 65						0.51			0.00	0.00			0.00	0.00			0.00	0.00	11.60															
Contribution From Street 16, Pipe 64 - 65						0.45			0.00	0.00			0.00	0.00			0.00	0.00	11.12															
	65	66	0.28	0.65	0.51	1.46			0.00	0.00			0.00	0.00			0.00	0.00	11.60	71.18	96.46	113.03	165.18	104	450	450	CONC	0.25	68.5	142.5531	0.8963	1.2737	0.731	
	66	67	0.38	0.65	0.69	2.15			0.00	0.00			0.00	0.00			0.00	0.00	12.87	67.30	91.14	106.77	155.98	145	525	525	CONC	0.20	88.0	192.3297	0.8885	1.6508	0.752	
Contribution From Street 23, Pipe 7000 - 67						0.11			0.00	0.00			0.00	0.00			0.00	0.00	10.90															
Contribution From Street 23, Pipe 90 - 67						1.97			0.00	0.70			0.00	0.00			0.00	0.00	14.88															
	67	68	0.15	0.65	0.27	4.50			0.00	0.70			0.00	0.00			0.00	0.00	14.88	62.05	83.94	98.30	143.55	338	750	750	CONC	0.15	58.5	431.1703	0.9760	0.9990	0.784	
Contribution From Street 25, Pipe 91 - 68						0.74			0.00	0.00			0.00	0.00			0.00	0.00	11.52															
	68	73	0.16	0.65	0.29	5.53			0.00	0.70			0.00	0.00			0.00	0.00	15.88	59.76	80.81	94.62	138.16	387	825	825	CONC	0.15	64.5	555.9418	1.0400	1.0337	0.696	
Contribution From Street 14, Pipe 72 - 73						2.62			0.00	0.00			0.00	0.00			0.00	0.00	16.82															
Contribution From Street 14, Pipe 93 - 73						0.80			0.00	0.00			0.00	0.00			0.00	0.00	11.56															
	73	75	0.10	0.65	0.18	9.13			0.00	0.70			0.00	0.00			0.00	0.00	16.92	57.59	77.84	91.13	133.03	580	975	975	CONC	0.15	63.0	867.9562	1.1625	0.9032	0.668	
Contribution From Street 3, Pipe 108 - 75						0.00			0.00	0.11			0.00	0.00			0.00	0.00	10.44															
Contribution From Street 3, Pipe 74 - 75						0.80			0.00	0.00																								

**STORM SEWER CALCULATION SHEET (RATIONAL METHOD)**



Local Roads Return Frequency = 2 years  
 Collector Roads Return Frequency = 5 years  
 Arterial Roads Return Frequency = 10 years

Manning 0.013

LOCATION			AREA (Ha)																FLOW					SEWER DATA										
			2 YEAR				5 YEAR				10 YEAR				100 YEAR				Time of Conc.	Intensity 2 Year	Intensity 5 Year	Intensity 10 Year	Intensity 100 Year	Peak Flow Q (l/s)	DIA. (mm) (actual)	DIA. (mm) (nominal)	TYPE	SLOPE (%)	LENGTH (m)	CAPACITY (l/s)	VELOCITY (m/s)	TIME OF LOW (min)	RATIO Q/Q full	
Location	From Node	To Node	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	(min)	(mm/h)	(mm/h)	(mm/h)	(mm/h)											
Contribution From Street 29, Pipe 116 - 122						8.57				1.48					0.00				0.00	19.60														
	122	124			0.00	9.52	0.06	0.65	0.11	5.69				0.00	0.00			0.00	19.60	52.69	71.15	83.27	121.50	907	975	975	CONC	0.23	17.0	1074.7714	1.4395	0.1968	0.844	
To Street 30, Pipe 124 - 125						9.52				5.69				0.00				0.00	19.79															
<b>Street 30</b>																																		
Contribution From Street 17, Pipe 122 - 124						9.52				5.69				0.00				0.00	19.79															
Contribution From Street 17, Pipe 123 - 124						0.00				0.22				0.00				0.00	10.29															
	124	125	0.16	0.65	0.29	9.81			0.00	5.91				0.00	0.00			19.79	52.37	70.71	82.75	120.74	932	1050	1050	CONC	0.19	34.5	1190.2955	1.3746	0.4183	0.783		
	125	OGS W1	0.20	0.65	0.36	10.17			0.00	5.91				0.00	0.00			20.21	51.69	69.79	81.67	119.16	938	1050	1050	CONC	0.19	35.0	1190.2955	1.3746	0.4244	0.788		

Definitions:  
 Q = 2.78 AIR, where  
 Q = Peak Flow in Litres per second (L/s)  
 A = Areas in hectares (ha)  
 I = Rainfall Intensity (mm/h)  
 R = Runoff Coefficient

Notes:  
 1) Ottawa Rainfall-Intensity Curve  
 2) Min. Velocity = 0.80 m/s



Designed: A.K.	PROJECT: BARRHAVEN CONSERVANCY WEST		
Checked: W.L.	LOCATION: City of Ottawa		
Dwg. Reference:	File Ref: 20-1226	Date: Oct 2021	Sheet No. SHEET 7 OF 7





**CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION  
BASED ON THE RATIONAL RAINFALL METHOD  
BASED ON A FINE PARTICLE SIZE DISTRIBUTION**



**Project Name:** 891 Conservancy East  
**Location:** Ottawa, ON  
**OGS #:** W1

**Engineer:** DSEL  
**Contact:** M. Pichette  
**Report Date:** 14-Oct-21

**Area** 8.92 ha  
**Weighted C** 0.65  
**CDS Model** 5640

**Rainfall Station #** 215  
**Particle Size Distribution** FINE  
**CDS Treatment Capacity** 255 l/s

<u>Rainfall Intensity<sup>1</sup></u> <u>(mm/hr)</u>	<u>Percent Rainfall Volume<sup>1</sup></u>	<u>Cumulative Rainfall Volume</u>	<u>Total Flowrate (l/s)</u>	<u>Treated Flowrate (l/s)</u>	<u>Operating Rate (%)</u>	<u>Removal Efficiency (%)</u>	<u>Incremental Removal (%)</u>
1.0	10.6%	19.8%	16.1	16.1	6.3	97.0	10.3
1.5	9.9%	29.7%	24.2	24.2	9.5	96.1	9.5
2.0	8.4%	38.1%	32.2	32.2	12.6	95.2	8.0
2.5	7.7%	45.8%	40.3	40.3	15.8	94.3	7.3
3.0	5.9%	51.7%	48.4	48.4	19.0	93.4	5.6
3.5	4.4%	56.1%	56.4	56.4	22.1	92.5	4.0
4.0	4.7%	60.7%	64.5	64.5	25.3	91.6	4.3
4.5	3.3%	64.0%	72.5	72.5	28.5	90.7	3.0
5.0	3.0%	67.1%	80.6	80.6	31.6	89.8	2.7
6.0	5.4%	72.4%	96.7	96.7	37.9	88.0	4.7
7.0	4.4%	76.8%	112.8	112.8	44.3	86.2	3.7
8.0	3.5%	80.3%	128.9	128.9	50.6	84.4	3.0
9.0	2.8%	83.2%	145.1	145.1	56.9	82.5	2.3
10.0	2.2%	85.3%	161.2	161.2	63.2	80.7	1.8
15.0	7.0%	92.3%	241.8	241.8	94.9	71.7	5.0
20.0	4.5%	96.9%	322.4	254.9	100.0	55.5	2.5
25.0	1.4%	98.3%	403.0	254.9	100.0	44.4	0.6
30.0	0.7%	99.0%	483.6	254.9	100.0	37.0	0.2
35.0	0.5%	99.5%	564.1	254.9	100.0	31.7	0.1
40.0	0.5%	100.0%	644.7	254.9	100.0	27.7	0.2
45.0	0.0%	100.0%	725.3	254.9	100.0	24.7	0.0
50.0	0.0%	100.0%	805.9	254.9	100.0	22.2	0.0

87.9

Removal Efficiency Adjustment<sup>2</sup> = 6.5%

**Predicted Net Annual Load Removal Efficiency = 81.4%**

**Predicted Annual Rainfall Treated = 97.6%**

1 - Based on 42 years of hourly rainfall data from Canadian Station 6105976, Ottawa ON

2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.

3 - CDS Efficiency based on testing conducted at the University of Central Florida

4 - CDS design flowrate and scaling based on standard manufacturer model & product specifications





**CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION  
BASED ON THE RATIONAL RAINFALL METHOD  
BASED ON A FINE PARTICLE SIZE DISTRIBUTION**



<b>Project Name:</b> 891 Conservancy East	<b>Engineer:</b> DSEL
<b>Location:</b> Ottawa, ON	<b>Contact:</b> M. Pichette
<b>OGS #:</b> W2	<b>Report Date:</b> 14-Oct-21
<b>Area</b> 8.22 ha	<b>Rainfall Station #</b> 215
<b>Weighted C</b> 0.65	<b>Particle Size Distribution</b> FINE
<b>CDS Model</b> 4045	<b>CDS Treatment Capacity</b> 212 l/s

<u>Rainfall Intensity<sup>1</sup></u> <u>(mm/hr)</u>	<u>Percent Rainfall Volume<sup>1</sup></u>	<u>Cumulative Rainfall Volume</u>	<u>Total Flowrate (l/s)</u>	<u>Treated Flowrate (l/s)</u>	<u>Operating Rate (%)</u>	<u>Removal Efficiency (%)</u>	<u>Incremental Removal (%)</u>
1.0	10.6%	19.8%	14.9	14.9	7.0	96.9	10.3
1.5	9.9%	29.7%	22.3	22.3	10.5	95.9	9.5
2.0	8.4%	38.1%	29.7	29.7	14.0	94.8	7.9
2.5	7.7%	45.8%	37.1	37.1	17.5	93.8	7.2
3.0	5.9%	51.7%	44.6	44.6	21.0	92.8	5.5
3.5	4.4%	56.1%	52.0	52.0	24.5	91.8	4.0
4.0	4.7%	60.7%	59.4	59.4	28.0	90.8	4.2
4.5	3.3%	64.0%	66.8	66.8	31.5	89.8	3.0
5.0	3.0%	67.1%	74.3	74.3	35.0	88.8	2.7
6.0	5.4%	72.4%	89.1	89.1	42.0	86.8	4.7
7.0	4.4%	76.8%	104.0	104.0	49.0	84.8	3.7
8.0	3.5%	80.3%	118.8	118.8	55.9	82.8	2.9
9.0	2.8%	83.2%	133.7	133.7	62.9	80.8	2.3
10.0	2.2%	85.3%	148.5	148.5	69.9	78.8	1.7
15.0	7.0%	92.3%	222.8	212.4	100.0	66.9	4.7
20.0	4.5%	96.9%	297.1	212.4	100.0	50.2	2.3
25.0	1.4%	98.3%	371.3	212.4	100.0	40.1	0.6
30.0	0.7%	99.0%	445.6	212.4	100.0	33.5	0.2
35.0	0.5%	99.5%	519.9	212.4	100.0	28.7	0.1
40.0	0.5%	100.0%	594.1	212.4	100.0	25.1	0.1
45.0	0.0%	100.0%	668.4	212.4	100.0	22.3	0.0
50.0	0.0%	100.0%	742.7	212.4	100.0	20.1	0.0

	Removal Efficiency Adjustment <sup>2</sup> =	6.5%
	<b>Predicted Net Annual Load Removal Efficiency =</b>	<b>80.2%</b>
	<b>Predicted Annual Rainfall Treated =</b>	<b>96.8%</b>

1 - Based on 42 years of hourly rainfall data from Canadian Station 6105976, Ottawa ON  
 2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.  
 3 - CDS Efficiency based on testing conducted at the University of Central Florida  
 4 - CDS design flowrate and scaling based on standard manufacturer model & product specifications



**CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION  
BASED ON THE RATIONAL RAINFALL METHOD  
BASED ON A FINE PARTICLE SIZE DISTRIBUTION**



**Project Name:** 891 Conservancy East

**Engineer:** DSEL

**Location:** Ottawa, ON

**Contact:** M. Pichette

**OGS #:** W3

**Report Date:** 14-Oct-21

**Area** 9.90 ha

**Rainfall Station #** 215

**Weighted C** 0.65

**Particle Size Distribution** FINE

**CDS Model** 5640

**CDS Treatment Capacity** 255 l/s

<u>Rainfall Intensity<sup>1</sup></u> <u>(mm/hr)</u>	<u>Percent Rainfall Volume<sup>1</sup></u>	<u>Cumulative Rainfall Volume</u>	<u>Total Flowrate (l/s)</u>	<u>Treated Flowrate (l/s)</u>	<u>Operating Rate (%)</u>	<u>Removal Efficiency (%)</u>	<u>Incremental Removal (%)</u>
1.0	10.6%	19.8%	17.9	17.9	7.0	96.8	10.3
1.5	9.9%	29.7%	26.8	26.8	10.5	95.8	9.5
2.0	8.4%	38.1%	35.8	35.8	14.0	94.8	7.9
2.5	7.7%	45.8%	44.7	44.7	17.5	93.8	7.2
3.0	5.9%	51.7%	53.7	53.7	21.1	92.8	5.5
3.5	4.4%	56.1%	62.6	62.6	24.6	91.8	4.0
4.0	4.7%	60.7%	71.6	71.6	28.1	90.8	4.2
4.5	3.3%	64.0%	80.5	80.5	31.6	89.8	3.0
5.0	3.0%	67.1%	89.4	89.4	35.1	88.8	2.7
6.0	5.4%	72.4%	107.3	107.3	42.1	86.8	4.7
7.0	4.4%	76.8%	125.2	125.2	49.1	84.8	3.7
8.0	3.5%	80.3%	143.1	143.1	56.1	82.8	2.9
9.0	2.8%	83.2%	161.0	161.0	63.2	80.8	2.3
10.0	2.2%	85.3%	178.9	178.9	70.2	78.7	1.7
15.0	7.0%	92.3%	268.3	254.9	100.0	66.7	4.7
20.0	4.5%	96.9%	357.8	254.9	100.0	50.0	2.3
25.0	1.4%	98.3%	447.2	254.9	100.0	40.0	0.6
30.0	0.7%	99.0%	536.7	254.9	100.0	33.3	0.2
35.0	0.5%	99.5%	626.1	254.9	100.0	28.6	0.1
40.0	0.5%	100.0%	715.6	254.9	100.0	25.0	0.1
45.0	0.0%	100.0%	805.0	254.9	100.0	22.2	0.0
50.0	0.0%	100.0%	894.5	254.9	100.0	20.0	0.0
							86.6

Removal Efficiency Adjustment<sup>2</sup> = 6.5%

**Predicted Net Annual Load Removal Efficiency = 80.1%**

**Predicted Annual Rainfall Treated = 96.7%**

1 - Based on 42 years of hourly rainfall data from Canadian Station 6105976, Ottawa ON

2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.

3 - CDS Efficiency based on testing conducted at the University of Central Florida

4 - CDS design flowrate and scaling based on standard manufacturer model & product specifications



**CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION  
BASED ON THE RATIONAL RAINFALL METHOD  
BASED ON A FINE PARTICLE SIZE DISTRIBUTION**



<b>Project Name:</b> 891 Conservancy East	<b>Engineer:</b> DSEL
<b>Location:</b> Ottawa, ON	<b>Contact:</b> M. Pichette
<b>OGS #:</b> W4	<b>Report Date:</b> 14-Oct-21
<b>Area</b> 8.60 ha	<b>Rainfall Station #</b> 215
<b>Weighted C</b> 0.65	<b>Particle Size Distribution</b> FINE
<b>CDS Model</b> 5640	<b>CDS Treatment Capacity</b> 255 l/s

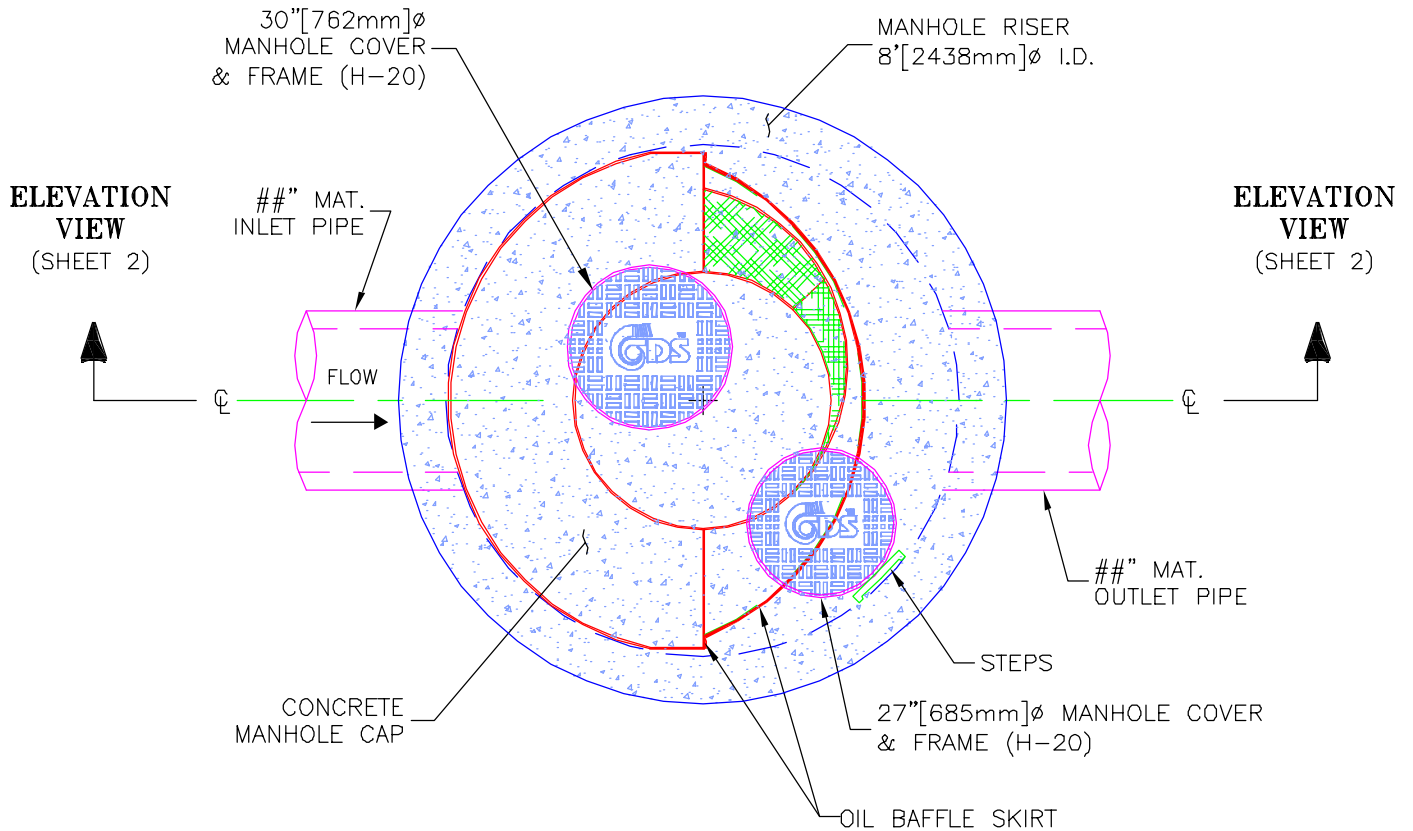
<u>Rainfall Intensity<sup>1</sup></u> <u>(mm/hr)</u>	<u>Percent Rainfall Volume<sup>1</sup></u>	<u>Cumulative Rainfall Volume</u>	<u>Total Flowrate (l/s)</u>	<u>Treated Flowrate (l/s)</u>	<u>Operating Rate (%)</u>	<u>Removal Efficiency (%)</u>	<u>Incremental Removal (%)</u>
1.0	10.6%	19.8%	15.5	15.5	6.1	97.1	10.3
1.5	9.9%	29.7%	23.3	23.3	9.1	96.2	9.5
2.0	8.4%	38.1%	31.1	31.1	12.2	95.4	8.0
2.5	7.7%	45.8%	38.9	38.9	15.2	94.5	7.3
3.0	5.9%	51.7%	46.6	46.6	18.3	93.6	5.6
3.5	4.4%	56.1%	54.4	54.4	21.3	92.7	4.0
4.0	4.7%	60.7%	62.2	62.2	24.4	91.9	4.3
4.5	3.3%	64.0%	69.9	69.9	27.4	91.0	3.0
5.0	3.0%	67.1%	77.7	77.7	30.5	90.1	2.7
6.0	5.4%	72.4%	93.2	93.2	36.6	88.4	4.8
7.0	4.4%	76.8%	108.8	108.8	42.7	86.6	3.8
8.0	3.5%	80.3%	124.3	124.3	48.8	84.9	3.0
9.0	2.8%	83.2%	139.9	139.9	54.9	83.1	2.3
10.0	2.2%	85.3%	155.4	155.4	61.0	81.4	1.8
15.0	7.0%	92.3%	233.1	233.1	91.5	72.6	5.1
20.0	4.5%	96.9%	310.8	254.9	100.0	57.6	2.6
25.0	1.4%	98.3%	388.5	254.9	100.0	46.1	0.7
30.0	0.7%	99.0%	466.2	254.9	100.0	38.4	0.3
35.0	0.5%	99.5%	543.9	254.9	100.0	32.9	0.2
40.0	0.5%	100.0%	621.6	254.9	100.0	28.8	0.2
45.0	0.0%	100.0%	699.3	254.9	100.0	25.6	0.0
50.0	0.0%	100.0%	777.0	254.9	100.0	23.0	0.0
							88.3

Removal Efficiency Adjustment<sup>2</sup> = 6.5%  
**Predicted Net Annual Load Removal Efficiency = 81.8%**  
**Predicted Annual Rainfall Treated = 97.8%**

1 - Based on 42 years of hourly rainfall data from Canadian Station 6105976, Ottawa ON  
2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.  
3 - CDS Efficiency based on testing conducted at the University of Central Florida  
4 - CDS design flowrate and scaling based on standard manufacturer model & product specifications



# PLAN VIEW



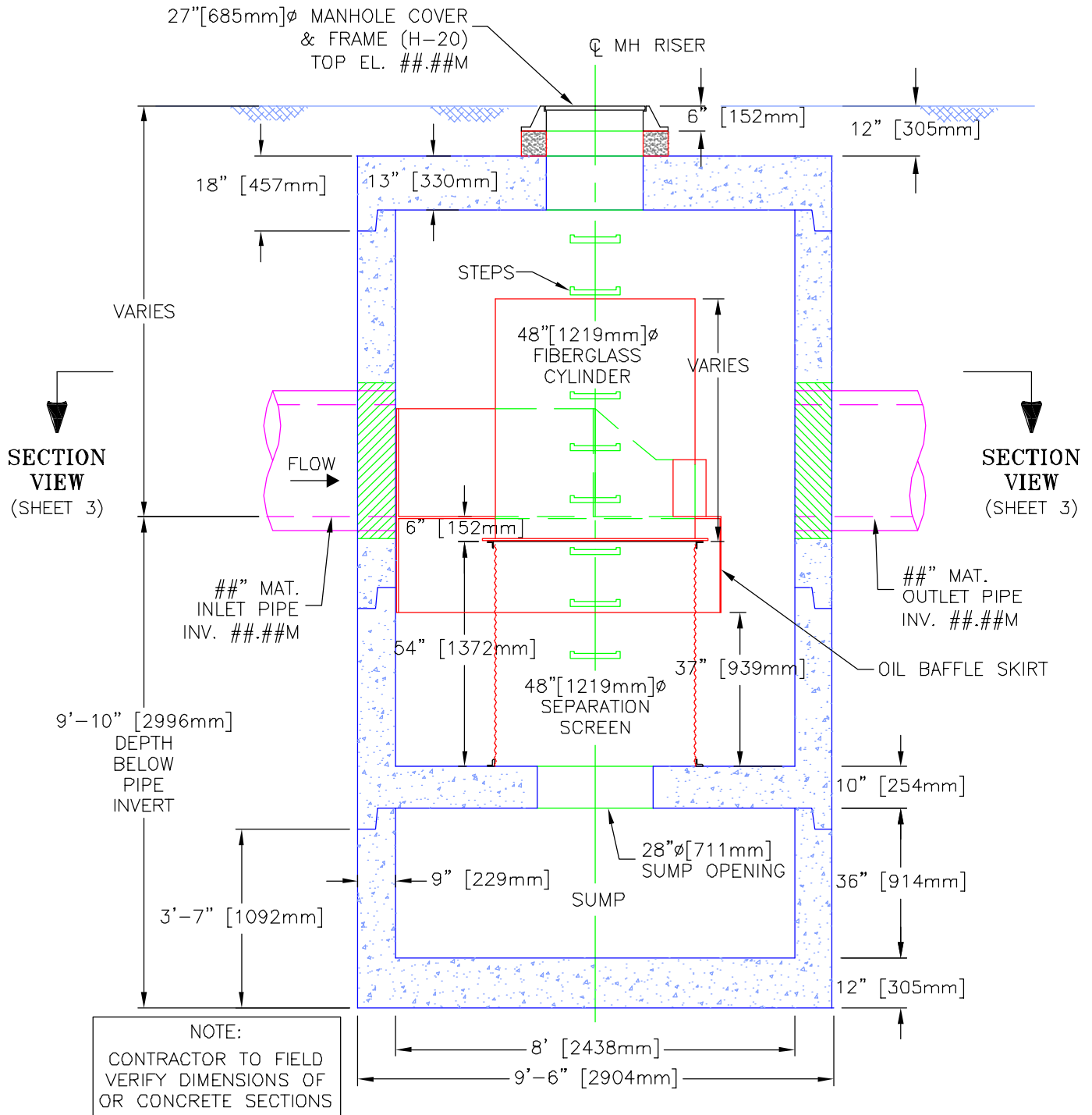
## CDS MODEL PMSU40\_45m, 7.5 CFS TREATMENT CAPACITY STORM WATER TREATMENT UNIT

	<b>PROJECT NAME</b> CITY, STATE	JOB#      XX-##-###	SCALE 1" = 3'
		DATE      ##/##/##	SHEET
		DRAWN    INITIALS	1
		APPROV.	





# ELEVATION VIEW



## CDS MODEL PMSU40\_45m, 7.5 CFS TREATMENT CAPACITY STORM WATER TREATMENT UNIT

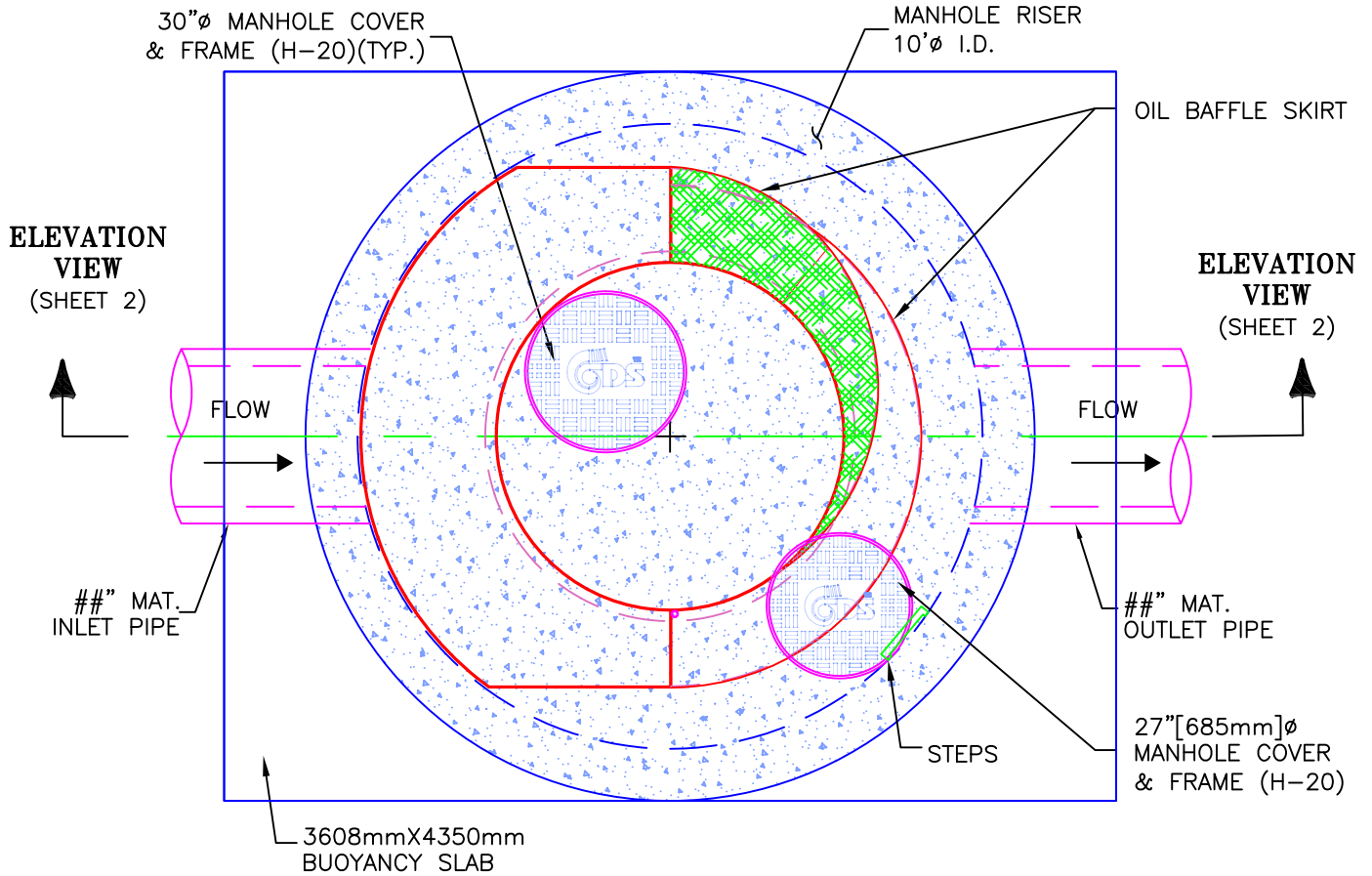


PROJECT NAME  
CITY, STATE

JOB#	XX-##-###	SCALE 1" = 3'
DATE	##/##/##	SHEET
DRAWN	INITIALS	2
APPROV.		



# PLAN VIEW



## CDS MODEL PMSU56\_40m, 9 CFS TREATMENT CAPACITY STORM WATER TREATMENT UNIT



**PROJECT NAME**  
CITY, STATE

JOB# XX-##-###

DATE ##/##/##

DRAWN INITIALS

APPROV.

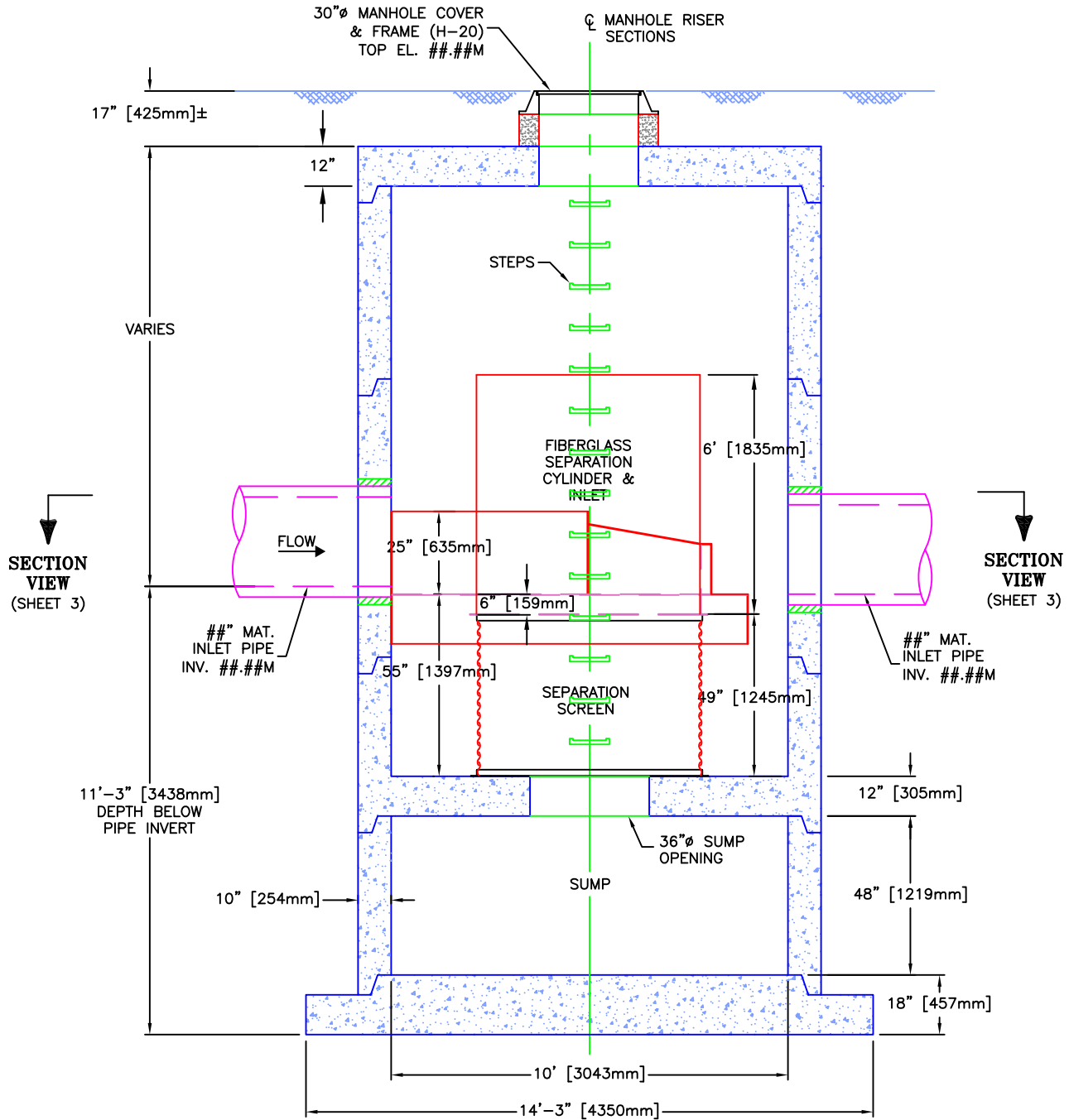
SCALE  
1" = 3'

SHEET

1



# ELEVATION VIEW



## CDS MODEL PMSU56\_40m, 9 CFS TREATMENT CAPACITY STORM WATER TREATMENT UNIT



PROJECT NAME  
CITY, STATE

JOB# XX-##-###  
DATE ##/##/##  
DRAWN INITIALS  
APPROV.

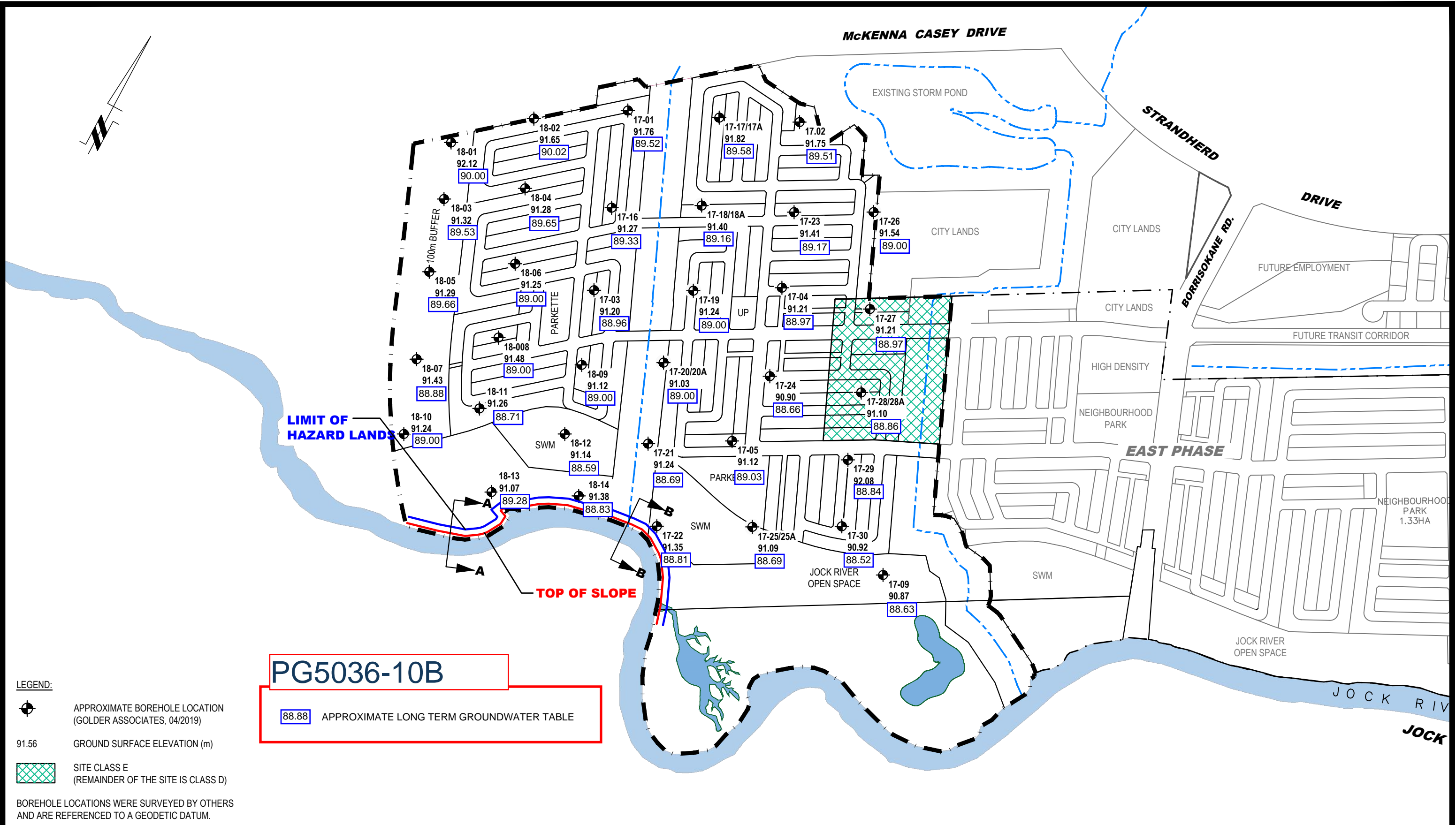
SCALE  
1" = 4'

SHEET

2







- LEGEND:**
- APPROXIMATE BOREHOLE LOCATION (GOLDER ASSOCIATES, 04/2019)
  - 91.56 GROUND SURFACE ELEVATION (m)
  - SITE CLASS E (REMAINDER OF THE SITE IS CLASS D)

BOREHOLE LOCATIONS WERE SURVEYED BY OTHERS AND ARE REFERENCED TO A GEODETIC DATUM.

**patersongroup**  
consulting engineers

154 Colonnade Road South  
Ottawa, Ontario K2E 7J5  
Tel: (613) 226-7381 Fax: (613) 226-6344

NO.	REVISIONS	DATE	INITIAL

**CAIVAN COMMUNITIES**  
**GEOTECHNICAL INVESTIGATION**  
**PROP. RESIDENTIAL DEVELOPMENT - CONSERVANCY LANDS WEST**  
**OTTAWA, ONTARIO**

Title: **TEST HOLE LOCATION PLAN**

Scale:	1:6000	Date:	09/2019
Drawn by:	MPG	Report No.:	PG5036-2
Checked by:	SD	<b>PG5036-4</b>	Revision No.:
Approved by:	SD		

p:\autoCAD drawings\geotechnical\pg5036\pg5036-3 final west land.dwg



October 14, 2021

Project Number: 1474

David Schaeffer Engineering Ltd  
120 Iber Road, Unit 103  
Ottawa, Ontario  
K2S 1E9

**Attention: Steve Pichette, P.Eng**

**Subject: BCDC Phase 3 – Preliminary HGL Analysis**

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## Introduction

Phase 3 of the Barrhaven Conservancy Development is located in Barrhaven, Ontario, north of the Jock River, east of highway 416 and west of the Foster Creek. The proposed development is approximately 35.6 ha that will primarily comprise of single and townhouse residential lots along with a 2.91 ha park. The following outlines the preliminary hydraulic grade line (HGL) assessment for the site, to ensure that the proposed minor system within the development is adequately sized to safely convey flows to the Jock River under various conditions. As such the following memo outlines the approach taken in assessing the development's HGL and summarises the findings of this analysis.

## Analysis Approach

Preliminary hydraulic grade line calculations for the proposed BCDC Phase 3 development were completed using PCSWMM modelling software. Pipe data, storm sewer layout and Rational Method flows in the storm sewer are as provided by DSEL. The Rational Method flows were calculated based on the 2-, 5- or 10-year level of service requirements, and the 100-year flows in the hydraulic grade line calculations were estimated as 14% greater than the Rational Method flows, to account for the additional flows captured by catchbasin grates, lead pipes and/or inlet control devices under the higher surface water depths of the 100-year storm. The proposed storm sewer infrastructure data was extracted from DSEL's detailed drawings and incorporated into a PCSWMM model, and flows derived by DSEL's rational method calculations were then applied to each Maintenance Hole (MH) in the model as steady flows (using the baseflow option). Exit losses were applied to all storm sewer pipes in the system based on the angle of the downstream connection. As with all other works completed for the BCDC development phases, the preliminary HGL analysis was completed under two conditions:

- 100-year rainfall event on the development and a 5-year spring water level on the Jock River
- 5-year rainfall event on the development and a 100-year spring water level on the Jock River

Note that the water level along the Jock River through the length of this development varies, and as such the nearest corresponding upstream water surface elevation calculated by RVCA's HEC-RAS floodplain mapping model of the Jock River was applied at each of the respective storm sewer outlets. Also, note that assuming a 5-year spring water level on the Jock River for a 100-year rainfall event on the development is an inherently conservative assumption, as the critical storm for the proposed development is a summer (intense rainfall) event while the critical storm for the Jock River is a Spring (snowmelt + rainfall) event. A preliminary Single Station Flood Frequency analysis was completed by JFSA using only summer flows (from May 15 to October 31) based on historical flow data recorded at the Moodie Drive Water Survey Canada gauge. This analysis found that the 100-year summer flow on the Jock River is around 99 m<sup>3</sup>/s, while the 5-year spring flow is around 123 m<sup>3</sup>/s.

## Results

The maximum HGL obtained at each MH has been extracted from the 100-year event / 5-year Jock River water level scenario and 5-year event / 100-year Jock River water level scenario, with the results from this analysis provided in Tables 1 & 2, respectively. As all proposed units within this development will have sump pumps, the simulated HGL was compared against the top of MH elevation to ensure that all storm sewers infrastructure is sufficiently sized and is not surcharging to the major system during the assessed events.

From this analysis, it was found that the critical scenario for HGL within the development was the 5-year development event and 100-year water level on the Jock River scenario. Based on this scenario, no MHs will have an HGL elevation above the top of MH (minimum freeboard of 0.07 m at MH-11300), with an average freeboard of 0.62 m from the top of MH throughout the proposed development. For the 100-year event and 5-year water level on the Jock River, no MHs will have HGL elevations above the top of MH (minimum freeboard of 0.64 m at MH-11300), with an average freeboard of 1.16 m from the top of MH throughout the proposed development. As such it can be concluded that the proposed storm sewer infrastructure is sufficiently sized, to safely convey minor system flows from the development under various extreme conditions.

## Conclusion

A preliminary HGL analysis for Phase 2 of the Barrhaven Conservancy Development was completed using PCSWMM based on storm sewer and flow details provided by DSEL. From this analysis, it was found that the proposed storm sewer infrastructure is sufficiently sized to convey all minor system flows to the Jock River and will not result in any MHs surcharging to the street under extreme events such as 100-year rainfall event on the development and a 5-year spring water level on the Jock River and, a 5-year rainfall event on the development and a 100-year spring water level on the Jock River. With the former being the more critical scenario for the HGL within the development.

Yours truly,  
**J.F Sabourin and Associates Inc.**



Jonathon Burnett, P.Eng  
Water Resources Engineer

cc: J.F Sabourin, M.Eng, P.Eng  
Director of Water Resources Projects





## **Figures**

Figure 1: PCSWMM Model Overview

## **Tables**

Table 1: HGL Result Tables - 100-Year BCDC Development & 5-Year Jock River

Table 2: HGL Result Tables - 5-Year BCDC Development & 100-Year Jock River

## **Attachments**

Attachment A: DSEL Rational Method Calculations

Attachment B: PCSWMM Model Input files



### Legend

- Junctions
- Conduits
- ▲ Outfalls
- Development Lines

**Table 1: BCDC Phase 3 - Preliminary HGL Analysis  
100-Year BCDC Development & 5-Year Jock River**

MH-ID	Invert Elevation	Top of MH (m)	Max HGL (m)	Freeboard (m)
1	91.42	93.84	92.26	1.58
2	91.69	93.73	92.16	1.57
3	91.46	93.63	92.04	1.59
4	91.27	93.62	92.00	1.62
5	91.05	93.51	91.92	1.59
6	90.91	93.38	91.83	1.55
7	90.72	93.30	91.75	1.55
8	91.12	93.35	91.78	1.57
9	91.23	93.31	91.78	1.53
10	90.62	93.22	91.70	1.52
11	91.82	93.69	92.25	1.44
12	91.67	93.66	92.21	1.45
13	91.44	93.65	92.14	1.51
14	91.19	93.54	92.03	1.51
15	90.99	93.45	91.94	1.51
16	90.88	93.36	91.88	1.48
17	90.71	93.25	91.77	1.48
18	90.61	93.23	91.73	1.50
19	90.45	93.15	91.64	1.51
20	91.71	93.68	92.25	1.43
21	91.43	93.58	92.12	1.46
22	91.16	93.48	91.98	1.50
23	90.93	93.39	91.88	1.51
24	90.73	93.26	91.76	1.50
25	90.60	93.20	91.69	1.51
26	90.43	93.14	91.61	1.53
27	90.71	93.15	91.63	1.52
28	90.65	93.13	91.61	1.52
29	90.15	93.05	91.48	1.57
31	91.78	93.78	92.56	1.22
32	91.82	93.76	92.54	1.22
33	91.65	93.71	92.45	1.26
34	91.46	93.69	92.42	1.27
35	91.15	93.58	92.33	1.25
36	91.02	93.46	92.29	1.17
37	90.91	93.37	92.24	1.13
38	91.47	93.66	92.44	1.22
39	91.44	93.56	92.32	1.24
40	91.22	93.53	92.32	1.21
41	91.08	93.44	92.27	1.17
42	91.17	93.38	92.16	1.22
43	90.88	93.35	92.17	1.18
44	90.66	93.28	92.14	1.14
45	91.22	93.50	92.22	1.28
46	90.97	93.32	92.12	1.20

**Table 1: BCDC Phase 3 - Preliminary HGL Analysis  
100-Year BCDC Development & 5-Year Jock River**

<b>MH-ID</b>	<b>Invert Elevation</b>	<b>Top of MH (m)</b>	<b>Max HGL (m)</b>	<b>Freeboard (m)</b>
47	90.50	93.19	92.02	1.17
48	90.39	93.12	91.96	1.16
49	90.78	93.12	91.96	1.16
50	90.30	93.09	91.91	1.18
51	90.21	93.08	91.88	1.20
52	90.02	93.00	91.71	1.29
53	90.72	93.00	91.62	1.38
54	89.92	92.95	91.61	1.34
55	89.75	92.82	91.48	1.34
56	89.70	92.81	91.45	1.36
57	90.70	92.95	91.73	1.22
58	90.48	92.88	91.62	1.26
59	90.32	92.81	91.50	1.31
60	90.26	92.80	91.46	1.34
61	89.61	92.77	91.34	1.43
63	91.68	93.61	92.61	1.00
64	91.62	93.66	92.56	1.10
65	91.30	93.52	92.46	1.06
66	91.05	93.42	92.34	1.08
67	90.65	93.29	92.21	1.08
68	90.49	93.20	92.13	1.07
69	91.28	93.49	92.44	1.05
70	91.03	93.36	92.32	1.04
71	90.88	93.26	92.26	1.00
72	90.69	93.20	92.14	1.06
73	90.24	93.11	92.06	1.05
74	90.95	93.27	92.12	1.15
75	90.12	93.01	91.98	1.03
76	89.96	92.92	91.82	1.10
77	89.82	92.82	91.66	1.16
78	89.67	92.71	91.53	1.18
79	89.62	92.69	91.48	1.21
80	90.40	92.80	91.61	1.19
81	90.18	92.68	91.47	1.21
82	90.08	92.66	91.43	1.23
83	89.52	92.65	91.35	1.30
85	91.75	93.63	92.61	1.02
86	91.52	93.59	92.54	1.05
87	91.34	93.57	92.51	1.06
88	91.23	93.53	92.42	1.11
89	91.04	93.52	92.37	1.15
90	90.89	93.45	92.31	1.14
91	91.18	93.31	92.32	0.99
92	91.14	93.09	92.32	0.77
93	91.09	93.23	92.21	1.02



**Table 1: BCDC Phase 3 - Preliminary HGL Analysis  
100-Year BCDC Development & 5-Year Jock River**

<b>MH-ID</b>	<b>Invert Elevation</b>	<b>Top of MH (m)</b>	<b>Max HGL (m)</b>	<b>Freeboard (m)</b>
94	90.87	92.98	92.20	0.78
95	91.47	93.55	92.44	1.11
96	91.24	93.15	92.39	0.76
97	91.12	93.13	92.38	0.75
98	90.92	93.04	92.29	0.75
99	90.76	92.95	92.19	0.76
100	90.71	92.93	92.16	0.77
101	90.54	92.92	92.10	0.82
102	90.37	92.83	92.00	0.83
103	91.16	93.24	91.91	1.33
104	90.17	92.81	91.87	0.94
105	90.07	92.73	91.84	0.89
106	89.96	92.65	91.77	0.88
107	89.89	92.63	91.74	0.89
108	90.87	93.08	91.98	1.10
109	90.73	92.68	91.93	0.75
110	90.72	92.75	92.04	0.71
111	90.94	92.82	91.95	0.87
112	90.68	92.77	91.91	0.86
113	90.53	92.54	91.75	0.79
114	90.44	92.60	91.90	0.70
115	90.28	92.67	91.86	0.81
116	89.80	92.62	91.69	0.93
117	90.83	92.94	91.83	1.11
118	90.58	92.52	91.74	0.78
119	90.47	92.51	91.73	0.78
120	90.17	92.45	91.70	0.75
121	89.97	92.57	91.61	0.96
122	89.59	92.53	91.51	1.02
123	90.59	92.87	91.33	1.54
124	89.48	92.50	91.30	1.20
125	89.40	92.45	91.24	1.21
1500	91.41	93.45	91.84	1.61
3200	91.97	93.77	92.70	1.07
4000	91.47	93.52	92.30	1.22
5200	90.89	93.00	91.75	1.25
6400	91.79	93.59	92.73	0.86
7000	91.25	93.37	92.21	1.16
7700	90.77	92.83	91.74	1.09
9000	90.94	93.30	91.74	1.56
10200	91.05	92.83	91.95	0.88
11000	90.93	92.74	91.95	0.79
11100	91.02	92.81	92.14	0.67
11200	90.64	92.76	91.93	0.83
11300	90.61	92.54	91.90	0.64

**Table 1: BCDC Phase 3 - Preliminary HGL Analysis  
100-Year BCDC Development & 5-Year Jock River**

<b>MH-ID</b>	<b>Invert Elevation</b>	<b>Top of MH (m)</b>	<b>Max HGL (m)</b>	<b>Freeboard (m)</b>	
90000	91.42	93.45	92.40	1.05	
11100	91.02	92.81	92.14	0.67	
11200	90.64	92.76	91.93	0.83	
11300	90.61	92.54	91.90	0.64	
90000	91.42	93.45	92.40	1.05	
				<b>Min</b>	0.64
				<b>Max</b>	1.62
				<b>Average</b>	1.16

Note: Analysis assumes 5 year spring water level on the Jock River

Model Name:BCDC-P3\_HGL\_v01-100YrDev-5YrJock.inp

**Table 2: BCDC Phase 3 - Preliminary HGL Analysis  
5-Year BCDC Development & 100-Year Jock River**

<b>MH-ID</b>	<b>Invert Elevation</b>	<b>Top of MH (m)</b>	<b>Max HGL (m)</b>	<b>Freeboard (m)</b>
1	91.42	93.84	92.76	1.08
2	91.69	93.73	92.68	1.05
3	91.46	93.63	92.58	1.05
4	91.27	93.62	92.56	1.06
5	91.05	93.51	92.49	1.02
6	90.91	93.38	92.43	0.95
7	90.72	93.30	92.37	0.93
8	91.12	93.35	92.39	0.96
9	91.23	93.31	92.39	0.92
10	90.62	93.22	92.33	0.89
11	91.82	93.69	92.75	0.94
12	91.67	93.66	92.72	0.94
13	91.44	93.65	92.67	0.98
14	91.19	93.54	92.58	0.96
15	90.99	93.45	92.51	0.94
16	90.88	93.36	92.47	0.89
17	90.71	93.25	92.38	0.87
18	90.61	93.23	92.35	0.88
19	90.45	93.15	92.28	0.87
20	91.71	93.68	92.75	0.93
21	91.43	93.58	92.65	0.93
22	91.16	93.48	92.55	0.93
23	90.93	93.39	92.47	0.92
24	90.73	93.26	92.37	0.89
25	90.60	93.20	92.32	0.88
26	90.43	93.14	92.26	0.88
27	90.71	93.15	92.27	0.88
28	90.65	93.13	92.26	0.87
29	90.15	93.05	92.16	0.89
30	90.00	93.04	92.06	0.98
31	91.78	93.78	92.99	0.79
32	91.82	93.76	92.97	0.79
33	91.65	93.71	92.90	0.81
34	91.46	93.69	92.88	0.81
35	91.15	93.58	92.81	0.77
36	91.02	93.46	92.78	0.68
37	90.91	93.37	92.74	0.63
38	91.47	93.66	92.89	0.77
39	91.44	93.56	92.81	0.75
40	91.22	93.53	92.81	0.72
41	91.08	93.44	92.77	0.67
42	91.17	93.38	92.68	0.70
43	90.88	93.35	92.68	0.67
44	90.66	93.28	92.66	0.62
45	91.22	93.50	92.73	0.77

**Table 2: BCDC Phase 3 - Preliminary HGL Analysis  
5-Year BCDC Development & 100-Year Jock River**

<b>MH-ID</b>	<b>Invert Elevation</b>	<b>Top of MH (m)</b>	<b>Max HGL (m)</b>	<b>Freeboard (m)</b>
46	90.97	93.32	92.65	0.67
47	90.50	93.19	92.58	0.61
48	90.39	93.12	92.53	0.59
49	90.78	93.12	92.52	0.60
50	90.30	93.09	92.49	0.60
51	90.21	93.08	92.47	0.61
52	90.02	93.00	92.33	0.67
53	90.72	93.00	92.27	0.73
54	89.92	92.95	92.26	0.69
55	89.75	92.82	92.16	0.66
56	89.70	92.81	92.14	0.67
57	90.70	92.95	92.35	0.60
58	90.48	92.88	92.27	0.61
59	90.32	92.81	92.18	0.63
60	90.26	92.80	92.14	0.66
61	89.61	92.77	92.05	0.72
62	89.57	92.77	92.02	0.75
63	91.68	93.61	93.02	0.59
64	91.62	93.66	92.99	0.67
65	91.30	93.52	92.91	0.61
66	91.05	93.42	92.81	0.61
67	90.65	93.29	92.71	0.58
68	90.49	93.20	92.65	0.55
69	91.28	93.49	92.90	0.59
70	91.03	93.36	92.80	0.56
71	90.88	93.26	92.76	0.50
72	90.69	93.20	92.66	0.54
73	90.24	93.11	92.60	0.51
74	90.95	93.27	92.65	0.62
75	90.12	93.01	92.54	0.47
76	89.96	92.92	92.42	0.50
77	89.82	92.82	92.30	0.52
78	89.67	92.71	92.19	0.52
79	89.62	92.69	92.16	0.53
80	90.40	92.80	92.26	0.54
81	90.18	92.68	92.15	0.53
82	90.08	92.66	92.12	0.54
83	89.52	92.65	92.06	0.59
84	89.46	92.65	92.02	0.63
85	91.75	93.63	93.02	0.61
86	91.52	93.59	92.97	0.62
87	91.34	93.57	92.94	0.63
88	91.23	93.53	92.88	0.65
89	91.04	93.52	92.84	0.68
90	90.89	93.45	92.79	0.66



**Table 2: BCDC Phase 3 - Preliminary HGL Analysis  
5-Year BCDC Development & 100-Year Jock River**

<b>MH-ID</b>	<b>Invert Elevation</b>	<b>Top of MH (m)</b>	<b>Max HGL (m)</b>	<b>Freeboard (m)</b>
91	91.18	93.31	92.80	0.51
92	91.14	93.09	92.80	0.29
93	91.09	93.23	92.71	0.52
94	90.87	92.98	92.70	0.28
95	91.47	93.55	92.88	0.67
96	91.24	93.15	92.84	0.31
97	91.12	93.13	92.83	0.30
98	90.92	93.04	92.77	0.27
99	90.76	92.95	92.69	0.26
100	90.71	92.93	92.67	0.26
101	90.54	92.92	92.63	0.29
102	90.37	92.83	92.54	0.29
103	91.16	93.24	92.48	0.76
104	90.17	92.81	92.45	0.36
105	90.07	92.73	92.42	0.31
106	89.96	92.65	92.36	0.29
107	89.89	92.63	92.34	0.29
108	90.87	93.08	92.54	0.54
109	90.73	92.68	92.49	0.19
110	90.72	92.75	92.57	0.18
111	90.94	92.82	92.50	0.32
112	90.68	92.77	92.47	0.30
113	90.53	92.54	92.35	0.19
114	90.44	92.60	92.46	0.14
115	90.28	92.67	92.43	0.24
116	89.80	92.62	92.30	0.32
117	90.83	92.94	92.41	0.53
118	90.58	92.52	92.34	0.18
119	90.47	92.51	92.33	0.18
120	90.17	92.45	92.31	0.14
121	89.97	92.57	92.24	0.33
122	89.59	92.53	92.16	0.37
123	90.59	92.87	92.02	0.85
124	89.48	92.50	92.00	0.50
125	89.40	92.45	91.95	0.50
126	89.35	92.41	91.90	0.51
1500	91.41	93.45	92.44	1.01
3200	91.97	93.77	93.10	0.67
4000	91.47	93.52	92.79	0.73
5200	90.89	93.00	92.37	0.63
6400	91.79	93.59	93.11	0.48
7000	91.25	93.37	92.72	0.65
7700	90.77	92.83	92.36	0.47
9000	90.94	93.30	92.36	0.94
10200	91.05	92.83	92.50	0.33

**Table 2: BCDC Phase 3 - Preliminary HGL Analysis  
5-Year BCDC Development & 100-Year Jock River**

<b>MH-ID</b>	<b>Invert Elevation</b>	<b>Top of MH (m)</b>	<b>Max HGL (m)</b>	<b>Freeboard (m)</b>
11000	90.93	92.74	92.51	0.23
11100	91.02	92.81	92.65	0.16
11200	90.64	92.76	92.49	0.27
11300	90.61	92.54	92.47	0.07
90000	91.42	93.45	92.86	0.59
			<b>Min</b>	0.07
			<b>Max</b>	1.08
			<b>Average</b>	0.62

Note: Analysis assumes 100 year spring water level on the Jock River  
Model Name:BCDC-P3\_HGL\_v01-5YrDev-100YrJock.inp



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Paris, ON  
Gatineau, QC  
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Québec, QC

# Attachment A

DSEL Rational Method Calculations

**STORM SEWER CALCULATION SHEET (RATIONAL METHOD)**

Local Roads Return Frequency = 2 years  
 Collector Roads Return Frequency = 5 years  
 Arterial Roads Return Frequency = 10 years



Manning 0.013

LOCATION		AREA (Ha)																FLOW					SEWER DATA												
		2 YEAR				5 YEAR				10 YEAR				100 YEAR				Time of	Intensity	Intensity	Intensity	Intensity	Peak Flow	DIA. (mm)	DIA. (mm)	TYPE	SLOPE	LENGTH	CAPACITY	VELOCITY	TIME OF	RATIO			
Location	From Node	To Node	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	Conc. (min)	2 Year (mm/h)	5 Year (mm/h)	10 Year (mm/h)	100 Year (mm/h)	Q (l/s)	(actual)	(nominal)	(%)	(m)	(l/s)	(m/s)	LOW (min)	Q/Q full			
<b>Unknown Road2 - 02</b>																																			
	9000	27	0.58	0.65	1.05	1.05			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	80	450	450	CONC	0.20	103.0	127.5033	0.8017	2.1413	0.631		
	27	28	0.11	0.65	0.20	1.25			0.00	0.00			0.00	0.00			0.00	0.00	12.14	69.46	94.10	110.25	161.10	87	450	450	CONC	0.20	12.5	127.5033	0.8017	0.2599	0.679		
	28	29	0.19	0.65	0.34	1.59			0.00	0.00			0.00	0.00			0.00	0.00	12.40	68.67	93.02	108.98	159.23	109	450	450	CONC	0.25	50.5	142.5531	0.8963	0.9390	0.766		
To Unknown Road1 - 01, Pipe 29 - 30					1.59				0.00				0.00				0.00		13.34																
	11	20	0.09	0.65	0.16	0.16			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	12	300	300	PVC	0.35	10.5	57.2089	0.8093	0.2162	0.218		
	20	21	0.40	0.65	0.72	0.89			0.00	0.00			0.00	0.00			0.00	0.00	10.22	75.98	103.06	120.81	176.61	67	375	375	PVC	0.30	67.0	96.0323	0.8695	1.2843	0.701		
	21	22	0.39	0.65	0.70	1.59			0.00	0.00			0.00	0.00			0.00	0.00	11.50	71.49	96.88	113.53	165.91	114	450	450	CONC	0.30	67.0	156.1591	0.9819	1.1373	0.728		
	22	23	0.36	0.65	0.65	2.24			0.00	0.00			0.00	0.00			0.00	0.00	12.64	67.97	92.06	107.85	157.57	152	525	525	CONC	0.25	61.5	215.0311	0.9933	1.0319	0.708		
	23	24	0.47	0.65	0.85	3.09			0.00	0.00			0.00	0.00			0.00	0.00	13.67	65.10	88.12	103.22	150.77	201	600	600	CONC	0.20	82.0	274.5943	0.9712	1.4072	0.733		
	24	25	0.24	0.65	0.43	3.52			0.00	0.00			0.00	0.00			0.00	0.00	15.08	61.59	83.31	97.56	142.47	217	600	600	CONC	0.25	41.5	307.0058	1.0858	0.6370	0.707		
	25	26	0.22	0.65	0.40	3.92			0.00	0.00			0.00	0.00			0.00	0.00	15.71	60.13	81.32	95.22	139.03	236	600	600	CONC	0.25	39.0	307.0058	1.0858	0.5986	0.768		
	26	29	0.32	0.65	0.58	4.50			0.00	0.00			0.00	0.00			0.00	0.00	16.31	58.83	79.54	93.13	135.97	265	675	675	CONC	0.20	63.0	375.9224	1.0505	0.9995	0.704		
To Unknown Road1 - 01, Pipe 29 - 30					4.50				0.00				0.00				0.00		17.31																
	11	12	0.18	0.65	0.33	0.33			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	25	300	300	PVC	0.35	46.5	57.2089	0.8093	0.9576	0.437		
	12	13	0.18	0.65	0.33	0.65			0.00	0.00			0.00	0.00			0.00	0.00	10.96	73.31	99.39	116.49	170.25	48	300	300	PVC	0.45	16.0	64.8688	0.9177	0.2906	0.735		
	13	14	0.40	0.65	0.72	1.37			0.00	0.00			0.00	0.00			0.00	0.00	11.25	72.32	98.03	114.89	167.90	99	450	450	CONC	0.25	70.0	142.5531	0.8963	1.3016	0.697		
	14	15	0.35	0.65	0.63	2.01			0.00	0.00			0.00	0.00			0.00	0.00	12.55	68.23	92.41	108.27	158.19	137	525	525	CONC	0.20	64.5	192.3297	0.8885	1.2100	0.712		
	15	16	0.34	0.65	0.61	2.62			0.00	0.00			0.00	0.00			0.00	0.00	13.76	64.86	87.79	102.83	150.20	170	600	600	CONC	0.15	60.5	237.8056	0.8411	1.1989	0.715		
	16	17	0.40	0.65	0.72	3.34			0.00	0.00			0.00	0.00			0.00	0.00	14.96	61.87	83.69	98.01	143.13	207	600	600	CONC	0.20	68.0	274.5943	0.9712	1.1670	0.753		
	17	18	0.13	0.65	0.23	3.58			0.00	0.00			0.00	0.00			0.00	0.00	16.13	59.23	80.09	93.77	136.91	212	600	600	CONC	0.20	16.0	274.5943	0.9712	0.2746	0.772		
	18	19	0.21	0.65	0.38	3.96			0.00	0.00			0.00	0.00			0.00	0.00	16.40	58.65	79.29	92.83	135.53	232	675	675	CONC	0.15	54.5	325.5584	0.9098	0.9984	0.713		
To Unknown Road3 - 03, Pipe 19 - 29					3.96				0.00				0.00				0.00		17.40																
<b>Unknown Road11 - 11</b>																																			
	1500	6	0.08	0.65	0.14	0.14			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	11	300	300	PVC	0.35	59.5	57.2089	0.8093	1.2253	0.194		
To Unknown Road3 - 03, Pipe 6 - 7					0.14				0.00				0.00				0.00		11.23																
<b>Unknown Road1 - 01</b>																																			
Contribution From Unknown Road3 - 03, Pipe 19 - 29						9.40				0.00				0.00				0.00	19.35																
Contribution From Unknown Road2 - 02, Pipe 26 - 29						4.50				0.00				0.00				0.00	17.31																
Contribution From Unknown Road2 - 02, Pipe 28 - 29						1.59				0.00				0.00				0.00	13.34																
	29	30	0.01	0.65	0.02	15.50			0.00	0.00			0.00	0.00			0.00	0.00	19.35	53.10	71.71	83.93	122.47	823	825	825	CONC	0.55	27.0	#####	1.9914	0.2260	0.773		
<b>Unknown Road17 - 18</b>																																			
	3200	38	0.34	0.65	0.61	0.61			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	47	300	300	PVC	0.40	86.5	61.1589	0.8652	1.6662	0.772		
	38	40	0.36	0.65	0.65	1.26			0.00	0.00			0.00	0.00			0.00	0.00	11.67	70.95	96.15	112.66	164.64	90	450	450	CONC	0.20	86.5	127.5033	0.8017	1.7983	0.704		
Contribution From Unknown Road22 - 23, Pipe 39 - 40						0.05				0.00				0.00			0.00	10.50																	
	40	41	0.23	0.65	0.42	1.73			0.00	0.00			0.00	0.00			0.00	0.00	13.46	65.65	88.87	104.10	152.07	114	525	525	CONC	0.20	61.5	192.3297	0.8885	1.1537	0.592		
	41	43	0.23	0.65	0.42	2.15			0.00	0.00			0.00	0.00			0.00	0.00	14.62	62.68	84.81	99.33	145.06	135	525	525	CONC	0.20	61.5	192.3297	0.8885	1.1537	0.701		
To Unknown Road14 - 14, Pipe 43 - 44					2.15				0.00				0.00				0.00		15.77																
<b>Unknown Road9 - 09</b>																																			
Contribution From Unknown Road3 - 03, Pipe 48 - 50						7.84				0.00				0.00			0.00	19.39																	
Contribution From Unknown Road3 - 03, Pipe 49 - 50						1.32				0.00				0.00			0.00	12.51																	
	50	51	0.01	0.65	0.02	9.18			0.00	0.00			0.00	0.00			0.00	0.00	19.39	53.03	71.61	83.81	122.29	487	900	900	CONC	0.15	13.0	701.1305	1.1021	0.1966	0.694		
	51	52	0.03	0.65	0.05	9.23			0.00	0.00			0.00	0.00			0.00	0.00	19.39	53.03	71.61	83.81	122.29	487	900	900	CONC	0.15	13.0	701.1305	1.1021	0.1966	0.694		
	51	52			0.00	9.23	2.91	0.40	3.24	3.24			0.00	0.00			0.00	0.00	19.59	52.70	71.16	83.28	121.52	717	975	975	CONC	0.20	55.0	#####	1.3424	0.6829	0.715		
To Unknown Road6 - 06, Pipe 52 - 54					9.23				3.24				0.00				0.00		20.27																



**STORM SEWER CALCULATION SHEET (RATIONAL METHOD)**

Local Roads Return Frequency = 2 years  
 Collector Roads Return Frequency = 5 years  
 Arterial Roads Return Frequency = 10 years



Manning 0.013

LOCATION		AREA (Ha)																FLOW										SEWER DATA									
		2 YEAR				5 YEAR				10 YEAR				100 YEAR				Time of	Intensity	Intensity	Intensity	Intensity	Peak Flow	DIA. (mm)	DIA. (mm)	TYPE	SLOPE	LENGTH	CAPACITY	VELOCITY	TIME OF	RATIO					
Location	From Node	To Node	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	Conc. (min)	2 Year (mm/h)	5 Year (mm/h)	10 Year (mm/h)	100 Year (mm/h)	Q (l/s)	(actual)	(nominal)	(%)	(m)	(l/s)	(m/s)	LOW (min)	Q/Q full					
	59	60	0.15	0.65	0.27	1.59			0.00	0.00			0.00	0.00			0.00	0.00	12.61	68.05	92.16	107.97	157.75	108	450	450	CONC	0.25	12.5	142.5531	0.8963	0.2324	0.759				
	60	61	0.07	0.65	0.13	1.72			0.00	0.00			0.00	0.00			0.00	0.00	12.84	67.37	91.24	106.89	156.16	116	450	450	CONC	0.30	19.0	156.1591	0.9819	0.3225	0.741				
To Unknown Road7 - 07, Pipe 61 - 62						1.72				0.00	0.00			0.00	0.00			0.00	0.00	13.17																	
Contribution From Unknown Road6 - 06, Pipe 52 - 54						9.41				3.24	0.00			0.00	0.00			0.00	0.00	20.68																	
Contribution From Unknown Road6 - 06, Pipe 53 - 54						0.22				0.00	0.00			0.00	0.00			0.00	0.00	10.57																	
	54	55	0.50	0.65	0.90	10.53			0.00	3.24			0.00	0.00			0.00	0.00	20.68	50.96	68.79	80.49	117.43	759	1050	1050	CONC	0.15	90.0	#####	1.2214	1.2281	0.718				
	55	56	0.10	0.65	0.18	10.72			0.00	3.24			0.00	0.00			0.00	0.00	21.91	49.15	66.32	77.59	113.18	741	1050	1050	CONC	0.15	11.0	#####	1.2214	0.1501	0.701				
	56	61	0.09	0.65	0.16	10.88			0.00	3.24			0.00	0.00			0.00	0.00	22.06	48.94	66.03	77.25	112.68	746	1050	1050	CONC	0.15	25.5	#####	1.2214	0.3480	0.705				
To Unknown Road7 - 07, Pipe 61 - 62						10.88				3.24	0.00			0.00	0.00			0.00	0.00	22.41																	
<b>Unknown Road7 - 07</b>																																					
Contribution From Unknown Road5 - 05, Pipe 56 - 61						10.88				3.24	0.00			0.00	0.00			0.00	0.00	22.41																	
Contribution From Unknown Road5 - 05, Pipe 60 - 61						1.72				0.00	0.00			0.00	0.00			0.00	0.00	13.17																	
	61	62	0.01	0.65	0.02	12.61			0.00	3.24			0.00	0.00			0.00	0.00	22.41	48.45	65.37	76.48	111.55	823	1050	1050	CONC	0.15	26.5	#####	1.2214	0.3616	0.778				
<b>Unknown Road8 - 08</b>																																					
Contribution From Unknown Road10 - 10, Pipe 81 - 82						1.66				0.00	0.00			0.00	0.00			0.00	0.00	13.23																	
	82	83	0.05	0.65	0.09	1.75			0.00	0.00			0.00	0.00			0.00	0.00	13.23	66.28	89.75	105.13	153.58	116	450	450	CONC	0.30	13.5	156.1591	0.9819	0.2292	0.744				
To Unknown Road12 - 12, Pipe 83 - 84						1.75				0.00	0.00			0.00	0.00			0.00	0.00	13.46																	
<b>Unknown Road20 - 21</b>																																					
	6400	69	0.34	0.65	0.61	0.61			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	47	300	300	PVC	0.40	90.5	61.1589	0.8652	1.7433	0.772				
	69	70	0.38	0.65	0.69	1.30			0.00	0.00			0.00	0.00			0.00	0.00	11.74	70.70	95.81	112.27	164.05	92	450	450	CONC	0.20	90.5	127.5033	0.8017	1.8814	0.721				
Contribution From Unknown Road22 - 23, Pipe 39 - 70						0.04				0.00	0.00			0.00	0.00			0.00	0.00	10.24																	
	70	71	0.23	0.65	0.42	1.75			0.00	0.00			0.00	0.00			0.00	0.00	13.62	65.22	88.28	103.41	151.05	114	525	525	CONC	0.20	61.5	192.3297	0.8885	1.1537	0.594				
	71	72	0.23	0.65	0.42	2.17			0.00	0.00			0.00	0.00			0.00	0.00	14.78	62.30	84.28	98.70	144.14	135	525	525	CONC	0.20	61.5	192.3297	0.8885	1.1537	0.702				
To Unknown Road14 - 14, Pipe 72 - 73						2.17				0.00	0.00			0.00	0.00			0.00	0.00	15.93																	
<b>Unknown Road22 - 23</b>																																					
	39	70	0.02	0.65	0.04	0.04			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	3	300	300	PVC	0.95	19.5	94.2522	1.3334	0.2437	0.029				
To Unknown Road20 - 21, Pipe 70 - 71						0.04				0.00	0.00			0.00	0.00			0.00	0.00	10.24																	
	39	40	0.03	0.65	0.05	0.05			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	4	300	300	PVC	0.35	24.5	57.2089	0.8093	0.5045	0.073				
To Unknown Road17 - 18, Pipe 40 - 41						0.05				0.00	0.00			0.00	0.00			0.00	0.00	10.50																	
	4000	36	0.06	0.65	0.11	0.11			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	8	300	300	PVC	0.35	44.5	57.2089	0.8093	0.9164	0.146				
To Unknown Road15 - 16, Pipe 36 - 37						0.11				0.00	0.00			0.00	0.00			0.00	0.00	10.92																	
	7000	67	0.06	0.65	0.11	0.11			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	8	300	300	PVC	0.35	43.5	57.2089	0.8093	0.8958	0.146				
To Unknown Road16 - 17, Pipe 67 - 68						0.11				0.00	0.00			0.00	0.00			0.00	0.00	10.90																	
Contribution From Unknown Road15 - 16, Pipe 89 - 90						1.01				0.70	0.00			0.00	0.00			0.00	0.00	12.90																	
	90	67	0.53	0.65	0.96	1.97			0.00	0.70			0.00	0.00			0.00	0.00	12.90	67.23	91.04	106.65	155.81	196	675	675	CONC	0.15	108.5	325.5584	0.9098	1.9877	0.603				
To Unknown Road16 - 17, Pipe 67 - 68						1.97				0.70	0.00			0.00	0.00			0.00	0.00	14.88																	
<b>Unknown Road6 - 06</b>																																					
	5200	57	0.12	0.65	0.22	0.22			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	17	300	300	PVC	0.35	34.0	57.2089	0.8093	0.7002	0.291				
To Unknown Road5 - 05, Pipe 57 - 58						0.22				0.00	0.00			0.00	0.00			0.00	0.00	10.70																	
	53	80	0.09	0.65	0.16	0.16			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	12	300	300	PVC	0.70	25.5	80.9057	1.1446	0.3713	0.154				
To Unknown Road10 - 10, Pipe 80 - 81						0.16				0.00	0.00			0.00	0.00			0.00	0.00	10.37																	
	53	54	0.12	0.65	0.22	0.22			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	17	300	300	PVC	0.35	27.5	57.2089	0.8093	0.5663	0.291				
To Unknown Road5 - 05, Pipe 54 - 55						0.22				0.00	0.00			0.00	0.00			0.00	0.00	10.57																	
	7700	80	0.25	0.65	0.45	0.45			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	35	300	300	PVC	0.35	64.0								

**STORM SEWER CALCULATION SHEET (RATIONAL METHOD)**

Local Roads Return Frequency = 2 years  
 Collector Roads Return Frequency = 5 years  
 Arterial Roads Return Frequency = 10 years



Manning 0.013

LOCATION		AREA (Ha)																FLOW										SEWER DATA							
		2 YEAR				5 YEAR				10 YEAR				100 YEAR				Time of Conc.	Intensity 2 Year	Intensity 5 Year	Intensity 10 Year	Intensity 100 Year	Peak Flow	DIA. (mm) (actual)	DIA. (mm) (nominal)	TYPE	SLOPE (%)	LENGTH (m)	CAPACITY (l/s)	VELOCITY (m/s)	TIME OF LOW (min)	RATIO Q/Q full			
Location	From Node	To Node	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	(min)	(mm/h)	(mm/h)	(mm/h)	(mm/h)	Q (l/s)											
	8	57	0.09	0.65	0.16	0.16							0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	12	300	300	PVC	1.40	25.0	114.4179	1.6187	0.2574	0.109		
To Unknown Road5 - 05, Pipe 57 - 58						0.16													10.26																
	8	9	0.12	0.65	0.22	0.22							0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	17	300	300	PVC	0.35	28.5	57.2089	0.8093	0.5869	0.291		
	9	10	0.21	0.65	0.38	0.60							0.00	0.00			0.00	0.00	10.59	74.62	101.19	118.61	173.37	44	300	300	PVC	0.40	59.0	61.1589	0.8652	1.1365	0.728		
To Unknown Road3 - 03, Pipe 10 - 19						0.60													0.00	11.72															
Contribution From Unknown Road16 - 17, Pipe 75 - 76						9.92													0.00	18.71															
	76	77	0.20	0.65	0.36	10.28							0.00	1.19			0.00	0.00	18.71	54.21	73.22	85.70	125.07	644	975	975	CONC	0.15	57.0	867.9562	1.1625	0.8172	0.742		
To Unknown Road10 - 10, Pipe 77 - 78						10.28													0.00	19.52															
Contribution From Unknown Road9 - 09, Pipe 51 - 52						9.23													0.00	20.27															
	52	54	0.10	0.65	0.18	9.41							0.00	3.24			0.00	0.00	20.27	51.60	69.66	81.51	118.93	711	1050	1050	CONC	0.15	30.0	#####	1.2214	0.4094	0.672		
To Unknown Road5 - 05, Pipe 54 - 55						9.41													0.00	20.68															
<b>Unknown Road10 - 10</b>																																			
Contribution From Unknown Road6 - 06, Pipe 53 - 80						0.16													0.00	10.37															
Contribution From Unknown Road6 - 06, Pipe 7700 - 80						0.45													0.00	11.32															
	80	81	0.43	0.65	0.78	1.39							0.00	0.00			0.00	0.00	11.32	72.09	97.71	114.51	167.35	100	450	450	CONC	0.20	79.5	127.5033	0.8017	1.6528	0.787		
	81	82	0.15	0.65	0.27	1.66							0.00	0.00			0.00	0.00	12.97	67.01	90.74	106.31	155.30	111	450	450	CONC	0.25	14.0	142.5531	0.8963	0.2603	0.781		
To Unknown Road8 - 08, Pipe 82 - 83						1.66													0.00	13.23															
Contribution From Unknown Road6 - 06, Pipe 76 - 77						10.28													0.00	19.52															
	77	78	0.43	0.65	0.78	11.06							0.00	1.19			0.00	0.00	19.52	52.81	71.31	83.46	121.78	669	975	975	CONC	0.15	78.0	867.9562	1.1625	1.1183	0.770		
	78	79	0.12	0.65	0.22	11.28							0.00	0.00			0.00	0.00	20.64	51.02	68.87	80.59	117.57	657	975	975	CONC	0.15	12.5	867.9562	1.1625	0.1792	0.757		
	79	83	0.11	0.65	0.20	11.47							0.00	1.19			0.00	0.00	20.82	50.75	68.50	80.15	116.93	664	975	975	CONC	0.15	31.0	867.9562	1.1625	0.4444	0.765		
To Unknown Road12 - 12, Pipe 83 - 84						11.47													0.00	21.27															
<b>Unknown Road12 - 12</b>																																			
Contribution From Unknown Road10 - 10, Pipe 79 - 83						11.47							1.19						0.00	21.27															
Contribution From Unknown Road8 - 08, Pipe 82 - 83						1.75													0.00	13.46															
	83	84	0.01	0.65	0.02	13.25							0.00	1.19			0.00	0.00	21.27	50.08	67.59	79.08	115.36	744	975	975	CONC	0.20	26.5	#####	1.3424	0.3290	0.742		
<b>Unknown Road25 - 26</b>																																			
Contribution From Unknown Road3 - 03, Pipe 10200 - 111						0.00								0.02					0.00	10.28															
	111	112	0.15	0.65	0.27	0.27							0.00	0.02			0.00	0.00	10.28	75.75	102.75	120.44	176.06	22	300	300	PVC	0.35	55.0	57.2089	0.8093	1.1326	0.391		
	112	115	0.15	0.65	0.27	0.54							0.00	0.02			0.00	0.00	11.41	71.78	97.29	114.01	166.62	41	375	375	PVC	0.30	57.0	96.0323	0.8695	1.0926	0.424		
To Unknown Road21 - 22, Pipe 115 - 116						0.54								0.02					0.00	12.50															
<b>Unknown Road23 - 24</b>																																			
Contribution From Unknown Road3 - 03, Pipe 11100 - 110						0.00								0.34					0.00	10.90															
	110	114	0.39	0.65	0.70	0.70							0.00	0.34			0.00	0.00	10.90	73.53	99.69	116.84	170.76	86	450	450	CONC	0.20	99.5	127.5033	0.8017	2.0685	0.675		
To Unknown Road21 - 22, Pipe 114 - 115						0.70								0.34					0.00	12.96															
<b>Unknown Road26 - 27</b>																																			
	11200	105	0.50	0.65	0.90	0.90							0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	69	450	450	CONC	0.20	98.5	127.5033	0.8017	2.0478	0.544		
To Unknown Road21 - 22, Pipe 105 - 106						0.90								0.00	0.00				0.00	12.05															
<b>Unknown Road24 - 25</b>																																			
	91	68	0.41	0.65	0.74	0.74							0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	57	375	375	PVC	0.30	79.5	96.0323	0.8695	1.5239	0.593		
To Unknown Road16 - 17, Pipe 68 - 73						0.74								0.00	0.00				0.00	11.52															
	91	92	0.12	0.65	0.22	0.22							0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	17	300	300	PVC	0.35	30.5	57.2089	0.8093	0.6281	0.291		
To Unknown Road15 - 16, Pipe 92 - 94						0.22								0.00	0.00				0.00	10.63															
<b>Unknown Road15 - 16</b>																																			
	31	64	0.06	0.65	0.11	0.11							0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	8	300	300	PVC	1.35	9.0	112.3561	1.5895	0.0944	0.074		
	64	65	0.19	0.65	0.34	0.45							0.00	0.00			0.00	0.00	10.09	76.44	103.70	121.56	177.70	35	300	300	PVC	0.35	50.0	57.2089	0.8093	1.0296	0.604		
To Unknown Road16 - 17, Pipe 65 - 66						0.45								0.00																					

**STORM SEWER CALCULATION SHEET (RATIONAL METHOD)**

Local Roads Return Frequency = 2 years  
 Collector Roads Return Frequency = 5 years  
 Arterial Roads Return Frequency = 10 years



Manning 0.013

LOCATION		AREA (Ha)																FLOW										SEWER DATA								
		2 YEAR				5 YEAR				10 YEAR				100 YEAR				Time of	Intensity	Intensity	Intensity	Intensity	Peak Flow	DIA. (mm)	DIA. (mm)	TYPE	SLOPE	LENGTH	CAPACITY	VELOCITY	TIME OF	RATIO				
Location	From Node	To Node	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	Conc. (min)	2 Year (mm/h)	5 Year (mm/h)	10 Year (mm/h)	100 Year (mm/h)	Q (l/s)	(actual)	(nominal)	(%)	(m)	(l/s)	(m/s)	LOW (min)	Q/Q full				
	85	63	0.04	0.65	0.07	0.07			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	6	300	300	PVC	0.35	10.5	57.2089	0.8093	0.2162	0.097			
	63	65	0.24	0.65	0.43	0.51			0.00	0.00			0.00	0.00			0.00	0.00	10.22	75.98	103.06	120.81	176.61	38	300	300	PVC	0.35	67.0	57.2089	0.8093	1.3797	0.672			
To Unknown Road16 - 17, Pipe 65 - 66						0.51			0.00				0.00					0.00	11.60																	
	90000	92	0.22	0.65	0.40	0.40			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	31	300	300	PVC	0.35	58.5	57.2089	0.8093	1.2047	0.534			
Contribution From Unknown Road24 - 25, Pipe 91 - 92						0.22			0.00				0.00					0.00	10.63																	
	92	94	0.21	0.65	0.38	0.99			0.00	0.00			0.00	0.00			0.00	0.00	11.20	72.47	98.23	115.12	168.25	72	375	375	PVC	0.30	65.0	96.0323	0.8695	1.2459	0.750			
To Unknown Road14 - 14, Pipe 94 - 101						0.99			0.00				0.00					0.00	12.45																	
	85	86	0.20	0.65	0.36	0.36			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	28	300	300	PVC	0.35	50.0	57.2089	0.8093	1.0296	0.485			
	86	87	0.12	0.65	0.22	0.58			0.00	0.00			0.00	0.00			0.00	0.00	11.03	73.07	99.05	116.09	169.66	42	300	300	PVC	0.35	9.5	57.2089	0.8093	0.1956	0.739			
			0.11	0.65	0.20	0.78			0.00	0.00			0.00	0.00			0.00	0.00																		
	87	88			0.00	0.78	0.63	0.40	0.70	0.70			0.00	0.00			0.00	0.00	11.23	72.40	98.14	115.01	168.08	125	450	450	CONC	0.30	27.0	156.1591	0.9819	0.4583	0.801			
	88	89	0.02	0.65	0.04	0.81			0.00	0.70			0.00	0.00			0.00	0.00	11.68	70.89	96.07	112.57	164.51	125	450	450	CONC	0.30	13.0	156.1591	0.9819	0.2207	0.800			
	89	90	0.11	0.65	0.20	1.01			0.00	0.70			0.00	0.00			0.00	0.00	11.90	70.19	95.11	111.44	162.84	138	600	600	CONC	0.15	50.0	237.8056	0.8411	0.9908	0.579			
To Unknown Road22 - 23, Pipe 90 - 67						1.01			0.70				0.00					0.00	12.90																	
	31	32	0.16	0.65	0.29	0.29			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	22	300	300	PVC	0.35	37.0	57.2089	0.8093	0.7619	0.388			
	32	33	0.15	0.65	0.27	0.56			0.00	0.00			0.00	0.00			0.00	0.00	10.76	74.00	100.33	117.60	171.88	41	300	300	PVC	0.35	40.0	57.2089	0.8093	0.8237	0.725			
	33	34	0.03	0.65	0.05	0.61			0.00	0.00			0.00	0.00			0.00	0.00	11.59	71.21	96.50	113.08	165.26	44	300	300	PVC	0.35	10.5	57.2089	0.8093	0.2162	0.765			
	34	35	0.32	0.65	0.58	1.19			0.00	0.00			0.00	0.00			0.00	0.00	11.80	70.52	95.55	111.96	163.61	84	450	450	CONC	0.20	77.0	127.5033	0.8017	1.6008	0.660			
	35	36	0.39	0.65	0.70	1.90			0.00	0.00			0.00	0.00			0.00	0.00	13.40	65.81	89.10	104.37	152.46	125	600	600	CONC	0.15	77.0	237.8056	0.8411	1.5258	0.525			
Contribution From Unknown Road22 - 23, Pipe 4000 - 36						1.11			0.00				0.00					0.00	10.92																	
	36	37	0.30	0.65	0.54	2.55			0.00	0.00			0.00	0.00			0.00	0.00	14.93	61.94	83.79	98.12	143.29	158	600	600	CONC	0.15	61.5	237.8056	0.8411	1.2187	0.664			
	37	44	0.28	0.65	0.51	3.05			0.00	0.00			0.00	0.00			0.00	0.00	16.15	59.19	80.03	93.70	136.80	181	600	600	CONC	0.15	61.5	237.8056	0.8411	1.2187	0.760			
To Unknown Road14 - 14, Pipe 44 - 47						3.05			0.00				0.00					0.00	17.37																	
<b>Unknown Road14 - 14</b>																																				
	93	73	0.44	0.65	0.80	0.80			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	61	375	375	PVC	0.30	81.5	96.0323	0.8695	1.5622	0.636			
To Unknown Road16 - 17, Pipe 73 - 75						0.80			0.00				0.00					0.00	11.56																	
	93	94	0.15	0.65	0.27	0.27			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	21	300	300	PVC	1.20	28.5	105.9304	1.4986	0.3170	0.197			
Contribution From Unknown Road15 - 16, Pipe 92 - 94						0.99			0.00				0.00					0.00	12.45																	
	94	101	0.15	0.65	0.27	1.54			0.00	0.00			0.00	0.00			0.00	0.00	12.45	68.52	92.81	108.74	158.88	105	450	450	CONC	0.25	44.0	142.5531	0.8963	0.8182	0.738			
To Unknown Road27 - 28, Pipe 101 - 102						1.54			0.00				0.00					0.00	13.27																	
	42	72	0.09	0.65	0.16	0.16			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	12	300	300	PVC	0.85	22.0	89.1537	1.2613	0.2907	0.140			
Contribution From Unknown Road20 - 21, Pipe 71 - 72						2.17			0.00				0.00					0.00	15.93																	
	72	73	0.16	0.65	0.29	2.62			0.00	0.00			0.00	0.00			0.00	0.00	15.93	59.65	80.66	94.45	137.90	156	600	600	CONC	0.15	45.0	237.8056	0.8411	0.8917	0.657			
To Unknown Road16 - 17, Pipe 73 - 75						2.62			0.00				0.00					0.00	16.82																	
	95	96	0.19	0.65	0.34	0.34			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	26	300	300	PVC	0.35	44.5	57.2089	0.8093	0.9164	0.461			
	96	97	0.12	0.65	0.22	0.56			0.00	0.00			0.00	0.00			0.00	0.00	10.92	73.46	99.59	116.72	170.59	41	375	375	PVC	0.30	13.0	96.0323	0.8695	0.2492	0.428			
	97	98	0.40	0.65	0.72	1.28			0.00	0.00			0.00	0.00			0.00	0.00	11.17	72.60	98.41	115.34	168.56	93	450	450	CONC	0.20	64.0	127.5033	0.8017	1.3305	0.731			
	98	99	0.40	0.65	0.72	2.01			0.00	0.00			0.00	0.00			0.00	0.00	12.50	68.39	92.63	108.53	158.56	137	525	525	CONC	0.20	64.0	192.3297	0.8885	1.2006	0.713			
	99	100	0.13	0.65	0.23	2.24			0.00	0.00			0.00	0.00			0.00	0.00	13.70	65.03	88.02	103.10	150.60	146	525	525	CONC	0.20	13.0	192.3297	0.8885	0.2439	0.758			
	100	101	0.03	0.65	0.05	2.29			0.00	0.00			0.00	0.00			0.00	0.00	13.94	64.39	87.14	102.07	149.09	148	525	525	CONC	0.20	8.0	192.3297	0.8885	0.1501	0.768			
To Unknown Road27 - 28, Pipe 101 - 102						2.29			0.00				0.00					0.00	14.09																	
	42	43	0.08	0.65	0.14	0.14			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122														

**STORM SEWER CALCULATION SHEET (RATIONAL METHOD)**

Local Roads Return Frequency = 2 years  
 Collector Roads Return Frequency = 5 years  
 Arterial Roads Return Frequency = 10 years



Manning 0.013

LOCATION			AREA (Ha)																FLOW										SEWER DATA							
			2 YEAR				5 YEAR				10 YEAR				100 YEAR				Time of Conc.	Intensity 2 Year	Intensity 5 Year	Intensity 10 Year	Intensity 100 Year	Peak Flow	DIA. (mm) (actual)	DIA. (mm) (nominal)	TYPE	SLOPE (%)	LENGTH (m)	CAPACITY (l/s)	VELOCITY (m/s)	TIME OF LOW (min)	RATIO Q/Q full			
Location	From Node	To Node	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	(min)	(mm/h)	(mm/h)	(mm/h)	(mm/h)	Q (l/s)												
<b>Unknown Road27 - 28</b>																																				
Contribution From Unknown Road14 - 14, Pipe 100 - 101					2.29				0.00					0.00				0.00		14.09																
Contribution From Unknown Road14 - 14, Pipe 94 - 101					1.54				0.00					0.00				0.00		13.27																
	101	102	0.05	0.65	0.09	3.92			0.00	0.00			0.00	0.00			0.00	0.00	14.09	64.00	86.62	101.45	148.17	251	675	675	CONC	0.15	62.0	325.5584	0.9098	1.1358	0.771			
To Unknown Road3 - 03, Pipe 102 - 104						3.92				0.00				0.00				0.00		15.23																
<b>Unknown Road21 - 22</b>																																				
	11300	114	0.12	0.65	0.22	0.22			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	17	450	450	CONC	0.20	45.0	127.5033	0.8017	0.9355	0.131			
Contribution From Unknown Road23 - 24, Pipe 110 - 114					0.70				0.34					0.00				0.00		12.96																
	114	115	0.17	0.65	0.31	1.23			0.00	0.34			0.00	0.00			0.00	0.00	12.96	67.03	90.77	106.34	155.35	114	525	525	CONC	0.20	45.0	192.3297	0.8885	0.8442	0.590			
Contribution From Unknown Road25 - 26, Pipe 112 - 115					0.54				0.02					0.00				0.00		12.50																
	115	116	0.49	0.65	0.89	2.66			0.00	0.36			0.00	0.00			0.00	0.00	13.81	64.73	87.62	102.63	149.90	204	600	600	CONC	0.20	88.0	274.5943	0.9712	1.5102	0.741			
To Unknown Road28 - 29, Pipe 116 - 122						2.66				0.36				0.00				0.00		15.32																
Contribution From Unknown Road3 - 03, Pipe 102 - 104					3.92				0.89					0.00				0.00		16.65																
Contribution From Unknown Road3 - 03, Pipe 103 - 104					0.00				0.23					0.00				0.00		10.32																
	104	105	0.18	0.65	0.33	4.25			0.00	1.12			0.00	0.00			0.00	0.00	16.65	58.12	78.57	91.99	134.29	335	825	825	CONC	0.15	55.0	555.9418	1.0400	0.8814	0.602			
Contribution From Unknown Road26 - 27, Pipe 11200 - 105					0.90				0.00					0.00				0.00		12.05																
	105	106	0.21	0.65	0.38	5.53			0.00	1.12			0.00	0.00			0.00	0.00	17.53	56.37	76.17	89.17	130.16	397	825	825	CONC	0.15	51.5	555.9418	1.0400	0.8253	0.714			
	106	107	0.13	0.65	0.23	5.76			0.00	1.12			0.00	0.00			0.00	0.00	18.36	54.83	74.07	86.70	126.53	399	825	825	CONC	0.15	9.5	555.9418	1.0400	0.1522	0.718			
	107	116	0.03	0.65	0.05	5.82			0.00	1.12			0.00	0.00			0.00	0.00	18.51	54.56	73.70	86.26	125.89	400	825	825	CONC	0.15	6.0	555.9418	1.0400	0.0962	0.720			
To Unknown Road28 - 29, Pipe 116 - 122						5.82				1.12				0.00				0.00		18.61																
<b>Unknown Road28 - 29</b>																																				
Contribution From Unknown Road21 - 22, Pipe 107 - 116					5.82				1.12					0.00				0.00		18.61																
Contribution From Unknown Road21 - 22, Pipe 115 - 116					2.66				0.36					0.00				0.00		15.32																
	116	122	0.05	0.65	0.09	8.57			0.00	1.48			0.00	0.00			0.00	0.00	18.61	54.38	73.46	85.99	125.49	575	900	900	CONC	0.16	67.5	724.1245	1.1383	0.9884	0.794			
To Unknown Road16 - 17, Pipe 122 - 124						8.57				1.48				0.00				0.00		19.60																
<b>Unknown Road3 - 03</b>																																				
	10200	111			0.00	0.00	0.01	0.65	0.02	0.02			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	2	300	300	PVC	0.35	13.5	57.2089	0.8093	0.2780	0.033			
To Unknown Road25 - 26, Pipe 111 - 112						0.00				0.02				0.00				0.00		10.28																
	103	104			0.00	0.00	0.13	0.65	0.23	0.23			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	24	300	300	PVC	1.45	32.0	116.4431	1.6473	0.3238	0.210			
To Unknown Road21 - 22, Pipe 104 - 105						0.00				0.23				0.00				0.00		10.32																
	108	75			0.00	0.00	0.06	0.65	0.11	0.11			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	11	300	300	PVC	0.35	21.5	57.2089	0.8093	0.4427	0.197			
To Unknown Road16 - 17, Pipe 75 - 76						0.00				0.11				0.00				0.00		10.44																
	108	109			0.00	0.00	0.11	0.65	0.20	0.20			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	21	300	300	PVC	0.35	26.5	57.2089	0.8093	0.5457	0.362			
To Unknown Road19 - 20, Pipe 109 - 113						0.00				0.20				0.00				0.00		10.55																
	11000	109			0.00	0.00	0.17	0.65	0.31	0.31			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	32	375	375	PVC	0.30	43.5	96.0323	0.8695	0.8338	0.333			
To Unknown Road19 - 20, Pipe 109 - 113						0.00				0.31				0.00				0.00		10.83																
	11100	110			0.00	0.00	0.19	0.65	0.34	0.34			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	36	300	300	PVC	0.35	43.5	57.2089	0.8093	0.8958	0.625			
To Unknown Road23 - 24, Pipe 110 - 114						0.00				0.34				0.00				0.00		10.90																
	74	75	0.44	0.65	0.80	0.80			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	61	375	375	PVC	0.30	78.0	96.0323	0.8695	1.4951	0.636			
To Unknown Road16 - 17, Pipe 75 - 76						0.80				0.00				0.00				0.00		11.50																
	74	49	0.67	0.65	1.21	1.21			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	93	450	450	CONC	0.20	107.5	127.5033	0.8017	2.2349	0.729			
	49	50	0.06	0.65	0.11	1.32			0.00	0.00			0.00	0.00			0.00	0.00	12.23	69.17	93.70	109.79	160.42	91	450	450	CONC	0.20	13.0	127.5033	0.8017	0.2703	0.716			
To Unknown Road9 - 09, Pipe 50 - 51						1.32				0.00				0.00				0.00		12.51																
Contribution From Unknown Road27 - 28, Pipe 101 - 102						3.92				0.00				0.00				0.00		15.23																
	102	104			0.00	3.92	0.49	0.65	0.89	0.89			0.00	0.00			0.00	0.00	15.23	61.24	82.83	97.00	141.64	313	750	750	CONC	0.15	83.5	431.1703	0.9760	1.4259	0.727			
To Unknown Road21 - 22, Pipe 104 - 105						3.92				0.89				0.00				0.00		16.65																

<p>Definitions:                  Q = 2.78 AIR, where                  Q = Peak Flow in Litres per second (L/s)                  A = Areas in hectares (ha)                  I = Rainfall Intensity (mm/h)                  R = Runoff Coefficient</p>	<p>Notes:                  1) Ottawa Rainfall-Intensity Curve                  2) Min. Velocity = 0.80 m/s</p>	<p>Designed:</p> <p>Checked:</p> <p>Dwg. Reference:</p>	<p>PROJECT:</p> <p>LOCATION:</p> <p style="text-align: center;"><b>City of Ottawa</b></p> <p>Date: 14 Oct 2021</p> <p>Sheet No. SHEET 5 OF 7</p>
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**STORM SEWER CALCULATION SHEET (RATIONAL METHOD)**

Local Roads Return Frequency = 2 years  
 Collector Roads Return Frequency = 5 years  
 Arterial Roads Return Frequency = 10 years

Manning 0.013



LOCATION		AREA (Ha)																FLOW										SEWER DATA								
		2 YEAR				5 YEAR				10 YEAR				100 YEAR				Time of	Intensity	Intensity	Intensity	Intensity	Peak Flow	DIA. (mm)	DIA. (mm)	TYPE	SLOPE	LENGTH	CAPACITY	VELOCITY	TIME OF	RATIO				
Location	From Node	To Node	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	Conc. (min)	2 Year (mm/h)	5 Year (mm/h)	10 Year (mm/h)	100 Year (mm/h)	Q (l/s)	(actual)	(nominal)	(%)	(m)	(l/s)	(m/s)	LOW (min)	Q/Q full				
	1	2	0.30	0.65	0.54	0.54			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	42	300	300	PVC	0.35	73.0	57.2089	0.8093	1.5033	0.728			
	2	3	0.26	0.65	0.47	1.01			0.00	0.00			0.00	0.00			0.00	0.00	11.50	71.48	96.87	113.52	165.89	72	375	375	PVC	0.30	67.0	96.0323	0.8695	1.2843	0.753			
	3	4	0.12	0.65	0.22	1.23			0.00	0.00			0.00	0.00			0.00	0.00	12.79	67.54	91.46	107.15	156.54	83	375	375	PVC	0.40	10.0	110.8885	1.0040	0.1660	0.748			
	4	5	0.44	0.65	0.80	2.02			0.00	0.00			0.00	0.00			0.00	0.00	12.95	67.06	90.81	106.38	155.42	136	525	525	CONC	0.20	73.0	192.3297	0.8885	1.3694	0.706			
	5	6	0.46	0.65	0.83	2.86			0.00	0.00			0.00	0.00			0.00	0.00	14.32	63.41	85.81	100.50	146.78	181	600	600	CONC	0.15	82.0	237.8056	0.8411	1.6249	0.761			
Contribution From Unknown Road11 - 11, Pipe 1500 - 6						0.14				0.00				0.00				0.00	11.23																	
	6	7	0.30	0.65	0.54	3.54			0.00	0.00			0.00	0.00			0.00	0.00	15.95	59.62	80.61	94.39	137.82	211	600	600	CONC	0.20	54.0	274.5943	0.9712	0.9267	0.769			
	7	10	0.25	0.65	0.45	3.99			0.00	0.00			0.00	0.00			0.00	0.00	16.87	57.67	77.95	91.26	133.22	230	675	675	CONC	0.15	54.5	325.5584	0.9098	0.9984	0.707			
Contribution From Unknown Road6 - 06, Pipe 9 - 10						0.60				0.00				0.00				0.00	11.72																	
	10	19	0.26	0.65	0.47	5.06			0.00	0.00			0.00	0.00			0.00	0.00	17.87	55.72	75.29	88.14	128.64	282	675	675	CONC	0.20	48.0	375.9224	1.0505	0.7615	0.750			
Contribution From Unknown Road2 - 02, Pipe 18 - 19						3.96				0.00				0.00				0.00	17.40																	
	19	29	0.21	0.65	0.38	9.40			0.00	0.00			0.00	0.00			0.00	0.00	18.63	54.34	73.40	85.91	125.37	511	750	750	CONC	0.35	64.0	658.6236	1.4908	0.7155	0.775			
To Unknown Road1 - 01, Pipe 29 - 30						9.40				0.00				0.00				0.00	19.35																	
	1	45	0.22	0.65	0.40	0.40			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	31	300	300	PVC	0.35	13.0	57.2089	0.8093	0.2677	0.534			
	45	46	0.36	0.65	0.65	1.05			0.00	0.00			0.00	0.00			0.00	0.00	10.27	75.79	102.80	120.50	176.15	79	450	450	CONC	0.20	88.0	127.5033	0.8017	1.8295	0.623			
	46	47	0.32	0.65	0.58	1.63			0.00	0.00			0.00	0.00			0.00	0.00	12.10	69.59	94.28	110.47	161.42	113	525	525	CONC	0.20	88.0	192.3297	0.8885	1.6508	0.588			
Contribution From Unknown Road14 - 14, Pipe 44 - 47						6.04				0.00				0.00				0.00	18.42																	
	47	48	0.08	0.65	0.14	7.81			0.00	0.00			0.00	0.00			0.00	0.00	18.42	54.71	73.91	86.51	126.25	427	825	825	CONC	0.15	48.0	555.9418	1.0400	0.7692	0.768			
	48	50	0.02	0.65	0.04	7.84			0.00	0.00			0.00	0.00			0.00	0.00	19.19	53.37	72.07	84.35	123.09	419	825	825	CONC	0.15	12.5	555.9418	1.0400	0.2003	0.753			
To Unknown Road9 - 09, Pipe 50 - 51						7.84				0.00				0.00				0.00	19.39																	
<b>Unknown Road19 - 20</b>																																				
Contribution From Unknown Road3 - 03, Pipe 108 - 109						0.00				0.20				0.00				0.00	10.55																	
Contribution From Unknown Road3 - 03, Pipe 11000 - 109						0.00				0.31				0.00				0.00	10.83																	
	109	113	0.36	0.65	0.65	0.65			0.00	0.51			0.00	0.00			0.00	0.00	10.83	73.75	99.99	117.19	171.28	99	450	450	CONC	0.20	88.5	127.5033	0.8017	1.8399	0.773			
	113	120	0.17	0.65	0.31	0.96			0.00	0.51			0.00	0.00			0.00	0.00	12.67	67.87	91.91	107.68	157.32	112	600	600	CONC	0.15	68.5	237.8056	0.8411	1.3574	0.469			
To Unknown Road16 - 17, Pipe 120 - 121						0.96				0.51				0.00				0.00	14.03																	
<b>Unknown Road16 - 17</b>																																				
	123	124			0.00	0.00	0.12	0.65	0.22	0.22			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	23	300	300	PVC	1.25	27.0	108.1147	1.5295	0.2942	0.209			
To Unknown Road29 - 30, Pipe 124 - 125						0.00				0.22				0.00				0.00	10.29																	
Contribution From Unknown Road15 - 16, Pipe 63 - 65						0.51				0.00				0.00				0.00	11.60																	
Contribution From Unknown Road15 - 16, Pipe 64 - 65						0.45				0.00				0.00				0.00	11.12																	
	65	66	0.28	0.65	0.51	1.46			0.00	0.00			0.00	0.00			0.00	0.00	11.60	71.18	96.46	113.03	165.18	104	450	450	CONC	0.25	68.5	142.5531	0.8963	1.2737	0.731			
	66	67	0.38	0.65	0.69	2.15			0.00	0.00			0.00	0.00			0.00	0.00	12.87	67.30	91.14	106.77	155.98	145	525	525	CONC	0.20	88.0	192.3297	0.8885	1.6508	0.752			
Contribution From Unknown Road22 - 23, Pipe 7000 - 67						0.11				0.00				0.00				0.00	10.90																	
Contribution From Unknown Road22 - 23, Pipe 90 - 67						1.97				0.70				0.00				0.00	14.88																	
	67	68	0.15	0.65	0.27	4.50			0.00	0.70			0.00	0.00			0.00	0.00	14.88	62.05	83.94	98.30	143.55	338	750	750	CONC	0.15	58.5	431.1703	0.9760	0.9990	0.784			
Contribution From Unknown Road24 - 25, Pipe 91 - 68						0.74				0.00				0.00				0.00	11.52																	
	68	73	0.16	0.65	0.29	5.53			0.00	0.70			0.00	0.00			0.00	0.00	15.88	59.76	80.81	94.62	138.16	387	825	825	CONC	0.15	64.5	555.9418	1.0400	1.0337	0.696			
Contribution From Unknown Road14 - 14, Pipe 72 - 73						2.62				0.00				0.00				0.00	16.82																	
Contribution From Unknown Road14 - 14, Pipe 93 - 73						0.80				0.00				0.00				0.00	11.56																	
	73	75	0.10	0.65	0.18	9.13			0.00	0.70			0.00	0.00			0.00	0.00	16.92	57.59	77.84	91.13	133.03	580	975	975	CONC	0.15	63.0	867.9562	1.1625	0.9032	0.668			
Contribution From Unknown Road3 - 03, Pipe 108 - 75						0.00				0.11				0.00	0.00			0.00	10.44																	
Contribution From Unknown Road3 - 03, Pipe 74 - 75						0.80				0.00				0.00	0.00																					



# Attachment B

PCSWMM Model Input Files

[TITLE]  
;;Project Title/Notes

[OPTIONS]  
;;Option Value  
FLOW\_UNITS LPS  
INFILTRATION HORTON  
FLOW\_ROUTING DYNWAVE  
LINK\_OFFSETS ELEVATION  
MIN\_SLOPE 0  
ALLOW\_PONDING NO  
SKIP\_STEADY\_STATE NO  
  
START\_DATE 10/13/2021  
START\_TIME 00:00:00  
REPORT\_START\_DATE 10/13/2021  
REPORT\_START\_TIME 00:00:00  
END\_DATE 10/14/2021  
END\_TIME 00:00:00  
SWEEP\_START 01/01  
SWEEP\_END 12/31  
DRY\_DAYS 0  
REPORT\_STEP 00:01:00  
WET\_STEP 00:05:00  
DRY\_STEP 00:05:00  
ROUTING\_STEP 5  
RULE\_STEP 00:00:00  
  
INERTIAL\_DAMPING PARTIAL  
NORMAL\_FLOW\_LIMITED BOTH  
FORCE\_MAIN\_EQUATION H-W  
VARIABLE\_STEP 0.75  
LENGTHENING\_STEP 0  
MIN\_SURFAREA 0  
MAX\_TRIALS 8  
HEAD\_TOLERANCE 0.0015  
SYS\_FLOW\_TOL 5  
LAT\_FLOW\_TOL 5  
MINIMUM\_STEP 0.5  
THREADS 6

[FILES]  
;;Interfacing Files  
USE HOTSTART "C:\OneDrive\J.F. Sabourin and Associates Inc\JFSA-OTTAWA-SERVER - Documents\PROJ\1474(03)\202110-BCDC Phase 3 - Detailed Design\Design\PCSWMM\202110-BCDC-Phase 3-Storm Sewer HGL\HotStart\BCDC-P3\_HGL\_v01-5YrDev-100YrJock.HSF"

[EVAPORATION]  
;;Data Source Parameters  
;;-----  
CONSTANT 0.0  
DRY\_ONLY NO



## [JUNCTIONS]

;;Name	Elevation	MaxDepth	InitDepth	SurDepth	Aponded
;;-----	-----	-----	-----	-----	-----
MH-1	91.419	2.421	0	0	0
MH-10	90.62	2.6	0	0	0
MH-100	90.705	2.225	0	0	0
MH-101	90.539	2.381	0	0	0
MH-102	90.371	2.459	0	0	0
MH-10200	91.05	1.78	0	0	0
MH-103	91.16	2.08	0	0	0
MH-104	90.171	2.639	0	0	0
MH-105	90.068	2.662	0	0	0
MH-106	89.961	2.689	0	0	0
MH-107	89.887	2.743	0	0	0
MH-108	90.867	2.213	0	0	0
MH-109	90.726	1.954	0	0	0
MH-11	91.82	1.87	0	0	0
MH-110	90.718	2.032	0	0	0
MH-11000	90.932	1.808	0	0	0
MH-111	90.943	1.877	0	0	0
MH-11100	91.02	1.79	0	0	0
MH-112	90.675	2.095	0	0	0
MH-11200	90.64	2.12	0	0	0
MH-113	90.529	2.011	0	0	0
MH-11300	90.609	1.931	0	0	0
MH-114	90.444	2.156	0	0	0
MH-115	90.279	2.391	0	0	0
MH-116	89.803	2.817	0	0	0
MH-117	90.829	2.111	0	0	0
MH-118	90.578	1.942	0	0	0
MH-119	90.471	2.039	0	0	0
MH-12	91.666	1.994	0	0	0
MH-120	90.167	2.283	0	0	0
MH-121	89.966	2.604	0	0	0
MH-122	89.593	2.937	0	0	0
MH-123	90.591	2.279	0	0	0
MH-124	89.475	3.025	0	0	0
MH-125	89.403	3.047	0	0	0
MH-13	91.444	2.206	0	0	0
MH-14	91.194	2.346	0	0	0
MH-15	90.99	2.46	0	0	0
MH-1500	91.413	2.037	0	0	0
MH-16	90.879	2.481	0	0	0
MH-17	90.713	2.537	0	0	0
MH-18	90.606	2.624	0	0	0
MH-19	90.449	2.701	0	0	0
MH-2	91.69	2.04	0	0	0
MH-20	91.708	1.972	0	0	0
MH-21	91.432	2.148	0	0	0
MH-22	91.156	2.324	0	0	0
MH-23	90.927	2.463	0	0	0
MH-24	90.733	2.527	0	0	0
MH-25	90.599	2.601	0	0	0
MH-26	90.426	2.714	0	0	0

MH-27	90.706	2.444	0	0	0
MH-28	90.651	2.479	0	0	0
MH-29	90.15	2.9	0	0	0
MH-3	91.459	2.171	0	0	0
MH-31	91.776	2.004	0	0	0
MH-32	91.815	1.945	0	0	0
MH-3200	91.967	1.803	0	0	0
MH-33	91.645	2.065	0	0	0
MH-34	91.458	2.232	0	0	0
MH-35	91.154	2.426	0	0	0
MH-36	91.018	2.442	0	0	0
MH-37	90.906	2.464	0	0	0
MH-38	91.471	2.189	0	0	0
MH-39	91.436	2.124	0	0	0
MH-4	91.269	2.351	0	0	0
MH-40	91.223	2.307	0	0	0
MH-4000	91.474	2.046	0	0	0
MH-41	91.08	2.36	0	0	0
MH-42	91.172	2.208	0	0	0
MH-43	90.882	2.468	0	0	0
MH-44	90.664	2.616	0	0	0
MH-45	91.223	2.277	0	0	0
MH-46	90.972	2.348	0	0	0
MH-47	90.496	2.694	0	0	0
MH-48	90.394	2.726	0	0	0
MH-49	90.776	2.344	0	0	0
MH-5	91.048	2.462	0	0	0
MH-50	90.3	2.79	0	0	0
MH-51	90.205	2.875	0	0	0
MH-52	90.02	2.98	0	0	0
MH-5200	90.889	2.111	0	0	0
MH-53	90.724	2.276	0	0	0
MH-54	89.915	3.035	0	0	0
MH-55	89.75	3.07	0	0	0
MH-56	89.703	3.107	0	0	0
MH-57	90.695	2.255	0	0	0
MH-58	90.483	2.397	0	0	0
MH-59	90.323	2.487	0	0	0
MH-6	90.905	2.475	0	0	0
MH-60	90.262	2.538	0	0	0
MH-61	89.605	3.165	0	0	0
MH-63	91.684	1.926	0	0	0
MH-64	91.624	2.036	0	0	0
MH-6400	91.794	1.796	0	0	0
MH-65	91.299	2.221	0	0	0
MH-66	91.053	2.367	0	0	0
MH-67	90.652	2.638	0	0	0
MH-68	90.489	2.711	0	0	0
MH-69	91.282	2.208	0	0	0
MH-7	90.722	2.578	0	0	0
MH-70	91.026	2.334	0	0	0
MH-7000	91.254	2.116	0	0	0
MH-71	90.883	2.377	0	0	0
MH-72	90.685	2.515	0	0	0

MH-73	90.242	2.868	0	0	0
MH-74	90.951	2.319	0	0	0
MH-75	90.117	2.893	0	0	0
MH-76	89.964	2.956	0	0	0
MH-77	89.818	3.002	0	0	0
MH-7700	90.769	2.061	0	0	0
MH-78	89.671	3.039	0	0	0
MH-79	89.622	3.068	0	0	0
MH-8	91.12	2.23	0	0	0
MH-80	90.395	2.405	0	0	0
MH-81	90.176	2.504	0	0	0
MH-82	90.081	2.579	0	0	0
MH-83	89.515	3.135	0	0	0
MH-85	91.751	1.879	0	0	0
MH-86	91.523	2.067	0	0	0
MH-87	91.34	2.23	0	0	0
MH-88	91.229	2.301	0	0	0
MH-89	91.04	2.48	0	0	0
MH-9	91.231	2.079	0	0	0
MH-90	90.89	2.56	0	0	0
MH-9000	90.942	2.358	0	0	0
MH-90000	91.424	2.026	0	0	0
MH-91	91.178	2.132	0	0	0
MH-92	91.144	1.946	0	0	0
MH-93	91.087	2.143	0	0	0
MH-94	90.874	2.106	0	0	0
MH-95	91.467	2.083	0	0	0
MH-96	91.236	1.914	0	0	0
MH-97	91.122	2.008	0	0	0
MH-98	90.919	2.121	0	0	0
MH-99	90.761	2.189	0	0	0

[OUTFALLS]

;;Name	Elevation	Type	Stage Data	Gated	Route To
;;-----	-----	-----	-----	-----	-----
;;Jock XS-6745					
MH-126	89.35	FIXED	91.9	NO	
;;Jock XS - 7657					
MH-30	90.001	FIXED	92.06	NO	
;;Jock XS -7441					
MH-62	89.565	FIXED	92.02	NO	
;;Jock XS -7441					
MH-84	89.462	FIXED	92.02	NO	

[CONDUITS]

;;Name	From Node	To Node	Length	Roughness
InOffset	OutOffset	InitFlow	MaxFlow	
;;-----	-----	-----	-----	-----
STM-100-101	MH-100	MH-101	8	0.013
90.705	90.689	0	0	
STM-101-102	MH-101	MH-102	62	0.013
90.539	90.446	0	0	

STM-10-19	MH-10	MH-19	48	0.013
90.62	90.524	0	0	
STM-10200-111	MH-10200	MH-111	13.5	0.013
91.05	91.003	0	0	
STM-102-104	MH-102	MH-104	83.5	0.013
90.371	90.246	0	0	
STM-103-104	MH-103	MH-104	32	0.013
91.16	90.696	0	0	
STM-104-105	MH-104	MH-105	55	0.013
90.171	90.088	0	0	
STM-105-106	MH-105	MH-106	51.5	0.013
90.068	89.991	0	0	
STM-106-107	MH-106	MH-107	9.5	0.013
89.961	89.947	0	0	
STM-107-116	MH-107	MH-116	6	0.013
89.887	89.878	0	0	
STM-108-109	MH-108	MH-109	26.5	0.013
90.969	90.876	0	0	
STM-108-75	MH-108	MH-75	21.5	0.013
90.867	90.792	0	0	
STM-109-113	MH-109	MH-113	88.5	0.013
90.726	90.549	0	0	
STM-11000-109	MH-11000	MH-109	43.5	0.013
90.932	90.801	0	0	
STM-110-114	MH-110	MH-114	99.5	0.013
90.718	90.519	0	0	
STM-11100-110	MH-11100	MH-110	43.5	0.013
91.02	90.868	0	0	
STM-111-112	MH-111	MH-112	55	0.013
90.943	90.75	0	0	
STM-11-12	MH-11	MH-12	46.5	0.013
91.889	91.726	0	0	
STM-11-20	MH-11	MH-20	10.5	0.013
91.82	91.783	0	0	
STM-11200-105	MH-11200	MH-105	98.5	0.013
90.64	90.443	0	0	
STM-112-115	MH-112	MH-115	57	0.013
90.675	90.504	0	0	
STM-11300-114	MH-11300	MH-114	45	0.013
90.609	90.519	0	0	
STM-113-120	MH-113	MH-120	68.5	0.013
90.399	90.296	0	0	
STM-114-115	MH-114	MH-115	45	0.013
90.444	90.354	0	0	
STM-115-116	MH-115	MH-116	88	0.013
90.279	90.103	0	0	
STM-116-122	MH-116	MH-122	67.5	0.013
89.803	89.695	0	0	
STM-117-118	MH-117	MH-118	73.5	0.013
90.643	90.496	0	0	
STM-118-119	MH-118	MH-119	10.5	0.013
90.421	90.4	0	0	
STM-119-120	MH-119	MH-120	39.5	0.013
90.325	90.266	0	0	

STM-1-2	MH-1	MH-2	73	0.013
92.021	91.765	0	0	
STM-120-121	MH-120	MH-121	84	0.013
90.116	89.99	0	0	
STM-121-122	MH-121	MH-122	98.5	0.013
89.915	89.767	0	0	
STM-12-13	MH-12	MH-13	16	0.013
91.666	91.594	0	0	
STM-122-124	MH-122	MH-124	17	0.013
89.617	89.578	0	0	
STM-123-124	MH-123	MH-124	27	0.013
90.591	90.253	0	0	
STM-124-125	MH-124	MH-125	34.5	0.013
89.503	89.437	0	0	
STM-125-126	MH-125	MH-126	35	0.013
89.403	89.35	0	0	
STM-13-14	MH-13	MH-14	70	0.013
91.444	91.269	0	0	
STM-14-15	MH-14	MH-15	64.5	0.013
91.194	91.065	0	0	
STM-1-45	MH-1	MH-45	13	0.013
91.419	91.373	0	0	
STM-1500-6	MH-1500	MH-6	59.5	0.013
91.413	91.205	0	0	
STM-15-16	MH-15	MH-16	60.5	0.013
90.99	90.899	0	0	
STM-16-17	MH-16	MH-17	68	0.013
90.879	90.743	0	0	
STM-17-18	MH-17	MH-18	16	0.013
90.713	90.681	0	0	
STM-18-19	MH-18	MH-19	54.5	0.013
90.606	90.524	0	0	
STM-19-29	MH-19	MH-29	64	0.013
90.449	90.225	0	0	
STM-20-21	MH-20	MH-21	67	0.013
91.708	91.507	0	0	
STM-21-22	MH-21	MH-22	67	0.013
91.432	91.231	0	0	
STM-22-23	MH-22	MH-23	61.5	0.013
91.156	91.002	0	0	
STM-2-3	MH-2	MH-3	67	0.013
91.69	91.489	0	0	
STM-23-24	MH-23	MH-24	82	0.013
90.927	90.763	0	0	
STM-24-25	MH-24	MH-25	41.5	0.013
90.733	90.629	0	0	
STM-25-26	MH-25	MH-26	39	0.013
90.599	90.501	0	0	
STM-26-29	MH-26	MH-29	63	0.013
90.426	90.3	0	0	
STM-27-28	MH-27	MH-28	12.5	0.013
90.706	90.681	0	0	
STM-28-29	MH-28	MH-29	50.5	0.013
90.651	90.525	0	0	



STM-29-30	MH-29	MH-30	27	0.013
90.15	90.001 0	0		
STM-31-32	MH-31	MH-32	37	0.013
91.965	91.835 0	0		
STM-31-64	MH-31	MH-64	9	0.013
91.776	91.654 0	0		
STM-3200-38	MH-3200	MH-38	86.5	0.013
91.967	91.621 0	0		
STM-32-33	MH-32	MH-33	40	0.013
91.815	91.675 0	0		
STM-33-34	MH-33	MH-34	10.5	0.013
91.645	91.608 0	0		
STM-3-4	MH-3	MH-4	10	0.013
91.459	91.419 0	0		
STM-34-35	MH-34	MH-35	77	0.013
91.458	91.304 0	0		
STM-35-36	MH-35	MH-36	77	0.013
91.154	91.038 0	0		
STM-36-37	MH-36	MH-37	61.5	0.013
91.018	90.926 0	0		
STM-37-44	MH-37	MH-44	61.5	0.013
90.906	90.814 0	0		
STM-38-40	MH-38	MH-40	86.5	0.013
91.471	91.298 0	0		
STM-39-40	MH-39	MH-40	24.5	0.013
91.534	91.448 0	0		
STM-39-70	MH-39	MH-70	19.5	0.013
91.436	91.251 0	0		
STM-4000-36	MH-4000	MH-36	44.5	0.013
91.474	91.318 0	0		
STM-40-41	MH-40	MH-41	61.5	0.013
91.223	91.1 0	0		
STM-41-43	MH-41	MH-43	61.5	0.013
91.08	90.957 0	0		
STM-42-43	MH-42	MH-43	22	0.013
91.259	91.182 0	0		
STM-42-72	MH-42	MH-72	22	0.013
91.172	90.985 0	0		
STM-43-44	MH-43	MH-44	45	0.013
90.882	90.814 0	0		
STM-44-47	MH-44	MH-47	62	0.013
90.664	90.571 0	0		
STM-4-5	MH-4	MH-5	73	0.013
91.269	91.123 0	0		
STM-45-46	MH-45	MH-46	88	0.013
91.223	91.047 0	0		
STM-46-47	MH-46	MH-47	88	0.013
90.972	90.796 0	0		
STM-47-48	MH-47	MH-48	48	0.013
90.496	90.424 0	0		
STM-48-50	MH-48	MH-50	12.5	0.013
90.394	90.375 0	0		
STM-49-50	MH-49	MH-50	13	0.013
90.776	90.75 0	0		

STM-50-51	MH-50	MH-51	13	0.013
90.3	90.28 0	0		
STM-51-52	MH-51	MH-52	55	0.013
90.205	90.095 0	0		
STM-5200-57	MH-5200	MH-57	34	0.013
90.889	90.77 0	0		
STM-52-54	MH-52	MH-54	30	0.013
90.02	89.975 0	0		
STM-53-54	MH-53	MH-54	27.5	0.013
90.761	90.665 0	0		
STM-53-80	MH-53	MH-80	25.5	0.013
90.724	90.545 0	0		
STM-54-55	MH-54	MH-55	90	0.013
89.915	89.78 0	0		
STM-55-56	MH-55	MH-56	11	0.013
89.75	89.733 0	0		
STM-5-6	MH-5	MH-6	82	0.013
91.048	90.925 0	0		
STM-56-61	MH-56	MH-61	25.5	0.013
89.703	89.665 0	0		
STM-57-58	MH-57	MH-58	45.5	0.013
90.695	90.558 0	0		
STM-58-59	MH-58	MH-59	50	0.013
90.483	90.383 0	0		
STM-59-60	MH-59	MH-60	12.5	0.013
90.323	90.292 0	0		
STM-60-61	MH-60	MH-61	19	0.013
90.262	90.205 0	0		
STM-61-62	MH-61	MH-62	26.5	0.013
89.605	89.565 0	0		
STM-63-65	MH-63	MH-65	67	0.013
91.684	91.449 0	0		
STM-6400-69	MH-6400	MH-69	90.5	0.013
91.794	91.432 0	0		
STM-64-65	MH-64	MH-65	50	0.013
91.624	91.449 0	0		
STM-65-66	MH-65	MH-66	68.5	0.013
91.299	91.128 0	0		
STM-66-67	MH-66	MH-67	88	0.013
91.053	90.877 0	0		
STM-6-7	MH-6	MH-7	54	0.013
90.905	90.797 0	0		
STM-67-68	MH-67	MH-68	58.5	0.013
90.652	90.564 0	0		
STM-68-73	MH-68	MH-73	64.5	0.013
90.489	90.392 0	0		
STM-69-70	MH-69	MH-70	90.5	0.013
91.282	91.101 0	0		
STM-7000-67	MH-7000	MH-67	43.5	0.013
91.254	91.102 0	0		
STM-70-71	MH-70	MH-71	61.5	0.013
91.026	90.903 0	0		
STM-7-10	MH-7	MH-10	54.5	0.013
90.722	90.64 0	0		

STM-71-72	MH-71	MH-72	61.5	0.013
90.883	90.76 0	0		
STM-72-73	MH-72	MH-73	45	0.013
90.685	90.617 0	0		
STM-73-75	MH-73	MH-75	63	0.013
90.242	90.147 0	0		
STM-74-49	MH-74	MH-49	107.5	0.013
91.021	90.806 0	0		
STM-74-75	MH-74	MH-75	78	0.013
90.951	90.717 0	0		
STM-75-76	MH-75	MH-76	62	0.013
90.117	90.024 0	0		
STM-76-77	MH-76	MH-77	57	0.013
89.964	89.878 0	0		
STM-7700-80	MH-7700	MH-80	64	0.013
90.769	90.545 0	0		
STM-77-78	MH-77	MH-78	78	0.013
89.818	89.701 0	0		
STM-78-79	MH-78	MH-79	12.5	0.013
89.671	89.652 0	0		
STM-79-83	MH-79	MH-83	31	0.013
89.622	89.575 0	0		
STM-80-81	MH-80	MH-81	79.5	0.013
90.395	90.236 0	0		
STM-81-82	MH-81	MH-82	14	0.013
90.176	90.141 0	0		
STM-82-83	MH-82	MH-83	13.5	0.013
90.081	90.04 0	0		
STM-83-84	MH-83	MH-84	26.5	0.013
89.515	89.462 0	0		
STM-85-63	MH-85	MH-63	10.5	0.013
91.751	91.714 0	0		
STM-8-57	MH-8	MH-57	25	0.013
91.12	90.77 0	0		
STM-85-86	MH-85	MH-86	50	0.013
91.758	91.583 0	0		
STM-86-87	MH-86	MH-87	9.5	0.013
91.523	91.49 0	0		
STM-87-88	MH-87	MH-88	27	0.013
91.34	91.259 0	0		
STM-88-89	MH-88	MH-89	13	0.013
91.229	91.19 0	0		
STM-8-9	MH-8	MH-9	28.5	0.013
91.351	91.251 0	0		
STM-89-90	MH-89	MH-90	50	0.013
91.04	90.965 0	0		
STM-90000-92	MH-90000	MH-92	58.5	0.013
91.424	91.219 0	0		
STM-9000-27	MH-9000	MH-27	103	0.013
90.942	90.736 0	0		
STM-90-67	MH-90	MH-67	108.5	0.013
90.89	90.727 0	0		
STM-9-10	MH-9	MH-10	59	0.013
91.231	90.995 0	0		

STM-91-68	MH-91	MH-68	79.5	0.013
91.178	90.939 0	0		
STM-91-92	MH-91	MH-92	30.5	0.013
91.326	91.219 0	0		
STM-92-94	MH-92	MH-94	65	0.013
91.144	90.949 0	0		
STM-93-73	MH-93	MH-73	81.5	0.013
91.087	90.842 0	0		
STM-93-94	MH-93	MH-94	28.5	0.013
91.366	91.024 0	0		
STM-94-101	MH-94	MH-101	44	0.013
90.874	90.764 0	0		
STM-95-96	MH-95	MH-96	44.5	0.013
91.467	91.311 0	0		
STM-96-97	MH-96	MH-97	13	0.013
91.236	91.197 0	0		
STM-97-98	MH-97	MH-98	64	0.013
91.122	90.994 0	0		
STM-98-99	MH-98	MH-99	64	0.013
90.919	90.791 0	0		
STM-99-100	MH-99	MH-100	13	0.013
90.761	90.735 0	0		

[XSECTIONS]

;;Link	Shape	Geom1	Geom2	Geom3	
Geom4	Barrels Culvert				
;;	-----	-----	-----	-----	-----
STM-100-101	CIRCULAR	0.525	0	0	0
1					
STM-101-102	CIRCULAR	0.675	0	0	0
1					
STM-10-19	CIRCULAR	0.675	0	0	0
1					
STM-10200-111	CIRCULAR	0.3	0	0	0
1					
STM-102-104	CIRCULAR	0.75	0	0	0
1					
STM-103-104	CIRCULAR	0.3	0	0	0
1					
STM-104-105	CIRCULAR	0.825	0	0	0
1					
STM-105-106	CIRCULAR	0.825	0	0	0
1					
STM-106-107	CIRCULAR	0.825	0	0	0
1					
STM-107-116	CIRCULAR	0.825	0	0	0
1					
STM-108-109	CIRCULAR	0.3	0	0	0
1					
STM-108-75	CIRCULAR	0.3	0	0	0
1					
STM-109-113	CIRCULAR	0.45	0	0	0
1					

STM-11000-109 1	CIRCULAR	0.375	0	0	0
STM-110-114 1	CIRCULAR	0.45	0	0	0
STM-11100-110 1	CIRCULAR	0.3	0	0	0
STM-111-112 1	CIRCULAR	0.3	0	0	0
STM-11-12 1	CIRCULAR	0.3	0	0	0
STM-11-20 1	CIRCULAR	0.3	0	0	0
STM-11200-105 1	CIRCULAR	0.45	0	0	0
STM-112-115 1	CIRCULAR	0.375	0	0	0
STM-11300-114 1	CIRCULAR	0.45	0	0	0
STM-113-120 1	CIRCULAR	0.6	0	0	0
STM-114-115 1	CIRCULAR	0.525	0	0	0
STM-115-116 1	CIRCULAR	0.6	0	0	0
STM-116-122 1	CIRCULAR	0.9	0	0	0
STM-117-118 1	CIRCULAR	0.45	0	0	0
STM-118-119 1	CIRCULAR	0.525	0	0	0
STM-119-120 1	CIRCULAR	0.6	0	0	0
STM-1-2 1	CIRCULAR	0.3	0	0	0
STM-120-121 1	CIRCULAR	0.75	0	0	0
STM-121-122 1	CIRCULAR	0.825	0	0	0
STM-12-13 1	CIRCULAR	0.3	0	0	0
STM-122-124 1	CIRCULAR	0.975	0	0	0
STM-123-124 1	CIRCULAR	0.3	0	0	0
STM-124-125 1	CIRCULAR	1.05	0	0	0
STM-125-126 1	CIRCULAR	1.05	0	0	0
STM-13-14 1	CIRCULAR	0.45	0	0	0
STM-14-15 1	CIRCULAR	0.525	0	0	0
STM-1-45 1	CIRCULAR	0.3	0	0	0



STM-1500-6 1	CIRCULAR	0.3	0	0	0
STM-15-16 1	CIRCULAR	0.6	0	0	0
STM-16-17 1	CIRCULAR	0.6	0	0	0
STM-17-18 1	CIRCULAR	0.6	0	0	0
STM-18-19 1	CIRCULAR	0.675	0	0	0
STM-19-29 1	CIRCULAR	0.75	0	0	0
STM-20-21 1	CIRCULAR	0.375	0	0	0
STM-21-22 1	CIRCULAR	0.45	0	0	0
STM-22-23 1	CIRCULAR	0.525	0	0	0
STM-2-3 1	CIRCULAR	0.375	0	0	0
STM-23-24 1	CIRCULAR	0.6	0	0	0
STM-24-25 1	CIRCULAR	0.6	0	0	0
STM-25-26 1	CIRCULAR	0.6	0	0	0
STM-26-29 1	CIRCULAR	0.675	0	0	0
STM-27-28 1	CIRCULAR	0.45	0	0	0
STM-28-29 1	CIRCULAR	0.45	0	0	0
STM-29-30 1	CIRCULAR	0.825	0	0	0
STM-31-32 1	CIRCULAR	0.3	0	0	0
STM-31-64 1	CIRCULAR	0.3	0	0	0
STM-3200-38 1	CIRCULAR	0.3	0	0	0
STM-32-33 1	CIRCULAR	0.3	0	0	0
STM-33-34 1	CIRCULAR	0.3	0	0	0
STM-3-4 1	CIRCULAR	0.375	0	0	0
STM-34-35 1	CIRCULAR	0.45	0	0	0
STM-35-36 1	CIRCULAR	0.6	0	0	0
STM-36-37 1	CIRCULAR	0.6	0	0	0
STM-37-44 1	CIRCULAR	0.6	0	0	0

STM-38-40 1	CIRCULAR	0.45	0	0	0
STM-39-40 1	CIRCULAR	0.3	0	0	0
STM-39-70 1	CIRCULAR	0.3	0	0	0
STM-4000-36 1	CIRCULAR	0.3	0	0	0
STM-40-41 1	CIRCULAR	0.525	0	0	0
STM-41-43 1	CIRCULAR	0.525	0	0	0
STM-42-43 1	CIRCULAR	0.3	0	0	0
STM-42-72 1	CIRCULAR	0.3	0	0	0
STM-43-44 1	CIRCULAR	0.6	0	0	0
STM-44-47 1	CIRCULAR	0.75	0	0	0
STM-4-5 1	CIRCULAR	0.525	0	0	0
STM-45-46 1	CIRCULAR	0.45	0	0	0
STM-46-47 1	CIRCULAR	0.525	0	0	0
STM-47-48 1	CIRCULAR	0.825	0	0	0
STM-48-50 1	CIRCULAR	0.825	0	0	0
STM-49-50 1	CIRCULAR	0.45	0	0	0
STM-50-51 1	CIRCULAR	0.9	0	0	0
STM-51-52 1	CIRCULAR	0.975	0	0	0
STM-5200-57 1	CIRCULAR	0.3	0	0	0
STM-52-54 1	CIRCULAR	1.05	0	0	0
STM-53-54 1	CIRCULAR	0.3	0	0	0
STM-53-80 1	CIRCULAR	0.3	0	0	0
STM-54-55 1	CIRCULAR	1.05	0	0	0
STM-55-56 1	CIRCULAR	1.05	0	0	0
STM-5-6 1	CIRCULAR	0.6	0	0	0
STM-56-61 1	CIRCULAR	1.05	0	0	0
STM-57-58 1	CIRCULAR	0.375	0	0	0

STM-58-59 1	CIRCULAR	0.45	0	0	0
STM-59-60 1	CIRCULAR	0.45	0	0	0
STM-60-61 1	CIRCULAR	0.45	0	0	0
STM-61-62 1	CIRCULAR	1.05	0	0	0
STM-63-65 1	CIRCULAR	0.3	0	0	0
STM-6400-69 1	CIRCULAR	0.3	0	0	0
STM-64-65 1	CIRCULAR	0.3	0	0	0
STM-65-66 1	CIRCULAR	0.45	0	0	0
STM-66-67 1	CIRCULAR	0.525	0	0	0
STM-6-7 1	CIRCULAR	0.6	0	0	0
STM-67-68 1	CIRCULAR	0.75	0	0	0
STM-68-73 1	CIRCULAR	0.825	0	0	0
STM-69-70 1	CIRCULAR	0.45	0	0	0
STM-7000-67 1	CIRCULAR	0.3	0	0	0
STM-70-71 1	CIRCULAR	0.525	0	0	0
STM-7-10 1	CIRCULAR	0.675	0	0	0
STM-71-72 1	CIRCULAR	0.525	0	0	0
STM-72-73 1	CIRCULAR	0.6	0	0	0
STM-73-75 1	CIRCULAR	0.975	0	0	0
STM-74-49 1	CIRCULAR	0.45	0	0	0
STM-74-75 1	CIRCULAR	0.375	0	0	0
STM-75-76 1	CIRCULAR	0.975	0	0	0
STM-76-77 1	CIRCULAR	0.975	0	0	0
STM-7700-80 1	CIRCULAR	0.3	0	0	0
STM-77-78 1	CIRCULAR	0.975	0	0	0
STM-78-79 1	CIRCULAR	0.975	0	0	0
STM-79-83 1	CIRCULAR	0.975	0	0	0

STM-80-81 1	CIRCULAR	0.45	0	0	0
STM-81-82 1	CIRCULAR	0.45	0	0	0
STM-82-83 1	CIRCULAR	0.45	0	0	0
STM-83-84 1	CIRCULAR	0.975	0	0	0
STM-85-63 1	CIRCULAR	0.3	0	0	0
STM-8-57 1	CIRCULAR	0.3	0	0	0
STM-85-86 1	CIRCULAR	0.3	0	0	0
STM-86-87 1	CIRCULAR	0.3	0	0	0
STM-87-88 1	CIRCULAR	0.45	0	0	0
STM-88-89 1	CIRCULAR	0.45	0	0	0
STM-8-9 1	CIRCULAR	0.3	0	0	0
STM-89-90 1	CIRCULAR	0.6	0	0	0
STM-90000-92 1	CIRCULAR	0.3	0	0	0
STM-9000-27 1	CIRCULAR	0.45	0	0	0
STM-90-67 1	CIRCULAR	0.675	0	0	0
STM-9-10 1	CIRCULAR	0.3	0	0	0
STM-91-68 1	CIRCULAR	0.375	0	0	0
STM-91-92 1	CIRCULAR	0.3	0	0	0
STM-92-94 1	CIRCULAR	0.375	0	0	0
STM-93-73 1	CIRCULAR	0.375	0	0	0
STM-93-94 1	CIRCULAR	0.3	0	0	0
STM-94-101 1	CIRCULAR	0.45	0	0	0
STM-95-96 1	CIRCULAR	0.3	0	0	0
STM-96-97 1	CIRCULAR	0.375	0	0	0
STM-97-98 1	CIRCULAR	0.45	0	0	0
STM-98-99 1	CIRCULAR	0.525	0	0	0
STM-99-100 1	CIRCULAR	0.525	0	0	0

[LOSSES]

;;Link	Kentry	Kexit	Kavg	Flap Gate	Seepage
STM-100-101	0	1.33	0	NO	0
STM-101-102	0	1.33	0	NO	0
STM-10-19	0	0.035	0	NO	0
STM-10200-111	0	1.33	0	NO	0
STM-102-104	0	1.33	0	NO	0
STM-103-104	0	1.33	0	NO	0
STM-104-105	0	0.02	0	NO	0
STM-105-106	0	0.47	0	NO	0
STM-106-107	0	0.47	0	NO	0
STM-107-116	0	1.33	0	NO	0
STM-108-109	0	1.33	0	NO	0
STM-108-75	0	1.33	0	NO	0
STM-109-113	0	0.035	0	NO	0
STM-11000-109	0	1.33	0	NO	0
STM-110-114	0	1.07	0	NO	0
STM-11100-110	0	1.33	0	NO	0
STM-111-112	0	0.035	0	NO	0
STM-11-12	0	0.54	0	NO	0
STM-11-20	0	0.32	0	NO	0
STM-11200-105	0	1.33	0	NO	0
STM-112-115	0	1.33	0	NO	0
STM-11300-114	0	0.035	0	NO	0
STM-113-120	0	1.07	0	NO	0
STM-114-115	0	0.08	0	NO	0
STM-115-116	0	1.33	0	NO	0
STM-116-122	0	1.33	0	NO	0
STM-117-118	0	0.47	0	NO	0
STM-118-119	0	0.26	0	NO	0
STM-119-120	0	0.035	0	NO	0
STM-1-2	0	0.035	0	NO	0
STM-120-121	0	0.08	0	NO	0
STM-121-122	0	0.035	0	NO	0
STM-12-13	0	0.54	0	NO	0
STM-122-124	0	1.33	0	NO	0
STM-123-124	0	1.33	0	NO	0
STM-124-125	0	0.02	0	NO	0
STM-13-14	0	0.035	0	NO	0
STM-14-15	0	0.02	0	NO	0
STM-1-45	0	0.47	0	NO	0
STM-1500-6	0	1.33	0	NO	0
STM-15-16	0	0.035	0	NO	0
STM-16-17	0	0.16	0	NO	0
STM-17-18	0	0.54	0	NO	0
STM-18-19	0	1.07	0	NO	0
STM-19-29	0	0.055	0	NO	0
STM-20-21	0	0.035	0	NO	0
STM-21-22	0	0.035	0	NO	0
STM-22-23	0	0.035	0	NO	0
STM-2-3	0	0.32	0	NO	0
STM-23-24	0	0.32	0	NO	0



STM-24-25	0	0.16	0	NO	0
STM-25-26	0	0.11	0	NO	0
STM-26-29	0	1.33	0	NO	0
STM-27-28	0	0.39	0	NO	0
STM-28-29	0	1.07	0	NO	0
STM-31-32	0	0.02	0	NO	0
STM-31-64	0	0.08	0	NO	0
STM-3200-38	0	0.035	0	NO	0
STM-32-33	0	0.32	0	NO	0
STM-33-34	0	0.32	0	NO	0
STM-3-4	0	0.32	0	NO	0
STM-34-35	0	0.035	0	NO	0
STM-35-36	0	0.02	0	NO	0
STM-36-37	0	0.02	0	NO	0
STM-37-44	0	1.33	0	NO	0
STM-38-40	0	0.02	0	NO	0
STM-39-40	0	1.33	0	NO	0
STM-39-70	0	1.33	0	NO	0
STM-4000-36	0	1.33	0	NO	0
STM-40-41	0	0.02	0	NO	0
STM-41-43	0	1.33	0	NO	0
STM-42-43	0	0.02	0	NO	0
STM-42-72	0	0.02	0	NO	0
STM-43-44	0	0.02	0	NO	0
STM-44-47	0	1.33	0	NO	0
STM-4-5	0	0.035	0	NO	0
STM-45-46	0	0.035	0	NO	0
STM-46-47	0	0.035	0	NO	0
STM-47-48	0	0.16	0	NO	0
STM-48-50	0	0.635	0	NO	0
STM-49-50	0	0.95	0	NO	0
STM-50-51	0	0.32	0	NO	0
STM-51-52	0	1.33	0	NO	0
STM-5200-57	0	1.33	0	NO	0
STM-52-54	0	1.33	0	NO	0
STM-53-54	0	1.33	0	NO	0
STM-53-80	0	1.33	0	NO	0
STM-54-55	0	0.39	0	NO	0
STM-55-56	0	0.32	0	NO	0
STM-5-6	0	0.02	0	NO	0
STM-56-61	0	1.33	0	NO	0
STM-57-58	0	0.035	0	NO	0
STM-58-59	0	0.54	0	NO	0
STM-59-60	0	0.39	0	NO	0
STM-60-61	0	1.33	0	NO	0
STM-63-65	0	1.33	0	NO	0
STM-6400-69	0	0.02	0	NO	0
STM-64-65	0	0.73	0	NO	0
STM-65-66	0	0.035	0	NO	0
STM-66-67	0	0.035	0	NO	0
STM-6-7	0	0.035	0	NO	0
STM-67-68	0	0.035	0	NO	0
STM-68-73	0	0.035	0	NO	0
STM-69-70	0	0.035	0	NO	0

STM-7000-67	0	1.33	0	NO	0
STM-70-71	0	0.02	0	NO	0
STM-7-10	0	0.035	0	NO	0
STM-71-72	0	1.33	0	NO	0
STM-72-73	0	1.33	0	NO	0
STM-73-75	0	0.055	0	NO	0
STM-74-49	0	0.11	0	NO	0
STM-74-75	0	1.33	0	NO	0
STM-75-76	0	1.33	0	NO	0
STM-76-77	0	1.33	0	NO	0
STM-7700-80	0	1.33	0	NO	0
STM-77-78	0	0.39	0	NO	0
STM-78-79	0	0.39	0	NO	0
STM-79-83	0	1.33	0	NO	0
STM-80-81	0	0.47	0	NO	0
STM-81-82	0	0.47	0	NO	0
STM-82-83	0	1.33	0	NO	0
STM-85-63	0	0.26	0	NO	0
STM-8-57	0	1.33	0	NO	0
STM-85-86	0	0.47	0	NO	0
STM-86-87	0	0.47	0	NO	0
STM-87-88	0	0.39	0	NO	0
STM-88-89	0	0.47	0	NO	0
STM-8-9	0	0.02	0	NO	0
STM-89-90	0	1.33	0	NO	0
STM-90000-92	0	0.02	0	NO	0
STM-9000-27	0	0.39	0	NO	0
STM-90-67	0	1.33	0	NO	0
STM-9-10	0	1.33	0	NO	0
STM-91-68	0	1.33	0	NO	0
STM-91-92	0	1.33	0	NO	0
STM-92-94	0	1.33	0	NO	0
STM-93-73	0	1.33	0	NO	0
STM-93-94	0	0.035	0	NO	0
STM-94-101	0	1.33	0	NO	0
STM-95-96	0	0.39	0	NO	0
STM-96-97	0	0.47	0	NO	0
STM-97-98	0	0.02	0	NO	0
STM-98-99	0	0.39	0	NO	0
STM-99-100	0	0.47	0	NO	0

[INFLOWS]

;;Node	Constituent	Time Series	Type	Mfactor
Sfactor	Baseline	Pattern		
;-----				
MH-1	FLOW	""	FLOW	1.0 1
72.2				
MH-10	FLOW	""	FLOW	1.0 1
7.1				
MH-100	FLOW	""	FLOW	1.0 1
2.1				
MH-102	FLOW	""	FLOW	1.0 1
62.5				

MH-10200 1.9	FLOW	" "	FLOW	1.0	1
MH-103 24.5	FLOW	" "	FLOW	1.0	1
MH-106 2	FLOW	" "	FLOW	1.0	1
MH-107 1	FLOW	" "	FLOW	1.0	1
MH-108 32	FLOW	" "	FLOW	1.0	1
MH-109 45.8	FLOW	" "	FLOW	1.0	1
MH-11 37.5	FLOW	" "	FLOW	1.0	1
MH-110 50.3	FLOW	" "	FLOW	1.0	1
MH-11000 32	FLOW	" "	FLOW	1.0	1
MH-111 20.5	FLOW	" "	FLOW	1.0	1
MH-11100 35.8	FLOW	" "	FLOW	1.0	1
MH-112 18.3	FLOW	" "	FLOW	1.0	1
MH-11200 69.4	FLOW	" "	FLOW	1.0	1
MH-113 12.9	FLOW	" "	FLOW	1.0	1
MH-11300 16.7	FLOW	" "	FLOW	1.0	1
MH-114 10.8	FLOW	" "	FLOW	1.0	1
MH-115 49.4	FLOW	" "	FLOW	1.0	1
MH-117 84.7	FLOW	" "	FLOW	1.0	1
MH-118 16.7	FLOW	" "	FLOW	1.0	1
MH-119 28.5	FLOW	" "	FLOW	1.0	1
MH-12 22.7	FLOW	" "	FLOW	1.0	1
MH-120 64.7	FLOW	" "	FLOW	1.0	1
MH-121 88.6	FLOW	" "	FLOW	1.0	1
MH-123 22.6	FLOW	" "	FLOW	1.0	1
MH-124 2.3	FLOW	" "	FLOW	1.0	1
MH-125 6.7	FLOW	" "	FLOW	1.0	1
MH-13 51.6	FLOW	" "	FLOW	1.0	1

MH-14 37.5	FLOW	" "	FLOW	1.0	1
MH-15 33.1	FLOW	" "	FLOW	1.0	1
MH-1500 11.1	FLOW	" "	FLOW	1.0	1
MH-16 36.9	FLOW	" "	FLOW	1.0	1
MH-17 5.1	FLOW	" "	FLOW	1.0	1
MH-18 20.2	FLOW	" "	FLOW	1.0	1
MH-2 30.7	FLOW	" "	FLOW	1.0	1
MH-20 54.8	FLOW	" "	FLOW	1.0	1
MH-21 46.4	FLOW	" "	FLOW	1.0	1
MH-22 38.6	FLOW	" "	FLOW	1.0	1
MH-23 48.8	FLOW	" "	FLOW	1.0	1
MH-24 15.9	FLOW	" "	FLOW	1.0	1
MH-25 18.8	FLOW	" "	FLOW	1.0	1
MH-26 28.9	FLOW	" "	FLOW	1.0	1
MH-27 6.1	FLOW	" "	FLOW	1.0	1
MH-28 22.6	FLOW	" "	FLOW	1.0	1
MH-3 10.7	FLOW	" "	FLOW	1.0	1
MH-31 30.5	FLOW	" "	FLOW	1.0	1
MH-32 19.2	FLOW	" "	FLOW	1.0	1
MH-3200 47.2	FLOW	" "	FLOW	1.0	1
MH-33 2.3	FLOW	" "	FLOW	1.0	1
MH-34 40.3	FLOW	" "	FLOW	1.0	1
MH-35 40.8	FLOW	" "	FLOW	1.0	1
MH-36 24.6	FLOW	" "	FLOW	1.0	1
MH-37 22.9	FLOW	" "	FLOW	1.0	1
MH-38 42.6	FLOW	" "	FLOW	1.0	1
MH-39 6.9	FLOW	" "	FLOW	1.0	1

MH-4 52.7	FLOW	" "	FLOW	1.0	1
MH-40 20	FLOW	" "	FLOW	1.0	1
MH-4000 8.3	FLOW	" "	FLOW	1.0	1
MH-41 20.9	FLOW	" "	FLOW	1.0	1
MH-42 23.6	FLOW	" "	FLOW	1.0	1
MH-43 10.2	FLOW	" "	FLOW	1.0	1
MH-44 5.3	FLOW	" "	FLOW	1.0	1
MH-45 48.9	FLOW	" "	FLOW	1.0	1
MH-46 33.7	FLOW	" "	FLOW	1.0	1
MH-5 45.3	FLOW	" "	FLOW	1.0	1
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MH-62	361539.895	5012702.429
MH-84	361635.023	5012758.53

[VERTICES]

;;Link

X-Coord

Y-Coord

;;-----



March 08, 2021

Project Number: 1474

David Schaeffer Engineering Ltd  
120 Iber Road, Unit 103  
Ottawa, Ontario  
K2S 1E9

**Attention: Steve Pichette, P.Eng.**

**Subject: Review of Quantity Control Requirement for Jock River-Reach One**

---

## Introduction

Phase 2 of the Barrhaven Conservancy Development (aka Conservancy East) is located in Barrhaven, Ontario, north of the Jock River, south of the Fraser Clarke Creek and east of the Foster Creek. The proposed development is approximately 59.26 ha that will primarily comprise of single and townhouse residential lots. As a part of the City of Ottawa's review of the proposed development draft plan of Phase 2 of the Barrhaven Conservancy Development, submitted in December 2020, it is proposed that flood quantity control measures will not need to be implemented as a part of this development. This assumption is based on the work completed by Stantec in June 2007 in the "Jock River Reach One Subwatershed Study" which concluded that for future developments within Reach 1 of the Jock River: "No quantity control storage is required for flood control purposes as the hydrograph from the subwatershed will peak before the upstream peak in the Jock River" and that "No erosion control storage is required to maintain the predevelopment in-stream erosion condition". Although this study did not consider the future development of the Barrhaven Conservancy Lands, and as such the modelling completed by Stantec has been updated by JFSA to reflect these changes. The following memo outlines data sources, assessed scenarios, assumptions, and conclusions of this independent Jock River Reach One study.

It is noted that RVCA is currently engaging in a formal update/review of the Jock River Reach One Subwatershed Study, with the findings of this study having the potential to affect the above-noted design criteria. While that study is underway J.F. Sabourin and Associates Inc. (JFSA) has completed an independent Jock River - Reach One study to re-assess/confirm that the assumptions presented in the original 2007 study by Stantec are still valid, as any changes to this conclusion could greatly impact the current BCDC Phase 2 development plan.

## Background Data

The following outlines all the model and data sources used in this analysis:

- "Jock River Floodplain Mapping Report", (2005 - PSR Group Ltd. & JFSA)
- "Jock River Reach One Subwatershed Study Final Report", (2007 – Stantec)
- "Corrigan Stormwater Management Facility Stormwater Management Report and Design Brief", (2010 - IBI Group)
- "Citi Gate, Highway 416 Employment Lands, Servicing Study and Stormwater Management Report (O'Keefe SWM)", (2012 – Novatech)
- "Foster Stormwater Management Facility, Environmental Study Report", (2013 - CH2MHill)
- "Todd Pond Model Keeper Analysis (Re-Assessment of Existing System Capacity)", (2015 – JFSA)

- “CitiGate 416 Corporate Campus Detailed Servicing and Stormwater Management Report (Phase 1)”, (2015 – Novatech)
- “Kennedy-Burnett Stormwater Management Facility Retrofit, Detailed Design Report”, (2020 – Novatech)
- “Half Moon Bay South / Addendum to April 2015 Todd Pond Model Keeper Analysis, Re-Assessment of Existing System Capacity Report” (2020 - JFSA).

## Model Development/Scenarios

The following section outlines the various hydrologic model scenarios developed as a part of this work, with a brief description of the data sources used for each scenario and how they have been incorporated into the existing Jock River subwatershed hydrologic model.

### Model 1 - Jock River Floodplain Model – JFSA, 2005

This hydrologic model was developed as a part of the floodplain mapping study of the Jock River completed in 2005. The hydrologic model of the Jock River was developed by JFSA using SWMHYMO, with independent models developed to simulate both summer and spring events. Both models were calibrated to field measured flows, recorded at the Water Survey Canada Flow Gauge at Moodie Drive. These models function as the basis for which all future models (both by JFSA and others) have been built on. Refer to Figure 1 (JFSA, 2005) for an overview of the subcatchments for reach one in this model, with full SWMHYMO input and summary files provided in Attachment A.

### Model 2 – Jock River Reach One Model – Stantec, 2007

The hydrologic analysis completed by Stantec in 2007 built upon the JFSA 2005 floodplain mapping modelling. As a part of the Stantec work, the lower reach of the Jock River (3,176 ha) which was represented as a single subcatchment in the 2005 study was subdivided into thirteen (13) subcatchments to better delineate the drainage areas to the various tributaries (O’Keefe, Fraser, Foster, Todd, Corrigan and Clarke) and to also provide a better representation of the existing development areas (Kennedy Burnett, Chapman Mills, Jockvale and Hearts Desire). The remaining natural/undeveloped areas within the Jock River corridor were subdivided into three smaller (3) sub-catchments. Refer to Figure 2 (Stantec, 2007) for an overview of the subcatchments for reach one in this model, with full SWMHYMO input and summary files provided in Attachment B.

As mentioned above from this study, it was concluded that developments located in the lower reaches of the Jock River do not require any quantity control storage for flood control purposes as the hydrograph from the subwatershed will peak before the upstream peak in the Jock River and that no erosion control storage is required to maintain the pre-development in-stream erosion conditions.

### Model 3 – Jock River Reach One Model Update – JFSA, 2021

As a part of the study outlined in this report, the 2007 Stantec SWMHYMO model of the Jock River was updated to reflect (as best as possible with the available information) proposed, approved and potential future developments, since the 2007 study.

At the time of the 2007 study, it was assumed that the floodplain of reach one of the Jock River (from Highway 416 to Greenbank Road) would not be filled and developed. Furthermore, the assumptions that were made in 2007 for the total imperviousness of future developments are not reflective of the actual constructed conditions observed in 2021; for example, the total impervious area for the Todd drainage area was assumed to be 43% in the 2007 study, while based on latest aerial photography it appears that the imperviousness for this area is closer to 58.5%). Additionally, SWM quantity controls were implemented in some tributaries within Reach One (e.g., O'Keefe, Foster and Kennedy-Burnett) to respect the hydraulic capacity of the local watercourses or other existing hydraulic constraints.

As outlined in the Background Data section of this memo, data from various reports and studies were collected and used to update Stantec's 2007 model, to best reflect existing conditions and known approved and planned development projects. As such, the thirteen (13) subcatchments of the 2007 Stantec model have been further discretized into one hundred ten (110) subcatchments, with numerous additional major system storage, SWM Ponds, and channel routing commands added. This updated existing condition model is reflective of current 2021 conditions, which assumes that the lower Jock River floodplain is undeveloped. It should also be noted that only subcatchments downstream of Highway 416 have been updated as a part of this analysis. Updates to other catchments of the Jock River further upstream, such as the Monahan Drain, Hobbs Creek, King Creek, and development areas in Richmond, where additional new information may be available, have not been included in the model updates at this time. Refer to Figure 3 for an overview of the subcatchments for reach one in this model, with full SWMHYMO input and summary files been provided in Attachment C, detailed schematics of the subcatchments updated as a part of this study have been provided in Attachment F.

Note that Novatech's PCSWMM model of the Kennedy-Burnett area was used to create a detailed SWMHYMO model of the same area. In creating this SWMHYMO model it was found that the 100-year peak outflows from the Kennedy Burnett facility were 1.4 times higher than that reported in the Novatech PCSWMM model. While it is expected that different modelling software will produce slightly different results, this difference is significant and should be investigated further; although it is unlikely that this difference is expected to change the fundamental conclusions of this analysis.

#### Model 4A & 4B – Jock River Reach One Future Conditions (without and with quantity SWM controls) – JFSA, 2021

Two additional models (4A and 4B) were created (which built on model 3) to evaluate the impacts of developing portions of the lower Jock River floodplain (from Highway 416 to Greenbank Road). These lands make up approximately 156 ha and would include BCDC and other properties on the south side of the Jock River. Model 4A assumes that these lands would be developed without any SWM quantity controls and Model 4B assumes that the lands would be developed with SWM Post to Pre-development quantity controls. Refer to Figure 4 for an overview of the subcatchments for reach one in these models, with full SWMHYMO input and summary files for scenarios 4A and 4B provided in Attachment D & E, respectively.

## Results

All hydrologic models were run using a 24 hours SCS storm for the 2-to-100-year events. Note that this analysis focuses on this particular rainfall event as for developed areas the summer rainfall events are more critical than the spring rainfall plus snowmelt conditions. Hence, only the summer peak flows have been summarized and compared for the various scenarios below, as the flow contributions from the developments in the lower Jock River under the spring rainfall + snowmelt event are negligible compared to the flows upstream from the greater Jock River. It is further noted that the same design storms were used in all models.

Peak flows at key locations along Reach One of the Jock River have been extracted from the various hydrologic models and provided in the following section. As a part of this analysis, 5 key locations on the Jock River have been selected to compare the simulated peak flows and are as follows: Highway 416, Borrisokane Road, Greenbank Road, Jockvale Road and the Jock River's confluence with the Rideau River. Note that for the older models (JFSA 2005 & Stantec 2007) results have only been provided at some locations, as these original models were not discretized to this higher level of detail. Additionally, the Stantec 2007 model did not assess flows on the Jock River for the 10- and 50-year events at any locations.

**Table 1: Comparison of Summer Peak Flows (m<sup>3</sup>/s) at Highway 416 (52483.00 ha)**

Scenario	Return Period					
	2-Year	5-Year	10-Year	25-Year	50-Year	100-Year
Model 1: 2005 Floodplain Study	45.676	66.292	82.076	104.643	122.469	141.415
Model 2: Stantec 2007 Reach One Analysis	45.789	66.413	n/a	104.834	n/a	141.853
Model 3: Updated Model 2 to current/ approved conditions	46.294	67.222	83.235	106.109	124.249	143.580
Model 4A: Model 3 with BCDC & others w/o SWM	46.294	67.222	83.235	106.109	124.249	143.580
Model 4B: Model 3 with BCDC & others with SWM	46.294	67.222	83.235	106.109	124.249	143.580

From Table 1 above it is seen that the peak flows on the Jock River at Highway 416 for Models 3, 4A and 4B are higher than in Models 1 and 2. This is because the computational time step in the updated models was reduced from 5 - 10 minutes to 1 minute. This change was necessary to provide stable results in the various models, especially with the additional ROUTE CHANNEL commands that have been added to the updated models. There were no other changes made to the models upstream of Highway 416.

**Table 2: Comparison of Summer Peak Flows (m<sup>3</sup>/s) at Borrisokane Road (53577.82 ha)**

Scenario	Return Period					
	2-Year	5- Year	10-Year	25-Year	50-Year	100-Year
Model 1: 2005 Floodplain Study	n/a	n/a	n/a	n/a	n/a	n/a
Model 2: Stantec 2007 Reach One Analysis	46.817	68.124	n/a	107.402	n/a	144.892
Model 3: Updated Model 2 to current/ approved conditions	47.379	69.117	85.613	108.988	127.740	147.849
Model 4A: Model 3 with BCDC & others w/o SWM	47.426	68.998	85.561	109.064	127.650	147.535
Model 4B: Model 3 with BCDC & others with SWM	47.599	69.319	85.870	109.449	128.055	147.939

From Table 2 it is seen that the peak flows on the Jock River at Borrisokane are generally lower in model 4A (developed without SWM controls) than under existing conditions (Model 3). The inclusion of SWM controls for these future developments results in the peak flows increasing from existing conditions for all return periods at this location. Note that the increase in flows at this location between the Stantec model (model 2) and the JFSA existing conditions model (model 3) again is due to the greater discretization of subcatchments at Borrisokane Road in the JFSA model. For example, in the Stantec model, the subcatchment that represents the currently undeveloped lands along the Jock River is represented as a single subcatchment (S-1). Where the JFSA updated model represents these lands as 14 individual subcatchments, all discharging to their respective locations within the Jock River (e.g. O’Keefe Creek, Foster Creek & Borrisokane Road).

**Table 3: Comparison of Summer Peak Flows (m<sup>3</sup>/s) at Greenbank Road (54717.80 ha)**

Scenario	Return Period					
	2-Year	5- Year	10-Year	25-Year	50-Year	100-Year
Model 1: 2005 Floodplain Study	n/a	n/a	n/a	n/a	n/a	n/a
Model 2: Stantec 2007 Reach One Analysis	49.195	71.220	n/a	111.172	n/a	149.236
Model 3: Updated Model 2 to current/ approved conditions	49.055	70.826	86.895	110.282	128.564	147.488
Model 4A: Model 3 with BCDC & others w/o SWM	48.599	69.773	85.389	103.842	126.050	144.531
Model 4B: Model 3 with BCDC & others with SWM	48.982	70.171	85.928	103.651	126.537	144.894



From Table 3 it is seen that peak flows on the Jock River at Greenbank Road are the lowest without SWM controls in place (Model 4A). With SWM controls in place, the peak flows are lower than the existing conditions, but not as low as when SWM controls are not implemented. Note that the JFSA existing conditions model (model 3) is presenting peak flows lower than the Stantec model (model 2) at this location, again this is due to the greater discretization in the JFSA model as discussed above.

**Table 4: Comparison of Summer Peak Flows (m<sup>3</sup>/s) at Jockvale Road (55476.26 ha)**

Scenario	Return Period					
	2-Year	5- Year	10-Year	25-Year	50-Year	100-Year
Model 1: 2005 Floodplain Study	n/a	n/a	n/a	n/a	n/a	n/a
Model 2: Stantec 2007 Reach One Analysis	49.870	72.143	n/a	112.074	n/a	150.033
Model 3: Updated Model 2 to current/ approved conditions	49.619	72.224	88.294	111.989	130.865	149.819
Model 4A: Model 3 with BCDC & others w/o SWM	49.482	71.017	86.165	105.082	128.174	146.840
Model 4B: Model 3 with BCDC & others with SWM	49.606	71.408	86.690	104.765	128.229	147.027

From Table 4 is seen that the peak flows at Jockvale Road are generally at their lowest without SWM controls in place, and that either implementing or not implementing SWM controls for future developments results in peak flows at this location being less than existing conditions.

**Table 5: Comparison of Summer Peak Flows (m<sup>3</sup>/s) at Outlet of Jock River (55579.20 ha)**

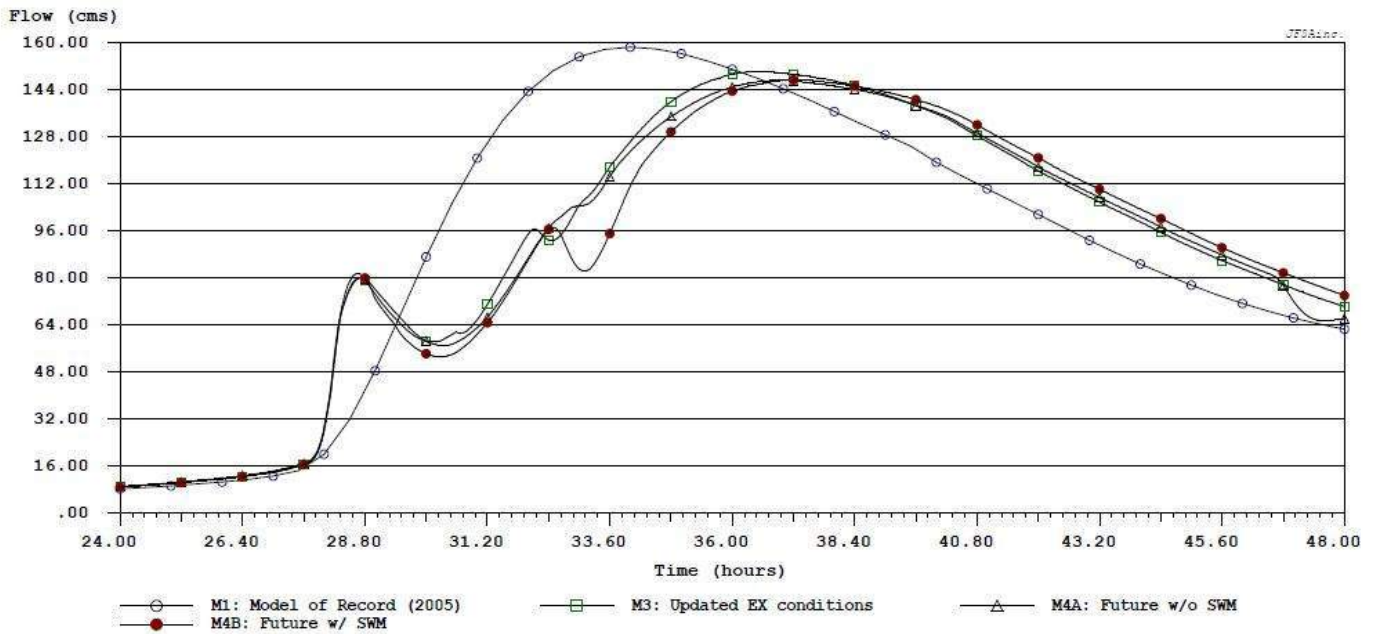
Scenario	Return Period					
	2-Year	5- Year	10-Year	25-Year	50-Year	100-Year
Model 1: 2005 Floodplain Study	49.16	72.08	89.96	115.84	136.46	158.42
Model 2: Stantec 2007 Reach One Analysis	50.78	73.65	n/a	113.97	n/a	157.69
Model 3: Updated Model 2 to current/ approved conditions	49.72	72.36	88.45	112.2	131.12	150.12
Model 4A: Model 3 with BCDC & others w/o SWM	49.58	71.17	86.35	105.27	128.42	147.10
Model 4B: Model 3 with BCDC & others with SWM	49.70	71.54	86.85	104.96	128.45	147.28

From Table 5 it is seen that the peak flows on the Jock River at the confluence with the Rideau River are generally at their lowest without SWM controls in place, and that either implementing or not implementing SWM controls for future developments results in peak flows at this location to be less than existing conditions.

### Discussion

Although not initially obvious, the reason that future urban developments within Reach One of the Jock River are decreasing peak flows on the Jock River is because developing land not only affects the peak of the hydrograph but also the overall shape. Figure A below provides a comparison of the simulated hydrographs at the Jock River's confluence with the Rideau River from the various model scenarios. During any rainfall event, the runoff from the existing and future developments within Reach One will have already peaked and decayed before the peak flows arrive at this location from the upstream drainage area. For the 100-Year SCS storm, the peak from the development in Reach One can be seen in the figure below at around 28 hours, while the peak flow on the Jock River from the upstream drainage areas occurs at around 36-37 hours, this is approximately a 9-hour difference in timing. As such, implementing SWM measures for developments in the lower portions of the Jock River will decrease peak flows from the development, but would also prolong the period of time during which they discharge into the Jock River, thus coinciding with flows from the greater Jock River, ultimately resulting in potential increases in peak flows on the Jock River. This is seen in the figure below with the future condition with SWM controls (Model 4B - Red Circles) having a higher flow in the tail than future conditions without SWM controls (Model 4A – Black Triangles). Note that the difference between Model 1 and all other scenarios is simply due to further discretization of subcatchments within Reach One.

Figure A: Comparison of simulated 100 yr Jock River hydrographs at the confluence with the Rideau River



### Hydrograph Statistics:

Legend	Filename & Comment	Time Step (min)	Drainage Area (ha)	Peak Flow (cms)	Time to Peak (hrs)	Runoff Volume (mm)	Runoff Volume (cu.m)	Duration of flow (hrs)	Average flow (cms)
○	N1_0100 : M1: Model of Record (2005)	30.00	55659.00	158.420	34.000	14.52	8.082E+06	24.000	93.538
□	SN_N1_0100 : M3: Updated EX conditions	1.00	55579.20	150.120	36.533	14.24	7.914E+06	24.000	91.603
△	SN_N1_0100 : M4A: Future w/o SWM	1.00	55579.20	147.102	36.917	14.12	7.848E+06	24.000	90.831
●	SN_N1_0100 : M4B: Future w/ SWM	1.00	55579.19	147.276	37.250	14.03	7.798E+06	24.000	90.252

## Conclusion

The hydrologic model developed as a part of the Jock River Reach One Subwatershed Study (Stantec 2007) has been updated to provide additional refinements in the lower reaches of the Jock River (downstream of Highway 416) and assumes the development of lands that were previously not considered in the 2007 analysis (e.g. Barrhaven Conservancy). Future development condition models were created with and without SWM controls assumed, and the peak flows extracted from these models at key locations along the lower Jock River. From this analysis, it was found that with these additional developments in the lower Jock River peak flows are generally less than existing conditions without SWM controls in place. Implementing SWM controls for these developments has also been found to generally decrease peak flows on the Jock River, but not at all locations and not to the same degree as without SWM controls. Ultimately these findings are consistent with the fundamental conclusions drawn in Stantec's 2007 Jock River Reach One study, which initially determined that for future developments within Reach One of the Jock River "No quantity control storage is required for flood control purposes as the hydrograph from the subwatershed will peak before the upstream peak in the Jock River" and that "No erosion control storage is required to maintain the pre-development in-stream erosion condition". Based on the results of the updated analysis outlined in this memo, it can confirm that the fundamental conclusions drawn in Stantec's 2007 for developments in reach one of the Jock River remain valid.

Yours truly,  
**J.F Sabourin and Associates Inc.**



Jonathon Burnett, P.Eng  
Water Resources Engineer

cc: J.F Sabourin, M.Eng, P.Eng  
Director of Water Resources Projects



## Figures

- Figure 1: Model 1 – Jock River Floodplain Model – JFSA, 2005
- Figure 2: Model 2 – Jock River Reach One Model – Stantec, 2007
- Figure 3: Model 3 – Jock River Reach One Model Update - JFSA, 2021
- Figure 4: Model 4A & 4B – Jock River Reach One Future Conditions - JFSA, 2021

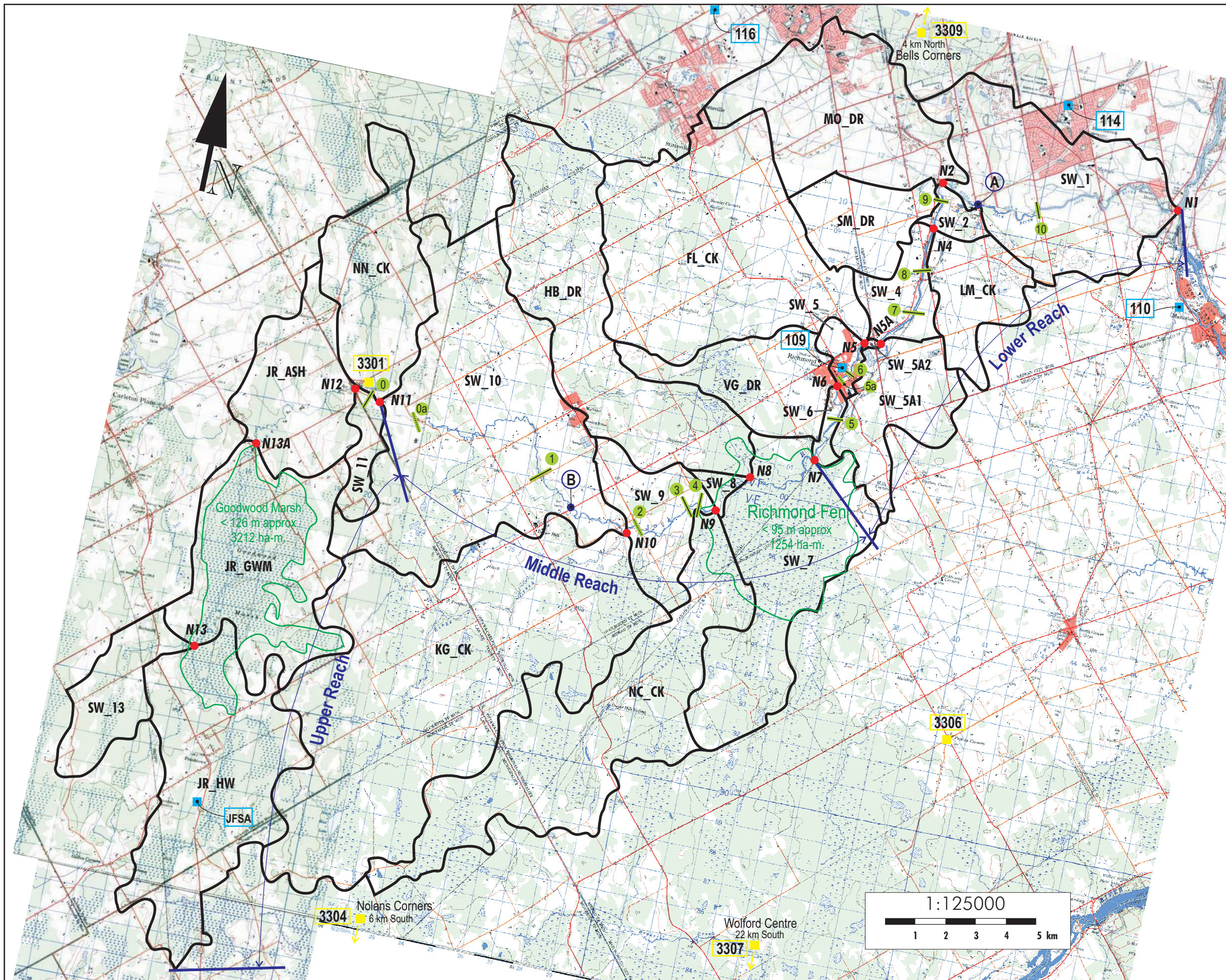
## Tables

- Table 1: Summer Peak Flows at Highway 416
- Table 2: Summer Peak Flows at Borrisokane Road.
- Table 3: Summer Peak Flows at Greenbank Road
- Table 4: Summer Peak Flows at Jockvale Road
- Table 5: Summer Peak Flows at Outlet of Jock River

## Attachments

- Attachment A: Model 1 - SWMHYMO Input & Summary files
- Attachment B: Model 2 - SWMHYMO Input & Summary files
- Attachment C: Model 3 - SWMHYMO Input & Summary files
- Attachment D: Model 4A - SWMHYMO Input & Summary files
- Attachment E: Model 4B - SWMHYMO Input & Summary files
- Attachment F: Updated Subcatchment Schematics & Tables





- Legend:**
- Watershed
  - Bogs (Reservoir)
  - Nodes
  - Flow gauges
  - Rain gauges
  - Snow course stations
  - River Cross-Sections (based on topo. maps)
  - River Cross-Sections adjusted with field data
  - Reaches limits
- Flow gauges ID**
- 02LA007- Jock River near Richmond
  - Jock River at Franktown Rd
- Rain gauges ID**
- Richmond
  - Manotick
  - Barrhaven
  - Maple Grove
  - JFSA Inc, Temporary Rain Gauge 2003
- Snow course stations ID**
- Ashton
  - Nolans Corners
  - Pierces Corners
  - Bells Corners
  - Wolford Centre

Client:

Project:  
Jock River Flood Plain Mapping Study

Title:  
Watershed Delineation

J.F. Sabourin & Associates Inc.  
WATER RESOURCES AND ENVIRONMENTAL CONSULTANTS  
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Figure 1 Ref. File: Base Map Jock River B.cdr





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Legend

- Existing SWM Facility
- Proposed Stormwater Facility
- Proposed Pond Outlet
- Jock River Tributary (Municipal Drain)
- Jock River Tributary (Non-Municipal Drain)
- Watershed Boundary
- Regulatory Flood Level
- Normal Water Level
- Woodlot Limits
- Sub-drainage Area Limit
- Sub-drainage Area Name
- Sub-drainage Area Size
- % Impervious or Time to Peak (hours)
- SCS Curve Number
- Application Plans Under Review
- 10 Year Flood Line
- 25 Year Flood Line
- 100 Year Flood Line

1	FINAL REPORT	BCB	N.C.	JUNE 2007
Revision		By	Appd.	YY.MM.DD
File Name:		Own.	Chgd.	Dgn.
				YY.MM.DD

Seal

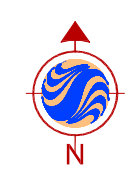
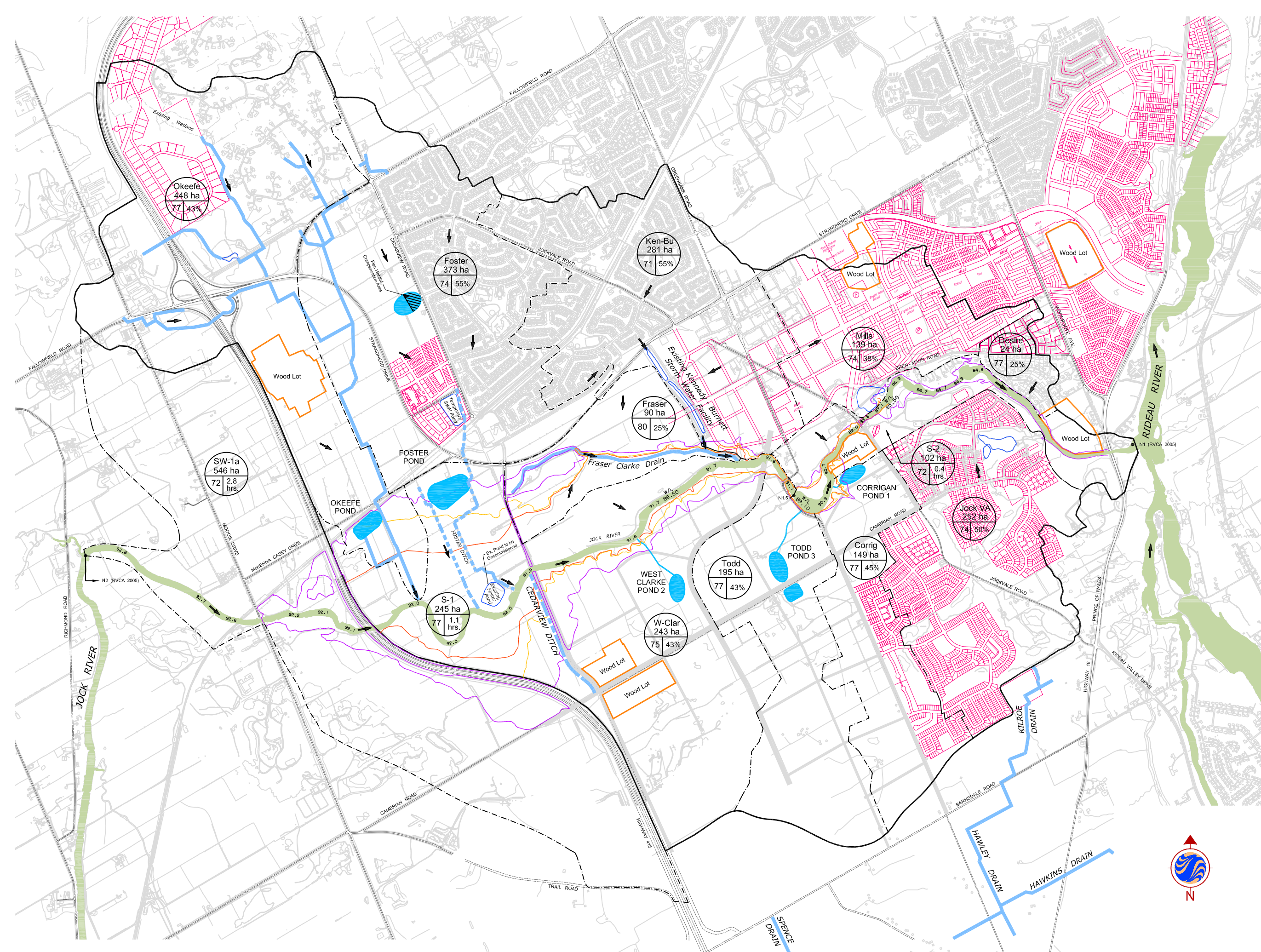
Client/Project

JOCK RIVER REACH ONE  
SUB-WATERSHED STUDY  
Ottawa ON Canada

Title  
PROPOSED CONDITIONS  
HYDROLOGIC MODEL  
DRAINAGE BOUNDARIES

Project No. 60400414 Scale 0 100 300 500m  
Drawing No. 1:10,000 Sheet 1 of 1

Figure 2 1 of 1 1







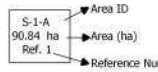




- Legend**
- Channel Cross Sections
  - S-1 Sub-catchments and Fraser Sub-catchments
  - S-1-A
  - S-1-B
  - S-1-D1
  - S-1-D2
  - S-1-D3
  - S-1-D4
  - S-1-D5
  - S-1-D6
  - S-1-D7
  - S-1-D8
  - S-1-FO-D1
  - S-1-FO-D2
  - S-1-FO-F-D
  - S-1-Okeefe
  - FRASER-DRN
  - FRASER-D
- Google Hybrid

File name: 20210304\_S-1\_Fraser\_Schematic-Model4A.pdf

XS 3633 Cross Section at station 3633



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PROJECT :  
 BCDC - Quantity Control Study

TITLE :  
 S-1 Sub-catchment and Fraser Clarke Sub-catchment Schematic

PROJECT NO. 1474-16

DRAWN: MM

DATE: Mar. 2021

Station	Channel Name	Channel Type	Channel Width (m)	Channel Depth (m)	Channel Slope	Channel Material	Channel Status	Channel Reference
3633	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3634	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3635	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3636	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3637	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3638	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3639	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3640	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3641	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3642	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3643	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3644	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3645	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3646	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3647	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3648	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3649	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3650	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3651	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3652	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3653	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
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3660	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3661	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3662	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3663	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3664	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3665	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3666	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3667	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3668	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3669	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
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3675	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3676	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3677	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3678	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3679	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3680	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3681	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3682	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
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3684	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3685	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3686	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3687	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3688	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3689	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3690	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3691	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3692	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3693	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3694	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3695	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3696	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3697	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3698	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3699	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15
3700	FRASER-D	Channel	10.0	1.0	0.001	Gravel	Open	Ref. 15









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# Attachment A

Model 1 – Jock River Floodplain Model

JFSA, 2005

SWMHYMO Input & Summary files



```

1  20    Metric units / ID numbers OFF
2  *#*****
3  *# SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
4  *#*****
5  *# Project Name: [Jock River]    Project Number: [411-02]
6  *# Date       : 06-06-2003
7  *# Modeller   : [JoF]
8  *# Company    : JFSAinc.
9  *# License #  : 2549237
10 *#*****
11 *# CALIBRATION OF SUMMER MODEL PARAMETERS
12 *# USING CONTINUOUS SIMULATIONS
13 *# Rainfall data from JFSA raingauge installed at site + other gauges by the City
14 *# Use data collected from May 1st to July 14, 2003
15 *
16 * Calibrated parameters for Summer 2003 data:  APII=50, APIK=0.85, CN=varies,
17 *                                                SK=0.01, InterEventTime=12,
18 *                                                GWResk=0.96, VHydCond=0.055
19 *
20 *# -----
21 *
22 *START          TZERO=[2003.0501], METOUT=[2], NSTORM=[1], NRUN=[001]
23 *              ["XAVG0315.STM"] average storm data a 15 minute time step
24 *              The above rainf file is an average of the JFSA gauge data
25 *              with the City of Ottawa rainfall data collected during
26 *              the same period.
27 *% 2 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
28 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[2]
29 *%              ["C24SC002.stm"] <--storm filename, one per line for NSTORM time
30 *%-----|-----|
31 *%-----|-----|
32 READ STORM     STORM_FILENAME=["storm.001"]
33 *%-----|-----|
34 MODIFY STORM   ICASEms=[1], NSHIFT=[96],
35 *%              RedFACT=[1],
36 *%-----|-----|
37 COMPUTE API    APII=[50], APIK=[.85]/day
38 *%-----|-----|
39 *%-----|-----|
40 *#
41 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
42 *# of 1.32
43 *%-----|-----|
44 CONTINUOUS NASHYD NHYD=["JR_HW"], DT=[30]min, AREA=[3680](ha),
45 *%              DWF=[0](cms), CN/C=[64], IA=[2.5](mm),
46 *%              N=[3.0], TP=[7.13]hrs,
47 *%              Continuous simulation parameters:
48 *%              IaREcper=[4](hrs),
49 *%              SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
50 *%              InterEventTime=[12](hrs)
51 *%              Baseflow simulation parameters:
52 *%              BaseFlowOption=[1] ,
53 *%              InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
54 *%              VHydCond=[0.055](mm/hr), END=-1
55 *%-----|-----|
56 *#
57 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
58 *# of 1.32
59 *%-----|-----|
60 CONTINUOUS NASHYD NHYD=["SW_13"], DT=[30]min, AREA=[971](ha),
61 *%              DWF=[0](cms), CN/C=[61], IA=[2.5](mm),
62 *%              N=[3.0], TP=[3.76]hrs,
63 *%              Continuous simulation parameters:
64 *%              IaREcper=[4](hrs),
65 *%              SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
66 *%              InterEventTime=[12](hrs)

```



```

67         Baseflow simulation parameters:
68         BaseFlowOption=[1] ,
69         InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
70         VHydCond=[0.055](mm/hr) ,    END=-1
71     *%-----|-----
72     *#
73     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
74     *# of 1.80
75     *%-----|-----
76     CONTINUOUS NASHYD  NHYD=["JR_GWM"] , DT=[30]min , AREA=[3074](ha) ,
77                       DWF=[0](cms) , CN/C=[55] , IA=[2.5](mm) ,
78                       N=[3] , TP=[11.33]hrs ,
79                       Continuous simulation parameters:
80                       IaRECPper=[4](hrs) ,
81                       SMIN=[-1](mm) , SMAX=[-1](mm) , SK=[0.010]/(mm) ,
82                       InterEventTime=[12](hrs)
83                       Baseflow simulation parameters:
84                       BaseFlowOption=[1] ,
85                       InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
86                       VHydCond=[0.055](mm/hr) ,    END=-1
87     *%-----|-----
88     CONTINUOUS NASHYD  NHYD=["JR_ASH"] , DT=[30]min , AREA=[1781](ha) ,
89                       DWF=[0](cms) , CN/C=[72] , IA=[2.5](mm) ,
90                       N=[3.0] , TP=[3.91]hrs ,
91                       Continuous simulation parameters:
92                       IaRECPper=[4](hrs) ,
93                       SMIN=[-1](mm) , SMAX=[-1](mm) , SK=[0.010]/(mm) ,
94                       InterEventTime=[12](hrs)
95                       Baseflow simulation parameters:
96                       BaseFlowOption=[1] ,
97                       InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
98                       VHydCond=[0.055](mm/hr) ,    END=-1
99     *%-----|-----
100    CONTINUOUS NASHYD  NHYD=["SW_11"] , DT=[30]min , AREA=[500](ha) ,
101                      DWF=[0](cms) , CN/C=[66] , IA=[2.5](mm) ,
102                      N=[3.0] , TP=[1.24]hrs ,
103                      Continuous simulation parameters:
104                      IaRECPper=[4](hrs) ,
105                      SMIN=[-1](mm) , SMAX=[-1](mm) , SK=[0.010]/(mm) ,
106                      InterEventTime=[12](hrs)
107                      Baseflow simulation parameters:
108                      BaseFlowOption=[1] ,
109                      InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
110                      VHydCond=[0.055](mm/hr) ,    END=-1
111    *%-----|-----
112    *#
113    *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
114    *# of 1.80
115    *%-----|-----
116    CONTINUOUS NASHYD  NHYD=["NN_CK"] , DT=[30]min , AREA=[1917](ha) ,
117                      DWF=[0](cms) , CN/C=[66] , IA=[2.5](mm) ,
118                      N=[3.0] , TP=[5.29]hrs ,
119                      Continuous simulation parameters:
120                      IaRECPper=[4](hrs) ,
121                      SMIN=[-1](mm) , SMAX=[-1](mm) , SK=[0.010]/(mm) ,
122                      InterEventTime=[12](hrs)
123                      Baseflow simulation parameters:
124                      BaseFlowOption=[1] ,
125                      InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
126                      VHydCond=[0.055](mm/hr) ,    END=-1
127    *%-----|-----
128    *#
129    *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
130    *# of 1.52
131    *%-----|-----
132    CONTINUOUS NASHYD  NHYD=["SW_10"] , DT=[30]min , AREA=[5666](ha) ,

```

```

133 DWF=[0](cms), CN/C=[72], IA=[2.5](mm),
134 N=[3.0], TP=[8.00]hrs,
135 Continuous simulation parameters:
136 IaREcper=[4](hrs),
137 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
138 InterEventTime=[12](hrs)
139 Baseflow simulation parameters:
140 BaseFlowOption=[1] ,
141 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
142 VHydCond=[0.055](mm/hr), END=-1
143 *%-----|-----
144 *#
145 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
146 *# of 1.75
147 *%-----|-----
148 CONTINUOUS NASHYD NHYD=["KG_CK"], DT=[30]min, AREA=[8376](ha),
149 DWF=[0](cms), CN/C=[66], IA=[2.5](mm),
150 N=[3.0], TP=[11.66]hrs,
151 Continuous simulation parameters:
152 IaREcper=[4](hrs),
153 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
154 InterEventTime=[12](hrs)
155 Baseflow simulation parameters:
156 BaseFlowOption=[1] ,
157 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
158 VHydCond=[0.055](mm/hr), END=-1
159 *%-----|-----
160 *#
161 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
162 *# of 1.68
163 *%-----|-----
164 CONTINUOUS NASHYD NHYD=["SW_9"], DT=[30]min, AREA=[1132](ha),
165 DWF=[0](cms), CN/C=[70], IA=[2.5](mm),
166 N=[3.0], TP=[2.51]hrs,
167 Continuous simulation parameters:
168 IaREcper=[4](hrs),
169 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
170 InterEventTime=[12](hrs)
171 Baseflow simulation parameters:
172 BaseFlowOption=[1] ,
173 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
174 VHydCond=[0.055](mm/hr), END=-1
175 *%-----|-----
176 *#
177 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
178 *# of 1.82
179 *%-----|-----
180 CONTINUOUS NASHYD NHYD=["NC_CK"], DT=[30]min, AREA=[4464](ha),
181 DWF=[0](cms), CN/C=[62], IA=[2.5](mm),
182 N=[3.0], TP=[11.32]hrs,
183 Continuous simulation parameters:
184 IaREcper=[4](hrs),
185 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
186 InterEventTime=[12](hrs)
187 Baseflow simulation parameters:
188 BaseFlowOption=[1] ,
189 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
190 VHydCond=[0.055](mm/hr), END=-1
191 *%-----|-----
192 *#
193 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
194 *# of 1.80
195 *%-----|-----
196 CONTINUOUS NASHYD NHYD=["SW_8"], DT=[30]min, AREA=[131](ha),
197 DWF=[0](cms), CN/C=[63], IA=[2.5](mm),
198 N=[3.0], TP=[0.90]hrs,

```

```

199         Continuous simulation parameters:
200         IaRECPper=[4](hrs),
201         SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
202         InterEventTime=[12](hrs)
203         Baseflow simulation parameters:
204         BaseFlowOption=[1] ,
205         InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
206         VHydCond=[0.055](mm/hr),  END=-1
207     *%-----|-----
208     *#
209     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
210     *# of 1.65
211     *%-----|-----
212     CONTINUOUS NASHYD  NHYD=["HB_DR"], DT=[30]min, AREA=[3854](ha),
213                       DWF=[0](cms),  CN/C=[66], IA=[2.5](mm),
214                       N=[3.0], TP=[8.42]hrs,
215                       Continuous simulation parameters:
216                       IaRECPper=[4](hrs),
217                       SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
218                       InterEventTime=[12](hrs)
219                       Baseflow simulation parameters:
220                       BaseFlowOption=[1] ,
221                       InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
222                       VHydCond=[0.055](mm/hr),  END=-1
223     *%-----|-----
224     *#
225     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
226     *# of 1.82
227     *%-----|-----
228     CONTINUOUS NASHYD  NHYD=["SW_7"], DT=[30]min, AREA=[3197](ha),
229                       DWF=[0](cms),  CN/C=[57], IA=[2.5](mm),
230                       N=[3.0], TP=[6.65]hrs,
231                       Continuous simulation parameters:
232                       IaRECPper=[4](hrs),
233                       SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
234                       InterEventTime=[12](hrs)
235                       Baseflow simulation parameters:
236                       BaseFlowOption=[1] ,
237                       InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
238                       VHydCond=[0.055](mm/hr),  END=-1
239     *%-----|-----
240     *#
241     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
242     *# of 1.75
243     *%-----|-----
244     CONTINUOUS NASHYD  NHYD=["SW_6"], DT=[30]min, AREA=[165](ha),
245                       DWF=[0](cms),  CN/C=[67], IA=[2.5](mm),
246                       N=[3.0], TP=[4.18]hrs,
247                       Continuous simulation parameters:
248                       IaRECPper=[4](hrs),
249                       SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
250                       InterEventTime=[12](hrs)
251                       Baseflow simulation parameters:
252                       BaseFlowOption=[1] ,
253                       InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
254                       VHydCond=[0.055](mm/hr),  END=-1
255     *%-----|-----
256     *#
257     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
258     *# of 1.67
259     *%-----|-----
260     CONTINUOUS NASHYD  NHYD=["VG_DR"], DT=[30]min, AREA=[1332](ha),
261                       DWF=[0](cms),  CN/C=[72], IA=[2.5](mm),
262                       N=[3.0], TP=[5.95]hrs,
263                       Continuous simulation parameters:
264                       IaRECPper=[4](hrs),

```

```

265 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
266 InterEventTime=[12](hrs)
267 Baseflow simulation parameters:
268 BaseFlowOption=[1] ,
269 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
270 VHydCond=[0.055](mm/hr), END=-1
271 *%-----|
272 CONTINUOUS NASHYD NHYD=["SW_5"], DT=[30]min, AREA=[224](ha),
273 DWF=[0](cms), CN/C=[77], IA=[2.5](mm),
274 N=[3.0], TP=[0.75]hrs,
275 Continuous simulation parameters:
276 IaREcper=[4](hrs),
277 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
278 InterEventTime=[12](hrs)
279 Baseflow simulation parameters:
280 BaseFlowOption=[1] ,
281 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
282 VHydCond=[0.055](mm/hr), END=-1
283 *%-----|
284 *#
285 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
286 *# of 1.20
287 *%-----|
288 CONTINUOUS NASHYD NHYD=["FL_CK"], DT=[30]min, AREA=[4945](ha),
289 DWF=[0](cms), CN/C=[74], IA=[2.5](mm),
290 N=[3.0], TP=[4.45]hrs,
291 Continuous simulation parameters:
292 IaREcper=[4](hrs),
293 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
294 InterEventTime=[12](hrs)
295 Baseflow simulation parameters:
296 BaseFlowOption=[1] ,
297 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
298 VHydCond=[0.055](mm/hr), END=-1
299 *%-----|
300 CONTINUOUS NASHYD NHYD=["SW_5A2"], DT=[30]min, AREA=[20](ha),
301 DWF=[0](cms), CN/C=[81], IA=[2.5](mm),
302 N=[3.0], TP=[0.62]hrs,
303 Continuous simulation parameters:
304 IaREcper=[4](hrs),
305 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
306 InterEventTime=[12](hrs)
307 Baseflow simulation parameters:
308 BaseFlowOption=[1] ,
309 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
310 VHydCond=[0.055](mm/hr), END=-1
311 *%-----|
312 *#
313 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
314 *# of 1.61
315 *%-----|
316 CONTINUOUS NASHYD NHYD=["SW_5A1"], DT=[30]min, AREA=[1412](ha),
317 DWF=[0](cms), CN/C=[75], IA=[2.5](mm),
318 N=[3.0], TP=[8.00]hrs,
319 Continuous simulation parameters:
320 IaREcper=[4](hrs),
321 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
322 InterEventTime=[12](hrs)
323 Baseflow simulation parameters:
324 BaseFlowOption=[1] ,
325 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
326 VHydCond=[0.055](mm/hr), END=-1
327 *%-----|
328 CONTINUOUS NASHYD NHYD=["SW_4"], DT=[30]min, AREA=[585](ha),
329 DWF=[0](cms), CN/C=[81], IA=[2.5](mm),
330 N=[3.0], TP=[1.75]hrs,

```

```

331 Continuous simulation parameters:
332 IaREcper=[4](hrs),
333 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
334 InterEventTime=[12](hrs)
335 Baseflow simulation parameters:
336 BaseFlowOption=[1] ,
337 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
338 VHydCond=[0.055](mm/hr), END=-1
339 *%-----|
340 CONTINUOUS NASHYD NHYD=["LM_CK"], DT=[30]min, AREA=[1021](ha),
341 DWF=[0](cms), CN/C=[80], IA=[2.5](mm),
342 N=[3.0], TP=[2.46]hrs,
343 Continuous simulation parameters:
344 IaREcper=[4](hrs),
345 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
346 InterEventTime=[12](hrs)
347 Baseflow simulation parameters:
348 BaseFlowOption=[1] ,
349 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
350 VHydCond=[0.055](mm/hr), END=-1
351 *%-----|
352 CONTINUOUS NASHYD NHYD=["SW_2"], DT=[30]min, AREA=[177](ha),
353 DWF=[0](cms), CN/C=[77], IA=[2.5](mm),
354 N=[3.0], TP=[0.75]hrs,
355 Continuous simulation parameters:
356 IaREcper=[4](hrs),
357 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
358 InterEventTime=[12](hrs)
359 Baseflow simulation parameters:
360 BaseFlowOption=[1] ,
361 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
362 VHydCond=[0.055](mm/hr), END=-1
363 *%-----|
364 CONTINUOUS NASHYD NHYD=["SM_DR"], DT=[30]min, AREA=[1122](ha),
365 DWF=[0](cms), CN/C=[81], IA=[2.5](mm),
366 N=[3.0], TP=[3.25]hrs,
367 Continuous simulation parameters:
368 IaREcper=[4](hrs),
369 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
370 InterEventTime=[12](hrs)
371 Baseflow simulation parameters:
372 BaseFlowOption=[1] ,
373 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
374 VHydCond=[0.055](mm/hr), END=-1
375 *%-----|
376 CONTINUOUS NASHYD NHYD=["MO_DR"], DT=[30]min, AREA=[2737](ha),
377 DWF=[0](cms), CN/C=[76], IA=[2.5](mm),
378 N=[3.0], TP=[3.03]hrs,
379 Continuous simulation parameters:
380 IaREcper=[4](hrs),
381 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
382 InterEventTime=[12](hrs)
383 Baseflow simulation parameters:
384 BaseFlowOption=[1] ,
385 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
386 VHydCond=[0.055](mm/hr), END=-1
387 *%-----|
388 CONTINUOUS NASHYD NHYD=["SW_1"], DT=[30]min, AREA=[3176](ha),
389 DWF=[0](cms), CN/C=[78], IA=[2.5](mm),
390 N=[3.0], TP=[3.56]hrs,
391 Continuous simulation parameters:
392 IaREcper=[4](hrs),
393 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
394 InterEventTime=[12](hrs)
395 Baseflow simulation parameters:
396 BaseFlowOption=[1] ,

```



```

397          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
398          VHydCond=[0.055](mm/hr),   END=-1
399  *%-----|-----
400  *#
401  *# Routing hydrographs
402  *#
403  *# Starting with the addition of Jock River Headwater and Subwatershed 13
404  *#
405  ADD HYD          NHYDsum=["S_N13"], NHYDs to add=["JR_HW"+"SW_13"]
406  *%-----|-----
407  *#
408  *# Sum of hydrographs from Node 13 routed to Node 13A
409  *# (Approximated cross-section - see cross-section 258)
410  *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
411  *#
412  ROUTE CHANNEL    NHYDout=["N13A"], NHYDin=["S_N13"],
413                  RDT=[30](min),
414                  CHLGTH=[9074](m),  CHSLOPE=[0.0220](%),
415                  FPSLOPE=[0.0220](%),
416                  SECNUM=[1.0],      NSEG=[1]
417                  ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
418                  ( DISTANCE (m), ELEVATION (m))=
419                      [-40, 132.5]
420                      [-30, 132]
421                      [-25, 131.5]
422                      [-13, 130]
423                      [-8, 127.00]
424                      [-7, 126.50]
425                      [-6, 126]
426                      [-5.5, 125.50]
427                      [0, 123.75]
428                      [4.5, 125.50]
429                      [6, 126]
430                      [7.5, 126.5]
431                      [9, 127]
432                      [10, 127.5]
433                      [11.5, 128.0]
434                      [15.5, 129.5]
435  *%-----|-----
436  *#
437  *# Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
438  *#
439  ADD HYD          NHYDsum=["SN13A"], NHYDs to add=["N13A"+"JR_GWM"]
440  *%-----|-----
441  *#
442  *# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
443  *#
444  ROUTE RESERVOIR NHYDout=["RES_GM"], NHYDin=["SN13A"],
445                  RDT=[30](min),
446                  TABLE of ( OUTFLOW-STORAGE ) values
447                      (cms) - (ha-m)
448                      [ 0.0 , 0.0 ]
449                      [1.991, 2.144 ]
450                      [2.693, 39.826 ]
451                      [3.509, 81.697 ]
452                      [4.578, 318.774 ]
453                      [5.647, 594.947 ]
454                      [7.109, 910.219 ]
455                      [8.616, 1264.589 ]
456                      [10.371, 1658.057 ]
457                      [12.402, 2090.622 ]
458                      [22.056, 3462.487 ]
459                      [ -1 , -1 ] (max twenty pts)
460                  NHYDovf=[" " ],
461  *%-----|-----
462  *#

```

```

463 SAVE HYD          NHYD=["RES_GM"], # OF PCYCLES=[-1], ICASEsh=[-1]
464                   HYD_FILENAME=["H_RESGM"]
465                   HYD_COMMENT=["Outflow from Res GM"]
466 *%-----|-----
467 *# Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
468 *# (Approximated cross-section - see cross-section 258)
469 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
470 ROUTE CHANNEL     NHYDout=["N12"] ,NHYDin=["RES_GM"] ,
471                   RDT=[30](min),
472                   CHLGTH=[5926](m),  CHSLOPE=[0.0759](%),
473                                     FPSLOPE=[0.0759](%),
474                   SECNUM=[1.0],      NSEG=[1]
475                   ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
476                   ( DISTANCE (m), ELEVATION (m))=
477                     [-40, 132.5]
478                     [-30, 132]
479                     [-25, 131.5]
480                     [-13, 130]
481                     [-8, 127.00]
482                     [-7, 126.50]
483                     [-6, 126]
484                     [-5.5, 125.50]
485                     [0, 123.75]
486                     [4.5, 125.50]
487                     [6, 126]
488                     [7.5, 126.5]
489                     [9, 127]
490                     [10, 127.5]
491                     [11.5, 128.00]
492                     [15.5, 129.5]
493 *%-----|-----
494 *#
495 *# Addition of Subwatershed Jock River at Ashton to Node 12
496 *#
497 ADD HYD           NHYDsum=["S_N12"], NHYDs to add=["N12"+"JR_ASH"]
498 SAVE HYD         NHYD=["S_N12"], # OF PCYCLES=[-1], ICASEsh=[-1]
499                   HYD_FILENAME=["H_SN12"]
500                   HYD_COMMENT=["flow at S_N12 near Ashton"]
501 *%-----|-----
502 *#
503 *# Sum of hydrographs from Node 12 routed to Node 11
504 *# (Approximated cross-section - see cross-section 258)
505 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
506 ROUTE CHANNEL     NHYDout=["N11"] ,NHYDin=["S_N12"] ,
507                   RDT=[30](min),
508                   CHLGTH=[972](m),  CHSLOPE=[0.0514](%),
509                                     FPSLOPE=[0.0514](%),
510                   SECNUM=[1.0],      NSEG=[1]
511                   ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
512                   ( DISTANCE (m), ELEVATION (m))=
513                     [-40, 132.5]
514                     [-30, 132]
515                     [-25, 131.5]
516                     [-13, 130]
517                     [-8, 127.00]
518                     [-7, 126.50]
519                     [-6, 126]
520                     [-5.5, 125.50]
521                     [0, 123.75]
522                     [4.5, 125.50]
523                     [6, 126]
524                     [7.5, 126.5]
525                     [9, 127]
526                     [10, 127.5]
527                     [11.5, 128.00]
528                     [15.5, 129.5]

```



```

595  *#
596  *# Addition of Subwatershed 10 to Node 10
597  *#
598  ADD HYD          NHYDsum=["S_N10"], NHYDs to add=["N10"+"SW_10"]
599  *%-----|-----|
600  SAVE HYD        NHYD=["S_N10"], # OF PCYCLES=[-1], ICASEsh=[-1]
601                HYD_FILENAME=["H_SN10"]
602                HYD_COMMENT=["flow at S_N10: N10 + SW_10"]
603  *%-----|-----|
604  *# Addition of Kings Creek to S_N10
605  *#
606  ADD HYD          NHYDsum=["S_N10A"], NHYDs to add=["S_N10"+"KG_CK"]
607  *%-----|-----|
608  *#
609  *# Sum of hydrographs from Node 10 routed to Node 9
610  *# Section 2
611  *#
612  ROUTE CHANNEL   NHYDout=["N9"] ,NHYDin=["S_N10A"] ,
613                RDT=[30](min),
614                CHLGTH=[3982](m),  CHSLOPE=[0.0753](%),
615                FPSLOPE=[0.0753](%),
616                SECNUM=[1.0],      NSEG=[4]
617                ( SEGROUGH, SEGDIST (m))=
618                [0.04,-30.27
619                0.05,-18.42
620                -0.05,18.42
621                0.04,131.58] NSEG times
622                ( DISTANCE (m), ELEVATION (m))=
623                [-446.74, 106.00]
624                [-415.68, 105.50]
625                [-285.40, 105.00]
626                [-173.77, 104.50]
627                [-144.95, 104.00]
628                [-111.18, 103.50]
629                [-94.06, 103.00]
630                [-71.02, 102.50]
631                [-30.27, 102.00]
632                [-19.33, 100.00]
633                [-18.42, 99.50]
634                [18.42, 99.50]
635                [20.77, 100.00]
636                [27.93, 101.00]
637                [52.29, 101.00]
638                [68.80, 101.50]
639                [79.66, 103.00]
640                [91.50, 103.50]
641                [131.58, 104.00]
642  *%-----|-----|
643  *#
644  *# Addition of Subwatershed 9 and Nichols Creek to Node 9
645  *#
646  ADD HYD          NHYDsum=["S_N9"], NHYDs to add=["N9"+"SW_9"+"NC_CK"]
647  *%-----|-----|
648  *#
649  *# Sum of hydrographs from Node 9 routed to Node 8
650  *# Section 3
651  *#
652  ROUTE CHANNEL   NHYDout=["N8"] ,NHYDin=["S_N9"] ,
653                RDT=[30](min),
654                CHLGTH=[2269](m),  CHSLOPE=[0.0882](%),
655                FPSLOPE=[0.0882](%),
656                SECNUM=[1.0],      NSEG=[3]
657                ( SEGROUGH, SEGDIST (m))=
658                [0.1,-17.99
659                -0.045,17.31
660                0.1,456.58] NSEG times

```

```

661      ( DISTANCE (m), ELEVATION (m))=
662          [-201.19,100.50]
663          [-135.21, 100.00]
664          [-94.83, 99.50]
665          [-67.05, 99.00]
666          [-17.99, 98.50]
667          [-16.02, 98.00]
668          [-13.95, 97.50]
669          [13.95, 97.50]
670          [15.64, 98.00]
671          [17.31, 98.50]
672          [162.02, 98.50]
673          [172.89 ,99.00]
674          [314.38, 99.00]
675          [343.78, 99.50]
676          [365.67, 100.00]
677          [376.68, 100.00 ]
678          [393.11, 99.50]
679          [404.97, 99.50]
680          [431.70, 100.00]
681          [456.58, 100.50 ]
682  *%-----|-----|
683  *#
684  *# Addition of Subwatershed 8 and Hobb's Drain to Node 8
685  *#
686  ADD HYD          NHYDsum=["S_N8"], NHYDs to add=["N8"+"SW_8"+"HB_DR"]
687  *%-----|-----|
688  *#
689  *# Sum of hydrographs from Node 8 routed to Node 7
690  *# Section 4
691  *#
692  ROUTE CHANNEL    NHYDout=["N7"] ,NHYDin=["S_N8"],
693                  RDT=[30](min),
694                  CHLGTH=[3750](m),  CHSLOPE=[0.0533](%),
695                                          FPSLOPE=[0.0533](%),
696                  SECNUM=[1.0],        NSEG=[3]
697                  ( SEGROUGH, SEGDIST (m))=
698                      [0.12,-18.11
699                      -0.07,17.22
700                      0.12,590.05] NSEG times
701      ( DISTANCE (m), ELEVATION (m))=
702          [-433.21, 102.00]
703          [-425.34, 101.50]
704          [-377.56, 101.50]
705          [-366.23, 101.00]
706          [-202.60, 100.50]
707          [-96.25, 99.50]
708          [-68.36 99.00]
709          [-18.11, 98.50]
710          [-13.81, 97.50]
711          [13.81, 97.50]
712          [17.22, 98.50]
713          [161.95, 98.50]
714          [173.11, 99.00]
715          [314.05, 99.00]
716          [365.52, 100.00]
717          [404.70, 99.50]
718          [476.74, 100.50]
719          [502.31, 101.00]
720          [584.69, 101.00]
721          [585.79, 101.00]
722          [590.05, 102.00]
723  *%-----|-----|
724  *#
725  *# Addition of Subwatershed 7 to Node 7
726  *#

```



```

727 ADD HYD          NHYDsum=["S_N7"], NHYDs to add=["N7"+"SW_7"]
728 *%-----|-----|
729 SAVE HYD        NHYD=["S_N7"], # OF PCYCLES=[-1], ICASEsh=[-1]
730                HYD_FILENAME=["H_SN7"]
731                HYD_COMMENT=["flow at S_N7: N7 + SW_7"]
732 *%-----|-----|
733 *# Insertion of a reservoir to simulate the effects of the Richmond Fen.
734 *# Storage area and volumes were estimated from available topo maps.
735 *# Release rate from fen was assumed to be controlled by the downstream
736 *# river cross-section for summer conditions. It is was assumed that for up to
737 *# 0.75 m of water, the main channel of the river provided the storage. Above
738 *# this depth, the wetland starts to signigicantly store water.
739 *#
740 ROUTE RESERVOIR NHYDout=["RES_RF"] ,NHYDin=["S_N7"] ,
741                RDT=[30](min),
742                TABLE of ( OUTFLOW-STORAGE ) values
743                (cms) - (ha-m)
744                TABLE of ( OUTFLOW-STORAGE ) values
745                (cms) - (ha-m)
746                [ 0.0 , 0.0 ]
747                [0.9051, 2.40]
748                [2.907, 4.13]
749                [9.744, 9.18]
750                [20.304, 14.96]
751                [34.167, 310.21]
752                [74.993, 605.46]
753                [104.876, 900.71]
754                [140.56, 2892.00]
755                [225.00, 3615.63]
756                [ -1 , -1 ] (max twenty pts)
757                NHYDovf=[" " ] ,
758 *%-----|-----|
759 SAVE HYD        NHYD=["RES_RF"], # OF PCYCLES=[-1], ICASEsh=[-1]
760                HYD_FILENAME=["H_ResRF"]
761                HYD_COMMENT=["outflow of Richmond Fen"]
762 *%-----|-----|
763 *#
764 *# Sum of hydrographs from Node 7 routed to Node 6
765 *# Section 5
766 *#
767 ROUTE CHANNEL   NHYDout=["N6"] ,NHYDin=["RES_RF"] ,
768                RDT=[30](min),
769                CHLGTH=[3056](m), CHSLOPE=[0.0818](%),
770                FPSLOPE=[0.0818](%),
771                SECNUM=[1.0], NSEG=[5]
772                ( SEGROUGH,SEGDIST (m))=
773                [0.025,-70.8
774                0.1,-23.9
775                -0.05,23.9
776                0.06,39.8
777                0.05,96.3] NSEG times
778                ( DISTANCE (m), ELEVATION (m))=
779                [-100.8, 97.00]
780                [-70.8, 96.50]
781                [-52.0, 96.00]
782                [-35.1, 95.50]
783                [-30.6, 95.00]
784                [-23.9, 94.54]
785                [23.9, 94.54]
786                [39.8, 95.00]
787                [50.4, 95.50]
788                [93.5, 96.00]
789                [94.9, 96.50]
790                [96.3, 97.00]
791 *%-----|-----|
792 *#

```

```

793  *# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
794  *#
795  ADD HYD                NHYDsum=["S_N6"], NHYDs to add=["N6"+"SW_6"+"VG_DR"]
796  *%-----|-----
797  *#
798  *# Sum of hydrographs from Node 6 routed to Node 5
799  *# Section 6
800  *#
801  ROUTE CHANNEL          NHYDout=["N5"] ,NHYDin=["S_N6"] ,
802                          RDT=[30](min),
803                          CHLGTH=[1852](m),  CHSLOPE=[0.0540](%),
804                                          FPSLOPE=[0.0540](%),
805                          SECNUM=[1.0],      NSEG=[3]
806                          ( SEGROUGH, SEGDIST (m))=
807                          [0.035,-131.59
808                          -0.045,48.96
809                          0.1,239.04] NSEG times
810                          ( DISTANCE (m), ELEVATION (m))=
811                          [-686.30, 94.50]
812                          [-675.70, 94.00]
813                          [-492.52, 93.00]
814                          [-467.28, 94.00]
815                          [-131.59, 94.00]
816                          [-92.79, 92.50]
817                          [-18.06, 91.00]
818                          [18.06, 91.00]
819                          [43.47, 92.50]
820                          [48.96, 94.00]
821                          [177.43, 94.00]
822                          [239.04,94.50]
823  *%-----|-----
824  *#
825  *# Addition of Subwatershed 5 and Flowing Creek to Node 5
826  *#
827  ADD HYD                NHYDsum=["S_N5"], NHYDs to add=["N5"+"SW_5"+"FL_CK"]
828  *%-----|-----
829  *#
830  *# Sum of hydrographs from Node 5 routed to Node 5A
831  *# Section 7
832  *#
833  ROUTE CHANNEL          NHYDout=["N5A"] ,NHYDin=["S_N5"] ,
834                          RDT=[30](min),
835                          CHLGTH=[556](m),  CHSLOPE=[0.0900](%),
836                                          FPSLOPE=[0.0900](%),
837                          SECNUM=[1.0],      NSEG=[4]
838                          ( SEGROUGH, SEGDIST (m))=
839                          [0.04,-41.5
840                          0.1,-14.0
841                          -0.045,14.0
842                          0.1,41.1] NSEG times
843                          ( DISTANCE (m), ELEVATION (m))=
844                          [-275.8, 93.00]
845                          [-248.6, 92.50]
846                          [-237.0, 92.00]
847                          [-219.3, 91.50]
848                          [-202.1, 91.50]
849                          [-186.0, 92.00]
850                          [-129.2, 92.00]
851                          [-117.6, 91.50]
852                          [-100.6, 91.00]
853                          [-41.5, 91.00]
854                          [-20.0, 91.00]
855                          [-14.0, 90.54]
856                          [14.0, 90.54]
857                          [15.3, 91.00]
858                          [17.3, 91.50]

```

```

859                                     [38.4, 92.00]
860                                     [39.8, 92.50]
861                                     [41.1, 93.00]
862 *%-----|-----
863 *#
864 *# Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
865 *#
866 ADD HYD                NHYDsum=["S_N5A"], NHYDs to add=["N5A"+"SW_5A2"+"SW_5A1"]
867 *%-----|-----
868 *#
869 *# Sum of hydrographs from Node 5A routed to Node 4
870 *# Section 8
871 *#
872 ROUTE CHANNEL        NHYDout=["N4"] ,NHYDin=["S_N5A"] ,
873                          RDT=[30](min),
874                          CHLGTH=[4630](m),  CHSLOPE=[0.0432](%),
875                          FPSLOPE=[0.0432](%),
876                          SECNUM=[1.0],      NSEG=[3]
877                          ( SEGROUGH, SEGDIST (m))=
878                          [0.05,-28.2
879                          -0.035,28.2
880                          0.05,173.1] NSEG times
881                          ( DISTANCE (m), ELEVATION (m))=
882                                     [-38.9, 92.00]
883                                     [-35.8, 91.50]
884                                     [-33.3, 91.00]
885                                     [-28.2, 90.50]
886                                     [-15.0, 87.48]
887                                     [-5.0, 88.34]
888                                     [5.0, 86.20]
889                                     [15.0, 88.55]
890                                     [28.2, 90.50]
891                                     [29.7, 91.00]
892                                     [46.5, 91.00]
893                                     [127.8, 91.00]
894                                     [148.7, 91.50]
895                                     [173.1, 92.00]
896 *%-----|-----
897 *#
898 *# Addition of Subwatershed 4 and Leamy Creek to Node 4
899 *#
900 ADD HYD                NHYDsum=["S_N4"], NHYDs to add=["N4"+"SW_4"+"LM_CK"]
901 SAVE HYD              NHYD=["S_N4"], # OF PCYCLES=[-1], ICASEsh=[1]
902                          HYD_COMMENT=["flow at S_N4"]
903 *%-----|-----
904 *#
905 *# Sum of hydrographs from Node 4 routed to Node 2
906 *# Section 9
907 *#
908 ROUTE CHANNEL        NHYDout=["N2"] ,NHYDin=["S_N4"] ,
909                          RDT=[30](min),
910                          CHLGTH=[1667](m),  CHSLOPE=[0.0600](%),
911                          FPSLOPE=[0.0600](%),
912                          SECNUM=[1.0],      NSEG=[4]
913                          ( SEGROUGH, SEGDIST (m))=
914                          [0.1,-28.0
915                          -0.04,28.4
916                          0.06,31.7
917                          0.04,80.2] NSEG times
918                          ( DISTANCE (m), ELEVATION (m))=
919                                     [-36.3, 92.00]
920                                     [-32.6, 91.50]
921                                     [-30.2, 91.00]
922                                     [-28.0, 90.45]
923                                     [-15.0, 87.48]
924                                     [-5.0, 88.34]

```

```

925             [5.0, 86.20]
926             [15.0, 88.55]
927             [28.0, 90.45]
928             [28.4, 90.50]
929             [30.4, 91.00]
930             [31.7, 91.50]
931             [80.2, 92.00]
932 *%-----|-----
933 *#
934 *# Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2
935 *#
936 ADD HYD           NHYDsum=["S_N2"], NHYDs to add=["N2"+"SW_2"+"SM_DR"+"MO_DR"]
937 *%-----|-----
938 SAVE HYD         NHYD=["S_N2"], # OF PCYCLES=[-1], ICASEsh=[-1]
939                   HYD_FILENAME=["H_SN2"]
940                   HYD_COMMENT=["flow at S_N2 Jock River Gauge at Moodie Dr."]
941 *%-----|-----
942 *#
943 *# Sum of hydrographs from Node 2 routed to Node 1
944 *# Section 10
945 *#
946 ROUTE CHANNEL   NHYDout=["N1"] ,NHYDin=["S_N2"] ,
947                   RDT=[30](min),
948                   CHLGTH=[10046](m),  CHSLOPE=[0.0498](%),
949                                           FPSLOPE=[0.0498](%),
950                   SECNUM=[1.0],      NSEG=[5]
951                   ( SEGROUGH, SEGDIST (m))=
952                     [0.04,-27.6
953                     0.06,-15.0
954                     -0.045,15.0
955                     0.06,25.4
956                     0.04,122.6] NSEG times
957                   ( DISTANCE (m), ELEVATION (m))=
958                     [-87.0, 91.50]
959                     [-32.4, 91.00]
960                     [-27.6, 90.50]
961                     [-25.0, 90.00]
962                     [-22.9, 89.57]
963                     [-15.0, 86.20]
964                     [-5.0, 84.83]
965                     [5.0, 84.83]
966                     [15.0, 88.11]
967                     [22.9, 89.57]
968                     [25.4, 90.00]
969                     [27.9, 90.50]
970                     [38.0, 91.00]
971                     [112.5, 91.00]
972                     [114.3, 90.50]
973                     [115.1, 90.26]
974                     [116.3, 90.50]
975                     [119.0, 91.00]
976                     [121.0, 91.50]
977                     [122.6, 92.00]
978 *%-----|-----
979 *#
980 *# Addition of Subwatershed 1 to Node 1
981 *#
982 ADD HYD           NHYDsum=["N1"], NHYDs to add=["N1"+"SW_1"]
983 SAVE HYD         NHYD=["N1"], # OF PCYCLES=[-1], ICASEsh=[1]
984                   HYD_COMMENT=["total outflow of Jock River"]
985 *%-----|-----
986 *#####
987 *% 5 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
988 START           TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[5]
989 *%               ["C24SC005.stm"] <--storm filename, one per line for NSTORM time
990 *%-----|-----

```

```
991  *% 10 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
992  START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[10]
993  *%              ["C24SC010.stm"] <--storm filename, one per line for NSTORM time
994  *%-----|-----|
995  *% 25 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
996  START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[25]
997  *%              ["C24SC025.stm"] <--storm filename, one per line for NSTORM time
998  *%-----|-----|
999  *% 50 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
1000 START         TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[50]
1001 *%              ["C24SC050.stm"] <--storm filename, one per line for NSTORM time
1002 *%-----|-----|
1003 *% 100 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
1004 START         TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
1005 *%              ["C24SC100.stm"] <--storm filename, one per line for NSTORM time
1006 FINISH
1007
```



```

00001 *****
00002 *****
00003 SSSSS W M M M H H Y Y M M O O 222 000 11 5555 *****
00004 S W M M M T T M M M O O 2 0 0 11 5 *****
00005 SSSSS W M M M H H H H Y Y M M M O 2 0 0 11 5 Ver 5.800 *****
00006 S W M M M H H Y Y M M O O 222 0 0 11 555 PRE 20.0 *****
00007 SSSSS W M M M M M M O O 2 0 0 11 5 *****
00008 *****
00009 Stormwater Management Hydrologic Model *****
00010 *****
00011 *****
00012 ***** SWHYMO Ver 5.800 *****
00013 ***** A single event and continuous hydrologic simulation model *****
00014 ***** based on the principles of HMO and its successors *****
00015 ***** OTTHMO-83 and OTTHMO-89 *****
00016 ***** *****
00017 ***** Distributed by: J.F. Sabourin and Associates Inc. *****
00018 ***** Ottawa, Ontario: (613) 886-8884 *****
00019 ***** Gatineau, Quebec: (819) 243-8888 *****
00020 ***** E-Mail: swhymo@jfsa.com *****
00021 ***** *****
00022 *****
00023 *****
00024 ***** Licensed user: JFSaInc. *****
00025 ***** SERIAL#:2549237 *****
00026 ***** *****
00027 *****
00028 *****
00029 ***** ***** PROGRAM ARRAY DIMENSIONS *****
00030 ***** *****
00031 ***** Maximum value for ID numbers : 11 *****
00032 ***** Max. number of rainfall points: 105408 *****
00033 ***** Max. number of flow points : 105408 *****
00034 *****
00035 *****
00036 ***** S U M M A R Y O U T P U T *****
00037 ***** *****
00038 ***** RUN DATE: 2021-02-22 TIME: 15:43:08 RUN COUNTER: 00199 *****
00039 ***** Input file: T:\PROJ\1474-16\Design\20201026-QuantityControlAnalysis\SWHYMO\SMR-Model\summe *****
00040 ***** *****
00041 ***** DAT *****
00042 ***** *****
00043 ***** Output file: T:\PROJ\1474-16\Design\20201026-QuantityControlAnalysis\SWHYMO\SMR-Model\summe *****
00044 ***** *****
00045 ***** Summary file: T:\PROJ\1474-16\Design\20201026-QuantityControlAnalysis\SWHYMO\SMR-Model\summe *****
00046 ***** *****
00047 ***** * 1 *****
00048 ***** * 2 *****
00049 ***** * 3 *****
00050 ***** *****
00051 *****
00052 *****
00053 ***** *****
00054 ***** SWHYMO Ver 5.800 SWHYMO INPUT DATA FILE *****
00055 ***** *****
00056 ***** Project Name: [Jock River] Project Number: (411-02) *****
00057 ***** Date : 06-06-2003 *****
00058 ***** Modeller : [JOP] *****
00059 ***** Company : JFSaInc. *****
00060 ***** License # : 2549237 *****
00061 ***** *****
00062 ***** CALIBRATION OF SUMMER MODEL PARAMETERS *****
00063 ***** *****
00064 ***** USING CONTINUOUS SIMULATIONS *****
00065 ***** Rainfall data from OPER rain gauge installed at site + other gauges by the City *****
00066 ***** Use data collected from May list to July 14, 2003 *****
00067 ***** *****
00068 ***** ** END OF RUN : 1 *****
00069 ***** *****
00070 *****
00071 *****
00072 *****
00073 *****
00074 *****
00075 ***** RUN COMMANDS *****
00076 ***** R0002:C0001 *****
00077 ***** START *****
00078 ***** [TZERO = .00 hrs on 0] *****
00079 ***** [MFORM = 2 (1=imperial, 2=metric output)] *****
00080 ***** [SMIN = 0] *****
00081 ***** [SMIN = 0002] *****
00082 ***** *****
00083 ***** SWHYMO Ver 5.800 SWHYMO INPUT DATA FILE *****
00084 ***** *****
00085 ***** Project Name: [Jock River] Project Number: (411-02) *****
00086 ***** Date : 06-06-2003 *****
00087 ***** Modeller : [JOP] *****
00088 ***** Company : JFSaInc. *****
00089 ***** License # : 2549237 *****
00090 ***** *****
00091 ***** CALIBRATION OF SUMMER MODEL PARAMETERS *****
00092 ***** *****
00093 ***** USING CONTINUOUS SIMULATIONS *****
00094 ***** Rainfall data from OPER rain gauge installed at site + other gauges by the City *****
00095 ***** Use data collected from May list to July 14, 2003 *****
00096 ***** *****
00097 ***** R0002:C0002 *****
00098 ***** HEAD STATION *****
00099 ***** Filename = storm.001 *****
00100 ***** Comment = Plus CCS de 24 hrs l=2 ans pour Ottawa CMA *****
00101 ***** [SFP=10.00] SUM = 24.00 [PROT = 45.51] *****
00102 ***** R0002:C0003 *****
00103 ***** [SFACT = 1.00] [TSHTF = 96.00 min] *****
00104 ***** [S12=10.00] [S20=10.00] [PROT = 45.51] *****
00105 ***** R0002:C0004 *****
00106 ***** COMPUTE API *****
00107 ***** [APIMax = 50.00] [APIDiv = 8500] [APIDiv = 9989] *****
00108 ***** [APIMax = 80.12] [APIDiv = 56.74] [APIMin = 44.87] *****
00109 ***** *****
00110 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00111 ***** of 1.5 *****
00112 ***** R0002:C0005 *****
00113 ***** CONTINUOUS NASHVD 30.0 01:30:00 3680.0 6.065 NoDate 37:00 11.44 251.000 *****
00114 ***** [Cm = 6.0] N = 3.00 Tp = 3.75 *****
00115 ***** [IAREC = 4.00] SMIN = 57.05 SMAX = 380.32 [EK = 0.10] *****
00116 ***** [InterEventTime = 12.00] *****
00117 ***** *****
00118 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00119 ***** of 1.5 *****
00120 ***** R0002:C0006 *****
00121 ***** CONTINUOUS NASHVD 30.0 01:30:00 3791.00 2.154 NoDate 32:30 10.72 236.000 *****
00122 ***** [Cm = 6.0] N = 3.00 Tp = 3.75 *****
00123 ***** [IAREC = 4.00] SMIN = 57.05 SMAX = 430.01 [EK = 0.10] *****
00124 ***** [InterEventTime = 12.00] *****
00125 ***** *****
00126 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00127 ***** of 1.5 *****
00128 ***** R0002:C0007 *****
00129 ***** CONTINUOUS NASHVD 30.0 01:30:00 3074.00 3.115 NoDate 39:30 9.41 207.000 *****
00130 ***** [Cm = 5.0] N = 3.00 Tp = 3.00 *****
00131 ***** [IAREC = 4.00] SMIN = 83.24 SMAX = 554.96 [EK = 0.10] *****
00132 ***** [InterEventTime = 12.00] *****
00133 ***** R0002:C0008 *****
00134 ***** CONTINUOUS NASHVD 30.0 01:30:00 1781.00 5.417 NoDate 32:30 13.91 306.000 *****
00135 ***** [Cm = 72.0] N = 3.00 Tp = 3.21 *****
00136 ***** [IAREC = 4.00] SMIN = 39.75 SMAX = 264.99 [EK = 0.10] *****
00137 ***** [InterEventTime = 12.00] *****
00138 ***** R0002:C0009 *****
00139 ***** CONTINUOUS NASHVD 30.0 01:30:00 500.00 2.663 NoDate 29:00 11.95 263.000 *****
00140 ***** [Cm = 66.0] N = 3.00 Tp = 3.24 *****
00141 ***** [IAREC = 4.00] SMIN = 52.62 SMAX = 350.79 [EK = 0.10] *****
00142 ***** [InterEventTime = 12.00] *****
00143 ***** *****
00144 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00145 ***** of 1.5 *****
00146 ***** R0002:C0010 *****
00147 ***** CONTINUOUS NASHVD 30.0 01:30:00 1937.00 3.966 NoDate 34:30 11.95 263.000 *****
00148 ***** [Cm = 66.0] N = 3.00 Tp = 3.24 *****
00149 ***** [IAREC = 4.00] SMIN = 52.62 SMAX = 350.79 [EK = 0.10] *****
00150 ***** [InterEventTime = 12.00] *****
00151 ***** *****
00152 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00153 ***** of 1.5 *****
00154 ***** R0002:C0011 *****
00155 ***** CONTINUOUS NASHVD 30.0 01:30:00 5666.00 10.936 NoDate 38:00 13.91 306.000 *****
00156 ***** [Cm = 72.0] N = 3.00 Tp = 3.00 *****
00157 ***** [IAREC = 4.00] SMIN = 39.75 SMAX = 264.99 [EK = 0.10] *****
00158 ***** [InterEventTime = 12.00] *****
00159 ***** *****
00160 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00161 ***** of 1.5 *****
00162 ***** R0002:C0012 *****
00163 ***** CONTINUOUS NASHVD 30.0 01:30:00 8376.00 10.656 NoDate 39:30 11.95 263.000 *****
00164 ***** [Cm = 66.0] N = 3.00 Tp = 3.24 *****
00165 ***** [IAREC = 4.00] SMIN = 52.62 SMAX = 350.79 [EK = 0.10] *****
00166 ***** [InterEventTime = 12.00] *****
00167 ***** *****
00168 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00169 ***** of 1.5 *****
00170 ***** R0002:C0013 *****
00171 ***** CONTINUOUS NASHVD 30.0 01:30:00 1937.00 3.966 NoDate 34:30 11.95 263.000 *****
00172 ***** [Cm = 70.0] N = 3.00 Tp = 2.51 *****
00173 ***** [IAREC = 4.00] SMIN = 52.62 SMAX = 287.10 [EK = 0.10] *****
00174 ***** [InterEventTime = 12.00] *****
00175 ***** *****
00176 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00177 ***** of 1.5 *****
00178 ***** R0002:C0014 *****
00179 ***** CONTINUOUS NASHVD 30.0 01:30:00 4464.00 5.312 NoDate 39:30 10.96 241.000 *****
00180 ***** [Cm = 60.0] N = 3.00 Tp = 11.32 *****
00181 ***** [IAREC = 4.00] SMIN = 6.00 SMAX = 412.66 [EK = 0.10] *****
00182 ***** [InterEventTime = 12.00] *****
00183 ***** *****
00184 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00185 ***** of 1.5 *****
00186 ***** R0002:C0015 *****
00187 ***** CONTINUOUS NASHVD 30.0 01:30:00 131.00 2.770 NoDate 28:30 11.20 246.000 *****

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00188 ***** [Cm = 63.0] N = 3.00 Tp = .90 *****
00189 ***** [IAREC = 4.00] SMIN = 52.62 SMAX = 396.11 [EK = 0.10] *****
00190 ***** [InterEventTime = 12.00] *****
00191 ***** *****
00192 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00193 ***** of 1.0 *****
00194 ***** R0002:C0016 *****
00195 ***** CONTINUOUS NASHVD 30.0 01:30:00 3854.00 6.083 NoDate 38:30 11.95 263.000 *****
00196 ***** [Cm = 66.0] N = 3.00 Tp = 8.42 *****
00197 ***** [IAREC = 4.00] SMIN = 52.62 SMAX = 350.79 [EK = 0.10] *****
00198 ***** [InterEventTime = 12.00] *****
00199 ***** *****
00200 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00201 ***** of 1.5 *****
00202 ***** R0002:C0017 *****
00203 ***** CONTINUOUS NASHVD 30.0 01:30:00 3197.00 4.957 NoDate 36:30 9.93 216.000 *****
00204 ***** [Cm = 57.0] N = 3.00 Tp = 6.65 *****
00205 ***** [IAREC = 4.00] SMIN = 76.32 SMAX = 508.81 [EK = 0.10] *****
00206 ***** [InterEventTime = 12.00] *****
00207 ***** *****
00208 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00209 ***** of 1.75 *****
00210 ***** R0002:C0018 *****
00211 ***** CONTINUOUS NASHVD 30.0 01:30:00 165.00 4.07 NoDate 33:00 12.21 268.000 *****
00212 ***** [Cm = 67.0] N = 3.00 Tp = 4.38 *****
00213 ***** [IAREC = 4.00] SMIN = 30.55 SMAX = 336.97 [EK = 0.10] *****
00214 ***** [InterEventTime = 12.00] *****
00215 ***** *****
00216 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00217 ***** of 1.6 *****
00218 ***** R0002:C0019 *****
00219 ***** CONTINUOUS NASHVD 30.0 01:30:00 1332.00 3.083 NoDate 39:00 13.91 306.000 *****
00220 ***** [Cm = 70.0] N = 3.00 Tp = 5.81 *****
00221 ***** [IAREC = 4.00] SMIN = 39.75 SMAX = 264.99 [EK = 0.10] *****
00222 ***** [InterEventTime = 12.00] *****
00223 ***** R0002:C0020 *****
00224 ***** CONTINUOUS NASHVD 30.0 01:30:00 224.00 2.527 NoDate 28:30 15.88 349.000 *****
00225 ***** [Cm = 77.0] N = 3.00 Tp = .75 *****
00226 ***** [IAREC = 4.00] SMIN = 31.15 SMAX = 207.66 [EK = 0.10] *****
00227 ***** [InterEventTime = 12.00] *****
00228 ***** *****
00229 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00230 ***** of 1.20 *****
00231 ***** R0002:C0021 *****
00232 ***** CONTINUOUS NASHVD 30.0 01:30:00 4945.00 14.878 NoDate 33:00 14.94 319.000 *****
00233 ***** [Cm = 74.0] N = 3.00 Tp = 4.45 *****
00234 ***** [IAREC = 4.00] SMIN = 30.55 SMAX = 244.49 [EK = 0.10] *****
00235 ***** [InterEventTime = 12.00] *****
00236 ***** *****
00237 ***** R0002:C0022 *****
00238 ***** CONTINUOUS NASHVD 30.0 01:30:00 20.00 2.87 NoDate 28:30 17.76 390.000 *****
00239 ***** [Cm = 81.0] N = 3.00 Tp = .62 *****
00240 ***** [IAREC = 4.00] SMIN = 32.44 SMAX = 168.09 [EK = 0.10] *****
00241 ***** [InterEventTime = 12.00] *****
00242 ***** *****
00243 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00244 ***** of 1.61 *****
00245 ***** R0002:C0023 *****
00246 ***** CONTINUOUS NASHVD 30.0 01:30:00 1412.00 3.007 NoDate 38:00 15.19 334.000 *****
00247 ***** [Cm = 74.0] N = 3.00 Tp = 4.85 *****
00248 ***** [IAREC = 4.00] SMIN = 33.81 SMAX = 225.43 [EK = 0.10] *****
00249 ***** [InterEventTime = 12.00] *****
00250 ***** R0002:C0024 *****
00251 ***** CONTINUOUS NASHVD 30.0 01:30:00 585.00 4.232 NoDate 29:30 17.76 390.000 *****
00252 ***** [Cm = 81.0] N = 3.00 Tp = .75 *****
00253 ***** [IAREC = 4.00] SMIN = 25.21 SMAX = 168.09 [EK = 0.10] *****
00254 ***** [InterEventTime = 12.00] *****
00255 ***** R0002:C0025 *****
00256 ***** CONTINUOUS NASHVD 30.0 01:30:00 1021.00 5.667 NoDate 30:30 17.36 382.000 *****
00257 ***** [Cm = 80.0] N = 3.00 Tp = 2.46 *****
00258 ***** [IAREC = 4.00] SMIN = 26.32 SMAX = 175.50 [EK = 0.10] *****
00259 ***** [InterEventTime = 12.00] *****
00260 ***** R0002:C0026 *****
00261 ***** CONTINUOUS NASHVD 30.0 01:30:00 177.00 1.996 NoDate 28:30 15.88 349.000 *****
00262 ***** [Cm = 77.0] N = 3.00 Tp = .75 *****
00263 ***** [IAREC = 4.00] SMIN = 31.15 SMAX = 207.66 [EK = 0.10] *****
00264 ***** [InterEventTime = 12.00] *****
00265 ***** R0002:C0027 *****
00266 ***** CONTINUOUS NASHVD 30.0 01:30:00 5.257 NoDate 33:30 17.76 390.000 *****
00267 ***** [Cm = 81.0] N = 3.00 Tp = 3.25 *****
00268 ***** [IAREC = 4.00] SMIN = 33.81 SMAX = 168.09 [EK = 0.10] *****
00269 ***** [InterEventTime = 12.00] *****
00270 ***** R0002:C0028 *****
00271 ***** CONTINUOUS NASHVD 30.0 01:30:00 3737.00 11.338 NoDate 33:30 15.93 341.000 *****
00272 ***** [Cm = 76.0] N = 3.00 Tp = 3.03 *****
00273 ***** [IAREC = 4.00] SMIN = 32.44 SMAX = 216.39 [EK = 0.10] *****
00274 ***** [InterEventTime = 12.00] *****
00275 ***** R0002:C0029 *****
00276 ***** CONTINUOUS NASHVD 30.0 01:30:00 4651.00 7.713 NoDate 39:30 11.29 n/a *****
00277 ***** [Cm = 78.0] N = 3.00 Tp = 3.56 *****
00278 ***** [IAREC = 4.00] SMIN = 39.49 SMAX = 199.22 [EK = 0.10] *****
00279 ***** [InterEventTime = 12.00] *****
00280 ***** Routing hydrographs *****
00281 ***** *****
00282 ***** Starting with the addition of Jock River Headwater and Subwatershed 13 *****
00283 ***** *****
00284 ***** R0002:C0030 *****
00285 ***** ADD HYD 30.0 02:18:30 3680.00 6.065 NoDate 37:00 11.44 n/a *****
00286 ***** [L/S = 9074. / .024 / 040] *****
00287 ***** [SFP=30.00] SUM = 30.0 02:18:30 971.00 2.154 NoDate 32:30 10.72 n/a *****
00288 ***** [L/S = 9074. / .024 / 040] *****
00289 ***** Sum of hydrographs from Node 13 routed to Node 13A *****
00290 ***** [Approximated cross-section - see cross-section 258] *****
00291 ***** [Use n=0.04 for summer conditions and n=0.025 for spring conditions] *****
00292 ***** *****
00293 ***** R0002:C0031 *****
00294 ***** ROUTE CHANNEL 30.0 02:18:30 4651.00 7.713 NoDate 39:30 11.29 n/a *****
00295 ***** [SFP=30.00] out = 30.0 01:30:13A 4651.00 6.154 NoDate 39:30 11.29 n/a *****
00296 ***** [L/S = 9074. / .024 / 040] *****
00297 ***** [Vmax = 427] [Dmax = 2.537] *****
00298 ***** *****
00299 ***** Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A *****
00300 ***** *****
00301 ***** R0002:C0032 *****
00302 ***** ADD HYD 30.0 02:18:30 4651.00 6.154 NoDate 39:30 11.29 n/a *****
00303 ***** [L/S = 9074. / .024 / 040] *****
00304 ***** [SFP=30.00] SUM = 30.0 01:30:13A 7725.00 9.269 NoDate 39:30 10.54 n/a *****
00305 ***** [L/S = 9074. / .024 / 040] *****
00306 ***** Insertion of a reservoir to simulate the effects of the Goodwood Marsh *****
00307 ***** *****
00308 ***** R0002:C0033 *****
00309 ***** ROUTE RESERVOIR 30.0 02:18:30 7725.00 9.269 NoDate 39:30 10.54 n/a *****
00310 ***** [L/S = 9074. / .024 / 040] *****
00311 ***** [NstUsed = 34988 = 02 m] *****
00312 ***** *****
00313 ***** R0002:C0034 *****
00314 ***** SAVE HYD 30.0 01:30:00 7725.00 2.603 NoDate 55:30 10.54 n/a *****
00315 ***** [L/S = 9074. / .024 / 040] *****
00316 ***** remark: Outflow from Res CM *****
00317 ***** Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12 *****
00318 ***** [Approximated cross-section - see cross-section 258] *****
00319 ***** [Use n=0.04 for summer conditions and n=0.025 for spring conditions] *****
00320 ***** R0002:C0035 *****
00321 ***** ROUTE CHANNEL 30.0 02:18:30 7725.00 2.603 NoDate 55:30 10.54 n/a *****
00322 ***** [SFP=30.00] out = 30.0 02:18:12 7725.00 2.594 NoDate 58:00 10.54 n/a *****
00323 ***** [L/S = 926. / .076 / 040] *****
00324 ***** [Vmax = 501] [Dmax = 1.326] *****
00325 ***** *****
00326 ***** Addition of Subwatershed Jock River at Ashton to Node 12 *****
00327 ***** *****
00328 ***** R0002:C0036 *****
00329 ***** ADD HYD 30.0 02:18:30 1781.00 5.417 NoDate 32:30 13.91 n/a *****
00330 ***** [L/S = 9074. / .024 / 040] *****
00331 ***** [SFP=30.00] SUM = 30.0 01:30:12 9506.00 7.371 NoDate 30:30 11.17 n/a *****
00332 ***** [L/S = 9074. / .024 / 040] *****
00333 ***** SAVE HYD 30.0 01:30:12 9506.00 7.371 NoDate 32:30 11.17 n/a *****
00334 ***** [L/S = 9074. / .024 / 040] *****
00335 ***** remark: flow at S_12 near Ashton *****
00336 ***** *****
00337 ***** Sum of hydrographs from Node 12 routed to Node 11 *****
00338 ***** [Approximated cross-section - see cross-section 258] *****
00339 ***** [Use n=0.04 for summer conditions and n=0.025 for spring conditions] *****
00340 ***** R0002:C0038 *****
00341 ***** ROUTE CHANNEL 30.0 02:18:12 9506.00 7.371 NoDate 32:30 11.17 n/a *****
00342 ***** [SFP=30.00] out = 30.0 01:30:11 9506.00 7.317 NoDate 33:00 11.17 n/a *****
00343 ***** [L/S = 972. / .051 / 040] *****
00344 ***** [Vmax = 589] [Dmax = 2.119] *****
00345 ***** *****
00346 ***** Sum of hydrographs from Node 12 routed to Node 11 with dummy section 248 *****
00347 ***** *****
00348 ***** R0002:C0039 *****
00349 ***** ROUTE CHANNEL 30.0 02:18:12 9506.00 7.371 NoDate 32:30 11.17 n/a *****
00350 ***** [SFP=30.00] out = 30.0 01:30:11 9506.00 7.320 NoDate 39:30 11.23 n/a *****
00351 ***** [L/S = 972. / .051 / 040] *****
00352 ***** [Vmax = 589] [Dmax = 2.098] *****
00353 ***** *****
00354 ***** Addition of Subwatershed 11 and No Name Creek to Node 11 *****
00355 ***** *****
00356 ***** R0002:C0040 *****
00357 ***** ADD HYD 30.0 02:18:12 9506.00 7.320 NoDate 39:30 11.17 n/a *****
00358 ***** [L/S = 972. / .051 / 040] *****
00359 ***** [SFP=30.00] SUM = 30.0 02:18:12 1937.00 3.966 NoDate 34:30 11.95 n/a *****
00360 ***** [L/S = 972. / .051 / 040] *****
00361 ***** [Vmax = 589] [Dmax = 2.098] *****
00362 ***** *****
00363 ***** Sum of hydrographs from Node 11 routed to Node 10 *****
00364 ***** Section 1 *****
00365 ***** R0002:C0041 *****
00366 ***** ROUTE CHANNEL 30.0 02:18:11 11923.00 11.215 NoDate 33:00 11.33 n/a *****
00367 ***** [SFP=30.00] out = 30.0 01:30:10 11923.00 11.215 NoDate 39:30 11.33 n/a *****
00368 ***** [L/S = 14028. / .157 / 040] *****
00369 ***** [Vmax = 460] [Dmax = .881] *****
00370 ***** *****
00371 ***** Addition of Subwatershed 10 to Node 10 *****
00372 ***** *****
00373 ***** R0002:C0042 *****
00374 ***** ADD HYD 30.0 02:18:10 11923.00 8.216 NoDate 39:30 11.33 n/a *****

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00375# + 30.0 02:SW_10 5666.00 10.936 No.Date 38:00 13.91 n/a .000
00376# ROUTE CHANNEl -> 30.0 02:SW_10 17859.00 19.098 No.Date 38:30 12.16 n/a .000
00377# R0002:CO0043 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00378# SAVE HYD 30.0 01:R_N10 17859.00 19.098 No.Date 38:30 12.16 n/a .000
00379# frame_H_N10
00380# remark:flow at @_N10: N10 + SW_10
00381# Addition of Kings Creek @ S212
00382#
00383# R0002:CO0044 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00384# ADD HYD 30.0 02:SW_10 17859.00 19.098 No.Date 38:30 12.16 n/a .000
00385# + 30.0 02:SW_10 8176.00 10.456 No.Date 39:30 11.98 n/a .000
00386# SUM= 30.0 01:R_N10A 25965.00 29.422 No.Date 39:30 12.09 n/a .000
00387#
00388# Sum of hydrographs from Node 10 routed to Node 9
00389# Section 2
00390#
00391# R0002:CO0045 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00392# ROUTE CHANNEl -> 30.0 02:SW_10A 25965.00 29.422 No.Date 39:30 12.09 n/a .000
00393# [RPT=30.00] out: 30.0 01:R_N10 25965.00 29.481 No.Date 39:30 12.09 n/a .000
00394# [L/R= 3982./ .076/.040]
00395# [Vmax= 591/Dmax= 1.193]
00396#
00397# Addition of Subwatershed 9 and Nichols Creek to Node 9
00398#
00399# R0002:CO0046 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00400# ADD HYD + 30.0 02:SW_9 25965.00 29.481 No.Date 39:30 12.09 n/a .000
00401# + 30.0 02:SW_9 1132.00 4.365 No.Date 30:30 13.32 n/a .000
00402# + 30.0 02:SW_9 4464.00 5.212 No.Date 39:30 10.96 n/a .000
00403# SUM= 30.0 01:R_N9 31561.00 35.488 No.Date 39:30 11.98 n/a .000
00404#
00405# Sum of hydrographs from Node 9 routed to Node 8
00406# Section 3
00407#
00408# R0002:CO0047 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00409# ROUTE CHANNEl -> 31561.00 35.488 No.Date 39:30 11.98 n/a .000
00410# [RPT=30.00] out: 30.0 01:R8 31561.00 33.301 No.Date 40:00 11.98 n/a .000
00411# [L/R= 2269./ .089/.045]
00412# [Vmax= 420/Dmax= 1.270]
00413#
00414# Addition of Subwatershed 8 and Hobbs' Drain to Node 8
00415#
00416# R0002:CO0048 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00417# ADD HYD 30.0 02:R8 31561.00 33.301 No.Date 40:00 11.98 n/a .000
00418# + 30.0 02:R8 131.00 .770 No.Date 28:30 11.20 n/a .000
00419# + 30.0 02:R8 3854.00 6.083 No.Date 38:30 11.85 n/a .000
00420# SUM= 30.0 01:R_N8 35546.00 39.356 No.Date 39:30 11.97 n/a .000
00421#
00422# Sum of hydrographs from Node 8 routed to Node 7
00423# Section 4
00424#
00425# R0002:CO0049 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00426# ROUTE CHANNEl -> 35546.00 39.356 No.Date 39:30 11.97 n/a .000
00427# [RPT=30.00] out: 30.0 01:R7 35546.00 32.170 No.Date 44:00 11.97 n/a .000
00428# [L/R= 2269./ .089/.045]
00429# [Vmax= 209/Dmax= 1.635]
00430#
00431# Addition of Subwatershed 7 to Node 7
00432#
00433# R0002:CO0050 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00434# ADD HYD 30.0 02:R7 35546.00 32.170 No.Date 44:00 11.97 n/a .000
00435# + 30.0 02:R7 2197.00 4.587 No.Date 28:30 9.63 n/a .000
00436# + 30.0 02:R7 38743.00 34.345 No.Date 43:00 11.79 n/a .000
00437# SUM= 30.0 01:R_N7 38743.00 34.345 No.Date 43:00 11.79 n/a .000
00438#
00439# R0002:CO0051 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00440# SAVE HYD 30.0 01:R_N7 38743.00 34.345 No.Date 43:00 11.79 n/a .000
00441# frame_H_N7
00442# remark:flow at @_N7: N7 + SW_7
00443# Insertion of a reservoir to simulate the effects of the Richmond Fen.
00444# Storage area and volumes were estimated from available top maps.
00445# Release rate from fen was assumed to be controlled by the downstream
00446# river cross-section for summer conditions. It was assumed that for up to
00447# 0.75 m of channel of the river provided the storage. Above
00448# this depth, the wetland starts to significantly store water.
00449#
00450# R0002:CO0052 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00451# ROUTE RESERVOIR -> 30.0 02:R7 38743.00 34.345 No.Date 43:00 11.79 n/a .000
00452# [MstOfUse= 7399E+02] SK= 1.00 [R= 1.00]
00453# [L/R= 3056./ .082/.025]
00454# [Vmax= 431/Dmax= 1.025]
00455#
00456# R0002:CO0053 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00457# SAVE HYD 30.0 01:RES_R7 38743.00 23.075 No.Date 54:30 11.79 n/a .000
00458# frame_H_RESR7
00459# remark:outflow of Richmond Fen
00460#
00461# Sum of hydrographs from Node 7 routed to Node 6
00462# Section 5
00463#
00464# R0002:CO0054 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00465# ROUTE CHANNEl -> 30.0 02:RES_R7 38743.00 23.075 No.Date 54:30 11.79 n/a .000
00466# [RPT=30.00] out: 30.0 01:R6 38743.00 23.075 No.Date 56:00 11.79 n/a .000
00467# [L/R= 3056./ .082/.025]
00468# [Vmax= 431/Dmax= 1.025]
00469#
00470# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
00471#
00472# R0002:CO0055 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00473# ADD HYD 30.0 02:R6 38743.00 23.075 No.Date 56:00 11.79 n/a .000
00474# + 30.0 02:R6 165.00 .407 No.Date 33:00 12.21 n/a .000
00475# + 30.0 02:R6 1321.00 3.221 No.Date 33:00 11.81 n/a .000
00476# SUM= 30.0 01:R_N6 40240.00 23.225 No.Date 33:00 12.21 n/a .000
00477#
00478# Sum of hydrographs from Node 6 routed to Node 5
00479# Section 6
00480#
00481# R0002:CO0056 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00482# ROUTE CHANNEl -> 30.0 01:R5 40240.00 23.217 No.Date 55:00 11.87 n/a .000
00483# [L/R= 1892./ .054/.035]
00484# [Vmax= 378/Dmax= 1.035]
00485#
00486# Addition of Subwatershed 5 and Flowing Creek to Node 5
00487#
00488# R0002:CO0057 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00489# ADD HYD 30.0 02:R5 40240.00 23.217 No.Date 55:00 11.87 n/a .000
00490# + 30.0 02:R5 224.00 2.527 No.Date 28:30 15.88 n/a .000
00491# + 30.0 02:R5 4945.00 14.878 No.Date 33:00 15.54 n/a .000
00492# SUM= 30.0 01:R_N5 45409.00 32.974 No.Date 37:00 12.18 n/a .000
00493#
00494# Sum of hydrographs from Node 5 routed to Node 5A
00495# Section 7
00496#
00497# R0002:CO0058 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00498# ROUTE CHANNEl -> 30.0 02:R5A 45409.00 32.974 No.Date 37:00 12.18 n/a .000
00499# [RPT=30.00] out: 30.0 01:R5A 45409.00 32.921 No.Date 37:00 12.18 n/a .000
00500# [L/R= 1892./ .054/.035]
00501# [Vmax= 443/Dmax= .935]
00502#
00503# Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
00504#
00505# R0002:CO0059 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00506# ADD HYD 30.0 02:R5A 45409.00 32.921 No.Date 37:00 12.18 n/a .000
00507# + 30.0 02:R5A1 20.00 .287 No.Date 28:30 17.36 n/a .000
00508# + 30.0 02:R5A1 1412.00 3.027 No.Date 38:00 15.29 n/a .000
00509# SUM= 30.0 01:R_N5A 46421.00 35.939 No.Date 37:00 12.27 n/a .000
00510#
00511# Sum of hydrographs from Node 5A routed to Node 4
00512# Section 8
00513#
00514# R0002:CO0060 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00515# ROUTE CHANNEl -> 30.0 01:R4 46421.00 35.939 No.Date 37:00 12.27 n/a .000
00516# [RPT=30.00] out: 30.0 01:R4 46421.00 35.066 No.Date 39:00 12.27 n/a .000
00517# [L/R= 4920./ .047/.040]
00518# [Vmax= .693/Dmax= 2.836]
00519#
00520# Addition of Subwatershed 4 and Leamy Creek to Node 4
00521#
00522# R0002:CO0061 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00523# ADD HYD 30.0 02:R4 46421.00 35.066 No.Date 39:00 12.27 n/a .000
00524# + 30.0 02:R4 585.00 4.232 No.Date 29:30 15.76 n/a .000
00525# + 30.0 02:R4 1021.00 5.667 No.Date 30:30 17.36 n/a .000
00526# SUM= 30.0 01:R_N4 48447.00 37.399 No.Date 38:30 12.44 n/a .000
00527#
00528# R0002:CO0062 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00529# SAVE HYD 30.0 01:R_N4 48447.00 37.399 No.Date 38:30 12.44 n/a .000
00530# frame_H_R4_0002
00531# remark:flow at @_R4
00532#
00533# Sum of hydrographs from Node 4 routed to Node 2
00534# Section 9
00535#
00536# R0002:CO0063 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00537# ROUTE CHANNEl -> 30.0 02:R4 48447.00 37.399 No.Date 38:30 12.44 n/a .000
00538# [RPT=30.00] out: 30.0 01:R2 48447.00 37.299 No.Date 39:00 12.44 n/a .000
00539# [L/R= 1667./ .067/.040]
00540# [Vmax= 741/Dmax= 2.841]
00541#
00542# Addition of Subwatershed 2 with Monahan Drain and Smith Drain to Node 2
00543#
00544# R0002:CO0064 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00545# ADD HYD 30.0 02:R2 48447.00 37.299 No.Date 39:00 12.44 n/a .000
00546# + 30.0 02:R2 177.00 1.996 No.Date 28:30 15.88 n/a .000
00547# + 30.0 02:R2 1122.00 5.257 No.Date 31:30 17.76 n/a .000
00548# + 30.0 02:R2 2737.00 11.338 No.Date 31:30 15.53 n/a .000
00549# SUM= 30.0 01:R_N2 52483.00 45.676 No.Date 33:30 12.73 n/a .000
00550#
00551# R0002:CO0065 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00552# SAVE HYD 30.0 01:R_N2 52483.00 45.676 No.Date 33:30 12.73 n/a .000
00553# frame_H_N2
00554# remark:flow at @_N2 Jock River Gauge at Moodle Dr.
00555#
00556# Sum of hydrographs from Node 2 routed to Node 1
00557# Section 10
00558#
00559# R0002:CO0066 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00560# ROUTE CHANNEl -> 30.0 02:R2 52483.00 45.676 No.Date 33:30 12.73 n/a .000
00561# [RPT=30.00] out: 30.0 01:R1 52483.00 42.605 No.Date 39:00 12.73 n/a .000
00562# [L/R= 1046./ .051/.040]
00563# [Vmax= .767/Dmax= 2.462]
00564#
00565# Addition of Subwatershed 1 to Node 1
00566#

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00567# R0002:CO0067 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00568# ADD HYD 30.0 02:R1 52483.00 42.605 No.Date 39:30 12.73 n/a .000
00569# + 30.0 02:SW_1 3376.00 12.490 No.Date 32:00 16.23 n/a .000
00570# + 30.0 02:SW_1 50481.00 42.605 No.Date 39:30 12.73 n/a .000
00571# SUM= 30.0 01:R_N1 108600.00 87.700 No.Date 39:30 12.93 n/a .000
00572#
00573# R0002:CO0068 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00574# SAVE HYD 30.0 01:R1 56569.00 49.164 No.Date 36:30 12.93 n/a .000
00575# frame_H_010002
00576# remark:total outflow of Jock River
00577# *****
00578# ** END OF RUN : 4
00579# *****
00580#
00581#
00582# [RPT=30.00] out: 30.0 01:R1 56569.00 49.164 No.Date 36:30 12.93 n/a .000
00583# [L/R= 3982./ .076/.040]
00584# [Vmax= 591/Dmax= 1.193]
00585#
00586# Addition of Subwatershed 9 and Nichols Creek to Node 9
00587#
00588# R0002:CO0069 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00589# ADD HYD 30.0 02:SW_9 25965.00 29.481 No.Date 39:30 12.09 n/a .000
00590# + 30.0 02:SW_9 1132.00 4.365 No.Date 30:30 13.32 n/a .000
00591# + 30.0 02:SW_9 4464.00 5.212 No.Date 39:30 10.96 n/a .000
00592# SUM= 30.0 01:R_N9 31561.00 35.488 No.Date 39:30 11.98 n/a .000
00593#
00594# Sum of hydrographs from Node 9 routed to Node 8
00595# Section 3
00596#
00597# R0002:CO0070 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00598# ROUTE CHANNEl -> 31561.00 35.488 No.Date 39:30 11.98 n/a .000
00599# [RPT=30.00] out: 30.0 01:R8 31561.00 33.301 No.Date 40:00 11.98 n/a .000
00600# [L/R= 2269./ .089/.045]
00601# [Vmax= 420/Dmax= 1.270]
00602#
00603# Addition of Subwatershed 8 and Hobbs' Drain to Node 8
00604#
00605# R0002:CO0071 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00606# ADD HYD 30.0 02:R8 31561.00 33.301 No.Date 40:00 11.98 n/a .000
00607# + 30.0 02:R8 131.00 .770 No.Date 28:30 11.20 n/a .000
00608# + 30.0 02:R8 3854.00 6.083 No.Date 38:30 11.85 n/a .000
00609# SUM= 30.0 01:R_N8 35546.00 39.356 No.Date 39:30 11.97 n/a .000
00610#
00611# Sum of hydrographs from Node 8 routed to Node 7
00612# Section 4
00613#
00614# R0002:CO0072 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00615# ROUTE CHANNEl -> 35546.00 39.356 No.Date 39:30 11.97 n/a .000
00616# [RPT=30.00] out: 30.0 01:R7 35546.00 32.170 No.Date 44:00 11.97 n/a .000
00617# [L/R= 2269./ .089/.045]
00618# [Vmax= 209/Dmax= 1.635]
00619#
00620# Addition of Subwatershed 7 to Node 7
00621#
00622# R0002:CO0073 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00623# ADD HYD 30.0 02:R7 35546.00 32.170 No.Date 44:00 11.97 n/a .000
00624# + 30.0 02:R7 2197.00 4.587 No.Date 28:30 9.63 n/a .000
00625# + 30.0 02:R7 38743.00 34.345 No.Date 43:00 11.79 n/a .000
00626# SUM= 30.0 01:R_N7 38743.00 34.345 No.Date 43:00 11.79 n/a .000
00627#
00628# R0002:CO0074 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00629# SAVE HYD 30.0 01:R_N7 38743.00 34.345 No.Date 43:00 11.79 n/a .000
00630# frame_H_N7
00631# remark:flow at @_N7: N7 + SW_7
00632# Insertion of a reservoir to simulate the effects of the Richmond Fen.
00633# Storage area and volumes were estimated from available top maps.
00634# Release rate from fen was assumed to be controlled by the downstream
00635# river cross-section for summer conditions. It was assumed that for up to
00636# 0.75 m of channel of the river provided the storage. Above
00637# this depth, the wetland starts to significantly store water.
00638#
00639# R0002:CO0075 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00640# ROUTE RESERVOIR -> 30.0 02:R7 38743.00 34.345 No.Date 43:00 11.79 n/a .000
00641# [MstOfUse= 7399E+02] SK= 1.00 [R= 1.00]
00642# [L/R= 3056./ .082/.025]
00643# [Vmax= 431/Dmax= 1.025]
00644#
00645# R0002:CO0076 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00646# SAVE HYD 30.0 01:RES_R7 38743.00 23.075 No.Date 54:30 11.79 n/a .000
00647# frame_H_RESR7
00648# remark:outflow of Richmond Fen
00649#
00650# Sum of hydrographs from Node 7 routed to Node 6
00651# Section 5
00652#
00653# R0002:CO0077 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00654# ROUTE CHANNEl -> 30.0 02:RES_R7 38743.00 23.075 No.Date 54:30 11.79 n/a .000
00655# [RPT=30.00] out: 30.0 01:R6 38743.00 23.075 No.Date 56:00 11.79 n/a .000
00656# [L/R= 3056./ .082/.025]
00657# [Vmax= 431/Dmax= 1.025]
00658#
00659# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
00660#
00661# R0002:CO0078 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00662# ADD HYD 30.0 02:R6 38743.00 23.075 No.Date 56:00 11.79 n/a .000
00663# + 30.0 02:R6 165.00 .407 No.Date 33:00 12.21 n/a .000
00664# + 30.0 02:R6 1321.00 3.221 No.Date 33:00 11.81 n/a .000
00665# SUM= 30.0 01:R_N6 40240.00 23.225 No.Date 33:00 12.21 n/a .000
00666#
00667# Sum of hydrographs from Node 6 routed to Node 5
00668# Section 6
00669#
00670# R0002:CO0079 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00671# ROUTE CHANNEl -> 30.0 01:R5 40240.00 23.217 No.Date 55:00 11.87 n/a .000
00672# [L/R= 1892./ .054/.035]
00673# [Vmax= 378/Dmax= 1.035]
00674#
00675# Addition of Subwatershed 5 and Flowing Creek to Node 5
00676#
00677# R0002:CO0080 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00678# ADD HYD 30.0 02:R5 40240.00 23.217 No.Date 55:00 11.87 n/a .000
00679# + 30.0 02:R5 224.00 2.527 No.Date 28:30 15.88 n/a .000
00680# + 30.0 02:R5 4945.00 14.878 No.Date 33:00 15.54 n/a .000
00681# SUM= 30.0 01:R_N5 45409.00 32.974 No.Date 37:00 12.18 n/a .000
00682#
00683# Sum of hydrographs from Node 5 routed to Node 5A
00684# Section 7
00685#
00686# R0002:CO0081 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00687# ROUTE CHANNEl -> 30.0 02:R5A 45409.00 32.974 No.Date 37:00 12.18 n/a .000
00688# [RPT=30.00] out: 30.0 01:R5A 45409.00 32.921 No.Date 37:00 12.18 n/a .000
00689# [L/R= 1892./ .054/.035]
00690# [Vmax= 443/Dmax= .935]
00691#
00692# Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
00693#
00694# R0002:CO0082 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00695# ADD HYD 30.0 02:R5A 45409.00 32.921 No.Date 37:00 12.18 n/a .000
00696# + 30.0 02:R5A1 20.00 .287 No.Date 28:30 17.36 n/a .000
00697# + 30.0 02:R5A1 1412.00 3.027 No.Date 38:00 15.29 n/a .000
00698# SUM= 30.0 01:R_N5A 46421.00 35.939 No.Date 37:00 12.27 n/a .000
00699#
00700# Sum of hydrographs from Node 5A routed to Node 4
00701# Section 8
00702#
00703# R0002:CO0083 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00704# ROUTE CHANNEl -> 30.0 01:R4 46421.00 35.939 No.Date 37:00 12.27 n/a .000
00705# [RPT=30.00] out: 30.0 01:R4 46421.00 35.066 No.Date 39:00 12.27 n/a .000
00706# [L/R= 4920./ .047/.040]
00707# [Vmax= .693/Dmax= 2.836]
00708#
00709# Addition of Subwatershed 4 and Leamy Creek to Node 4
00710#
00711# R0002:CO0084 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00712# ADD HYD 30.0 02:R4 46421.00 35.066 No.Date 39:00 12.27 n/a .000
00713# + 30.0 02:R4 585.00 4.232 No.Date 29:30 15.76 n/a .000
00714# + 30.0 02:R4 1021.00 5.667 No.Date 30:30 17.36 n/a .000
00715# SUM= 30.0 01:R_N4 48447.00 37.399 No.Date 38:30 12.44 n/a .000
00716#
00717# R0002:CO0085 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00718# SAVE HYD 30.0 01:R_N4 48447.00 37.399 No.Date 38:30 12.44 n/a .000
00719# frame_H_R4_0002
00720# remark:flow at @_R4
00721#
00722# Sum of hydrographs from Node 4 routed to Node 2
00723# Section 9
00724#
00725# R0002:CO0086 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00726# ROUTE CHANNEl -> 30.0 02:R4 48447.00 37.399 No.Date 38:30 12.44 n/a .000
00727# [RPT=30.00] out: 30.0 01:R2 48447.00 37.299 No.Date 39:00 12.44 n/a .000
00728# [L/R= 1667./ .067/.040]
00729# [Vmax= 741/Dmax= 2.841]
00730#
00731# Addition of Subwatershed 2 with Monahan Drain and Smith Drain to Node 2
00732#
00733# R0002:CO0087 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00734# ADD HYD 30.0 02:R2 48447.00 37.299 No.Date 39:00 12.44 n/a .000
00735# + 30.0 02:R2 177.00 1.996 No.Date 28:30 15.88 n/a .000
00736# + 30.0 02:R2 1122.00 5.257 No.Date 31:30 17.76 n/a .000
00737# + 30.0 02:R2 2737.00 11.338 No.Date 31:30 15.53 n/a .000
00738# SUM= 30.0 01:R_N2 52483.00 45.676 No.Date 33:30 12.73 n/a .000
00739#
00740# R0002:CO0088 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00741# SAVE HYD 30.0 01:R_N2 52483.00 45.676 No.Date 33:30 12.73 n/a .000
00742# frame_H_N2
00743# remark:flow at @_N2 Jock River Gauge at Moodle Dr.
00744#
00745# Sum of hydrographs from Node 2 routed to Node 1
00746# Section 10
00747#
00748# R0002:CO0089 -----Dtn-ID:HYD-----AREHA-GPEARCS-TPeakDate_hh:mm-----Rvm-R.C-----DWPFms
00749# ROUTE CHANNEl -> 30.0 02:R2 52483.00 45.676 No.Date 33:30 12.73 n/a .000
00750# [RPT=30.00] out: 30.0 01:R1 52483.00 42.605 No
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00749# CONTINUOUS NASHVD 30.0 01:5M_SAI 1412.00 4.515 No_date 37:30 21.96 384 .000
00750# [Cm 76.0 No 3.00 Tm 1.75]
00751# [IAREK 4.001 SMIN 33.81; SMAK=225.43; EK= 010]
00752# [InterVTime= 12.00]
00753# ROUTE CHANNEL -> 30.0 01:5M_SAI 1412.00 4.515 No_date 37:30 21.96 384 .000
00754# CONTINUOUS NASHVD 30.0 01:5M_S 585.00 6.551 No_date 29:30 25.59 448 .000
00755# [Cm 81.0 No 3.00 Tm 1.75]
00756# [IAREK 4.001 SMIN 25.21; SMAK=168.09; EK= 010]
00757# [InterVTime= 12.00]
00758# ROUTE CHANNEL -> 30.0 01:5M_S 585.00 6.551 No_date 29:30 25.59 448 .000
00759# CONTINUOUS NASHVD 30.0 01:5M_S 1021.00 8.738 No_date 30:30 25.04 438 .000
00760# [Cm 80.0 No 3.00 Tm 1.75]
00761# [IAREK 4.001 SMIN 26.32; SMAK=175.50; EK= 010]
00762# [InterVTime= 12.00]
00763# ROUTE CHANNEL -> 30.0 01:5M_S 1122.00 3.149 No_date 28:30 22.94 402 .000
00764# CONTINUOUS NASHVD 30.0 01:5M_S 177.00 3.149 No_date 28:30 22.94 402 .000
00765# [Cm 77.0 No 3.00 Tm 1.75]
00766# [IAREK 4.001 SMIN 31.15; SMAK=207.66; EK= 010]
00767# [InterVTime= 12.00]
00768# ROUTE CHANNEL -> 30.0 01:5M_S 1122.00 8.043 No_date 31:30 25.59 448 .000
00769# CONTINUOUS NASHVD 30.0 01:5M_S 1122.00 8.043 No_date 31:30 25.59 448 .000
00770# [Cm 81.0 No 3.00 Tm 3.25]
00771# [IAREK 4.001 SMIN 25.71; SMAK=168.09; EK= 010]
00772# [InterVTime= 12.00]
00773# ROUTE CHANNEL -> 30.0 01:5M_S 2937.00 57.548 No_date 31:30 22.44 393 .000
00774# CONTINUOUS NASHVD 30.0 01:5M_S 2937.00 57.548 No_date 31:30 22.44 393 .000
00775# [Cm 76.0 No 3.00 Tm 3.01]
00776# [IAREK 4.001 SMIN 23.46; SMAK=216.39; EK= 010]
00777# [InterVTime= 12.00]
00778# ROUTE CHANNEL -> 30.0 01:5M_S 3176.00 19.206 No_date 32:00 23.45 411 .000
00779# CONTINUOUS NASHVD 30.0 01:5M_S 3176.00 19.206 No_date 32:00 23.45 411 .000
00780# [Cm 78.0 No 3.00 Tm 3.54]
00781# [IAREK 4.001 SMIN 23.81; SMAK=199.22; EK= 010]
00782# [InterVTime= 12.00]
00783#
00784# Routing hydrographs
00785#
00786# Starting with the addition of Jock River Headwater and Subwatershed 13
00787#
00788# ROUTE CHANNEL -> 30.0 01:5M_S 4651.00 11.088 No_date 39:30 16.15 n/a .000
00789# ADD HYD + 30.0 02:1R_S 3680.00 9.169 No_date 37:00 16.38 n/a .000
00790# + 30.0 02:1R_S 1.250 No_date 39:30 13.20 n/a .000
00791# SUM 30.0 01:5M_S13 4651.00 10.488 No_date 35:30 16.15 n/a .000
00792#
00793# Sum of hydrographs from Node 13 routed to Node 13A
00794# [Approximated cross-section - see cross-section 258]
00795# [Use n=0.04 for summer conditions and n=0.025 for spring conditions]
00796#
00797# ROUTE CHANNEL -> 30.0 01:5M_S 4651.00 9.343 No_date 39:30 16.15 n/a .000
00798# [RDP=30.00] out-< 30.0 01:5M_S 4651.00 9.343 No_date 39:30 16.15 n/a .000
00799# [L/S= 5024. / .027 / .040]
00800# [Vmax= .475; Dmax= 1.83]
00801#
00802#
00803# Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
00804#
00805# ROUTE CHANNEL -> 30.0 01:5M_S 4651.00 11.088 No_date 39:30 16.15 n/a .000
00806# ADD HYD + 30.0 02:1R_S 4651.00 9.343 No_date 39:30 16.15 n/a .000
00807# + 30.0 02:1R_S 4651.00 9.343 No_date 39:30 16.15 n/a .000
00808# SUM 30.0 01:5M_S14 7725.00 13.855 No_date 39:30 14.97 n/a .000
00809#
00810# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
00811#
00812# ROUTE CHANNEL -> 30.0 01:5M_S 7725.00 13.855 No_date 39:30 14.97 n/a .000
00813# ROUTE RESERVOIR -> 30.0 02:1R_S 7725.00 13.855 No_date 39:30 14.97 n/a .000
00814# [Mdtotused=.619E+02 m3]
00815#
00816# ROUTE CHANNEL -> 30.0 01:5M_S 7725.00 13.855 No_date 39:30 14.97 n/a .000
00817# SAVE HYD 30.0 01:RES_H 7725.00 13.855 No_date 39:30 14.97 n/a .000
00818# [Vmax= .525; Dmax= 1.424]
00819#
00820# remark:Outflow from Res CM
00821# Output of Res CM at Goodwood Marsh routed from Node 13A to Node 12
00822# [Approximated cross-section - see cross-section 258]
00823# [Use n=0.04 for summer conditions and n=0.025 for spring conditions]
00824# ROUTE CHANNEL -> 30.0 01:5M_S 7725.00 13.855 No_date 39:30 14.97 n/a .000
00825# ROUTE CHANNEL -> 30.0 02:RES_H 7725.00 13.855 No_date 39:30 14.97 n/a .000
00826# [RDP=30.00] out-< 30.0 01:5M_S 7725.00 13.855 No_date 39:30 14.97 n/a .000
00827# [L/S= 5926. / .076 / .040]
00828# [Vmax= .525; Dmax= 1.424]
00829#
00830# Addition of Subwatershed Jock River at Ashton to Node 12
00831#
00832# ROUTE CHANNEL -> 30.0 01:5M_S 7725.00 13.855 No_date 39:30 14.97 n/a .000
00833# ADD HYD + 30.0 02:1R_S 1781.00 8.382 No_date 32:30 20.09 n/a .000
00834# + 30.0 02:1R_S 9506.00 10.361 No_date 32:30 15.93 n/a .000
00835# SUM 30.0 01:5M_S12 9506.00 10.361 No_date 32:30 15.93 n/a .000
00836# ROUTE CHANNEL -> 30.0 01:5M_S 9506.00 10.361 No_date 32:30 15.93 n/a .000
00837# SAVE HYD 30.0 01:RES_H 9506.00 10.361 No_date 32:30 15.93 n/a .000
00838# [Vmax= .634; Dmax= 2.417]
00839#
00840# remark:flow at S_N12 near Ashton
00841#
00842# Sum of hydrographs from Node 12 routed to Node 11
00843# [Approximated cross-section - see cross-section 258]
00844# [Use n=0.04 for summer conditions and n=0.025 for spring conditions]
00845# ROUTE CHANNEL -> 30.0 01:5M_S 9506.00 10.361 No_date 32:30 15.93 n/a .000
00846# ROUTE CHANNEL -> 30.0 01:5M_S 9506.00 10.361 No_date 32:30 15.93 n/a .000
00847# [RDP=30.00] out-< 30.0 01:5M_S 9506.00 10.361 No_date 32:30 15.93 n/a .000
00848# [L/S= 972. / .051 / .040]
00849# [Vmax= .642; Dmax= 2.392]
00850#
00851# Sum of hydrographs from Node 12 routed to Node 10
00852#
00853# ROUTE CHANNEL -> 30.0 02:1R_S 9506.00 10.361 No_date 32:30 15.93 n/a .000
00854# [RDP=30.00] out-< 30.0 01:5M_S 9506.00 10.361 No_date 32:30 15.93 n/a .000
00855# [L/S= 972. / .051 / .040]
00856# [Vmax= .642; Dmax= 2.392]
00857#
00858# Addition of Subwatershed 11 and No Name Creek to Node 11
00859#
00860# ROUTE CHANNEL -> 30.0 02:1R_S 9506.00 10.361 No_date 32:30 15.93 n/a .000
00861# ADD HYD + 30.0 02:1R_S 9506.00 10.361 No_date 32:30 15.93 n/a .000
00862# + 30.0 02:1R_S 1937.00 6.085 No_date 34:00 17.15 n/a .000
00863# SUM 30.0 01:5M_S11 11923.00 17.312 No_date 33:00 16.18 n/a .000
00864# ROUTE CHANNEL -> 30.0 01:5M_S 11923.00 17.312 No_date 33:00 16.18 n/a .000
00865# [L/S= 1428. / .157 / .040]
00866# [Vmax= .462; Dmax= 1.078]
00867#
00868# Addition of Subwatershed 10 to Node 10
00869#
00870# ROUTE CHANNEL -> 30.0 02:1R_S 11923.00 17.312 No_date 33:00 16.18 n/a .000
00871# [RDP=30.00] out-< 30.0 01:5M_S 11923.00 17.312 No_date 33:00 16.18 n/a .000
00872# [L/S= 1428. / .157 / .040]
00873# [Vmax= .462; Dmax= 1.078]
00874#
00875# Addition of Subwatershed 10 to Node 10
00876#
00877# ROUTE CHANNEL -> 30.0 01:5M_S 11923.00 17.312 No_date 33:00 16.18 n/a .000
00878# ADD HYD + 30.0 02:1R_S 11923.00 17.312 No_date 33:00 16.18 n/a .000
00879# + 30.0 02:1R_S 5666.00 16.454 No_date 38:00 20.59 n/a .000
00880# SUM 30.0 01:5M_S10 17889.00 28.336 No_date 38:00 17.44 n/a .000
00881# ROUTE CHANNEL -> 30.0 01:5M_S 17889.00 28.336 No_date 38:00 17.44 n/a .000
00882# SAVE HYD 30.0 01:RES_H 17889.00 28.336 No_date 38:00 17.44 n/a .000
00883# [Vmax= .510; Dmax= 1.759]
00884#
00885# remark:flow at S_N10; M10 + SW10
00886# Addition of Kings Creek to S_M10
00887#
00888# ROUTE CHANNEL -> 30.0 01:5M_S 17889.00 28.336 No_date 38:00 17.44 n/a .000
00889# ADD HYD + 30.0 02:1R_S 8376.00 15.668 No_date 39:30 17.15 n/a .000
00890# + 30.0 01:5M_S14 25965.00 43.586 No_date 39:30 17.35 n/a .000
00891# SUM 30.0 01:5M_S14 25965.00 43.586 No_date 39:30 17.35 n/a .000
00892#
00893# Sum of hydrographs from Node 10 routed to Node 9
00894#
00895# ROUTE CHANNEL -> 30.0 02:1R_S 25965.00 43.586 No_date 39:30 17.35 n/a .000
00896# [RDP=30.00] out-< 30.0 01:5M_S 25965.00 43.586 No_date 39:30 17.35 n/a .000
00897# [L/S= 2982. / .079 / .040]
00898# [Vmax= .463; Dmax= 1.480]
00899#
00900#
00901# Addition of Subwatershed 9 and Nichols Creek to Node 9
00902#
00903# ROUTE CHANNEL -> 30.0 02:1R_S 25965.00 43.586 No_date 39:30 17.35 n/a .000
00904# ADD HYD + 30.0 02:1R_S 25965.00 43.586 No_date 39:30 17.35 n/a .000
00905# + 30.0 02:1R_S 4464.00 7.795 No_date 39:30 15.63 n/a .000
00906# SUM 30.0 01:5M_S9 31565.00 52.066 No_date 39:30 17.17 n/a .000
00907#
00908# Sum of hydrographs from Node 9 routed to Node 8
00909#
00910# ROUTE CHANNEL -> 30.0 02:1R_S 31565.00 52.066 No_date 39:30 17.17 n/a .000
00911# [RDP=30.00] out-< 30.0 01:5M_S 31565.00 52.066 No_date 39:30 17.17 n/a .000
00912# [L/S= 2269. / .089 / .045]
00913# [Vmax= .371; Dmax= 1.510]
00914#
00915# Addition of Subwatershed 8 and Robb's Drain to Node 8
00916#
00917# ROUTE CHANNEL -> 30.0 01:5M_S 31565.00 52.066 No_date 39:30 17.17 n/a .000
00918# ADD HYD + 30.0 02:1R_S 31565.00 52.066 No_date 39:30 17.17 n/a .000
00919# + 30.0 02:1R_S 131.00 1.239 No_date 28:30 16.00 n/a .000
00920# SUM 30.0 01:5M_S8 31565.00 52.066 No_date 39:30 17.17 n/a .000
00921# [RDP=30.00] out-< 30.0 01:5M_S 31565.00 52.066 No_date 39:30 17.17 n/a .000
00922# [L/S= 3790. / .051 / .070]
00923# [Vmax= .207; Dmax= 1.839]
00924#
00925# Sum of hydrographs from Node 8 routed to Node 7
00926#
00927# ROUTE CHANNEL -> 30.0 01:5M_S 31565.00 52.066 No_date 39:30 17.17 n/a .000
00928#
00929# Addition of Subwatershed 7 to Node 7
00930#
00931# ROUTE CHANNEL -> 30.0 02:1R_S 31565.00 52.066 No_date 39:30 17.17 n/a .000
00932# [RDP=30.00] out-< 30.0 01:5M_S 31565.00 52.066 No_date 39:30 17.17 n/a .000
00933# [L/S= 3790. / .051 / .070]
00934# [Vmax= .207; Dmax= 1.839]
00935#
00936# Addition of Subwatershed 7 to Node 7

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00936#
00937# ROUTE CHANNEL -> 30.0 01:5M_S 31565.00 52.066 No_date 39:30 17.17 n/a .000
00938# ADD HYD + 30.0 02:1R_S 3554.00 46.889 No_date 45:00 17.17 n/a .000
00939# + 30.0 02:1R_S 6.873 No_date 35:00 13.87 n/a .000
00940# SUM 30.0 01:5M_S7 38743.00 50.119 No_date 43:30 16.89 n/a .000
00941# ROUTE CHANNEL -> 30.0 01:5M_S 38743.00 50.119 No_date 43:30 16.89 n/a .000
00942# SAVE HYD 30.0 01:RES_H 38743.00 50.119 No_date 43:30 16.89 n/a .000
00943# [Vmax= .438; Dmax= .889]
00944#
00945# remark:flow at S_37; N7 + SW_7
00946# Insertion of a reservoir to simulate the effects of the Richmond Fen.
00947# Storage area and volume were estimated from available top maps.
00948# Release rate from fen was assumed to be controlled by the downstream
00949# river cross-section for summer conditions. It is assumed that for up to
00950# 0.75 m of water, the main channel of the river provided the storage. Above
00951# this depth, the wetland starts to significantly store water.
00952#
00953# ROUTE RESERVOIR -> 30.0 02:1R_S 38743.00 50.119 No_date 43:30 16.89 n/a .000
00954# [Mdtotused=.171E+03 m3]
00955#
00956# ROUTE CHANNEL -> 30.0 01:5M_S 38743.00 50.119 No_date 43:30 16.89 n/a .000
00957# SAVE HYD 30.0 01:RES_H 38743.00 50.119 No_date 43:30 16.89 n/a .000
00958# [Vmax= .438; Dmax= .889]
00959#
00960# remark:outflow of Richmond Fen
00961#
00962# Sum of hydrographs from Node 7 routed to Node 6
00963#
00964# ROUTE CHANNEL -> 30.0 01:5M_S 38743.00 50.119 No_date 43:30 16.89 n/a .000
00965# ADD HYD + 30.0 02:1R_S 38743.00 50.119 No_date 43:30 16.89 n/a .000
00966# SUM 30.0 01:5M_S6 40240.01 47.687 No_date 59:30 17.00 n/a .000
00967# [L/S= 3056. / .082 / .025]
00968# [Vmax= .438; Dmax= .889]
00969#
00970# Addition of Subwatershed 6 and Van Gal Drain to Node 6
00971#
00972# ROUTE CHANNEL -> 30.0 01:5M_S 40240.01 47.687 No_date 59:30 17.00 n/a .000
00973# ADD HYD + 30.0 02:1R_S 165.00 6.830 No_date 33:00 17.55 n/a .000
00974# + 30.0 02:1R_S 1332.00 7.000 No_date 33:00 21.01 n/a .000
00975# SUM 30.0 01:5M_S6 40240.01 47.687 No_date 59:30 17.00 n/a .000
00976#
00977# Sum of hydrographs from Node 6 routed to Node 5
00978#
00979# ROUTE CHANNEL -> 30.0 01:5M_S 40240.01 47.687 No_date 59:30 17.00 n/a .000
00980#
00981# ROUTE CHANNEL -> 30.0 02:1R_S 45409.01 43.159 No_date 35:30 17.47 n/a .000
00982# [RDP=30.00] out-< 30.0 01:5M_S 40240.01 47.687 No_date 59:30 17.00 n/a .000
00983# [L/S= 1482. / .054 / .035]
00984# [Vmax= .396; Dmax= .197]
00985#
00986# Addition of Subwatershed 5 and Flowing Creek to Node 5
00987#
00988# ROUTE CHANNEL -> 30.0 02:1R_S 45409.01 43.159 No_date 35:30 17.47 n/a .000
00989# ADD HYD + 30.0 02:1R_S 424.00 3.985 No_date 28:30 22.94 n/a .000
00990# + 30.0 02:1R_S 4945.00 22.432 No_date 33:00 21.01 n/a .000
00991# SUM 30.0 01:5M_S5 45409.01 43.159 No_date 35:00 17.47 n/a .000
00992#
00993# Sum of hydrographs from Node 5 routed to Node 5A
00994#
00995# ROUTE CHANNEL -> 30.0 01:5M_S 45409.01 43.159 No_date 35:30 17.47 n/a .000
00996#
00997#
00998# ROUTE CHANNEL -> 30.0 02:1R_S 45409.01 43.159 No_date 35:30 17.47 n/a .000
00999# [RDP=30.00] out-< 30.0 01:5M_S 45409.01 43.159 No_date 35:30 17.47 n/a .000
01000# [L/S= 1574. / .057 / .040]
01001# [Vmax= .464; Dmax= 1.057]
01002#
01003# Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
01004#
01005# ROUTE CHANNEL -> 30.0 02:1R_S 45409.01 43.159 No_date 35:30 17.47 n/a .000
01006# ADD HYD + 30.0 02:1R_S 448.00 6.551 No_date 28:30 25.59 n/a .000
01007# + 30.0 02:1R_S 448.00 6.551 No_date 28:30 25.59 n/a .000
01008# SUM 30.0 01:5M_S4 45409.01 43.159 No_date 35:00 17.47 n/a .000
01009#
01010# Sum of hydrographs from Node 5A routed to Node 4
01011#
01012# ROUTE CHANNEL -> 30.0 01:5M_S 45409.01 43.159 No_date 35:30 17.47 n/a .000
01013#
01014#
01015# ROUTE CHANNEL -> 30.0 02:1R_S 45409.01 43.159 No_date 35:30 17.47 n/a .000
01016# [RDP=30.00] out-< 30.0 01:5M_S 45409.01 43.159 No_date 35:30 17.47 n/a .000
01017# [L/S= 1467. / .057 / .040]
01018# [Vmax= .753; Dmax= 3.105]
01019#
01020# Addition of Subwatershed 4 and Leamy Creek to Node 4
01021#
01022# ROUTE CHANNEL -> 30.0 02:1R_S 45409.01 43.159 No_date 35:30 17.47 n/a .000
01023# ADD HYD + 30.0 02:1R_S 4684.01 45.852 No_date 37:30 17.61 n/a .000
01024# + 30.0 02:1R_S 985.00 6.551 No_date 28:30 25.59 n/a .000
01025# SUM 30.0 01:5M_S4 46844.01 47.514 No_date 35:30 17.61 n/a .000
01026#
01027# Sum of hydrographs from Node 4 routed to Node 2
01028#
01029# ROUTE CHANNEL -> 30.0 01:5M_S 46844.01 47.514 No_date 35:30 17.61 n/a .000
01030#
01031#
01032# ROUTE CHANNEL -> 30.0 02:1R_S 46844.01 47.514 No_date 35:30 17.61 n/a .000
01033# [RDP=30.00] out-< 30.0 01:5M_S 46844.01 47.514 No_date 35:30 17.61 n/a .000
01034# [L/S= 1467. / .057 / .040]
01035# [Vmax= .753; Dmax= 3.105]
01036#
01037# Addition of Subwatershed 2 with Monahan Drain and Smith Drain to Node 2
01038#
01039# ROUTE CHANNEL -> 30.0 02:1R_S 46844.01 47.514 No_date 35:30 17.61 n/a .000
01040# ADD HYD + 30.0 02:1R_S 4847.00 49.884 No_date 37:00 17.86 n/a .000
01041# + 30.0 02:1R_S 1212.00 8.043 No_date 31:30 25.59 n/a .000
01042# + 30.0 02:1R_S 1212.00 8.043 No_date 31:30 25.59 n/a .000
01043# SUM 30.0 01:5M_S3 46844.01 47.514 No_date 35:30 17.61 n/a .000
01044#
01045# Sum of hydrographs from Node 2 routed to Node 1
01046#
01047# ROUTE CHANNEL -> 30.0 02:1R_S 46844.01 47.514 No_date 35:30 17.61 n/a .000
01048# [RDP=30.00] out-< 30.0 01:5M_S 46844.01 47.514 No_date 35:30 17.61 n/a .000
01049# [L/S= 1048. / .057 / .040]
01050# [Vmax= .861; Dmax= 3.201]
01051#
01052# Addition of Subwatershed 1 to Node 1
01053#
01054# ROUTE CHANNEL -> 30.0 02:1R_S 46844.01 47.514 No_date 35:30 17.61 n/a .000
01055# ADD HYD + 30.0 02:1R_S 52485.00 59.697 No_date 37:00 18.28 n/a .000
01056# + 30.0 02:1R_S 1375.00 18.206 No_date 32:00 23.45 n/a .000
01057# SUM 30.0 01:5M_S2 52485.00 59.697 No_date 37:00 18.28 n/a .000
01058#
01059# Sum of hydrographs from Node 1 routed to Node 1
01060#
01061# ROUTE CHANNEL -> 30.0 01:5M_S 52485.00 59.697 No_date 37:00 18.28 n/a .000
01062# [RDP=30.00] out-< 30.0 01:5M_S 52485.00 59.697 No_date 37:00 18.28 n/a .000
01063# [L/S= 1048. / .057 / .040]
01064# [Vmax= .861; Dmax= 3.201]
01065#
01066# Addition of Subwatershed 1 to Node 1
01067#
01068# ROUTE CHANNEL -> 30.0 02:1R_S 52485.00 59.697 No_date 37:00 18.28 n/a .000
01069# ADD HYD + 30.0 02:1R_S 52485.00 59.697 No_date 37:00 18.28 n/a .000
01070# + 30.0 02:1R_S 1375.00 18.206 No_date 32:00 23.45 n/a .000
01071# SUM 30.0 01:5M_S1 52485.00 59.697 No_date 37:00 18.28 n/a .000
01072#
01073# Sum of hydrographs from Node 1 routed to Node 1
01074#
01075# ROUTE CHANNEL -> 30.0 01:5M_S 52485.00 59.697 No_date 37:00 18.28 n/a .000
01076#
01077#
01078#
01079#
01080#
01081#
01082#
01083#
01084#
01085#
01086#
01087#
01088#
01089#
01090#
01091#
01092#
01093#
01094#
01095#
01096#
01097#
01098#
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01115#
01116#
01117#
01118#
01119#
01120#
01121#
01122#

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01223 [IAREC: 4.00] SMIN: 57.05: SMAX=380.32: EK: .010]
01224 [InterVntTime: 12.00]
01225 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01226 # of 1.32
01227 R0101<C00006-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01228 CONTINUOUS NASHVD 30.0 01:SR_13 971.00 4.293 NoDate 32:30 38.81 291 .000
01229 [Cm: 61.0: N: 3.00: Tp: 1.76]
01230 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01231 [InterVntTime: 12.00]
01232 #
01233 #
01234 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01235 # of 1.80
01236 R0101<C00007-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01237 CONTINUOUS NASHVD 30.0 01:SR_CM 3074.00 5.604 NoDate 39:30 16.19 250 .000
01238 [Cm: 61.0: N: 3.00: Tp: 1.93]
01239 [IAREC: 4.00] SMIN: 81.24: SMAX=554.96: EK: .010]
01240 [InterVntTime: 12.00]
01241 R0101<C00008-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01242 CONTINUOUS NASHVD 30.0 01:SR_ASH 1781.00 10.659 NoDate 32:30 24.78 383 .000
01243 [Cm: 72.0: N: 3.00: Tp: 1.93]
01244 [IAREC: 4.00] SMIN: 39.75: SMAX=264.99: EK: .010]
01245 [InterVntTime: 12.00]
01246 R0101<C00009-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01247 CONTINUOUS NASHVD 30.0 01:SR_11 500.00 5.516 NoDate 29:00 21.17 327 .000
01248 [Cm: 66.0: N: 3.00: Tp: 1.88]
01249 [IAREC: 4.00] SMIN: 52.62: SMAX=350.79: EK: .010]
01250 [InterVntTime: 12.00]
01251 #
01252 #
01253 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01254 # of 1.80
01255 R0101<C00010-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01256 CONTINUOUS NASHVD 30.0 01:SR_CM 1947.00 7.737 NoDate 34:00 21.17 327 .000
01257 [Cm: 66.0: N: 3.00: Tp: 1.29]
01258 [IAREC: 4.00] SMIN: 52.62: SMAX=350.79: EK: .010]
01259 [InterVntTime: 12.00]
01260 #
01261 #
01262 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01263 # of 1.52
01264 R0101<C00011-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01265 CONTINUOUS NASHVD 30.0 01:SR_10 5666.00 20.651 NoDate 37:30 24.78 383 .000
01266 [Cm: 72.0: N: 3.00: Tp: 1.93]
01267 [IAREC: 4.00] SMIN: 39.75: SMAX=264.99: EK: .010]
01268 [InterVntTime: 12.00]
01269 #
01270 #
01271 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01272 # of 1.78
01273 R0101<C00012-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01274 CONTINUOUS NASHVD 30.0 01:SR_CM 8376.00 19.522 NoDate 39:30 21.17 327 .000
01275 [Cm: 66.0: N: 3.00: Tp: 1.88]
01276 [IAREC: 4.00] SMIN: 52.62: SMAX=350.79: EK: .010]
01277 [InterVntTime: 12.00]
01278 #
01279 #
01280 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01281 # of 1.68
01282 R0101<C00013-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01283 CONTINUOUS NASHVD 30.0 01:SR_CM 8376.00 19.522 NoDate 39:30 21.17 327 .000
01284 [Cm: 70.0: N: 3.00: Tp: 2.51]
01285 [IAREC: 4.00] SMIN: 57.05: SMAX=287.10: EK: .010]
01286 [InterVntTime: 12.00]
01287 #
01288 #
01289 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01290 # of 1.82
01291 R0101<C00014-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01292 CONTINUOUS NASHVD 30.0 01:SR_CM 4464.00 9.718 NoDate 39:30 19.27 298 .000
01293 [Cm: 67.0: N: 3.00: Tp: 1.93]
01294 [IAREC: 4.00] SMIN: 61.90: SMAX=412.66: EK: .010]
01295 [InterVntTime: 12.00]
01296 #
01297 #
01298 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01299 # of 1.80
01300 R0101<C00015-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01301 CONTINUOUS NASHVD 30.0 01:SR_CM 131.00 1.610 NoDate 28:30 19.73 305 .000
01302 [Cm: 63.0: N: 3.00: Tp: .90]
01303 [IAREC: 4.00] SMIN: 59.42: SMAX=396.11: EK: .010]
01304 [InterVntTime: 12.00]
01305 #
01306 #
01307 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01308 # of 1.65
01309 R0101<C00016-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01310 CONTINUOUS NASHVD 30.0 01:SR_RR 3854.00 11.473 NoDate 38:30 21.17 327 .000
01311 [Cm: 66.0: N: 3.00: Tp: 8.42]
01312 [IAREC: 4.00] SMIN: 52.62: SMAX=350.79: EK: .010]
01313 [InterVntTime: 12.00]
01314 #
01315 #
01316 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01317 # of 1.82
01318 R0101<C00017-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01319 CONTINUOUS NASHVD 30.0 01:SR_7 3197.00 8.697 NoDate 36:00 17.04 263 .000
01320 [Cm: 67.0: N: 3.00: Tp: 1.69]
01321 [IAREC: 4.00] SMIN: 76.32: SMAX=508.81: EK: .010]
01322 [InterVntTime: 12.00]
01323 #
01324 #
01325 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01326 # of 1.75
01327 R0101<C00018-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01328 CONTINUOUS NASHVD 30.0 01:SR_1 165.00 .804 NoDate 33:00 21.66 335 .000
01329 [Cm: 67.0: N: 3.00: Tp: 4.18]
01330 [IAREC: 4.00] SMIN: 50.55: SMAX=336.97: EK: .010]
01331 [InterVntTime: 12.00]
01332 #
01333 #
01334 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01335 # of 1.67
01336 R0101<C00019-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01337 CONTINUOUS NASHVD 30.0 01:SR_VR 1332.00 5.936 NoDate 35:00 24.78 383 .000
01338 [Cm: 72.0: N: 3.00: Tp: 5.93]
01339 [IAREC: 4.00] SMIN: 39.75: SMAX=264.99: EK: .010]
01340 [InterVntTime: 12.00]
01341 R0101<C00020-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01342 CONTINUOUS NASHVD 30.0 01:SR_CM 1021.00 11.041 NoDate 30:30 30.69 474 .000
01343 [Cm: 80.0: N: 3.00: Tp: 1.44]
01344 [IAREC: 4.00] SMIN: 25.21: SMAX=168.09: EK: .010]
01345 [InterVntTime: 12.00]
01346 R0101<C00021-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01347 CONTINUOUS NASHVD 30.0 01:SR_2 177.00 4.027 NoDate 28:30 28.21 436 .000
01348 [Cm: 81.0: N: 3.00: Tp: .62]
01349 [IAREC: 4.00] SMIN: 31.15: SMAX=207.66: EK: .010]
01350 [InterVntTime: 12.00]
01351 #
01352 #
01353 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01354 # of 1.20
01355 R0101<C00022-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01356 CONTINUOUS NASHVD 30.0 01:SR_S1 1412.00 5.651 NoDate 37:30 27.03 418 .000
01357 [Cm: 75.0: N: 3.00: Tp: 8.00]
01358 [IAREC: 4.00] SMIN: 51.81: SMAX=225.43: EK: .010]
01359 [InterVntTime: 12.00]
01360 R0101<C00023-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01361 CONTINUOUS NASHVD 30.0 01:SR_4 585.00 8.289 NoDate 29:30 31.34 484 .000
01362 [Cm: 81.0: N: 3.00: Tp: 1.75]
01363 [IAREC: 4.00] SMIN: 25.21: SMAX=168.09: EK: .010]
01364 [InterVntTime: 12.00]
01365 R0101<C00024-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01366 CONTINUOUS NASHVD 30.0 01:SR_CM 1021.00 11.041 NoDate 30:30 30.69 474 .000
01367 [Cm: 77.0: N: 3.00: Tp: .78]
01368 [IAREC: 4.00] SMIN: 31.15: SMAX=207.66: EK: .010]
01369 [InterVntTime: 12.00]
01370 R0101<C00025-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01371 CONTINUOUS NASHVD 30.0 01:SR_2 177.00 4.027 NoDate 28:30 28.21 436 .000
01372 [Cm: 81.0: N: 3.00: Tp: 1.44]
01373 [IAREC: 4.00] SMIN: 25.21: SMAX=168.09: EK: .010]
01374 [InterVntTime: 12.00]
01375 R0101<C00026-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01376 CONTINUOUS NASHVD 30.0 01:SR_RR 1122.00 10.121 NoDate 31:30 31.34 484 .000
01377 [Cm: 81.0: N: 3.00: Tp: 1.44]
01378 [IAREC: 4.00] SMIN: 25.21: SMAX=168.09: EK: .010]
01379 [InterVntTime: 12.00]
01380 R0101<C00027-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01381 CONTINUOUS NASHVD 30.0 01:SR_RR 2737.00 22.263 NoDate 31:30 27.61 427 .000
01382 [Cm: 76.0: N: 3.00: Tp: 3.03]
01383 [IAREC: 4.00] SMIN: 32.46: SMAX=216.39: EK: .010]
01384 [InterVntTime: 12.00]
01385 R0101<C00028-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01386 CONTINUOUS NASHVD 30.0 01:SR_1 3176.00 24.273 NoDate 32:00 28.81 445 .000
01387 [Cm: 78.0: N: 3.00: Tp: 1.51]
01388 [IAREC: 4.00] SMIN: 29.88: SMAX=199.22: EK: .010]
01389 [InterVntTime: 12.00]
01390 #
01391 #
01392 # Routing hydrographs
01393 #
01394 # Starting with the addition of Jock River Headwater and Subwatershed 13
01395 #
01396 R0101<C00030-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01397 ADD HYD 30.0 02:SR_RM 3680.00 11.582 NoDate 36:30 20.20 n/a .000
01398 [L/S/N: 9074. / .022 / .040]
01399 [Vmax: 505: Dmax: 9.9]
01400 #
01401 #
01402 # Sum of hydrographs from Node 13 routed to Node 13A
01403 # [Approximated cross-section - see cross-section 258]
01404 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
01405 #
01406 R0101<C00031-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01407 ROUTE CHANNEL -> 30.0 02:SR_M13 4651.00 14.791 NoDate 38:00 19.91 n/a .000
01408 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01409 [L/S/N: 9074. / .022 / .040]
01410 [Vmax: 505: Dmax: 9.9]
01411 #
01412 #
01413 # Addition of Subwatershed Jock River at Goodwood Marsh to Node 11A
01414 #
01415 R0101<C00032-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS

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01310 ADD HYD 30.0 02:SR_M13A 4651.00 11.868 NoDate 39:30 19.91 n/a .000
01311 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01312 [InterVntTime: 12.00]
01313 #
01314 #
01315 # Insertion of a reservoir to simulate the effects of the Goodwood Marsh
01316 #
01317 R0101<C00033-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01318 ROUTE RESERVOIR -> 30.0 02:SR_M13A 7725.00 17.472 NoDate 39:30 18.43 n/a .000
01319 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01320 [InterVntTime: 12.00]
01321 #
01322 #
01323 # Insertion of a reservoir to simulate the effects of the Goodwood Marsh
01324 #
01325 R0101<C00034-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01326 SAVE HYD 30.0 01:SR_CM 7725.00 3.517 NoDate 59:00 18.43 n/a .000
01327 [Cm: 66.0: N: 3.00: Tp: 1.88]
01328 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01329 [InterVntTime: 12.00]
01330 #
01331 #
01332 # Output of Reservoir Goodwood Marsh routed from Node 13A to Node 11
01333 # [Approximated cross-section - see cross-section 258]
01334 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
01335 #
01336 R0101<C00035-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01337 ROUTE CHANNEL -> 30.0 02:SR_CM 7725.00 3.517 NoDate 59:00 18.43 n/a .000
01338 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01339 [L/S/N: 5926. / .076 / .040]
01340 [Vmax: 546: Dmax: 1.498]
01341 #
01342 #
01343 # Addition of Subwatershed Jock River at Ashton to Node 12
01344 #
01345 R0101<C00036-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01346 ADD HYD 30.0 02:SR_M12 7725.00 3.517 NoDate 61:00 18.43 n/a .000
01347 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01348 [InterVntTime: 12.00]
01349 #
01350 #
01351 # Sum of hydrographs from Node 12 routed to Node 12
01352 # [Approximated cross-section - see cross-section 258]
01353 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
01354 #
01355 R0101<C00037-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01356 ROUTE CHANNEL -> 30.0 02:SR_M12 9506.00 12.656 NoDate 32:30 19.62 n/a .000
01357 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01358 [L/S/N: 972. / .054 / .040]
01359 [Vmax: 677: Dmax: 2.584]
01360 #
01361 #
01362 # Addition of Subwatershed 11 and No Name Creek to Node 11
01363 #
01364 R0101<C00038-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01365 ADD HYD 30.0 02:SR_M11 9506.00 12.499 NoDate 33:00 19.62 n/a .000
01366 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01367 [InterVntTime: 12.00]
01368 #
01369 #
01370 # Sum of hydrographs from Node 11 routed to Node 10
01371 # Section 1
01372 #
01373 R0101<C00039-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01374 ROUTE CHANNEL -> 30.0 02:SR_M11 11921.00 21.461 NoDate 33:00 19.93 n/a .000
01375 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01376 [L/S/N: 14028. / .157 / .040]
01377 [Vmax: 451: Dmax: 1.206]
01378 #
01379 #
01380 # Addition of Subwatershed 10 to Node 10
01381 #
01382 R0101<C00040-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01383 ADD HYD 30.0 02:SR_M10 9506.00 12.499 NoDate 33:00 19.62 n/a .000
01384 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01385 [InterVntTime: 12.00]
01386 #
01387 #
01388 # Sum of hydrographs from Node 10 routed to Node 9
01389 # Section 2
01390 #
01391 R0101<C00041-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01392 ADD HYD 30.0 02:SR_M9 9506.00 12.499 NoDate 33:00 19.62 n/a .000
01393 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01394 [InterVntTime: 12.00]
01395 #
01396 #
01397 # Sum of hydrographs from Node 10 routed to Node 9
01398 # Section 2
01399 #
01400 R0101<C00042-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01401 ROUTE CHANNEL -> 30.0 02:SR_M10 11921.00 21.461 NoDate 33:00 19.93 n/a .000
01402 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01403 [L/S/N: 3982. / .075 / .040]
01404 [Vmax: 679: Dmax: 1.676]
01405 #
01406 #
01407 # Addition of Subwatershed 9 and Nichols Creek to Node 9
01408 #
01409 R0101<C00043-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01410 ADD HYD 30.0 02:SR_M9 25865.00 52.431 NoDate 39:30 21.17 n/a .000
01411 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01412 [InterVntTime: 12.00]
01413 #
01414 #
01415 # Sum of hydrographs from Node 9 routed to Node 8
01416 # Section 3
01417 #
01418 R0101<C00044-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01419 ROUTE CHANNEL -> 30.0 02:SR_M9 31561.00 64.367 NoDate 39:30 21.17 n/a .000
01420 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01421 [L/S/N: 2269. / .088 / .045]
01422 [Vmax: 364: Dmax: 1.604]
01423 #
01424 #
01425 # Addition of Subwatershed 8 and Hobb's Drain to Node 8
01426 #
01427 R0101<C00045-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01428 ADD HYD 30.0 02:SR_M8 31561.00 59.731 NoDate 44:00 20.83 n/a .000
01429 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01430 [InterVntTime: 12.00]
01431 #
01432 #
01433 # Sum of hydrographs from Node 8 routed to Node 7
01434 # Section 4
01435 #
01436 R0101<C00046-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01437 ROUTE CHANNEL -> 30.0 02:SR_M8 38743.00 71.021 NoDate 39:30 21.17 n/a .000
01438 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01439 [L/S/N: 3750. / .033 / .070]
01440 [Vmax: 214: Dmax: 1.965]
01441 #
01442 #
01443 # Addition of Subwatershed 7 to Node 7
01444 #
01445 R0101<C00047-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01446 ADD HYD 30.0 02:SR_M7 38743.00 59.731 NoDate 44:00 20.83 n/a .000
01447 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01448 [InterVntTime: 12.00]
01449 #
01450 #
01451 # Insertion of a reservoir to simulate the effects of the Richmond Fen
01452 #
01453 R0101<C00048-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01454 ROUTE RESERVOIR -> 30.0 02:SR_M7 38743.00 64.039 NoDate 44:00 20.83 n/a .000
01455 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01456 [L/S/N: 25078. / .03 / .03]
01457 [Vmax: 411: Dmax: 1.064]
01458 #
01459 #
01460 # Addition of Subwatershed 6 and Van Gaal Drain to Node 6
01461 #
01462 R0101<C00049-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01463 SAVE HYD 30.0 01:SR_M7 38743.00 31.370 NoDate 60:30 20.83 n/a .000
01464 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01465 [InterVntTime: 12.00]
01466 #
01467 #
01468 # Sum of hydrographs from Node 7 routed to Node 6
01469 # Section 5
01470 #
01471 R0101<C00050-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01472 ROUTE CHANNEL -> 30.0 02:SR_M7 38743.00 31.370 NoDate 60:30 20.83 n/a .000
01473 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01474 [L/S/N: 1852. / .054 / .035]
01475 [Vmax: 411: Dmax: 1.064]
01476 #
01477 #
01478 # Addition of Subwatershed 6 and Van Gaal Drain to Node 6
01479 #
01480 R0101<C00051-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01481 ADD HYD 30.0 02:SR_M6 42042.01 31.366 NoDate 61:00 20.86 n/a .000
01482 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01483 [InterVntTime: 12.00]
01484 #
01485 #
01486 # Sum of hydrographs from Node 6 routed to Node 5
01487 # Section 6
01488 #
01489 R0101<C00052-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01490 ROUTE CHANNEL -> 30.0 02:SR_M6 42042.01 31.366 NoDate 61:00 20.86 n/a .000
01491 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01492 [L/S/N: 1852. / .054 / .035]
01493 [Vmax: 411: Dmax: 1.064]
01494 #
01495 #
01496 # Addition of Subwatershed 5 and Flowing Creek to Node 5
01497 #
01498 R0101<C00053-----DtnIn-ID:HYD-----AREHA-GPEAFCS=PeakDate_hh:mm-----Rvm-R.C-----DWPFCS
01499 ADD HYD 30.0 02:SR_M5 224.00 5.097 NoDate 28:30 28.21 n/a .000
01500 [IAREC: 4.00] SMIN: 57.05: SMAX=430.01: EK: .010]
01501 [InterVntTime: 12.00]

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014977 SUM= 30.0 01:R_N5 45409.01 50.940 No_date 34:30 21.53 n/a .000
014978 # Sum of hydrographs from Node 5 routed to Node 5A
01500 # Section 7
01501 #
01502 R0010:CO00058-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01503 ROUTE CHANNEL -> 30.0 02:R_N5 45409.01 50.940 No_date 34:30 21.53 n/a .000
01504 [RPT=30.00] out-< 30.0 01:R5A 45409.01 50.883 No_date 35:00 21.53 n/a .000
01505 [L/S=1667./_047.035]
01506 [Vmax=.484;Dmax=1.127]
01507 #
01508 # Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
01509 #
01510 R0010:CO00059-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01511 ADD HYD + 30.0 02:R5A 45409.01 50.883 No_date 35:00 21.53 n/a .000
01512 + 30.0 02:R5A 45409.01 50.883 No_date 35:00 21.53 n/a .000
01513 + 30.0 02:R5A 45409.01 50.883 No_date 35:00 21.53 n/a .000
01514 + 30.0 02:R5A 45409.01 50.883 No_date 35:00 21.53 n/a .000
01515 SUM= 30.0 01:R_N5A 46841.01 56.195 No_date 35:00 21.70 n/a .000
01516 # Sum of hydrographs from Node 5A routed to Node 4
01517 # Section 5
01518 #
01519 R0010:CO00060-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01520 ROUTE CHANNEL -> 30.0 02:R_N5A 46841.01 56.195 No_date 35:00 21.70 n/a .000
01521 [RPT=30.00] out-< 30.0 01:R4 46841.01 54.050 No_date 36:00 21.70 n/a .000
01522 [L/S=1667./_047.035]
01523 [Vmax=.790;Dmax=3.283]
01524 #
01525 # Addition of Subwatershed 4 and Leamy Creek to Node 4
01526 #
01527 R0010:CO00061-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01528 ADD HYD + 30.0 02:R4 46841.01 54.050 No_date 36:00 21.70 n/a .000
01529 + 30.0 02:R4 46841.01 54.050 No_date 36:00 21.70 n/a .000
01530 + 30.0 02:R4 46841.01 54.050 No_date 36:00 21.70 n/a .000
01531 SUM= 30.0 01:R_N4 48447.00 59.486 No_date 36:00 22.01 n/a .000
01532 R0010:CO00062-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01533 SAVE HYD + 30.0 01:R_N4 48447.00 59.486 No_date 36:00 22.01 n/a .000
01534 # name H_S4_0104
01535 # remark:flow at S_N4
01536 #
01537 # Sum of hydrographs from Node 4 routed to Node 2
01538 # Section 9
01539 #
01540 R0010:CO00063-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01541 ROUTE CHANNEL -> 30.0 01:R2 48447.00 59.486 No_date 36:00 22.01 n/a .000
01542 [RPT=30.00] out-< 30.0 01:R2 48447.00 59.258 No_date 36:00 22.01 n/a .000
01543 [L/S=1046./_050.437]
01544 [Vmax=.822;Dmax=3.316]
01545 #
01546 # Addition of Subwatershed 2 with Monahan Drain and Smith Drain to Node 2
01547 #
01548 R0010:CO00064-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01549 ADD HYD + 30.0 02:R2 48447.00 59.258 No_date 36:00 22.01 n/a .000
01550 + 30.0 02:R2 48447.00 59.258 No_date 36:00 22.01 n/a .000
01551 + 30.0 02:R2 48447.00 59.258 No_date 36:00 22.01 n/a .000
01552 + 30.0 02:R2 48447.00 59.258 No_date 36:00 22.01 n/a .000
01553 SUM= 30.0 01:R_N2 52483.00 82.076 No_date 33:00 22.52 n/a .000
01554 R0010:CO00065-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01555 SAVE HYD + 30.0 01:R_N2 52483.00 82.076 No_date 33:00 22.52 n/a .000
01556 # name H_S2
01557 # remark:flow at S_N2 Jock River Gauge at Moccie Dr.
01558 #
01559 # Sum of hydrographs from Node 2 routed to Node 1
01560 # Section 10
01561 #
01562 R0010:CO00066-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01563 ROUTE CHANNEL -> 30.0 02:R_N2 52483.00 82.076 No_date 33:00 22.52 n/a .000
01564 [RPT=30.00] out-< 30.0 01:R1 52483.00 72.984 No_date 36:00 22.52 n/a .000
01565 [L/S=1046./_050.437]
01566 [Vmax=.924;Dmax=3.339]
01567 #
01568 # Addition of Subwatershed 1 to Node 1
01569 #
01570 R0010:CO00067-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01571 ADD HYD + 30.0 02:R1 52483.00 72.984 No_date 36:00 22.52 n/a .000
01572 + 30.0 02:R1 52483.00 72.984 No_date 36:00 22.52 n/a .000
01573 SUM= 30.0 01:R_N1 55559.00 89.955 No_date 34:30 22.88 n/a .000
01574 R0010:CO00068-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01575 SAVE HYD + 30.0 01:R_N1 55559.00 89.955 No_date 34:30 22.88 n/a .000
01576 # name NL_010
01577 # remark:flow at Jock River
01578 #####
01579 # END OF SUM 21
01580 #####
01581 #####
01582 #####
01583 #####
01584 #####
01585 #####
01586 #####
01587 RUN:COMMANDE
01588 R0025:CO00001-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01589 START
01590 [TZERO=.00 hrs on 0]
01591 [NPTIME= 2 [Imperial, 2:metric output]]
01592 [NPTIME= 1 ]
01593 [MIN= ]
01594 #-----
01595 # SWMFD Ver: 0.02/Jan 2001 -CERES / INPUT DATA FILE
01596 #-----
01597 # Project Name: [Jock River] INPUT NUMBER: [411-02]
01598 # Date: 06-08-03
01599 # Modeler: [JOP]
01600 # Company: [JFSaInc]
01601 # License #: 2549237
01602 #-----
01603 # CALIBRATION OF SUMMER MODEL PARAMETERS
01604 # USING CONTINUOUS SIMULATIONS
01605 # Rainfall data from USFS rain gauge installed at site + other gauges by the City
01606 # Use data collected from May list to July 14, 2003
01607 #
01608 R0025:CO00002-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01609 READ STORM
01610 # name storm_001
01611 # Comment # Pluie SCS de 24 hrs 1:25 ans pour Ottawa CDA
01612 [RPT=30.00] out-< 30.0 01:R1 3074.00 15.104 No_date 36:30 25.77 n/a .000
01613 R0025:CO00003-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01614 MODIFY STORM
01615 [RPT=30.00] out-< 30.0 01:R1 3074.00 15.104 No_date 36:30 25.77 n/a .000
01616 [L/S=10.00;SDR= 40.00;PRT= 74.39]
01617 R0025:CO00004-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01618 COMPUTE API
01619 [API=50.00;ADIKty= 8500;ADIPin= 9980]
01620 [APImax=106.76;ADlavg= 65.09;ADPin= 44.87]
01621 #
01622 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01623 # of 1.52
01624 R0025:CO00005-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01625 CONTINUOUS NASHYD 30.0 01:R_N1 3074.00 15.104 No_date 36:30 25.77 346 .000
01626 [CN= 44.0; N= 3.00; Tp= 1.13]
01627 [IAREC= 4.00; SMIN= 59.24; SMAX=380.32; SK= .010]
01628 [InterEventTime= 12.00]
01629 #
01630 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01631 # of 1.32
01632 R0025:CO00006-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01633 CONTINUOUS NASHYD 30.0 01:R_N1 3074.00 15.104 No_date 36:30 25.77 346 .000
01634 [CN= 61.0; N= 3.00; Tp= 1.76]
01635 [IAREC= 4.00; SMIN= 64.50; SMAX=430.01; SK= .010]
01636 [InterEventTime= 12.00]
01637 #
01638 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01639 # of 1.80
01640 R0025:CO00007-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01641 CONTINUOUS NASHYD 30.0 01:R_N1 3074.00 15.104 No_date 36:30 25.77 346 .000
01642 [CN= 50.0; N= 3.00; Tp= 1.13]
01643 [IAREC= 4.00; SMIN= 83.24; SMAX=554.66; SK= .010]
01644 [InterEventTime= 12.00]
01645 #
01646 R0025:CO00008-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01647 CONTINUOUS NASHYD 30.0 01:R_N1 3074.00 15.104 No_date 36:30 25.77 346 .000
01648 [CN= 72.0; N= 3.00; Tp= 3.91]
01649 [IAREC= 4.00; SMIN= 39.75; SMAX=264.99; SK= .010]
01650 [InterEventTime= 12.00]
01651 R0025:CO00009-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01652 CONTINUOUS NASHYD 30.0 01:R_N1 3074.00 15.104 No_date 36:30 25.77 346 .000
01653 [CN= 66.0; N= 3.00; Tp= 1.24]
01654 [IAREC= 4.00; SMIN= 52.62; SMAX=350.79; SK= .010]
01655 [InterEventTime= 12.00]
01656 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01657 # of 1.81
01658 R0025:CO00010-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01659 CONTINUOUS NASHYD 30.0 01:R_N1 3074.00 15.104 No_date 36:30 25.77 346 .000
01660 [CN= 66.0; N= 3.00; Tp= 1.16]
01661 [IAREC= 4.00; SMIN= 52.62; SMAX=350.79; SK= .010]
01662 [InterEventTime= 12.00]
01663 #
01664 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01665 # of 1.52
01666 R0025:CO00011-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01667 CONTINUOUS NASHYD 30.0 01:R_N1 3074.00 15.104 No_date 36:30 25.77 346 .000
01668 [CN= 72.0; N= 3.00; Tp= 8.00]
01669 [IAREC= 4.00; SMIN= 39.75; SMAX=264.99; SK= .010]
01670 [InterEventTime= 12.00]
01671 #
01672 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01673 # of 1.75
01674 R0025:CO00012-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01675 CONTINUOUS NASHYD 30.0 01:R_N1 3074.00 15.104 No_date 36:30 25.77 346 .000
01676 [CN= 66.0; N= 3.00; Tp= 11.66]
01677 [IAREC= 4.00; SMIN= 52.62; SMAX=350.79; SK= .010]
01678 [InterEventTime= 12.00]
01679 #
01680 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01681 # of 1.68
01682 R0025:CO00013-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01683 CONTINUOUS NASHYD 30.0 01:R_N1 3074.00 15.104 No_date 36:30 25.77 346 .000
01684 [CN= 66.0; N= 3.00; Tp= 11.66]
01685 [IAREC= 4.00; SMIN= 52.62; SMAX=350.79; SK= .010]
01686 [InterEventTime= 12.00]
01687 #
01688 # Addition of Subwatershed 11 and No Name Creek to Node 11
01689 #
01690 R0025:CO00014-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01691 ROUTE CHANNEL -> 30.0 02:R_N11 8906.00 15.946 No_date 33:30 24.99 n/a .000
01692 [RPT=30.00] out-< 30.0 01:R11 8906.00 15.946 No_date 33:30 24.99 n/a .000
01693 [L/S= 972./_051.040]
01694 [Vmax=.705;Dmax=2.858]
01695 #
01696 # Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
01697 #
01698 R0025:CO00015-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01699 ADD HYD + 30.0 02:R11 8906.00 15.946 No_date 33:30 24.99 n/a .000
01700 + 30.0 02:R11 8906.00 15.946 No_date 33:30 24.99 n/a .000
01701 SUM= 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01702 R0025:CO00016-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01703 SAVE HYD + 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01704 # name H_S11
01705 # remark:flow at S_11 near Ashton
01706 #
01707 # Sum of hydrographs from Node 12 routed to Node 11
01708 # (Approximated cross-section - see cross-section 258)
01709 #
01710 R0025:CO00017-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01711 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01712 [CN= 67.0; N= 3.00; Tp= 4.18]
01713 [IAREC= 4.00; SMIN= 36.67; SMAX=336.97; SK= .010]
01714 [InterEventTime= 12.00]
01715 #
01716 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01717 # of 1.67
01718 R0025:CO00018-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01719 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01720 [CN= 72.0; N= 3.00; Tp= 8.00]
01721 [IAREC= 4.00; SMIN= 39.75; SMAX=264.99; SK= .010]
01722 [InterEventTime= 12.00]
01723 #
01724 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01725 # of 1.63
01726 R0025:CO00019-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01727 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01728 [CN= 72.0; N= 3.00; Tp= 8.00]
01729 [IAREC= 4.00; SMIN= 39.75; SMAX=264.99; SK= .010]
01730 [InterEventTime= 12.00]
01731 #
01732 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01733 # of 1.63
01734 R0025:CO00020-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01735 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01736 [CN= 72.0; N= 3.00; Tp= 8.00]
01737 [IAREC= 4.00; SMIN= 39.75; SMAX=264.99; SK= .010]
01738 [InterEventTime= 12.00]
01739 #
01740 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01741 # of 1.63
01742 R0025:CO00021-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01743 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01744 [CN= 74.0; N= 3.00; Tp= 4.45]
01745 [IAREC= 4.00; SMIN= 36.67; SMAX=244.49; SK= .010]
01746 [InterEventTime= 12.00]
01747 #
01748 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01749 # of 1.63
01750 R0025:CO00022-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01751 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01752 [CN= 81.0; N= 3.00; Tp= .62]
01753 [IAREC= 4.00; SMIN= 35.41; SMAX=168.09; SK= .010]
01754 [InterEventTime= 12.00]
01755 #
01756 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01757 # of 1.63
01758 R0025:CO00023-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01759 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01760 [CN= 75.0; N= 3.00; Tp= 8.00]
01761 [IAREC= 4.00; SMIN= 39.75; SMAX=226.43; SK= .010]
01762 [InterEventTime= 12.00]
01763 #
01764 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01765 # of 1.63
01766 R0025:CO00024-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01767 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01768 [CN= 81.0; N= 3.00; Tp= 8.00]
01769 [IAREC= 4.00; SMIN= 35.41; SMAX=168.09; SK= .010]
01770 [InterEventTime= 12.00]
01771 #
01772 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01773 # of 1.63
01774 R0025:CO00025-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01775 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01776 [CN= 81.0; N= 3.00; Tp= 8.00]
01777 [IAREC= 4.00; SMIN= 35.41; SMAX=168.09; SK= .010]
01778 [InterEventTime= 12.00]
01779 #
01780 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01781 # of 1.63
01782 R0025:CO00026-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01783 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01784 [CN= 81.0; N= 3.00; Tp= 8.00]
01785 [IAREC= 4.00; SMIN= 35.41; SMAX=168.09; SK= .010]
01786 [InterEventTime= 12.00]
01787 #
01788 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01789 # of 1.63
01790 R0025:CO00027-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01791 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01792 [CN= 81.0; N= 3.00; Tp= 8.00]
01793 [IAREC= 4.00; SMIN= 35.41; SMAX=168.09; SK= .010]
01794 [InterEventTime= 12.00]
01795 #
01796 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01797 # of 1.63
01798 R0025:CO00028-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01799 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01800 [CN= 76.0; N= 3.00; Tp= 3.03]
01801 [IAREC= 4.00; SMIN= 32.46; SMAX=216.39; SK= .010]
01802 [InterEventTime= 12.00]
01803 #
01804 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01805 # of 1.63
01806 R0025:CO00029-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01807 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01808 [CN= 78.0; N= 3.00; Tp= 3.56]
01809 [IAREC= 4.00; SMIN= 29.88; SMAX=199.22; SK= .010]
01810 [InterEventTime= 12.00]
01811 #
01812 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01813 # of 1.63
01814 R0025:CO00030-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01815 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01816 [CN= 78.0; N= 3.00; Tp= 3.56]
01817 [IAREC= 4.00; SMIN= 29.88; SMAX=199.22; SK= .010]
01818 [InterEventTime= 12.00]
01819 #
01820 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01821 # of 1.63
01822 R0025:CO00031-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01823 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01824 [CN= 78.0; N= 3.00; Tp= 3.56]
01825 [IAREC= 4.00; SMIN= 29.88; SMAX=199.22; SK= .010]
01826 [InterEventTime= 12.00]
01827 #
01828 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01829 # of 1.63
01830 R0025:CO00032-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01831 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01832 [CN= 78.0; N= 3.00; Tp= 3.56]
01833 [IAREC= 4.00; SMIN= 29.88; SMAX=199.22; SK= .010]
01834 [InterEventTime= 12.00]
01835 #
01836 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01837 # of 1.63
01838 R0025:CO00033-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01839 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01840 [CN= 78.0; N= 3.00; Tp= 3.56]
01841 [IAREC= 4.00; SMIN= 29.88; SMAX=199.22; SK= .010]
01842 [InterEventTime= 12.00]
01843 #
01844 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01845 # of 1.63
01846 R0025:CO00034-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01847 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01848 [CN= 78.0; N= 3.00; Tp= 3.56]
01849 [IAREC= 4.00; SMIN= 29.88; SMAX=199.22; SK= .010]
01850 [InterEventTime= 12.00]
01851 #
01852 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01853 # of 1.63
01854 R0025:CO00035-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01855 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01856 [CN= 78.0; N= 3.00; Tp= 3.56]
01857 [IAREC= 4.00; SMIN= 29.88; SMAX=199.22; SK= .010]
01858 [InterEventTime= 12.00]
01859 #
01860 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01861 # of 1.63
01862 R0025:CO00036-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01863 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01864 [CN= 78.0; N= 3.00; Tp= 3.56]
01865 [IAREC= 4.00; SMIN= 29.88; SMAX=199.22; SK= .010]
01866 [InterEventTime= 12.00]
01867 #
01868 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01869 # of 1.63
01870 R0025:CO00037-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01871 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01872 [CN= 78.0; N= 3.00; Tp= 3.56]
01873 [IAREC= 4.00; SMIN= 29.88; SMAX=199.22; SK= .010]
01874 [InterEventTime= 12.00]
01875 #
01876 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01877 # of 1.63
01878 R0025:CO00038-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01879 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01880 [CN= 78.0; N= 3.00; Tp= 3.56]
01881 [IAREC= 4.00; SMIN= 29.88; SMAX=199.22; SK= .010]
01882 [InterEventTime= 12.00]
01883 #
01884 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
01885 # of 1.63
01886 R0025:CO00039-----DtnIn-ID:HYD-----AREAh-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
01887 CONTINUOUS NASHYD 30.0 01:R_N11 17812.00 31.892 No_date 33:30 24.99 n/a .000
01888 [CN= 78.0; N= 3.00; Tp= 3.56]
01889 [IAREC
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01871# + 30.0 0218M_CK 1917.00 10.139 NoDate 34:00 26.99 n/a .000
01872# SUM# 11.0218M_N10 11923.00 27.440 NoDate 33:00 25.40 n/a .000
01873# #
01874# # Sum of hydrographs from Node 11 routed to Node 10
01875# # Section 1
01876# #
01877# ROUTES-C00041-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
01878# ROUTE CHANNEL -> 30.0 0218M_N11 11923.00 27.440 NoDate 33:00 25.40 n/a .000
01879# [RD7-30.00] out-> 30.0 0118M_N10 11923.00 17.756 NoDate 40:00 25.40 n/a .000
01880# [L/S/N= 14028./ .157./040]
01881# [Vmax= .463/Dmax= 1.320]
01882# #
01883# # Addition of Subwatershed 10 to Node 10
01884# #
01885# ROUTES-C00042-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
01886# ADD HYD + 30.0 0218M_N10 31564.00 68.824 NoDate 38:30 27.35 n/a .000
01887# + 30.0 0218M_N10 5666.00 26.665 NoDate 37:30 31.47 n/a .000
01888# SUM# 30.0 0118M_N10 17859.00 44.045 NoDate 38:30 27.35 n/a .000
01889# ROUTES-C00043-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
01890# SAVE HYD 30.0 0118M_N10 17859.00 44.045 NoDate 38:30 27.35 n/a .000
01891# #
01892# # name_H_SMI0
01893# # remark:flow at R_N10: N10 = SW_N10
01894# # Addition of Kings Creek to S_M10
01895# #
01896# ROUTES-C00044-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
01897# ADD HYD + 30.0 0218M_N10 17859.00 68.824 NoDate 38:30 27.35 n/a .000
01898# + 30.0 0218M_N10 8376.00 25.107 NoDate 39:30 26.99 n/a .000
01899# SUM# 30.0 0118M_N10 25865.00 68.824 NoDate 39:30 27.24 n/a .000
01900# #
01901# # Sum of hydrographs from Node 10 routed to Node 9
01902# # Section 2
01903# #
01904# ROUTES-C00045-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
01905# ROUTE CHANNEL -> 30.0 0218M_N10A 25865.00 68.824 NoDate 39:30 27.24 n/a .000
01906# [RD7-30.00] out-> 30.0 0118M_N10 25865.00 65.905 NoDate 39:30 27.24 n/a .000
01907# [L/S/N= 3982./ .075./040]
01908# [Vmax= .713/Dmax= 1.864]
01909# #
01910# # Addition of Subwatershed 9 and Nichols Creek to Node 9
01911# #
01912# ROUTES-C00046-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
01913# ADD HYD + 30.0 0218M_N9 25865.00 68.824 NoDate 39:30 27.24 n/a .000
01914# + 30.0 0218M_N9 1132.00 11.574 NoDate 30:30 30.25 n/a .000
01915# + 30.0 0218M_N9 4464.00 12.525 NoDate 39:30 24.58 n/a .000
01916# SUM# 30.0 0118M_N9 31561.00 82.923 NoDate 39:30 26.57 n/a .000
01917# #
01918# # Sum of hydrographs from Node 9 routed to Node 8
01919# # Section 3
01920# #
01921# ROUTES-C00047-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
01922# ROUTE CHANNEL -> 30.0 0218M_N9 31561.00 82.923 NoDate 39:30 26.57 n/a .000
01923# [RD7-30.00] out-> 30.0 0118M_N9 31561.00 77.115 NoDate 40:00 26.57 n/a .000
01924# [L/S/N= 2269./ .088./045]
01925# [Vmax= .362/Dmax= 1.727]
01926# #
01927# # Addition of Subwatershed 8 and Robb's Drain to Node 8
01928# #
01929# ROUTES-C00048-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
01930# ADD HYD + 30.0 0218M_N8 31561.00 77.115 NoDate 40:00 26.57 n/a .000
01931# + 30.0 0218M_N8 131.00 2.156 NoDate 28:30 25.17 n/a .000
01932# + 30.0 0218M_N8 35546.00 91.271 NoDate 39:30 26.56 n/a .000
01933# SUM# 30.0 0118M_N8 31561.00 77.115 NoDate 39:30 26.56 n/a .000
01934# #
01935# # Sum of hydrographs from Node 8 routed to Node 7
01936# # Section 4
01937# #
01938# ROUTES-C00049-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
01939# ROUTE CHANNEL -> 30.0 0218M_N8 31561.00 91.271 NoDate 39:30 26.56 n/a .000
01940# [RD7-30.00] out-> 30.0 0118M_N8 31561.00 86.007 NoDate 40:00 26.56 n/a .000
01941# [L/S/N= 3750./ .051./070]
01942# [Vmax= .227/Dmax= 1.000]
01943# #
01944# # Addition of Subwatershed 7 to Node 7
01945# #
01946# ROUTES-C00050-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
01947# ADD HYD + 30.0 0218M_N7 31561.00 86.007 NoDate 40:00 26.56 n/a .000
01948# + 30.0 0218M_N7 3137.00 11.391 NoDate 36:00 21.73 n/a .000
01949# SUM# 30.0 0118M_N7 34700.00 97.400 NoDate 40:00 26.56 n/a .000
01950# ROUTES-C00051-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
01951# SAVE HYD 30.0 0118M_N7 34700.00 97.400 NoDate 44:00 26.53 n/a .000
01952# #
01953# # name_H_SHT7
01954# # remark:flow at R_N7: NT = SW_N7
01955# # Insertion of a reservoir to simulate the effects of the Richmond Fen.
01956# # Storage area and volumes were estimated from available top maps.
01957# # Release rate from fen was assumed to be controlled by the downstream
01958# # river cross-section for summer conditions. It is assumed that for up
01959# # to 0.75 m of water, the main channel of the river provides the storage. Above
01960# # this depth, the wetland starts to significantly store water.
01961# #
01962# ROUTES-C00052-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
01963# ROUTE RESERVOIR -> 30.0 0218M_N7 34700.00 84.011 NoDate 44:00 26.53 n/a .000
01964# out-> 30.0 0118M_N7 34700.00 40.725 NoDate 60:30 26.53 n/a .000
01965# [Mod:0.000000 1577E+01 0]
01966# #
01967# ROUTES-C00053-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
01968# SAVE HYD 30.0 0118M_N7 34700.00 40.725 NoDate 60:30 26.53 n/a .000
01969# #
01970# # name_H_RESR7
01971# # remark:outflow of Richmond Fen
01972# #
01973# # Sum of hydrographs from Node 7 routed to Node 6
01974# # Section 5
01975# #
01976# ROUTES-C00054-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
01977# ROUTE CHANNEL -> 30.0 0218M_N7 34700.00 40.725 NoDate 60:30 26.53 n/a .000
01978# [RD7-30.00] out-> 30.0 0118M_N7 34700.00 40.549 NoDate 61:30 26.53 n/a .000
01979# [L/S/N= 3056./ .082./035]
01980# [Vmax= .510/Dmax= 1.011]
01981# #
01982# # Addition of Subwatershed 6 and Van Gaal Drain to Node 6
01983# #
01984# ROUTES-C00055-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
01985# ADD HYD + 30.0 0218M_N6 34700.00 40.549 NoDate 61:30 26.53 n/a .000
01986# + 30.0 0218M_N6 165.00 1.069 NoDate 33:00 27.61 n/a .000
01987# + 30.0 0218M_N6 1332.00 7.707 NoDate 35:00 31.47 n/a .000
01988# SUM# 30.0 0118M_N6 40240.01 40.613 NoDate 61:30 26.70 n/a .000
01989# #
01990# # Sum of hydrographs from Node 6 routed to Node 5
01991# # Section 6
01992# #
01993# ROUTES-C00056-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
01994# ROUTE CHANNEL -> 30.0 0218M_N6 40240.01 40.613 NoDate 61:30 26.70 n/a .000
01995# [RD7-30.00] out-> 30.0 0118M_N6 40240.01 40.523 NoDate 62:30 26.70 n/a .000
01996# [L/S/N= 1852./ .054./035]
01997# [Vmax= .440/Dmax= 1.203]
01998# #
01999# # Addition of Subwatershed 5 and Flowing Creek to Node 5
02000# #
02001# ROUTES-C00057-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
02002# ADD HYD + 30.0 0218M_N5 45409.01 61.906 NoDate 34:00 27.41 n/a .000
02003# + 30.0 0218M_N5 224.00 6.682 NoDate 28:30 35.63 n/a .000
02004# + 30.0 0218M_N5 45409.01 61.906 NoDate 34:00 27.41 n/a .000
02005# SUM# 30.0 0118M_N5 45409.01 61.906 NoDate 34:00 27.41 n/a .000
02006# #
02007# # Sum of hydrographs from Node 5 routed to Node 4
02008# # Section 7
02009# #
02010# ROUTES-C00058-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
02011# ROUTE CHANNEL -> 30.0 0218M_N5 45409.01 61.906 NoDate 34:00 27.41 n/a .000
02012# [RD7-30.00] out-> 30.0 0118M_N5 45409.01 61.906 NoDate 34:00 27.41 n/a .000
02013# [L/S/N= 556./ .097./040]
02014# [Vmax= .510/Dmax= 1.217]
02015# #
02016# # Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
02017# #
02018# ROUTES-C00059-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
02019# ADD HYD + 30.0 0218M_5A1 45409.01 61.906 NoDate 34:00 27.41 n/a .000
02020# + 30.0 0218M_5A2 20.00 .739 NoDate 28:30 39.33 n/a .000
02021# + 30.0 0218M_5A2 1422.00 7.269 NoDate 37:30 34.21 n/a .000
02022# SUM# 30.0 0118M_5A 46841.01 68.494 NoDate 34:30 27.62 n/a .000
02023# #
02024# # Sum of hydrographs from Node 5A routed to Node 4
02025# # Section 8
02026# #
02027# ROUTES-C00060-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
02028# ROUTE CHANNEL -> 30.0 0218M_5A 46841.01 68.494 NoDate 34:30 27.62 n/a .000
02029# [RD7-30.00] out-> 30.0 0118M_5A 46841.01 65.794 NoDate 36:30 27.62 n/a .000
02030# [L/S/N= 4630./ .047./035]
02031# [Vmax= .838/Dmax= 3.161]
02032# #
02033# # Addition of Subwatershed 4 and Leamy Creek to Node 4
02034# #
02035# ROUTES-C00061-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
02036# ADD HYD + 30.0 0218M_4 46841.01 65.794 NoDate 36:30 27.62 n/a .000
02037# + 30.0 0218M_4 585.00 10.793 NoDate 29:30 39.33 n/a .000
02038# + 30.0 0218M_4 1021.00 14.279 NoDate 30:30 38.17 n/a .000
02039# SUM# 30.0 0118M_4 48447.00 73.162 NoDate 35:30 27.99 n/a .000
02040# #
02041# ROUTES-C00062-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
02042# SAVE HYD 30.0 0118M_4 48447.00 73.162 NoDate 35:30 27.99 n/a .000
02043# #
02044# # name_R_N4_0025
02045# # remark:flow at R_N4
02046# #
02047# # Sum of hydrographs from Node 4 routed to Node 3
02048# # Section 9
02049# #
02050# ROUTES-C00063-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
02051# ROUTE CHANNEL -> 30.0 0218M_4 48447.00 73.162 NoDate 35:30 27.99 n/a .000
02052# [RD7-30.00] out-> 30.0 0118M_4 48447.00 72.527 NoDate 35:30 27.99 n/a .000
02053# [L/S/N= 1667./ .067./040]
02054# [Vmax= .971/Dmax= 3.161]
02055# #
02056# # Addition of Subwatershed 3 with Monahan Drain and Smith Drain to Node 2
02057# #
02058# ROUTES-C00064-----DTrain-ID:HYD-----AREAhA-QPEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWPFms
02059# ADD HYD + 30.0 0218M_2 177.00 5.280 NoDate 28:30 35.63 n/a .000
02060# + 30.0 0218M_2 177.00 5.280 NoDate 28:30 35.63 n/a .000
02061# + 30.0 0218M_2 177.00 5.280 NoDate 28:30 35.63 n/a .000
02062# SUM# 30.0 0118M_2 2737.00 28.975 NoDate 31:00 34.91 n/a .000
02063# + 30.0 0118M_2 52483.00 104.643 NoDate 33:00 28.62 n/a .000

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02619 # Comment = Piliu SCS de 34 hres 1:00 ans pour Ottawa CDA
02620 [SP71.0:0:SDM: 24.01:PROT: 88.57]
02621 R0100<C0009>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02622 MODIFY STOM
02623 [RFACT= 1.00:TSHPIT= 960.0 min]
02624 [SP71.0:0:SDM: 40.00:PROT: 88.57]
02625 R0100<C0010>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02626 COMPUTE API
02627 [AP1max:19.84: AD1avo: 69.19: AD1min: 44.87]
02628 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02629 # of 1.32
02630 CONTINUOUS NASHVD 30.0 01:3R_WJ 3680.0 21.054 No_date 36:30 35.15 397 .000
02631 [Cm 60.0: N: 3.00: Tp= 7.11]
02632 [IAREC= 4.00: SMIN: 57.05: SMAX:380.32: EK: .010]
02633 [InterVntTime= 12.00]
02634 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02635 # of 1.33
02636 R0100<C0006>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02637 CONTINUOUS NASHVD 30.0 01:3R_L3 971.00 8.058 No_date 32:30 32.81 370 .000
02638 [Cm 61.0: N: 3.00: Tp= 3.76]
02639 [IAREC= 4.00: SMIN: 64.50: SMAX:430.01: EK: .010]
02640 [InterVntTime= 12.00]
02641 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02642 # of 1.80
02643 R0100<C0007>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02644 CONTINUOUS NASHVD 30.0 01:3R_GOM 3074.00 9.983 No_date 39:30 28.27 319 .000
02645 [Cm 55.0: N: 3.00: Tp=11.33]
02646 [IAREC= 4.00: SMIN: 81.24: SMAX:554.96: EK: .010]
02647 [InterVntTime= 12.00]
02648 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02649 # of 1.75
02650 R0100<C0008>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02651 CONTINUOUS NASHVD 30.0 01:3R_ASH 1781.00 19.356 No_date 32:30 42.46 479 .000
02652 [Cm 72.0: N: 3.00: Tp= 3.91]
02653 [IAREC= 4.00: SMIN: 52.62: SMAX:264.99: EK: .010]
02654 [InterVntTime= 12.00]
02655 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02656 # of 1.82
02657 R0100<C0009>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02658 CONTINUOUS NASHVD 30.0 01:3M_L1 500.00 10.499 No_date 29:00 36.74 415 .000
02659 [Cm 46.0: N: 3.00: Tp= 12.45]
02660 [IAREC= 4.00: SMIN: 52.62: SMAX:350.79: EK: .010]
02661 [InterVntTime= 12.00]
02662 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02663 # of 1.88
02664 R0100<C0010>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02665 CONTINUOUS NASHVD 30.0 01:3M_CK 1917.00 14.197 No_date 34:00 36.74 415 .000
02666 [Cm 46.0: N: 3.00: Tp= 5.29]
02667 [IAREC= 4.00: SMIN: 52.62: SMAX:350.79: EK: .010]
02668 [InterVntTime= 12.00]
02669 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02670 # of 1.52
02671 R0100<C0011>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02672 CONTINUOUS NASHVD 30.0 01:3M_D1 3650.00 36.560 No_date 37:30 42.46 479 .000
02673 [Cm 72.0: N: 3.00: Tp= 8.00]
02674 [IAREC= 4.00: SMIN: 52.62: SMAX:264.99: EK: .010]
02675 [InterVntTime= 12.00]
02676 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02677 # of 1.75
02678 R0100<C0012>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02679 CONTINUOUS NASHVD 30.0 01:3M_G 8736.00 34.456 No_date 39:30 36.74 415 .000
02680 [Cm 60.0: N: 3.00: Tp= 8.00]
02681 [IAREC= 4.00: SMIN: 52.62: SMAX:350.79: EK: .010]
02682 [InterVntTime= 12.00]
02683 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02684 # of 1.48
02685 R0100<C0013>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02686 CONTINUOUS NASHVD 30.0 01:3M_GK 1132.00 16.257 No_date 30:30 40.80 461 .000
02687 [Cm 70.0: N: 3.00: Tp= 2.51]
02688 [IAREC= 4.00: SMIN: 43.07: SMAX:287.10: EK: .010]
02689 [InterVntTime= 12.00]
02690 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02691 # of 3.82
02692 R0100<C0014>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02693 CONTINUOUS NASHVD 30.0 01:3M_CK 4464.00 17.270 No_date 39:30 33.59 379 .000
02694 [Cm 62.0: N: 3.00: Tp=11.32]
02695 [IAREC= 4.00: SMIN: 52.62: SMAX:412.66: EK: .010]
02696 [InterVntTime= 12.00]
02697 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02698 # of 1.82
02699 R0100<C0015>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02700 CONTINUOUS NASHVD 30.0 01:3M_CK 4664.00 17.270 No_date 39:30 33.59 379 .000
02701 [Cm 62.0: N: 3.00: Tp=11.32]
02702 [IAREC= 4.00: SMIN: 52.62: SMAX:412.66: EK: .010]
02703 [InterVntTime= 12.00]
02704 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02705 # of 1.82
02706 R0100<C0016>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02707 CONTINUOUS NASHVD 30.0 01:3M_G 131.00 3.096 No_date 28:30 34.37 389 .000
02708 [Cm 40.0: N: 3.00: Tp= 4.98]
02709 [IAREC= 4.00: SMIN: 59.42: SMAX:394.11: EK: .010]
02710 [InterVntTime= 12.00]
02711 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02712 # of 1.65
02713 R0100<C0017>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02714 CONTINUOUS NASHVD 30.0 01:3M_G 3854.00 20.590 No_date 38:00 36.74 415 .000
02715 [Cm 66.0: N: 3.00: Tp= 8.42]
02716 [IAREC= 4.00: SMIN: 52.62: SMAX:350.79: EK: .010]
02717 [InterVntTime= 12.00]
02718 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02719 # of 1.82
02720 R0100<C0018>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02721 CONTINUOUS NASHVD 30.0 01:3M_G 3197.00 16.027 No_date 36:00 29.76 336 .000
02722 [Cm 57.0: N: 3.00: Tp= 6.61]
02723 [IAREC= 4.00: SMIN: 74.12: SMAX:508.81: EK: .010]
02724 [InterVntTime= 12.00]
02725 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02726 # of 1.75
02727 R0100<C0019>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02728 CONTINUOUS NASHVD 30.0 01:3M_G 165.00 1.482 No_date 33:00 37.54 424 .000
02729 [Cm 64.0: N: 3.00: Tp= 5.95]
02730 [IAREC= 4.00: SMIN: 50.55: SMAX:336.97: EK: .010]
02731 [InterVntTime= 12.00]
02732 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02733 # of 1.82
02734 R0100<C0020>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02735 CONTINUOUS NASHVD 30.0 01:3M_G 1412.00 19.515 No_date 30:30 51.13 577 .000
02736 [Cm 80.0: N: 3.00: Tp= 2.46]
02737 [IAREC= 4.00: SMIN: 31.15: SMAX:207.66: EK: .010]
02738 [InterVntTime= 12.00]
02739 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02740 # of 1.30
02741 R0100<C0021>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02742 CONTINUOUS NASHVD 30.0 01:3M_G 4945.00 51.121 No_date 33:00 44.15 498 .000
02743 [Cm 81.0: N: 3.00: Tp= 1.75]
02744 [IAREC= 4.00: SMIN: 168.09: EK: .010]
02745 [InterVntTime= 12.00]
02746 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02747 # of 1.47
02748 R0100<C0022>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02749 CONTINUOUS NASHVD 30.0 01:3M_G 1021.00 19.515 No_date 30:30 51.13 577 .000
02750 [Cm 80.0: N: 3.00: Tp= 2.46]
02751 [IAREC= 4.00: SMIN: 31.15: SMAX:207.66: EK: .010]
02752 [InterVntTime= 12.00]
02753 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02754 # of 1.47
02755 R0100<C0023>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02756 CONTINUOUS NASHVD 30.0 01:3M_G 1122.00 17.710 No_date 31:30 52.03 587 .000
02757 [Cm 81.0: N: 3.00: Tp= 1.21]
02758 [IAREC= 4.00: SMIN: 31.15: SMAX:207.66: EK: .010]
02759 [InterVntTime= 12.00]
02760 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02761 # of 1.47
02762 R0100<C0024>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02763 CONTINUOUS NASHVD 30.0 01:3M_DR 2737.00 40.026 No_date 31:00 46.72 527 .000
02764 [Cm 78.0: N: 3.00: Tp= 1.56]
02765 [IAREC= 4.00: SMIN: 29.88: SMAX:199.22: EK: .010]
02766 [InterVntTime= 12.00]
02767 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02768 # of 1.47
02769 R0100<C0025>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02770 CONTINUOUS NASHVD 30.0 01:3M_L1 3176.00 43.079 No_date 32:00 48.46 547 .000
02771 [Cm 78.0: N: 3.00: Tp= 1.56]
02772 [IAREC= 4.00: SMIN: 29.88: SMAX:199.22: EK: .010]
02773 [InterVntTime= 12.00]
02774 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02775 # of 1.47
02776 R0100<C0026>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02777 CONTINUOUS NASHVD 30.0 01:3M_DR 2737.00 40.026 No_date 31:00 46.72 527 .000
02778 [Cm 78.0: N: 3.00: Tp= 1.56]
02779 [IAREC= 4.00: SMIN: 29.88: SMAX:199.22: EK: .010]
02780 [InterVntTime= 12.00]
02781 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02782 # of 1.47
02783 R0100<C0027>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02784 CONTINUOUS NASHVD 30.0 01:3M_DR 2737.00 40.026 No_date 31:00 46.72 527 .000
02785 [Cm 78.0: N: 3.00: Tp= 1.56]
02786 [IAREC= 4.00: SMIN: 29.88: SMAX:199.22: EK: .010]
02787 [InterVntTime= 12.00]
02788 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02789 # of 1.47
02790 R0100<C0028>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02791 CONTINUOUS NASHVD 30.0 01:3M_DR 2737.00 40.026 No_date 31:00 46.72 527 .000
02792 [Cm 78.0: N: 3.00: Tp= 1.56]
02793 [IAREC= 4.00: SMIN: 29.88: SMAX:199.22: EK: .010]
02794 [InterVntTime= 12.00]
02795 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02796 # of 1.47
02797 R0100<C0029>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02798 CONTINUOUS NASHVD 30.0 01:3M_DR 2737.00 40.026 No_date 31:00 46.72 527 .000
02799 [Cm 78.0: N: 3.00: Tp= 1.56]
02800 [IAREC= 4.00: SMIN: 29.88: SMAX:199.22: EK: .010]
02801 [InterVntTime= 12.00]
02802 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02803 # of 1.47
02804 R0100<C0030>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02805 CONTINUOUS NASHVD 30.0 02:3R_WJ 3680.00 21.054 No_date 36:30 35.15 n/a .000

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02806> 30.0 02:3M_L3 971.00 8.058 No_date 32:30 32.81 n/a .000
02807> SUM= 30.0 01:3M_L3 4651.00 27.020 No_date 35:00 34.66 n/a .000
02808>
02809> Sum of hydrographs from Node 13 routed to Node 13A
02810> (Approximated cross-section - see cross-section 218)
02811> Use n=0.04 for summer conditions and n=0.025 for spring conditions
02812>
02813> R0100<C00031>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02814> ROUTE CHANNEL -> 30.0 02:3M_L3 4651.00 27.020 No_date 35:00 34.66 n/a .000
02815> [RPT=30.00] out<- 30.0 01:3M_L3 4651.00 22.149 No_date 38:30 34.66 n/a .000
02816> [L/S/n= 9074.0 / .022 / .040]
02817> [Vmax= 394:Max= 4.118]
02818>
02819> Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
02820>
02821> R0100<C00032>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02822> ADD HYD 30.0 02:3M_L3 4651.00 22.149 No_date 38:30 34.66 n/a .000
02823> [RPT=30.00] out<- 30.0 02:3R_GOM 3074.00 9.983 No_date 39:30 28.27 n/a .000
02824> SUM= 30.0 01:3M_L3 7725.00 31.987 No_date 38:30 32.12 n/a .000
02825>
02826> Insertion of a reservoir to simulate the effects of the Goodwood Marsh
02827>
02828> R0100<C00033>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02829> ROUTE RESERVOIR -> 30.0 02:3M_L3 7725.00 31.987 No_date 39:30 32.12 n/a .000
02830> out<- 30.0 01:3M_GM 7725.00 3.938 No_date 63:30 32.12 n/a .000
02831> [NoStoRes=17678:3.883]
02832>
02833> R0100<C00034>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02834> SAVE HYD 30.0 01:3M_GM 7725.00 3.938 No_date 63:30 32.12 n/a .000
02835>
02836> frame H_RESUM
02837> remark:outflow from Res GM
02838>
02839> Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
02840> (Approximated cross-section - see cross-section 218)
02841> Use n=0.04 for summer conditions and n=0.025 for spring conditions
02842>
02843> R0100<C00035>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02844> ROUTE CHANNEL -> 30.0 02:3M_GM 7725.00 3.938 No_date 63:30 32.12 n/a .000
02845> [RPT=30.00] out<- 30.0 02:3M_GM 7725.00 3.938 No_date 66:30 32.12 n/a .000
02846> [L/S/n= 972.0 / .051 / .040]
02847> [Vmax= 560:Max= 1.558]
02848>
02849> Addition of Subwatershed Jock River at Ashton to Node 12
02850>
02851> R0100<C00036>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02852> ADD HYD 30.0 02:3M_GM 7725.00 3.938 No_date 66:30 32.12 n/a .000
02853> [RPT=30.00] out<- 30.0 02:3R_ASH 1781.00 19.356 No_date 32:30 42.46 n/a .000
02854> SUM= 30.0 01:3M_GM 9506.00 21.410 No_date 32:30 34.06 n/a .000
02855>
02856> R0100<C00037>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02857> SAVE HYD 30.0 01:3M_GM 9506.00 21.410 No_date 32:30 34.06 n/a .000
02858>
02859> frame H_S12
02860> remark:flow at S_12 near Ashton
02861>
02862> Sum of hydrographs from Node 12 routed to Node 11
02863> (Approximated cross-section - see cross-section 218)
02864> Use n=0.04 for summer conditions and n=0.025 for spring conditions
02865>
02866> R0100<C00038>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02867> ROUTE CHANNEL -> 30.0 02:3M_GM 9506.00 21.410 No_date 32:30 34.06 n/a .000
02868> [RPT=30.00] out<- 30.0 02:3M_GM 9506.00 21.410 No_date 32:30 34.06 n/a .000
02869> [L/S/n= 972.0 / .051 / .040]
02870> [Vmax= 762.0 / .051 / .040]
02871>
02872> Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
02873>
02874> R0100<C00039>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02875> ROUTE CHANNEL -> 30.0 02:3M_GM 9506.00 21.410 No_date 32:30 34.06 n/a .000
02876> [RPT=30.00] out<- 30.0 01:3M_GM 9506.00 21.410 No_date 29:00 36.74 n/a .000
02877> [L/S/n= 972.0 / .051 / .040]
02878> [Vmax= 774:Max= 3.175]
02879>
02880> Addition of Subwatershed 11 and No Name Creek to Node 11
02881>
02882> R0100<C00040>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02883> ADD HYD 30.0 02:3M_GM 9506.00 21.410 No_date 32:30 34.06 n/a .000
02884> [RPT=30.00] out<- 30.0 02:3M_GM 9506.00 21.410 No_date 32:30 34.06 n/a .000
02885> [L/S/n= 972.0 / .051 / .040]
02886> [Vmax= 484:Max= 1.483]
02887>
02888> Addition of Subwatershed 10 to Node 10
02889>
02890> R0100<C00041>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02891> ROUTE CHANNEL -> 30.0 02:3M_GM 11923.00 37.433 No_date 33:00 34.60 n/a .000
02892> [RPT=30.00] out<- 30.0 01:3M_GM 11923.00 23.312 No_date 39:00 34.60 n/a .000
02893> [L/S/n= 14028.0 / 137.040]
02894> [Vmax= 484:Max= 1.483]
02895>
02896> Addition of Subwatershed 10 to Node 10
02897>
02898> R0100<C00042>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02899> ADD HYD 30.0 02:3M_GM 11923.00 37.433 No_date 33:00 34.60 n/a .000
02900> [RPT=30.00] out<- 30.0 01:3M_GM 11923.00 23.312 No_date 39:00 34.60 n/a .000
02901> [L/S/n= 14028.0 / 137.040]
02902> [Vmax= 484:Max= 1.483]
02903>
02904> Addition of Subwatershed 9 to Node 9
02905>
02906> R0100<C00043>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02907> ROUTE CHANNEL -> 30.0 02:3M_GM 25965.00 93.246 No_date 39:30 37.01 n/a .000
02908> [RPT=30.00] out<- 30.0 01:3M_GM 25965.00 93.246 No_date 39:30 37.01 n/a .000
02909> [L/S/n= 1982.0 / 075.040]
02910> [Vmax= 769:Max= 2.125]
02911>
02912> Addition of Subwatershed 9 and Nichols Creek to Node 9
02913>
02914> R0100<C00044>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02915> ADD HYD 30.0 02:3M_GM 25965.00 93.246 No_date 39:30 37.01 n/a .000
02916> [RPT=30.00] out<- 30.0 02:3M_GM 25965.00 93.246 No_date 39:30 37.01 n/a .000
02917> [L/S/n= 1982.0 / 075.040]
02918> [Vmax= 769:Max= 2.125]
02919>
02920> Sum of hydrographs from Node 9 routed to Node 8
02921>
02922> R0100<C00045>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02923> ROUTE CHANNEL -> 30.0 02:3M_GM 25965.00 93.246 No_date 39:30 37.01 n/a .000
02924> [RPT=30.00] out<- 30.0 01:3M_GM 25965.00 93.246 No_date 39:30 37.01 n/a .000
02925> [L/S/n= 1982.0 / 075.040]
02926> [Vmax= 372:Max= 1.905]
02927>
02928> Addition of Subwatershed 8 and Hobb's Drain to Node 8
02929>
02930> R0100<C00046>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02931> ADD HYD 30.0 02:3M_GM 31561.00 106.464 No_date 40:00 36.66 n/a .000
02932> [RPT=30.00] out<- 30.0 02:3M_GM 31561.00 106.464 No_date 40:00 36.66 n/a .000
02933> [L/S/n= 1056.0 / 082.025]
02934> [Vmax= 372:Max= 1.905]
02935>
02936> Addition of Subwatershed 8 and Hobb's Drain to Node 8
02937>
02938> R0100<C00047>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02939> ADD HYD 30.0 02:3M_GM 31561.00 106.464 No_date 40:00 36.66 n/a .000
02940> [RPT=30.00] out<- 30.0 02:3M_GM 31561.00 106.464 No_date 40:00 36.66 n/a .000
02941> [L/S/n= 1056.0 / 082.025]
02942> [Vmax= 372:Max= 1.905]
02943>
02944> Sum of hydrographs from Node 8 routed to Node 7
02945>
02946> R0100<C00048>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02947> ROUTE CHANNEL -> 30.0 02:3M_GM 31561.00 106.464 No_date 40:00 36.66 n/a .000
02948> [RPT=30.00] out<- 30.0 01:3M_GM 31561.00 106.464 No_date 44:30 36.66 n/a .000
02949> [L/S/n= 1750.0 / 053.070]
02950> [Vmax= 236:Max= 2.384]
02951>
02952> Addition of Subwatershed 7 to Node 7
02953>
02954> R0100<C00049>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02955> ADD HYD 30.0 02:3M_GM 31561.00 106.464 No_date 40:00 36.66 n/a .000
02956> [RPT=30.00] out<- 30.0 02:3M_GM 31561.00 106.464 No_date 40:00 36.66 n/a .000
02957> [L/S/n= 1750.0 / 053.070]
02958> [Vmax= 236:Max= 2.384]
02959>
02960> Insertion of a reservoir to simulate the effects of the Richmond Fen.
02961>
02962> R0100<C00050>-----Dtn-ID:HYD-----AREHA-OP&EAcms-Tp&eDate_hh:mm-----RvM-R.C-----DWfMS
02963> ROUTE RESERVOIR -> 30.0 02:3M_GM 31561.00 106.464 No_date 40:00 36.66 n/a .000
02964> [RPT=30.00] out<- 30.0 01:3M
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02993 #
02994 # Sum of hydrographs from Node 6 routed to Node 5
02995 # Section 6
02996 #
02997 R0100:C00056-----Dtain-ID:HYD-----AREAb-QPEAKGms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
02998 ROUTE CHANNEL > 30.0 02:R_M6 45409.01 60.497 No_date 59:30 36.31 n/a .000
02999 [RFS=30.00] out< 30.0 01:R_M5 40240.01 60.383 No_date 60:30 36.31 n/a .000
03000 [L/S/= 1852./ .054/.035]
03001 [Vmax= .490/Dmax= 1.451]
03002 #
03003 # Addition of Subwatershed 5 and Flowing Creek to Node 5
03004 #
03005 R0100:C00057-----Dtain-ID:HYD-----AREAb-QPEAKGms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
03006 ADD HYD + 30.0 02:R_M5 40240.01 60.383 No_date 60:30 36.31 n/a .000
03007 + 30.0 02:SM_5 224.00 9.294 No_date 28:30 47.59 n/a .000
03008 + 30.0 02:PL_CK 4848.00 51.121 No_date 33:00 44.15 n/a .000
03009 SUM= 30.0 01:R_M5 45409.01 79.891 No_date 34:00 37.22 n/a .000
03010 #
03011 # Sum of hydrographs from Node 5 routed to Node 5A
03012 # Section 7
03013 #
03014 R0100:C00058-----Dtain-ID:HYD-----AREAb-QPEAKGms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
03015 ROUTE CHANNEL > 30.0 02:R_M5 45409.01 79.891 No_date 34:00 37.22 n/a .000
03016 [RFS=30.00] out< 30.0 01:R_M5A 45409.01 79.815 No_date 34:00 37.22 n/a .000
03017 [L/S/= 556./ .090/.040]
03018 [Vmax= .544/Dmax= 1.346]
03019 #
03020 # Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
03021 #
03022 R0100:C00059-----Dtain-ID:HYD-----AREAb-QPEAKGms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
03023 ADD HYD + 30.0 02:R_M5A 45409.01 79.815 No_date 34:00 37.22 n/a .000
03024 + 30.0 02:SM_SA2 20.00 1.014 No_date 28:30 52.03 n/a .000
03025 + 30.0 02:SM_SA1 1432.00 9.486 No_date 37:30 45.85 n/a .000
03026 SUM= 30.0 01:R_M5A 46841.01 88.619 No_date 34:30 37.48 n/a .000
03027 #
03028 # Sum of hydrographs from Node 5A routed to Node 4
03029 # Section 8
03030 #
03031 R0100:C00060-----Dtain-ID:HYD-----AREAb-QPEAKGms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
03032 ROUTE CHANNEL > 30.0 02:R_M5A 46841.01 88.619 No_date 34:30 37.48 n/a .000
03033 [RFS=30.00] out< 30.0 01:R_M4 46841.01 84.955 No_date 36:00 37.48 n/a .000
03034 [L/S/= 4631./ .041/.051]
03035 [Vmax= .901/Dmax= 3.849]
03036 #
03037 # Addition of Subwatershed 4 and Leamy Creek to Node 4
03038 #
03039 R0100:C00061-----Dtain-ID:HYD-----AREAb-QPEAKGms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
03040 ADD HYD + 30.0 02:R_M4 46841.01 84.955 No_date 36:00 37.48 n/a .000
03041 + 30.0 02:SM_4 585.00 14.644 No_date 29:30 52.03 n/a .000
03042 + 30.0 02:SM_CK 1021.00 19.515 No_date 30:30 51.13 n/a .000
03043 SUM= 30.0 01:R_M4 48447.00 95.694 No_date 34:30 37.95 n/a .000
03044 R0100:C00062-----Dtain-ID:HYD-----AREAb-QPEAKGms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
03045 SAVE HYD + 30.0 01:R_M4 48447.00 95.694 No_date 34:30 37.95 n/a .000
03046 fname 'S_M4.0100
03047 remark:flow at S_M4
03048 #
03049 # Sum of hydrographs from Node 4 routed to Node 2
03050 # Section 9
03051 #
03052 R0100:C00063-----Dtain-ID:HYD-----AREAb-QPEAKGms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
03053 ROUTE CHANNEL > 30.0 02:R_M4 48447.00 95.694 No_date 34:30 37.95 n/a .000
03054 [RFS=30.00] out< 30.0 01:R_M2 48447.00 95.694 No_date 35:00 38.74 n/a .000
03055 [L/S/= 1667./ .060/.040]
03056 [Vmax= .942/Dmax= 3.915]
03057 #
03058 # Addition of Subwatershed 2 with Mosohan Drain and Smith Drain to Node 2
03059 #
03060 R0100:C00064-----Dtain-ID:HYD-----AREAb-QPEAKGms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
03061 ADD HYD + 30.0 02:R_M2 48447.00 95.342 No_date 35:00 37.95 n/a .000
03062 + 30.0 02:SM_2 177.00 7.344 No_date 28:30 47.59 n/a .000
03063 + 30.0 02:SM_DR 1122.00 17.710 No_date 31:30 52.03 n/a .000
03064 + 30.0 02:MO_DR 2737.00 40.026 No_date 31:00 46.72 n/a .000
03065 SUM= 30.0 01:R_M2 52483.00 141.415 No_date 32:30 38.74 n/a .000
03066 R0100:C00065-----Dtain-ID:HYD-----AREAb-QPEAKGms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
03067 SAVE HYD + 30.0 01:R_M2 52483.00 141.415 No_date 32:30 38.74 n/a .000
03068 fname 'S_M2.0100
03069 remark:flow at S_M2 Jock River Gauge at Moodie Dr.
03070 #
03071 # Sum of hydrographs from Node 2 routed to Node 1
03072 # Section 10
03073 #
03074 R0100:C00066-----Dtain-ID:HYD-----AREAb-QPEAKGms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
03075 ROUTE CHANNEL > 30.0 02:R_M2 52483.00 141.415 No_date 32:30 38.74 n/a .000
03076 [RFS=30.00] out< 30.0 01:R1 52483.00 124.304 No_date 35:00 38.74 n/a .000
03077 [L/S/=1046./ .050/.040]
03078 [Vmax= 1.091/Dmax= 4.553]
03079 #
03080 # Addition of Subwatershed 1 to Node 1
03081 #
03082 R0100:C00067-----Dtain-ID:HYD-----AREAb-QPEAKGms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
03083 ADD HYD + 30.0 02:R1 52483.00 124.304 No_date 35:00 38.74 n/a .000
03084 + 30.0 02:SM_1 3176.00 43.079 No_date 32:00 48.46 n/a .000
03085 SUM= 30.0 01:R1 55659.00 158.420 No_date 34:00 39.29 n/a .000
03086 R0100:C00068-----Dtain-ID:HYD-----AREAb-QPEAKGms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
03087 SAVE HYD + 30.0 01:R1 55659.00 158.420 No_date 34:00 39.29 n/a .000
03088 fname 'R1.0100
03089 remark:outflow of Jock River
03090 #####
03091 R0100:C00002-----Dtain-ID:HYD-----AREAb-QPEAKGms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
03092 FINISH
03093 #
03094 #
03095 # WARNINGS / ERRORS / NOTES
03096 #
03097 R0202:C00015 CONTINUOUS HABYD
03098 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03099 R0202:C00020 CONTINUOUS HABYD
03100 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03101 R0202:C00022 CONTINUOUS HABYD
03102 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03103 R0202:C00024 CONTINUOUS HABYD
03104 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03105 R0205:C00015 CONTINUOUS HABYD
03106 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03107 R0205:C00020 CONTINUOUS HABYD
03108 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03109 R0205:C00022 CONTINUOUS HABYD
03110 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03111 R0205:C00026 CONTINUOUS HABYD
03112 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03113 R0101:C00015 CONTINUOUS HABYD
03114 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03115 R0101:C00020 CONTINUOUS HABYD
03116 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03117 R0101:C00022 CONTINUOUS HABYD
03118 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03119 R0101:C00026 CONTINUOUS HABYD
03120 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03121 R0225:C00015 CONTINUOUS HABYD
03122 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03123 R0225:C00020 CONTINUOUS HABYD
03124 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03125 R0225:C00022 CONTINUOUS HABYD
03126 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03127 R0225:C00026 CONTINUOUS HABYD
03128 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03129 R0250:C00015 CONTINUOUS HABYD
03130 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03131 R0250:C00020 CONTINUOUS HABYD
03132 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03133 R0250:C00022 CONTINUOUS HABYD
03134 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03135 R0250:C00026 CONTINUOUS HABYD
03136 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03137 R0101:C00015 CONTINUOUS HABYD
03138 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03139 R0101:C00020 CONTINUOUS HABYD
03140 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03141 R0101:C00022 CONTINUOUS HABYD
03142 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03143 R0101:C00026 CONTINUOUS HABYD
03144 *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03145 Simulation ended on 2021-02-22 at 15:43:22
03146 #
03147 #
03148 #

```

# Attachment B

Model 2 – Jock River Reach One Model

Stantec, 2007

SWMHYMO Input & Summary files



```

1 2 Metric units
2 *#*****
3 *# Project Name: [Jock River Reach 1 SubWatershed Study]Project #: [160400414]
4 *# Date : October 2006
5 *# Modeller : [Navin Gautam/ Original by Ana M Paerez]
6 *# Company : Stantec.
7 *# License # : 3824306
8 *#*****
9 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[002]
10 *% ["C24SC002.stm"] <--storm filename, one per line for NSTORM time
11 *#-----|-----|
12 READ STORM STORM_FILENAME=["storm.001"]
13 *#-----|-----|
14 MODIFY STORM ICASEms=[1], NSHIFT=[96],
15 RedFACT=[1],
16 *#-----|-----|
17 DEFAULT VALUES ICASEdv=[1], read and print values
18 DEFVAL_FILENAME=["MODIFIED.VAL"]
19 COMPUTE API APII=[50], APIK=[.85]/day
20 *#*****
21 *#
22 *# JOCK RIVER REACH 1 SUBWATERSHED STUDY DISCRETIZED MODEL
23 *# PROPOSED CONDITIONS DESIGN STORM MODEL (SUMMER)
24 *#
25 *# Version: Draft Final Report, October 2006
26 *# Revision History
27 *# -Draft Interim Condition Report, Nov. 2005
28 *#*****
29 *# Assumptions
30 *# - All catchments are assumed to be developed except S-1, S-2, and SW-1a
31 *# - SWM facilities are modeled
32 *# - Rating curves were estimated based on existing reports and modeling for the
33 *# proposed SWM facilities
34 *# - The rating curve for the existing Kennedy Burnett SWM Facility was obtained from
35 *# the Urban Runoff Treatment in the Kennedy Burnett Settling Pond (URTKBP)- Regional
36 *# Municipality of Ottawa Carleton, March 1983
37 *# - River routing modeled
38 *# - River cross sections obtained from RVCA's HEC-RAS hydraulic model
39 *#-----|-----|
40 *# Parameters
41 *# - Design Storms: 2,5,10,25,50 & 1 00yr events: 24hr SCS (DT=10min)-model comparison
42 *# - Impervious area weighted based on: rural subdivision @20%, urban @55%
43 *# - NRCS(SCS) CN based on landuse (airphoto) and soil type (base mapping)
44 *# - Time to peak using Uplands Method
45 *#-----|-----|
46 *#*****
47 *#Read hydrograph upstream of N2 from RVCA Jock R. floodrisk watershed modeling
48 *#*****
49 READ HYD ID=[ 1 ], NHYD=["S_N2"],
50 HYD_FILENAME=["H-S_N2"]
51 *#-----|-----|
52 *#
53 *# Hydrograph from Node 2 routed to Node 416
54 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 9025
55 *#
56 ROUTE CHANNEL IDout=[4], NHYD=["N_416"], IDin=[1] ,
57 RDT=[10](min),
58 CHLGTH=[2327](m), CHSLOPE=[0.0498](%),
59 FPSLOPE=[0.0498](%),
60 SECNUM=[1.0], NSEG=[3]
61 ( SEGROUGH, SEGDIST (m))=
62 [0.075,-23.96
63 -0.055,23.96
64 0.075,157.38] NSEG times
65 ( DISTANCE (m), ELEVATION (m))=
66 [-336.97,93.5]

```

```

67      [-318.85,93]
68      [-259,92.5]
69      [-133.18,92]
70      [-33.17,92]
71      [-27.21,92]
72      [-26.14,91.5]
73      [-24.99,91]
74      [-23.96,90.5]
75      [-14.33,88.26]
76      [-0.68,88.12]
77      [14.33,88.26]
78      [23.96,90.5]
79      [32.12,91]
80      [43.74,91.5]
81      [57.09,92]
82      [73.53,92.5]
83      [108.27,93]
84      [125.88,93.5]
85      [144.81,94]
86      [157.38,94.5]
87      *%-----|-----|
88      *#*****|*****|
89      *#      Catchment SW-1a
90      *#      - Portion of RVCA catchment SW_1 outside of Reach 1 subwatershed
91      *#      - Undeveloped agricultural land
92      *#*****|*****|
93      CONTINUOUS NASHYD      ID=[2], NHYD=["SW_1a"], DT=[5]min, AREA=[546](ha),
94                          DWF=[0](cms), CN/C=[72], IA=[4.67](mm),
95                          N=[3], TP=[2.79]hrs,
96                          Continuous simulation parameters:
97                          IaREcper=[4](hrs),
98                          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
99                          InterEventTime=[12](hrs)
100                         Baseflow simulation parameters:
101                         BaseFlowOption=[1] ,
102                         InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
103                         VHydCond=[0.055](mm/hr), END=-1
104      *%-----|-----|
105      ADD HYD                IDsum=[ 3 ], NHYD=["SN_416"], IDs to add=[4,2]
106      *%-----|-----|
107      SAVE HYD              ID=[ 3 ], # OF PCYCLES=[-1], ICASEsh=[1]
108                          HYD_COMMENT=["Total Flows at Highway 416"]
109      *%-----|-----|
110      *#
111      *# Hydrograph from Node 416 routed to Node at Okeefe drain
112      *# Channel X-Section obtained from RVCA Hydraulic Model - Station 7245
113      *#
114      ROUTE CHANNEL        IDout=[1], NHYD=["N_OK"] ,IDin=[3] ,
115                          RDT=[5](min),
116                          CHLGTH=[497](m), CHSLOPE=[0.3018](%),
117                          FPSLOPE=[0.3018](%),
118                          SECNUM=[1.0], NSEG=[3]
119                          ( SEGROUGH, SEGDIST (m))=
120                          [0.075,-19.40
121                          -0.055,19.40
122                          0.075,377.02] NSEG times
123                          ( DISTANCE (m), ELEVATION (m))=
124                          [-1062.81, 93.00]
125                          [-1061.41, 92.50]
126                          [-945.91, 92.00]
127                          [-783.64, 91.50]
128                          [-136.74, 91.00]
129                          [-134.06, 91.00]
130                          [-128.97, 91.00]
131                          [-86.04, 91.00]
132                          [-20.86, 91.00]

```

```

133          [-20.18, 90.50]
134          [-19.40, 90.00]
135          [-11.68, 86.89]
136          [0.00, 86.10]
137          [12.09, 86.81]
138          [19.40, 90.00]
139          [34.68, 90.50]
140          [60.56, 91.00]
141          [170.14, 91.00]
142          [175.05, 90.50]
143          [180.29, 90.00]
144          [193.41, 90.00]
145          [195.98, 90.50]
146          [377.02, 92.50]
147  *%-----|-----|
148  *#*****|
149  *#      Catchment OKEEFE
150  *#      - To O'Keefe drain (north of the Jock)
151  *#      - Developed with assumed 43% imp.
152  *#*****|
153  CONTINUOUS STANDHYD ID=[2], NHYD=["OKEEFE"], DT=[5](min), AREA=[448](ha),
154          XIMP=[0.43], TIMP=[0.43], DWF=[0](cms), LOSS=[2],
155          SCS curve number CN=[77],
156          Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
157          LGP=[40](m), MNP=[0.25], SCP=[0](min),
158          Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
159          LGI=[1728](m), MNI=[0.013], SCI=[0](min),
160          Continuous simulation parameters:
161          IaREcper=[4](hrs), IaREcimp=[4](hrs),
162          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
163          InterEventTime=[18](hrs), END=-1
164
165  *#*****|
166  *#      Okeefe Pond
167  *#      - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
168  *#      and a ratio of the catchment area to the West Clarke pond rating curve
169  *#      from the MSS for the next coordinates
170  *#*****|
171  ROUTE RESERVOIR      IDout=[4], NHYD=["P_OKE"], IDin=[2],
172          RDT=[5](min),
173          TABLE of ( OUTFLOW-STORAGE ) values
174          (cms) - (ha-m)
175          [ 0.0 , 0.0 ]
176          [ 0.20 , 1.72]
177          [ -1 , -1 ] (max twenty pts)
178          IDovf=[9], NHYDovf=["ok-OVF"]
179
180  *%-----|-----|
181  ADD HYD              IDsum=[ 3 ], NHYD=["SN_OK"], IDs to add=[1,4,9]
182  *%-----|-----|
183  SAVE HYD            ID=[ 3 ], # OF PCYCLES=[-1], ICASEsh=[1]
184          HYD_COMMENT=["Total Flows at Okeefe Drain"]
185  *%-----|-----|
186  *#
187  *# Hydrograph from Node Okeefe routed to Node at Foster Drain
188  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
189  *#
190  ROUTE CHANNEL        IDout=[1], NHYD=["N_FO"], IDin=[3],
191          RDT=[5](min),
192          CHLGTH=[1183](m), CHSLOPE=[0.0761](%),
193          FPSLOPE=[0.0761](%),
194          SECNUM=[1.0], NSEG=[3]
195          ( SEGROUGH, SEGDIST (m))=
196          [0.050,-33.89
197          -0.035,31.59
198          0.050,854.54] NSEG times

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```

199      ( DISTANCE (m), ELEVATION (m))=
200      [-1075.50, 93.00]
201      [-1070.59, 92.50]
202      [-1003.21, 92.00]
203      [-1001.67, 92.00]
204      [-986.64, 92.00]
205      [-816.61, 91.50]
206      [-797.29, 91.00]
207      [-794.18, 91.00]
208      [-775.41, 91.50]
209      [-702.63, 91.50]
210      [-546.19, 91.50]
211      [-529.54, 91.50]
212      [-323.44, 91.00]
213      [-320.71, 91.00]
214      [-183.59, 91.00]
215      [-182.54, 90.50]
216      [-181.36, 90.00]
217      [-177.37, 90.00]
218      [-87.70, 90.00]
219      [-33.89, 90.00]
220      [-18.52, 86.88]
221      [0.00,85.20]
222      [16.20, 86.83]
223      [31.59, 90.00]
224      [33.03, 90.50]
225      [34.41, 91.00]
226      [34.99, 91.00]
227      [72.19, 91.00]
228      [208.76, 91.50]
229      [846.25, 92.00]
230      [854.54, 94.00]
231  *%-----|-----|
232  *#*****|
233  *#      Catchment FOSTER
234  *#      - To Foster ditch (north of the Jock)
235  *#      - Partially developed (medium density); remaining agricultural
236  *#*****|
237  CONTINUOUS STANDHYD ID=[2], NHYD=["FOSTER"], DT=[5]min, AREA=[373](ha),
238  XIMP=[0.55], TIMP=[0.55], DWF=[0](cms), LOSS=[2],
239  SCS curve number CN=[74],
240  Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
241  LGP=[40](m), MNP=[0.25], SCP=[0](min),
242  Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
243  LGI=[1577](m), MNI=[0.013], SCI=[0](min),
244  Continuous simulation parameters:
245  IaREcper=[4](hrs), IaREcimp=[4](hrs),
246  SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
247  InterEventTime=[18](hrs), END=-1
248
249  *#*****|
250  *#      Foster Pond
251  *#      - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
252  *#      and a ratio of the catchment area to the West Clarke pond rating curve
253  *#      from the MSS for the next coordinates
254  *#*****|
255  ROUTE RESERVOIR IDout=[4], NHYD=["P_FOS"], IDin=[2],
256  RDT=[5](min),
257  TABLE of ( OUTFLOW-STORAGE ) values
258  (cms) - (ha-m)
259  [ 0.0 , 0.0 ]
260  [ 0.20 , 1.72]
261  [ -1 , -1 ] (max twenty pts)
262  IDovf=[9], NHYDovf=["FO-OVF"]
263  *%-----|-----|
264  ADD HYD IDsum=[ 3 ], NHYD=["SN_FO"], IDs to add=[1,4,9]

```

```

265 *%-----|-----|
266 SAVE HYD ID=[ 3 ], # OF PCYCLES=[-1], ICASEsh=[1]
267 HYD_COMMENT=["Total Flows at Foster Drain"]
268 *%-----|-----|
269 *#
270 *# Hydrograph from Node Foster routed to Node at Cedarview Road
271 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6016
272 *#
273 ROUTE CHANNEL IDout=[1], NHYD=["N_CE"] ,IDin=[3] ,
274 RDT=[5](min),
275 CHLGTH=[159](m), CHSLOPE=[0.0818](%),
276 FPSLOPE=[0.0818](%),
277 SECNUM=[1.0], NSEG=[3]
278 ( SEGROUGH, SEGDIST (m))=
279 [0.050,-15.46
280 -0.035,26.55
281 0.050,1299.52] NSEG times
282 ( DISTANCE (m), ELEVATION (m))=
283 [-891.38, 93.00]
284 [-882.49, 93.00]
285 [-880.92, 92.50]
286 [-879.37, 92.00]
287 [-877.72, 91.50]
288 [-876.10, 91.00]
289 [-873.23, 91.00]
290 [-871.82, 91.50]
291 [-870.40, 92.00]
292 [-803.44, 92.00]
293 [-645.23, 91.50]
294 [-391.20, 91.50]
295 [-91.00, 91.50]
296 [-85.52, 91.50]
297 [-15.46, 89.40]
298 [-9.79, 89.31]
299 [-3.22, 86.24]
300 [3.22, 85.07]
301 [10.96, 85.79]
302 [16.44, 86.49]
303 [26.55, 89.45]
304 [29.03, 90.27]
305 [35.76, 90.67]
306 [36.67, 91.00]
307 [108.08, 91.00]
308 [109.82, 90.50]
309 [112.04, 90.50]
310 [114.62, 91.00]
311 [116.76, 91.50]
312 [118.42, 92.00]
313 [449.53, 92.50]
314 [571.98, 92.50]
315 [1093.81, 93.50]
316 [1150.48, 94.00]
317 [1299.52, 95.00]
318 *%-----|-----|
319 *#*****
320 *# Catchment S-1
321 *# - To Jock River (north and south of Jock)
322 *# - Primarily agricultural fields; portion of sand quarry
323 *#*****
324 CONTINUOUS NASHYD ID=[2], NHYD=["S-1"], DT=[5]min, AREA=[245](ha),
325 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
326 N=[3], TP=[1.10]hrs,
327 Continuous simulation parameters:
328 IaRECper=[4](hrs),
329 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
330 InterEventTime=[12](hrs)

```



```

331 Baseflow simulation parameters:
332 BaseFlowOption=[1] ,
333 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
334 VHydCond=[0.055](mm/hr), END=-1
335
336 *%-----|-----|
337 ADD HYD IDsum=[ 3 ], NHYD=["SN_CE"], IDs to add=[1,2]
338 *%-----|-----|
339 SAVE HYD ID=[ 3 ], # OF PCYCLES=[-1], ICASEsh=[1]
340 HYD_COMMENT=["Total Flows at Cedarview Road"]
341 *%-----|-----|
342 *#
343 *# Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain
344 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5002
345 *#
346 ROUTE CHANNEL IDout=[1], NHYD=["N_WC"] ,IDin=[3] ,
347 RDT=[5](min),
348 CHLGTH=[825](m), CHSLOPE=[0.01](%),
349 FPSLOPE=[0.01](%),
350 SECNUM=[1.0], NSEG=[3]
351 ( SEGRROUGH, SEGDIST (m))=
352 [0.050,-37.5
353 -0.035,37.50
354 0.050,1367.08] NSEG times
355 ( DISTANCE (m), ELEVATION (m))=
356 [-1095.18, 94.00]
357 [-1091.79, 93.50]
358 [-1088.95, 93.00]
359 [-1086.77, 93.00]
360 [-1069.38, 93.00]
361 [-1063.14, 93.00]
362 [-1017.52, 93.00]
363 [-899.70, 93.00]
364 [-877.78, 93.00]
365 [-859.62, 92.50]
366 [-803.18, 93.00]
367 [-789.92, 92.00]
368 [-37.50, 90.00]
369 [-19.61, 87.04]
370 [0.00, 85.70]
371 [14.87, 86.93]
372 [37.50, 90.00]
373 [38.54, 90.50]
374 [42.23, 91]
375 [157.05,91.50]
376 [161.44, 91.50]
377 [236.48, 93.00]
378 [385.47, 92.50]
379 [390.78, 92.50]
380 [863.80, 93.00]
381 [866.13, 93.00]
382 [990.85, 92.50]
383 [991.82, 92.50]
384 [993.04, 93.00]
385 [994.81, 93.50]
386 [1005.36, 93.00]
387 [1190.52, 93.00]
388 [1267.97, 93.50]
389 [1318.99, 94.00]
390 [1367.08, 94.50]
391 *%-----|-----|
392 *#*****|*****|
393 *# Catchment W_CLAR
394 *# - To West Clarke Drain (south of the Jock)
395 *# - Subdivision with 43% imp. as per Barrhaven South MSS
396 *#*****|*****|

```

```

397 CONTINUOUS STANDHYD ID=[2], NHYD=["W_CLAR"], DT=[5]min, AREA=[243](ha),
398 XIMP=[0.43], TIMP=[0.43], DWF=[0](cms), LOSS=[2],
399 SCS curve number CN=[75],
400 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
401 LGP=[40](m), MNP=[0.25], SCP=[0](min),
402 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
403 LGI=[1273](m), MNI=[0.013], SCI=[0](min),
404 Continuous simulation parameters:
405 IaRECper=[4](hrs), IaRECimp=[4](hrs),
406 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
407 InterEventTime=[18](hrs), END=-1
408
409 *%-----|-----|
410 *#*****|
411 *# West Clarke Pond 2
412 *# - Rating curve obtained from Barrhaven South MSS modeling
413 *# - Tributary Drainage Area to MSS Pond 2 = 241 ha
414 *#*****|
415 ROUTE RESERVOIR IDout=[8], NHYD=["MS_P2"], IDin=[2],
416 RDT=[5](min),
417 TABLE of ( OUTFLOW-STORAGE ) values
418 (cms) - (ha-m)
419 [ 0.0 , 0.0 ]
420 [ 0.11 , 0.96]
421 [ -1 , -1 ] (max twenty pts)
422 IDovf=[9], NHYDovf=["P2-OVF"]
423 *%-----|-----|
424 ADD HYD IDsum=[ 4 ], NHYD=["SN_WC"], IDs to add=[8,9,1]
425 *%-----|-----|
426 SAVE HYD ID=[4], # OF PCYCLES=[-1], ICASEsh=[1]
427 HYD_COMMENT=["Total Flows at West Clarke Pond Outlet"]
428 *%-----|-----|
429 *# Hydrograph from Node West Clarke routed to Node at Kennedy - Burnett Drain
430 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4534
431 *#
432 ROUTE CHANNEL IDout=[1], NHYD=["N_KB"] ,IDin=[4] ,
433 RDT=[5](min),
434 CHLGTH=[1020](m), CHSLOPE=[0.0498](%),
435 FPSLOPE=[0.0498](%),
436 SECNUM=[1.0], NSEG=[3]
437 ( SEGROUGH, SEGDIST (m))=
438 [0.050,-23.63
439 -0.035,23.63
440 0.050,728.3] NSEG times
441 ( DISTANCE (m), ELEVATION (m))=
442 [-1082.01,94]
443 [-1028.17,92.5]
444 [-992.3,93.5]
445 [-279.34,90]
446 [-23.63,90]
447 [-13.45,87.13]
448 [-0.07,86.24]
449 [10.54,87.15]
450 [23.63,90]
451 [24.86,90.5]
452 [26.72,91]
453 [45.07,91.5]
454 [128.17,91.5]
455 [270.7,92.5]
456 [728.3,95]
457
458 *%-----|-----|
459 *#*****|
460 *# Catchment KEN_BU
461 *# - To Kennedy-Burnett SWM Facility
462 *# - Outlets to Fraser-Clarke drain (north of the Jock)

```

```

463 *# - Medium density residential subdivision
464 *#*****
465 CONTINUOUS STANDHYD ID=[2], NHYD=["KEN_BU"], DT=[5]min, AREA=[281](ha),
466 XIMP=[0.55], TIMP=[0.55], DWF=[0](cms), LOSS=[2],
467 SCS curve number CN=[71],
468 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
469 LGP=[40](m), MNP=[0.25], SCP=[0](min),
470 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
471 LGI=[1369](m), MNI=[0.013], SCI=[0](min),
472 Continuous simulation parameters:
473 IaREcper=[4](hrs), IaREcimp=[4](hrs),
474 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
475 InterEventTime=[18](hrs), END=-1
476 *%-----|-----|
477 *#*****
478 *# Existing Kennedy-Burnett SWM Facility
479 *# - Rating curve obtained from URTKBP
480 *# - Tributary Drainage Area to Pond = 160 ha
481 *#*****
482 ROUTE RESERVOIR IDout=[5], NHYD=["KEN_P"], IDin=[2],
483 RDT=[5](min),
484 TABLE of ( OUTFLOW-STORAGE ) values
485 (cms) - (ha-m)
486 [ 0.0 , 0.0 ]
487 [ 0.13 , 0.26 ]
488 [ 0.43 , 0.56 ]
489 [ 0.67 , 0.90 ]
490 [ 0.86 , 1.32 ]
491 [ 1.01 , 1.79 ]
492 [ 1.15 , 2.33 ]
493 [ -1 , -1 ] (max twenty pts)
494 IDovf=[6], NHYDovf=["KEN-OV"]
495 *%-----|-----|
496 *#*****
497 *# Catchment FRASER
498 *# - To Fraser-Clarke drain (north of the Jock)
499 *# - Developed land with assumed 43% imp.
500 *#*****
501 CONTINUOUS STANDHYD ID=[7], NHYD=["FRASER"], DT=[5]min, AREA=[90](ha),
502 XIMP=[0.25], TIMP=[0.25], DWF=[0](cms), LOSS=[2],
503 SCS curve number CN=[80],
504 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
505 LGP=[40](m), MNP=[0.25], SCP=[0](min),
506 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
507 LGI=[775](m), MNI=[0.013], SCI=[0](min),
508 Continuous simulation parameters:
509 IaREcper=[4](hrs), IaREcimp=[4](hrs),
510 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
511 InterEventTime=[18](hrs), END=-1
512
513 *%-----|-----|
514 ROUTE RESERVOIR IDout=[8], NHYD=["MS_P2"], IDin=[7],
515 RDT=[5](min),
516 TABLE of ( OUTFLOW-STORAGE ) values
517 (cms) - (ha-m)
518 [ 0.0 , 0.0 ]
519 [ 0.04 , 0.36 ]
520 [ -1 , -1 ] (max twenty pts)
521 IDovf=[9], NHYDovf=["P2-OVF"]
522 *%-----|-----|
523 ADD HYD IDsum=[ 4 ], NHYD=["SN_KB"], IDs to add=[5,6,8,9,1]
524 *%-----|-----|
525 SAVE HYD ID=[4], # OF PCYCLES=[-1], ICASEsh=[1]
526 HYD_COMMENT=["Total Flows at Ken-Burnett Outlet"]
527 *%-----|-----|
528 *# Hydrograph from Node Kennedy - Burnett Drain to Node Todd Drain

```

```

529  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 3633
530  *#
531  ROUTE CHANNEL      IDout=[1], NHYD=["N_TO"] ,IDin=[4] ,
532                    RDT=[5](min),
533                    CHLGTH=[650](m),  CHSLOPE=[0.0498](%),
534                    FPSLOPE=[0.0498](%),
535                    SECNUM=[1.0],      NSEG=[3]
536                    ( SEGRROUGH, SEGDIST (m))=
537                      [0.050,-23.74
538                      -0.035,23.74
539                      0.050,74.7] NSEG times
540                    ( DISTANCE (m), ELEVATION (m))=
541                      [-74.18, 92.5]
542                      [-65.96, 92]
543                      [-54.17, 91.5]
544                      [-29.24, 91]
545                      [-27.41, 90.5]
546                      [-25.64, 90]
547                      [-23.74, 89.5]
548                      [-22,89. 26]
549                      [-20, 88.51]
550                      [-19, 88.32]
551                      [-15, 88.1]
552                      [-10, 88.11]
553                      [-5, 88.17]
554                      [0, 88.27]
555                      [5, 88.19]
556                      [10, 88.06]
557                      [15, 88.48]
558                      [16, 88.7]
559                      [23.74, 89.5]
560                      [24.68, 90]
561                      [25.57, 90.5]
562                      [26.5, 91]
563                      [47.55, 91]
564                      [74.7, 92.5]
565  *%-----|-----|
566
567  *#*****
568  *#      Catchment TODD
569  *#      - To Todd Drain (south of the Jock)
570  *#      - Subdivision with 43% imp. as per Barrhaven South MSS
571  *#*****
572  CONTINUOUS STANDHYD ID=[3], NHYD=["TODD"], DT=[5]min, AREA=[195](ha),
573                    XIMP=[0.43], TIMP=[0.43], DWF=[0](cms), LOSS=[2],
574                    SCS curve number CN=[77],
575                    Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
576                    LGP=[40](m), MNP=[0.25], SCP=[0](min),
577                    Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
578                    LGI=[1140](m), MNI=[0.013], SCI=[0](min),
579                    Continuous simulation parameters:
580                    IaRECper=[4](hrs), IaRECimp=[4](hrs),
581                    SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
582                    InterEventTime=[18](hrs), END=-1
583
584  *#*****
585  *#      Todd Pond 3
586  *#      - Rating curve obtained from Barrhaven South MSS modeling
587  *#      - Tributary Drainage Area to MSS Pond 3 = 193 ha
588  *#*****
589  ROUTE RESERVOIR    IDout=[2],  NHYD=["MS_P3"],  IDin=[3],
590                    RDT=[5](min),
591                    TABLE of ( OUTFLOW-STORAGE ) values
592                    (cms) - (ha-m)
593                    [ 0.0 , 0.0 ]
594                    [ 0.08 , 0.78]

```

```

595                                     [ -1 , -1 ] (max twenty pts)
596                                     IDovf=[9], NHYDovf=["P3-OVF"]
597 *%-----|-----|
598 ADD HYD                               IDsum=[10], NHYD=["SN_TO"], IDs to add=[1,2,9]
599 *%-----|-----|
600 SAVE HYD                               ID=[ 10 ], # OF PCYCLES=[-1], ICASEsh=[1]
601                                     HYD_COMMENT=["Total Flows at Todd Drain"]
602 *%-----|-----|
603 *#
604 *# Hydrograph from Todd Drain routed to Corrigan Drain
605 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
606 *#
607 ROUTE CHANNEL                          IDout=[1], NHYD=["N_TO"] ,IDin=[10] ,
608                                     RDT=[5](min),
609                                     CHLGTH=[280](m), CHSLOPE=[0.033](%),
610                                     FPSLOPE=[0.033](%),
611                                     SECNUM=[1.0], NSEG=[3]
612                                     ( SEGROUGH, SEGDIST (m))=
613                                     [0.075,-17.72
614                                     -0.045,17.72
615                                     0.075,80.62] NSEG times
616                                     ( DISTANCE (m), ELEVATION (m))=
617                                     [-83.32, 90.00]
618                                     [-81.36, 89.50]
619                                     [-79.12, 89.00]
620                                     [-76.13, 88.50]
621                                     [-20.46, 88.00]
622                                     [-19.36, 87.50]
623                                     [-18.51, 87.00]
624                                     [-17.72, 86.50]
625                                     [-11.95, 85.24]
626                                     [-0.11, 85.12]
627                                     [11.49, 85.20]
628                                     [17.72, 86.50]
629                                     [19.74, 87.00]
630                                     [21.22, 87.50]
631                                     [22.68, 88.00]
632                                     [24.28, 88.50]
633                                     [26.79, 89.00]
634                                     [71.98, 90.00]
635                                     [80.62, 90.50]
636 *%-----|-----|
637 *#*****|*****|
638 *# Catchment CORRIG
639 *# - To Corrigan Drain (south of the Jock)
640 *# - Primarily Developed (medium density)
641 *#*****|*****|
642 CONTINUOUS STANDHYD ID=[2], NHYD=["CORRIG"], DT=[5]min, AREA=[149](ha),
643                                     XIMP=[0.45], TIMP=[0.45], DWF=[0](cms), LOSS=[2],
644                                     SCS curve number CN=[77],
645                                     Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
646                                     LGP=[40](m), MNP=[0.25], SCP=[0](min),
647                                     Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
648                                     LGI=[997](m), MNI=[0.013], SCI=[0](min),
649                                     Continuous simulation parameters:
650                                     IaREcper=[4](hrs), IaREcimp=[4](hrs),
651                                     SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
652                                     InterEventTime=[18](hrs), END=-1
653
654 *%-----|-----|
655 *#*****|*****|
656 *# Corrigan Pond 1
657 *# - Rating curve obtained from Barrhaven South MSS modeling
658 *# - Tributary Drainage Area to MSS Pond 1 = 145 ha
659 *#*****|*****|
660 ROUTE RESERVOIR IDout=[5], NHYD=["MS_P1"], IDin=[2],

```



```

661 RDT=[5](min),
662 TABLE of ( OUTFLOW-STORAGE ) values
663 (cms) - (ha-m)
664 [ 0.0 , 0.0 ]
665 [ 0.06 , 0.58]
666 [ -1 , -1 ] (max twenty pts)
667 IDovf=[4], NHYDovf=["P1-OVF"]
668 *%-----|-----|
669 ADD HYD IDsum=[ 3 ], NHYD=["SN_CO"], IDs to add=[1,4,5]
670 *%-----|-----|
671 SAVE HYD ID=[ 3 ], # OF PCYCLES=[-1], ICASEsh=[1]
672 HYD_COMMENT=["Total Flows at Corrigan Drain"]
673 *%-----|-----|
674 *#
675 *# Hydrograph from Corrigan Drain routed to Jockvale Road
676 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
677 *#
678 ROUTE CHANNEL IDout=[1], NHYD=["N_MI"] ,IDin=[3] ,
679 RDT=[5](min),
680 CHLGTH=[580](m), CHSLOPE=[0.4448](%),
681 FPSLOPE=[0.4448](%),
682 SECNUM=[1.0], NSEG=[3]
683 ( SEGROUGH, SEGDIST (m))=
684 [0.075,-17.72
685 -0.045,17.72
686 0.075,80.62] NSEG times
687 ( DISTANCE (m), ELEVATION (m))=
688 [-83.32, 90.00]
689 [-81.36, 89.50]
690 [-79.12, 89.00]
691 [-76.13, 88.50]
692 [-20.46, 88.00]
693 [-19.36, 87.50]
694 [-18.51, 87.00]
695 [-17.72, 86.50]
696 [-11.95, 85.24]
697 [-0.11, 85.12]
698 [11.49, 85.20]
699 [17.72, 86.50]
700 [19.74, 87.00]
701 [21.22, 87.50]
702 [22.68, 88.00]
703 [24.28, 88.50]
704 [26.79, 89.00]
705 [71.98, 90.00]
706 [80.62, 90.50]
707 *%-----|-----|
708 *#*****
709 *# Catchment MILLS
710 *# - To SWM Facility north of the Jock
711 *# - Primarily residential development
712 *#*****
713 CONTINUOUS STANDHYD ID=[2], NHYD=["MILLS"], DT=[5]min, AREA=[139](ha),
714 XIMP=[0.38], TIMP=[0.38], DWF=[0](cms), LOSS=[2],
715 SCS curve number CN=[74],
716 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
717 LGP=[40](m), MNP=[0.25], SCP=[0](min),
718 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
719 LGI=[963](m), MNI=[0.013], SCI=[0](min),
720 Continuous simulation parameters:
721 IaRECper=[4](hrs), IaRECimp=[4](hrs),
722 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
723 InterEventTime=[18](hrs), END=-1
724
725 *%-----|-----|
726 *#*****

```

```

727 *# Chapman Mills SWM Pond
728 *# - Rating curve obtained from CCL hydraulic modeling
729 *#*****
730 ROUTE RESERVOIR IDout=[5], NHYD=["MILL_P"], IDin=[2],
731 RDT=[5](min),
732 TABLE of ( OUTFLOW-STORAGE ) values
733 (cms) - (ha-m)
734 [ 0.0 , 0.0 ]
735 [ 0.01 , 0.01]
736 [ 0.05 , 0.06]
737 [ 0.09 , 0.11]
738 [ 0.13 , 0.15]
739 [ 0.18 , 0.19]
740 [ 0.28 , 0.28]
741 [ 0.37 , 0.34]
742 [ 0.45 , 0.40]
743 [ 0.51 , 0.44]
744 [ 0.56 , 0.47]
745 [ 0.64 , 0.52]
746 [ 0.76 , 0.59]
747 [ 0.86 , 0.65]
748 [ 1.09 , 0.78]
749 [ 1.44 , 0.96]
750 [ 3.18 , 1.84]
751 [ 4.05 , 2.31]
752 [ -1 , -1 ] (max twenty pts)
753 IDovf=[4], NHYDovf=["MIL-OV"]
754 *%-----|-----|
755 ADD HYD IDsum=[ 3 ], NHYD=["SN_MI"], IDs to add=[1,4,5]
756 *%-----|-----|
757 SAVE HYD ID=[ 3 ], # OF PCYCLES=[-1], ICASEsh=[1]
758 HYD_COMMENT=["Total Flows at Jockvale Road"]
759 *%-----|-----|
760 *#
761 *# Hydrograph from Jockvale Road routed to Heart's Desire
762 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 689
763 *#
764 ROUTE CHANNEL IDout=[1], NHYD=["N_DE"] ,IDin=[3] ,
765 RDT=[5](min),
766 CHLGTH=[1962](m), CHSLOPE=[0.2227](%),
767 FPSLOPE=[0.2227](%),
768 SECNUM=[1.0], NSEG=[3]
769 ( SEGRROUGH, SEGDIST (m))=
770 [0.075,-17.56
771 -0.045,18.27
772 0.075,67.59] NSEG times
773 ( DISTANCE (m), ELEVATION (m))=
774 [-111.59, 88.00]
775 [-102.58, 87.50]
776 [-96.20, 87.00]
777 [-90.04, 86.50]
778 [-84.02, 86.00]
779 [-77.54, 85.50]
780 [-54.07, 85.00]
781 [-39.43, 84.50]
782 [-28.30, 84.00]
783 [-24.12, 83.50]
784 [-22.30, 83.00]
785 [-20.55, 82.50]
786 [-17.56, 82.00]
787 [-12.63, 81.22]
788 [-0.11, 80.75]
789 [11.55, 81.22]
790 [18.27, 82.00]
791 [19.82, 82.50]
792 [22.48, 83.00]

```

793 [27.90, 83.50]  
794 [29.31, 84.00]  
795 [30.81, 84.50]  
796 [32.51, 85.00]  
797 [34.24, 85.50]  
798 [36.34, 86.00]  
799 [41.65, 86.50]  
800 [62.64, 87.00]  
801 [65.14, 87.50]  
802 [67.59, 88.00]

\*%-----|-----|  
804 \*#\*\*\*\*\*  
805 \*# Catchment DESIRE  
806 \*# - To Jock River (north of the Jock)  
807 \*# - Rural-estate subdivision (Heart's Desire Community)  
808 \*#\*\*\*\*\*  
809 **CONTINUOUS STANDHYD** ID=[2], NHYD=["DESIRE"], DT=[5]min, AREA=[24](ha),  
810 XIMP=[0.25], TIMP=[0.25], DWF=[0](cms), LOSS=[2],  
811 SCS curve number CN=[77],  
812 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),  
813 LGP=[40](m), MNP=[0.25], SCP=[0](min),  
814 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),  
815 LGI=[400](m), MNI=[0.013], SCI=[0](min),  
816 Continuous simulation parameters:  
817 IaREcper=[4](hrs), IaREcimp=[4](hrs),  
818 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),  
819 InterEventTime=[18](hrs), END=-1

\*%-----|-----|  
822 \*#\*\*\*\*\*  
823 \*# Catchment JOCKVA  
824 \*# - To Jockvale SWM Facility  
825 \*# - Residential development & golf course  
826 \*#\*\*\*\*\*  
827 **CONTINUOUS STANDHYD** ID=[3], NHYD=["JOCKVA"], DT=[5]min, AREA=[252](ha),  
828 XIMP=[0.50], TIMP=[0.50], DWF=[0](cms), LOSS=[2],  
829 SCS curve number CN=[74],  
830 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),  
831 LGP=[40](m), MNP=[0.25], SCP=[0](min),  
832 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),  
833 LGI=[1296](m), MNI=[0.013], SCI=[0](min),  
834 Continuous simulation parameters:  
835 IaREcper=[4](hrs), IaREcimp=[4](hrs),  
836 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),  
837 InterEventTime=[18](hrs), END=-1

\*%-----|-----|  
840 \*#\*\*\*\*\*  
841 \*# Jockvale SWM Facility  
842 \*# - Rating curve obtained from Jockvale Servicing Study (CCL 1999)  
843 \*#\*\*\*\*\*

844 **ROUTE RESERVOIR** IDout=[5], NHYD=["JOCK\_P"], IDin=[3],  
845 RDT=[5](min),  
846 TABLE of ( OUTFLOW-STORAGE ) values  
847 (cms) - (ha-m)  
848 [ 0.0 , 0.0 ]  
849 [ 0.27 , 0.03 ]  
850 [ 0.28 , 0.55 ]  
851 [ 0.29 , 1.14 ]  
852 [ 0.30 , 1.80 ]  
853 [ 0.31 , 2.32 ]  
854 [ 1.12 , 2.87 ]  
855 [ 2.92 , 3.45 ]  
856 [ 4.64 , 4.07 ]  
857 [ 6.69 , 4.72 ]  
858 [ 9.02 , 5.39 ]

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859             [ 11.62 , 6.10]
860             [ 14.42 , 6.85]
861             [ 17.45 , 7.62]
862             [ 20.69 , 8.44]
863             [ 24.08 , 9.28]
864             [ 27.68 , 10.17]
865             [ -1 , -1 ] (max twenty pts)
866             IDovf=[4], NHYDovf=["JO-OVF"]
867 *%-----|-----|
868 ADD HYD      IDsum=[ 3 ], NHYD=["SN_DE"], IDs to add=[1,2,4,5]
869 *%-----|-----|
870 SAVE HYD     ID=[ 3 ], # OF PCYCLES=[-1], ICASEsh=[1]
871             HYD_COMMENT=["Total Flows at Heart's Desire"]
872 *%-----|-----|
873 *#
874 *# Hydrograph from Heart's Desire routed to Rideau River
875 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 0
876 *#
877 ROUTE CHANNEL IDout=[1], NHYD=["N1"] ,IDin=[3] ,
878             RDT=[5](min),
879             CHLGTH=[563](m), CHSLOPE=[0.9668](%),
880             FPSLOPE=[0.9668](%),
881             SECNUM=[1.0], NSEG=[3]
882             ( SEGROUGH, SEGDIST (m))=
883             [0.075,-30.20
884             -0.045,30.20
885             0.075,168.81] NSEG times
886             ( DISTANCE (m), ELEVATION (m))=
887             [-170.17, 86.00]
888             [-164.75, 85.50]
889             [-158.08, 85.00]
890             [-113.12, 82.00]
891             [-98.46, 81.50]
892             [-92.24, 81.00]
893             [-86.88, 80.50]
894             [-81.54, 80.00]
895             [-74.36, 79.50]
896             [-63.54, 79.00]
897             [-39.23, 78.50]
898             [-34.51, 78.00]
899             [-33.01, 77.50]
900             [-30.20, 77.00]
901             [-13.42, 76.18]
902             [-1.14, 76.09]
903             [17.06, 76.18]
904             [30.20, 77.00]
905             [32.95, 77.50]
906             [34.06, 78.00]
907             [35.11, 78.50]
908             [36.32, 79.00]
909             [37.74, 79.50]
910             [48.48, 81.50]
911             [49.25, 82.00]
912             [55.61, 84.50]
913             [57.09, 85.00]
914             [59.51, 85.50]
915             [64.34, 86.00]
916             [66.30, 86.00]
917             [76.71, 86.50]
918             [101.83, 86.50]
919             [119.73, 87.00]
920             [142.04, 87.50]
921             [168.81, 88.00]
922 *%-----|-----|
923 *#*****
924 *# Catchment S-2

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925 *# - To Jock River (north and south)
926 *# - Undeveloped floodplain and river
927 *#*****
928 CONTINUOUS NASHYD ID=[2], NHYD=["S-2"], DT=[5]min, AREA=[102](ha),
929 DWF=[0](cms), CN/C=[72], IA=[4.67](mm),
930 N=[3], TP=[0.40]hrs,
931 Continuous simulation parameters:
932 IaRECper=[4](hrs),
933 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
934 InterEventTime=[12](hrs)
935 Baseflow simulation parameters:
936 BaseFlowOption=[1] ,
937 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
938 VHydCond=[0.055](mm/hr), END=-1
939
940 *%-----|-----|
941 ADD HYD IDsum=[ 3 ], NHYD=["SN_N1"], IDs to add=[1,2]
942 *%-----|-----|
943 SAVE HYD ID=[ 3 ], # OF PCYCLES=[-1], ICASEsh=[1]
944 HYD_COMMENT=["Total Flows at Rideau River"]
945 *%-----|-----|
946 *% 5 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
947 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[005]
948 *% ["C24SC005.stm"] <--storm filename, one per line for NSTORM time
949 *%-----|-----|
950 *% 10 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
951 *%START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[010]
952 *% ["C24SC010.stm"] <--storm filename, one per line for NSTORM time
953 *%-----|-----|
954 *% 25 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
955 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[025]
956 *% ["C24SC025.stm"] <--storm filename, one per line for NSTORM time
957 *%-----|-----|
958 *% 50 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
959 *%START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[050]
960 *% ["C24SC050.stm"] <--storm filename, one per line for NSTORM time
961 *%-----|-----|
962 *% 100 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
963 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
964 *% ["C24SC100.stm"] <--storm filename, one per line for NSTORM time
965 *%-----|-----|
966
967 *#####
968 FINISH
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00001 .....
00002 .....
00003 SSSSS W W M H H Y Y M M O O O 999 999 .....
00004 S W M M M M M H H H H Y Y M M M O O # 9 9 9 9 Ver5 Beta
00005 SSSSS W W M M M H H H H Y Y M M M O O # 9 9 9 9 Ver5 Beta
00006 S W M M M H H Y Y M M O O 9999 9999 Sept 2000
00007 SSSSS W W M M M H H Y Y M M O O 9 9 9 9 .....
00008 .....
00009 Stormwater Management Hydrologic Model
00010 .....
00011 Stormwater Management Hydrologic Model
00012 .....
00013 ***** SMWHD00 Ver/5 Beta *****
00014 ***** A single event and continuous hydrologic simulation model *****
00015 ***** based on the principles of HWSO and its successor *****
00016 ***** OTTHYD03 and OTTHYD09 *****
00017 ***** Distributed by: J.P. Sabourin and Associates Inc. *****
00018 ***** Ottawa, Ontario: (613) 727-5199 *****
00019 ***** Ottawa, Quebec: (819) 243-6188 *****
00020 ***** E-Mail: smwbyso@jfsa.com *****
00021 *****
00022 *****
00023 *****
00024 ***** Licensed user: Ottawa - Ottawa - 604 *****
00025 ***** SERIAL#:3783815 *****
00026 *****
00027 *****
00028 *****
00029 ***** PROGRAM ARRAY DIMENSIONS *****
00030 ***** Maximum value for ID numbers: 10 *****
00031 ***** Max. number of rainfall points: 52750 *****
00032 ***** Max. number of flow points: 52750 *****
00033 *****
00034 ***** DESCRIPTION SUMMARY TABLE HEADERS (units depend on MOUTPUT in START) *****
00035 ***** ID: Hydrograph identification numbers. (1-10) *****
00036 ***** HNRID: Hydrograph reference numbers. (6 digits or characters) *****
00037 ***** AREA: Drainage area associated with hydrograph, (in) or (ha). *****
00038 ***** QPEAK: Peak flow of simulated hydrograph. (ft3/s) or (m3/s). *****
00039 ***** TpeakDate_hh:mm is the date and time of the peak flow. *****
00040 ***** R.V.: Runoff volume of simulated hydrograph, (in) or (mm). *****
00041 ***** R.C.: Runoff Coefficient of simulated hydrograph. (ratio). *****
00042 ***** : see WARNING or NOTE message printed at end of run. *****
00043 ***** : *****
00044 ***** *****
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00051 ***** *****
00052 ***** *****
00053 ***** S U M M A R Y O U T P U T *****
00054 ***** *****
00055 ***** DATE: 2006-11-15 TIME: 14:33:15 RUN COUNTER: 000132 *****
00056 ***** *****
00057 ***** *****
00058 ***** Input filename: C:\Navin\OCT08-1\CORNTIN-1\SM_POST\SM_POST.dat *****
00059 ***** Output filename: C:\Navin\OCT08-1\CORNTIN-1\SM_POST\SM_POST.out *****
00060 ***** Summary filename: C:\Navin\OCT08-1\CORNTIN-1\SM_POST\SM_POST.sum *****
00061 ***** User comments: *****
00062 ***** 1 *****
00063 ***** 2 *****
00064 ***** 3 *****
00065 ***** *****
00066 ***** *****
00067 ***** PROJECT NAME [Jock River Reach 1 Subwatershed Study/Project #: 160400044] *****
00068 ***** Date [October 2006] *****
00069 ***** Modeller [Nevin Gautam/ Original by Ana M Paeres] *****
00070 ***** Company [Stantec] *****
00071 ***** License # [3824306] *****
00072 ***** *****
00073 ***** *****
00074 ***** END OF RUN : 1 *****
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014977 # Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
014980 02510044 -----ID:HYDR-----AREA-----OPEAK-TPeakDate_bhm-----R-V-R-C-
014981 ROUTE CHANNEL -> 03:IN_DE 54904.01 11.061 No_date 35:20 29.29 n/a
014982 [R/S/N= 5.00] out<- 01:R_TO 54904.01 11.070 No_date 35:20 29.29 n/a
014983 [L/S/N= 280 / .037/.045]
014984 [Vmax= 217.0;Dmax= 3.188]
015000 # Catchment CORRID
015001 # - To Corrigan Drain (south of the Jock)
015002 # - Primarily Developed (medium density)
015003 # - Residential development & golf course
015009 02510044 -----ID:HYDR-----AREA-----OPEAK-TPeakDate_bhm-----R-V-R-C-
015010 CONTINUOUS STANDBYD02:CORRID 149.00 14.272 No_date 28:05 49.32 .663
015011 [L/S/N= 2 CM= 77.0]
015012 [Previous area: IArea= 4.67;SLUP=1.00;LDP= 40.0;MNP=250;ICP= 0]
015013 [Impervious area: IAlp= 1.57;SLIP=1.00;LMI= 997.0;MMI=.013;SICI= .0]
015014 [Infiltration: IInfil= 4.00; IARECPer= 4.00]
015015 [SIN= 31.15; SMA=207.66; SE=.010]
015016 [L/S/N= 21.709;Dmax= .034]
015017 # Rating curve obtained from Barrhaven South MSE modeling
015018 # - Tributary Drainage Area to MSE Pond 1 = 145 ha
015019 # - Rating curve obtained from Barrhaven South MSE modeling
015020 # - Tributary Drainage Area to MSE Pond 1 = 145 ha
015021 [InterEventTime= 12.00]
015022 02510044 -----ID:HYDR-----AREA-----OPEAK-TPeakDate_bhm-----R-V-R-C-
015023 ROUTE RESERVOIR -> 02:CORRID 149.00 14.272 No_date 28:05 49.32 n/a
015024 [R/S/N= 5.00] out<- 01:R_TO 54904.01 11.061 No_date 35:20 29.29 n/a
015025 [L/S/N= 280 / .037/.045]
015026 [Vmax= 217.0;Dmax= 3.188]
015027 (MetStoUsed=1720E+01, TotVolVol=.000E+00, N-Off= 0, TotDurVol= 16.96)
015028 ADD HYD 01:R_TO 54904.01 11.070 No_date 35:20 29.29 n/a
015029 [Infiltration: IInfil= 4.00; IARECPer= 4.00]
015030 [SIN= 31.15; SMA=207.66; SE=.010]
015031 [L/S/N= 21.709;Dmax= .034]
015032 02510044 -----ID:HYDR-----AREA-----OPEAK-TPeakDate_bhm-----R-V-R-C-
015033 SAVED HYD 03:IN_CO 55053.01 11.193 No_date 35:20 29.35 n/a
015034 frame c:\Navin\OCTOBS-1\CONTIN-1\VMR_POSTV-IR-SM_CO.025
015035 remark:Total Flows at Corrigan Drain
015036 #
015037 # Hydrograph from Corrigan Drain routed to Jockvale Road
015038 # Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
015039 #
015040 02510044 -----ID:HYDR-----AREA-----OPEAK-TPeakDate_bhm-----R-V-R-C-
015041 ROUTE CHANNEL -> 03:IN_DE 55053.01 11.200 No_date 35:25 29.35 n/a
015042 [R/S/N= 5.00] out<- 01:R_TO 55053.01 11.200 No_date 35:25 29.35 n/a
015043 [L/S/N= 280 / .037/.045]
015044 [Vmax= 1.965;Dmax= 1.852]
015045 # Catchment MILLS
015046 # - To SWM Facility north of the Jock
015047 # - Primarily Residential development
015048 # - Residential development & golf course
015049 02510044 -----ID:HYDR-----AREA-----OPEAK-TPeakDate_bhm-----R-V-R-C-
015050 CONTINUOUS STANDBYD03:MILLS 139.00 11.666 No_date 28:05 44.62 .600
015051 [L/S/N= 38;TIMP= 38]
015052 [Previous area: IArea= 4.67;SLUP=1.00;LDP= 40.0;MNP=250;ICP= 0]
015053 [Impervious area: IAlp= 1.57;SLIP=1.00;LMI= 963.0;MMI=.013;SICI= .0]
015054 [Infiltration: IInfil= 4.00; IARECPer= 4.00]
015055 [SIN= 31.15; SMA=241.49; SE=.010]
015056 [L/S/N= 47.0;Dmax= .034]
015057 # Chapman Mills SWM Pond
015058 # Rating curve obtained from CCL hydraulic modeling
015059 # - Rating curve obtained from CCL hydraulic modeling
015060 # - Rating curve obtained from CCL hydraulic modeling
015061 [InterEventTime= 12.00]
015062 02510044 -----ID:HYDR-----AREA-----OPEAK-TPeakDate_bhm-----R-V-R-C-
015063 ROUTE RESERVOIR -> 03:MILLS 139.00 11.666 No_date 28:05 44.62 n/a
015064 [R/S/N= 5.00] out<- 03:MILLS 139.00 11.666 No_date 28:05 44.62 n/a
015065 [L/S/N= 5.00] out<- 04:ML-OF 0.00 .000 No_date 0:00 .00 n/a
015066 (MetStoUsed=.2157E+01, TotVolVol=.000E+00, N-Off= 0, TotDurVol= 0.00)
015067 02510044 -----ID:HYDR-----AREA-----OPEAK-TPeakDate_bhm-----R-V-R-C-
015068 ADD HYD 01:R_TO 55053.01 11.200 No_date 35:25 29.35 n/a
015069 [Infiltration: IInfil= 4.00; IARECPer= 4.00]
015070 [SIN= 31.15; SMA=207.66; SE=.010]
015071 [L/S/N= 21.709;Dmax= .034]
015072 [Previous area: IArea= 4.67;SLUP=1.00;LDP= 40.0;MNP=250;ICP= 0]
015073 [Impervious area: IAlp= 1.57;SLIP=1.00;LMI= 997.0;MMI=.013;SICI= .0]
015074 [Infiltration: IInfil= 4.00; IARECPer= 4.00]
015075 [SIN= 31.15; SMA=207.66; SE=.010]
015076 [L/S/N= 21.709;Dmax= .034]
015077 # Hydrograph from Jockvale Road routed to Heart's Desire
015078 # Channel X-Section obtained from RVCA Hydraulic Model - Station 689
015079 #
015080 02510052 -----ID:HYDR-----AREA-----OPEAK-TPeakDate_bhm-----R-V-R-C-
015081 ROUTE CHANNEL -> 03:IN_DE 55192.01 11.709 No_date 35:25 29.35 n/a
015082 [R/S/N= 5.00] out<- 01:R_DE 55192.01 11.156 No_date 36:05 29.38 n/a
015083 [L/S/N= 1982 / .227/.045]
015084 [Vmax= 940.0;Dmax= 2.61]
015085 # Catchment OKEEFE
015086 # - To Jock River (north of the Jock)
015087 # - Rural estate subdivision (Heart's Desire Community)
015088 # - Residential development & golf course
015089 02510052 -----ID:HYDR-----AREA-----OPEAK-TPeakDate_bhm-----R-V-R-C-
015090 CONTINUOUS STANDBYD04:OKEEFE 24.00 2.012 No_date 28:00 40.77 .348
015091 [L/S/N= 25;TIMP= 25]
015092 [Previous area: IArea= 4.67;SLUP=1.00;LDP= 40.0;MNP=250;ICP= 0]
015093 [Impervious area: IAlp= 1.57;SLIP=1.00;LMI= 400.0;MMI=.013;SICI= .0]
015094 [Infiltration: IInfil= 4.00; IARECPer= 4.00]
015095 [SIN= 31.15; SMA=207.66; SE=.010]
015096 [L/S/N= 31.15; SMA=207.66; SE=.010]
015097 # Catchment JOCKVA
015098 # - To Jockvale SWM Facility
015099 # - Residential development & golf course
015100 # - Residential development & golf course
015101 # - Residential development & golf course
015102 02510054 -----ID:HYDR-----AREA-----OPEAK-TPeakDate_bhm-----R-V-R-C-
015103 CONTINUOUS STANDBYD05:JOCKVA 252.00 22.732 No_date 28:05 50.08 .673
015104 [L/S/N= 50;TIMP= 50]
015105 [Previous area: IArea= 4.67;SLUP=1.00;LDP= 40.0;MNP=250;ICP= 0]
015106 [Impervious area: IAlp= 1.57;SLIP=1.00;LMI= 1296.0;MMI=.013;SICI= .0]
015107 [Infiltration: IInfil= 4.00; IARECPer= 4.00]
015108 [SIN= 36.67; SMA=344.49; SE=.010]
015109 [L/S/N= 36.67; SMA=344.49; SE=.010]
015110 # Technical SWM Facility
015111 # - Rating curve obtained from Jockvale Servicing Study (CCL 1999)
015112 # - Rating curve obtained from Jockvale Servicing Study (CCL 1999)
015113 # - Rating curve obtained from Jockvale Servicing Study (CCL 1999)
015114 02510055 -----ID:HYDR-----AREA-----OPEAK-TPeakDate_bhm-----R-V-R-C-
015115 ROUTE RESERVOIR -> 02:JOCKVA 252.00 22.732 No_date 28:05 50.08 n/a
015116 [R/S/N= 5.00] out<- 03:JOCKVA 252.00 22.732 No_date 28:05 50.08 n/a
015117 [R/S/N= 5.00] out<- 04:JOCKVA 252.00 22.732 No_date 28:05 50.08 n/a
015118 (MetStoUsed=.5153E+00, TotVolVol=.000E+00, N-Off= 0, TotDurVol= 0.00)
015119 [Infiltration: IInfil= 4.00; IARECPer= 4.00]
015120 [SIN= 36.67; SMA=344.49; SE=.010]
015121 02510056 -----ID:HYDR-----AREA-----OPEAK-TPeakDate_bhm-----R-V-R-C-
015122 ADD HYD 01:R_DE 55192.01 11.156 No_date 36:05 29.38 n/a
015123 [Infiltration: IInfil= 4.00; IARECPer= 4.00]
015124 [SIN= 31.15; SMA=207.66; SE=.010]
015125 [L/S/N= 21.709;Dmax= .034]
015126 [Previous area: IArea= 4.67;SLUP=1.00;LDP= 40.0;MNP=250;ICP= 0]
015127 [Impervious area: IAlp= 1.57;SLIP=1.00;LMI= 1296.0;MMI=.013;SICI= .0]
015128 [Infiltration: IInfil= 4.00; IARECPer= 4.00]
015129 [SIN= 31.15; SMA=207.66; SE=.010]
015130 [L/S/N= 21.709;Dmax= .034]
015131 # Hydrograph from Heart's Desire routed to Rideau River
015132 # Channel X-Section obtained from RVCA Hydraulic Model - Station 0
015133 #
015134 02510058 -----ID:HYDR-----AREA-----OPEAK-TPeakDate_bhm-----R-V-R-C-
015135 ROUTE CHANNEL -> 03:IN_DE 55468.00 11.074 No_date 36:00 29.48 n/a
015136 [R/S/N= 5.00] out<- 01:R_DE 55468.00 11.074 No_date 36:05 29.48 n/a
015137 [L/S/N= 583 / .967/.045]
015138 [Vmax= 2.709;Dmax= .034]
015139 # Catchment R-2
015140 # - To Jock River (north and south)
015141 # - Undeveloped floodplain and river
015142 # - Undeveloped floodplain and river
015143 # - Undeveloped floodplain and river
015144 02510059 -----ID:HYDR-----AREA-----OPEAK-TPeakDate_bhm-----R-V-R-C-
015145 CONTINUOUS STANDBYD06:R2 102.00 3.924 No_date 28:20 30.12 .405
015146 [L/S/N= 72.0; R= 3.00]
015147 [Previous area: IArea= 4.67;SLUP=1.00;LDP= 40.0;MNP=250;ICP= 0]
015148 [Impervious area: IAlp= 1.57;SLIP=1.00;LMI= 1296.0;MMI=.013;SICI= .0]
015149 [Infiltration: IInfil= 4.00; IARECPer= 4.00]
015150 [SIN= 36.67; SMA=344.49; SE=.010]
015151 ADD HYD 01:R_DE 55192.01 11.156 No_date 36:05 29.38 n/a
015152 [Infiltration: IInfil= 4.00; IARECPer= 4.00]
015153 [SIN= 31.15; SMA=207.66; SE=.010]
015154 [L/S/N= 21.709;Dmax= .034]
015155 [Previous area: IArea= 4.67;SLUP=1.00;LDP= 40.0;MNP=250;ICP= 0]
015156 [Impervious area: IAlp= 1.57;SLIP=1.00;LMI= 1296.0;MMI=.013;SICI= .0]
015157 [Infiltration: IInfil= 4.00; IARECPer= 4.00]
015158 [SIN= 31.15; SMA=207.66; SE=.010]
015159 [L/S/N= 21.709;Dmax= .034]
015160 # Hydrograph from Rideau River
015161 # Channel X-Section obtained from RVCA Hydraulic Model - Station 616
015162 #
015163 02510061 -----ID:HYDR-----AREA-----OPEAK-TPeakDate_bhm-----R-V-R-C-
015164 ROUTE CHANNEL -> 03:IN_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015165 [R/S/N= 5.00] out<- 01:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015166 [L/S/N= 1187.0 / .076/.035]
015167 [Vmax= 1.826;Dmax= .032]
015168 # Catchment FOSTER
015169 # - To Foster ditch (north of the Jock)
015170 # - Partially developed (medium density); remaining agricultural
015171 # - Partially developed (medium density); remaining agricultural
015172 02510062 -----ID:HYDR-----AREA-----OPEAK-TPeakDate_bhm-----R-V-R-C-
015173 CONTINUOUS STANDBYD07:FOSTER 373.00 38.921 No_date 28:05 65.13 .735
015174 [L/S/N= 50;TIMP= 55]
015175 [Previous area: IArea= 4.67;SLUP=1.00;LDP= 40.0;MNP=250;ICP= 0]
015176 [Impervious area: IAlp= 1.57;SLIP=1.00;LMI= 1577.0;MMI=.013;SICI= .0]
015177 [Infiltration: IInfil= 4.00; IARECPer= 4.00]
015178 [SIN= 36.67; SMA=344.49; SE=.010]
015179 # Foster Pond
015180 # - Rating curve obtained assuming 40m/h in 24 hours for quality control
015181 # - and a ratio of the catchment area to the West Clarke pond rating curve
015182 # - from the MSF for the next coordinates
015183 # - from the MSF for the next coordinates
015184 # - from the MSF for the next coordinates
015185 02510063 -----ID:HYDR-----AREA-----OPEAK-TPeakDate_bhm-----R-V-R-C-
015186 ROUTE RESERVOIR -> 02:FOSTER 373.00 38.921 No_date 28:05 65.13 n/a
015187 [R/S/N= 5.00] out<- 04:P_FOS 48.28 .200 No_date 24:30 65.13 n/a
015188 [R/S/N= 5.00] out<- 05:P_FOS 124.72 18.557 No_date 28:10 65.13 n/a
015189 (MetStoUsed=.1720E+01, TotVolVol=.2155E+02, N-Off= 2, TotDurVol= 16.96)
015190 [Infiltration: IInfil= 4.00; IARECPer= 4.00]
015191 [SIN= 31.15; SMA=207.66; SE=.010]
015192 [L/S/N= 5.00] out<- 01:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015193 [L/S/N= 5.00] out<- 02:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015194 [L/S/N= 5.00] out<- 03:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015195 [L/S/N= 5.00] out<- 04:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015196 [L/S/N= 5.00] out<- 05:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015197 [L/S/N= 5.00] out<- 06:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015198 [L/S/N= 5.00] out<- 07:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015199 [L/S/N= 5.00] out<- 08:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015200 [L/S/N= 5.00] out<- 09:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015201 [L/S/N= 5.00] out<- 10:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015202 [L/S/N= 5.00] out<- 11:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015203 [L/S/N= 5.00] out<- 12:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015204 [L/S/N= 5.00] out<- 13:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015205 [L/S/N= 5.00] out<- 14:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015206 [L/S/N= 5.00] out<- 15:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015207 [L/S/N= 5.00] out<- 16:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015208 [L/S/N= 5.00] out<- 17:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015209 [L/S/N= 5.00] out<- 18:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015210 [L/S/N= 5.00] out<- 19:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015211 [L/S/N= 5.00] out<- 20:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015212 [L/S/N= 5.00] out<- 21:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015213 [L/S/N= 5.00] out<- 22:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015214 [L/S/N= 5.00] out<- 23:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015215 [L/S/N= 5.00] out<- 24:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015216 [L/S/N= 5.00] out<- 25:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015217 [L/S/N= 5.00] out<- 26:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015218 [L/S/N= 5.00] out<- 27:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015219 [L/S/N= 5.00] out<- 28:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015220 [L/S/N= 5.00] out<- 29:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015221 [L/S/N= 5.00] out<- 30:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015222 [L/S/N= 5.00] out<- 31:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015223 [L/S/N= 5.00] out<- 32:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015224 [L/S/N= 5.00] out<- 33:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015225 [L/S/N= 5.00] out<- 34:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015226 [L/S/N= 5.00] out<- 35:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015227 [L/S/N= 5.00] out<- 36:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015228 [L/S/N= 5.00] out<- 37:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015229 [L/S/N= 5.00] out<- 38:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015230 [L/S/N= 5.00] out<- 39:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015231 [L/S/N= 5.00] out<- 40:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015232 [L/S/N= 5.00] out<- 41:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015233 [L/S/N= 5.00] out<- 42:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015234 [L/S/N= 5.00] out<- 43:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015235 [L/S/N= 5.00] out<- 44:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015236 [L/S/N= 5.00] out<- 45:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015237 [L/S/N= 5.00] out<- 46:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015238 [L/S/N= 5.00] out<- 47:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015239 [L/S/N= 5.00] out<- 48:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015240 [L/S/N= 5.00] out<- 49:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015241 [L/S/N= 5.00] out<- 50:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015242 [L/S/N= 5.00] out<- 51:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015243 [L/S/N= 5.00] out<- 52:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015244 [L/S/N= 5.00] out<- 53:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015245 [L/S/N= 5.00] out<- 54:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015246 [L/S/N= 5.00] out<- 55:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015247 [L/S/N= 5.00] out<- 56:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015248 [L/S/N= 5.00] out<- 57:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015249 [L/S/N= 5.00] out<- 58:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015250 [L/S/N= 5.00] out<- 59:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015251 [L/S/N= 5.00] out<- 60:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015252 [L/S/N= 5.00] out<- 61:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015253 [L/S/N= 5.00] out<- 62:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015254 [L/S/N= 5.00] out<- 63:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015255 [L/S/N= 5.00] out<- 64:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015256 [L/S/N= 5.00] out<- 65:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015257 [L/S/N= 5.00] out<- 66:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015258 [L/S/N= 5.00] out<- 67:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015259 [L/S/N= 5.00] out<- 68:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015260 [L/S/N= 5.00] out<- 69:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015261 [L/S/N= 5.00] out<- 70:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015262 [L/S/N= 5.00] out<- 71:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015263 [L/S/N= 5.00] out<- 72:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015264 [L/S/N= 5.00] out<- 73:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015265 [L/S/N= 5.00] out<- 74:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015266 [L/S/N= 5.00] out<- 75:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015267 [L/S/N= 5.00] out<- 76:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015268 [L/S/N= 5.00] out<- 77:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015269 [L/S/N= 5.00] out<- 78:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015270 [L/S/N= 5.00] out<- 79:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015271 [L/S/N= 5.00] out<- 80:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015272 [L/S/N= 5.00] out<- 81:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015273 [L/S/N= 5.00] out<- 82:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015274 [L/S/N= 5.00] out<- 83:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015275 [L/S/N= 5.00] out<- 84:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015276 [L/S/N= 5.00] out<- 85:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015277 [L/S/N= 5.00] out<- 86:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015278 [L/S/N= 5.00] out<- 87:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015279 [L/S/N= 5.00] out<- 88:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015280 [L/S/N= 5.00] out<- 89:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015281 [L/S/N= 5.00] out<- 90:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015282 [L/S/N= 5.00] out<- 91:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015283 [L/S/N= 5.00] out<- 92:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015284 [L/S/N= 5.00] out<- 93:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015285 [L/S/N= 5.00] out<- 94:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015286 [L/S/N= 5.00] out<- 95:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015287 [L/S/N= 5.00] out<- 96:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015288 [L/S/N= 5.00] out<- 97:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015289 [L/S/N= 5.00] out<- 98:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015290 [L/S/N= 5.00] out<- 99:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015291 [L/S/N= 5.00] out<- 100:R_DE 55477.00 14.892 No_date 33:40 39.14 n/a
015292
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01871 [IARCK 4.00] SMIN 31.15: SMAK=207.66: SK= .010]
01872 [Intersect 12.00]
01873 10010023 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
01874 ADD HYD ----- 01:RMC 5285.02 146.383 No\_date 33:40 39.17 n/a
01875 [DTS=5.00] SUM= 03:SNM\_CE 54095.02 147.622 No\_date 33:35 39.17 n/a
01876 ROUTE CHANNEL -> 03:SNM\_CE 54095.02 147.622 No\_date 33:35 39.17 n/a
01877 [RDT=5.00] out<- 01:RMC 54095.02 147.622 No\_date 33:35 39.17 n/a
01878 [L/S=N 825 / .010/.035]
01879 [Vmax 1.281Dmax .999]
01880 remark:Total Flows at Cedarview Road
01881 #
01882 # Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain
01883 # Channel X-Section obtained from RVCA Hydraulic Model - Station 5002
01884 #
01885 10010029 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
01886 ROUTE CHANNEL -> 03:SNM\_CE 54095.02 147.622 No\_date 33:35 39.17 n/a
01887 [RDT=5.00] out<- 01:RMC 54095.02 147.622 No\_date 33:35 39.17 n/a
01888 [L/S=N 825 / .010/.035]
01889 [Vmax 1.281Dmax .999]
01890 #
01891 # Catchment 85 CLAR
01892 # - To West Clarke Drain (south of the Joek)
01893 # - Subdivision with 438 imp. as per Barhaven South MSS
01894 #
01895 10010026 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
01896 CONTINUOUS STANBYD02:CLAR 243.00 27.368 No\_date 28:05 60.27 n/a
01897 [XIMP= 43:TIMP= 43]
01898 [LOSS= 2:CN= 75.0]
01899 [Impervious area: IArea= 4.67:SLP=1.00:LD= 40:MNW=250:SCP= .0]
01900 [Impervious area: IArea= 1.57:SLP=1.00:LD=1273:MNW=.013:SCP=.0]
01901 [IARCKimp= 4.00: IARCKPer= 4.00]
01902 [SMIN= 33.81: SMAK=225.41: SK= .010]
01903 #
01904 # West Clarke Pond 2
01905 # - Rating curve obtained from Barhaven South MSS modeling
01906 # - Tributary Drainage Area to MESS Pond 2 = 241 ha
01907 #
01908 10010027 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
01909 ROUTE RESERVOIR -> 02:ICM\_CLAR 243.00 27.368 No\_date 28:05 60.27 n/a
01910 [RDT=5.00] out<- 01:RMC 28.68 110 No\_date 28:05 60.27 n/a
01911 [RDT=5.00] out<- 01:RMC 28.68 110 No\_date 28:05 60.27 n/a
01912 [MdtotUsed=.3600E+00, TotOfVol=.1292E+02, N-Ovt= .2, TotOfDur=.16 hrs]
01913 #
01914 10010028 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
01915 ADD HYD ----- 01:RMC 28.68 110 No\_date 28:05 60.27 n/a
01916 [RDT=5.00] out<- 01:RMC 28.68 110 No\_date 28:05 60.27 n/a
01917 [DTS=5.00] SUM= 04:SNM\_CE 5438.02 147.477 No\_date 33:45 39.27 n/a
01918 [RDT=5.00] out<- 01:RMC 5438.02 147.477 No\_date 33:45 39.27 n/a
01919 [L/S=N 1020 / .050/.035]
01920 [Vmax 1.940Dmax 1.391]
01921 #
01922 # Hydrograph from Node West Clarke routed to Node at Kennedy - Burnett Drain
01923 # Channel X-Section obtained from RVCA Hydraulic Model - Station 4534
01924 #
01925 10010030 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
01926 ROUTE CHANNEL -> 04:SNM\_CE 5438.02 147.477 No\_date 33:45 39.27 n/a
01927 [RDT=5.00] out<- 01:RMC 5438.02 147.477 No\_date 33:45 39.27 n/a
01928 [L/S=N 1020 / .050/.035]
01929 [Vmax 1.940Dmax 1.391]
01930 #
01931 # Catchment 85N BU
01932 # - To Kennedy-Burnett SSM Facility
01933 # - Outlets to Fraser-Clarke drain (north of the Joek)
01934 # - Medium density residential development
01935 #
01936 10010031 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
01937 CONTINUOUS STANBYD02:KEN\_BU 281.00 35.633 No\_date 28:05 64.01 .723
01938 [XIMP= 55:TIMP= 55]
01939 [LOSS= 2:CN= 71.0]
01940 [Impervious area: IArea= 4.67:SLP=1.00:LD= 40:MNW=250:SCP= .0]
01941 [Impervious area: IArea= 1.57:SLP=1.00:LD=1369:MNW=.013:SCP=.0]
01942 [IARCKimp= 4.00: IARCKPer= 4.00]
01943 [SMIN= 31.38: SMAK=271.81: SK= .010]
01944 #
01945 # Existing Kennedy-Burnett SSM Facility
01946 # - Rating curve obtained from Barhaven South MSS
01947 # - Tributary Drainage Area to Pond = 160 ha
01948 #
01949 10010032 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
01950 ROUTE RESERVOIR -> 02:KEN\_BU 281.00 35.633 No\_date 28:05 64.01 n/a
01951 [RDT=5.00] out<- 01:RMC 132.84 1150 No\_date 27:45 64.01 n/a
01952 [RDT=5.00] out<- 01:RMC 132.84 1150 No\_date 27:45 64.01 n/a
01953 [MdtotUsed=.2380E+00, TotOfVol=.4402E+01, N-Ovt= .2, TotOfDur=.16 hrs]
01954 #
01955 # Catchment FRASER
01956 # - To Fraser-Clarke drain (north of the Joek)
01957 # - Developed land with assumed 438 imp.
01958 #
01959 10010033 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
01960 CONTINUOUS STANBYD02:FRASER 90.00 9.664 No\_date 28:05 59.76 .830
01961 [XIMP= 25:TIMP= 25]
01962 [LOSS= 2:CN= 80.0]
01963 [Impervious area: IArea= 4.67:SLP=1.00:LD= 40:MNW=250:SCP= .0]
01964 [Impervious area: IArea= 1.57:SLP=1.00:LD=1775:MNW=.013:SCP=.0]
01965 [IARCKimp= 4.00: IARCKPer= 4.00]
01966 [SMIN= 26.32: SMAK=175.50: SK= .010]
01967 #
01968 10010034 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
01969 ROUTE RESERVOIR -> 07:FRASER 90.00 9.664 No\_date 28:05 59.76 n/a
01970 [RDT=5.00] out<- 01:RMC 11.04 1104 No\_date 26:20 59.76 n/a
01971 [RDT=5.00] out<- 01:RMC 78.96 9.263 No\_date 28:05 59.76 n/a
01972 [MdtotUsed=.3599E+00, TotOfVol=.4402E+01, N-Ovt= .2, TotOfDur=.16 hrs]
01973 #
01974 10010035 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
01975 ADD HYD ----- 01:RMC 11.04 1104 No\_date 27:45 64.01 n/a
01976 [RDT=5.00] out<- 01:RMC 11.04 1104 No\_date 27:45 64.01 n/a
01977 [DTS=5.00] SUM= 04:SNM\_CE 54709.01 149.216 No\_date 33:55 39.42 n/a
01978 [RDT=5.00] out<- 01:RMC 54709.01 149.216 No\_date 33:55 39.42 n/a
01979 [L/S=N 650 / .030/.045]
01980 [Vmax .281Dmax .999]
01981 #
01982 # Hydrograph from Node Kennedy - Burnett Drain to Node Todd Drain
01983 # Channel X-Section obtained from RVCA Hydraulic Model - Station 3633
01984 #
01985 10010037 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
01986 ROUTE CHANNEL -> 04:SNM\_CE 54709.01 149.216 No\_date 33:55 39.42 n/a
01987 [RDT=5.00] out<- 01:RMC 54709.01 149.216 No\_date 33:55 39.42 n/a
01988 [L/S=N 650 / .030/.045]
01989 [Vmax .281Dmax .999]
01990 #
01991 # Catchment TODD
01992 # - To Todd Drain (south of the Joek)
01993 # - Subdivision with 438 imp. as per Barhaven South MSS
01994 #
01995 10010038 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
01996 CONTINUOUS STANBYD02:TODD 195.00 22.652 No\_date 28:05 61.25 .692
01997 [XIMP= 43:TIMP= 43]
01998 [LOSS= 2:CN= 77.0]
01999 [Impervious area: IArea= 4.67:SLP=1.00:LD= 40:MNW=250:SCP= .0]
02000 [Impervious area: IArea= 1.57:SLP=1.00:LD=1140:MNW=.013:SCP=.0]
02001 [IARCKimp= 4.00: IARCKPer= 4.00]
02002 [SMIN= 31.15: SMAK=207.66: SK= .010]
02003 #
02004 # Todd Pond 3
02005 # - Rating curve obtained from Barhaven South MSS modeling
02006 # - Tributary Drainage Area to MESS Pond 3 = 191 ha
02007 #
02008 10010039 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
02009 ROUTE RESERVOIR -> 03:TODD 195.00 22.652 No\_date 28:05 61.25 n/a
02010 [RDT=5.00] out<- 01:RMC 21.86 .080 No\_date 24:40 61.25 n/a
02011 [RDT=5.00] out<- 01:RMC 173.14 22.232 No\_date 28:05 61.25 n/a
02012 [MdtotUsed=.7796E+00, TotOfVol=.1060E+02, N-Ovt= .2, TotOfDur=.16 hrs]
02013 #
02014 10010040 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
02015 ADD HYD ----- 01:RMC 21.86 .080 No\_date 24:40 61.25 n/a
02016 [RDT=5.00] out<- 01:RMC 21.86 .080 No\_date 24:40 61.25 n/a
02017 [DTS=5.00] SUM= 10:SNM\_CE 54904.01 148.767 No\_date 35:05 39.50 n/a
02018 [RDT=5.00] out<- 01:RMC 54904.01 148.767 No\_date 35:05 39.50 n/a
02019 [L/S=N 280 / .033/.045]
02020 [Vmax .714Dmax .489]
02021 #
02022 # Hydrograph from Todd Drain to Corrigan Drain
02023 # Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
02024 #
02025 10010042 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
02026 ROUTE CHANNEL -> 10:SNM\_CE 54904.01 148.767 No\_date 35:05 39.50 n/a
02027 [RDT=5.00] out<- 01:RMC 54904.01 148.767 No\_date 35:05 39.50 n/a
02028 [L/S=N 280 / .033/.045]
02029 [Vmax .714Dmax .489]
02030 #
02031 # Catchment CORRIG
02032 # - To Corrigan Drain (south of the Joek)
02033 # - Primarily Developed (medium density)
02034 #
02035 10010043 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
02036 CONTINUOUS STANBYD02:CORRIG 149.00 19.025 No\_date 28:05 62.15 .702
02037 [XIMP= 45:TIMP= 45]
02038 [LOSS= 2:CN= 77.0]
02039 [Impervious area: IArea= 4.67:SLP=1.00:LD= 40:MNW=250:SCP= .0]
02040 [Impervious area: IArea= 1.57:SLP=1.00:LD=1997:MNW=.013:SCP=.0]
02041 [IARCKimp= 4.00: IARCKPer= 4.00]
02042 [SMIN= 31.15: SMAK=207.66: SK= .010]
02043 #
02044 # Corrigan Pond 1
02045 # - Rating curve obtained from Barhaven South MSS modeling
02046 # - Tributary Drainage Area to MESS Pond Area = 345 ha
02047 #
02048 10010044 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
02049 ROUTE RESERVOIR -> 02:CORRIG 149.00 19.025 No\_date 28:05 62.15 n/a
02050 [RDT=5.00] out<- 01:RMC 16.12 .060 No\_date 24:20 62.15 n/a
02051 [RDT=5.00] out<- 01:RMC 132.88 18.764 No\_date 28:05 62.15 n/a
02052 [MdtotUsed=.5800E+00, TotOfVol=.8289E+01, N-Ovt= .2, TotOfDur=.16 hrs]
02053 #
02054 10010045 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
02055 ADD HYD ----- 01:RMC 16.12 .060 No\_date 24:20 62.15 n/a
02056 [RDT=5.00] out<- 01:RMC 132.88 18.764 No\_date 28:05 62.15 n/a
02057 [L/S=N 280 / .033/.045]
02058 [Vmax .714Dmax .489]
02059 #
02060 # Hydrograph from Node Todd Drain to Corrigan Drain
02061 # Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
02062 #
02063 10010046 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
02064 ROUTE CHANNEL -> 03:SNM\_CE 5593.02 149.052 No\_date 35:25 39.56 n/a
02065 [RDT=5.00] out<- 01:RMC 5593.02 149.052 No\_date 35:25 39.56 n/a
02066 [L/S=N 562 / .485/.045]
02067 #
02068 # Catchment MILLS
02069 # - To SSM Facility north of the Joek
02070 # - Primarily residential development
02071 #
02072 10010047 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
02073 ROUTE CHANNEL -> 03:SNM\_CE 5593.02 149.052 No\_date 35:25 39.56 n/a
02074 [RDT=5.00] out<- 01:RMC 5593.02 149.052 No\_date 35:25 39.56 n/a
02075 [L/S=N 562 / .485/.045]
02076 [Vmax 2.191Dmax 2.152]
02077 #
02078 # Catchment MILLS
02079 # - To SSM Facility north of the Joek
02080 # - Primarily residential development
02081 #
02082 10010048 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
02083 CONTINUOUS STANBYD02:MILLS 139.00 15.807 No\_date 28:05 56.87 .642
02084 [XIMP= 38:TIMP= 38]
02085 [LOSS= 2:CN= 74.0]
02086 [Impervious area: IArea= 4.67:SLP=1.00:LD= 40:MNW=250:SCP= .0]
02087 [Impervious area: IArea= 1.57:SLP=1.00:LD=1273:MNW=.013:SCP=.0]
02088 [IARCKimp= 4.00: IARCKPer= 4.00]
02089 [SMIN= 16.67: SMAK=244.49: SK= .010]
02090 #
02091 # Chapman Mills SSM Pond
02092 # - Rating curve obtained from CCL Hydraulic modeling
02093 #
02094 10010049 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
02095 ROUTE RESERVOIR -> 02:MILLS 139.00 15.807 No\_date 28:05 56.87 n/a
02096 [RDT=5.00] out<- 01:RMC 159.02 4.050 No\_date 28:05 56.87 n/a
02097 [RDT=5.00] out<- 01:RMC 10.46 7.805 No\_date 28:15 56.87 n/a
02098 [MdtotUsed=.2108E+01, TotOfVol=.1948E+00, N-Ovt= .2, TotOfDur=.1 hrs]
02099 #
02100 10010050 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
02101 ADD HYD ----- 01:RMC 159.02 4.050 No\_date 28:15 56.87 n/a
02102 [RDT=5.00] out<- 01:RMC 159.02 4.050 No\_date 28:15 56.87 n/a
02103 [DTS=5.00] SUM= 03:SNM\_CE 55192.02 149.684 No\_date 35:20 39.61 n/a
02104 [RDT=5.00] out<- 01:RMC 55192.02 149.684 No\_date 35:20 39.61 n/a
02105 [L/S=N 1962 / .233/.045]
02106 [Vmax .940Dmax .152]
02107 #
02108 # Hydrograph from Joekville Road routed to Heart's Desire
02109 # Channel X-Section obtained from RVCA Hydraulic Model - Station 689
02110 #
02111 10010052 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
02112 ROUTE CHANNEL -> 03:SNM\_CE 55192.02 149.684 No\_date 35:20 39.61 n/a
02113 [RDT=5.00] out<- 01:RMC 55192.02 149.684 No\_date 35:20 39.61 n/a
02114 [L/S=N 1962 / .233/.045]
02115 [Vmax .940Dmax .152]
02116 #
02117 # Catchment DESIRE
02118 # - To Joekville SSM Facility
02119 # - Residential development & golf course
02120 #
02121 10010053 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
02122 CONTINUOUS STANBYD02:DESIRE 24.00 2.882 No\_date 28:00 53.12 .600
02123 [XIMP= 28:TIMP= 28]
02124 [LOSS= 2:CN= 77.0]
02125 [Impervious area: IArea= 4.67:SLP=1.00:LD= 40:MNW=250:SCP= .0]
02126 [Impervious area: IArea= 1.57:SLP=1.00:LD=1400:MNW=.013:SCP=.0]
02127 [IARCKimp= 4.00: IARCKPer= 4.00]
02128 [SMIN= 31.15: SMAK=207.66: SK= .010]
02129 #
02130 # Catchment JOEKVILLE
02131 # - To Joekville SSM Facility
02132 # - Residential development & golf course
02133 #
02134 10010054 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
02135 CONTINUOUS STANBYD02:JOEKV 252.00 30.693 No\_date 28:05 62.70 .708
02136 [XIMP= 40:TIMP= 40]
02137 [LOSS= 2:CN= 74.0]
02138 [Impervious area: IArea= 4.67:SLP=1.00:LD= 40:MNW=250:SCP= .0]
02139 [Impervious area: IArea= 1.57:SLP=1.00:LD=1296:MNW=.013:SCP=.0]
02140 [IARCKimp= 4.00: IARCKPer= 4.00]
02141 [SMIN= 36.67: SMAK=244.49: SK= .010]
02142 #
02143 # Joekville SSM Facility
02144 # - Rating curve obtained from Joekville Servicing Study (CCL 1998)
02145 #
02146 10010055 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
02147 ROUTE RESERVOIR -> 03:JOEKV 252.00 30.693 No\_date 28:05 62.70 n/a
02148 [RDT=5.00] out<- 01:RMC 252.00 11.951 No\_date 28:15 62.70 n/a
02149 [RDT=5.00] out<- 01:RMC 252.00 11.951 No\_date 28:15 62.70 n/a
02150 [MdtotUsed=.4202E+01, TotOfVol=.0000E+00, N-Ovt= .0, TotOfDur=.0 hrs]
02151 #
02152 10010056 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
02153 ADD HYD ----- 02:DESIRE 24.00 2.882 No\_date 28:00 53.12 n/a
02154 [RDT=5.00] out<- 01:RMC 24.00 .000 No\_date 0:00 .00 n/a
02155 [RDT=5.00] out<- 01:RMC 252.00 11.951 No\_date 28:15 62.70 n/a
02156 [DTS=5.00] SUM= 03:SNM\_CE 55468.01 150.033 No\_date 36:00 39.72 n/a
02157 [RDT=5.00] out<- 01:RMC 55468.01 150.033 No\_date 36:00 39.72 n/a
02158 [L/S=N 563 / .967/.045]
02159 [Vmax 2.703Dmax .046]
02160 #
02161 # Hydrograph from Heart's Desire routed to Risdau River
02162 # Channel X-Section obtained from RVCA Hydraulic Model - Station 0
02163 #
02164 10010058 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
02165 ROUTE CHANNEL -> 03:SNM\_CE 55468.01 150.033 No\_date 36:00 39.72 n/a
02166 [RDT=5.00] out<- 01:RMC 55468.01 150.033 No\_date 36:00 39.72 n/a
02167 [L/S=N 563 / .967/.045]
02168 [Vmax 2.703Dmax .046]
02169 #
02170 # Catchment P-2
02171 # - To Joek River (north and south)
02172 # - Undeveloped floodplain and river
02173 #
02174 10010059 -----ID:HNVD-----AREA-----OPEAK-TPeakDate\_hmm-----R-V-R-C-
02175 CONTINUOUS BASIN0 02:5-2 102.00 5.616 No\_date 28:15 40.95 .462
02176 [CN= 72.0: N= 3.00]
02177 [TP= 40:TP2= 8.00]
02178 [IARCK= 4.00: SMW= 39.75: SMAK=264.99: SK= .010]
02179 [InterEventTime= 12.00]
02180 #
02181 # ADD HYD ----- 01:RMC 55468.01 150.033 No\_date 36:05 39.72 n/a
02182 [RDT=5.00] out<- 01:RMC 102.00 5.616 No\_date 28:15 40.95 n/a
02183 [DTS=5.00] SUM= 03:SNM\_CE 55570.01 150.190 No\_date 36:05 39.72 n/a
02184 [RDT=5.00] out<- 01:RMC 55570.01 150.190 No\_date 36:05 39.72 n/a
02185 [L/S=N 563 / .967/.045]
02186 [Vmax 2.703Dmax .046]
02187 #
02188 # FINISH
02189 #
02190 #
02191 #
02192 #
02193 #
02194 #
02195 #
02196 #
02197 #
02198 #
02199 #
02200 #
02201 #
02194 \*\*\* WARNING: TRAVEL TIME TABLE was exceeded
02195 \*\*\* WARNING: TRAVEL TIME TABLE was exceeded
02196 \*\*\* WARNING: TRAVEL TIME TABLE was exceeded
02197 \*\*\* WARNING: TRAVEL TIME TABLE was exceeded
02198 Simulation ended on 2006-11-15 at 14:33:35
02199
02200
02201

# Attachment C

Model 3 – Jock River Reach One Update

JFSA, 2021

SWMHYMO Input & Summary files

```

1  20    Metric units / ID numbers OFF
2  *#*****
3  *# SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
4  *#*****
5  *# Project Name: [Jock River]    Project Number: [1474-16]
6  *# Date       : 04-03-2021
7  *# Modeller   : [M.M.]
8  *# Company    : JFSAinc.
9  *# License #  : 2549237
10 *#*****
11 *# CALIBRATION OF SUMMER MODEL PARAMETERS
12 *# USING CONTINUOUS SIMULATIONS
13 *# Rainfall data from JFSA raingauge installed at site + other gauges by the City
14 *# Use data collected from May 1st to July 14, 2003
15 *# 2020-11-30 change TMJSTO in COMPUTE DUALHYD (TMJSTO = 0.1 instead of 0.0001)
16 *# 2020-12-01 correct pond curve values
17 *# 2020-12-01 change W_CLAR_BRAZ XIMP to 0.55, SLPI=[0.5](%) (impervious slope), and
LGI up to 700m
18 *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 2462 (NHYDout=["N_TO"]
,NHYDin=["SN_TO"]) from 0.033 % (as per Stantec Report 2007) to 0.05 % so the model
will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELs
aren't well suited to really flat slopes.
19 *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHYDout=["N_WC"]
,NHYDin=["SN_CE"]) from 0.01 % (as per Stantec Report 2007) to 0.0255 % so the model
will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELs
aren't well suited to really flat slopes.
20 *
21 * Calibrated parameters for Summer 2003 data:  APII=50, APIK=0.85, CN=varies,
22 *                                               SK=0.01, InterEventTime=12,
23 *                                               GWResk=0.96, VHydCond=0.055
24 *
25 *# -----
26 *
27 *START          TZERO=[2003.0501], METOUT=[2], NSTORM=[1], NRUN=[001]
28 *              ["XAVG0315.STM"] average storm data a 15 minute time step
29 *              The above rainf file is an average of the JFSA gauge data
30 *              with the City of Ottawa rainfall data collected during
31 *              the same period.
32 *% 2 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
33 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[2]
34                ["C24SC002.stm"] <--storm filename, one per line for NSTORM time
35 *%-----|-----|
36 *%-----|-----|
37 READ STORM    STORM_FILENAME=["storm.001"]
38 *%-----|-----|
39 MODIFY STORM  ICASEms=[1], NSHIFT=[96],
40                RedFACT=[1],
41 *%-----|-----|
42 DEFAULT VALUES ICASEdef=[1], read and print values
43                DEFVAL_FILENAME=["CitiGate.DEF"]
44 *%-----|-----|
45 COMPUTE API   APII=[50], APIK=[.85]/day
46 *%-----|-----|
47 *%-----|-----|
48 *#
49 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
50 *# of 1.32
51 *%-----|-----|
52 CONTINUOUS NASHYD NHYD=["JR_HW"], DT=[1]min, AREA=[3680](ha),
53                DWF=[0](cms), CN/C=[64], IA=[2.5](mm),
54                N=[3.0], TP=[7.13]hrs,
55                Continuous simulation parameters:
56                IaRECper=[4](hrs),
57                SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
58                InterEventTime=[12](hrs)
59                Baseflow simulation parameters:

```

```

60         BaseFlowOption=[1] ,
61         InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
62         VHydCond=[0.055](mm/hr),   END=-1
63     *%-----|-----
64     *#
65     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
66     *# of 1.32
67     *%-----|-----
68     CONTINUOUS NASHYD  NHYD=["SW_13"], DT=[1]min, AREA=[971](ha),
69                        DWF=[0](cms),  CN/C=[61], IA=[2.5](mm),
70                        N=[3.0], TP=[3.76]hrs,
71                        Continuous simulation parameters:
72                        IaRECper=[4](hrs),
73                        SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
74                        InterEventTime=[12](hrs)
75                        Baseflow simulation parameters:
76                        BaseFlowOption=[1] ,
77                        InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
78                        VHydCond=[0.055](mm/hr),   END=-1
79     *%-----|-----
80     *#
81     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
82     *# of 1.80
83     *%-----|-----
84     CONTINUOUS NASHYD  NHYD=["JR_GWM"], DT=[1]min, AREA=[3074](ha),
85                        DWF=[0](cms),  CN/C=[55], IA=[2.5](mm),
86                        N=[3], TP=[11.33]hrs,
87                        Continuous simulation parameters:
88                        IaRECper=[4](hrs),
89                        SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
90                        InterEventTime=[12](hrs)
91                        Baseflow simulation parameters:
92                        BaseFlowOption=[1] ,
93                        InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
94                        VHydCond=[0.055](mm/hr),   END=-1
95     *%-----|-----
96     CONTINUOUS NASHYD  NHYD=["JR_ASH"], DT=[1]min, AREA=[1781](ha),
97                        DWF=[0](cms),  CN/C=[72], IA=[2.5](mm),
98                        N=[3.0], TP=[3.91]hrs,
99                        Continuous simulation parameters:
100                       IaRECper=[4](hrs),
101                       SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
102                       InterEventTime=[12](hrs)
103                       Baseflow simulation parameters:
104                       BaseFlowOption=[1] ,
105                       InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
106                       VHydCond=[0.055](mm/hr),   END=-1
107     *%-----|-----
108     CONTINUOUS NASHYD  NHYD=["SW_11"], DT=[1]min, AREA=[500](ha),
109                        DWF=[0](cms),  CN/C=[66], IA=[2.5](mm),
110                        N=[3.0], TP=[1.24]hrs,
111                        Continuous simulation parameters:
112                        IaRECper=[4](hrs),
113                        SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
114                        InterEventTime=[12](hrs)
115                        Baseflow simulation parameters:
116                        BaseFlowOption=[1] ,
117                        InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
118                        VHydCond=[0.055](mm/hr),   END=-1
119     *%-----|-----
120     *#
121     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
122     *# of 1.80
123     *%-----|-----
124     CONTINUOUS NASHYD  NHYD=["NN_CK"], DT=[1]min, AREA=[1917](ha),
125                        DWF=[0](cms),  CN/C=[66], IA=[2.5](mm),

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```

126 N=[3.0], TP=[5.29]hrs,
127 Continuous simulation parameters:
128 IaRECper=[4](hrs),
129 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
130 InterEventTime=[12](hrs)
131 Baseflow simulation parameters:
132 BaseFlowOption=[1] ,
133 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
134 VHydCond=[0.055](mm/hr), END=-1
135 *%-----|-----
136 *#
137 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
138 *# of 1.52
139 *%-----|-----
140 CONTINUOUS NASHYD NHYD=["SW_10"], DT=[1]min, AREA=[5666](ha),
141 DWF=[0](cms), CN/C=[72], IA=[2.5](mm),
142 N=[3.0], TP=[8.00]hrs,
143 Continuous simulation parameters:
144 IaRECper=[4](hrs),
145 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
146 InterEventTime=[12](hrs)
147 Baseflow simulation parameters:
148 BaseFlowOption=[1] ,
149 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
150 VHydCond=[0.055](mm/hr), END=-1
151 *%-----|-----
152 *#
153 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
154 *# of 1.75
155 *%-----|-----
156 CONTINUOUS NASHYD NHYD=["KG CK"], DT=[1]min, AREA=[8376](ha),
157 DWF=[0](cms), CN/C=[66], IA=[2.5](mm),
158 N=[3.0], TP=[11.66]hrs,
159 Continuous simulation parameters:
160 IaRECper=[4](hrs),
161 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
162 InterEventTime=[12](hrs)
163 Baseflow simulation parameters:
164 BaseFlowOption=[1] ,
165 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
166 VHydCond=[0.055](mm/hr), END=-1
167 *%-----|-----
168 *#
169 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
170 *# of 1.68
171 *%-----|-----
172 CONTINUOUS NASHYD NHYD=["SW_9"], DT=[1]min, AREA=[1132](ha),
173 DWF=[0](cms), CN/C=[70], IA=[2.5](mm),
174 N=[3.0], TP=[2.51]hrs,
175 Continuous simulation parameters:
176 IaRECper=[4](hrs),
177 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
178 InterEventTime=[12](hrs)
179 Baseflow simulation parameters:
180 BaseFlowOption=[1] ,
181 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
182 VHydCond=[0.055](mm/hr), END=-1
183 *%-----|-----
184 *#
185 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
186 *# of 1.82
187 *%-----|-----
188 CONTINUOUS NASHYD NHYD=["NC CK"], DT=[1]min, AREA=[4464](ha),
189 DWF=[0](cms), CN/C=[62], IA=[2.5](mm),
190 N=[3.0], TP=[11.32]hrs,
191 Continuous simulation parameters:

```



```

192         IaREcper=[4](hrs),
193         SMIN=[-1](mm),  SMAx=[-1](mm), SK=[0.010]/(mm),
194         InterEventTime=[12](hrs)
195         Baseflow simulation parameters:
196         BaseFlowOption=[1] ,
197         InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
198         VHydCond=[0.055](mm/hr),  END=-1
199     *%-----|-----
200     *#
201     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
202     *# of 1.80
203     *%-----|-----
204     CONTINUOUS NASHYD  NHYD=["SW_8"], DT=[1]min, AREA=[131](ha),
205                       DWF=[0](cms),  CN/C=[63], IA=[2.5](mm),
206                       N=[3.0], TP=[0.90]hrs,
207                       Continuous simulation parameters:
208                       IaREcper=[4](hrs),
209                       SMIN=[-1](mm),  SMAx=[-1](mm), SK=[0.010]/(mm),
210                       InterEventTime=[12](hrs)
211                       Baseflow simulation parameters:
212                       BaseFlowOption=[1] ,
213                       InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
214                       VHydCond=[0.055](mm/hr),  END=-1
215     *%-----|-----
216     *#
217     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
218     *# of 1.65
219     *%-----|-----
220     CONTINUOUS NASHYD  NHYD=["HB_DR"], DT=[1]min, AREA=[3854](ha),
221                       DWF=[0](cms),  CN/C=[66], IA=[2.5](mm),
222                       N=[3.0], TP=[8.42]hrs,
223                       Continuous simulation parameters:
224                       IaREcper=[4](hrs),
225                       SMIN=[-1](mm),  SMAx=[-1](mm), SK=[0.010]/(mm),
226                       InterEventTime=[12](hrs)
227                       Baseflow simulation parameters:
228                       BaseFlowOption=[1] ,
229                       InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
230                       VHydCond=[0.055](mm/hr),  END=-1
231     *%-----|-----
232     *#
233     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
234     *# of 1.82
235     *%-----|-----
236     CONTINUOUS NASHYD  NHYD=["SW_7"], DT=[1]min, AREA=[3197](ha),
237                       DWF=[0](cms),  CN/C=[57], IA=[2.5](mm),
238                       N=[3.0], TP=[6.65]hrs,
239                       Continuous simulation parameters:
240                       IaREcper=[4](hrs),
241                       SMIN=[-1](mm),  SMAx=[-1](mm), SK=[0.010]/(mm),
242                       InterEventTime=[12](hrs)
243                       Baseflow simulation parameters:
244                       BaseFlowOption=[1] ,
245                       InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
246                       VHydCond=[0.055](mm/hr),  END=-1
247     *%-----|-----
248     *#
249     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
250     *# of 1.75
251     *%-----|-----
252     CONTINUOUS NASHYD  NHYD=["SW_6"], DT=[1]min, AREA=[165](ha),
253                       DWF=[0](cms),  CN/C=[67], IA=[2.5](mm),
254                       N=[3.0], TP=[4.18]hrs,
255                       Continuous simulation parameters:
256                       IaREcper=[4](hrs),
257                       SMIN=[-1](mm),  SMAx=[-1](mm), SK=[0.010]/(mm),

```

```

258 InterEventTime=[12](hrs)
259 Baseflow simulation parameters:
260 BaseFlowOption=[1] ,
261 InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
262 VHydCond=[0.055](mm/hr) , END=-1
263 *%-----|-----
264 *#
265 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
266 *# of 1.67
267 *%-----|-----
268 CONTINUOUS NASHYD NHYD=["VG_DR"] , DT=[1]min , AREA=[1332](ha) ,
269 DWF=[0](cms) , CN/C=[72] , IA=[2.5](mm) ,
270 N=[3.0] , TP=[5.95]hrs ,
271 Continuous simulation parameters:
272 IaREcper=[4](hrs) ,
273 SMIN=[-1](mm) , SMAX=[-1](mm) , SK=[0.010]/(mm) ,
274 InterEventTime=[12](hrs)
275 Baseflow simulation parameters:
276 BaseFlowOption=[1] ,
277 InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
278 VHydCond=[0.055](mm/hr) , END=-1
279 *%-----|-----
280 CONTINUOUS NASHYD NHYD=["SW_5"] , DT=[1]min , AREA=[224](ha) ,
281 DWF=[0](cms) , CN/C=[77] , IA=[2.5](mm) ,
282 N=[3.0] , TP=[0.75]hrs ,
283 Continuous simulation parameters:
284 IaREcper=[4](hrs) ,
285 SMIN=[-1](mm) , SMAX=[-1](mm) , SK=[0.010]/(mm) ,
286 InterEventTime=[12](hrs)
287 Baseflow simulation parameters:
288 BaseFlowOption=[1] ,
289 InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
290 VHydCond=[0.055](mm/hr) , END=-1
291 *%-----|-----
292 *#
293 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
294 *# of 1.20
295 *%-----|-----
296 CONTINUOUS NASHYD NHYD=["FL_CK"] , DT=[1]min , AREA=[4945](ha) ,
297 DWF=[0](cms) , CN/C=[74] , IA=[2.5](mm) ,
298 N=[3.0] , TP=[4.45]hrs ,
299 Continuous simulation parameters:
300 IaREcper=[4](hrs) ,
301 SMIN=[-1](mm) , SMAX=[-1](mm) , SK=[0.010]/(mm) ,
302 InterEventTime=[12](hrs)
303 Baseflow simulation parameters:
304 BaseFlowOption=[1] ,
305 InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
306 VHydCond=[0.055](mm/hr) , END=-1
307 *%-----|-----
308 CONTINUOUS NASHYD NHYD=["SW_5A2"] , DT=[1]min , AREA=[20](ha) ,
309 DWF=[0](cms) , CN/C=[81] , IA=[2.5](mm) ,
310 N=[3.0] , TP=[0.62]hrs ,
311 Continuous simulation parameters:
312 IaREcper=[4](hrs) ,
313 SMIN=[-1](mm) , SMAX=[-1](mm) , SK=[0.010]/(mm) ,
314 InterEventTime=[12](hrs)
315 Baseflow simulation parameters:
316 BaseFlowOption=[1] ,
317 InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
318 VHydCond=[0.055](mm/hr) , END=-1
319 *%-----|-----
320 *#
321 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
322 *# of 1.61
323 *%-----|-----

```

```

324 CONTINUOUS NASHYD NHYD=["SW_5A1"], DT=[1]min, AREA=[1412](ha),
325 DWF=[0](cms), CN/C=[75], IA=[2.5](mm),
326 N=[3.0], TP=[8.00]hrs,
327 Continuous simulation parameters:
328 IaREcper=[4](hrs),
329 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
330 InterEventTime=[12](hrs)
331 Baseflow simulation parameters:
332 BaseFlowOption=[1] ,
333 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
334 VHydCond=[0.055](mm/hr), END=-1
335 *%-----|
336 CONTINUOUS NASHYD NHYD=["SW_4"], DT=[1]min, AREA=[585](ha),
337 DWF=[0](cms), CN/C=[81], IA=[2.5](mm),
338 N=[3.0], TP=[1.75]hrs,
339 Continuous simulation parameters:
340 IaREcper=[4](hrs),
341 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
342 InterEventTime=[12](hrs)
343 Baseflow simulation parameters:
344 BaseFlowOption=[1] ,
345 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
346 VHydCond=[0.055](mm/hr), END=-1
347 *%-----|
348 CONTINUOUS NASHYD NHYD=["LM_CK"], DT=[1]min, AREA=[1021](ha),
349 DWF=[0](cms), CN/C=[80], IA=[2.5](mm),
350 N=[3.0], TP=[2.46]hrs,
351 Continuous simulation parameters:
352 IaREcper=[4](hrs),
353 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
354 InterEventTime=[12](hrs)
355 Baseflow simulation parameters:
356 BaseFlowOption=[1] ,
357 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
358 VHydCond=[0.055](mm/hr), END=-1
359 *%-----|
360 CONTINUOUS NASHYD NHYD=["SW_2"], DT=[1]min, AREA=[177](ha),
361 DWF=[0](cms), CN/C=[77], IA=[2.5](mm),
362 N=[3.0], TP=[0.75]hrs,
363 Continuous simulation parameters:
364 IaREcper=[4](hrs),
365 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
366 InterEventTime=[12](hrs)
367 Baseflow simulation parameters:
368 BaseFlowOption=[1] ,
369 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
370 VHydCond=[0.055](mm/hr), END=-1
371 *%-----|
372 CONTINUOUS NASHYD NHYD=["SM_DR"], DT=[1]min, AREA=[1122](ha),
373 DWF=[0](cms), CN/C=[81], IA=[2.5](mm),
374 N=[3.0], TP=[3.25]hrs,
375 Continuous simulation parameters:
376 IaREcper=[4](hrs),
377 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
378 InterEventTime=[12](hrs)
379 Baseflow simulation parameters:
380 BaseFlowOption=[1] ,
381 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
382 VHydCond=[0.055](mm/hr), END=-1
383 *%-----|
384 CONTINUOUS NASHYD NHYD=["MO_DR"], DT=[1]min, AREA=[2737](ha),
385 DWF=[0](cms), CN/C=[76], IA=[2.5](mm),
386 N=[3.0], TP=[3.03]hrs,
387 Continuous simulation parameters:
388 IaREcper=[4](hrs),
389 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),

```

```

390 InterEventTime=[12](hrs)
391 Baseflow simulation parameters:
392 BaseFlowOption=[1] ,
393 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
394 VHydCond=[0.055](mm/hr), END=-1
395 *%-----|-----
396 * -JFSA 2020 replaced SW_1 with a detailed model from Stantec Report 2007
397 *CONTINUOUS NASHYD NHYD=["SW_1"], DT=[1]min, AREA=[3176](ha),
398 * DWF=[0](cms), CN/C=[78], IA=[2.5](mm),
399 * N=[3.0], TP=[3.56]hrs,
400 * Continuous simulation parameters:
401 * IaRECper=[4](hrs),
402 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
403 * InterEventTime=[12](hrs)
404 * Baseflow simulation parameters:
405 * BaseFlowOption=[1] ,
406 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
407 * VHydCond=[0.055](mm/hr), END=-1
408 *%-----|-----
409 *#
410 *# Routing hydrographs
411 *#
412 *# Starting with the addition of Jock River Headwater and Subwatershed 13
413 *#
414 ADD HYD NHYDsum=["S_N13"], NHYDs to add=["JR_HW"+"SW_13"]
415 *%-----|-----
416 *#
417 *# Sum of hydrographs from Node 13 routed to Node 13A
418 *# (Approximated cross-section - see cross-section 258)
419 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
420 *#
421 ROUTE CHANNEL NHYDout=["N13A"] ,NHYDin=["S_N13"],
422 RDT=[1](min),
423 CHLGTH=[9074](m), CHSLOPE=[0.0220](%),
424 FPSLOPE=[0.0220](%),
425 SECNUM=[1.0], NSEG=[1]
426 ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
427 ( DISTANCE (m), ELEVATION (m))=
428 [-40, 132.5]
429 [-30, 132]
430 [-25, 131.5]
431 [-13, 130]
432 [-8, 127.00]
433 [-7, 126.50]
434 [-6, 126]
435 [-5.5, 125.50]
436 [0, 123.75]
437 [4.5, 125.50]
438 [6, 126]
439 [7.5, 126.5]
440 [9, 127]
441 [10, 127.5]
442 [11.5, 128.0]
443 [15.5, 129.5]
444 *%-----|-----
445 *#
446 *# Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
447 *#
448 ADD HYD NHYDsum=["SN13A"], NHYDs to add=["N13A"+"JR_GWM"]
449 *%-----|-----
450 *#
451 *# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
452 *#
453 ROUTE RESERVOIR NHYDout=["RES_GM"] ,NHYDin=["SN13A"],
454 RDT=[1](min),
455 TABLE of ( OUTFLOW-STORAGE ) values

```

```

456 (cms) - (ha-m)
457 [ 0.0 , 0.0 ]
458 [1.991, 2.144 ]
459 [2.693, 39.826 ]
460 [3.509, 81.697 ]
461 [4.578, 318.774 ]
462 [5.647, 594.947 ]
463 [7.109, 910.219 ]
464 [8.616, 1264.589 ]
465 [10.371, 1658.057 ]
466 [12.402, 2090.622 ]
467 [22.056, 3462.487 ]
468 [ -1 , -1 ] (max twenty pts)
469

```

```
NHYDovf=[ " " ] ,
```

```

470 *%-----|-----
471 *#
472 SAVE HYD          NHYD=["RES_GM"], # OF PCYCLES=[-1], ICASEsh=[-1]
473                   HYD_FILENAME=["H_RESGM"]
474                   HYD_COMMENT=["Outflow from Res GM"]
475 *%-----|-----

```

```

476 *# Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
477 *# (Approximated cross-section - see cross-section 258)
478 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions

```

```

479 ROUTE CHANNEL    NHYDout=["N12"] ,NHYDin=["RES_GM"] ,
480                   RDT=[1](min),
481                   CHLGTH=[5926](m),  CHSLOPE=[0.0759](%),
482                                     FPSLOPE=[0.0759](%),
483                   SECNUM=[1.0],      NSEG=[1]
484                   ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
485                   ( DISTANCE (m), ELEVATION (m))=
486                       [-40, 132.5]
487                       [-30, 132]
488                       [-25, 131.5]
489                       [-13, 130]
490                       [-8, 127.00]
491                       [-7, 126.50]
492                       [-6, 126]
493                       [-5.5, 125.50]
494                       [0, 123.75]
495                       [4.5, 125.50]
496                       [6, 126]
497                       [7.5, 126.5]
498                       [9, 127]
499                       [10, 127.5]
500                       [11.5, 128.00]
501                       [15.5, 129.5]

```

```

502 *%-----|-----
503 *#
504 *# Addition of Subwatershed Jock River at Ashton to Node 12
505 *#

```

```

506 ADD HYD          NHYDsum=["S_N12"], NHYDs to add=["N12"+"JR_ASH"]
507 SAVE HYD        NHYD=["S_N12"], # OF PCYCLES=[-1], ICASEsh=[-1]
508                   HYD_FILENAME=["H_SN12"]
509                   HYD_COMMENT=["flow at S_N12 near Ashton"]

```

```

510 *%-----|-----
511 *#
512 *# Sum of hydrographs from Node 12 routed to Node 11
513 *# (Approximated cross-section - see cross-section 258)
514 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
515 *ROUTE CHANNEL    NHYDout=["N11"] ,NHYDin=["S_N12"] ,
516 *                 RDT=[1](min),
517 *                 CHLGTH=[972](m),  CHSLOPE=[0.0514](%),
518 *                                     FPSLOPE=[0.0514](%),
519 *                 SECNUM=[1.0],      NSEG=[1]
520 *                 ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
521 *                 ( DISTANCE (m), ELEVATION (m))=

```



```

522 * [-40, 132.5]
523 * [-30, 132]
524 * [-25, 131.5]
525 * [-13, 130]
526 * [-8, 127.00]
527 * [-7, 126.50]
528 * [-6, 126]
529 * [-5.5, 125.50]
530 * [0, 123.75]
531 * [4.5, 125.50]
532 * [6, 126]
533 * [7.5, 126.5]
534 * [9, 127]
535 * [10, 127.5]
536 * [11.5, 128.00]
537 * [15.5, 129.5]
538 *%-----|-----
539 *#
540 *# Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
541 *#
542 ROUTE CHANNEL NHYDout=["Dum11"] ,NHYDin=["S_N12"] ,
543 RDT=[1](min),
544 CHLGTH=[972](m), CHSLOPE=[0.054](%),
545 FPSLOPE=[0.054](%),
546 SECNUM=[1.0], NSEG=[1]
547 ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
548 ( DISTANCE (m), ELEVATION (m))=
549 [-40, 132.5]
550 [-30, 132]
551 [-25, 131.5]
552 [-13, 130]
553 [-8, 127.00]
554 [-7, 126.50]
555 [-6, 126]
556 [-5.5, 125.50]
557 [0, 123.75]
558 [4.5, 125.50]
559 [6, 126]
560 [7.5, 126.5]
561 [9, 127]
562 [10, 127.5]
563 [11.5, 128.00]
564 [15.5, 129.5]
565 *%-----|-----
566 *#
567 *# Addition of Subwatershed 11 and No Name Creek to Node 11
568 *#
569 ADD HYD NHYDsum=["S_N11"], NHYDs to add=["Dum11"+"SW_11"+"NN_CK"]
570 *%-----|-----
571 *#
572 *# Sum of hydrographs from Node 11 routed to Node 10
573 *# Section 1
574 *#
575 ROUTE CHANNEL NHYDout=["N10"] ,NHYDin=["S_N11"] ,
576 RDT=[1](min),
577 CHLGTH=[14028](m), CHSLOPE=[0.1568](%),
578 FPSLOPE=[0.1568](%),
579 SECNUM=[1.0], NSEG=[5]
580 ( SEGROUGH, SEGDIST (m))=
581 [0.04,-52.82
582 0.1,-6.47
583 -0.05,6.47
584 0.1,45.36
585 0.04,423.88] NSEG times
586 ( DISTANCE (m), ELEVATION (m))=
587 [-226.24 ,112.50]

```

```

588 [-167.50 ,111.50]
589 [-106.81 ,111.00]
590 [-92.37 ,110.00]
591 [-52.82 ,109.00]
592 [-24.90, 109.00]
593 [-17.02, 108.50]
594 [-6.47, 108.00]
595 [6.47, 108.00]
596 [15.67, 108.50]
597 [18.95, 109.00]
598 [45.36, 109.50]
599 [120.79, 110.00]
600 [145.72, 111.00]
601 [181.56, 111.50]
602 [423.88, 112.50]
603 *%-----|-----|
604 *#
605 *# Addition of Subwatershed 10 to Node 10
606 *#
607 ADD HYD NHYDsum=["S_N10"], NHYDs to add=["N10"+"SW_10"]
608 *%-----|-----|
609 SAVE HYD NHYD=["S_N10"], # OF PCYCLES=[-1], ICASEsh=[-1]
610 HYD_FILENAME=["H_SN10"]
611 HYD_COMMENT=["flow at S_N10: N10 + SW_10"]
612 *%-----|-----|
613 *# Addition of Kings Creek to S_N10
614 *#
615 ADD HYD NHYDsum=["S_N10A"], NHYDs to add=["S_N10"+"KG_CK"]
616 *%-----|-----|
617 *#
618 *# Sum of hydrographs from Node 10 routed to Node 9
619 *# Section 2
620 *#
621 ROUTE CHANNEL NHYDout=["N9"] ,NHYDin=["S_N10A"] ,
622 RDT=[1](min),
623 CHLGTH=[3982](m), CHSLOPE=[0.0753](%),
624 FPSLOPE=[0.0753](%),
625 SECNUM=[1.0], NSEG=[4]
626 ( SEGROUGH, SEGDIST (m))=
627 [0.04,-30.27
628 0.05,-18.42
629 -0.05,18.42
630 0.04,131.58] NSEG times
631 ( DISTANCE (m), ELEVATION (m))=
632 [-446.74, 106.00]
633 [-415.68, 105.50]
634 [-285.40, 105.00]
635 [-173.77, 104.50]
636 [-144.95, 104.00]
637 [-111.18, 103.50]
638 [-94.06, 103.00]
639 [-71.02, 102.50]
640 [-30.27, 102.00]
641 [-19.33, 100.00]
642 [-18.42, 99.50]
643 [18.42, 99.50]
644 [20.77, 100.00]
645 [27.93, 101.00]
646 [52.29, 101.00]
647 [68.80, 101.50]
648 [79.66, 103.00]
649 [91.50, 103.50]
650 [131.58, 104.00]
651 *%-----|-----|
652 *#
653 *# Addition of Subwatershed 9 and Nichols Creek to Node 9

```

```

654  *#
655  ADD HYD          NHYDsum=["S_N9"], NHYDs to add=["N9"+"SW_9"+"NC_CK"]
656  *%-----|-----
657  *#
658  *# Sum of hydrographs from Node 9 routed to Node 8
659  *# Section 3
660  *#
661  ROUTE CHANNEL    NHYDout=["N8"] ,NHYDin=["S_N9"] ,
662                  RDT=[1](min),
663                  CHLGTH=[2269](m),  CHSLOPE=[0.0882](%),
664                                          FPSLOPE=[0.0882](%),
665                  SECNUM=[1.0],      NSEG=[3]
666                  ( SEGROUGH, SEGDIST (m))=
667                    [0.1,-17.99
668                    -0.045,17.31
669                    0.1,456.58] NSEG times
670                  ( DISTANCE (m), ELEVATION (m))=
671                    [-201.19,100.50]
672                    [-135.21, 100.00]
673                    [-94.83, 99.50]
674                    [-67.05, 99.00]
675                    [-17.99, 98.50]
676                    [-16.02, 98.00]
677                    [-13.95, 97.50]
678                    [13.95, 97.50]
679                    [15.64, 98.00]
680                    [17.31, 98.50]
681                    [162.02, 98.50]
682                    [172.89 ,99.00]
683                    [314.38, 99.00]
684                    [343.78, 99.50]
685                    [365.67, 100.00]
686                    [376.68, 100.00 ]
687                    [393.11, 99.50]
688                    [404.97, 99.50]
689                    [431.70, 100.00]
690                    [456.58, 100.50 ]
691  *%-----|-----
692  *#
693  *# Addition of Subwatershed 8 and Hobb's Drain to Node 8
694  *#
695  ADD HYD          NHYDsum=["S_N8"], NHYDs to add=["N8"+"SW_8"+"HB_DR"]
696  *%-----|-----
697  *#
698  *# Sum of hydrographs from Node 8 routed to Node 7
699  *# Section 4
700  *#
701  ROUTE CHANNEL    NHYDout=["N7"] ,NHYDin=["S_N8"],
702                  RDT=[1](min),
703                  CHLGTH=[3750](m),  CHSLOPE=[0.0533](%),
704                                          FPSLOPE=[0.0533](%),
705                  SECNUM=[1.0],      NSEG=[3]
706                  ( SEGROUGH, SEGDIST (m))=
707                    [0.12,-18.11
708                    -0.07,17.22
709                    0.12,590.05] NSEG times
710                  ( DISTANCE (m), ELEVATION (m))=
711                    [-433.21, 102.00]
712                    [-425.34, 101.50]
713                    [-377.56, 101.50]
714                    [-366.23, 101.00]
715                    [-202.60, 100.50]
716                    [-96.25, 99.50]
717                    [-68.36 99.00]
718                    [-18.11, 98.50]
719                    [-13.81, 97.50]

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720             [13.81, 97.50]
721             [17.22, 98.50]
722             [161.95, 98.50]
723             [173.11, 99.00]
724             [314.05, 99.00]
725             [365.52, 100.00]
726             [404.70, 99.50]
727             [476.74, 100.50]
728             [502.31, 101.00]
729             [584.69, 101.00]
730             [585.79, 101.00]
731             [590.05, 102.00]
732 *%-----|-----
733 *#
734 *# Addition of Subwatershed 7 to Node 7
735 *#
736 ADD HYD           NHYDsum=["S_N7"], NHYDs to add=["N7"+"SW_7"]
737 *%-----|-----
738 SAVE HYD         NHYD=["S_N7"], # OF PCYCLES=[-1], ICASEsh=[-1]
739                   HYD_FILENAME=["H_SN7"]
740                   HYD_COMMENT=["flow at S_N7: N7 + SW_7"]
741 *%-----|-----
742 *# Insertion of a reservoir to simulate the effects of the Richmond Fen.
743 *# Storage area and volumes were estimated from available topo maps.
744 *# Release rate from fen was assumed to be controlled by the downstream
745 *# river cross-section for summer conditions. It is was assumed that for up to
746 *# 0.75 m of water, the main channel of the river provided the storage. Above
747 *# this depth, the wetland starts to signigicantly store water.
748 *#
749 ROUTE RESERVOIR  NHYDout=["RES_RF"] ,NHYDin=["S_N7"] ,
750                   RDT=[1](min),
751                   TABLE of ( OUTFLOW-STORAGE ) values
752                             (cms) - (ha-m)
753                   TABLE of ( OUTFLOW-STORAGE ) values
754                             (cms) - (ha-m)
755                             [ 0.0 , 0.0 ]
756                             [0.9051, 2.40]
757                             [2.907, 4.13]
758                             [9.744, 9.18]
759                             [20.304, 14.96]
760                             [34.167, 310.21]
761                             [74.993, 605.46]
762                             [104.876, 900.71]
763                             [140.56, 2892.00]
764                             [225.00, 3615.63]
765                             [ -1 , -1 ] (max twenty pts)
766                   NHYDovf=[" " ] ,
767 *%-----|-----
768 SAVE HYD         NHYD=["RES_RF"], # OF PCYCLES=[-1], ICASEsh=[-1]
769                   HYD_FILENAME=["H_ResRF"]
770                   HYD_COMMENT=["outflow of Richmond Fen"]
771 *%-----|-----
772 *#
773 *# Sum of hydrographs from Node 7 routed to Node 6
774 *# Section 5
775 *#
776 ROUTE CHANNEL   NHYDout=["N6"] ,NHYDin=["RES_RF"] ,
777                   RDT=[1](min),
778                   CHLGTH=[3056](m), CHSLOPE=[0.0818](%),
779                   FPSLOPE=[0.0818](%),
780                   SECNUM=[1.0], NSEG=[5]
781                   ( SEGROUGH, SEGDIST (m))=
782                   [0.025,-70.8
783                   0.1,-23.9
784                   -0.05,23.9
785                   0.06,39.8

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786             0.05,96.3] NSEG times
787             ( DISTANCE (m), ELEVATION (m))=
788                 [-100.8, 97.00]
789                 [-70.8, 96.50]
790                 [-52.0, 96.00]
791                 [-35.1, 95.50]
792                 [-30.6, 95.00]
793                 [-23.9, 94.54]
794                 [23.9, 94.54]
795                 [39.8, 95.00]
796                 [50.4, 95.50]
797                 [93.5, 96.00]
798                 [94.9, 96.50]
799                 [96.3, 97.00]
800 *%-----|-----
801 *#
802 *# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
803 *#
804 ADD HYD           NHYDsum=["S_N6"], NHYDs to add=["N6"+"SW_6"+"VG_DR"]
805 *%-----|-----
806 *#
807 *# Sum of hydrographs from Node 6 routed to Node 5
808 *# Section 6
809 *#
810 ROUTE CHANNEL   NHYDout=["N5"] ,NHYDin=["S_N6"] ,
811                   RDT=[1](min),
812                   CHLGTH=[1852](m),   CHSLOPE=[0.0540](%),
813                                           FPSLOPE=[0.0540](%),
814                   SECNUM=[1.0],       NSEG=[3]
815                   ( SEGROUGH, SEGDIST (m))=
816                       [0.035,-131.59
817                       -0.045,48.96
818                       0.1,239.04] NSEG times
819                   ( DISTANCE (m), ELEVATION (m))=
820                       [-686.30, 94.50]
821                       [-675.70, 94.00]
822                       [-492.52, 93.00]
823                       [-467.28, 94.00]
824                       [-131.59, 94.00]
825                       [-92.79, 92.50]
826                       [-18.06, 91.00]
827                       [18.06, 91.00]
828                       [43.47, 92.50]
829                       [48.96, 94.00]
830                       [177.43, 94.00]
831                       [239.04,94.50]
832 *%-----|-----
833 *#
834 *# Addition of Subwatershed 5 and Flowing Creek to Node 5
835 *#
836 ADD HYD           NHYDsum=["S_N5"], NHYDs to add=["N5"+"SW_5"+"FL_CK"]
837 *%-----|-----
838 *#
839 *# Sum of hydrographs from Node 5 routed to Node 5A
840 *# Section 7
841 *#
842 ROUTE CHANNEL   NHYDout=["N5A"] ,NHYDin=["S_N5"] ,
843                   RDT=[1](min),
844                   CHLGTH=[556](m),   CHSLOPE=[0.0900](%),
845                                           FPSLOPE=[0.0900](%),
846                   SECNUM=[1.0],       NSEG=[4]
847                   ( SEGROUGH, SEGDIST (m))=
848                       [0.04,-41.5
849                       0.1,-14.0
850                       -0.045,14.0
851                       0.1,41.1] NSEG times

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852          ( DISTANCE (m), ELEVATION (m))=
853              [-275.8, 93.00]
854              [-248.6, 92.50]
855              [-237.0, 92.00]
856              [-219.3, 91.50]
857              [-202.1, 91.50]
858              [-186.0, 92.00]
859              [-129.2, 92.00]
860              [-117.6, 91.50]
861              [-100.6, 91.00]
862              [-41.5, 91.00]
863              [-20.0, 91.00]
864              [-14.0, 90.54]
865              [14.0, 90.54]
866              [15.3, 91.00]
867              [17.3, 91.50]
868              [38.4, 92.00]
869              [39.8, 92.50]
870              [41.1, 93.00]
871  *%-----|-----
872  *#
873  *# Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
874  *#
875  ADD HYD          NHYDsum=["S_N5A"], NHYDs to add=["N5A"+"SW_5A2"+"SW_5A1"]
876  *%-----|-----
877  *#
878  *# Sum of hydrographs from Node 5A routed to Node 4
879  *# Section 8
880  *#
881  ROUTE CHANNEL    NHYDout=["N4"] ,NHYDin=["S_N5A"] ,
882                  RDT=[1](min),
883                  CHLGTH=[4630](m),  CHSLOPE=[0.0432](%),
884                                      FPSLOPE=[0.0432](%),
885                  SECNUM=[1.0],      NSEG=[3]
886                  ( SEGROUGH, SEGDIST (m))=
887                      [0.05,-28.2
888                      -0.035,28.2
889                      0.05,173.1] NSEG times
890                  ( DISTANCE (m), ELEVATION (m))=
891                      [-38.9, 92.00]
892                      [-35.8, 91.50]
893                      [-33.3, 91.00]
894                      [-28.2, 90.50]
895                      [-15.0, 87.48]
896                      [-5.0, 88.34]
897                      [5.0, 86.20]
898                      [15.0, 88.55]
899                      [28.2, 90.50]
900                      [29.7, 91.00]
901                      [46.5, 91.00]
902                      [127.8, 91.00]
903                      [148.7, 91.50]
904                      [173.1, 92.00]
905  *%-----|-----
906  *#
907  *# Addition of Subwatershed 4 and Leamy Creek to Node 4
908  *#
909  ADD HYD          NHYDsum=["S_N4"], NHYDs to add=["N4"+"SW_4"+"LM_CK"]
910  SAVE HYD         NHYD=["S_N4"], # OF PCYCLES=[-1], ICASEsh=[1]
911                  HYD_COMMENT=["flow at S_N4"]
912  *%-----|-----
913  *#
914  *# Sum of hydrographs from Node 4 routed to Node 2
915  *# Section 9
916  *#
917  ROUTE CHANNEL    NHYDout=["N2"] ,NHYDin=["S_N4"] ,

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918 RDT=[1](min),
919 CHLGTH=[1667](m), CHSLOPE=[0.0600](%),
920 FPSLOPE=[0.0600](%),
921 SECNUM=[1.0], NSEG=[4]
922 ( SEGROUGH, SEGDIST (m))=
923 [0.1,-28.0
924 -0.04,28.4
925 0.06,31.7
926 0.04,80.2] NSEG times
927 ( DISTANCE (m), ELEVATION (m))=
928 [-36.3, 92.00]
929 [-32.6, 91.50]
930 [-30.2, 91.00]
931 [-28.0, 90.45]
932 [-15.0, 87.48]
933 [-5.0, 88.34]
934 [5.0, 86.20]
935 [15.0, 88.55]
936 [28.0, 90.45]
937 [28.4, 90.50]
938 [30.4, 91.00]
939 [31.7, 91.50]
940 [80.2, 92.00]
941 *%-----|-----
942 *#
943 *# Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2
944 *#
945 ADD HYD NHYDsum=["S_N2"], NHYDs to add=["N2"+"SW_2"+"SM_DR"+"MO_DR"]
946 *%-----|-----
947 SAVE HYD NHYD=["S_N2"], # OF PCYCLES=[-1], ICASEsh=[-1]
948 HYD_FILENAME=["H_SN2"]
949 HYD_COMMENT=["flow at S_N2 Jock River Gauge at Moodie Dr."]
950 *%-----|-----
951 *#
952 *# Sum of hydrographs from Node 2 routed to Node 1
953 *# Section 10
954 *#
955 *#*****
956 *%READ HYD NHYD=["S_N2"],
957 *% HYD_FILENAME=["H-S_N2"]
958 *%-----|-----
959 *#
960 *# Hydrograph from Node 2 routed to Node 416
961 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 9025
962 *#
963 ROUTE CHANNEL NHYDout=["N_416"] ,NHYDin=["S_N2"] ,
964 RDT=[1](min),
965 CHLGTH=[2327](m), CHSLOPE=[0.0498](%),
966 FPSLOPE=[0.0498](%),
967 SECNUM=[1.0], NSEG=[3]
968 ( SEGROUGH, SEGDIST (m))=
969 [0.075,-23.96
970 -0.055,23.96
971 0.075,157.38] NSEG times
972 ( DISTANCE (m), ELEVATION (m))=
973 [-336.97,93.5]
974 [-318.85,93]
975 [-259,92.5]
976 [-133.18,92]
977 [-33.17,92]
978 [-27.21,92]
979 [-26.14,91.5]
980 [-24.99,91]
981 [-23.96,90.5]
982 [-14.33,88.26]
983 [-0.68,88.12]

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984 [14.33,88.26]
985 [23.96,90.5]
986 [32.12,91]
987 [43.74,91.5]
988 [57.09,92]
989 [73.53,92.5]
990 [108.27,93]
991 [125.88,93.5]
992 [144.81,94]
993 [157.38,94.5]
994 *%-----|-----|
995 *#*****|
996 *# Catchment SW-1a
997 *# - Portion of RVCA catchment SW_1 outside of Reach 1 subwatershed
998 *# - Undeveloped agricultural land
999 *#*****|
1000 CONTINUOUS NASHYD NHYD=["SW_1a"], DT=[1]min, AREA=[536.42](ha),
1001 DWF=[0](cms), CN/C=[72], IA=[4.67](mm),
1002 N=[3], TP=[2.79]hrs,
1003 Continuous simulation parameters:
1004 IaREcper=[4](hrs),
1005 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1006 InterEventTime=[12](hrs)
1007 Baseflow simulation parameters:
1008 BaseFlowOption=[1] ,
1009 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1010 VHydCond=[0.055](mm/hr), END=-1
1011 *%-----|-----|
1012 * -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
before station 7245 on Jock River
1013 *CONTINUOUS STANDHYD NHYD=["S-1-Okeefe"], DT=[1](min), AREA=[44.93](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
1014 * LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
IAper=[4.67](mm), SLPP=[2.0](%),
1015 * LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
1016 * LGI=[547.296](m), MNI=[0.013], SCI=[0](min),
1017 * Continuous simulation parameters:
1018 * IaREcper=[4](hrs), IaREcimp=[4](hrs),
1019 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1020 * InterEventTime=[12](hrs), END=-1
1021 *%-----|-----|
1022 CONTINUOUS NASHYD NHYD=["S-1-Okeefe"], DT=[1]min, AREA=[44.93](ha),
1023 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
1024 N=[3], TP=[1.049]hrs,
1025 Continuous simulation parameters:
1026 IaREcper=[4](hrs),
1027 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1028 InterEventTime=[12](hrs)
1029 Baseflow simulation parameters:
1030 BaseFlowOption=[1] ,
1031 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1032 VHydCond=[0.055](mm/hr), END=-1
1033 *%-----|-----|
1034 *COMPUTE DUALHYD NHYDin=["S-1-Okeefe"], CINLET=[4.796](cms), NINLET=[1],
1035 * MajNHYD=["S-1-OkMJ"]
1036 * MinNHYD=["S-1-OkMN"]
1037 * TMJSTO=[9999999](cu-m)
1038 *%-----|-----|
1039 *ADD HYD NHYDsum=["S-1-OkS"], NHYDs to add=["S-1-OkMJ"+"S-1-OkMN"]
1040 *%-----|-----|
1041 *ROUTE RESERVOIR NHYDout=["S-1-OkSR"],NHYDin=["S-1-OkS"] ,
1042 * RDT=[1](min),
1043 * TABLE of ( OUTFLOW-STORAGE ) values
1044 * (cms) - (ha-m)
1045 * [ 0.0 , 0.0 ]

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1046 * [ 0.5370, 1.7917 ]
1047 * [ -1 , -1 ] (max twenty pts)
1048 * NHYDovf=["S-1-OkSovf"]
1049 *%-----|-----|
1050 ADD HYD NHYDsum=["SN_416"], NHYDs to add=["N_416"+"SW_1a"+"S-1-Okeefe"]
1051 *%-----|-----|
1052 SAVE HYD NHYD=["SN_416"], # OF PCYCLES=[-1], ICASEsh=[1]
1053 HYD_COMMENT=["Total Flows at Highway 416"]
1054 *%-----|-----|
1055 *#
1056 *# Hydrograph from Node 416 routed to Node at Okeefe drain
1057 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 7245
1058 *#
1059 ROUTE CHANNEL NHYDout=["N_OK"] ,NHYDin=["SN_416"] ,
1060 RDT=[1](min),
1061 CHLGTH=[497](m), CHSLOPE=[0.3018](%),
1062 FPSLOPE=[0.3018](%),
1063 SECNUM=[1.0], NSEG=[3]
1064 ( SEGROUGH, SEGDIST (m))=
1065 [0.075,-19.40
1066 -0.055,19.40
1067 0.075,377.02] NSEG times
1068 ( DISTANCE (m), ELEVATION (m))=
1069 [-1061.41, 92.50]
1070 [-945.91, 92.00]
1071 [-783.64, 91.50]
1072 [-136.74, 91.00]
1073 [-86.04, 91.00]
1074 [-20.86, 91.00]
1075 [-20.18, 90.50]
1076 [-19.40, 90.00]
1077 [-11.68, 86.89]
1078 [0.00, 86.10]
1079 [12.09, 86.81]
1080 [19.40, 90.00]
1081 [34.68, 90.50]
1082 [60.56, 91.00]
1083 [170.14, 91.00]
1084 [175.05, 90.50]
1085 [180.29, 90.00]
1086 [193.41, 90.00]
1087 [195.98, 90.50]
1088 [377.02, 92.50]
1089 *%-----|-----|
1090 *#*****
1091 *# Catchment OKEEFE
1092 *# - To O'Keefe drain (north of the Jock)
1093 *# - Developed with assumed 43% imp.
1094 *# - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area
1095 513.02 HA)
1096 *# - 2020-11-20 Okeefe detailed model was added as per the NOVATECH SWMHYMO model
1097 (Citi-Gate 2014).
1098 *%-----|-----|
1099 *#*****
1100 CONTINUOUS NASHYD NHYD=["O-1"], DT=[1]min, AREA=[63.72](ha),
1101 DWF=[0](cms), CN/C=[61], IA=[6.2](mm), N=[3], TP=[.9]hrs,
1102 Continuous simulation parameters:
1103 IaRECper=[4](hrs),
1104 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1105 InterEventTime=[12](hrs)
1106 Baseflow simulation parameters:
1107 BaseFlowOption=[1] ,
1108 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1109 VHydCond=[0.055](mm/hr), END=-1

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1110 *%-----|-----
1111 *ROUTE FLOW THROUGH AREA 0-2
1112 ROUTE CHANNEL NHYDout=["O-1R"], NHYDin=["O-1"], RDT=[1](min),
1113 CHLGTH=[960](m), CHSLOPE=[0.63](%), FPSLOPE=[0.63](%),
1114 SECNUM=[1], NSEG=[3]
1115 ( SEGROUGH, SEGDIST (m))=[0.06,4 -.043,6 0.06,10] NSEG times
1116 ( DISTANCE (m), ELEVATION (m))=[0.00, 2.0]
1117 [0.0, 2.0]
1118 [4.0, 0.0]
1119 [6.0, 0.0]
1120 [10.0, 2.0]
1121 *%-----|-----
1122 CONTINUOUS NASHYD NHYD=["O-2"], DT=[1]min, AREA=[28.61](ha),
1123 DWF=[0](cms), CN/C=[57], IA=[5.2](mm), N=[3], TP=[1.1]hrs,
1124 Continuous simulation parameters:
1125 IaRECper=[4](hrs),
1126 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1127 InterEventTime=[12](hrs)
1128 Baseflow simulation parameters:
1129 BaseFlowOption=[1] ,
1130 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1131 VHydCond=[0.055](mm/hr), END=-1
1132 *%-----|-----
1133 CONTINUOUS NASHYD NHYD=["O-4"], DT=[1]min, AREA=[46.94](ha),
1134 DWF=[0](cms), CN/C=[49], IA=[9.2](mm), N=[3], TP=[0.9]hrs,
1135 Continuous simulation parameters:
1136 IaRECper=[4](hrs),
1137 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1138 InterEventTime=[12](hrs)
1139 Baseflow simulation parameters:
1140 BaseFlowOption=[1] ,
1141 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1142 VHydCond=[0.055](mm/hr), END=-1
1143 *%-----|-----
1144 *TOTAL EXTERNAL FLOW NORTH OF O'KEEFE CT. CROSSING
1145 ADD HYD NHYDsum=["OKF-N"], NHYDs to add=["O-1R"+"O-2"+"O-4"]
1146 *%-----|-----
1147 *ROUTE FLOW THROUGH AREA 0-6
1148 ROUTE CHANNEL ROUTE CHANNEL NHYDout=["OKF-NR"], NHYDin=["OKF-N"], RDT=[1](min),
1149 CHLGTH=[210](m), CHSLOPE=[.81](%), FPSLOPE=[.81](%),
1150 SECNUM=[1], NSEG=[3]
1151 ( SEGROUGH, SEGDIST (m))=[0.043,22.43 -0.043,25.07
1152 0.043,45.54] NSEG times
1153 ( DISTANCE (m), ELEVATION (m))=[0.00, 3.73]
1154 (14.62, 1.56)
1155 (18.41, 1.44)
1156 (22.43, 0.00)
1157 (25.07, 0.70)
1158 (29.10, 1.79)
1159 (33.73, 2.71)
1160 (45.54, 3.58)
1161 *%-----|-----
1162 CONTINUOUS NASHYD NHYD=["O-6"], DT=[1]min, AREA=[16.46](ha),
1163 DWF=[0](cms), CN/C=[43], IA=[9.2](mm), N=[3], TP=[0.7]hrs,
1164 Continuous simulation parameters:
1165 IaRECper=[4](hrs),
1166 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1167 InterEventTime=[12](hrs)
1168 Baseflow simulation parameters:
1169 BaseFlowOption=[1] ,
1170 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1171 VHydCond=[0.055](mm/hr), END=-1
1172 *%-----|-----
1173 CONTINUOUS STANDHYD NHYD=["O-3"], DT=[1](min), AREA=[39.67](ha), XIMP=[0.15],
TIMP=[0.30], DWF=[0](cms),

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1174      LOSS=[2], SCS curve number CN=[50], Pervious surfaces:
1175      IAper=[4.67](mm), SLPP=[0.32](%),
1176      LGP=[440](m), MNP=[0.035], SCP=[0](min), Impervious surfaces:
1177      IAimp=[1.57](mm), SLPI=[0.32](%),
1178      LGI=[1880](m), MNI=[0.013], SCI=[0](min),
1179      Continuous simulation parameters:
1180      IaRECPper=[4](hrs), IaRECImp=[4](hrs),
1181      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1182      InterEventTime=[12](hrs), END=-1
1183 *%-----|-----|
1184 CONTINUOUS STANDHYD NHYD=["O-5"], DT=[1](min), AREA=[60.63](ha), XIMP=[0.13],
1185 TIMP=[0.26], DWF=[0](cms),
1186      LOSS=[2], SCS curve number CN=[61],
1187      Pervious surfaces: IAper=[4.67](mm), SLPP=[1.38](%),
1188      LGP=[550](m), MNP=[0.035], SCP=[0](min), Impervious surfaces:
1189      IAimp=[1.57](mm), SLPI=[1.38](%),
1190      LGI=[1450](m), MNI=[0.013], SCI=[0](min),
1191      Continuous simulation parameters:
1192      IaRECPper=[4](hrs), IaRECImp=[4](hrs),
1193      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1194      InterEventTime=[12](hrs), END=-1
1195 *%-----|-----|
1196 *TOTAL EXTERNAL FLOWS WEST OF THE SITE AND NORTH OF O'KEEFE CRT
1197 *%-----|-----|
1198 ADD HYD NHYDsum=["PT1"], NHYDs to add=["OKF-NR"+"O-3"+"O-5"+"O-6"]
1199 *%-----|-----|
1200 CONTINUOUS NASHYD NHYD=["O-7"], DT=[1]min, AREA=[5.28](ha),
1201 DWF=[0](cms), CN/C=[54], IA=[7.5](mm), N=[3], TP=[0.6]hrs,
1202 Continuous simulation parameters:
1203 IaRECPper=[4](hrs),
1204 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1205 InterEventTime=[12](hrs)
1206 Baseflow simulation parameters:
1207 BaseFlowOption=[1] ,
1208 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1209 VHydCond=[0.055](mm/hr), END=-1
1210 *%-----|-----|
1211 *ANALYSIS POINT 1 - TOTAL FLOW NORTH OF FALLOWFIELD DR. AND O'KEEFE CRT.
1212 ADD HYD NHYDsum=["FF"], NHYDs to add=["PT1"+"O-7"]
1213 *%-----|-----|
1214 *ROUTE FLOW through O'Keefe Drain 1
1215 ROUTE CHANNEL NHYDout=["DRAIN1"], NHYDin=["FF"], RDT=[1](min),
1216 CHLGTH=[302]{m}, CHSLOPE=[1.00](%), FPSLOPE=[1.00](%),
1217 SECNUM=[1], NSEG=[3]
1218 ( SEGROUGH, SEGDIST (m))=[0.07,13.45 -0.043,16.55 0.07,30.00] NSEG
1219 times
1220 ( DISTANCE (m), ELEVATION (m))=[0.00, 1.70]
1221 (3.45, 0.60)
1222 (13.45, 0.50)
1223 (14.45, 0.00)
1224 (15.55, 0.00)
1225 (16.55, 0.50)
1226 (26.55, 0.60)
1227 (30.00, 1.70)
1228 *%-----|-----|
1229 CONTINUOUS NASHYD NHYD=["D1"], DT=[1]min, AREA=[1.17](ha),
1230 DWF=[0](cms), CN/C=[84], IA=[9.0](mm), N=[3], TP=[0.28]hrs,
1231 Continuous simulation parameters:
1232 IaRECPper=[4](hrs),
1233 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1234 InterEventTime=[12](hrs)
1235 Baseflow simulation parameters:
1236 BaseFlowOption=[1] ,
1237 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1238 VHydCond=[0.055](mm/hr), END=-1
1239 *%-----|-----|

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1235 CONTINUOUS STANDHYD NHYD=["A1"], DT=[1]min, AREA=[2.50](ha), XIMP=[0.68], TIMP=[0.85],
DWF=[0](cms), LOSS=[1]:
1236 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1237 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1238 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[223.607](m), MNI=[0.013], SCI=[0](min),
1239 Continuous simulation parameters:
1240 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1241 *%-----|-----|
1242 ROUTE RESERVOIR NHYDout=["A1-STR"], NHYDin=["A1"], RDT=[1](min),
1243 TABLE of ( OUTFLOW-STORAGE ) values
1244 (cms) - (ha-m)
1245 [ 0.000 , 0.000 ]
1246 [ 0.035 , 0.038 ]
1247 [ 0.072 , 0.051 ]
1248 [ 0.100 , 0.059 ]
1249 [ 0.125 , 0.070 ]
1250 [ 0.160 , 0.074 ]
1251 [ 0.185 , 0.081 ]
1252 [ -1 , -1 ] (max twenty pts)
1253 NHYDovf=["A1-OVF"]
1254 *%-----|-----|
1255 CONTINUOUS STANDHYD NHYD=["ST-2"], DT=[1]min, AREA=[0.59](ha), XIMP=[0.46],
TIMP=[0.57], DWF=[0](cms), LOSS=[1]:
1256 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1257 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1258 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[108.628](m), MNI=[0.013], SCI=[0](min),
1259 Continuous simulation parameters:
1260 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1261 *%-----|-----|
1262 ROUTE RESERVOIR NHYDout=["ST2STR"], NHYDin=["ST-2"], RDT=[1](min),
1263 TABLE of ( OUTFLOW-STORAGE ) values
1264 (cms) - (ha-m)
1265 [ 0.000 , 0.0000 ]
1266 [ 0.052 , 0.0010 ]
1267 [ 0.053 , 0.0080 ]
1268 [ -1 , -1 ] (max twenty pts)
1269 NHYDovf=["ST2OVF"]
1270 *%-----|-----|
1271 *%-----|-----|
1272 *TOTAL FLOW NORTH OF STRANDHERD DR. (EAST BRANCH) CROSSING
1273 *%-----|-----|
1274 CONTINUOUS NASHYD NHYD=["O-8"], DT=[1]min, AREA=[60.55](ha),
1275 DWF=[0](cms), CN/C=[69], IA=[4.0](mm), N=[3], TP=[1.0]hrs,
1276 Continuous simulation parameters:
1277 IaRECper=[4](hrs),
1278 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1279 InterEventTime=[12](hrs)
1280 Baseflow simulation parameters:
1281 BaseFlowOption=[1] ,
1282 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1283 VHydCond=[0.055](mm/hr), END=-1
1284 *%-----|-----|
1285 ROUTE PIPE PTYPE=[2]rect, NHYDout=["O8PIPE"], RNUMBER=[1], PWIDTH=[1800](mm),
PHEIGHT=[1200](mm), PLNGTH=[335.1](m),
1286 PROUGH=[0.013], PSLOPE=[0.001](m/m), NHYDin=["O-8"], RDT=[1](min)
1287 *%-----|-----|
1288 *%-----|-----|
1289 ADD HYD NHYDsum=["ST2-IN"], NHYDs to

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add=["DRAIN1"+"D1"+"A1-STR"+"A1-OVF"+"ST2STR"+"ST2OVF"+"O8PIPE"]
1290 *%-----|-----|
1291 CONTINUOUS STANDHYD NHYD=["A7"], DT=[1]min, AREA=[3.51](ha), XIMP=[0.68], TIMP=[0.85],
DWF=[0](cms), LOSS=[1]:
1292 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1293 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1294 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[264.953](m), MNI=[0.013], SCI=[0](min),
1295 Continuous simulation parameters:
1296 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1297 *%-----|-----|
1298 ROUTE RESERVOIR NHYDout=["A7-STR"], NHYDin=["A7"], RDT=[1](min),
1299 TABLE of ( OUTFLOW-STORAGE ) values
1300 (cms) - (ha-m)
1301 [ 0.000 , 0.000 ]
1302 [ 0.049 , 0.054 ]
1303 [ 0.102 , 0.072 ]
1304 [ 0.140 , 0.082 ]
1305 [ 0.175 , 0.099 ]
1306 [ 0.225 , 0.105 ]
1307 [ 0.260 , 0.114 ]
1308 [ -1 , -1 ] (max twenty pts)
1309 NHYDovf=["A7-OVF"]
1310 *%-----|-----|
1311 CONTINUOUS STANDHYD NHYD=["ST-3"], DT=[1]min, AREA=[0.71](ha), XIMP=[0.46],
TIMP=[0.57], DWF=[0](cms), LOSS=[1]:
1312 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1313 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1314 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[119.164](m), MNI=[0.013], SCI=[0](min),
1315 Continuous simulation parameters:
1316 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1317 *%-----|-----|
1318 ROUTE RESERVOIR NHYDout=["ST3STR"], NHYDin=["ST-3"], RDT=[1](min),
1319 TABLE of ( OUTFLOW-STORAGE ) values
1320 (cms) - (ha-m)
1321 [ 0.000 , 0.0000 ]
1322 [ 0.063 , 0.0010 ]
1323 [ 0.064 , 0.0094 ]
1324 [ -1 , -1 ] (max twenty pts)
1325 NHYDovf=["ST3OVF"]
1326 *%-----|-----|
1327 *ANALYSIS POINT 2 - TOTAL FLOW AT OUTLET OF STREET 2/3 INTERSECTION
1328 *%-----|-----|
1329 ADD HYD NHYDsum=["PT2ST3"], NHYDs to
add=["ST2-IN"+"A7-STR"+"A7-OVF"+"ST3STR"+"ST3OVF"]
1330 *%-----|-----|
1331 *ROUTE FLOW through O'Keefe Drain 2
1332 ROUTE CHANNEL NHYDout=["DRAIN2"], NHYDin=["PT2ST3"], RDT=[1](min),
1333 CHLGTH=[592](m), CHSLOPE=[.23](%), FPSLOPE=[.23](%),
1334 SECNUM=[1], NSEG=[3]
1335 ( SEGROUGH, SEGDIST (m))=[0.07,12.60 -0.043,17.40 0.07,30.00] NSEG
times
1336 ( DISTANCE (m), ELEVATION (m))=[0.00, 1.70]
1337 (2.60, 0.95)
1338 (12.60, 0.75)
1339 (14.10, 0.00)
1340 (15.90, 0.00)
1341 (17.40, 0.75)
1342 (27.40, 0.95)

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1343         (30.00, 1.70)
1344  *%-----|-----|
1345  CONTINUOUS NASHYD  NHYD=["D2"], DT=[1]min, AREA=[2.28](ha), DWF=[0](cms), CN/C=[84],
IA=[9.0](mm),
1346         N=[3], TP=[0.99]hrs,
1347         Continuous simulation parameters:
1348         IaRECper=[4](hrs),
1349         SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
1350         InterEventTime=[12](hrs)
1351         Baseflow simulation parameters:
1352         BaseFlowOption=[1] ,
1353         InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1354         VHydCond=[0.055](mm/hr),  END=-1
1355  *%-----|-----|
1356  CONTINUOUS STANDHYD NHYD=["A17"], DT=[1]min, AREA=[12.04](ha), XIMP=[0.68],
TIMP=[0.85], DWF=[0](cms), LOSS=[1]:
1357         Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1358         Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1359         Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[490.714](m), MNI=[0.013], SCI=[0](min),
1360         Continuous simulation parameters:
1361         IaRECper=[4](hrs),  IaRECImp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1362  *%-----|-----|
1363  ROUTE RESERVOIR  NHYDout=["A17STR"], NHYDin=["A17"], RDT=[1](min),
1364         TABLE of ( OUTFLOW-STORAGE ) values
1365         (cms) - (ha-m)
1366         [ 0.000 , 0.000 ]
1367         [ 0.169 , 0.185 ]
1368         [ 0.349 , 0.248 ]
1369         [ 0.482 , 0.283 ]
1370         [ 0.602 , 0.338 ]
1371         [ 0.771 , 0.359 ]
1372         [ 0.891 , 0.391 ]
1373         [ -1 , -1 ] (max twenty pts)
1374         NHYDovf=["A17OVF"]
1375  *%-----|-----|
1376  CONTINUOUS STANDHYD NHYD=["ST-4"], DT=[1]min, AREA=[0.35](ha), XIMP=[0.46],
TIMP=[0.57], DWF=[0](cms), LOSS=[1]:
1377         Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1378         Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1379         Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[83.666](m),
MNI=[0.013], SCI=[0](min),
1380         Continuous simulation parameters:
1381         IaRECper=[4](hrs),  IaRECImp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1382  *%-----|-----|
1383  ROUTE RESERVOIR  NHYDout=["ST4STR"], NHYDin=["ST-4"], RDT=[1](min),
1384         TABLE of ( OUTFLOW-STORAGE ) values
1385         (cms) - (ha-m)
1386         [ 0.000 , 0.0000 ]
1387         [ 0.031 , 0.0010 ]
1388         [ 0.032 , 0.0050 ]
1389         [ -1 , -1 ] (max twenty pts)
1390         NHYDovf=["ST4OVF"]
1391  *%-----|-----|
1392  CONTINUOUS STANDHYD NHYD=["A18"], DT=[1]min, AREA=[5.30](ha), XIMP=[0.68], TIMP=[0.85],
DWF=[0](cms), LOSS=[1]:
1393         Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1394         Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),

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1395      Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
1396      LGI=[325.576](m), MNI=[0.013], SCI=[0](min),
1397      Continuous simulation parameters:
1397      IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
1397      END=-1
1398  *%-----|-----|
1399  ROUTE RESERVOIR  NHYDout=["A18STR"], NHYDin=["A18"], RDT=[1](min),
1400                   TABLE of ( OUTFLOW-STORAGE ) values
1401                   (cms) - (ha-m)
1402                   [ 0.000 , 0.000 ]
1403                   [ 0.074 , 0.082 ]
1404                   [ 0.154 , 0.109 ]
1405                   [ 0.212 , 0.125 ]
1406                   [ 0.265 , 0.149 ]
1407                   [ 0.339 , 0.158 ]
1408                   [ 0.392 , 0.172 ]
1409                   [ -1 , -1 ] (max twenty pts)
1410                   NHYDovf=["A18OVF"]
1411  *%-----|-----|
1412  *ANALYSIS POINT 3 - TOTAL FLOW AT OUTLET OF STREET 4
1413  *%-----|-----|
1414  ADD HYD          NHYDsum=["PT3ST4"], NHYDs to
1414  add=["DRAIN2"+"D2"+"A17STR"+"A17OVF"+"ST4STR"+"ST4OVF"+"A18STR"+"A18OVF"]
1415  *%-----|-----|
1416  *ROUTE FLOW through O'Keefe Drain 3
1417  ROUTE CHANNEL   NHYDout=["DRAIN3"], NHYDin=["PT3ST4"], RDT=[1](min),
1418                   CHLGTH=[525]{m}, CHSLOPE=[.23](%), FPSLOPE=[.23](%),
1419                   SECNUM=[1], NSEG=[3]
1420                   ( SEGRROUGH, SEGDIST (m))=[0.07,12.50 -0.043,17.50 0.07,30.00] NSEG
1421                   times
1422                   ( DISTANCE (m), ELEVATION (m))=[0.00, 1.70]
1423                   (2.50, 1.00)
1424                   (12.50, 0.80)
1425                   (14.10, 0.00)
1426                   (15.90, 0.00)
1427                   (17.50, 0.80)
1428                   (27.50, 1.00)
1429                   (30.00, 1.70)
1429  *%-----|-----|
1430  CONTINUOUS NASHYD  NHYD=["D3"], DT=[1]min, AREA=[2.51](ha),
1431                   DWF=[0](cms), CN/C=[86], IA=[8.7](mm), N=[3], TP=[0.73]hrs,
1432                   Continuous simulation parameters:
1433                   IaREcper=[4](hrs),
1434                   SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1435                   InterEventTime=[12](hrs)
1436                   Baseflow simulation parameters:
1437                   BaseFlowOption=[1] ,
1438                   InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1439                   VHydCond=[0.055](mm/hr), END=-1
1440  *%-----|-----|
1441  CONTINUOUS STANDHYD  NHYD=["C1"], DT=[1]min, AREA=[3.41](ha), XIMP=[0.68], TIMP=[0.85],
1442  DWF=[0](cms), LOSS=[1]:
1443                   Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1444                   F=[0.00](mm),
1445                   Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1446                   MNP=[0.250], SCP=[0](min),
1447                   Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
1448                   LGI=[261.151](m), MNI=[0.013], SCI=[0](min),
1449                   Continuous simulation parameters:
1450                   IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
1451                   END=-1
1451  *%-----|-----|
1452  ROUTE RESERVOIR  NHYDout=["C1-STR"], NHYDin=["C1"], RDT=[1](min),
1453                   TABLE of ( OUTFLOW-STORAGE ) values
1454                   (cms) - (ha-m)
1455                   [ 0.000 , 0.000 ]

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1452         [ 0.048 , 0.052 ]
1453         [ 0.099 , 0.070 ]
1454         [ 0.136 , 0.080 ]
1455         [ 0.170 , 0.096 ]
1456         [ 0.218 , 0.102 ]
1457         [ 0.252 , 0.111 ]
1458         [ -1 , -1 ] (max twenty pts)
1459         NHYDovf=["C1-OVF"]
1460 *%-----|-----|
1461 CONTINUOUS STANDHYD NHYD=["ST-5"], DT=[1]min, AREA=[0.45](ha), XIMP=[0.46],
TIMP=[0.57], DWF=[0](cms), LOSS=[1]:
1462         Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1463         Pervious areas: IAPER=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1464         Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[94.868](m),
MNI=[0.013], SCI=[0](min),
1465         Continuous simulation parameters:
1466         IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1467 *%-----|-----|
1468 ROUTE RESERVOIR NHYDout=["ST5STR"], NHYDin=["ST-5"], RDT=[1](min),
1469         TABLE of ( OUTFLOW-STORAGE ) values
1470         (cms) - (ha-m)
1471         [ 0.000 , 0.0000 ]
1472         [ 0.040 , 0.0010 ]
1473         [ 0.041 , 0.0062 ]
1474         [ -1 , -1 ] (max twenty pts)
1475         NHYDovf=["ST5OVF"]
1476 *%-----|-----|
1477 ADD HYD NHYDsum=["ST5-E"], NHYDs to
add=["DRAIN3"+"D3"+"C1-STR"+"C1-OVF"+"ST5STR"+"ST5OVF"]
1478 *%-----|-----|
1479 CONTINUOUS STANDHYD NHYD=["STRAND"], DT=[1](min), AREA=[7.59](ha),
1480 XIMP=[0.64], TIMP=[0.85], DWF=[0](cms), LOSS=[1]:
1481         Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1482         Pervious areas: IAPER=[4.67](mm), SLPP=[0.5](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
1483         Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[1230](m),
MNI=[0.013], SCI=[0](min),
1484         Continuous simulation parameters:
1485         IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1486 *%-----|-----|
1487 ROUTE RESERVOIR NHYDout=["S-POND"], NHYDin=["STRAND"], RDT=[1](min),
1488         TABLE of ( OUTFLOW-STORAGE ) values
1489         (cms) - (ha-m)
1490         [ 0.000 , 0.000 ]
1491         [ 0.033 , 0.188 ]
1492         [ 0.057 , 0.253 ]
1493         [ 0.104 , 0.287 ]
1494         [ 0.160 , 0.336 ]
1495         [ 0.340 , 0.346 ]
1496         [ 0.471 , 0.360 ]
1497         [ 0.824 , 0.390 ]
1498         [ -1 , -1 ] (max twenty pts)
1499         NHYDovf=["S-OVF"]
1500 *%-----|-----|
1501 ADD HYD NHYDsum=["SSAOUT"], NHYDs to add=["ST5-E"+"S-POND"+"S-OVF"]
1502 *%-----|-----|
1503 SAVE HYD NHYD=["SSAOUT"], # OF PCYCLES=[5], ICASEsh=[1]
1504         HYD_COMMENT=["SSAOUT"]
1505 *%-----|-----|
1506 CONTINUOUS STANDHYD NHYD=["Area-A"], DT=[1]min, AREA=[66.75](ha), XIMP=[0.64],
TIMP=[0.80], DWF=[0](cms), LOSS=[1]:

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1507 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1508 F=[0.00](mm),
1509 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1510 MNP=[0.250], SCP=[0](min),
1511 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
1512 LGI=[1155.422](m), MNI=[0.013], SCI=[0](min),
1513 Continuous simulation parameters:
1514 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
1515 END=-1
1516 *%-----|-----|
1517 SAVE HYD NHYD=["Area-A"], # OF PCYCLES=[1], ICASEsh=[1]
1518 HYD_COMMENT=["SMWF-A Inflow"]
1519 *%-----|-----|
1520 ROUTE RESERVOIR NHYDout=["SWMF-A"], NHYDin=["Area-A"], RDT=[1](min),
1521 TABLE of ( OUTFLOW-STORAGE ) values
1522 (cms) - (ha-m)
1523 [ 0.000 , 0.000 ]
1524 [ 0.103 , 1.077 ]
1525 [ 0.128 , 1.749 ]
1526 [ 0.382 , 2.282 ]
1527 [ 0.703 , 2.582 ]
1528 [ 1.256 , 2.978 ]
1529 [ 1.567 , 3.202 ]
1530 [ 1.955 , 3.493 ]
1531 [ 2.100 , 3.600 ]
1532 [ -1 , -1 ] (max twenty pts)
1533 NHYDovf=["SWMAOV"]
1534 *%-----|-----|
1535 SAVE HYD NHYD=["SWMF-A"], # OF PCYCLES=[1], ICASEsh=[1]
1536 HYD_COMMENT=["SMWF-A Outflow"]
1537 *%-----|-----|
1538 *ANALYSIS POINT 4 - TOTAL FLOW AT OUTLET OF STREET 5
1539 *%-----|-----|
1540 ADD HYD NHYDsum=["PT4ST5"], NHYDs to add=["SSAOUT"+"SWMF-A"+"SWMAOV"]
1541 *%-----|-----|
1542 CONTINUOUS STANDHYD NHYD=["C6"], DT=[1]min, AREA=[1.87](ha), XIMP=[0.68], TIMP=[0.85],
1543 DWF=[0](cms), LOSS=[1]:
1544 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1545 F=[0.00](mm),
1546 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1547 MNP=[0.250], SCP=[0](min),
1548 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
1549 LGI=[193.391](m), MNI=[0.013], SCI=[0](min),
1550 Continuous simulation parameters:
1551 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
1552 END=-1
1553 *%-----|-----|
1554 ROUTE RESERVOIR NHYDout=["C6-STR"], NHYDin=["C6"], RDT=[1](min),
1555 TABLE of ( OUTFLOW-STORAGE ) values
1556 (cms) - (ha-m)
1557 [ 0.000 , 0.000 ]
1558 [ 0.026 , 0.029 ]
1559 [ 0.054 , 0.038 ]
1560 [ 0.075 , 0.044 ]
1561 [ 0.093 , 0.052 ]
1562 [ 0.120 , 0.056 ]
1563 [ 0.138 , 0.061 ]
1564 [ -1 , -1 ] (max twenty pts)
1565 NHYDovf=["C6-OVF"]
1566 *%-----|-----|
1567 CONTINUOUS STANDHYD NHYD=["C7"], DT=[1]min, AREA=[1.62](ha), XIMP=[0.68], TIMP=[0.85],
1568 DWF=[0](cms), LOSS=[1]:
1569 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1570 F=[0.00](mm),
1571 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1572 MNP=[0.250], SCP=[0](min),

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1561      Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
1562      LGI=[180.000](m), MNI=[0.013], SCI=[0](min),
1563      Continuous simulation parameters:
1564      IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
1565      END=-1
1566
1567 *%-----|-----|
1568 ROUTE RESERVOIR NHYDout=["C7-STR"], NHYDin=["C7"], RDT=[1](min),
1569      TABLE of ( OUTFLOW-STORAGE ) values
1570      (cms) - (ha-m)
1571      [ 0.000 , 0.000 ]
1572      [ 0.023 , 0.025 ]
1573      [ 0.047 , 0.033 ]
1574      [ 0.065 , 0.038 ]
1575      [ 0.081 , 0.045 ]
1576      [ 0.104 , 0.048 ]
1577      [ 0.120 , 0.053 ]
1578      [ -1 , -1 ] (max twenty pts)
1579      NHYDovf=["C7-OVF"]
1580
1581 *%-----|-----|
1582 CONTINUOUS STANDHYD NHYD=["ST-6"], DT=[1]min, AREA=[0.41](ha), XIMP=[0.46], TIMP=[0.57],
1583 DWF=[0](cms), LOSS=[1]:
1584      Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1585      F=[0.00](mm),
1586      Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1587      MNP=[0.250], SCP=[0](min),
1588      Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[90.554](m),
1589      MNI=[0.013], SCI=[0](min),
1590      Continuous simulation parameters:
1591      IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
1592      END=-1
1593
1594 *%-----|-----|
1595 ROUTE RESERVOIR NHYDout=["ST6STR"], NHYDin=["ST-6"], RDT=[1](min),
1596      TABLE of ( OUTFLOW-STORAGE ) values
1597      (cms) - (ha-m)
1598      [ 0.000 , 0.0000 ]
1599      [ 0.036 , 0.0010 ]
1600      [ 0.037 , 0.0058 ]
1601      [ -1 , -1 ] (max twenty pts)
1602      NHYDovf=["ST6OVF"]
1603
1604 *%-----|-----|
1605 *ANALYSIS POINT 5 - TOTAL FLOW AT OUTLET OF STREET 6
1606 *%-----|-----|
1607 ADD HYD NHYDsum=["PT5ST6"], NHYDs to
1608 add=["PT4ST5"+"C6-STR"+"C6-OVF"+"C7-STR"+"C7-OVF"+"ST6STR"+"ST6OVF"]
1609 *%-----|-----|
1610 *ROUTE FLOW through O'Keefe Drain 4
1611 ROUTE CHANNEL NHYDout=["DRAIN4"], NHYDin=["PT5ST6"], RDT=[1](min),
1612      CHLGTH=[324]{m}, CHSLOPE=[.10](%), FPSLOPE=[.10](%),
1613      SECNUM=[1], NSEG=[3]
1614      ( SEGROUGH, SEGDIST (m))=[0.07,12.00 -0.043,18.00 0.07,30.00] NSEG
1615      times
1616      ( DISTANCE (m), ELEVATION (m))=[0.00, 2.00]
1617      (2.00, 1.20)
1618      (12.00, 1.00)
1619      (14.00, 0.00)
1620      (16.00, 0.00)
1621      (18.00, 1.00)
1622      (28.00, 1.20)
1623      (30.00, 2.00)
1624
1625 *%-----|-----|
1626 CONTINUOUS NASHYD NHYD=["D4"], DT=[1]min, AREA=[1.73](ha), DWF=[0](cms), CN/C=[88],
1627 IA=[8.4](mm),
1628 N=[3], TP=[0.60]hrs,
1629      Continuous simulation parameters:
1630      IaREcper=[4](hrs),
1631      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),

```

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1617 InterEventTime=[12](hrs)
1618 Baseflow simulation parameters:
1619 BaseFlowOption=[1] ,
1620 InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
1621 VHydCond=[0.055](mm/hr) , END=-1
1622 *%-----|-----|
1623 CONTINUOUS STANDHYD NHYD=["Area-B"] , DT=[1]min , AREA=[24.04](ha) , XIMP=[0.62] ,
TIMP=[0.77] , DWF=[0](cms) , LOSS=[1]:
1624 Horton: Fo=[76.20](mm/hr) , Fc=[13.20](mm/hr) , DCAY=[4.14](/hr) ,
F=[0.00](mm) ,
1625 Pervious areas: IAper=[4.67](mm) , SLPP=[1.4](%) , LGP=[50](m) ,
MNP=[0.250] , SCP=[0](min) ,
1626 Impervious areas: IAimp=[1.57](mm) , SLPI=[1.4](%) ,
LGI=[693.397](m) , MNI=[0.013] , SCI=[0](min) ,
1627 Continuous simulation parameters:
1628 IaREcper=[4](hrs) , IaREcimp=[4](hrs) , InterEventTime=[12](hrs) ,
END=-1
1629 *%-----|-----|
1630 ROUTE RESERVOIR NHYDout=["SWMF-B"] , NHYDin=["Area-B"] , RDT=[1](min) ,
1631 TABLE of ( OUTFLOW-STORAGE ) values
1632 (cms) - (ha-m)
1633 [ 0.000 , 0.000 ]
1634 [ 0.025 , 0.090 ]
1635 [ 0.175 , 0.510 ]
1636 [ 0.350 , 0.710 ]
1637 [ 0.495 , 0.820 ]
1638 [ 0.648 , 0.980 ]
1639 [ 0.965 , 1.045 ]
1640 [ 1.072 , 1.140 ]
1641 [ -1 , -1 ] (max twenty pts)
1642 NHYDovf=["SWMBOVF"]
1643 *%-----|-----|
1644 ADD HYD NHYDsum=["D4-EX"] , NHYDs to add=["DRAIN4"+"D4"+"SWMF-B"+"SWMBOVF"]
1645 *%-----|-----|
1646 *ROUTE FLOW THROUGH O'Keefe Drain 5
1647 * JFSA: Nov. 2020, added en points to close X-Section
1648 ROUTE CHANNEL NHYDout=["DRAIN5"] , NHYDin=["D4-EX"] , RDT=[1](min) ,
1649 CHLGTH=[413.0](m) , CHSLOPE=[0.16](%) , FPSLOPE=[0.16](%) ,
1650 SECNUM=[1] , NSEG=[3]
1651 ( SEGROUGH , SEGDIST (m))=[0.043,12.29 -0.033,17.97
1652 0.043,32.84] NSEG times
1653 ( DISTANCE (m) , ELEVATION (m))=(-0.01 , 2.50)
1654 [0.00 , 1.41]
1655 [6.13 , 0.97]
1656 [12.29 , 0.89]
1657 [15.71 , 0.00]
1658 [17.97 , 0.39]
1659 [23.04 , 0.35]
1660 [32.83 , 0.96]
1661 [32.84 , 2.50]
1662 *%-----|-----|
1663 CONTINUOUS NASHYD NHYD=["D5"] , DT=[1]min , AREA=[1.90](ha) ,
1664 DWF=[0](cms) , CN/C=[86] , IA=[8.7](mm) , N=[3] , TP=[0.69]hrs ,
1665 Continuous simulation parameters:
1666 IaREcper=[4](hrs) ,
1667 SMIN=[-1](mm) , SMAX=[-1](mm) , SK=[0.010]/(mm) ,
1668 InterEventTime=[12](hrs)
1669 Baseflow simulation parameters:
1670 BaseFlowOption=[1] ,
1671 InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
1672 VHydCond=[0.055](mm/hr) , END=-1
1673 *%-----|-----|
1674 *EXTERNAL FLOWS SOUTHEAST OF THE SITE NORTH OF MCKENNA CASEY DR.
1675 CONTINUOUS NASHYD NHYD=["O-13SDF"] , DT=[1]min , AREA=[9.74](ha) ,
1676 DWF=[0](cms) , CN/C=[81] , IA=[4.0](mm) , N=[3] , TP=[.43]hrs ,
1677 Continuous simulation parameters:

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1678 IaREcper=[4](hrs),
1679 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1680 InterEventTime=[12](hrs)
1681 Baseflow simulation parameters:
1682 BaseFlowOption=[1] ,
1683 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1684 VHydCond=[0.055](mm/hr), END=-1
1685 *%-----|-----
1686 *SNOW DISPOSAL FACILITY
1687 *PARAMETERS BASED ON ROBINSON 2006 MODEL
1688 ROUTE RESERVOIR NHYDout=["SDF"], NHYDin=["O-13SDF"], RDT=[1](min),
1689 TABLE of ( OUTFLOW-STORAGE ) values
1690 (cms) - (ha-m)
1691 [0.000,0.000]
1692 [0.150,0.600]
1693 (0.200,1.500)
1694 [ -1 , -1 ] (max twenty pts)
1695 NHYDovf=["OVFSDF"]
1696 *%-----|-----
1697 *ANALYSIS POINT 6 - McKenna Casey Dr.
1698 *%-----|-----
1699 ADD HYD NHYDsum=["PT6MC"], NHYDs to add=["DRAIN5"+"D5"+"SDF"]
1700 *%-----|-----
1701 CONTINUOUS NASHYD NHYD=["O-15"], DT=[1]min, AREA=[10.67](ha),
1702 DWF=[0](cms), CN/C=[82], IA=[7.5](mm), N=[3], TP=[0.30]hrs,
1703 Continuous simulation parameters:
1704 IaREcper=[4](hrs),
1705 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1706 InterEventTime=[12](hrs)
1707 Baseflow simulation parameters:
1708 BaseFlowOption=[1] ,
1709 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1710 VHydCond=[0.055](mm/hr), END=-1
1711 *%-----|-----
1712 *TOTAL FLOW NORTH OF McKENNA CASEY DR.
1713 ADD HYD NHYDsum=["M-C"], NHYDs to add=["PT6MC"+"O-15"]
1714 *%-----|-----
1715 *ROUTE FLOW THROUGH AREA O-14
1716 * JFSA: Nov. 2020, added end points to close X-section
1717 ROUTE CHANNEL NHYDout=["O-14Ch"], NHYDin=["M-C"], RDT=[1](min),
1718 CHLGTH=[845.3](m), CHSLOPE=[0.10](%), FPSLOPE=[0.10](%),
1719 SECNUM=[1], NSEG=[3]
1720 ( SEGROUGH, SEGDIST (m))=[0.06,15.00 -0.033,18.04 0.06,31.85] NSEG
times
1721 ( DISTANCE (m), ELEVATION (m))=[-0.01, 2.5
1722 (0.00, 1.53]
1723 (5.56, 1.47)
1724 (9.21, 1.45)
1725 (12.45, 1.53)
1726 (13.70, 1.50)
1727 (15.00, 0.69)
1728 (15.34, 0.00)
1729 (16.51, 0.05)
1730 (17.30, 0.17)
1731 (18.04, 0.74)
1732 (19.29, 1.32)
1733 (22.73, 1.47)
1734 (31.84, 1.41)
1735 (31.85, 2.50)
1736 *%-----|-----
1737 *% -Change O-14 from NASHYD to STANDHYD, name it "S-1-Okeefe" and add it to S-1
subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
1738 *% -JFSA 2021-02-16, add detailed subcatchment drainage area for each subcatchment
in Corrigan sub-catchment. After adding part of O-14 to S_1 sub-catchment so O-14
becomes 5 ha instead of 30.02 ha and TP becomes 0.133 (5*0.8/30.02) instead of 0.8
1739 CONTINUOUS NASHYD NHYD=["O-14"], DT=[1]min, AREA=[5](ha),

```



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1740 DWF=[0](cms), CN/C=[82], IA=[7.5](mm), N=[3], TP=[0.133]hrs,
1741 Continuous simulation parameters:
1742 IaRECPper=[4](hrs),
1743 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1744 InterEventTime=[12](hrs)
1745 Baseflow simulation parameters:
1746 BaseFlowOption=[1] ,
1747 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1748 VHydCond=[0.055](mm/hr), END=-1
1749 *
1750 *%-----|-----|
1751 *ANALYSIS POINT 7 - JOCK RIVER
1752 * 2020-12-01 To Foster Drain
1753 * 2020-12-01 replace ("PT7JR") by ("OKEEFE")
1754 *%-----|-----|
1755 ADD HYD NHYDsum=["OKEEFE"], NHYDs to add=["O-14Ch"+"O-14"]
1756 *%-----|-----|
1757 *CONTINUOUS STANDHYD NHYD=["OKEEFE"], DT=[1](min), AREA=[448](ha),
1758 * XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
1759 * SCS curve number CN=[77],
1760 * Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
1761 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
1762 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
1763 * LGI=[1728](m), MNI=[0.013], SCI=[0](min),
1764 * Continuous simulation parameters:
1765 * IaRECPper=[4](hrs), IaRECImp=[4](hrs),
1766 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1767 * InterEventTime=[18](hrs), END=-1
1768 *#*****
1769 *# Okeefe Pond
1770 *# - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1771 *# and a ratio of the catchment area to the West Clarke pond rating curve
1772 *# from the MSS for the next coordinates
1773 *#*****
1774 *ROUTE RESERVOIR NHYDout=["P_OKE"], NHYDin=["OKEEFE"],
1775 * RDT=[1](min),
1776 * TABLE of ( OUTFLOW-STORAGE ) values
1777 * (cms) - (ha-m)
1778 * [ 0.0 , 0.0]
1779 * [ 14.13 , 13.0]
1780 * [ -1 , -1 ] (maximum one hundred pairs of points)
1781 * NHYDovf=["ok-OVF"],
1782 *%-----|-----|
-----|
1783 * -JFSA 2021-02-25 "S-1-D2" and "S-1-D3" are part of S-1 sub-catchment. They are
moved to drain before station 6215 on Jock River
1784 *CONTINUOUS STANDHYD NHYD=["S-1-D2"], DT=[1](min), AREA=[18.67](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
1785 * LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
IAper=[4.67](mm), SLPP=[2.0](%),
1786 * LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
1787 * LGI=[352.798](m), MNI=[0.013], SCI=[0](min),
1788 *
1789 * IaRECPper=[4](hrs), IaRECImp=[4](hrs),
1790 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1791 * InterEventTime=[12](hrs), END=-1
1792 *%-----|-----|
1793 CONTINUOUS NASHYD NHYD=["S-1-D2"], DT=[1]min, AREA=[18.67](ha),
1794 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
1795 N=[3], TP=[1.120]hrs,
1796 Continuous simulation parameters:
1797 IaRECPper=[4](hrs),
1798 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1799 InterEventTime=[12](hrs)
1800 Baseflow simulation parameters:

```

```

1801 BaseFlowOption=[1] ,
1802 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1803 VHydCond=[0.055](mm/hr), END=-1
1804 *%-----|-----|
1805 *COMPUTE DUALHYD NHYDin=["S-1-D2"], CINLET=[2.062](cms), NINLET=[1],
1806 * MajNHYD=["S-1-D2J"]
1807 * MinNHYD=["S-1-D2N"]
1808 * TMJSTO=[9999999](cu-m)
1809 *%-----|-----|
1810 *ADD HYD NHYDsum=["S-1-D2S"], NHYDs to add=["S-1-D2J"+"S-1-D2N"]
1811 *%-----|-----|
1812 *ROUTE RESERVOIR NHYDout=["S-1-D2R"],NHYDin=["S-1-D2S"] ,
1813 * RDT=[1](min),
1814 * TABLE of ( OUTFLOW-STORAGE ) values
1815 * (cms) - (ha-m)
1816 * [ 0.0 , 0.0 ]
1817 * [ 0.2231, 0.7445 ]
1818 * [ -1 , -1 ] (max twenty pts)
1819 * NHYDovf=["S-1-D2Rovf"]
1820 *%-----|-----|
1821 *CONTINUOUS STANDHYD NHYD=["S-1-D3"], DT=[1](min), AREA=[6.79](ha), XIMP=[0.65],
1822 * TIMP=[0.65], DWF=[0](cms),
1823 * LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
1824 * IAper=[4.67](mm), SLPP=[2.0](%),
1825 * LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
1826 * IAimp=[1.57](mm), SLPI=[0.75](%),
1827 * LGI=[212.760](m), MNI=[0.013], SCI=[0](min),
1828 * Continuous simulation parameters:
1829 * IaREcper=[4](hrs), IaREcimp=[4](hrs),
1830 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1831 * InterEventTime=[12](hrs), END=-1
1832 *%-----|-----|
1833 CONTINUOUS NASHYD NHYD=["S-1-D3"], DT=[1]min, AREA=[6.79](ha),
1834 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
1835 * N=[3], TP=[1.281]hrs,
1836 * Continuous simulation parameters:
1837 * IaREcper=[4](hrs),
1838 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1839 * InterEventTime=[12](hrs)
1840 * Baseflow simulation parameters:
1841 * BaseFlowOption=[1] ,
1842 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1843 * VHydCond=[0.055](mm/hr), END=-1
1844 *%-----|-----|
1845 *COMPUTE DUALHYD NHYDin=["S-1-D3"], CINLET=[0.719](cms), NINLET=[1],
1846 * MajNHYD=["S-1-D3J"]
1847 * MinNHYD=["S-1-D3N"]
1848 * TMJSTO=[9999999](cu-m)
1849 *%-----|-----|
1850 *ADD HYD NHYDsum=["S-1-D3S"], NHYDs to add=["S-1-D3J"+"S-1-D3N"]
1851 *%-----|-----|
1852 *ROUTE RESERVOIR NHYDout=["S-1-D3R"],NHYDin=["S-1-D3S"] ,
1853 * RDT=[1](min),
1854 * TABLE of ( OUTFLOW-STORAGE ) values
1855 * (cms) - (ha-m)
1856 * [ 0.0 , 0.0 ]
1857 * [ 0.0811, 0.2708 ]
1858 * [ -1 , -1 ] (max twenty pts)
1859 * NHYDovf=["S-1-D3Rovf"]
1860 *%-----|-----|
1861 ADD HYD NHYDsum=["SN_OK"], NHYDs to add=["N_OK"+"OKEEFE"+"S-1-D2"+"S-1-D3"]
1862 *%-----|-----|
1863 SAVE HYD NHYD=["SN_OK"], # OF PCYCLES=[-1], ICASEsh=[1]
1864 * HYD_COMMENT=["Total Flows at Okeefe Drain"]
1865 *%-----|-----|
1866 *#

```

```

1864  *# Hydrograph from Node Okeefe routed to Node at Foster Drain
1865  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
1866  *#
1867  ROUTE CHANNEL      NHYDout=["N_FO"] ,NHYDin=["SN_OK"] ,
1868                    RDT=[1](min),
1869                    CHLGTH=[1183](m),  CHSLOPE=[0.0761](%),
1870                    FPSLOPE=[0.0761](%),
1871                    SECNUM=[1.0],      NSEG=[3]
1872                    ( SEGRROUGH, SEGDIST (m))=
1873                      [0.050,-33.89
1874                      -0.035,31.59
1875                      0.050,34.41] NSEG times
1876                    ( DISTANCE (m), ELEVATION (m))=
1877                      [-794.18, 91.00]
1878                      [-775.41, 91.50]
1879                      [-702.63, 91.50]
1880                      [-546.19, 91.50]
1881                      [-529.54, 91.50]
1882                      [-323.44, 91.00]
1883                      [-320.71, 91.00]
1884                      [-183.59, 91.00]
1885                      [-182.54, 90.50]
1886                      [-181.36, 90.00]
1887                      [-177.37, 90.00]
1888                      [-87.70, 90.00]
1889                      [-33.89, 90.00]
1890                      [-18.52, 86.88]
1891                      [0.00,85.20]
1892                      [16.20, 86.83]
1893                      [31.59, 90.00]
1894                      [33.03, 90.50]
1895                      [34.41, 91.00]
1896  *%-----|-----|
1897  *#*****
1898  *#   Catchment FOSTER
1899  *#   - To Foster ditch (north of the Jock)
1900  *#   - Partially developed (medium density); remaining agricultural
1901  *#   - 2020-12-01 JFSA Foster area is 332 as per Foster SWMF Environmental Study
1902  *#   - 2020-12-01 decrease Foster drainage area from (373 HA) to (307.98 HA) after
1903  *#   - 2021-02-12 update Foster area to 325.44 ha as measured from QGIS
1904  *#*****
1905  CONTINUOUS STANDHYD NHYD=["FOSTER"], DT=[1]min, AREA=[325.44](ha),
1906                    XIMP=[0.55], TIMP=[0.55], DWF=[0](cms), LOSS=[2],
1907                    SCS curve number CN=[74],
1908                    Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
1909                    LGP=[40](m), MNP=[0.25], SCP=[0](min),
1910                    Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
1911                    LGI=[1472.956](m), MNI=[0.013], SCI=[0](min),
1912                    Continuous simulation parameters:
1913                    IaRECper=[4](hrs), IaRECimp=[4](hrs),
1914                    SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1915                    InterEventTime=[18](hrs), END=-1
1916  *#*****
1917  *#   Foster Pond
1918  *#   - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1919  *#   and a ratio of the catchment area to the West Clarke pond rating curve
1920  *#   from the MSS for the next coordinates
1921  *#*****
1922  ROUTE RESERVOIR    NHYDout=["P_FOS"],  NHYDin=["FOSTER"],
1923                    RDT=[1](min),
1924                    TABLE of ( OUTFLOW-STORAGE ) values
1925                    (cms) - (ha-m)
1926                    [ 0.0 , 0.0 ]

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1927         [ 10.34 , 10]
1928         [ -1 , -1 ] (max twenty pts)
1929         NHYDovf=["FO-OVF"]
1930 *%-----|-----|
1931 ADD HYD          NHYDsum=["FOSTER-OUT"], NHYDs to add=["P_FOS"+"FO-OVF"]
1932 *%-----|-----|
1933 *#*****
1934 *   -Brazeau area from P 1800-19 =[71.751], change to 63.59 ha based on GIS measurements
1935 *   -JFSA, 2021-01-19 update "W_CLAR_BRAZ" to 73.29 ha based on GIS measurements
1936 *   -JFSA, 2021-01-22 Brazeau ("MS_P10"+"P10-OVF")brazeau pond discharges directly
to the jock river through a road side ditch on the west side of Borrisokane road
(station 6016)
1937 CONTINUOUS STANDHYD NHYD=["W_CLAR_BRAZ"], DT=[1]min, AREA=[73.29](ha),
1938 XIMP=[0.6], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
1939 SCS curve number CN=[77],
1940 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
1941 LGP=[40](m), MNP=[0.25], SCP=[0](min),
1942 Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
1943 LGI=[699.00](m), MNI=[0.013], SCI=[0](min),
1944 Continuous simulation parameters:
1945 IaRECper=[4](hrs), IaRECimp=[4](hrs),
1946 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1947 InterEventTime=[18](hrs), END=-1
1948 *%-----|-----|
1949 * 2020-12-01 correct pond curve values
1950 ROUTE RESERVOIR   NHYDout=["MS_P10"], NHYDin=["W_CLAR_BRAZ"],
1951 RDT=[1](min),
1952         TABLE of ( OUTFLOW-STORAGE ) values
1953         (cms) - (ha-m)
1954         [ 0.0 , 0.0 ]
1955         [ 0.068 , 0.001 ]
1956         [ 0.271 , 0.022 ]
1957         [ 0.379 , 0.051 ]
1958         [ 0.48 , 0.091 ]
1959         [ 0.853 , 0.341 ]
1960         [ 1.005 , 0.61 ]
1961         [ 1.128 , 1.231 ]
1962         [ 1.155 , 1.592 ]
1963         [ 1.194 , 1.876 ]
1964         [ 1.2 , 1.921 ]
1965         [ 1.259 , 2.369 ]
1966         [ 1.3 , 2.665 ]
1967         [ 1.349 , 2.813 ]
1968         [ -1 , -1 ] (max twenty pts)
1969         NHYDovf=["P10-OVF"]
1970 *%-----|-----|
1971 *   -JFSA 2021-02-26 "S-1-FO-D2" is a part of S-1 sub-catchment. It is moved to drain
before station 980 on Foster Drain
1972 *CONTINUOUS STANDHYD NHYD=["S-1-FO-D2"], DT=[1]min, AREA=[4.94](ha),
1973 * XIMP=[0.55], TIMP=[0.55], DWF=[0](cms), LOSS=[2],
1974 * SCS curve number CN=[74],
1975 * Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
1976 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
1977 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
1978 * LGI=[181.475](m), MNI=[0.013], SCI=[0](min),
1979 * Continuous simulation parameters:
1980 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
1981 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1982 * InterEventTime=[18](hrs), END=-1
1983 *%-----|-----|
1984 CONTINUOUS NASHYD  NHYD=["S-1-FO-D2"], DT=[1]min, AREA=[4.94](ha),
1985 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
1986 N=[3], TP=[1.10]hrs,
1987 Continuous simulation parameters:
1988 IaRECper=[4](hrs),
1989 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),

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1990 InterEventTime=[12](hrs)
1991 Baseflow simulation parameters:
1992 BaseFlowOption=[1] ,
1993 InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
1994 VHydCond=[0.055](mm/hr) , END=-1
1995 *%-----|-----|
1996 *COMPUTE DUALHYD NHYDin=["S-1-FO-D2"] , CINLET=[0.508](cms) , NINLET=[1] ,
1997 * MajNHYD=["S-1-FO-D2J"]
1998 * MinNHYD=["S-1-FO-D2N"]
1999 * TMJSTO=[9999999](cu-m)
2000 *%-----|-----|
2001 *ADD HYD NHYDsum=["S-1-FO-D2S"] , NHYDs to add=["S-1-FO-D2J"+"S-1-FO-D2N"]
2002 *%-----|-----|
2003 *ROUTE RESERVOIR NHYDout=["S-1-FO-D2R"] ,NHYDin=["S-1-FO-D2S"] ,
2004 * RDT=[1](min) ,
2005 * TABLE of ( OUTFLOW-STORAGE ) values
2007 * [ 0.0 , 0.0 ]
2008 * [ 0.0590, 0.1970 ]
2009 * [ -1 , -1 ] (max twenty pts)
2010 * NHYDovf=["S-1FOD2ovf"]
2011 *%-----|-----|
2012 ADD HYD NHYDsum=["980"] ,NHYDs to add=["FOSTER-OUT"+"S-1-FO-D2"]
2013 *%-----|-----|
2014 SAVE HYD NHYD=["980"] , # OF PCYCLES=[-1] , ICASEsh=[1]
2015 HYD_COMMENT=["Total Flows at Station 980 on Foster Drain"]
2016 *%-----|-----|
2017 *#
2018 *# Hydrograph from Node Foster SWM (Station 980)to Node at station 520
2019 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 980
2020 *#
2021 ROUTE CHANNEL NHYDout=["980-out"] ,NHYDin=["980"] ,
2022 RDT=[1](min) ,
2023 CHLGTH=[460](m) , CHSLOPE=[0.04348](%) ,
2024 FPSLOPE=[0.04348](%) ,
2025 SECNUM=[1.0] , NSEG=[3]
2026 ( SEGROUGH, SEGDIST (m))=
2027 [0.050,45.90
2028 -0.035,53.30
2029 0.050,100] NSEG times
2030 ( DISTANCE (m), ELEVATION (m))=
2031 [0, 91.75 ]
2032 [42.4, 92.18 ]
2033 [43.5, 92.16 ]
2034 [44.1, 92.1 ]
2035 [44.6, 92 ]
2036 [44.8, 91.86 ]
2037 [45.9, 91.04 ]
2038 [46.4, 90.65 ]
2039 [46.8, 90.36 ]
2040 [47.9, 90.32 ]
2041 [48.7, 90.35 ]
2042 [50.7, 90.33 ]
2043 [52.2, 90.38 ]
2044 [52.5, 90.59 ]
2045 [53.3, 91.28 ]
2046 [54, 91.83 ]
2047 [54.3, 92 ]
2048 [54.8, 92.08 ]
2049 [55.4, 92.12 ]
2050 [100, 91.84 ]
2051 *%-----|-----|
2052 * -JFSA 2021-02-26 "S-1-FO-D1" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2053 *CONTINUOUS STANDHYD NHYD=["S-1-FO-D1"] , DT=[1]min , AREA=[5.11](ha) ,
2054 * XIMP=[0.65] , TIMP=[0.65] , DWF=[0](cms) , LOSS=[2] ,

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2055 *           SCS curve number CN=[74],
2056 *           Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2057 *           LGP=[40](m), MNP=[0.25], SCP=[0](min),
2058 *           Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2059 *           LGI=[184.572](m), MNI=[0.013], SCI=[0](min),
2060 *           Continuous simulation parameters:
2061 *           IaREcper=[4](hrs), IaREcimp=[4](hrs),
2062 *           SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2063 *           InterEventTime=[18](hrs), END=-1
2064 *%-----|-----|
2065 CONTINUOUS NASHYD NHYD=["S-1-FO-D1"], DT=[1]min, AREA=[5.11](ha),
2066 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2067 N=[3], TP=[1.10]hrs,
2068 Continuous simulation parameters:
2069 IaREcper=[4](hrs),
2070 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2071 InterEventTime=[12](hrs)
2072 Baseflow simulation parameters:
2073 BaseFlowOption=[1],
2074 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2075 VHydCond=[0.055](mm/hr), END=-1
2076 *%-----|-----|
2077 *COMPUTE DUALHYD NHYDin=["S-1-FO-D1"], CINLET=[0.605](cms), NINLET=[1],
2078 *           MajNHYD=["S-1-FO-D1J"]
2079 *           MinNHYD=["S-1-FO-D1N"]
2080 *           TMJSTO=[9999999](cu-m)
2081 *%-----|-----|
2082 *ADD HYD NHYDsum=["S-1-FO-D1S"], NHYDs to add=["S-1-FO-D1N"+"S-1-FO-D1J"]
2083 *%-----|-----|
2084 *ROUTE RESERVOIR NHYDout=["S-1-FO-D1R"],NHYDin=["S-1-FO-D1S"],
2085 *           RDT=[1](min),
2086 *           TABLE of ( OUTFLOW-STORAGE ) values
2087 *           (cms) - (ha-m)
2088 *           [ 0.0      , 0.0 ]
2089 *           [ 0.0611, 0.2038 ]
2090 *           [ -1     , -1     ] (max twenty pts)
2091 *           NHYDovf=["S-1FOD1ovf"]
2092 *%-----|-----|
2093 ADD HYD NHYDsum=["520"], NHYDs to add=["980-out"+"S-1-FO-D1"]
2094 *%-----|-----|
2095 SAVE HYD NHYD=["520"], # OF PCYCLES=[-1], ICASEsh=[1]
2096 HYD_COMMENT=["Total Flows at Sation 520 on Foster Drain"]
2097 *%-----|-----|
2098 *# Hydrograph from Node at Station 520 (Foster Drain) to Node at station 6016 (Jock
River)
2099 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 520
2100 *#
2101 ROUTE CHANNEL NHYDout=["520-out"],NHYDin=["520"],
2102 RDT=[1](min),
2103 CHLGTH=[860](m), CHSLOPE=[0.5872](%),
2104 FPSLOPE=[0.5872](%),
2105 SECNUM=[1.0], NSEG=[3]
2106 ( SEGROUGH, SEGDIST (m))=
2107 [0.050,45.90
2108 -0.035,54.3
2109 0.050,100.1097] NSEG times
2110 ( DISTANCE (m), ELEVATION (m))=
2111 [0, 91.26 ]
2112 [44.9, 91.46 ]
2113 [45.1, 91.37 ]
2114 [45.9, 90.84 ]
2115 [47, 90.32 ]
2116 [47.5, 90.22 ]
2117 [48, 90.17 ]
2118 [50.7, 90.19 ]
2119 [51.5, 90.17 ]

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2120 [52.2, 90.13 ]
2121 [52.7, 90.12 ]
2122 [53.3, 90.14 ]
2123 [53.5, 90.31 ]
2124 [53.9, 90.59 ]
2125 [54.3, 90.87 ]
2126 [54.7, 91.04 ]
2127 [55.3, 91.24 ]
2128 [55.5, 91.26 ]
2129 [63.7, 91.37 ]
2130 [100.1097, 91.43 ]
2131 *%-----|-----|
2132 * -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2133 *CONTINUOUS STANDHYD NHYD=["S-1-FO-F-D"], DT=[1]min, AREA=[14.96](ha),
2134 * XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2135 * SCS curve number CN=[74],
2136 * Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2137 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
2138 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2139 * LGI=[315.806](m), MNI=[0.013], SCI=[0](min),
2140 * Continuous simulation parameters:
2141 * IaREcper=[4](hrs), IaREcimp=[4](hrs),
2142 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2143 * InterEventTime=[18](hrs), END=-1
2144 *%-----|-----|
2145 CONTINUOUS NASHYD NHYD=["S-1-FO-F-D"], DT=[1]min, AREA=[14.96](ha),
2146 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2147 N=[3], TP=[1.007]hrs,
2148 Continuous simulation parameters:
2149 IaREcper=[4](hrs),
2150 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2151 InterEventTime=[12](hrs)
2152 Baseflow simulation parameters:
2153 BaseFlowOption=[1],
2154 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2155 VHydCond=[0.055](mm/hr), END=-1
2156 *%-----|-----|
2157 *COMPUTE DUALHYD NHYDin=["S-1-FO-F-D"], CINLET=[1.749](cms), NINLET=[1],
2158 * MajNHYD=["S-1FO-F-DJ"]
2159 * MinNHYD=["S-1FO-F-DN"]
2160 * TMJSTO=[9999999](cu-m)
2161 *%-----|-----|
2162 *ADD HYD NHYDsum=["S-1FO-F-DS"], NHYDs to add=["S-1FO-F-DJ"+"S-1FO-F-DN"]
2163 *%-----|-----|
2164 *ROUTE RESERVOIR NHYDout=["S-1FO-F-DR"],NHYDin=["S-1FO-F-DS"],
2165 * RDT=[1](min),
2166 * TABLE of ( OUTFLOW-STORAGE ) values
2167 * (cms) - (ha-m)
2168 * [ 0.0 , 0.0 ]
2169 * [ 0.1788, 0.5966 ]
2170 * [ -1 , -1 ] (max twenty pts)
2171 * NHYDovf=["S-1FoFDovf"]
2172 *%-----|-----|
2173 * -JFSA 2021-02-26 "S-1-D8" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2174 * -JFSA 2021-03-02 "S-1-D8" is Borrisokane Rd. so it will remain STANDHYD in all
scenarios
2175 CONTINUOUS STANDHYD NHYD=["S-1-D8"], DT=[1](min), AREA=[5.27](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
2176 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
IAPER=[4.67](mm), SLPP=[2.0](%),
2177 LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
2178 LGI=[187.439](m), MNI=[0.013], SCI=[0](min),
2179 Continuous simulation parameters:

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2180 IaREcper=[4](hrs), IaREcimp=[4](hrs),
2181 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2182 InterEventTime=[12](hrs), END=-1
2183 *%-----|-----
2184 * This is a road so it is always STANDHYD
2185 *CONTINUOUS NASHYD NHYD=["S-1-D8"], DT=[1]min, AREA=[5.27](ha),
2186 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2187 * N=[3], TP=[1.10]hrs,
2188 * Continuous simulation parameters:
2189 * IaREcper=[4](hrs),
2190 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2191 * InterEventTime=[12](hrs)
2192 * Baseflow simulation parameters:
2193 * BaseFlowOption=[1] ,
2194 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2195 * VHydCond=[0.055](mm/hr), END=-1
2196 *%-----|-----
2197 *COMPUTE DUALHYD NHYDin=["S-1-D8"], CINLET=[2.279](cms), NINLET=[1],
2198 * MajNHYD=["S-1-D8J"]

2200 * TMJSTO=[9999999](cu-m)
2201 *%-----|-----
2202 *ADD HYD NHYDsum=["S-1-D8S"], NHYDs to add=["S-1-D8J"+"S-1-D8N"]
2203 *%-----|-----
2204 *ADD HYD NHYDsum=["S-1-D"], NHYDs to add=["S-1-Okeefe"+"S-1"+"S-1-Post"]
2205 *%-----|-----
2206 *COMPUTE DUALHYD NHYDin=["S-1-D"], CINLET=[11.616](cms), NINLET=[1],
2207 * MajNHYD=["S-1-D-MJ"]
2208 * MinNHYD=["S-1-D-MN"]
2209 * TMJSTO=[5974](cu-m)
2210 *%-----|-----
2211 *ADD HYD NHYDsum=["S-1-DEV"], NHYDs to add=["S-1-D-MJ"+"S-1-D-MN"]
2212 *%-----|-----
2213 *ROUTE RESERVOIR NHYDout=["S-1-D8R"],NHYDin=["S-1-D8S"],
2214 * RDT=[1](min),
2215 * TABLE of ( OUTFLOW-STORAGE ) values
2216 * (cms) - (ha-m)
2217 * [ 0.0 , 0.0 ]
2218 * [ 0.0630, 0.2102 ]
2219 * [ -1 , -1 ] (max twenty pts)
2220 * NHYDovf=["S-1-D8Rovf"]
2221 *%-----|-----
2222 * -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2223 CONTINUOUS NASHYD NHYD=["S-1-A"], DT=[1]min, AREA=[75.88](ha),
2224 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2225 N=[3], TP=[0.619]hrs,
2226 Continuous simulation parameters:
2227 IaREcper=[4](hrs),
2228 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2229 InterEventTime=[12](hrs)
2230 Baseflow simulation parameters:
2231 BaseFlowOption=[1] ,
2232 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2233 VHydCond=[0.055](mm/hr), END=-1
2234 *%-----|-----
2235 * -JFSA, 2021-01-22 "W_CLAR_UNDE" (west of Clarke sub-catchment) discharges
directly to the jock river through a road side ditch on the west side of Borrisokane
road (station 6016)
2236 CONTINUOUS NASHYD NHYD=["W_CLAR_UNDE"], DT=[1]min, AREA=[35.65](ha),
2237 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2238 N=[3], TP=[1.10]hrs,
2239 Continuous simulation parameters:
2240 IaREcper=[4](hrs),
2241 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2242 InterEventTime=[12](hrs)

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2243 Baseflow simulation parameters:
2244 BaseFlowOption=[1] ,
2245 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2246 VHydCond=[0.055](mm/hr), END=-1
2247 *%-----|-----|
2248 ADD HYD NHYDsum=["SN_FO"], NHYDs to
add=["N_FO"+"520-out"+"MS_P10"+"P10-OVF"+"W_CLAR_UNDE"+"S-1-FO-F-D"+"S-1-D8"+"S-1-A"]
2249 *%-----|-----|
2250 SAVE HYD NHYD=["SN_FO"], # OF PCYCLES=[-1], ICASEsh=[1]
2251 HYD_COMMENT=["Total Flows at Foster Drain"]
2252 *%-----|-----|
2253 *# Hydrograph from Node Foster routed to Node at Cedarview Road
2254 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6016
2255 *#
2256 ROUTE CHANNEL NHYDout=["N_CE"] ,NHYDin=["SN_FO"] ,
2257 RDT=[1](min),
2258 CHLGTH=[159](m), CHSLOPE=[0.0818](%),
2259 FPSLOPE=[0.0818](%),
2260 SECNUM=[1.0], NSEG=[3]
2261 ( SEGRROUGH, SEGDIST (m))=
2262 [0.050,-15.46
2263 -0.035,26.55
2264 0.050,116.76] NSEG times
2265 ( DISTANCE (m), ELEVATION (m))=
2266 [-645.23, 91.50]
2267 [-391.20, 91.50]
2268 [-91.00, 91.50]
2269 [-85.52, 91.50]
2270 [-15.46, 89.40]
2271 [-9.79, 89.31]
2272 [-3.22, 86.24]
2273 [3.22, 85.07]
2274 [10.96, 85.79]
2275 [16.44, 86.49]
2276 [26.55, 89.45]
2277 [29.03, 90.27]
2278 [35.76, 90.67]
2279 [36.67, 91.00]
2280 [108.08, 91.00]
2281 [109.82, 90.50]
2282 [112.04, 90.50]
2283 [114.62, 91.00]
2284 [116.76, 91.50]
2285 *%-----|-----|
2286 *#*****
2287 *# Catchment S-1
2288 *# - To Jock River (north and south of Jock)
2289 *# - Primarily agricultural fields; portion of sand quarry
2290 *%-----|-----|
2291 *# -2020-12-17 "S-1-Undev" and "S-1-Fost" was a part of Foster drain, they are below
the foster pond. Now they are added to S-1 subcatchment based on Project 1474-BCDC,
JFSA, Nov. 2020
2292 *# -2020-12-17 Change O-14 (it was part of Okeefe drain) to "S-1-Okeefe" and add it
to S-1 subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
2293 *# -2020-12-17 Add "S-1-BCDC" as NASHYD
2294 *# -2020-12-17 all other S-1 subcatchment as STANDHYD with DUALHYD and ROUTE RESERVOIR
2295 *%-----|-----|
2296 *#*****
2297 *# -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2298 *CONTINUOUS NASHYD NHYD=["S-1-A"], DT=[1]min, AREA=[75.88](ha),
2299 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2300 * N=[3], TP=[0.619]hrs,
2301 * Continuous simulation parameters:
2302 * IaRECper=[4](hrs),
2303 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),

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2304 *           InterEventTime=[12](hrs)
2305 *           Baseflow simulation parameters:
2306 *           BaseFlowOption=[1] ,
2307 *           InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
2308 *           VHydCond=[0.055](mm/hr) ,   END=-1
2309 *%-----|-----|
2310 CONTINUOUS NASHYD NHYD=["S-1-B"], DT=[1]min, AREA=[55.36](ha) ,
2311 DWF=[0](cms) , CN/C=[77] ,   IA=[4.67](mm) ,
2312 N=[3] , TP=[0.451]hrs ,
2313 Continuous simulation parameters:
2314 IaRECper=[4](hrs) ,
2315 SMIN=[-1](mm) ,   SMAX=[-1](mm) , SK=[0.010]/(mm) ,
2316 InterEventTime=[12](hrs)
2317 Baseflow simulation parameters:
2318 BaseFlowOption=[1] ,
2319 InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
2320 VHydCond=[0.055](mm/hr) ,   END=-1
2321 *%-----|-----|
2322 *# - JFSA 2021-02-24 change the name from S-1-BCDC to S-1-A and S-1-B. Change their
TP values based on the new areas compared to the old ones.
2323 *CONTINUOUS NASHYD NHYD=["S-1-BCDC"], DT=[1]min, AREA=[134.9](ha) ,
2324 * DWF=[0](cms) , CN/C=[77] ,   IA=[4.67](mm) ,
2325 * N=[3] , TP=[1.10]hrs ,
2326 * Continuous simulation parameters:
2327 * IaRECper=[4](hrs) ,
2328 * SMIN=[-1](mm) ,   SMAX=[-1](mm) , SK=[0.010]/(mm) ,
2329 * InterEventTime=[12](hrs)
2330 * Baseflow simulation parameters:
2331 * BaseFlowOption=[1] ,
2332 * InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
2333 * VHydCond=[0.055](mm/hr) ,   END=-1
2334 *%-----|-----|
2335 *# - JFSA 2021-02-24 "S-1-BCDC-1" and "S-1-BCDC-2" are not existing anymore.
"S-1-BCDC-1" is part of "S-1-FO-D2" and "S-1-BCDC-2" is part of "S-1-D2" and "S-1-D3"
2336 *CONTINUOUS NASHYD NHYD=["S-1-BCDC-1"], DT=[1]min, AREA=[0.3](ha) ,
2337 * DWF=[0](cms) , CN/C=[77] ,   IA=[4.67](mm) ,
2338 * N=[3] , TP=[1.10]hrs ,
2339 * Continuous simulation parameters:
2340 * IaRECper=[4](hrs) ,
2341 * SMIN=[-1](mm) ,   SMAX=[-1](mm) , SK=[0.010]/(mm) ,
2342 * InterEventTime=[12](hrs)
2343 * Baseflow simulation parameters:
2344 * BaseFlowOption=[1] ,
2345 * InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
2346 * VHydCond=[0.055](mm/hr) ,   END=-1
2347 *%-----|-----|
2348 *CONTINUOUS NASHYD NHYD=["S-1-BCDC-2"], DT=[1]min, AREA=[1.3](ha) ,
2349 * DWF=[0](cms) , CN/C=[77] ,   IA=[4.67](mm) ,
2350 * N=[3] , TP=[1.10]hrs ,
2351 * Continuous simulation parameters:
2352 * IaRECper=[4](hrs) ,
2353 * SMIN=[-1](mm) ,   SMAX=[-1](mm) , SK=[0.010]/(mm) ,
2354 * InterEventTime=[12](hrs)
2355 * Baseflow simulation parameters:
2356 * BaseFlowOption=[1] ,
2357 * InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
2358 * VHydCond=[0.055](mm/hr) ,   END=-1
2359 *%-----|-----|
2360 *# - JFSA 2021-01-19, after adding Greenbank pond, "S-1-BCDC-3" is not existing
anymore
2361 *CONTINUOUS NASHYD NHYD=["S-1-BCDC-3"], DT=[1]min, AREA=[3.9](ha) ,
2362 * DWF=[0](cms) , CN/C=[77] ,   IA=[4.67](mm) ,
2363 * N=[3] , TP=[1.10]hrs ,
2364 * Continuous simulation parameters:
2365 * IaRECper=[4](hrs) ,
2366 * SMIN=[-1](mm) ,   SMAX=[-1](mm) , SK=[0.010]/(mm) ,

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2367 *           InterEventTime=[12](hrs)
2368 *           Baseflow simulation parameters:
2369 *           BaseFlowOption=[1] ,
2370 *           InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2371 *           VHydCond=[0.055](mm/hr),   END=-1
2372 *%-----|-----|
2373 *   -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
before station 7245 on Jock River
2374 *CONTINUOUS STANDHYD NHYD=["S-1-Okeefe"], DT=[1](min), AREA=[44.93](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
2375 *           LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
IAper=[4.67](mm), SLPP=[2.0](%),
2376 *           LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
2377 *           LGI=[547.296](m), MNI=[0.013], SCI=[0](min),
2378 *           Continuous simulation parameters:
2379 *           IaRECper=[4](hrs), IaRECimp=[4](hrs),
2380 *           SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2381 *           InterEventTime=[12](hrs),   END=-1
2382 *%-----|-----|
2383 *COMPUTE DUALHYD NHYDin=["S-1-Okeefe"], CINLET=[4.796](cms), NINLET=[1],
2384 *           MajNHYD=["S-1-OkMJ"]
2385 *           MinNHYD=["S-1-OkMN"]
2386 *           TMJSTO=[9999999](cu-m)
2387 *%-----|-----|
2388 *ADD HYD NHYDsum=["S-1-OkS"], NHYDs to add=["S-1-OkMJ"+"S-1-OkMN"]
2389 *%-----|-----|
2390 *ROUTE RESERVOIR NHYDout=["S-1-OkSR"] ,NHYDin=["S-1-OkS"] ,
2391 *           RDT=[1](min),
2392 *           TABLE of ( OUTFLOW-STORAGE ) values
2393 *           (cms) - (ha-m)
2394 *           [ 0.0      , 0.0 ]
2395 *           [ 0.5370, 1.7917 ]
2396 *           [   -1   ,  -1   ] (max twenty pts)
2397 *           NHYDovf=["S-1-OkSovf"]
2398 *%-----|-----|
2399 *CONTINUOUS NASHYD NHYD=["S-1-Okeefe"], DT=[1]min, AREA=[44.93](ha),
2400 *           DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2401 *           N=[3], TP=[1.049]hrs,
2402 *           Continuous simulation parameters:
2403 *           IaRECper=[4](hrs),
2404 *           SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2405 *           InterEventTime=[12](hrs)
2406 *           Baseflow simulation parameters:
2407 *           BaseFlowOption=[1] ,
2408 *           InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2409 *           VHydCond=[0.055](mm/hr),   END=-1
2410 *%-----|-----|
2411 *   -JFSA 2021-02-26 "S-1-FO-D1" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2412 *CONTINUOUS STANDHYD NHYD=["S-1-FO-D1"], DT=[1]min, AREA=[5.11](ha),
2413 *           XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2414 *           SCS curve number CN=[74],
2415 *           Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2416 *           LGP=[40](m), MNP=[0.25], SCP=[0](min),
2417 *           Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2418 *           LGI=[184.572](m), MNI=[0.013], SCI=[0](min),
2419 *           Continuous simulation parameters:
2420 *           IaRECper=[4](hrs), IaRECimp=[4](hrs),
2421 *           SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2422 *           InterEventTime=[18](hrs),   END=-1
2423 *%-----|-----|
2424 *COMPUTE DUALHYD NHYDin=["S-1-FO-D1"], CINLET=[0.605](cms), NINLET=[1],
2425 *           MajNHYD=["S-1-FO-D1J"]
2426 *           MinNHYD=["S-1-FO-D1N"]
2427 *           TMJSTO=[9999999](cu-m)

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2428 *%-----|-----|
2429 *ADD HYD          NHYDsum=["S-1-FO-D1S"], NHYDs to add=["S-1-FO-D1N"+"S-1-FO-D1J"]
2430 *%-----|-----|
2431 *ROUTE RESERVOIR NHYDout=["S-1-FO-D1R"], NHYDin=["S-1-FO-D1S"],
2432 *                RDT=[1](min),
2433 *                TABLE of ( OUTFLOW-STORAGE ) values
2434 *                (cms) - (ha-m)
2435 *                [ 0.0      , 0.0 ]
2436 *                [ 0.0611, 0.2038 ]
2437 *                [   -1   ,  -1   ] (max twenty pts)
2438 *                NHYDovf=["S-1FOD1ovf"]
2439 *%-----|-----|
2440 *CONTINUOUS NASHYD NHYD=["S-1-FO-D1"], DT=[1]min, AREA=[5.11](ha),
2441 *                DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2442 *                N=[3], TP=[1.10]hrs,
2443 *                Continuous simulation parameters:
2444 *                IaRECper=[4](hrs),
2445 *                SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2446 *                InterEventTime=[12](hrs)
2447 *                Baseflow simulation parameters:
2448 *                BaseFlowOption=[1],
2449 *                InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2450 *                VHydCond=[0.055](mm/hr), END=-1
2451 *%-----|-----|
2452 * -JFSA 2021-02-26 "S-1-FO-D2" is a part of S-1 sub-catchment. It is moved to drain
before station 980 on Foster Drain
2453 *CONTINUOUS STANDHYD NHYD=["S-1-FO-D2"], DT=[1]min, AREA=[4.94](ha),
2454 *                XIMP=[0.55], TIMP=[0.55], DWF=[0](cms), LOSS=[2],
2455 *                SCS curve number CN=[74],
2456 *                Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2457 *                LGP=[40](m), MNP=[0.25], SCP=[0](min),
2458 *                Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2459 *                LGI=[181.475](m), MNI=[0.013], SCI=[0](min),
2460 *                Continuous simulation parameters:
2461 *                IaRECper=[4](hrs), IaRECimp=[4](hrs),
2462 *                SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2463 *                InterEventTime=[18](hrs), END=-1
2464 *%-----|-----|
2465 *CONTINUOUS NASHYD NHYD=["S-1-FO-D2"], DT=[1]min, AREA=[4.94](ha),
2466 *                DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2467 *                N=[3], TP=[1.10]hrs,
2468 *                Continuous simulation parameters:
2469 *                IaRECper=[4](hrs),
2470 *                SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2471 *                InterEventTime=[12](hrs)
2472 *                Baseflow simulation parameters:
2473 *                BaseFlowOption=[1],
2474 *                InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2475 *                VHydCond=[0.055](mm/hr), END=-1
2476 *%-----|-----|
2477 *COMPUTE DUALHYD  NHYDin=["S-1-FO-D2"], CINLET=[0.508](cms), NINLET=[1],
2478 *                MajNHYD=["S-1-FO-D2J"]
2479 *                MinNHYD=["S-1-FO-D2N"]
2480 *                TMJSTO=[9999999](cu-m)
2481 *%-----|-----|
2482 *ADD HYD          NHYDsum=["S-1-FO-D2S"], NHYDs to add=["S-1-FO-D2J"+"S-1-FO-D2N"]
2483 *%-----|-----|
2484 *ROUTE RESERVOIR NHYDout=["S-1-FO-D2R"], NHYDin=["S-1-FO-D2S"],
2485 *                RDT=[1](min),
2486 *                TABLE of ( OUTFLOW-STORAGE ) values
2487 *                (cms) - (ha-m)
2488 *                [ 0.0      , 0.0 ]
2489 *                [ 0.0590, 0.1970 ]
2490 *                [   -1   ,  -1   ] (max twenty pts)
2491 *                NHYDovf=["S-1FOD2ovf"]
2492 *%-----|-----|

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2493 * -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2494 *CONTINUOUS STANDHYD NHYD=["S-1-FO-F-D"], DT=[1]min, AREA=[14.96](ha),
2495 * XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2496 * SCS curve number CN=[74],
2497 * Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2498 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
2499 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2500 * LGI=[315.806](m), MNI=[0.013], SCI=[0](min),
2501 * Continuous simulation parameters:
2502 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
2503 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2504 * InterEventTime=[18](hrs), END=-1
2505 *%-----|-----|
2506 *CONTINUOUS NASHYD NHYD=["S-1-FO-F-D"], DT=[1]min, AREA=[14.96](ha),
2507 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2508 * N=[3], TP=[1.007]hrs,
2509 * Continuous simulation parameters:
2510 * IaRECper=[4](hrs),
2511 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2512 * InterEventTime=[12](hrs)
2513 * Baseflow simulation parameters:
2514 * BaseFlowOption=[1] ,
2515 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2516 * VHydCond=[0.055](mm/hr), END=-1
2517 *%-----|-----|
2518 *COMPUTE DUALHYD NHYDin=["S-1-FO-F-D"], CINLET=[1.749](cms), NINLET=[1],
2519 * MajNHYD=["S-1FO-F-DJ"]
2520 * MinNHYD=["S-1FO-F-DN"]
2521 * TMJSTO=[9999999](cu-m)
2522 *%-----|-----|
2523 *ADD HYD NHYDsum=["S-1FO-F-DS"], NHYDs to add=["S-1FO-F-DJ"+"S-1FO-F-DN"]
2524 *%-----|-----|
2525 *ROUTE RESERVOIR NHYDout=["S-1FO-F-DR"],NHYDin=["S-1FO-F-DS"] ,
2526 * RDT=[1](min),
2527 * TABLE of ( OUTFLOW-STORAGE ) values
2528 * (cms) - (ha-m)
2529 * [ 0.0 , 0.0 ]
2530 * [ 0.1788, 0.5966 ]
2531 * [ -1 , -1 ] (max twenty pts)
2532 * NHYDovf=["S-1FoFDovf"]
2533 *%-----|-----|
2534 *CONTINUOUS STANDHYD NHYD=["S-1-D1"], DT=[1](min), AREA=[21.67](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
2535 * LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
IAper=[4.67](mm), SLPP=[2.0](%),
2536 * LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
2537 * LGI=[380.088](m), MNI=[0.013], SCI=[0](min),
2538 * Continuous simulation parameters:
2539 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
2540 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2541 * InterEventTime=[12](hrs), END=-1
2542 *%-----|-----|
2543 CONTINUOUS NASHYD NHYD=["S-1-D1"], DT=[1]min, AREA=[21.67](ha),
2544 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2545 N=[3], TP=[1.066]hrs,
2546 Continuous simulation parameters:
2547 IaRECper=[4](hrs),
2548 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2549 InterEventTime=[12](hrs)
2550 Baseflow simulation parameters:
2551 BaseFlowOption=[1] ,
2552 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2553 VHydCond=[0.055](mm/hr), END=-1
2554 *%-----|-----|

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2614 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
2615 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2616 * InterEventTime=[12](hrs), END=-1
2617 *%-----|-----
2618 *CONTINUOUS NASHYD NHYD=["S-1-D3"], DT=[1]min, AREA=[6.79](ha),
2619 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2620 * N=[3], TP=[1.281]hrs,
2621 * Continuous simulation parameters:
2622 * IaRECper=[4](hrs),
2623 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2624 * InterEventTime=[12](hrs)
2625 * Baseflow simulation parameters:
2626 * BaseFlowOption=[1] ,
2627 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2628 * VHydCond=[0.055](mm/hr), END=-1
2629 *%-----|-----
2630 *COMPUTE DUALHYD NHYDin=["S-1-D3"], CINLET=[0.719](cms), NINLET=[1],
2631 * MajNHYD=["S-1-D3J"]
2632 * MinNHYD=["S-1-D3N"]
2633 * TMJSTO=[9999999](cu-m)
2634 *%-----|-----
2635 *ADD HYD NHYDsum=["S-1-D3S"], NHYDs to add=["S-1-D3J"+"S-1-D3N"]
2636 *%-----|-----
2637 *ROUTE RESERVOIR NHYDout=["S-1-D3R"],NHYDin=["S-1-D3S"] ,
2638 * RDT=[1](min),
2639 * TABLE of ( OUTFLOW-STORAGE ) values
2640 * (cms) - (ha-m)
2641 * [ 0.0 , 0.0 ]
2642 * [ 0.0811, 0.2708 ]
2643 * [ -1 , -1 ] (max twenty pts)
2644 * NHYDovf=["S-1-D3Rovf"]
2645 *%-----|-----
2646 *CONTINUOUS STANDHYD NHYD=["S-1-D4"], DT=[1](min), AREA=[3.28](ha), XIMP=[0.65],
2647 * TIMP=[0.65], DWF=[0](cms),
2648 * LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
2649 * IAper=[4.67](mm), SLPP=[2.0](%),
2650 * LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
2651 * IAimp=[1.57](mm), SLPI=[0.75](%),
2652 * LGI=[147.874](m), MNI=[0.013], SCI=[0](min),
2653 * Continuous simulation parameters:
2654 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
2655 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2656 * InterEventTime=[12](hrs), END=-1
2657 *%-----|-----
2658 CONTINUOUS NASHYD NHYD=["S-1-D4"], DT=[1]min, AREA=[3.28](ha),
2659 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2660 * N=[3], TP=[1.10]hrs,
2661 * Continuous simulation parameters:
2662 * IaRECper=[4](hrs),
2663 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2664 * InterEventTime=[12](hrs)
2665 * Baseflow simulation parameters:
2666 * BaseFlowOption=[1] ,
2667 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2668 * VHydCond=[0.055](mm/hr), END=-1
2669 *%-----|-----
2670 *COMPUTE DUALHYD NHYDin=["S-1-D4"], CINLET=[0.373](cms), NINLET=[1],
2671 * MajNHYD=["S-1-D4J"]
2672 * MinNHYD=["S-1-D4N"]
2673 * TMJSTO=[9999999](cu-m)
2674 *%-----|-----
2675 *ADD HYD NHYDsum=["S-1-D4S"], NHYDs to add=["S-1-D4J"+"S-1-D4N"]
2676 *%-----|-----
2677 *ROUTE RESERVOIR NHYDout=["S-1-D4R"],NHYDin=["S-1-D4S"] ,
2678 * RDT=[1](min),
2679 * TABLE of ( OUTFLOW-STORAGE ) values

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2677 *                (cms) - (ha-m)
2678 *                [ 0.0      , 0.0 ]
2679 *                [ 0.0392, 0.1308 ]
2680 *                [   -1   ,   -1   ] (max twenty pts)
2681 *                NHYDovf=["S-1-D4Rovf"]
2682 *%-----|-----|
2683 *CONTINUOUS STANDHYD NHYD=["S-1-D5"], DT=[1](min), AREA=[12.84](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
2685 *                LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
2686 *                LGI=[292.57](m), MNI=[0.013], SCI=[0](min),
2687 *                Continuous simulation parameters:
2688 *                IaRECper=[4](hrs), IaRECimp=[4](hrs),
2689 *                SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2690 *                InterEventTime=[12](hrs), END=-1
2691 *%-----|-----|
2692 CONTINUOUS NASHYD NHYD=["S-1-D5"], DT=[1]min, AREA=[12.84](ha),
2693 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2694 N=[3], TP=[1.10]hrs,
2695 Continuous simulation parameters:
2696 IaRECper=[4](hrs),
2697 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2698 InterEventTime=[12](hrs)
2699 Baseflow simulation parameters:
2700 BaseFlowOption=[1] ,
2701 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2702 VHydCond=[0.055](mm/hr), END=-1
2703 *%-----|-----|
2704 *COMPUTE DUALHYD NHYDin=["S-1-D5"], CINLET=[1.395](cms), NINLET=[1],
2705 *                MajNHYD=["S-1-D5J"]
2706 *                MinNHYD=["S-1-D5N"]
2707 *                TMJSTO=[9999999](cu-m)
2708 *%-----|-----|
2709 *ADD HYD NHYDsum=["S-1-D5S"], NHYDs to add=["S-1-D5J"+"S-1-D5N"]
2710 *%-----|-----|
2711 *ROUTE RESERVOIR NHYDout=["S-1-D5R"] ,NHYDin=["S-1-D5S"] ,
2712 *                RDT=[1](min),
2713 *                TABLE of ( OUTFLOW-STORAGE ) values
2714 *                (cms) - (ha-m)
2715 *                [ 0.0      , 0.0 ]
2717 *                [   -1   ,   -1   ] (max twenty pts)
2718 *                NHYDovf=["S-1-D5Rovf"]
2719 *%-----|-----|
2720 *CONTINUOUS STANDHYD NHYD=["S-1-D6"], DT=[1](min), AREA=[1.75](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
2721 *                LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
IAper=[4.67](mm), SLPP=[2.0](%),
2722 *                LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
2723 *                LGI=[108.01](m), MNI=[0.013], SCI=[0](min),
2724 *                Continuous simulation parameters:
2725 *                IaRECper=[4](hrs), IaRECimp=[4](hrs),
2726 *                SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2727 *                InterEventTime=[12](hrs), END=-1
2728 *%-----|-----|
2729 CONTINUOUS NASHYD NHYD=["S-1-D6"], DT=[1]min, AREA=[1.75](ha),
2730 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2731 N=[3], TP=[1.10]hrs,
2732 Continuous simulation parameters:
2733 IaRECper=[4](hrs),
2734 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2735 InterEventTime=[12](hrs)
2736 Baseflow simulation parameters:

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2737 BaseFlowOption=[1] ,
2738 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2739 VHydCond=[0.055](mm/hr), END=-1
2740 *%-----|-----|
2741 *COMPUTE DUALHYD NHYDin=["S-1-D6"], CINLET=[0.218](cms), NINLET=[1],
2742 * MajNHYD=["S-1-D6J"]
2743 * MinNHYD=["S-1-D6N"]
2744 * TMJSTO=[9999999](cu-m)
2745 *%-----|-----|
2746 *ADD HYD NHYDsum=["S-1-D6S"], NHYDs to add=["S-1-D6J"+"S-1-D6N"]
2747 *%-----|-----|
2748 *ROUTE RESERVOIR NHYDout=["S-1-D6R"],NHYDin=["S-1-D6S"] ,
2749 * RDT=[1](min),
2750 * TABLE of ( OUTFLOW-STORAGE ) values
2751 * (cms) - (ha-m)
2752 * [ 0.0 , 0.0 ]
2753 * [ 0.0209, 0.0698 ]
2754 * [ -1 , -1 ] (max twenty pts)
2755 * NHYDovf=["S-1-D6Rovf"]
2756 *%-----|-----|
2757 *CONTINUOUS STANDHYD NHYD=["S-1-D7"], DT=[1](min), AREA=[2.03](ha), XIMP=[0.65],
2758 * TIMP=[0.65], DWF=[0](cms),
2759 * LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
2760 * IAper=[4.67](mm), SLPP=[2.0](%),
2761 * LGI=[116.33](m), MNI=[0.013], SCI=[0](min),
2762 * Continuous simulation parameters:
2763 * IaREcper=[4](hrs), IaREcimp=[4](hrs),
2764 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2765 * InterEventTime=[12](hrs), END=-1
2766 *%-----|-----|
2767 CONTINUOUS NASHYD NHYD=["S-1-D7"], DT=[1]min, AREA=[2.03](ha),
2768 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2769 * N=[3], TP=[1.10]hrs,
2770 * Continuous simulation parameters:
2771 * IaREcper=[4](hrs),
2772 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2773 * InterEventTime=[12](hrs)
2774 * Baseflow simulation parameters:
2775 * BaseFlowOption=[1] ,
2776 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2777 * VHydCond=[0.055](mm/hr), END=-1
2778 *%-----|-----|
2779 *COMPUTE DUALHYD NHYDin=["S-1-D7"], CINLET=[2.279](cms), NINLET=[1],
2780 * MajNHYD=["S-1-D7J"]
2781 * MinNHYD=["S-1-D7N"]
2782 * TMJSTO=[9999999](cu-m)
2783 *%-----|-----|
2784 *ADD HYD NHYDsum=["S-1-D7S"], NHYDs to add=["S-1-D7J"+"S-1-D7N"]
2785 *%-----|-----|
2786 *ROUTE RESERVOIR NHYDout=["S-1-D7R"],NHYDin=["S-1-D7S"] ,
2787 * RDT=[1](min),
2788 * TABLE of ( OUTFLOW-STORAGE ) values
2789 * (cms) - (ha-m)
2790 * [ 0.0 , 0.0 ]
2791 * [ 0.0243, 0.0810 ]
2792 * [ -1 , -1 ] (max twenty pts)
2793 * NHYDovf=["S-1-D8Rovf"]
2794 *%-----|-----|
2795 * -JFSA 2021-02-26 "S-1-D8" is a part of S-1 sub-catchment. It is moved to drain
2796 * before station 6016 on Jock River
2797 *CONTINUOUS STANDHYD NHYD=["S-1-D8"], DT=[1](min), AREA=[5.27](ha), XIMP=[0.65],
2798 * TIMP=[0.65], DWF=[0](cms),
2799 * LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
2800 * IAper=[4.67](mm), SLPP=[2.0](%),

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2797 *           LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
2798 *           LGI=[187.439](m), MNI=[0.013], SCI=[0](min),
2799 *           Continuous simulation parameters:
2800 *           IaRECper=[4](hrs), IaRECimp=[4](hrs),
2801 *           SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2802 *           InterEventTime=[12](hrs), END=-1
2803 *%-----|-----
2804 *CONTINUOUS NASHYD NHYD=["S-1-D8"], DT=[1]min, AREA=[5.27](ha),
2805 *           DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2806 *           N=[3], TP=[1.10]hrs,
2807 *           Continuous simulation parameters:
2808 *           IaRECper=[4](hrs),
2809 *           SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2810 *           InterEventTime=[12](hrs)
2811 *           Baseflow simulation parameters:
2812 *           BaseFlowOption=[1],
2813 *           InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2814 *           VHydCond=[0.055](mm/hr), END=-1
2815 *%-----|-----
2816 *COMPUTE DUALHYD NHYDin=["S-1-D8"], CINLET=[2.279](cms), NINLET=[1],
2817 *           MajNHYD=["S-1-D8J"]
2818 *           MinNHYD=["S-1-D8N"]
2819 *           TMJSTO=[9999999](cu-m)
2820 *%-----|-----
2821 *ADD HYD NHYDsum=["S-1-D8S"], NHYDs to add=["S-1-D8J"+"S-1-D8N"]
2822 *%-----|-----
2823 *ADD HYD NHYDsum=["S-1-D"], NHYDs to add=["S-1-Okeefe"+"S-1"+"S-1-Fost"]
2824 *%-----|-----
2825 *COMPUTE DUALHYD NHYDin=["S-1-D"], CINLET=[11.616](cms), NINLET=[1],
2826 *           MajNHYD=["S-1-D-MJ"]
2827 *           MinNHYD=["S-1-D-MN"]
2828 *           TMJSTO=[5974](cu-m)
2829 *%-----|-----
2830 *ADD HYD NHYDsum=["S-1-DEV"], NHYDs to add=["S-1-D-MJ"+"S-1-D-MN"]
2831 *%-----|-----
2832 *ROUTE RESERVOIR NHYDout=["S-1-D8R"], NHYDin=["S-1-D8S"],
2833 *           RDT=[1](min),
2834 *           TABLE of ( OUTFLOW-STORAGE ) values
2835 *                   (cms) - (ha-m)
2836 *                   [ 0.0      , 0.0 ]
2837 *                   [ 0.0630, 0.2102 ]
2838 *                   [   -1   ,  -1   ] (max twenty pts)
2839 *           NHYDovf=["S-1-D8Rovf"]
2840 *%-----|-----
2841 *%-----|-----
2842 *           -JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
(W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
2843 *# Catchment W_CLAR
2844 *# - To West Clarke Drain (south of the Jock)
2845 *# - Subdivision with 43% imp. as per Barrhaven South MSS
2846 *# - 2020-11-30 update CLARKE Tributary Drainage Area to = 121 ha based on
P598(04)-11
2847 *# - 2020-11-30 split CLARKE Drainage Area to MAJOR and ALL
2848 *#*****
2849 CONTINUOUS STANDHYD NHYD=["W_CLAR_MJ"], DT=[1]min, AREA=[1.772](ha),
2850 XIMP=[0.46], TIMP=[0.59], DWF=[0](cms), LOSS=[2],
2851 SCS curve number CN=[77],
2852 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
2853 LGP=[40](m), MNP=[0.25], SCP=[0](min),
2854 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
2855 LGI=[109](m), MNI=[0.013], SCI=[0](min),
2856 Continuous simulation parameters:
2857 IaRECper=[4](hrs), IaRECimp=[4](hrs),
2858 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2859 InterEventTime=[18](hrs), END=-1

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2860 *%-----|-----|
2861 *COMPUTE DUALHYD      NHYDin=["W_CLAR_MJ"], CINLET=[0.213](cms), NINLET=[1],
2862 *                      MajNHYD=["W_CLAR_MJj"]
2863 *                      MinNHYD=["W_CLAR_MJn"]
2864 *                      TMJSTO=[0.1](cu-m)
2865 *%-----|-----|
2866 *# 5-Year + 12% Capture
2867 ROUTE RESERVOIR      NHYDout=["W_CLAR_MJn"],NHYDin=["W_CLAR_MJ"],
2868                      RDT=[1](min),
2869                      TABLE of ( OUTFLOW-STORAGE ) values
2870                      (cms) - (ha-m)
2871                      [ 0.0      , 0.0 ]
2872                      [ 0.213  , 0.0001 ]
2873                      [      -1  , -1      ] (max twenty pts)
2874                      NHYDovf=["W_CLAR_MJj"],
2875 *%-----|-----|
2876 *      -Clarke_All area from P 598(04)-11 = 120.207 ha, change to 127.298 ha based on
GIS measurements,
2877 *      -JFSA, 2021-01-19 update W_CLAR_ALL to (121.17-1.772=119.398) ha based on GIS
measurements W_CLAR is 121.17 ha and W_CLAR_MJ is 1.772 ha
2878 CONTINUOUS STANDHYD NHYD=["W_CLAR_ALL"], DT=[1]min, AREA=[119.398](ha),
2879                      XIMP=[0.60], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2880                      SCS curve number CN=[77],
2881                      Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
2882                      LGP=[40](m), MNP=[0.25], SCP=[0](min),
2883                      Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
2884                      LGI=[892.18](m), MNI=[0.013], SCI=[0](min),
2885                      Continuous simulation parameters:
2886                      IaRECPper=[4](hrs), IaRECimp=[4](hrs),
2887                      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2888                      InterEventTime=[18](hrs), END=-1
2889 *%-----|-----|
2890 ADD HYD              NHYDsum=["W_CLAR"], NHYDs to add=["W_CLAR_ALL"+"W_CLAR_MJj"]
2891 *%-----|-----|
2892 SAVE HYD            NHYD=["W_CLAR"], # OF PCYCLES=[-1], ICASEsh=[1]
2893                      HYD_COMMENT=["Total Flows to West Clarke"]
2894 *#*****
2895 *#      West Clarke Pond 2
2896 *#      - Rating curve obtained from Barrhaven South MSS modeling
2897 *#      - Tributary Drainage Area to MSS Pond 2 = 241 ha
2898 *#*****
2899 ROUTE RESERVOIR      NHYDout=["MS_P2"], NHYDin=["W_CLAR"],
2900                      RDT=[1](min),
2901                      TABLE of ( OUTFLOW-STORAGE ) values
2902                      (cms) - (ha-m)
2903                      [ 0.0      , 0.0 ]
2904                      [ 0.128  , 0.161 ]
2905                      [ 0.138  , 0.409 ]
2906                      [ 0.148  , 0.68 ]
2907                      [ 0.227  , 0.931 ]
2908                      [ 0.354  , 1.223 ]
2909                      [ 0.505  , 1.52 ]
2910                      [ 0.666  , 1.821 ]
2911                      [ 0.831  , 2.123 ]
2912                      [ 0.995  , 2.434 ]
2913                      [ 1.069  , 2.583 ]
2914                      [ 1.51   , 2.647 ]
2915                      [ 4.904  , 2.861 ]
2916                      [ 13.048 , 3.188 ]
2917                      [ 23.745 , 3.523 ]
2918                      [ 36.474 , 3.871 ]
2919                      [ 45.938 , 4.127 ]
2920                      [ 61.652 , 4.539 ]
2921                      [      -1  , -1      ] (max twenty pts)
2922                      NHYDovf=["P2-OVF"]
2923 *%-----|-----|

```

```

2924 *#*****
2925 * -JFSA, 2021-01-22 "W_CLAR_UNDE" (west of Clarke sub-catchment) discharges
directly to the jock river through a road side ditch on the west side of Borrisokane
road (station 6016)
2926 *CONTINUOUS NASHYD NHYD=["W_CLAR_UNDE"], DT=[1]min, AREA=[35.65](ha),
2927 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2928 * N=[3], TP=[1.10]hrs,
2929 * Continuous simulation parameters:
2930 * IaRECper=[4](hrs),
2931 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2932 * InterEventTime=[12](hrs)
2933 * Baseflow simulation parameters:
2934 * BaseFlowOption=[1] ,
2935 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2936 * VHydCond=[0.055](mm/hr), END=-1
2937 *%-----|-----|
2938 ADD HYD NHYDsum=["SN_CE"], NHYDs to add=["N_CE"+
2939 + "S-1-D4"+"S-1-D5"+"MS_P2"+"P2-OVF" ]
2940 *%-----|-----|
2941 SAVE HYD NHYD=["SN_CE"], # OF PCYCLES=[-1], ICASEsh=[1]
2942 HYD_COMMENT=["Total Flows before Station 5737 on Jock River"]
2943 *%-----|-----|
2944 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5737
2945 *# JFSA 2021-02-25 add station 5737 before station 5002. Station 5737 was extracted
from the HEC-RAS model
T:\PROJ\1474-16\Design\20201026-QuantityControlAnalysis\HEC-RAS\JockLidar2005
2946 *# JFSA 2021-03-02 change the slope to 0.1% instead of 0.0175 to stabilize the model
2947 ROUTE CHANNEL NHYDout=["5737"] ,NHYDin=["SN_CE"] ,
2948 RDT=[1](min),
2949 CHLGTH=[270](m), CHSLOPE=[0.0175](%),
2950 FPSLOPE=[0.0175](%),
2951 SECNUM=[1.0], NSEG=[3]
2952 ( SEGRROUGH, SEGDIST (m))=
2953 [0.050,-24.04
2954 -0.035,23.92
2955 0.050,1130.8] NSEG times
2956 ( DISTANCE (m), ELEVATION (m))=
2957 [-1060.52, 94 ]
2958 [-268.6, 91.5 ]
2959 [-259.43, 91.5 ]
2960 [-179.48, 91.5 ]
2961 [-67.9, 91.5 ]
2962 [-59.21, 91.5 ]
2963 [-33.19, 91 ]
2964 [-26.08, 90.5 ]
2965 [-24.04, 90 ]
2966 [-13.14, 86.77 ]
2967 [0, 85 ]
2968 [14.68, 86.74 ]
2969 [23.92, 90 ]
2970 [25.78, 90.5 ]
2971 [31.91, 91 ]
2972 [91.95, 91.5 ]
2973 [772.15, 92 ]
2974 [961.49, 92.5 ]
2975 [1044.69, 93 ]
2976 [1130.8, 95 ]
2977 *%-----|-----|
2978 ADD HYD NHYDsum=["5002"], NHYDs to add=["5737"+
2979 + "S-1-D1"+"S-1-D6"+"S-1-D7" ]
2980 *%-----|-----|
2981 SAVE HYD NHYD=["5002"], # OF PCYCLES=[-1], ICASEsh=[1]
2982 HYD_COMMENT=["Total Flows before Station 5002 on Jock River"]
2983 *%-----|-----|
2984 *# Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain
2985 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5002

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2986  *# JFSA 2021-02-19 Change the slope from 0.01 % (as per Stantec Report 2007) to 0.0255
      % so the model will be more stable and give reasonable results. It is justifiable as
      ROUTE CHANNELs aren't well suited to really flat slopes.
2987  *# JFSA 2021-02-19 Change to three ROUTE CHANNEL with length 275 m each instead of one
      with 825 m length so the model will be more stable
2988  *# JFSA 2021-02-26 change the length of 5002 route channel from 825 m to 736 m. That is
      because of adding station 5737 between station 6016 and station 5002. Then the length
      from station 5737 to station 5002 is 736 m. Change the slope from 0.0255 % to 0.09511 %
2989  *
2990  ROUTE CHANNEL      NHYDout=["N_WCa" ] ,NHYDin=["5002" ] ,
2991                    RDT=[1](min) ,
2992                    CHLGTH=[245.33333](m) ,   CHSLOPE=[0.09511](%) ,
2993                    FPSLOPE=[0.09511](%) ,
2994                    SECNUM=[1.0] ,           NSEG=[3]
2995                    ( SEGROUGH, SEGDIST (m))=
2996                      [0.050,-37.5
2997                      -0.035,37.50
2998                      0.050,157.05] NSEG times
2999                    ( DISTANCE (m), ELEVATION (m))=
3000                    [-601.81, 91.5]
3001                    [-37.50, 90.00]
3002                    [-19.61, 87.04]
3003                    [0.00, 85.70]
3004                    [14.87, 86.93]
3005                    [37.50, 90.00]
3006                    [38.54, 90.50]
3007                    [42.23, 91]
3008                    [157.05,91.50]
3009  *                  [161.44, 91.50]
3010  *                  [236.48, 93.00]
3011  *                  [385.47, 92.50]
3012  *                  [390.78, 92.50]
3013  *%-----|
3014  ROUTE CHANNEL      NHYDout=["N_WCb" ] ,NHYDin=["N_WCa" ] ,
3015                    RDT=[1](min) ,
3016                    CHLGTH=[245.33333](m) ,   CHSLOPE=[0.09511](%) ,
3017                    FPSLOPE=[0.09511](%) ,
3018                    SECNUM=[1.0] ,           NSEG=[3]
3019                    ( SEGROUGH, SEGDIST (m))=
3020                      [0.050,-37.5
3021                      -0.035,37.50
3022                      0.050,157.05] NSEG times
3023                    ( DISTANCE (m), ELEVATION (m))=
3024                    [-601.81, 91.5]
3025                    [-37.50, 90.00]
3026                    [-19.61, 87.04]
3027                    [0.00, 85.70]
3028                    [14.87, 86.93]
3029                    [37.50, 90.00]
3030                    [38.54, 90.50]
3031                    [42.23, 91]
3032                    [157.05,91.50]
3033  *%-----|
3034  ROUTE CHANNEL      NHYDout=["N_WC" ] ,NHYDin=["N_WCb" ] ,
3035                    RDT=[1](min) ,
3036                    CHLGTH=[245.33333](m) ,   CHSLOPE=[0.09511](%) ,
3037                    FPSLOPE=[0.09511](%) ,
3038                    SECNUM=[1.0] ,           NSEG=[3]
3039                    ( SEGROUGH, SEGDIST (m))=
3040                      [0.050,-37.5
3041                      -0.035,37.50
3042                      0.050,157.05] NSEG times
3043                    ( DISTANCE (m), ELEVATION (m))=
3044                    [-601.81, 91.5]
3045                    [-37.50, 90.00]
3046                    [-19.61, 87.04]

```

```

3047         [0.00, 85.70]
3048         [14.87, 86.93]
3049         [37.50, 90.00]
3050         [38.54, 90.50]
3051         [42.23, 91]
3052         [157.05,91.50]
3053 *#*****
3054 *       -JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
(W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
3055 *ADD HYD          NHYDsum=["SN_WC"], NHYDs to
add=["MS_P2"+"P2-OVF"+"N_WC"+"W_CLAR_UNDE"]
3056 *%-----|-----|
3057 *SAVE HYD          NHYD=["SN_WC"], # OF PCYCLES=[-1], ICASEsh=[1]
3058 *                HYD_COMMENT=["Total Flows at West Clarke Pond Outlet"]
3059 *%-----|-----|
3060 *# Hydrograph from Node West Clarke routed to Node at Kennedy - Burnett Drain
3061 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4534
3062 *#
3063 ROUTE CHANNEL    NHYDout=["N_KB"] ,NHYDin=["N_WC"] ,
3064                    RDT=[1](min),
3065                    CHLGTH=[1020](m),  CHSLOPE=[0.0498](%),
3066                    FPSLOPE=[0.0498](%),
3067                    SECNUM=[1.0],      NSEG=[3]
3068                    ( SEGROUGH, SEGDIST (m))=
3069                    [0.050,-23.63
3070                    -0.035,23.63
3071                    0.050,728.3] NSEG times
3072                    ( DISTANCE (m), ELEVATION (m))=
3073                    [-1082.01,94]
3074                    [-1028.17,92.5]
3075                    [-992.3,93.5]
3076                    [-279.34,90]
3077                    [-23.63,90]
3078                    [-13.45,87.13]
3079                    [-0.07,86.24]
3080                    [10.54,87.15]
3081                    [23.63,90]
3082                    [24.86,90.5]
3083                    [26.72,91]
3084                    [45.07,91.5]
3085                    [128.17,91.5]
3086                    [270.7,92.5]
3087                    [728.3,95]
3088 *%-----|-----|
3089 *#*****
3090 *#       Catchment KEN_BU
3091 *#       - To Kennedy-Burnett SWM Facility
3092 *#       - Outlets to Fraser-Clarke drain (north of the Jock)
3093 *#       - Medium density residential subdivision
3094 *       - Add Kennedy Burnett model (Convert PCSWMM from NOVATECH June, 2020 to SWMHYMO)
3095 *#*****
3096 *CONTINUOUS STANDHYD NHYD=["KEN_BU"], DT=[1]min, AREA=[281](ha),
3097 *                XIMP=[0.55], TIMP=[0.55], DWF=[0](cms), LOSS=[2],
3098 *                SCS curve number CN=[71],
3099 *                Pervious  surfaces: IAper=[4.67](mm), SLPP=[1](%),
3100 *                LGP=[40](m), MNP=[0.25], SCP=[0](min),
3101 *                Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3102 *                LGI=[1369](m), MNI=[0.013], SCI=[0](min),
3103 *                Continuous simulation parameters:
3104 *                IaRECper=[4](hrs),  IaRECimp=[4](hrs),
3105 *                SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
3106 *                InterEventTime=[18](hrs),  END=-1
3107 *%-----|-----|
3108 *#*****
3109 *#       Existing Kennedy-Burnett SWM Facility
3110 *#       - Rating curve obtained from URTKBP

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3111 *# - Tributary Drainage Area to Pond = 160 ha
3112 *#*****
3113 *ROUTE RESERVOIR NHYDout=["KEN_P"], NHYDin=["KEN_BU"],
3114 * RDT=[1](min),
3115 *
3116 * TABLE of ( OUTFLOW-STORAGE ) values
3117 * (cms) - (ha-m)
3118 * [ 0.0 , 0.0 ]
3119 * [ 0.13 , 0.26 ]
3120 * [ 0.43 , 0.56 ]
3121 * [ 0.67 , 0.90 ]
3122 * [ 0.86 , 1.32 ]
3123 * [ 1.01 , 1.79 ]
3124 * [ 1.15 , 2.33 ]
3125 * [ -1 , -1 ] (max twenty pts)
3126 * NHYDovf=["KEN-OV"]
3127 *%-----|-----
3128 * -JFSA, 2021-01-19 update all KEN_BU areas based on GIS measurements
3129 CONTINUOUS STANDHYD NHYD=["KB-01A"], DT=[1]min, AREA=[40.82](ha), XIMP=[0.097],
3130 TIMP=[0.4], DWF=[0](cms), LOSS=[1]:
3131 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3132 F=[0.00](mm),
3133 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[40](m),
3134 MNP=[0.250], SCP=[0](min),
3135 Impervious areas: IAimp=[0.785](mm), SLPI=[0.5](%),
3136 LGI=[521.664](m), MNI=[0.013], SCI=[0](min),
3137 Continuous simulation parameters:
3138 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
3139 END=-1
3140 *%-----|-----
3141 COMPUTE DUALHYD NHYDin=["KB-01A"], CINLET=[3.6](cms), NINLET=[1],
3142 MajNHYD=["KB-01A-MJ"]
3143 MinNHYD=["KB-01A-MN"]
3144 TMJSTO=[4995](cu-m)
3145 *%-----|-----
3146 ADD HYD NHYDsum=["KB-01A-S"], NHYDs to add=["KB-01A-MJ"+"KB-01A-MN"]
3147 *%-----|-----
3148 CONTINUOUS STANDHYD NHYD=["KB-01B"], DT=[1]min, AREA=[31.1](ha), XIMP=[0.1875],
3149 TIMP=[0.375], DWF=[0](cms), LOSS=[1]:
3150 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3151 F=[0.00](mm),
3152 Pervious areas: IAper=[4.67](mm), SLPP=[0.42](%), LGP=[40](m),
3153 MNP=[0.250], SCP=[0](min),
3154 Impervious areas: IAimp=[0.785](mm), SLPI=[0.42](%),
3155 LGI=[455.339](m), MNI=[0.013], SCI=[0](min),
3156 Continuous simulation parameters:
3157 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
3158 END=-1
3159 *%-----|-----
3160 COMPUTE DUALHYD NHYDin=["KB-01B"], CINLET=[1.585](cms), NINLET=[1],
3161 MajNHYD=["KB-01B-MJ"]
3162 MinNHYD=["KB-01B-MN"]
3163 TMJSTO=[6075](cu-m)
3164 *%-----|-----
3165 ADD HYD NHYDsum=["KB-01B-S"], NHYDs to add=["KB-01B-MJ"+"KB-01B-MN"]
3166 *%-----|-----
3167 CONTINUOUS STANDHYD NHYD=["KB-01C"], DT=[1]min, AREA=[13.78](ha), XIMP=[0.2045],
3168 TIMP=[0.409], DWF=[0](cms), LOSS=[1]:
3169 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3170 F=[0.00](mm),
3171 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3172 MNP=[0.250], SCP=[0](min),
3173 Impervious areas: IAimp=[0.785](mm), SLPI=[0.5](%),
3174 LGI=[303.095](m), MNI=[0.013], SCI=[0](min),
3175 Continuous simulation parameters:
3176 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
3177 END=-1

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3162 *%-----|-----|
3163 COMPUTE DUALHYD NHYDin=["KB-01C"], CINLET=[1.35](cms), NINLET=[1],
3164 MajNHYD=["KB-01C-MJ"]
3165 MinNHYD=["KB-01C-MN"]
3166 TMJSTO=[1880](cu-m)
3167 *%-----|-----|
3168 ADD HYD NHYDsum=["KB-01C-S"], NHYDs to add=["KB-01C-MJ"+"KB-01C-MN"]
3169 *%-----|-----|
3170 CONTINUOUS STANDHYD NHYD=["KB-03"], DT=[1]min, AREA=[84.78](ha), XIMP=[0.197],
TIMP=[0.394], DWF=[0](cms), LOSS=[1]:
3171 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3172 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3173 Impervious areas: IAimp=[0.785](mm), SLPI=[0.63](%),
LGI=[751.798](m), MNI=[0.013], SCI=[0](min),
3174 Continuous simulation parameters:
3175 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3176 *%-----|-----|
3177 COMPUTE DUALHYD NHYDin=["KB-03"], CINLET=[5.27](cms), NINLET=[1],
3178 MajNHYD=["KB-03-MJ"]
3179 MinNHYD=["KB-03-MN"]
3180 TMJSTO=[15500](cu-m)
3181 *%-----|-----|
3182 ADD HYD NHYDsum=["KB-03-S"], NHYDs to add=["KB-03-MJ"+"KB-03-MN"]
3183 *%-----|-----|
3184 CONTINUOUS STANDHYD NHYD=["KB-04"], DT=[1]min, AREA=[6.95](ha), XIMP=[0.85],
TIMP=[0.85], DWF=[0](cms), LOSS=[1]:
3185 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3186 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3187 Impervious areas: IAimp=[0.942](mm), SLPI=[0.5](%),
LGI=[215.252](m), MNI=[0.013], SCI=[0](min),
3188 Continuous simulation parameters:
3189 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3190 *%-----|-----|
3191 COMPUTE DUALHYD NHYDin=["KB-04"], CINLET=[0.503](cms), NINLET=[1],
3192 MajNHYD=["KB-04-MJ"]
3193 MinNHYD=["KB-04-MN"]
3194 TMJSTO=[1972](cu-m)
3195 *%-----|-----|
3196 ADD HYD NHYDsum=["KB-04-S"], NHYDs to add=["KB-04-MJ"+"KB-04-MN"]
3197 *%-----|-----|
3198 CONTINUOUS STANDHYD NHYD=["KB-05"], DT=[1]min, AREA=[5.19](ha), XIMP=[0.93],
TIMP=[0.93], DWF=[0](cms), LOSS=[1]:
3199 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3200 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3201 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[186.011](m), MNI=[0.013], SCI=[0](min),
3202 Continuous simulation parameters:
3203 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3204 *%-----|-----|
3205 *%-----|-----|
3206 CONTINUOUS STANDHYD NHYD=["KB-06"], DT=[1]min, AREA=[12.93](ha), XIMP=[0.873],
TIMP=[0.873], DWF=[0](cms), LOSS=[1]:
3207 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3208 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3209 Impervious areas: IAimp=[0.942](mm), SLPI=[4.75](%),

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3210 LGI=[293.598](m), MNI=[0.013], SCI=[0](min),
3211 Continuous simulation parameters:
3212 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
3213 END=-1
3214 *%-----|-----|
3215 COMPUTE DUALHYD NHYDin=["KB-06"], CINLET=[2.262](cms), NINLET=[1],
3216 MajNHYD=["KB-06-MJ"]
3217 MinNHYD=["KB-06-MN"]
3218 TMJSTO=[1950](cu-m)
3219 *%-----|-----|
3220 ADD HYD NHYDsum=["KB-06-S"], NHYDs to add=["KB-06-MJ"+"KB-06-MN"]
3221 *%-----|-----|
3222 CONTINUOUS STANDHYD NHYD=["KB-11"], DT=[1]min, AREA=[4.03](ha), XIMP=[0.675],
3223 TIMP=[0.675], DWF=[0](cms), LOSS=[1]:
3224 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3225 F=[0.00](mm),
3226 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3227 MNP=[0.250], SCP=[0](min),
3228 Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%),
3229 LGI=[163.911](m), MNI=[0.013], SCI=[0](min),
3230 Continuous simulation parameters:
3231 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
3232 END=-1
3233 *%-----|-----|
3234 COMPUTE DUALHYD NHYDin=["KB-11"], CINLET=[0.5773](cms), NINLET=[1],
3235 MajNHYD=["KB-11-MJ"]
3236 MinNHYD=["KB-11-MN"]
3237 TMJSTO=[597](cu-m)
3238 *%-----|-----|
3239 ADD HYD NHYDsum=["KB-11-S"], NHYDs to add=["KB-11-MJ"+"KB-11-MN"]
3240 *%-----|-----|
3241 CONTINUOUS STANDHYD NHYD=["S1"], DT=[1]min, AREA=[4.99](ha), XIMP=[0.93], TIMP=[0.93],
3242 DWF=[0](cms), LOSS=[1]:
3243 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3244 F=[0.00](mm),
3245 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3246 MNP=[0.250], SCP=[0](min),
3247 Impervious areas: IAimp=[1.57](mm), SLPI=[2.0](%),
3248 LGI=[182.392](m), MNI=[0.013], SCI=[0](min),
3249 Continuous simulation parameters:
3250 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
3251 END=-1
3252 *%-----|-----|
3253 CONTINUOUS STANDHYD NHYD=["KB-15"], DT=[1]min, AREA=[2.15](ha), XIMP=[0.79],
3254 TIMP=[0.79], DWF=[0](cms), LOSS=[1]:
3255 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3256 F=[0.00](mm),
3257 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3258 MNP=[0.250], SCP=[0](min),
3259 Impervious areas: IAimp=[0.157](mm), SLPI=[0.3](%),
3260 LGI=[119.722](m), MNI=[0.013], SCI=[0](min),
3261 Continuous simulation parameters:
3262 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
3263 END=-1
3264 *%-----|-----|
3265 ADD HYD NHYDsum=["KB-P1"], NHYDs to
3266 add=["KB-01A-S"+"KB-01B-S"+"KB-01C-S"+"KB-03-S"+"KB-04-S"+"KB-05"+"KB-06-S"+"KB-11-S"+"KB
3267 -15"+"S1"]
3268 *%-----|-----|
3269 ROUTE RESERVOIR NHYDout=["KB-P1R"], NHYDin=["KB-P1"],
3270 RDT=[1](min),
3271 TABLE of ( OUTFLOW-STORAGE ) values
3272 (cms) - (ha-m)
3273 [ 0.0 , 0.0 ]
3274 [0.076,0.003]

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3257 [0.088,0.006]
3258 [0.136,0.011]
3259 [0.301,0.017]
3260 [0.454,0.027]
3261 [0.631,0.041]
3262 [1.173,0.068]
3263 [1.91,0.111]
3264 [4.847,0.231]
3265 [9.813,0.436]
3266 [12.134,0.617]
3267 [12.438,0.732]
3268 [12.424,0.811]
3269 [12.425,0.894]
3270 [ -1 , -1 ] (max twenty pts)
3271 NHYDovf=["KB-Plovf"]
3272 *%-----|-----|
3273 ADD HYD NHYDsum=["KB-Pond1"], NHYDs to add=["KB-P1R"+"KB-Plovf"]
3274 *%-----|-----|
3275 SAVE HYD NHYD=["KB-Pond1"], # OF PCYCLES=[-1], ICASEsh=[1]
3276 HYD_COMMENT=["Total Flows at KB first pond"]
3277 *%-----|-----|
3278 CONTINUOUS STANDHYD NHYD=["KB-07"], DT=[1]min, AREA=[10.86](ha), XIMP=[0.86],
TIMP=[0.86], DWF=[0](cms), LOSS=[1]:
3279 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3280 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3281 Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%),
LGI=[269.072](m), MNI=[0.013], SCI=[0](min),
3282 Continuous simulation parameters:
3283 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3284 *%-----|-----|
3285 COMPUTE DUALHYD NHYDin=["KB-07"], CINLET=[2.094](cms), NINLET=[1],
3286 MaJNHYD=["KB-07-MJ"]
3287 MinNHYD=["KB-07-MN"]
3288 TMJSTO=[1378](cu-m)
3289 *%-----|-----|
3290 ADD HYD NHYDsum=["KB-07-S"], NHYDs to add=["KB-07-MJ"+"KB-07-MN"]
3291 *%-----|-----|
3292 CONTINUOUS STANDHYD NHYD=["KB-08"], DT=[1]min, AREA=[6.61](ha), XIMP=[0.64],
TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3293 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3294 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3295 Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%),
LGI=[209.921](m), MNI=[0.013], SCI=[0](min),
3296 Continuous simulation parameters:
3297 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3298 *%-----|-----|
3299 COMPUTE DUALHYD NHYDin=["KB-08"], CINLET=[1.058](cms), NINLET=[1],
3300 MaJNHYD=["KB-08-MJ"]
3301 MinNHYD=["KB-08-MN"]
3302 TMJSTO=[787](cu-m)
3303 *%-----|-----|
3304 ADD HYD NHYDsum=["KB-08-S"], NHYDs to add=["KB-08-MJ"+"KB-08-MN"]
3305 *%-----|-----|
3306 CONTINUOUS STANDHYD NHYD=["KB-09"], DT=[1]min, AREA=[2.6](ha), XIMP=[0.86],
TIMP=[0.86], DWF=[0](cms), LOSS=[1]:
3307 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3308 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3309 Impervious areas: IAimp=[1.57](mm), SLPI=[2.0](%),

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3310          LGI=[131.656](m), MNI=[0.013], SCI=[0](min),
3311          Continuous simulation parameters:
3312          IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
3313          END=-1
3314          *%-----|-----|
3315          *%-----|-----|
3316          CONTINUOUS STANDHYD NHYD=["KB-10_1"], DT=[1]min, AREA=[2.37](ha), XIMP=[0.86],
3317          TIMP=[0.86], DWF=[0](cms), LOSS=[1]:
3318          Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3319          F=[0.00](mm),
3320          Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3321          MNP=[0.250], SCP=[0](min),
3322          Impervious areas: IAimp=[1.57](mm), SLPI=[2.0](%),
3323          LGI=[125.698](m), MNI=[0.013], SCI=[0](min),
3324          Continuous simulation parameters:
3325          IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
3326          END=-1
3327          *%-----|-----|
3328          *%-----|-----|
3329          CONTINUOUS STANDHYD NHYD=["KB-10_2"], DT=[1]min, AREA=[1.14](ha), XIMP=[0.86],
3330          TIMP=[0.86], DWF=[0](cms), LOSS=[1]:
3331          Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3332          F=[0.00](mm),
3333          Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3334          MNP=[0.250], SCP=[0](min),
3335          Impervious areas: IAimp=[1.57](mm), SLPI=[2.0](%), LGI=[87.178](m),
3336          MNI=[0.013], SCI=[0](min),
3337          Continuous simulation parameters:
3338          IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
3339          END=-1
3340          *%-----|-----|
3341          *%-----|-----|
3342          CONTINUOUS STANDHYD NHYD=["KB-12"], DT=[1]min, AREA=[4.86](ha), XIMP=[0.79],
3343          TIMP=[0.79], DWF=[0](cms), LOSS=[1]:
3344          Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3345          F=[0.00](mm),
3346          Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3347          MNP=[0.250], SCP=[0](min),
3348          Impervious areas: IAimp=[1.099](mm), SLPI=[2.0](%),
3349          LGI=[180.000](m), MNI=[0.013], SCI=[0](min),
3350          Continuous simulation parameters:
3351          IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
3352          END=-1
3353          *%-----|-----|
3354          *%-----|-----|
3355          COMPUTE DUALHYD NHYDin=["KB-12"], CINLET=[0.8665](cms), NINLET=[1],
3356          MajNHYD=["KB-12-MJ"]
3357          MinNHYD=["KB-12-MN"]
3358          TMJSTO=[632](cu-m)
3359          *%-----|-----|
3360          *%-----|-----|
3361          ADD HYD NHYDsum=["KB-12-S"], NHYDs to add=["KB-12-MJ"+"KB-12-MN"]
3362          *%-----|-----|
3363          *%-----|-----|
3364          CONTINUOUS STANDHYD NHYD=["KB-13"], DT=[1]min, AREA=[10.19](ha), XIMP=[0.64],
3365          TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3366          Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3367          F=[0.00](mm),
3368          Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3369          MNP=[0.250], SCP=[0](min),
3370          Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%),
3371          LGI=[260.640](m), MNI=[0.013], SCI=[0](min),
3372          Continuous simulation parameters:
3373          IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
3374          END=-1
3375          *%-----|-----|
3376          *%-----|-----|
3377          COMPUTE DUALHYD NHYDin=["KB-13"], CINLET=[1.722](cms), NINLET=[1],
3378          MajNHYD=["KB-13-MJ"]
3379          MinNHYD=["KB-13-MN"]
3380          TMJSTO=[1077](cu-m)

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3354 *%-----|-----|
3355 ADD HYD      NHYDsum=["KB-13-S"], NHYDs to add=["KB-13-MJ"+"KB-13-MN"]
3356 *%-----|-----|
3357 CONTINUOUS STANDHYD NHYD=["KB-14"], DT=[1]min, AREA=[5.47](ha), XIMP=[0.64],
TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3358 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3359 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3360 Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%),
LGI=[190.962](m), MNI=[0.013], SCI=[0](min),
3361 Continuous simulation parameters:
3362 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3363 *%-----|-----|
3364 COMPUTE DUALHYD NHYDin=["KB-14"], CINLET=[0.8734](cms), NINLET=[1],
3365 MajNHYD=["KB-14-MJ"]
3366 MinNHYD=["KB-14-MN"]
3367 TMJSTO=[631](cu-m)
3368 *%-----|-----|
3369 ADD HYD      NHYDsum=["KB-14-S"], NHYDs to add=["KB-14-MJ"+"KB-14-MN"]
3370 *%-----|-----|
3371 *%-----|-----|
3372 CONTINUOUS STANDHYD NHYD=["KB-16_2"], DT=[1]min, AREA=[3.42](ha), XIMP=[0.71],
TIMP=[0.71], DWF=[0](cms), LOSS=[1]:
3373 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3374 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3375 Impervious areas: IAimp=[0.157](mm), SLPI=[0.3](%),
LGI=[150.997](m), MNI=[0.013], SCI=[0](min),
3376 Continuous simulation parameters:
3377 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3378 *%-----|-----|
3379 ADD HYD      NHYDsum=["KB-P2"], NHYDs to
add=["KB-Pond1"+"KB-07-S"+"KB-08-S"+"KB-09"+"KB-10_1"+"KB-10_2"+"KB-12-S"+"KB-13-S"+"KB-1
4-S"+"KB-16_2"]
3380 *%-----|-----|
3381 ROUTE RESERVOIR NHYDout=["KB-P2R"], NHYDin=["KB-P2"],
3382 RDT=[1](min),
3383 TABLE of ( OUTFLOW-STORAGE ) values
3384 (cms) - (ha-m)
3385 [ 0.0 , 0.0 ]
3386 [0.053,0.005]
3387 [0.132,0.009]
3388 [0.269,0.014]
3389 [0.455,0.023]
3390 [0.699,0.037]
3391 [0.947,0.056]
3392 [1.853,0.09]
3393 [2.712,0.146]
3394 [6.626,0.287]
3395 [11.228,0.515]
3396 [14.885,0.738]
3397 [16.473,0.893]
3398 [17.311,0.998]
3399 [17.633,1.063]
3400 [17.634,1.112]
3401 [ -1 , -1 ] (max twenty pts)
3402 NHYDovf=["KB-P2ovf"]
3403 *%-----|-----|
3404 ADD HYD      NHYDsum=["KB-Pond2"], NHYDs to add=["KB-P2R"+"KB-P2ovf"]
3405 *%-----|-----|
3406 SAVE HYD     NHYD=["KB-Pond2"], # OF PCYCLES=[-1], ICASEsh=[1]
3407 HYD_COMMENT=["Total Flows at KB second pond"]

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3408 *%-----|-----|
3409 CONTINUOUS STANDHYD NHYD=["KB-16_1"], DT=[1]min, AREA=[2.8](ha), XIMP=[0.75],
TIMP=[0.75], DWF=[0](cms), LOSS=[1]:
3410 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3411 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3412 Impervious areas: IAimp=[0.157](mm), SLPI=[0.3](%),
LGI=[136.626](m), MNI=[0.013], SCI=[0](min),
3413 Continuous simulation parameters:
3414 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3415 *%-----|-----|
3416 ADD HYD NHYDsum=["KB-P3"], NHYDs to add=["KB-Pond2"+"KB-16_1"]
3417 *%-----|-----|
3418 *%-----|-----|
3419 * One inflow node from pond 3 is added to the model (ROUTE RESERVOIR)
3420 * Another inflow node from right side of pond 3 is not added to the model
3421 ROUTE RESERVOIR NHYDout=["KB-P3R"], NHYDin=["KB-P3"],
3422 RDT=[1](min),
3423 TABLE of ( OUTFLOW-STORAGE ) values
3424 (cms) - (ha-m)
3425 [ 0.0 , 0.0 ]
3426 [0.051,0.002]
3427 [0.048,0.003]
3428 [0.057,0.029]
3429 [0.089,0.045]
3430 [0.133,0.069]
3431 [0.199,0.106]
3432 [0.321,0.172]
3433 [1.029,0.306]
3434 [4.036,0.527]
3435 [8.332,0.761]
3436 [11.727,0.941]
3437 [14.125,1.067]
3438 [15.675,1.149]
3439 [16.555,1.196]
3440 [16.911,1.214]
3441 [ -1 , -1 ] (max twenty pts)
3442 NHYDovf=["KB-P3ovf"]
3443 *%-----|-----|
3444 ADD HYD NHYDsum=["KB-Pond3"], NHYDs to add=["KB-P3R"+"KB-P3ovf"]
3445 *%-----|-----|
3446 SAVE HYD NHYD=["KB-Pond3"], # OF PCYCLES=[-1], ICASEsh=[1]
3447 HYD_COMMENT=["Total Flows at KB third pond"]
3448 *%-----|-----|
3449 *#*****
3450 *# EXISTING / PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118080), SWM
Modeling Approach, NOVATECH Report June, 2020)
3451 *# - TO FRASER-CLARKE DRAIN
3452 *#*****
3453 CONTINUOUS STANDHYD NHYD=["FC-01"], DT=[1]min, AREA=[8.03](ha), XIMP=[0.47],
TIMP=[0.47], DWF=[0](cms), LOSS=[1]:
3454 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3455 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3456 Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
LGI=[231.373](m), MNI=[0.013], SCI=[0](min),
3457 Continuous simulation parameters:
3458 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3459 *%-----|-----|
3460 COMPUTE DUALHYD NHYDin=["FC-01"], CINLET=[0.756](cms), NINLET=[1],
3461 MajNHYD=["FC-01-MJ"]
3462 MinNHYD=["FC-01-MN"]

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3463          TMJSTO=[714](cu-m)
3464  *%-----|-----|
3465  ADD HYD      NHYDsum=["FC-01-S"], NHYDs to add=["FC-01-MJ"+"FC-01-MN"]
3466  *%-----|-----|
3467  CONTINUOUS STANDHYD NHYD=["FC-02"], DT=[1]min, AREA=[16.05](ha), XIMP=[0.93],
TIMP=[0.93], DWF=[0](cms), LOSS=[1]:
3468          Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3469          Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3470          Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
LGI=[327.109](m), MNI=[0.013], SCI=[0](min),
3471          Continuous simulation parameters:
3472          IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3473  *%-----|-----|
3474  COMPUTE DUALHYD NHYDin=["FC-02"], CINLET=[1.159](cms), NINLET=[1],
3475          MajNHYD=["FC-02-MJ"]
3476          MinNHYD=["FC-02-MN"]
3477          TMJSTO=[2385](cu-m)
3478  *%-----|-----|
3479  ADD HYD      NHYDsum=["FC-02-S"], NHYDs to add=["FC-02-MJ"+"FC-02-MN"]
3480  *%-----|-----|
3481  CONTINUOUS STANDHYD NHYD=["FC-03"], DT=[1]min, AREA=[7.37](ha), XIMP=[0.64],
TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3482          Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3483          Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3484          Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
LGI=[221.660](m), MNI=[0.013], SCI=[0](min),
3485          Continuous simulation parameters:
3486          IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3487  *%-----|-----|
3488  COMPUTE DUALHYD NHYDin=["FC-03"], CINLET=[0.358](cms), NINLET=[1],
3489          MajNHYD=["FC-03-MJ"]
3490          MinNHYD=["FC-03-MN"]
3491          TMJSTO=[1131](cu-m)
3492  *%-----|-----|
3493  ADD HYD      NHYDsum=["FC-03-S"], NHYDs to add=["FC-03-MJ"+"FC-03-MN"]
3494  *%-----|-----|
3495  CONTINUOUS STANDHYD NHYD=["FC-04"], DT=[1]min, AREA=[12.87](ha), XIMP=[0.64],
TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3496          Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3497          Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3498          Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
LGI=[292.916](m), MNI=[0.013], SCI=[0](min),
3499          Continuous simulation parameters:
3500          IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3501  *%-----|-----|
3502  COMPUTE DUALHYD NHYDin=["FC-04"], CINLET=[0.741](cms), NINLET=[1],
3503          MajNHYD=["FC-04-MJ"]
3504          MinNHYD=["FC-04-MN"]
3505          TMJSTO=[1794](cu-m)
3506  *%-----|-----|
3507  ADD HYD      NHYDsum=["FC-04-S"], NHYDs to add=["FC-04-MJ"+"FC-04-MN"]
3508  *%-----|-----|
3509  *#*****
3510  *#   PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118080), SWM Modeling
Approach, NOVATECH Report June, 2020)
3511  *#   - TO JOCK RIVER
3512  *#*****

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3513 CONTINUOUS STANDHYD NHYD=["JR-01"], DT=[1]min, AREA=[8.24](ha), XIMP=[0.64],
TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3514 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3515 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3516 Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
LGI=[234.379](m), MNI=[0.013], SCI=[0](min),
3517 Continuous simulation parameters:
3518 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3519 *%-----|-----|
3520 COMPUTE DUALHYD NHYDin=["JR-01"], CINLET=[0.563](cms), NINLET=[1],
3521 MajNHYD=["JR-01-MJ"]
3522 MinNHYD=["JR-01-MN"]
3523 TMJSTO=[1040](cu-m)
3524 *%-----|-----|
3525 ADD HYD NHYDsum=["JR-01-S"], NHYDs to add=["JR-01-MJ"+"JR-01-MN"]
3526 *%-----|-----|
3527 CONTINUOUS STANDHYD NHYD=["JR-02"], DT=[1]min, AREA=[1.59](ha), XIMP=[0.64],
TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3528 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3529 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3530 Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
LGI=[102.956](m), MNI=[0.013], SCI=[0](min),
3531 Continuous simulation parameters:
3532 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3533 *%-----|-----|
3534 COMPUTE DUALHYD NHYDin=["JR-02"], CINLET=[0.153](cms), NINLET=[1],
3535 MajNHYD=["JR-02-MJ"]
3536 MinNHYD=["JR-02-MN"]
3537 TMJSTO=[153](cu-m)
3538 *%-----|-----|
3539 ADD HYD NHYDsum=["JR-02-S"], NHYDs to add=["JR-02-MJ"+"JR-02-MN"]
3540 *%-----|-----|
3541 *#*****
3542 *# Catchment FRASER
3543 *# - To Fraser-Clarke drain (north of the Jock)
3544 *# - Developed land with assumed 43% imp.
3545 *# - 2020-12-17 Change Fraser area to be 35.1 as measured from QGIS
3546 *# - 2020-12-17 All Fraser is undeveloped (Nashyd)
3547 *#*****
3548 CONTINUOUS NASHYD NHYD=["FRASER-DRN"], DT=[1]min, AREA=[13.65](ha),
3549 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
3550 N=[3], TP=[0.4258]hrs,
3551 Continuous simulation parameters:
3552 IaRECper=[4](hrs),
3553 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3554 InterEventTime=[12](hrs)
3555 Baseflow simulation parameters:
3556 BaseFlowOption=[1],
3557 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
3558 VHydCond=[0.055](mm/hr), END=-1
3559 *%-----|-----|
3560 *CONTINUOUS STANDHYD NHYD=["FRASER-D"], DT=[1]min, AREA=[21.61](ha),
3561 * XIMP=[0.585], TIMP=[0.585], DWF=[0](cms), LOSS=[2],
3562 * SCS curve number CN=[80],
3563 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3564 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3565 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3566 * LGI=[379.561](m), MNI=[0.013], SCI=[0](min),
3567 * Continuous simulation parameters:
3568 * IaRECper=[4](hrs), IaRECimp=[4](hrs),

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3569 *          SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
3570 *          InterEventTime=[18](hrs),  END=-1
3571 *%-----|-----|
3572 CONTINUOUS NASHYD  NHYD=["FRASER-D"], DT=[1]min, AREA=[21.61](ha),
3573 DWF=[0](cms), CN/C=[77],  IA=[4.67](mm),
3574 N=[3], TP=[0.674]hrs,
3575 Continuous simulation parameters:
3576 IaREcper=[4](hrs),
3577 SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
3578 InterEventTime=[12](hrs)
3579 Baseflow simulation parameters:
3580 BaseFlowOption=[1] ,
3581 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
3582 VHydCond=[0.055](mm/hr),  END=-1
3583 *%-----|-----|
3584 *COMPUTE DUALHYD  NHYDin=["FRASER-D"], CINLET=[3.545](cms), NINLET=[1],
3585 *          MajNHYD=["FRASER-J"]
3586 *          MinNHYD=["FRASER-N"]
3587 *          TMJSTO=[9999999](cu-m)
3588 *%-----|-----|
3589 *ADD HYD          NHYDsum=["FRASER-S"], NHYDs to add=["FRASER-J"+"FRASER-N"]
3590 *%-----|-----|
3591 *ROUTE RESERVOIR NHYDout=["MS_P20"], NHYDin=["FRASER"],
3592 *          RDT=[1](min),
3593 *          TABLE of ( OUTFLOW-STORAGE ) values
3594 *          (cms) - (ha-m)
3595 *          [ 0.0 , 0.0 ]
3596 *          [ 0.04 , 0.36 ]
3597 *          [ -1 , -1 ] (max twenty pts)
3598 *          NHYDovf=["P20-OVF"]
3599 *%-----|-----|
3600 ADD HYD          NHYDsum=["4241"], NHYDs to
add=["KB-Pond3"+"S-1-B"+"FRASER-DRN"+"FRASER-D"+"N_KB"+"FC-01-S"+"FC-02-S"+"FC-03-S"]
3601 *%-----|-----|
3602 SAVE HYD        NHYD=["4241"], # OF PCYCLES=[-1], ICASEsh=[1]
3603 HYD_COMMENT=["Total Flows at Ken-Burnett Outlet"]
3604 *%-----|-----|
3605 *# Hydrograph from Node Ken-Burnett to station 3633
3606 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4241
3607 *#
3608 ROUTE CHANNEL  NHYDout=["4241-out"], NHYDin=["4241"], RDT=[1](min),
3609 CHLGTH=[294](m),  CHSLOPE=[0.1088](%), FPSLOPE=[0.1088](%),
3610 SECNUM=[1.0],      NSEG=[3]
3611 ( SEGROUGH, SEGDIST (m))=[0.05, -20.12
3612 -0.035, 45.26
3613 0.05, 403.84] NSEG times
3614 ( DISTANCE (m), ELEVATION (m))=[]
3615 [-909.72, 95 ]
3616 [-907.09, 94.5 ]
3617 [-904.65, 94 ]
3618 [-902.26, 93.5 ]
3619 [-44.51, 91.5 ]
3620 [-25.1, 91.5 ]
3621 [-20.98, 91 ]
3622 [-20.61, 90.5 ]
3623 [-20.12, 90 ]
3624 [-6.13, 87.26 ]
3625 [17.51, 86.56 ]
3626 [31.37, 87.2 ]
3627 [45.26, 90 ]
3628 [50.41, 90.5 ]
3629 [63.06, 91 ]
3630 [134.5, 91.5 ]
3631 [190.63, 92 ]
3632 [251.98, 92.5 ]
3633 [321.32, 93.5 ]

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3634 [403.84, 95 ]
3635 *%-----|-----|
3636 ADD HYD NHYDsum=["SN_KB"], NHYDs to
add=["4241-out"+"FC-04-S"+"JR-01-S"+"JR-02-S"]
3637 *%-----|-----|
3638 SAVE HYD NHYD=["SN_KB"], # OF PCYCLES=[-1], ICASEsh=[1]
3639 HYD_COMMENT=["Total Flows before Station 3633"]
3640 *%-----|-----|
3641 *# Hydrograph from Station 3633 to Node Todd
3642 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 3633
3643 *# JFSA 2021-02-26 change the channel length (at station 3633) from 650m to 608m and
change the slope from 0.0498% to 0.24671%. That is because of adding station 4241
between station 4534 and station 3633
3644 *#
3645 ROUTE CHANNEL NHYDout=["N_TO"], NHYDin=["SN_KB"], RDT=[1](min),
3646 CHLGTH=[608](m), CHSLOPE=[0.24671](%), FPSLOPE=[0.24671](%),
3647 SECNUM=[1.0], NSEG=[3]
3648 ( SEGROUGH, SEGDIST (m))=[0.05, -23.74
3649 -0.035, 23.74
3650 0.05, 26.50] NSEG times
3651 ( DISTANCE (m), ELEVATION (m))=[]
3652 -29.24, 91.0
3653 -27.41, 90.5
3654 -25.64, 90
3655 -23.74, 89.5
3656 -22, 89.26
3657 -20, 88.51
3658 -19, 88.32
3659 -15, 88.1
3660 -10, 88.11
3661 -5, 88.17
3662 0, 88.27
3663 5, 88.19
3664 10, 88.06
3665 15, 88.48
3666 16, 88.7
3667 23.74, 89.5
3668 24.68, 90
3669 25.57, 90.5
3670 26.50, 91.0
3671 * [-29.24, 91]
3672 * [-27.41, 90.5]
3673 * [-25.64, 90]
3674 * [-23.74, 89.5]
3675 * [-22, 89.26]
3676 * [-20, 88.51]
3677 * [-19, 88.32]
3678 * [-15, 88.1]
3679 * [-10, 88.11]
3680 * [-5, 88.17]
3681 * [0, 88.27]
3682 * [5, 88.19]
3683 * [10, 88.06]
3684 * [15, 88.48]
3685 * [16, 88.7]
3686 * [23.74, 89.5]
3687 * [24.68, 90]
3688 * [25.57, 90.5]
3689 *%-----|-----|
3690 *#*****
3691 *# Catchment Greenbank
3692 *# - To Greenbank Drain (south of the Jock)
3693 *# - JFSA 2021-01-18 add Greenbank pond as per JFSA, P598(06)-15, June 2016
3694 *# - JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GIS measurements
3695 *#*****
3696 CONTINUOUS STANDHYD NHYD=["Greenbank"], DT=[1]min, AREA=[36.6](ha),

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3697 XIMP=[0.639], TIMP=[0.682], DWF=[0](cms), LOSS=[2],
3698 SCS curve number CN=[77],
3699 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3700 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3701 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3702 LGI=[493.96](m), MNI=[0.013], SCI=[0](min),
3703 Continuous simulation parameters:
3704 IaRECper=[4](hrs), IaRECimp=[4](hrs),
3705 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3706 InterEventTime=[18](hrs), END=-1
3707 *%-----|-----|
3708 ROUTE RESERVOIR NHYDout=["GreenB_MN"], NHYDin=["Greenbank"],
3709 RDT=[1](min),
3710 TABLE of ( OUTFLOW-STORAGE ) values
3711 (cms) - (ha-m)
3712 [ 0.0 , 0.0 ]
3713 [ 0.033 , 0.084 ]
3714 [ 0.039 , 0.201 ]
3715 [ 0.113 , 0.292 ]
3716 [ 0.237 , 0.386 ]
3717 [ 0.382 , 0.484 ]
3718 [ 0.539 , 0.585 ]
3719 [ 0.7 , 0.692 ]
3720 [ 0.86 , 0.804 ]
3721 [ 4.684 , 0.922 ]
3722 [ 11.539 , 1.052 ]
3723 [ 20.867 , 1.168 ]
3724 [ 103.616 , 1.974 ]
3725 [ -1 , -1 ] (max twenty pts)
3726 NHYDovf=["GreenB_MJ"],
3727 *%-----|-----|
3728 *%-----|-----|
3729 ADD HYD NHYDsum=["GreenB"], NHYDs to add=["N_TO"+"GreenB_MJ"+"GreenB_MN"]
3730 *%-----|-----|
3731 SAVE HYD NHYD=["GreenB"], # OF PCYCLES=[-1], ICASEsh=[1]
3732 HYD_COMMENT=["Total Flows at Greenbank Drain"]
3733 *%-----|-----|
3734 *#*****|*****|
3735 *# Catchment TODD
3736 *# - To Todd Drain (south of the Jock)
3737 *# - Subdivision with 43% imp. as per Barrhaven South MSS
3738 *# - 2020-11-30 increase imp. based on P598(04)-11
3739 *# - 2020-11-30 update TODD Tributary Drainage Area to = 146.015 ha based on
P598(04)-11
3740 *# - 2020-11-30 split TODD Drainage Area to MAJOR, MINOR, POND and ALL
3741 *#*****|*****|
3742 *# - JFSA 2021-01-19 add "TODD_MN1" as part of Clarke("W_CLAR_MJ") and remove it
from Todd
3743 *CONTINUOUS STANDHYD NHYD=["TODD_MN1"], DT=[1]min, AREA=[1.772](ha),
3744 * XIMP=[0.53], TIMP=[0.57], DWF=[0](cms), LOSS=[2],
3745 * SCS curve number CN=[77],
3746 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3747 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3748 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3749 * LGI=[108.689](m), MNI=[0.013], SCI=[0](min),
3750 * Continuous simulation parameters:
3751 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
3752 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3753 * InterEventTime=[18](hrs), END=-1
3754 *%-----|-----|
3755 CONTINUOUS STANDHYD NHYD=["TODD_MN2"], DT=[1]min, AREA=[2.1](ha),
3756 XIMP=[0.53], TIMP=[0.57], DWF=[0](cms), LOSS=[2],
3757 SCS curve number CN=[77],
3758 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3759 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3760 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),

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3761             LGI=[118.322](m), MNI=[0.013], SCI=[0](min),
3762 Continuous simulation parameters:
3763 IaREcper=[4](hrs), IaREcimp=[4](hrs),
3764 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3765 InterEventTime=[18](hrs), END=-1
3766 *%-----|-----|
3767 CONTINUOUS STANDHYD NHYD=["TODD_MN3"], DT=[1]min, AREA=[0.117](ha),
3768 XIMP=[0.53], TIMP=[0.57], DWF=[0](cms), LOSS=[2],
3769 SCS curve number CN=[77],
3770 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3771             LGP=[40](m), MNP=[0.25], SCP=[0](min),
3772 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3773             LGI=[27.928](m), MNI=[0.013], SCI=[0](min),
3774 Continuous simulation parameters:
3775 IaREcper=[4](hrs), IaREcimp=[4](hrs),
3776 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3777 InterEventTime=[18](hrs), END=-1
3778 *%-----|-----|
3779 CONTINUOUS STANDHYD NHYD=["TODD_MJ"], DT=[1]min, AREA=[30.230](ha),
3780 XIMP=[0.52], TIMP=[0.64], DWF=[0](cms), LOSS=[2],
3781 SCS curve number CN=[77],
3782 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3783             LGP=[40](m), MNP=[0.25], SCP=[0](min),
3784 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3785             LGI=[448.925](m), MNI=[0.013], SCI=[0](min),
3786 Continuous simulation parameters:
3787 IaREcper=[4](hrs), IaREcimp=[4](hrs),
3788 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3789 InterEventTime=[18](hrs), END=-1
3790 *%-----|-----|
3791 * -JFSA, 2021-01-19 update "TODD_ALL" area from 108.741 ha to 112.908 ha based on
GIS measurements (148.41-30.23-0.117-2.1-3.055=112.908 ha)
3792 CONTINUOUS STANDHYD NHYD=["TODD_ALL"], DT=[1]min, AREA=[112.908](ha),
3793 XIMP=[0.52], TIMP=[0.57], DWF=[0](cms), LOSS=[2],
3794 SCS curve number CN=[77],
3795 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3796             LGP=[40](m), MNP=[0.25], SCP=[0](min),
3797 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3798             LGI=[867.594](m), MNI=[0.013], SCI=[0](min),
3799 Continuous simulation parameters:
3800 IaREcper=[4](hrs), IaREcimp=[4](hrs),
3801 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3802 InterEventTime=[18](hrs), END=-1
3803 *%-----|-----|
3804 CONTINUOUS STANDHYD NHYD=["TODD_P"], DT=[1]min, AREA=[3.055](ha),
3805 XIMP=[0.63], TIMP=[0.63], DWF=[0](cms), LOSS=[2],
3806 SCS curve number CN=[77],
3807 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3808             LGP=[40](m), MNP=[0.25], SCP=[0](min),
3809 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3810             LGI=[142.712](m), MNI=[0.013], SCI=[0](min),
3811 Continuous simulation parameters:
3812 IaREcper=[4](hrs), IaREcimp=[4](hrs),
3813 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3814 InterEventTime=[18](hrs), END=-1
3815 *%-----|-----|
3816 *%-----|-----|
3817 * -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"
and its parameters remain the same.
3818 *CONTINUOUS STANDHYD NHYD=["TODD_DEVL"], DT=[1]min, AREA=[15.87](ha),
3819 * XIMP=[0.63], TIMP=[0.63], DWF=[0](cms), LOSS=[2],
3820 * SCS curve number CN=[77],
3821 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3822 *             LGP=[40](m), MNP=[0.25], SCP=[0](min),
3823 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),

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3824 *           LGI=[325.27](m), MNI=[0.013], SCI=[0](min),
3825 *           Continuous simulation parameters:
3826 *           IaRECper=[4](hrs), IaRECimp=[4](hrs),
3827 *           SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3828 *           InterEventTime=[18](hrs), END=-1
3829 *%-----|-----|
3830 *           -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
is called "corr2" and its parameters remain the same.
3831 *CONTINUOUS NASHYD NHYD=["TODD_UnD"], DT=[1]min, AREA=[12.47](ha),
3832 *           DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
3833 *           N=[3], TP=[1.10]hrs,
3834 *           Continuous simulation parameters:
3835 *           IaRECper=[4](hrs),
3836 *           SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3837 *           InterEventTime=[12](hrs)
3838 *           Baseflow simulation parameters:
3839 *           BaseFlowOption=[1],
3840 *           InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
3841 *           VHydCond=[0.055](mm/hr), END=-1
3842 *%-----|-----|
3843 *# 5-Year + 12% Capture
3844 *COMPUTE DUALHYD NHYDin=["TODD_MJ"], CINLET=[3.314](cms), NINLET=[1],
3845 *           MajNHYD=["TODD_MJj"]
3846 *           MinNHYD=["TODD_MJn"]
3847 *           TMJSTO=[0.1](cu-m)
3848 ROUTE RESERVOIR NHYDout=["TODD_MJn"],NHYDin=["TODD_MJ"],
3849 RDT=[1](min),
3850           TABLE of ( OUTFLOW-STORAGE ) values
3851           (cms) - (ha-m)
3852           [ 0.0 , 0.0 ]
3853           [ 3.314 , 0.0001 ]
3854           [ -1 , -1 ] (max twenty pts)
3855           NHYDovf=["TODD_MJj"],
3856 *%-----|-----|
3857 *# 5-Year + 12% Capture
3858 *COMPUTE DUALHYD NHYDin=["TODD_MN1"], CINLET=[0.227](cms), NINLET=[1],
3859 *           MajNHYD=["TODD_MN1j"]
3860 *           MinNHYD=["TODD_MN1n"]
3861 *           TMJSTO=[0.1](cu-m)
3862 *ROUTE RESERVOIR NHYDout=["TODD_MN1n"],NHYDin=["TODD_MN1"],
3863 RDT=[1](min),
3864           TABLE of ( OUTFLOW-STORAGE ) values
3865           (cms) - (ha-m)
3866           [ 0.0 , 0.0 ]
3867           [ 0.227 , 0.0001 ]
3868           [ -1 , -1 ] (max twenty pts)
3869           NHYDovf=["TODD_MN1j"],
3870 *%-----|-----|
3871 *COMPUTE DUALHYD NHYDin=["TODD_MN2"], CINLET=[0.268](cms), NINLET=[1],
3872 *           MajNHYD=["TODD_MN2j"]
3873 *           MinNHYD=["TODD_MN2n"]
3874 *           TMJSTO=[0.1](cu-m)
3875 ROUTE RESERVOIR NHYDout=["TODD_MN2n"],NHYDin=["TODD_MN2"],
3876 RDT=[1](min),
3877           TABLE of ( OUTFLOW-STORAGE ) values
3878           (cms) - (ha-m)
3879           [ 0.0 , 0.0 ]
3880           [ 0.268 , 0.0001 ]
3881           [ -1 , -1 ] (max twenty pts)
3882           NHYDovf=["TODD_MN2j"],
3883 *%-----|-----|
3884 *COMPUTE DUALHYD NHYDin=["TODD_MN3"], CINLET=[0.016](cms), NINLET=[1],
3885 *           MajNHYD=["TODD_MN3j"]
3886 *           MinNHYD=["TODD_MN3n"]
3887 *           TMJSTO=[0.1](cu-m)
3888 ROUTE RESERVOIR NHYDout=["TODD_MN3n"],NHYDin=["TODD_MN3"],

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3889 RDT=[1](min),
3890 TABLE of ( OUTFLOW-STORAGE ) values
3891 (cms) - (ha-m)
3892 [ 0.0 , 0.0 ]
3893 [ 0.016 , 0.0001 ]
3894 [ -1 , -1 ] (max twenty pts)
3895 NHYDovf=["TODD_MN3j"] ,
3896 *%-----|-----|
3897 * -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
major system from A2 can be added to Todd
3898 CONTINUOUS STANDHYD NHYD=["A2"], DT=[1]min, AREA=[25.5](ha),
3899 XIMP=[0.42], TIMP=[0.52], DWF=[0](cms), LOSS=[2],
3900 SCS curve number CN=[75],
3901 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3902 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3903 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3904 LGI=[566](m), MNI=[0.013], SCI=[0](min),
3905 Continuous simulation parameters:
3906 IaRECper=[4](hrs), IaRECimp=[4](hrs),
3907 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3908 InterEventTime=[18](hrs), END=-1
3909 *%-----|-----|
3910 COMPUTE DUALHYD NHYDin=["A2"], CINLET=[1.818](cms), NINLET=[1],
3911 MajNHYD=["A2-MJ"]
3912 MinNHYD=["A2-MN"]
3913 TMJSTO=[924](cu-m)
3914 *%-----|-----|
3915 ADD HYD NHYDsum=["TODD"], NHYDs to
add=["TODD_MN2n"+"TODD_MN3n"+"TODD_MJj"+"TODD_P"+"TODD_ALL"+"W_CLAR_MJn"]
3916 *%-----|-----|
3917 SAVE HYD NHYD=["TODD"], # OF PCYCLES=[-1], ICASEsh=[1]
3918 HYD_COMMENT=["Total Flows at Todd Drain"]
3919 *%-----|-----|
3920 *#*****
3921 *# Todd Pond 3
3922 *# - Rating curve obtained from Barrhaven South MSS modeling
3923 *# - stantec 2007, Tributary Drainage Area to MSS Pond 3 = 193 ha
3924 *#*****
3925 ROUTE RESERVOIR NHYDout=["MS_P3"], NHYDin=["TODD"],
3926 RDT=[1](min),
3927 TABLE of ( OUTFLOW-STORAGE ) values
3928 (cms) - (ha-m)
3929 [ 0.0 , 0.0 ]
3930 [ 0.014 , 0.155 ]
3931 [ 0.048 , 0.394 ]
3932 [ 0.061 , 0.56 ]
3933 [ 0.08 , 0.909 ]
3934 [ 0.088 , 1.089 ]
3935 [ 0.109 , 1.652 ]
3936 [ 0.118 , 1.952 ]
3937 [ 0.122 , 2.099 ]
3938 [ 1.972 , 2.269 ]
3939 [ 9.135 , 2.598 ]
3940 [ 15.608 , 2.826 ]
3941 [ 19.256 , 2.942 ]
3942 [ 27.282 , 3.181 ]
3943 [ 40.957 , 3.55 ]
3944 [ 56.372 , 3.929 ]
3945 [ 73.349 , 4.317 ]
3946 [ 85.469 , 4.579 ]
3947 [ 104.771 , 4.977 ]
3948 [ -1 , -1 ] (max twenty pts)
3949 NHYDovf=["P3-OVF"]
3950 *%-----|-----|
3951 ADD HYD NHYDsum=["SN_TO"], NHYDs to
add=["GreenB"+"MS_P3"+"P3-OVF"+"TODD_MN2j"+"A2-MJ"]

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3952 *%-----|-----|
3953 SAVE HYD      NHYD=["SN_TO"], # OF PCYCLES=[-1], ICASEsh=[1]
3954              HYD_COMMENT=["Total Flows at Todd Drain"]
3955 *%-----|-----|
3956 *#
3957 *# Hydrograph from Todd Drain routed to Corrigan Drain
3958 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
3959 *# 2021-02-19 Change the slope from 0.033 % (as per Stantec Report 2007) to 0.05 % so
the model will be more stable and give reasonable results. It is justifiable as ROUTE
CHANNELs aren't well suited to really flat slopes.
3960 *
3961 ROUTE CHANNEL  NHYDout=["N_TO"] ,NHYDin=["SN_TO"] ,
3962              RDT=[1](min),
3963              CHLGTH=[280](m),  CHSLOPE=[0.05](%),
3964              FPSLOPE=[0.05](%),
3965              SECNUM=[1.0],      NSEG=[3]
3966              ( SEGROUGH, SEGDIST (m))=
3967              [0.075,-17.72
3968              -0.045,17.72
3969              0.075,80.62] NSEG times
3970              ( DISTANCE (m), ELEVATION (m))=
3971              [-83.32, 90.00]
3972              [-81.36, 89.50]
3973              [-79.12, 89.00]
3974              [-76.13, 88.50]
3975              [-20.46, 88.00]
3976              [-19.36, 87.50]
3977              [-18.51, 87.00]
3978              [-17.72, 86.50]
3979              [-11.95, 85.24]
3980              [-0.11, 85.12]
3981              [11.49, 85.20]
3982              [17.72, 86.50]
3983              [19.74, 87.00]
3984              [21.22, 87.50]
3985              [22.68, 88.00]
3986              [24.28, 88.50]
3987              [26.79, 89.00]
3988              [71.98, 90.00]
3989              [80.62, 90.50]
3990 *%-----|-----|
3991 SAVE HYD      NHYD=["N_TO"], # OF PCYCLES=[-1], ICASEsh=[1]
3992              HYD_COMMENT=["Total inflows at Station 2462"]
3993 *%-----|-----|
3994 *#*****
3995 *# Catchment CORRIG
3996 *# - To Corrigan Drain (south of the Jock)
3997 *# - Primarily Developed (medium density)
3998 *# - JFSA JAN 2021, add Corrigan subcatchments as per IBI, July 2008
3999 *#*****
4000 *ROUTE RESERVOIR  NHYDout=["MS_P1"], NHYDin=["CORRIG"],
4001 *              RDT=[1](min),
4002 *              TABLE of ( OUTFLOW-STORAGE ) values
4003 *              (cms) - (ha-m)
4004 *              [ 0.0 , 0.0 ]
4005 *              [ 0.06 , 0.58]
4006 *              [ -1 , -1 ] (max twenty pts)
4007 *              NHYDovf=["P1-OVF"]
4008 *%-----|-----|
4009 *ADD HYD      NHYDsum=["SN_CO"], NHYDs to add=["N_TO"+"P1-OVF"+"MS_P1"]
4010 *%-----|-----|
4011 *SAVE HYD      NHYD=["SN_CO"], # OF PCYCLES=[-1], ICASEsh=[1]
4012 *              HYD_COMMENT=["Total Flows at Corrigan Drain"]
4013 *%-----|-----|
4014 * -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"

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and its parameters remain the same.
4015 CONTINUOUS STANDHYD NHYD=["corr1"], DT=[1]min, AREA=[15.87](ha),
4016 XIMP=[0.63], TIMP=[0.63], DWF=[0](cms), LOSS=[2],
4017 SCS curve number CN=[77],
4018 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4019 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4020 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4021 LGI=[325.27](m), MNI=[0.013], SCI=[0](min),
4022 Continuous simulation parameters:
4023 IaREcper=[4](hrs), IaREcimp=[4](hrs),
4024 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4025 InterEventTime=[18](hrs), END=-1
4026 *%-----|-----|
4027 * -JFSA 2021-02-23 add DUALHYD for "corr1". "corr1" DUALHYD Parameters are the
same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to "corr1".
4028 * At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for
Al-Corrig
4029 COMPUTE DUALHYD NHYDin=["corr1"], CINLET=[1.818](cms), NINLET=[1],
4030 MajNHYD=["corr1-MJ"]
4031 MinNHYD=["corr1-MN"]
4032 TMJSTO=[924](cu-m)
4033 *%-----|-----|
4034 * -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
is called "corr2" and its parameters remain the same.
4035 CONTINUOUS NASHYD NHYD=["corr2"], DT=[1]min, AREA=[12.47](ha),
4036 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
4037 N=[3], TP=[1.10]hrs,
4038 Continuous simulation parameters:
4039 IaREcper=[4](hrs),
4040 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4041 InterEventTime=[12](hrs)
4042 Baseflow simulation parameters:
4043 BaseFlowOption=[1] ,
4044 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4045 VHydCond=[0.055](mm/hr), END=-1
4046 *%-----|-----|
4047 * -JFSA 2021-01-19 change Al-Corrig to be developed as per geottawa website and
apply the parameters of A2, the nearest sub-catchment to Al-Corrig, LGI is calculated
based on Al-Corrig area
4048 * -JFSA 2021-01-19 update all Corrigan areas based on GIS measurements, and keep
LGI as it is from Corrigan Report, IBI Group, 2008 because LGI calculated is less than
LGI from the Corrigan Report
4049 CONTINUOUS STANDHYD NHYD=["Al-Corrig"], DT=[1]min, AREA=[15.75](ha),
4050 XIMP=[0.42], TIMP=[0.52], DWF=[0](cms), LOSS=[2],
4051 SCS curve number CN=[75],
4052 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4053 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4054 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4055 LGI=[324.037](m), MNI=[0.013], SCI=[0](min),
4056 Continuous simulation parameters:
4057 IaREcper=[4](hrs), IaREcimp=[4](hrs),
4058 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4059 InterEventTime=[18](hrs), END=-1
4060 *
4061 * -JFSA 2021-01-25 add DUALHYD for Al-Corrig. Al-Corrig DUALHYD Parameters are the
same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to Al-Corrig.
4062 * At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for
Al-Corrig
4063 COMPUTE DUALHYD NHYDin=["Al-Corrig"], CINLET=[1.818](cms), NINLET=[1],
4064 MajNHYD=["Al-MJ"]
4065 MinNHYD=["Al-MN"]
4066 TMJSTO=[924](cu-m)
4067 *%-----|-----|
4068 *CONTINUOUS NASHYD NHYD=["Al-Corrig"], DT=[1]min, AREA=[15.75](ha),
4069 * DWF=[0](cms), CN/C=[66], IA=[2.5](mm),
4070 * N=[3.0], TP=[0.36]hrs,

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4071 *           Continuous simulation parameters:
4072 *           IaRECper=[4](hrs),
4073 *           SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
4074 *           InterEventTime=[12](hrs)
4075 *           Baseflow simulation parameters:
4076 *           BaseFlowOption=[1] ,
4077 *           InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4078 *           VHydCond=[0.055](mm/hr),  END=-1
4079 *%-----|-----
4080 CONTINUOUS NASHYD NHYD=["B1"], DT=[1]min, AREA=[2.77](ha),
4081 DWF=[0](cms),  CN/C=[56], IA=[2.5](mm),
4082 N=[3.0], TP=[0.23]hrs,
4083 Continuous simulation parameters:
4084 IaRECper=[4](hrs),
4085 SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
4086 InterEventTime=[12](hrs)
4087 Baseflow simulation parameters:
4088 BaseFlowOption=[1] ,
4089 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4090 VHydCond=[0.055](mm/hr),  END=-1
4091 *%-----|-----
4092 CONTINUOUS STANDHYD NHYD=["A4"], DT=[1]min, AREA=[1.27](ha),
4093 XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
4094 SCS curve number CN=[75],
4095 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4096 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4097 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4098 LGI=[253](m), MNI=[0.013], SCI=[0](min),
4099 Continuous simulation parameters:
4100 IaRECper=[4](hrs),  IaRECimp=[4](hrs),
4101 SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
4102 InterEventTime=[18](hrs),  END=-1
4103 *%-----|-----
4104 COMPUTE DUALHYD NHYDin=["A4"], CINLET=[0.405](cms), NINLET=[1],
4105 MajNHYD=["A4-MJ"]
4106 MinNHYD=["A4-MN"]
4107 TMJSTO=[68](cu-m)
4108 *%-----|-----
4109 ADD HYD NHYDsum=["MH101"], NHYDs to
add=["A1-MJ"+"A1-MN"+"corr1-MJ"+"corr1-MN"+"corr2"+"B1"+"A4-MN"]
4110 *%-----|-----
4111 SAVE HYD NHYD=["MH101"], # OF PCYCLES=[-1], ICASEsh=[1]
4112 HYD_COMMENT=["Total Flows at MH101"]
4113 *%-----|-----
4114 ROUTE PIPE PTYPE=[1]circ, NHYDout=["101-102"], RNUMBER=[1.0], PDIAM=[1050](mm),
4115 PLNGTH=[368](m), PROUGH=[0.013], PSLOPE=[0.0054](m/m),
NHYDin=["MH101"], RDT=[1]
4116 *%-----|-----
4117 * -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
major system from A2 can be added to Todd
4118 *CONTINUOUS STANDHYD NHYD=["A2"], DT=[1]min, AREA=[25.5](ha),
4119 * XIMP=[0.42], TIMP=[0.52], DWF=[0](cms), LOSS=[2],
4120 * SCS curve number CN=[75],
4121 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4122 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
4123 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4124 * LGI=[566](m), MNI=[0.013], SCI=[0](min),
4125 * Continuous simulation parameters:
4126 * IaRECper=[4](hrs),  IaRECimp=[4](hrs),
4127 * SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
4128 * InterEventTime=[18](hrs),  END=-1
4129 *%-----|-----
4130 *COMPUTE DUALHYD NHYDin=["A2"], CINLET=[1.818](cms), NINLET=[1],
4131 * MajNHYD=["A2-MJ"]
4132 * MinNHYD=["A2-MN"]
4133 * TMJSTO=[924](cu-m)

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4134 *%-----|-----|
4135 ADD HYD      NHYDsum=["MH102"], NHYDs to add=["A2-MN"+"101-102"]
4136 *%-----|-----|
4137 SAVE HYD     NHYD=["MH102"], # OF PCYCLES=[-1], ICASEsh=[1]
4138             HYD_COMMENT=["Total Flows at MH102"]
4139 *%-----|-----|
4140 CONTINUOUS STANDHYD NHYD=["A5"], DT=[1]min, AREA=[1.6](ha),
4141             XIMP=[0.71], TIMP=[0.71], DWF=[0](cms), LOSS=[2],
4142             SCS curve number CN=[75],
4143             Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4144             LGP=[40](m), MNP=[0.25], SCP=[0](min),
4145             Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4146             LGI=[300](m), MNI=[0.013], SCI=[0](min),
4147             Continuous simulation parameters:
4148             IaRECper=[4](hrs), IaRECimp=[4](hrs),
4149             SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4150             InterEventTime=[18](hrs), END=-1
4151 *%-----|-----|
4152 ADD HYD      NHYDsum=["A5T"], NHYDs to add=["A4-MJ"+"A5"]
4153 *%-----|-----|
4154 COMPUTE DUALHYD NHYDin=["A5T"], CINLET=[0.357](cms), NINLET=[1],
4155             MajNHYD=["A5-MJ"]
4156             MinNHYD=["A5-MN"]
4157             TMJSTO=[60](cu-m)
4158 *%-----|-----|
4159 * -JFSA Jan. 2021, A3 is a part of Todd so it is removed
4160 * -JFSA Jan. 2021, "A2-MJ" added to "Todd"
4161 *CONTINUOUS STANDHYD NHYD=["A3"], DT=[1]min, AREA=[18.4](ha),
4162 *             XIMP=[0.58], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
4163 *             SCS curve number CN=[75],
4164 *             Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4165 *             LGP=[40](m), MNP=[0.25], SCP=[0](min),
4166 *             Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4167 *             LGI=[450](m), MNI=[0.013], SCI=[0](min),
4168 *             Continuous simulation parameters:
4169 *             IaRECper=[4](hrs), IaRECimp=[4](hrs),
4170 *             SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4171 *             InterEventTime=[18](hrs), END=-1
4172 *%-----|-----|
4173 *ADD HYD      NHYDsum=["A3-A2MJ"], NHYDs to add=["A2-MJ"+"A3"]
4174 *%-----|-----|
4175 *COMPUTE DUALHYD NHYDin=["A3-A2MJ"], CINLET=[2.208](cms), NINLET=[1],
4176 *             MajNHYD=["A3R-MJ"]
4177 *             MinNHYD=["A3R-MN"]
4178 *             TMJSTO=[908](cu-m)
4179 *%-----|-----|
4180 ROUTE PIPE    PTYPE=[1]circ, NHYDout=["102-103"], RNUMBER=[1.0], PDIAM=[1500](mm),
4181             PLNGTH=[504](m), PROUGH=[0.013], PSLOPE=[0.0028](m/m),
4182             NHYDin=["MH102"], RDT=[1]
4183 *%-----|-----|
4184 ADD HYD      NHYDsum=["MH103"], NHYDs to add=["102-103"+"A5-MN"]
4185 *%-----|-----|
4186 SAVE HYD     NHYD=["MH103"], # OF PCYCLES=[-1], ICASEsh=[1]
4187             HYD_COMMENT=["Total Flows at MH103"]
4188 *%-----|-----|
4189 ROUTE PIPE    PTYPE=[1]circ, NHYDout=["103-104"], RNUMBER=[1.0], PDIAM=[1650](mm),
4190             PLNGTH=[438](m), PROUGH=[0.013], PSLOPE=[0.0046](m/m),
4191             NHYDin=["MH103"], RDT=[1]
4192 *%-----|-----|
4193 CONTINUOUS STANDHYD NHYD=["A6"], DT=[1]min, AREA=[1.56](ha),
4194             XIMP=[0.71], TIMP=[0.71], DWF=[0](cms), LOSS=[2],
4195             SCS curve number CN=[75],
4196             Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4197             LGP=[40](m), MNP=[0.25], SCP=[0](min),
4198             Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4199             LGI=[280](m), MNI=[0.013], SCI=[0](min),

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4198 Continuous simulation parameters:
4199 IaRECPper=[4](hrs), IaRECImp=[4](hrs),
4200 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4201 InterEventTime=[18](hrs), END=-1
4202 *%-----|-----|
4203 ADD HYD NHYDsum=["A6T"], NHYDs to add=["A5-MJ"+"A6"]
4204 *%-----|-----|
4205 COMPUTE DUALHYD NHYDin=["A6T"], CINLET=[0.357](cms), NINLET=[1],
4206 MajNHYD=["A6-MJ"]
4207 MinNHYD=["A6-MN"]
4208 TMJSTO=[60](cu-m)
4209 *%-----|-----|
4210 * -JFSA Jan. 2021, A7-corrig is a part of Todd so it is removed
4211 *CONTINUOUS STANDHYD NHYD=["A7-corrig"], DT=[1]min, AREA=[11.8](ha),
4212 * XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4213 * SCS curve number CN=[75],
4214 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4215 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
4216 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4217 * LGI=[438](m), MNI=[0.013], SCI=[0](min),
4218 * Continuous simulation parameters:
4219 * IaRECPper=[4](hrs), IaRECImp=[4](hrs),
4220 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4221 * InterEventTime=[18](hrs), END=-1
4222 *%-----|-----|
4223 *ADD HYD NHYDsum=["A7-A3RMJ"], NHYDs to add=["A3R-MJ"+"A7-corrig"]
4224 *%-----|-----|
4225 *COMPUTE DUALHYD NHYDin=["A7-A3RMJ"], CINLET=[1.003](cms), NINLET=[1],
4226 * MajNHYD=["A7R-MJ"]
4227 * MinNHYD=["A7R-MN"]
4228 * TMJSTO=[496](cu-m)
4229 *%-----|-----|
4230 ADD HYD NHYDsum=["MH104"], NHYDs to add=["A6-MN"+"103-104"+"TODD_MJn"]
4231 *%-----|-----|
4232 SAVE HYD NHYD=["MH104"], # OF PCYCLES=[-1], ICASEsh=[1]
4233 HYD_COMMENT=["Total Flows at MH104"]
4234 *%-----|-----|
4235 CONTINUOUS STANDHYD NHYD=["B2"], DT=[1]min, AREA=[12.31](ha),
4236 XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4237 SCS curve number CN=[75],
4238 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4239 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4240 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4241 LGI=[417](m), MNI=[0.013], SCI=[0](min),
4242 Continuous simulation parameters:
4243 IaRECPper=[4](hrs), IaRECImp=[4](hrs),
4244 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4245 InterEventTime=[18](hrs), END=-1
4246 *%-----|-----|
4247 COMPUTE DUALHYD NHYDin=["B2"], CINLET=[1.029](cms), NINLET=[1],
4248 MajNHYD=["B2-MJ"]
4249 MinNHYD=["B2-MN"]
4250 TMJSTO=[508](cu-m)
4251 *%-----|-----|
4252 ROUTE PIPE PTYPE=[1]circ, NHYDout=["315-333"], RNUMBER=[1.0], PDIAM=[1200](mm),
4253 PLNGTH=[254](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["B2-MN"], RDT=[1]
4254 *%-----|-----|
4255 CONTINUOUS STANDHYD NHYD=["B3"], DT=[1]min, AREA=[5.59](ha),
4256 XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4257 SCS curve number CN=[75],
4258 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4259 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4260 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4261 LGI=[345](m), MNI=[0.013], SCI=[0](min),
4262 Continuous simulation parameters:

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4263 IaREcper=[4](hrs), IaREcimp=[4](hrs),
4264 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4265 InterEventTime=[18](hrs), END=-1
4266 *%-----|
4267 COMPUTE DUALHYD NHYDin=["B3"], CINLET=[0.459](cms), NINLET=[1],
4268 MajNHYD=["B3-MJ"]
4269 MinNHYD=["B3-MN"]
4270 TMJSTO=[227](cu-m)
4271 *%-----|
4272 ADD HYD NHYDsum=["MH333"], NHYDs to add=["B3-MN"+"315-333"]
4273 *%-----|
4274 SAVE HYD NHYD=["MH333"], # OF PCYCLES=[-1], ICASEsh=[1]
4275 HYD_COMMENT=["Total Flows at MH333"]
4276 *%-----|
4277 ROUTE PIPE PTYPE=[1]circ, NHYDout=["333-335"], RNUMBER=[1.0], PDIAM=[1200](mm),
4278 PLNGTH=[251](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["MH333"], RDT=[1]
4279 *%-----|
4280 ROUTE PIPE PTYPE=[1]circ, NHYDout=["335-338"], RNUMBER=[1.0], PDIAM=[1200](mm),
4281 PLNGTH=[185](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["333-335"], RDT=[1]
4282 *%-----|
4283 ROUTE PIPE PTYPE=[1]circ, NHYDout=["338-340"], RNUMBER=[1.0], PDIAM=[1350](mm),
4284 PLNGTH=[233](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["335-338"], RDT=[1]
4285 *%-----|
4286 CONTINUOUS STANDHYD NHYD=["B4"], DT=[1]min, AREA=[7.6](ha),
4287 XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4288 SCS curve number CN=[75],
4289 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4290 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4291 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4292 LGI=[388](m), MNI=[0.013], SCI=[0](min),
4293 Continuous simulation parameters:
4294 IaREcper=[4](hrs), IaREcimp=[4](hrs),
4295 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4296 InterEventTime=[18](hrs), END=-1
4297 *%-----|
4298 COMPUTE DUALHYD NHYDin=["B4"], CINLET=[0.655](cms), NINLET=[1],
4299 MajNHYD=["B4-MJ"]
4300 MinNHYD=["B4-MN"]
4301 TMJSTO=[323](cu-m)
4302 *%-----|
4303 ADD HYD NHYDsum=["MH340"], NHYDs to add=["338-340"+"B4-MN"]
4304 *%-----|
4305 SAVE HYD NHYD=["MH340"], # OF PCYCLES=[-1], ICASEsh=[1]
4306 HYD_COMMENT=["Total Flows at MH340"]
4307 *%-----|
4308 ROUTE PIPE PTYPE=[1]circ, NHYDout=["340-104"], RNUMBER=[1.0], PDIAM=[1650](mm),
4309 PLNGTH=[240](m), PROUGH=[0.013], PSLOPE=[0.0015](m/m),
NHYDin=["MH340"], RDT=[1]
4310 *%-----|
4311 ADD HYD NHYDsum=["MH104T"], NHYDs to add=["340-104"+"MH104"]
4312 *%-----|
4313 ROUTE PIPE PTYPE=[2]rect, NHYDout=["104-105"], RNUMBER=[1.0],
4314 PWIDTH=[2400](mm) by PHEIGHT=[2100](mm),
PLNGTH=[380](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["MH104T"], RDT=[1]
4315 *%-----|
4316 CONTINUOUS STANDHYD NHYD=["B5"], DT=[1]min, AREA=[2.2](ha),
4317 XIMP=[0.57], TIMP=[0.57], DWF=[0](cms), LOSS=[2],
4318 SCS curve number CN=[75],
4319 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4320 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4321 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),

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4322             LGI=[187](m), MNI=[0.013], SCI=[0](min),
4323 Continuous simulation parameters:
4324 IaRECper=[4](hrs), IaRECimp=[4](hrs),
4325 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4326 InterEventTime=[18](hrs), END=-1
4327 *%-----|-----|
4328 COMPUTE DUALHYD NHYDin=["B5"], CINLET=[0.260](cms), NINLET=[1],
4329 MajNHYD=["B5-MJ"]
4330 MinNHYD=["B5-MN"]
4331 TMJSTO=[250](cu-m)
4332 *%-----|-----|
4333 CONTINUOUS STANDHYD NHYD=["A8"], DT=[1]min, AREA=[0.96](ha),
4334 XIMP=[0.71], TIMP=[0.71], DWF=[0](cms), LOSS=[2],
4335 SCS curve number CN=[75],
4336 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4337 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4338 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4339 LGI=[186](m), MNI=[0.013], SCI=[0](min),
4340 Continuous simulation parameters:
4341 IaRECper=[4](hrs), IaRECimp=[4](hrs),
4342 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4343 InterEventTime=[18](hrs), END=-1
4344 *%-----|-----|
4345 ADD HYD NHYDsum=["A8T"], NHYDs to add=["A6-MJ"+"A8"]
4346 *%-----|-----|
4347 COMPUTE DUALHYD NHYDin=["A8T"], CINLET=[0.238](cms), NINLET=[1],
4348 MajNHYD=["A8-MJ"]
4349 MinNHYD=["A8-MN"]
4350 TMJSTO=[40](cu-m)
4351 *%-----|-----|
4352 ADD HYD NHYDsum=["MH105"], NHYDs to
add=["104-105"+"B5-MN"+"A8-MN"+"TODD_MN3j"]
4353 *%-----|-----|
4354 SAVE HYD NHYD=["MH105"], # OF PCYCLES=[-1], ICASEsh=[1]
4355 HYD_COMMENT=["Total Flows at MH105"]
4356 *%-----|-----|
4357 DIVERT HYD NHYDin=["A8-MJ"] NIDout=[2]max five,
4358 outflow hydrographs (NHYDs)=["A8-MJ-JR" "A8-MJ-B6"]
4359 flow distribution table: (modify as necessary)
4360 Note: all flows are in (cms)
4361 QIDi + QIDii = QTOTAL
4362 [ 0 + 0 = 0 ]
4363 [ 50 + 50 = 100 ] end
4364 *%-----|-----|
4365 DIVERT HYD NHYDin=["MH105"] NIDout=[2]max five,
4366 outflow hydrographs (NHYDs)=["MH105-JR" "MH105-B6"]
4367 flow distribution table: (modify as necessary)
4368 Note: all flows are in (cms)
4369 QIDi + QIDii = QTOTAL
4370 [ 0 + 0 = 0 ]
4371 [ 0 + 3.0 = 3.0 ]
4372 [ 96.9+ 3.1 = 100 ] end
4373 *%-----|-----|
4374 CONTINUOUS STANDHYD NHYD=["B7"], DT=[1]min, AREA=[7.19](ha),
4375 XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4376 SCS curve number CN=[75],
4377 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4378 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4379 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4380 LGI=[211](m), MNI=[0.013], SCI=[0](min),
4381 Continuous simulation parameters:
4382 IaRECper=[4](hrs), IaRECimp=[4](hrs),
4383 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4384 InterEventTime=[18](hrs), END=-1

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4385 *%-----|-----|
4386 ADD HYD          NHYDsum=["B7-B4MJ"], NHYDs to add=["B4-MJ"+"B7"]
4387 *%-----|-----|
4388 COMPUTE DUALHYD  NHYDin=["B7-B4MJ"], CINLET=[0.629](cms), NINLET=[1],
4389                  MajNHYD=["B7R-MJ"]
4390                  MinNHYD=["B7R-MN"]
4391                  TMJSTO=[311](cu-m)
4392 *%-----|-----|
4393 ROUTE PIPE       PTYPE=[1]circ, NHYDout=["360-106A"], RNUMBER=[1.0], PDIAM=[1050](mm),
4394                  PLNGTH=[167](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
4395                  NHYDin=["B7R-MN"], RDT=[1]
4396 *%-----|-----|
4397 *       -JFSA 2021-01-19 change B6 to be developed as per geottawa website and apply the
4398 parameters of A7, the nearest sub-catchment to B6, LGI is calculated based on B6 area
4399 CONTINUOUS STANDHYD NHYD=["B6"], DT=[1]min, AREA=[3.29](ha),
4400                  XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4401                  SCS curve number CN=[75],
4402                  Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4403                  LGP=[40](m), MNP=[0.25], SCP=[0](min),
4404                  Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4405                  LGI=[148.099](m), MNI=[0.013], SCI=[0](min),
4406                  Continuous simulation parameters:
4407                  IaRECper=[4](hrs), IaRECimp=[4](hrs),
4408                  SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4409                  InterEventTime=[18](hrs), END=-1
4410 *%-----|-----|
4411 *       -JFSA 2021-01-25 add B1 DUALHYD as per Corrigan Report, IBI Group, 2008
4412 COMPUTE DUALHYD  NHYDin=["B6"], CINLET=[0.064](cms), NINLET=[1],
4413                  MajNHYD=["B6-MJ"]
4414                  MinNHYD=["B6-MN"]
4415                  TMJSTO=[5484](cu-m)
4416 *%-----|-----|
4417 *CONTINUOUS NASHYD NHYD=["B6"], DT=[1]min, AREA=[3.29](ha),
4418 *                  DWF=[0](cms), CN/C=[75], IA=[2.5](mm),
4419 *                  N=[3.0], TP=[0.36]hrs,
4420 *                  Continuous simulation parameters:
4421 *                  IaRECper=[4](hrs),
4422 *                  SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4423 *                  InterEventTime=[12](hrs)
4424 *                  Baseflow simulation parameters:
4425 *                  BaseFlowOption=[1],
4426 *                  InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4427 *                  VHydCond=[0.055](mm/hr), END=-1
4428 *%-----|-----|
4429 *%       -EX-LAND is external land. It is a part of JOCKVA sub-catchment as per Corrigan
4430 Report, IBI Group, 2008
4431 CONTINUOUS STANDHYD NHYD=["EX-LAND"], DT=[1]min, AREA=[32.5](ha),
4432                  XIMP=[0.50], TIMP=[0.50], DWF=[0](cms), LOSS=[2],
4433                  SCS curve number CN=[74],
4434                  Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4435                  LGP=[40](m), MNP=[0.25], SCP=[0](min),
4436                  Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4437                  LGI=[465.475](m), MNI=[0.013], SCI=[0](min),
4438                  Continuous simulation parameters:
4439                  IaRECper=[4](hrs), IaRECimp=[4](hrs),
4440                  SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4441                  InterEventTime=[18](hrs), END=-1
4442 *%-----|-----|
4443 COMPUTE DUALHYD  NHYDin=["EX-LAND"], CINLET=[2.275](cms), NINLET=[1],
4444                  MajNHYD=["EX-LAND-MJ"]
4445                  MinNHYD=["EX-LAND-MN"]
4446                  TMJSTO=[1365](cu-m)
4447 *%-----|-----|
4448 ADD HYD          NHYDsum=["B6-B7ExMJ"], NHYDs to
4449 add=["B7R-MJ"+"EX-LAND-MJ"+"B5-MJ"+"B6-MJ"+"B6-MN"+"A8-MJ-B6"]
4450 *%-----|-----|

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4447 COMPUTE DUALHYD NHYDin=["B6-B7ExMJ"], CINLET=[0.064](cms), NINLET=[1],
4448 MajNHYD=["B6R-MJ"]
4449 MinNHYD=["B6R-MN"]
4450 TMJSTO=[5484](cu-m)
4451 *%-----|-----|
4452 ROUTE PIPE PTYPE=[1]circ, NHYDout=["105-106A"], RNUMBER=[1.0], PDIAM=[1800](mm),
4453 PLNGTH=[208](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["MH105-B6"], RDT=[1]
4454 *%-----|-----|
4455 ADD HYD NHYDsum=["MH106A"], NHYDs to
add=["360-106A"+"105-106A"+"B6R-MN"+"B6R-MJ"]
4456 *%-----|-----|
4457 SAVE HYD NHYD=["MH106A"], # OF PCYCLES=[-1], ICASEsh=[1]
4458 HYD_COMMENT=["Total Flows at MH106A"]
4459 *%-----|-----|
4460 *% -JFSA 2021-01-12 THE MANHOLE MH106 is called MH117/106 in Corrigan Report, IBI
Group, July 2008
4461 *%
4462 ROUTE PIPE PTYPE=[1]circ, NHYDout=["106A-106"], RNUMBER=[1.0], PDIAM=[1800](mm),
4463 PLNGTH=[190](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["MH106A"], RDT=[1]
4464 *%-----|-----|
4465 CONTINUOUS STANDHYD NHYD=["A9"], DT=[1]min, AREA=[2.44](ha),
4466 XIMP=[0.71], TIMP=[0.71], DWF=[0](cms), LOSS=[2],
4467 SCS curve number CN=[75],
4468 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4469 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4470 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4471 LGI=[262](m), MNI=[0.013], SCI=[0](min),
4472 Continuous simulation parameters:
4473 IaRECper=[4](hrs), IaRECimp=[4](hrs),
4474 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4475 InterEventTime=[18](hrs), END=-1
4476 *%-----|-----|
4477 COMPUTE DUALHYD NHYDin=["A9"], CINLET=[0.547](cms), NINLET=[1],
4478 MajNHYD=["A9-MJ"]
4479 MinNHYD=["A9-MN"]
4480 TMJSTO=[0](cu-m)
4481 *%-----|-----|
4482 ADD HYD NHYDsum=["MH106"], NHYDs to add=["106A-106"+"A9-MN"]
4483 *%-----|-----|
4484 SAVE HYD NHYD=["MH106"], # OF PCYCLES=[-1], ICASEsh=[1]
4485 HYD_COMMENT=["Total Flows at MH106"]
4486 *%-----|-----|
4487 *% -JFSA 2021-01-12 THE MANHOLE MH107 is called MH118/107 in Corrigan Report, IBI
Group, July 2008
4488 *%
4489 ROUTE PIPE PTYPE=[1]circ, NHYDout=["106-107"], RNUMBER=[1.0], PDIAM=[1800](mm),
4490 PLNGTH=[122.5](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["MH106"], RDT=[1]
4491 *%-----|-----|
4492 CONTINUOUS STANDHYD NHYD=["A10"], DT=[1]min, AREA=[4.14](ha),
4493 XIMP=[0.35], TIMP=[0.47], DWF=[0](cms), LOSS=[2],
4494 SCS curve number CN=[75],
4495 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4496 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4497 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4498 LGI=[183](m), MNI=[0.013], SCI=[0](min),
4499 Continuous simulation parameters:
4500 IaRECper=[4](hrs), IaRECimp=[4](hrs),
4501 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4502 InterEventTime=[18](hrs), END=-1
4503 *%-----|-----|
4504 COMPUTE DUALHYD NHYDin=["A10"], CINLET=[0.310](cms), NINLET=[1],
4505 MajNHYD=["A10-MJ"]
4506 MinNHYD=["A10-MN"]

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4507          TMJSTO=[228](cu-m)
4508  *%-----|-----
4509  CONTINUOUS STANDHYD NHYD=["A11"], DT=[1]min, AREA=[10.61](ha),
4510          XIMP=[0.53], TIMP=[0.62], DWF=[0](cms), LOSS=[2],
4511          SCS curve number CN=[75],
4512          Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4513          LGP=[40](m), MNP=[0.25], SCP=[0](min),
4514          Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4515          LGI=[379](m), MNI=[0.013], SCI=[0](min),
4516          Continuous simulation parameters:
4517          IaREcper=[4](hrs), IaREcimp=[4](hrs),
4518          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4519          InterEventTime=[18](hrs), END=-1
4520  *%-----|-----
4521  COMPUTE DUALHYD     NHYDin=["A11"], CINLET=[0.993](cms), NINLET=[1],
4522          MajNHYD=["A11-MJ"]
4523          MinNHYD=["A11-MN"]
4524          TMJSTO=[556](cu-m)
4525  *%-----|-----
4526  ADD HYD             NHYDsum=["MH107"], NHYDs to add=["106-107"+"A10-MN"+"A11-MN"]
4527  *%-----|-----
4528  SAVE HYD           NHYD=["MH107"], # OF PCYCLES=[-1], ICASEsh=[1]
4529          HYD_COMMENT=["Total Flows at MH107"]
4530  *%-----|-----
4531  ROUTE PIPE         PTYPE=[1]circ, NHYDout=["107-119"], RNUMBER=[1.0], PDIAM=[1800](mm),
4532          PLNGTH=[114](m), PROUGH=[0.013], PSLOPE=[0.0012](m/m),
          NHYDin=["MH107"], RDT=[1]
4533  *%-----|-----
4534  *% -JFSA 2021-01-12 THE MANHOLE MH108 is called MH120/108 in Corrigan Report, IBI
Group, July 2008
4535  *%
4536  ROUTE PIPE         PTYPE=[1]circ, NHYDout=["119-108"], RNUMBER=[1.0], PDIAM=[1800](mm),
4537          PLNGTH=[65.8](m), PROUGH=[0.013], PSLOPE=[0.0012](m/m),
          NHYDin=["107-119"], RDT=[1]
4538  *%-----|-----
4539  CONTINUOUS STANDHYD NHYD=["A12"], DT=[1]min, AREA=[12.29](ha),
4540          XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4541          SCS curve number CN=[75],
4542          Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4543          LGP=[40](m), MNP=[0.25], SCP=[0](min),
4544          Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4545          LGI=[183](m), MNI=[0.013], SCI=[0](min),
4546          Continuous simulation parameters:
4547          IaREcper=[4](hrs), IaREcimp=[4](hrs),
4548          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4549          InterEventTime=[18](hrs), END=-1
4550  *%-----|-----
4551  COMPUTE DUALHYD     NHYDin=["A12"], CINLET=[1.029](cms), NINLET=[1],
4552          MajNHYD=["A12-MJ"]
4553          MinNHYD=["A12-MN"]
4554          TMJSTO=[672](cu-m)
4555  *%-----|-----
4556  CONTINUOUS STANDHYD NHYD=["A13"], DT=[1]min, AREA=[2.59](ha),
4557          XIMP=[0.71], TIMP=[0.71], DWF=[0](cms), LOSS=[2],
4558          SCS curve number CN=[75],
4559          Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4560          LGP=[40](m), MNP=[0.25], SCP=[0](min),
4561          Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4562          LGI=[379](m), MNI=[0.013], SCI=[0](min),
4563          Continuous simulation parameters:
4564          IaREcper=[4](hrs), IaREcimp=[4](hrs),
4565          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4566          InterEventTime=[18](hrs), END=-1
4567  *%-----|-----
4568  COMPUTE DUALHYD     NHYDin=["A13"], CINLET=[0.571](cms), NINLET=[1],
4569          MajNHYD=["A13-MJ"]

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4570 MinNHYD=["A13-MN"]
4571 TMJSTO=[0](cu-m)
4572 *%-----|-----
4573 * -JFSA 2021-01-22 add the Corrigan pond area ("Pond-Block")
4574 CONTINUOUS STANDHYD NHYD=["Pond-Block"], DT=[1]min, AREA=[2.94](ha),
4575 XIMP=[0.415], TIMP=[0.415], DWF=[0](cms), LOSS=[2],
4576 SCS curve number CN=[75],
4577 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4578 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4579 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4580 LGI=[183](m), MNI=[0.013], SCI=[0](min),
4581 Continuous simulation parameters:
4582 IaRECPper=[4](hrs), IaRECImp=[4](hrs),
4583 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4584 InterEventTime=[18](hrs), END=-1
4585 *%-----|-----
4586 ADD HYD NHYDsum=["MH108"], NHYDs to add=["119-108"+"A13-MN"+"A12-MN"]
4587 *%-----|-----
4588 SAVE HYD NHYD=["MH108"], # OF PCYCLES=[-1], ICASEsh=[1]
4589 HYD_COMMENT=["Total Flows at MH108"]
4590 *%-----|-----
4591 ROUTE PIPE PTYPE=[1]circ, NHYDout=["108-116"], RNUMBER=[1.0], PDIAM=[1800](mm),
4592 PLNGTH=[76.6](m), PROUGH=[0.013], PSLOPE=[0.0013](m/m),
4593 NHYDin=["MH108"], RDT=[1]
4594 *%-----|-----
4595 ROUTE PIPE PTYPE=[1]circ, NHYDout=["116-corrig"], RNUMBER=[1.0],
4596 PDIAM=[1800](mm),
4597 PLNGTH=[79.5](m), PROUGH=[0.013], PSLOPE=[0.0013](m/m),
4598 NHYDin=["108-116"], RDT=[1]
4599 *%-----|-----
4600 ADD HYD NHYDsum=["Corrigan"], NHYDs to add=["116-corrig"+"Pond-Block"]
4601 *%-----|-----
4602 SAVE HYD NHYD=["Corrigan"], # OF PCYCLES=[-1], ICASEsh=[1]
4603 HYD_COMMENT=["Total Flows at Corrigan Pond"]
4604 *%-----|-----
4605 ROUTE RESERVOIR NHYDout=["Co-P"], NHYDin=["Corrigan"],
4606 RDT=[1](min),
4607 TABLE of ( OUTFLOW-STORAGE ) values
4608 (cms) - (ha-m)
4609 [ 0.0 , 0.0 ]
4610 [ 0.015 , 0.04118 ]
4611 [ 0.030 , 0.08297 ]
4612 [ 0.045 , 0.12537 ]
4613 [ 0.060 , 0.16837 ]
4614 [ 0.075 , 0.21199 ]
4615 [ 0.090 , 0.27545 ]
4616 [ 0.105 , 0.34650 ]
4617 [ 0.120 , 0.42049 ]
4618 [ 0.135 , 0.50188 ]
4619 [ 0.186 , 0.60307 ]
4620 [ 2.110 , 0.79083 ]
4621 [ 5.874 , 1.00271 ]
4622 [ 11.395 , 1.29643 ]
4623 [ 18.770 , 1.62054 ]
4624 [ 28.143 , 1.97516 ]
4625 [ -1 , -1 ] (max twenty pts)
4626 NHYDovf=["Co-P-OVF"]
4627 *%-----|-----
4628 ADD HYD NHYDsum=["corrig"], NHYDs to
4629 add=["Co-P-OVF"+"Co-P"+"N_TO"+"MH105-JR"+"A8-MJ-JR"+"A9-MJ"+"A10-MJ"+"A11-MJ"+"A12-MJ"+"A
4630 13-MJ"]
4631 *%-----|-----
4632 SAVE HYD NHYD=["corrig"], # OF PCYCLES=[-1], ICASEsh=[1]
4633 HYD_COMMENT=["Total Flows at Corrigan Pond"]
4634 *%-----|-----
4635 *#*****

```



```

4631 *#   Corrigan Pond 1
4632 *#   - Rating curve obtained from Barrhaven South MSS modeling
4633 *#   - Tributary Drainage Area to MSS Pond 1 = 145 ha
4634 *#*****
4635 *ROUTE RESERVOIR      NHYDout=["MS_P1"],  NHYDin=["CORRIG"],
4636 *                      RDT=[1](min),
4637 *                      TABLE of ( OUTFLOW-STORAGE ) values
4638 *                      (cms) - (ha-m)
4639 *                      [ 0.0 , 0.0 ]
4640 *                      [ 0.06 , 0.58]
4641 *                      [ -1 , -1 ] (max twenty pts)
4642 *                      NHYDovf=["P1-OVF"]
4643 *%-----|-----
4644 *ADD HYD              NHYDsum=["SN_CO"], NHYDs to add=["N_TO"+"P1-OVF"+"MS_P1"]
4645 *%-----|-----
4646 *SAVE HYD            NHYD=["SN_CO"], # OF PCYCLES=[-1], ICASEsh=[1]
4647 *                      HYD_COMMENT=["Total Flows at Corrigan Drain"]
4648 *%-----|-----
4649 *#
4650 *# Hydrograph from Corrigan Drain routed to Jockvale Road
4651 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
4652 *#
4653 ROUTE CHANNEL      NHYDout=["N_MI"] ,NHYDin=["corrig"] ,
4654 *                      RDT=[1](min),
4655 *                      CHLGTH=[580](m),  CHSLOPE=[0.4448](%),
4656 *                      FPSLOPE=[0.4448](%),
4657 *                      SECNUM=[1.0],      NSEG=[3]
4658 *                      ( SEGRROUGH, SEGDIST (m))=
4659 *                      [0.075,-17.72
4660 *                      -0.045,17.72
4661 *                      0.075,80.62] NSEG times
4662 *                      ( DISTANCE (m), ELEVATION (m))=
4663 *                      [-83.32, 90.00]
4664 *                      [-81.36, 89.50]
4665 *                      [-79.12, 89.00]
4666 *                      [-76.13, 88.50]
4667 *                      [-20.46, 88.00]
4668 *                      [-19.36, 87.50]
4669 *                      [-18.51, 87.00]
4670 *                      [-17.72, 86.50]
4671 *                      [-11.95, 85.24]
4672 *                      [-0.11, 85.12]
4673 *                      [11.49, 85.20]
4674 *                      [17.72, 86.50]
4675 *                      [19.74, 87.00]
4676 *                      [21.22, 87.50]
4677 *                      [22.68, 88.00]
4678 *                      [24.28, 88.50]
4679 *                      [26.79, 89.00]
4680 *                      [71.98, 90.00]
4681 *                      [80.62, 90.50]
4682 *%-----|-----
4683 *#*****
4684 *#   Catchment MILLS
4685 *#   - To SWM Facility north of the Jock
4686 *#   - Primarily residential development
4687 *#*****
4688 CONTINUOUS STANDHYD NHYD=["MILLS"], DT=[1]min, AREA=[175.99](ha),
4689 *                      XIMP=[0.38], TIMP=[0.38], DWF=[0](cms), LOSS=[2],
4690 *                      SCS curve number CN=[74],
4691 *                      Pervious surfaces: IAPER=[4.67](mm), SLPP=[1](%),
4692 *                      LGP=[40](m), MNP=[0.25], SCP=[0](min),
4693 *                      Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4694 *                      LGI=[1118.123](m), MNI=[0.013], SCI=[0](min),
4695 *                      Continuous simulation parameters:
4696 *                      IaREcper=[4](hrs), IaREcimp=[4](hrs),

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4697          SMIN=[-1](mm),   SMAX=[-1](mm), SK=[0.010]/(mm),
4698          InterEventTime=[18](hrs),   END=-1
4699  *%-----|-----|
4700  *#*****|
4701  *#   Chapman Mills SWM Pond
4702  *#   - Rating curve obtained from CCL hydraulic modeling
4703  *#*****|
4704  ROUTE RESERVOIR   NHYDout=["MILL_P"],   NHYDin=["MILLS"],
4705                    RDT=[1](min),
4706                    TABLE of ( OUTFLOW-STORAGE ) values
4707                    (cms) - (ha-m)
4708                    [ 0.0 , 0.0 ]
4709                    [ 0.01 , 0.01]
4710                    [ 0.05 , 0.06]
4711                    [ 0.09 , 0.11]
4712                    [ 0.13 , 0.15]
4713                    [ 0.18 , 0.19]
4714                    [ 0.28 , 0.28]
4715                    [ 0.37 , 0.34]
4716                    [ 0.45 , 0.40]
4717                    [ 0.51 , 0.44]
4718                    [ 0.56 , 0.47]
4719                    [ 0.64 , 0.52]
4720                    [ 0.76 , 0.59]
4721                    [ 0.86 , 0.65]
4722                    [ 1.09 , 0.78]
4723                    [ 1.44 , 0.96]
4724                    [ 3.18 , 1.84]
4725                    [ 4.05 , 2.31]
4726                    [ -1 , -1 ] (max twenty pts)
4727                    NHYDovf=["MIL-OV"]
4728  *%-----|-----|
4729  ADD HYD          NHYDsum=["SN_MI"], NHYDs to add=["N_MI"+"MIL-OV"+"MILL_P"]
4730  *%-----|-----|
4731  SAVE HYD       NHYD=["SN_MI"],   # OF PCYCLES=[-1], ICASEsh=[1]
4732                    HYD_COMMENT=["Total Flows at Jockvale Road"]
4733  *%-----|-----|
4734  *#
4735  *# Hydrograph from Jockvale Road routed to Heart's Desire
4736  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 689
4737  *#
4738  ROUTE CHANNEL   NHYDout=["N_DE"] ,NHYDin=["SN_MI"] ,
4739                    RDT=[1](min),
4740                    CHLGTH=[1962](m),   CHSLOPE=[0.2227](%),
4741                    FPSLOPE=[0.2227](%),
4742                    SECNUM=[1.0],   NSEG=[3]
4743                    ( SEGROUGH, SEGDIST (m))=
4744                    [0.075,-17.56
4745                    -0.045,18.27
4746                    0.075,32.51] NSEG times
4747                    ( DISTANCE (m), ELEVATION (m))=
4748                    [-54.07, 85.00]
4749                    [-39.43, 84.50]
4750                    [-28.30, 84.00]
4751                    [-24.12, 83.50]
4752                    [-22.30, 83.00]
4753                    [-20.55, 82.50]
4754                    [-17.56, 82.00]
4755                    [-12.63, 81.22]
4756                    [-0.11, 80.75]
4757                    [11.55, 81.22]
4758                    [18.27, 82.00]
4759                    [19.82, 82.50]
4760                    [22.48, 83.00]
4761                    [27.90, 83.50]
4762                    [29.31, 84.00]

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4763             [30.81, 84.50]
4764             [32.51, 85.00]
4765 *%-----|-----|
4766 *#*****|
4767 *#   Catchment DESIRE
4768 *#   - To Jock River (north of the Jock)
4769 *#   - Rural-estate subdivision (Heart's Desire Community)
4770 *#*****|
4771 CONTINUOUS STANDHYD NHYD=["DESIRE"], DT=[1]min, AREA=[23.78](ha),
4772 XIMP=[0.25], TIMP=[0.25], DWF=[0](cms), LOSS=[2],
4773 SCS curve number CN=[77],
4774 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4775 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4776 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4777 LGI=[400](m), MNI=[0.013], SCI=[0](min),
4778 Continuous simulation parameters:
4779 IaRECper=[4](hrs), IaRECimp=[4](hrs),
4780 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4781 InterEventTime=[18](hrs), END=-1
4782 *%-----|-----|
4783 *#*****|
4784 *#   Catchment JOCKVA
4785 *#   - To Jockvale SWM Facility
4786 *#   - Residential development & golf course
4787 *#   - JFSA 2021-01-11 update JOCKVA after updating CORRIG as per IBI GROUP, July 2008.
4788 *#   JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two
4789 *#   areas JOCKVA and EX-LAND 32.5 ha as per IBI GROUP, July 2008.
4790 *#*****|
4791 CONTINUOUS STANDHYD NHYD=["JOCKVA"], DT=[1]min, AREA=[225.13](ha),
4792 XIMP=[0.50], TIMP=[0.50], DWF=[0](cms), LOSS=[2],
4793 SCS curve number CN=[74],
4794 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4795 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4796 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4797 LGI=[1310.55](m), MNI=[0.013], SCI=[0](min),
4798 Continuous simulation parameters:
4799 IaRECper=[4](hrs), IaRECimp=[4](hrs),
4800 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4801 InterEventTime=[18](hrs), END=-1
4802 *%-----|-----|
4803 ADD HYD NHYDsum=["JOCKVA-TO"], NHYDs to
4804 add=["EX-LAND-MN"+"JOCKVA"+"B2-MJ"+"B3-MJ"]
4805 *%-----|-----|
4806 SAVE HYD NHYD=["JOCKVA-TO"], # OF PCYCLES=[-1], ICASEsh=[1]
4807 HYD_COMMENT=["Total Flows at KB first pond"]
4808 *%-----|-----|
4809 *#*****|
4810 *#   Jockvale SWM Facility
4811 *#   - Rating curve obtained from Jockvale Servicing Study (CCL 1999)
4812 *#*****|
4813 ROUTE RESERVOIR NHYDout=["JOCK_P"], NHYDin=["JOCKVA-TO"],
4814 RDT=[1](min),
4815 TABLE of ( OUTFLOW-STORAGE ) values
4816 (cms) - (ha-m)
4817 [ 0.0 , 0.0 ]
4818 [ 0.27 , 0.03 ]
4819 [ 0.28 , 0.55 ]
4820 [ 0.29 , 1.14 ]
4821 [ 0.30 , 1.80 ]
4822 [ 0.31 , 2.32 ]
4823 [ 1.12 , 2.87 ]
4824 [ 2.92 , 3.45 ]
4825 [ 4.64 , 4.07 ]
4826 [ 6.69 , 4.72 ]
4827 [ 9.02 , 5.39 ]
4828 [ 11.62 , 6.10 ]

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4827             [ 14.42 , 6.85]
4828             [ 17.45 , 7.62]
4829             [ 20.69 , 8.44]
4830             [ 24.08 , 9.28]
4831             [ 27.68 , 10.17]
4832             [ -1 , -1 ] (max twenty pts)
4833             NHYDovf=["JO-OVF"]
4834 *%-----|-----|
4835 ADD HYD      NHYDsum=["SN_DE"], NHYDs to add=["N_DE"+"DESIRE"+"JO-OVF"+"JOCK_P"]
4836 *%-----|-----|
4837 SAVE HYD     NHYD=["SN_DE"], # OF PCYCLES=[-1], ICASEsh=[1]
4838             HYD_COMMENT=["Total Flows at Heart's Desire"]
4839 *%-----|-----|
4840 *#
4841 *# Hydrograph from Heart's Desire routed to Rideau River
4842 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 0
4843 *#
4844 ROUTE CHANNEL NHYDout=["N1"] ,NHYDin=["SN_DE"] ,
4845             RDT=[1](min),
4846             CHLGTH=[563](m), CHSLOPE=[0.9668](%),
4847             FPSLOPE=[0.9668](%),
4848             SECNUM=[1.0], NSEG=[3]
4849             ( SEGROUGH, SEGDIST (m))=
4850             [0.075,-30.20
4851             -0.045,30.20
4852             0.075,48.48] NSEG times
4853             ( DISTANCE (m), ELEVATION (m))=
4854             [-98.46, 81.50]
4855             [-92.24, 81.00]
4856             [-86.88, 80.50]
4857             [-81.54, 80.00]
4858             [-74.36, 79.50]
4859             [-63.54, 79.00]
4860             [-39.23, 78.50]
4861             [-34.51, 78.00]
4862             [-33.01, 77.50]
4863             [-30.20, 77.00]
4864             [-13.42, 76.18]
4865             [-1.14, 76.09]
4866             [17.06, 76.18]
4867             [30.20, 77.00]
4868             [32.95, 77.50]
4869             [34.06, 78.00]
4870             [35.11, 78.50]
4871             [36.32, 79.00]
4872             [37.74, 79.50]
4873             [48.48, 81.50]
4874 *%-----|-----|
4875 *#*****|*****|
4876 *# Catchment S-2
4877 *# - To Jock River (north and south)
4878 *# - Undeveloped floodplain and river
4879 *#*****|*****|
4880 CONTINUOUS NASHYD NHYD=["S-2"], DT=[1]min, AREA=[102.94](ha),
4881             DWF=[0](cms), CN/C=[72], IA=[4.67](mm),
4882             N=[3], TP=[0.40]hrs,
4883             Continuous simulation parameters:
4884             IaRECper=[4](hrs),
4885             SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4886             InterEventTime=[12](hrs)
4887             Baseflow simulation parameters:
4888             BaseFlowOption=[1] ,
4889             InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4890             VHydCond=[0.055](mm/hr), END=-1
4891 *%-----|-----|
4892 ADD HYD      NHYDsum=["SN_N1"], NHYDs to add=["N1"+"S-2"]

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4893  *%-----|-----|
4894  SAVE HYD          NHYD=["SN_N1"], # OF PCYCLES=[-1], ICASEsh=[1]
4895                   HYD_COMMENT=["Total Flows at Rideau River"]
4896  *%-----|-----|
4897  *#####
4898  *% 5 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4899  START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[5]
4900  *%               ["C24SC005.stm"] <--storm filename, one per line for NSTORM time
4901  *%-----|-----|
4902  *% 10 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4903  START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[10]
4904  *%               ["C24SC010.stm"] <--storm filename, one per line for NSTORM time
4905  *%-----|-----|
4906  *% 25 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4907  START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[25]
4908  *%               ["C24SC025.stm"] <--storm filename, one per line for NSTORM time
4909  *%-----|-----|
4910  *% 50 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4911  START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[50]
4912  *%               ["C24SC050.stm"] <--storm filename, one per line for NSTORM time
4913  *%-----|-----|
4914  *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4915  *START           TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4916  *%               ["100YC3H.STM"] <--storm filename, one per line for NSTORM time
4917  *%-----|-----|
4918  *% 100 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4919  START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4920  *%               ["C24SC100.stm"] <--storm filename, one per line for NSTORM time
4921  *%-----|-----|
4922  *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4923  *START           TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4924  *%               ["C24SC100.stm"] <--storm filename, one per line for NSTORM time
4925  *START           TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[101]
4926  *%               ["A24SC100.stm"] <--storm filename, one per line for NSTORM time
4927  *START           TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[102]
4928  *%               ["A24SC100_60.stm"] <--storm filename, one per line for NSTORM time
4929  FINISH
4930

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00001 .....
00002 .....
00003 SSSS W W M M H H Y Y V V M M OOO 222 000 11 5555 .....
00004 S W W M M H H T T M M M O O 2 0 0 11 5 .....
00005 SSSS W W M M M H H H H H Y Y M M M O O 2 0 0 11 5 Ver 5.800
00006 S W W M M H H Y Y M M O O 222 0 0 11 555 PRE 2015
00007 SSSS W W M M H H Y Y M M O O 2 0 0 11 5 .....
00008 .....
00009 Stormwater Management Hydrologic Model 222 0 0 11 5 .....
00010 .....
00011 .....
00012 ***** SWHYMO Ver 5.800 *****
00013 ***** A single event and continuous hydrologic simulation model *****
00014 ***** based on the principles of HMO and its successors *****
00015 ***** OTTHMO=83 and OTTHMO=89 *****
00016 *****
00017 ***** Distributed by: J.F. Sabourin and Associates Inc. *****
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00021 ***** E-Mail: swhymo@jfsa.com *****
00022 *****
00023 *****
00024 ***** Licensed user: JFSaInc *****
00025 ***** Ottawa SERIAL#:2549237 *****
00026 *****
00027 *****
00028 *****
00029 ***** PROGRAM ARRAY DIMENSIONS *****
00030 ***** Maximum value for flow numbers : 11 *****
00031 ***** Max. number of rainfall points: 105408 *****
00032 ***** Max. number of ID points : 105408 *****
00033 *****
00034 *****
00035 ***** SUMMARY OUTPUT *****
00036 *****
00037 ***** RUN DATE: 2021-03-04 TIME: 11:49:14 RUN COUNTER: 022982 *****
00038 *****
00039 ***** Input file: T:\PROJ\1474-16\Design\20210226-QuantityControlAnalysis\SWHYMO\SMR-Model\Updated\
00040 ***** 3\SMR_S-1-Fr-Mat.dat *****
00041 *****
00042 ***** Output file: T:\PROJ\1474-16\Design\20210226-QuantityControlAnalysis\SWHYMO\SMR-Model\Updated\
00043 ***** 3\SMR_S-1-Fr-Mat.out *****
00044 *****
00045 ***** Summary file: T:\PROJ\1474-16\Design\20210226-QuantityControlAnalysis\SWHYMO\SMR-Model\Updated\
00046 ***** 3\SMR_S-1-Fr-Mat.sum *****
00047 *****
00048 ***** 1 *****
00049 ***** 2 *****
00050 ***** 3 *****
00051 *****
00052 *****
00053 *****
00054 ***** SWHYMO Ver 5.800 ***** INPUT DATA FILE *****
00055 *****
00056 ***** Project Name: [Jock River] Project Number: [1474-16] *****
00057 ***** Date [04-03-2021] *****
00058 ***** Modeller [J.F.M.] *****
00059 ***** Company [JFSaInc.] *****
00060 ***** License # [2549237] *****
00061 *****
00062 ***** CALIBRATION OF SUMMER MODEL PARAMETERS *****
00063 ***** USING CONTINUOUS SIMULATIONS *****
00064 ***** Rainfall data from JFSA raingauge installed at site + other gauges by the City *****
00065 ***** Use data collected from May 1st to July 14, 2003 *****
00066 ***** 2020-11-30 change WMPDRO in COMPUTE CHANNEL WMPDRO = 0.1 instead of 0.0001 *****
00067 ***** 2020-12-01 correct pond curve values *****
00068 ***** 2020-12-01 change W_CLEAR_SLOPE to 0.55, SLPD=[0.5*(H)] (impervious slope), and LGT up to 70m *****
00069 ***** 2021-02-19 Change the slope for ROUTE CHANNEL STATION 2462 (HWYDout="R_MC") ,HWYDin("SM_TO") from 0.03 K (as per st *****
00070 ***** 2021-02-19 Change the slope for ROUTE CHANNEL STATION 5002 (HWYDout="R_MC") ,HWYDin("SM_MC") from 0.01 K (as per st *****
00071 *****
00072 ***** ** END OF RUN : 1 *****
00073 *****
00074 *****
00075 *****
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00188 ***** [InterEventTime= 12.00] *****
00189 *****
00190 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00191 ***** # of 1.3 *****
00192 ***** R0021C00013-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00193 ***** CONTINUOUS NASHVD 1.0 01:HW_CK 8376.00 11.072 No.Date 39:59 11.98 263 .000 *****
00194 ***** [Cm: 70.0; H: 3.00; Tp: 2.51] *****
00195 ***** [IAREC: 4.00; SMIN: 52.62; SMAX:350.79; SK: .010] *****
00196 ***** [InterEventTime= 12.00] *****
00197 *****
00198 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00199 ***** # of 1.68 *****
00200 ***** R0021C00014-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00201 ***** CONTINUOUS NASHVD 1.0 01:HW_S 1132.00 4.434 No.Date 39:59 11.98 293 .000 *****
00202 ***** [Cm: 70.0; H: 3.00; Tp: 2.51] *****
00203 ***** [IAREC: 4.00; SMIN: 43.07; SMAX:287.10; SK: .010] *****
00204 ***** [InterEventTime= 12.00] *****
00205 *****
00206 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00207 ***** # of 1.62 *****
00208 ***** R0021C00015-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00209 ***** CONTINUOUS NASHVD 1.0 01:HW_CK 4664.00 5.504 No.Date 39:59 10.98 241 .000 *****
00210 ***** [Cm: 62.0; H: 3.00; Tp: 1.32] *****
00211 ***** [IAREC: 4.00; SMIN: 61.90; SMAX:412.66; SK: .010] *****
00212 ***** [InterEventTime= 12.00] *****
00213 *****
00214 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00215 ***** # of 3.80 *****
00216 ***** R0021C00016-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00217 ***** CONTINUOUS NASHVD 1.0 01:HW_S 131.00 .805 No.Date 28:57 11.22 247 .000 *****
00218 ***** [Cm: 63.0; H: 3.00; Tp: .93] *****
00219 ***** [IAREC: 4.00; SMIN: 59.42; SMAX:396.11; SK: .010] *****
00220 ***** [InterEventTime= 12.00] *****
00221 *****
00222 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00223 ***** # of 1.65 *****
00224 ***** R0021C00017-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00225 ***** CONTINUOUS NASHVD 1.0 01:HW_S 889.00 4.242 No.Date 38:46 11.98 263 .000 *****
00226 ***** [Cm: 66.0; H: 3.00; Tp: 8.42] *****
00227 ***** [IAREC: 4.00; SMIN: 51.81; SMAX:350.79; SK: .010] *****
00228 ***** [InterEventTime= 12.00] *****
00229 *****
00230 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00231 ***** # of 1.82 *****
00232 ***** R0021C00018-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00233 ***** CONTINUOUS NASHVD 1.0 01:HW_7 3197.00 4.651 No.Date 36:31 9.85 217 .000 *****
00234 ***** [Cm: 62.0; H: 3.00; Tp: .93] *****
00235 ***** [IAREC: 4.00; SMIN: 76.32; SMAX:508.81; SK: .010] *****
00236 ***** [InterEventTime= 12.00] *****
00237 *****
00238 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00239 ***** # of 1.75 *****
00240 ***** R0021C00019-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00241 ***** CONTINUOUS NASHVD 1.0 01:HW_S 165.00 .413 No.Date 33:07 12.24 269 .000 *****
00242 ***** [Cm: 67.0; H: 3.00; Tp: 4.18] *****
00243 ***** [IAREC: 4.00; SMIN: 60.55; SMAX:336.97; SK: .010] *****
00244 ***** [InterEventTime= 12.00] *****
00245 *****
00246 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00247 ***** # of 1.67 *****
00248 ***** R0021C00020-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00249 ***** CONTINUOUS NASHVD 1.0 01:VLDR 1332.00 3.148 No.Date 35:23 13.94 306 .000 *****
00250 ***** [Cm: 72.0; H: 3.00; Tp: 5.93] *****
00251 ***** [IAREC: 4.00; SMIN: 39.75; SMAX:264.99; SK: .010] *****
00252 ***** [InterEventTime= 12.00] *****
00253 ***** R0021C00021-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00254 ***** CONTINUOUS NASHVD 1.0 01:HW_S 224.00 2.597 No.Date 28:45 15.91 350 .000 *****
00255 ***** [Cm: 77.0; H: 3.00; Tp: .78] *****
00256 ***** [IAREC: 4.00; SMIN: 31.31; SMAX:207.66; SK: .010] *****
00257 ***** [InterEventTime= 12.00] *****
00258 *****
00259 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00260 ***** # of 1.23 *****
00261 ***** R0021C00022-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00262 ***** CONTINUOUS NASHVD 1.0 01:FL_CK 4945.00 14.839 No.Date 33:25 14.57 320 .000 *****
00263 ***** [Cm: 74.0; H: 3.00; Tp: 4.63] *****
00264 ***** [IAREC: 4.00; SMIN: 36.67; SMAX:244.49; SK: .010] *****
00265 ***** [InterEventTime= 12.00] *****
00266 ***** R0021C00023-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00267 ***** CONTINUOUS NASHVD 1.0 01:HW_S 20.00 .309 No.Date 28:36 17.79 391 .000 *****
00268 ***** [Cm: 81.0; H: 3.00; Tp: .21] *****
00269 ***** [IAREC: 4.00; SMIN: 25.21; SMAX:168.09; SK: .010] *****
00270 ***** [InterEventTime= 12.00] *****
00271 *****
00272 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) *****
00273 ***** # of 1.61 *****
00274 ***** R0021C00024-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00275 ***** CONTINUOUS NASHVD 1.0 01:HW_S 141.00 3.090 No.Date 38:04 15.22 334 .000 *****
00276 ***** [Cm: 75.0; H: 3.00; Tp: 8.00] *****
00277 ***** [IAREC: 4.00; SMIN: 33.81; SMAX:225.43; SK: .010] *****
00278 ***** [InterEventTime= 12.00] *****
00279 ***** R0021C00025-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00280 ***** CONTINUOUS NASHVD 1.0 01:HW_4 585.00 4.325 No.Date 29:58 17.79 391 .000 *****
00281 ***** [Cm: 81.0; H: 3.00; Tp: 1.78] *****
00282 ***** [IAREC: 4.00; SMIN: 25.21; SMAX:168.09; SK: .010] *****
00283 ***** [InterEventTime= 12.00] *****
00284 ***** R0021C00026-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00285 ***** CONTINUOUS NASHVD 1.0 01:HW_CK 1021.00 5.747 No.Date 30:50 17.39 382 .000 *****
00286 ***** [Cm: 80.0; H: 3.00; Tp: .86] *****
00287 ***** [IAREC: 4.00; SMIN: 38.32; SMAX:175.50; SK: .010] *****
00288 ***** [InterEventTime= 12.00] *****
00289 ***** R0021C00027-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00290 ***** CONTINUOUS NASHVD 1.0 01:HW_2 177.00 2.052 No.Date 28:45 15.91 350 .000 *****
00291 ***** [Cm: 77.0; H: 3.00; Tp: .78] *****
00292 ***** [IAREC: 4.00; SMIN: 31.31; SMAX:207.66; SK: .010] *****
00293 ***** [InterEventTime= 12.00] *****
00294 ***** R0021C00028-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00295 ***** CONTINUOUS NASHVD 1.0 01:HW_CK 1122.00 5.337 No.Date 31:50 17.79 391 .000 *****
00296 ***** [Cm: 81.0; H: 3.00; Tp: 2.85] *****
00297 ***** [IAREC: 4.00; SMIN: 25.21; SMAX:168.09; SK: .010] *****
00298 ***** [InterEventTime= 12.00] *****
00299 ***** R0021C00029-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00300 ***** CONTINUOUS NASHVD 1.0 01:HW_LR 2737.00 11.528 No.Date 31:35 15.56 342 .000 *****
00301 ***** [Cm: 76.0; H: 3.00; Tp: .81] *****
00302 ***** [IAREC: 4.00; SMIN: 32.46; SMAX:216.39; SK: .010] *****
00303 ***** [InterEventTime= 12.00] *****
00304 *****
00305 ***** Routing hydrographs *****
00306 *****
00307 ***** Starting with the addition of Jock River Headwater and Subwatershed 13 *****
00308 *****
00309 ***** R0021C00030-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00310 ***** ADD HYD 3680.00 6.204 No.Date 37:06 11.47 n/a .000 *****
00311 ***** SUM = 1.0 02:SM_13 971.00 2.187 No.Date 32:37 10.75 n/a .000 *****
00312 ***** SUM = 1.0 01:SM_13 4651.00 7.871 No.Date 35:37 11.32 n/a .000 *****
00313 *****
00314 ***** Sum of hydrographs from Node 13 routed to Node 13A *****
00315 ***** [Approximated cross-section - see cross-section 258] *****
00316 ***** Use n=0.04 for summer conditions and n=0.025 for spring conditions *****
00317 *****
00318 ***** R0021C00031-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00319 ***** ROUTE CHANNEL -> 1.0 02:R_313 4651.00 7.871 No.Date 35:37 11.32 n/a .000 *****
00320 ***** [IAREC: 4.00; SMIN: 32.46; SMAX:216.39; SK: .010] *****
00321 ***** [I/S/N= 9074./ .022/.040] *****
00322 ***** [Wmax= 429;Dmax=2.557] *****
00323 *****
00324 ***** Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A *****
00325 *****
00326 ***** R0021C00032-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00327 ***** ADD HYD 4651.00 6.208 No.Date 39:59 11.32 n/a .000 *****
00328 ***** SUM = 1.0 02:R_GMW 3074.00 3.218 No.Date 39:59 9.43 n/a .000 *****
00329 ***** SUM = 1.0 01:SM13A 7725.00 9.475 No.Date 39:59 10.57 n/a .000 *****
00330 *****
00331 ***** Insertion of a reservoir to simulate the effects of the Goodwood Marsh *****
00332 *****
00333 ***** R0021C00033-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00334 ***** ROUTE CHANNEL -> 1.0 02:SM13A 7725.00 9.475 No.Date 39:59 10.57 n/a .000 *****
00335 ***** [Use: <= 1.0 01:RES_GM 7725.00 2.619 No.Date 55:07 10.57 n/a .000 *****
00336 ***** [MStoUse=3.5858-02 m] *****
00337 *****
00338 ***** R0021C00034-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00339 ***** SAVE HYD 7725.00 2.619 No.Date 55:07 10.57 n/a .000 *****
00340 ***** fname =H_RESGM *****
00341 ***** remark=Outflow from Res GM *****
00342 ***** Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12 *****
00343 ***** [Approximated cross-section - see cross-section 258] *****
00344 ***** Use n=0.04 for summer conditions and n=0.025 for spring conditions *****
00345 ***** R0021C00035-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00346 ***** ROUTE CHANNEL -> 1.0 02:SM12 7725.00 2.619 No.Date 55:07 10.57 n/a .000 *****
00347 ***** [IAREC: 4.00; SMIN: 32.46; SMAX:216.39; SK: .010] *****
00348 ***** [I/S/N= 9074./ .022/.040] *****
00349 ***** [Wmax= 501;Dmax=1.329] *****
00350 *****
00351 ***** Addition of Subwatershed Jock River at Ashton to Node 12 *****
00352 *****
00353 ***** R0021C00036-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00354 ***** ADD HYD 7725.00 2.609 No.Date 58:08 10.57 n/a .000 *****
00355 ***** SUM = 1.0 02:HM12 7725.00 2.609 No.Date 58:08 10.57 n/a .000 *****
00356 ***** SUM = 1.0 02:R_SM12 9506.00 5.904 No.Date 32:45 13.26 n/a .000 *****
00357 ***** [IAREC: 4.00; SMIN: 32.46; SMAX:216.39; SK: .010] *****
00358 ***** R0021C00037-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00359 ***** SAVE HYD 9506.00 7.458 No.Date 32:50 11.20 n/a .000 *****
00360 ***** fname =H_SM12 *****
00361 ***** remark=flow at S_SM12 near Ashton *****
00362 *****
00363 ***** Sum of hydrographs from Node 12 routed to Node 11 *****
00364 ***** [Approximated cross-section - see cross-section 258] *****
00365 ***** Use n=0.04 for summer conditions and n=0.025 for spring conditions *****
00366 ***** Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248 *****
00367 *****
00368 ***** R0021C00038-----Dtn-ID:HWYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms *****
00369 ***** ROUTE CHANNEL -> 1.0 02:R_SM11 9506.00 7.458 No.Date 32:50 11.20 n/a .000 *****
00370 ***** [IAREC: 4.00; SMIN: 32.46; SMAX:216.39; SK: .010] *****
00371 ***** [I/S/N= 972./ .014/.040] *****
00372 ***** [Wmax= 591;Dmax=2.108] *****
00373 *****
00374 ***** Addition of Subwatershed 11 and No Name Creek to Node 11 *****

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00375# #
00376# R002/C00039-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00377# ADD HYD + 1.0 02:01M1 9506.00 7.379_MDate 33:12 11.20 n/a .000
00378# ROUTE CHANNEL -> 1.0 02:01M1 500.00 2.720_MDate 29:22 11.98 n/a .000
00379# + 1.0 02:01M2 1917.00 4.042_MDate 34:34 11.98 n/a .000
00380# SUM= 1.0 02:01M1 11923.00 12.077_MDate 33:14 11.36 n/a .000
00381#
00382# Sum of hydrographs from Node 11 routed to Node 10
00383# Section 1
00384#
00385# R002/C00040-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00386# ROUTE CHANNEL -> 1.0 02:01M1 11923.00 12.077_MDate 33:14 11.36 n/a .000
00387# [RPT= 1.00] out<- 1.0 02:01M1 11923.00 8.276_MDate 39:46 11.36 n/a .000
00388# [L/S= 3982 / .057 / .040]
00389# [Vmax=.462;Dmax=.886]
00390#
00391# Addition of Subwatershed 10 to Node 10
00392#
00393# R002/C00041-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00394# ADD HYD + 1.0 02:01M1 11923.00 8.276_MDate 39:46 11.36 n/a .000
00395# + 1.0 02:01M2 5646.00 11.228_MDate 38:07 13.94 n/a .000
00396# SUM= 1.0 02:01M1 17569.00 19.451_MDate 38:31 12.19 n/a .000
00397# R002/C00042-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00398# SAVE HYD + 1.0 02:01M1 17569.00 19.451_MDate 38:31 12.19 n/a .000
00399# frame_H_SMI10
00400# remark:flow at S_M10: M10 + SW_10
00401# Addition of Kings Creek to S_M10
00402#
00403# R002/C00043-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00404# ADD HYD + 1.0 02:01M1 17569.00 19.451_MDate 38:31 12.19 n/a .000
00405# + 1.0 02:01M2 8376.00 11.072_MDate 39:59 11.98 n/a .000
00406# SUM= 1.0 02:01M1 25945.00 30.328_MDate 39:58 12.12 n/a .000
00407#
00408# Sum of hydrographs from Node 10 routed to Node 9
00409# Section 2
00410#
00411# R002/C00044-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00412# ROUTE CHANNEL -> 1.0 02:01M1 25945.00 30.328_MDate 39:58 12.12 n/a .000
00413# [RPT= 1.00] out<- 1.0 02:01M1 25945.00 29.579_MDate 39:59 12.12 n/a .000
00414# [L/S= 3982 / .075 / .040]
00415# [Vmax=.595;Dmax=1.208]
00416#
00417# Addition of Subwatershed 8 and Nichols Creek to Node 9
00418#
00419# R002/C00045-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00420# ADD HYD + 1.0 02:01M1 25945.00 29.579_MDate 39:59 12.12 n/a .000
00421# + 1.0 02:01M2 1132.00 4.404_MDate 39:59 12.12 n/a .000
00422# + 1.0 02:01M3 4464.00 5.504_MDate 39:59 10.98 n/a .000
00423# SUM= 1.0 02:01M1 31661.00 36.313_MDate 39:59 12.00 n/a .000
00424#
00425# Sum of hydrographs from Node 9 routed to Node 8
00426# Section 3
00427#
00428# R002/C00046-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00429# ROUTE CHANNEL -> 1.0 02:01M1 31661.00 36.313_MDate 39:59 12.00 n/a .000
00430# [RPT= 1.00] out<- 1.0 02:01M1 31661.00 34.713_MDate 39:59 12.00 n/a .000
00431# [L/S= 3982 / .087 / .040]
00432# [Vmax=.418;Dmax=1.281]
00433#
00434# Addition of Subwatershed 8 and Bobb's Drain to Node 8
00435#
00436# R002/C00047-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00437# ADD HYD + 1.0 02:01M1 31661.00 34.713_MDate 39:59 12.00 n/a .000
00438# + 1.0 02:01M2 3156.00 34.713_MDate 39:59 12.00 n/a .000
00439# + 1.0 02:01M3 3854.00 6.242_MDate 38:46 11.98 n/a .000
00440# SUM= 1.0 02:01M1 38546.00 40.474_MDate 39:59 12.00 n/a .000
00441#
00442# Sum of hydrographs from Node 8 routed to Node 7
00443# Section 4
00444#
00445# R002/C00048-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00446# ROUTE CHANNEL -> 1.0 02:01M1 38546.00 40.474_MDate 39:59 12.00 n/a .000
00447# [RPT= 1.00] out<- 1.0 02:01M1 38546.00 32.892_MDate 44:30 12.00 n/a .000
00448# [L/S= 3750 / .057 / .040]
00449# [Vmax=.208;Dmax=1.651]
00450#
00451# Addition of Subwatershed 7 to Node 7
00452#
00453# R002/C00049-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00454# ADD HYD + 1.0 02:01M1 38546.00 32.892_MDate 44:30 12.00 n/a .000
00455# + 1.0 02:01M2 3197.00 4.451_MDate 36:31 8.45 n/a .000
00456# SUM= 1.0 02:01M1 38743.00 35.071_MDate 43:33 11.82 n/a .000
00457# R002/C00050-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00458# SAVE HYD + 1.0 02:01M1 38743.00 35.071_MDate 43:33 11.82 n/a .000
00459# frame_H_SMI7
00460# remark:flow at S_M7: M7 + SW_7
00461# Insertion of a Reservoir to simulate the effects of the Richmond Fen.
00462# Storage area and volumes were estimated from available topo maps.
00463# Release rate from Fen was assumed to be controlled by the downstream
00464# river cross-section for which it is assumed that for up to
00465# 0.75 m of water, the main channel of the river provided the storage. Above
00466# this depth, the wetland starts to significantly store water.
00467#
00468# R002/C00051-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00469# ROUTE CHANNEL -> 1.0 02:01M1 38743.00 35.071_MDate 43:33 11.82 n/a .000
00470# out<- 1.0 02:01RES_RP 38743.00 23.265_MDate 55:09 11.82 n/a .000
00471# [Med:0.000;Vol:0.000]
00472# R002/C00052-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00473# SAVE HYD + 1.0 02:01RES_RP 38743.00 23.265_MDate 55:09 11.82 n/a .000
00474# frame_H_ResFen
00475# remark:outflow of Richmond Fen
00476#
00477# Sum of hydrographs from Node 7 routed to Node 6
00478# Section 5
00479#
00480# R002/C00053-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00481# ROUTE CHANNEL -> 1.0 02:01RES_RP 38743.00 23.265_MDate 55:09 11.82 n/a .000
00482# [RPT= 1.00] out<- 1.0 02:01RES_RP 38743.00 23.228_MDate 56:38 11.82 n/a .000
00483# [L/S= 3066 / .087 / .040]
00484# [Vmax=.432;Dmax=.808]
00485#
00486# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
00487#
00488# R002/C00054-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00489# ADD HYD + 1.0 02:01RES_RP 38743.00 23.228_MDate 56:38 11.82 n/a .000
00490# + 1.0 02:01M2 1455.00 4.412_MDate 36:31 8.45 n/a .000
00491# + 1.0 02:01M3 1332.00 3.148_MDate 35:23 13.94 n/a .000
00492# SUM= 1.0 02:01M1 40240.00 23.318_MDate 39:59 11.89 n/a .000
00493#
00494# Sum of hydrographs from Node 6 routed to Node 5
00495# Section 6
00496#
00497# R002/C00055-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00498# ROUTE CHANNEL -> 1.0 02:01M1 40240.00 23.318_MDate 39:59 11.89 n/a .000
00499# [RPT= 1.00] out<- 1.0 02:01M1 40240.00 23.285_MDate 56:09 11.89 n/a .000
00500# [L/S= 3066 / .057 / .040]
00501# [Vmax=.378;Dmax=.917]
00502#
00503# Addition of Subwatershed 5 and Flowing Creek to Node 5
00504#
00505# R002/C00056-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00506# ADD HYD + 1.0 02:01M1 40240.00 23.285_MDate 56:09 11.89 n/a .000
00507# + 1.0 02:01M2 224.94 2.587_MDate 45:45 15.21 n/a .000
00508# + 1.0 02:01M3 4949.00 14.839_MDate 33:25 14.57 n/a .000
00509# SUM= 1.0 02:01M1 45408.00 31.366_MDate 37:08 12.20 n/a .000
00510#
00511# Sum of hydrographs from Node 5 routed to Node 5A
00512# Section 7
00513#
00514# R002/C00057-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00515# ROUTE CHANNEL -> 1.0 02:01M1 45408.00 31.366_MDate 37:08 12.20 n/a .000
00516# [RPT= 1.00] out<- 1.0 02:01M1 45409.00 31.316_MDate 37:10 12.20 n/a .000
00517# [L/S= 556 / .097 / .040]
00518# [Vmax=.443;Dmax=.937]
00519#
00520# Addition of Subwatershed 5A and Subwatershed 5A2 to Node 5A
00521#
00522# R002/C00058-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00523# ADD HYD + 1.0 02:01M1 45409.00 31.316_MDate 37:10 12.20 n/a .000
00524# + 1.0 02:01M2 54.00 0.509_MDate 28:36 17.79 n/a .000
00525# + 1.0 02:01M3 1622.00 3.090_MDate 38:04 15.22 n/a .000
00526# SUM= 1.0 02:01M1 46841.00 36.216_MDate 37:28 12.30 n/a .000
00527#
00528# Sum of hydrographs from Node 5A routed to Node 4
00529# Section 8
00530#
00531# R002/C00059-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00532# ROUTE CHANNEL -> 1.0 02:01M1 46841.00 36.216_MDate 37:28 12.30 n/a .000
00533# [RPT= 1.00] out<- 1.0 02:01M1 46841.00 35.288_MDate 39:22 12.30 n/a .000
00534# [L/S= 4630 / .047 / .035]
00535# [Vmax=.695;Dmax=2.444]
00536#
00537# Addition of Subwatershed 4 and Leamy Creek to Node 4
00538#
00539# R002/C00060-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00540# ADD HYD + 1.0 02:01M1 46841.00 35.288_MDate 39:22 12.30 n/a .000
00541# + 1.0 02:01M2 585.00 4.325_MDate 29:58 17.79 n/a .000
00542# + 1.0 02:01M3 1022.00 5.747_MDate 30:50 17.39 n/a .000
00543# SUM= 1.0 02:01M1 48447.00 37.581_MDate 38:13 12.47 n/a .000
00544# R002/C00061-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00545# SAVE HYD + 1.0 02:01M1 48447.00 37.581_MDate 38:13 12.47 n/a .000
00546# frame_H_4A.0002
00547# remark:flow at S_4A
00548#
00549# Sum of hydrographs from Node 4 routed to Node 2
00550# Section 9
00551#
00552# R002/C00062-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00553# ROUTE CHANNEL -> 1.0 02:01M1 48447.00 37.581_MDate 38:13 12.47 n/a .000
00554# [RPT= 1.00] out<- 1.0 02:01M1 48447.00 37.455_MDate 38:19 12.47 n/a .000
00555# [L/S= 1467 / .067 / .040]
00556# [Vmax=.715;Dmax=2.485]
00557#
00558# Addition of Subwatershed 2 with Monahan Drain and Smith Drain to Node 2
00559#
00560# R002/C00063-----DtnIn-ID:HYD-----AREHA-QPEARCS-TPeakDate_hh:mm-----RvM-R.C-----DWPFMS
00561# ADD HYD + 1.0 02:01M1 48447.00 37.455_MDate 38:19 12.47 n/a .000

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01123 [IAREC 4.00] SMIN 31.15: SMAX=207.66: EK= .010]
01124 *****
01125 R002C00184-----DRAIN-DI-HYD-----AREHA-GPEARCS-TpeakDate_hhm-----RVM-R-C-----DWPFCS
01126 ADD HYD + 1.0 02:05-D1 21.67 18.78 MoDate 29:10 14.83 n/a .000
01127 [IAREC 4.00] SMIN 31.15: SMAX=207.66: EK= .010]
01128 *****
01129 R002C00185-----DRAIN-DI-HYD-----AREHA-GPEARCS-TpeakDate_hhm-----RVM-R-C-----DWPFCS
01130 SAVE HYD + 1.0 01:50-0 330.38 3.933 MoDate 29:12 28.36 n/a .000
01131 *****
01132 *****
01133 *****
01134 # Hydrograph from Node Foster SHM (Station 980) to Node at station 520
01135 # Channel X-Section obtained from RWCA Hydraulic Model - Station 980
01136 *****
01137 R002C00187-----DRAIN-DI-HYD-----AREHA-GPEARCS-TpeakDate_hhm-----RVM-R-C-----DWPFCS
01138 ROUTE CHANNEL -> 1.0 02:01-0 330.38 3.933 MoDate 29:12 28.36 n/a .000
01139 [IAREC 4.00] SMIN 31.15: SMAX=207.66: EK= .010]
01140 *****
01141 *****
01142 R002C00188-----DRAIN-DI-HYD-----AREHA-GPEARCS-TpeakDate_hhm-----RVM-R-C-----DWPFCS
01143 CONTINUOUS STANDBY 1.0 01:01-PO-0 5.11 .041 MoDate 29:12 14.83 326 .000
01144 [IAREC 4.00] SMIN 31.15: SMAX=207.66: EK= .010]
01145 *****
01146 *****
01147 R002C00189-----DRAIN-DI-HYD-----AREHA-GPEARCS-TpeakDate_hhm-----RVM-R-C-----DWPFCS
01148 ADD HYD + 1.0 02:01-0 330.38 3.933 MoDate 29:12 28.36 n/a .000
01149 *****
01150 *****
01151 R002C00190-----DRAIN-DI-HYD-----AREHA-GPEARCS-TpeakDate_hhm-----RVM-R-C-----DWPFCS
01152 SAVE HYD + 1.0 01:50-0 335.49 3.844 MoDate 29:12 28.15 n/a .000
01153 *****
01154 *****
01155 # Hydrograph from Node at Station 520 (Foster Drain) to Node at station 6016 (Jock River)
01156 # Channel X-Section obtained from RWCA Hydraulic Model - Station 520
01157 *****
01158 R002C00191-----DRAIN-DI-HYD-----AREHA-GPEARCS-TpeakDate_hhm-----RVM-R-C-----DWPFCS
01159 ROUTE CHANNEL -> 1.0 02:02-0 335.49 3.844 MoDate 29:12 28.15 n/a .000
01160 [IAREC 4.00] SMIN 31.15: SMAX=207.66: EK= .010]
01161 *****
01162 *****
01163 R002C00192-----DRAIN-DI-HYD-----AREHA-GPEARCS-TpeakDate_hhm-----RVM-R-C-----DWPFCS
01164 CONTINUOUS STANDBY 1.0 01:01-PO-0 14.96 .128 MoDate 29:05 14.83 326 .000
01165 [IAREC 4.00] SMIN 31.15: SMAX=207.66: EK= .010]
01166 *****
01167 *****
01168 R002C00193-----DRAIN-DI-HYD-----AREHA-GPEARCS-TpeakDate_hhm-----RVM-R-C-----DWPFCS
01169 CONTINUOUS STANDBY 1.0 01:01-0-08 5.27 .498 MoDate 28:00 32.20 707 .000
01170 [IAREC 4.00] SMIN 31.15: SMAX=207.66: EK= .010]
01171 *****
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01309 *****

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01871# # - 2020-11-30 Increase Imp. based on P598(04)-11
01872# # - 2020-11-30 update RUDS Tributary Drainage Area to = 146.015 ha based on P598(04)-11
01873# # - 2020-11-30 split TOOD Drainage Area to MAJOR, MINOR, POND and ALL
01874# # *****
01875# # - JFSA 2021-01-19 add TOOD_MN1 as part of Clarke's M_Clarke_M1 and remove it from Todd
01876# # *****
01877# # CONTINUOUS STANDBY 1.0 01:TOOD_MN2 2.10 1.79 No_date 28:00 28.91 635 0.000
01878# [XMP= 53:TMP= 57]
01879# [LOSS= 2 CN= 77.0]
01880# [Previous area IArea= 4.67:SLP=1.00:LDP= 40.0:MP= 250:SCP= 0]
01881# [Impervious area IArea= 1.57:SLP=1.00:LDP= 118.0:MI= 013:SCI= 0]
01882# [IARECimp= 4.00: IARECPE= 4.00]
01883# [SMIN= 31.15: SMAK=207.66: SK= 010]
01884# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
01885# CONTINUOUS STANDBY 1.0 01:TOOD_MN2 12 .011 No_date 28:00 28.91 635 0.000
01886# [XMP= 53:TMP= 57]
01887# [LOSS= 2 CN= 77.0]
01888# [Previous area IArea= 4.67:SLP=1.00:LDP= 40.0:MP= 250:SCP= 0]
01889# [Impervious area IArea= 1.57:SLP=1.00:LDP= 28.0:MI= 013:SCI= 0]
01890# [IARECimp= 4.00: IARECPE= 4.00]
01891# [SMIN= 31.15: SMAK=207.66: SK= 010]
01892# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
01893# CONTINUOUS STANDBY 1.0 01:TOOD_MN2 30.23 2.154 No_date 28:03 29.64 651 0.000
01894# [XMP= 52:TMP= 64]
01895# [LOSS= 2 CN= 77.0]
01896# [Previous area IArea= 4.67:SLP=1.00:LDP= 40.0:MP= 250:SCP= 0]
01897# [Impervious area IArea= 1.57:SLP=1.00:LDP= 449.0:MI= 013:SCI= 0]
01898# [IARECimp= 4.00: IARECPE= 4.00]
01899# [SMIN= 31.15: SMAK=207.66: SK= 010]
01900# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
01901# CONTINUOUS STANDBY 1.0 01:TOOD_ALL 112.91 6.533 No_date 28:06 28.70 631 0.000
01902# [XMP= 52:TMP= 64]
01903# [LOSS= 2 CN= 77.0]
01904# [Previous area IArea= 4.67:SLP=1.00:LDP= 40.0:MP= 250:SCP= 0]
01905# [Impervious area IArea= 1.57:SLP=1.00:LDP= 868.0:MI= 013:SCI= 0]
01906# [IARECimp= 4.00: IARECPE= 4.00]
01907# [SMIN= 31.15: SMAK=207.66: SK= 010]
01908# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
01909# CONTINUOUS STANDBY 1.0 01:TOOD_P 3.06 .295 No_date 28:00 31.76 698 0.000
01910# [XMP= 63:TMP= 63]
01911# [LOSS= 2 CN= 77.0]
01912# [Previous area IArea= 4.67:SLP=1.00:LDP= 40.0:MP= 250:SCP= 0]
01913# [Impervious area IArea= 1.57:SLP=1.00:LDP= 143.0:MI= 013:SCI= 0]
01914# [IARECimp= 4.00: IARECPE= 4.00]
01915# [SMIN= 31.15: SMAK=221.43: SK= 010]
01916# # 5-Year + 124 Capture
01917# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
01918# ROUTE RESERVOIR -> 1.0 02:TOOD_MN 30.23 2.154 No_date 28:03 29.64 n/a 0.000
01919# out -> 1.0 01:TOOD_MN 30.23 2.154 No_date 28:03 29.64 n/a 0.000
01920# overflow -> 0.00 0.00 No_date 0:00 .00 n/a 0.000
01921# [MxTotVol=68516-04 n3, TotVolVol=00000-00 n3, N-Ovrf= 0, TotDurOvf= 0 hrs]
01922# # 5-Year + 124 Capture
01923# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
01924# ROUTE RESERVOIR -> 1.0 01:TOOD_MN2 2.10 1.79 No_date 28:00 28.91 n/a 0.000
01925# out -> 1.0 01:TOOD_MN2 2.10 1.79 No_date 28:00 28.91 n/a 0.000
01926# overflow -> 1.0 03:TOOD_MN2 0.00 .000 No_date 0:00 .00 n/a 0.000
01927# [MxTotVol=67616-00 n3, TotVolVol=00000-00 n3, N-Ovrf= 0, TotDurOvf= 0 hrs]
01928# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
01929# ROUTE RESERVOIR -> 1.0 01:TOOD_MN 12 .010 No_date 28:00 28.91 n/a 0.000
01930# out -> 1.0 01:TOOD_MN 12 .010 No_date 28:00 28.91 n/a 0.000
01931# overflow -> 0.00 0.00 No_date 0:00 .00 n/a 0.000
01932# [MxTotVol=6666-04 n3, TotVolVol=00000-00 n3, N-Ovrf= 0, TotDurOvf= 0 hrs]
01933# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
01934# CONTINUOUS STANDBY 1.0 01:TOOD_P 25.50 1.427 No_date 28:04 25.60 563 0.000
01935# [XMP= 42:TMP= 52]
01936# [LOSS= 2 CN= 75.0]
01937# [Previous area IArea= 4.67:SLP=1.00:LDP= 40.0:MP= 250:SCP= 0]
01938# [Impervious area IArea= 1.57:SLP=1.00:LDP= 566.0:MI= 013:SCI= 0]
01939# [IARECimp= 4.00: IARECPE= 4.00]
01940# [SMIN= 33.81: SMAK=221.43: SK= 010]
01941# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
01942# COMPUTE DIALYD 1.0 01:AD 25.50 1.427 No_date 28:04 25.60 n/a 0.000
01943# Major System / 1.0 02:AD-MJ 25.50 1.427 No_date 28:04 25.60 n/a 0.000
01944# Minor System / 1.0 03:AD-MN 25.50 1.427 No_date 28:04 25.60 n/a 0.000
01945# [MjSysVol=00000-00, TotVolVol=00000-00, N-Ovrf= 0, TotDurOvf= 0 hrs]
01946# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
01947# ADD HYD + 1.0 02:TOOD_MN2 2.10 1.79 No_date 28:00 28.91 n/a 0.000
01948# + 1.0 02:TOOD_MN 12 .010 No_date 28:00 28.91 n/a 0.000
01949# + 1.0 02:TOOD_MJ 0.00 .000 No_date 0:00 .00 n/a 0.000
01950# + 1.0 02:TOOD_P 3.06 .295 No_date 28:00 31.76 n/a 0.000
01951# + 1.0 01:TOOD_ALL 112.91 6.533 No_date 28:06 28.70 n/a 0.000
01952# + 1.0 02:CLAR_MN 1.77 .141 No_date 28:00 27.78 n/a 0.000
01953# [SMIN= 33.81: SMAK=221.43: SK= 010]
01954# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
01955# SAVE HYD 1.0 01:AD 119.95 6.892 No_date 28:05 28.77 n/a 0.000
01956# remark TODD.0002
01957# remark Total Flows at Todd Drain
01958# *****
01959# # Todd Pond
01960# # Rating Curve obtained from Barhaven South MSB modeling
01961# # - stantec 2007, Tributary Drainage Area to MSB Pond = 193 ha
01962# # *****
01963# # CONTINUOUS STANDBY 1.0 01:TOOD_MN2 2.10 1.79 No_date 28:00 28.91 n/a 0.000
01964# ROUTE RESERVOIR -> 1.0 02:TOOD_P 119.95 6.892 No_date 28:05 28.77 n/a 0.000
01965# overflow -> 1.0 03:TOOD_P 119.95 6.892 No_date 28:05 28.77 n/a 0.000
01966# overflow -> 1.0 03:TOOD_P 0.00 .000 No_date 0:00 .00 n/a 0.000
01967# [MxTotVol=103316-00 n3, TotVolVol=00000-00 n3, N-Ovrf= 0, TotDurOvf= 0 hrs]
01968# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
01969# ADD HYD + 1.0 02:TOOD_P 54737.73 49.025 No_date 37:10 13.05 n/a 0.000
01970# + 1.0 02:TOOD_MN 119.95 6.892 No_date 28:00 28.91 n/a 0.000
01971# + 1.0 02:TOOD_P 0.00 .000 No_date 0:00 .00 n/a 0.000
01972# + 1.0 02:TOOD_MN2 2.10 1.79 No_date 28:00 28.91 n/a 0.000
01973# + 1.0 02:AD-MJ 0.00 .000 No_date 0:00 .00 n/a 0.000
01974# [SMIN= 33.81: SMAK=221.43: SK= 010]
01975# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
01976# CONTINUOUS STANDBY 1.0 01:AD 54837.69 48.869 No_date 38:25 13.08 n/a 0.000
01977# SAVE HYD 1.0 01:AD 54837.69 48.869 No_date 37:09 13.08 n/a 0.000
01978# remark USN_TOOD.0002
01979# *****
01980# # Hydrograph from Todd Drain routed to Corrigan Drain
01981# # Channel X-Section obtained from RUDS Hydraulic Model at Station 2462
01982# # 021-02-19 Change the slope from 0.033 % (as per Stantec Report 2007) to 0.05 % so the model will be more stable and g
01983# # *****
01984# # CONTINUOUS STANDBY 1.0 01:TOOD_P 54837.69 48.869 No_date 38:25 13.08 n/a 0.000
01985# [RDP= 1.00] out -> 1.0 01:TOOD_P 54837.69 48.869 No_date 38:25 13.08 n/a 0.000
01986# [L/S= 1.00] out -> 1.0 01:TOOD_P 54837.69 48.869 No_date 38:25 13.08 n/a 0.000
01987# [Vmax= 730:Dmax= 2.134]
01988# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
01989# SAVE HYD 54837.69 48.869 No_date 38:25 13.08 n/a 0.000
01990# *****
01991# # Continous Flows at Station 2462
01992# # *****
01993# # - To Corrigan Drain (south of the Jock)
01994# # - Primarily Developed (medium density)
01995# # - JFSA JAN 2021, add Corrigan subcatchments as per IRI, July 2008
01996# # *****
01997# # CONTINUOUS STANDBY 1.0 01:corr1 15.87 1.352 No_date 28:02 31.77 698 0.000
01998# [XMP= 63:TMP= 63]
01999# [LOSS= 2 CN= 77.0]
02000# [Previous area IArea= 4.67:SLP=1.00:LDP= 40.0:MP= 250:SCP= 0]
02001# [Impervious area IArea= 1.57:SLP=1.00:LDP= 325.0:MI= 013:SCI= 0]
02002# [IARECimp= 4.00: IARECPE= 4.00]
02003# [SMIN= 31.81: SMAK=221.43: SK= 010]
02004# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02005# COMPUTE DIALYD 1.0 01:corr1 15.87 1.352 No_date 28:02 31.77 n/a 0.000
02006# Major System / 1.0 03:corr1-MJ 0.00 .000 No_date 0:00 .00 n/a 0.000
02007# Minor System / 1.0 03:corr1-MN 15.87 1.352 No_date 28:02 31.77 n/a 0.000
02008# [MjSysVol=00000-00, TotVolVol=00000-00, N-Ovrf= 0, TotDurOvf= 0 hrs]
02009# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02010# CONTINUOUS STANDBY 1.0 01:corr2 12.47 .100 No_date 29:12 14.83 136 0.000
02011# [CN= 77.0] N= 3.001 Tpe= 1.10]
02012# [IAREC= 4.00: SMIN= 31.15: SMAK=207.66: SK= 010]
02013# [LOSS= 2 CN= 75.0]
02014# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02015# CONTINUOUS STANDBY 1.0 01:corr1 15.75 .992 No_date 28:02 25.60 563 0.000
02016# [XMP= 42:TMP= 52]
02017# [LOSS= 2 CN= 75.0]
02018# [Previous area IArea= 4.67:SLP=1.00:LDP= 40.0:MP= 250:SCP= 0]
02019# [Impervious area IArea= 1.57:SLP=1.00:LDP= 324.0:MI= 013:SCI= 0]
02020# [IARECimp= 4.00: IARECPE= 4.00]
02021# [SMIN= 33.81: SMAK=221.43: SK= 010]
02022# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02023# COMPUTE DIALYD 1.0 01:corr1 15.75 .992 No_date 28:02 25.60 n/a 0.000
02024# Major System / 1.0 02:corr1-MJ 15.75 .992 No_date 28:02 25.60 n/a 0.000
02025# Minor System / 1.0 03:corr1-MN 15.75 .992 No_date 28:02 25.60 n/a 0.000
02026# [MjSysVol=00000-00, TotVolVol=00000-00, N-Ovrf= 0, TotDurOvf= 0 hrs]
02027# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02028# CONTINUOUS STANDBY 1.0 01:BL 2.77 .033 No_date 28:09 9.64 212 0.000
02029# [CN= 56.0] 1.00 Tpe= 1.20]
02030# [IAREC= 4.00: SMIN= 75.69: SMAK=531.24: SK= 010]
02031# [InterValTime= 12.00]
02032# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02033# CONTINUOUS STANDBY 1.0 01:AD 1.27 .116 No_date 28:01 32.20 707 0.000
02034# [XMP= 63:TMP= 63]
02035# [LOSS= 2 CN= 75.0]
02036# [Previous area IArea= 4.67:SLP=1.00:LDP= 40.0:MP= 250:SCP= 0]
02037# [Impervious area IArea= 1.57:SLP=1.00:LDP= 251.0:MI= 013:SCI= 0]
02038# [IARECimp= 4.00: IARECPE= 4.00]
02039# [SMIN= 31.81: SMAK=221.43: SK= 010]
02040# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02041# COMPUTE DIALYD 1.0 01:AD 1.27 .116 No_date 28:01 32.20 n/a 0.000
02042# Major System / 1.0 02:AD-MJ 1.27 .116 No_date 28:01 32.20 n/a 0.000
02043# Minor System / 1.0 03:AD-MN 1.27 .116 No_date 28:01 32.20 n/a 0.000
02044# [MjSysVol=00000-00, TotVolVol=00000-00, N-Ovrf= 0, TotDurOvf= 0 hrs]
02045# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02046# CONTINUOUS STANDBY 1.0 01:AD 48.13 2.497 No_date 28:02 24.10 n/a 0.000
02047# SAVE HYD
02048# *****
02049# # Continous Flows at Station 2462
02050# # *****
02051# # - To Corrigan Drain (south of the Jock)
02052# # - Primarily Developed (medium density)
02053# # - JFSA JAN 2021, add Corrigan subcatchments as per IRI, July 2008
02054# # *****
02055# # CONTINUOUS STANDBY 1.0 01:corr1 15.87 1.352 No_date 28:02 31.77 698 0.000
02056# [XMP= 63:TMP= 63]
02057# [LOSS= 2 CN= 77.0]
02058# [Previous area IArea= 4.67:SLP=1.00:LDP= 40.0:MP= 250:SCP= 0]
02059# [Impervious area IArea= 1.57:SLP=1.00:LDP= 325.0:MI= 013:SCI= 0]
02060# [IARECimp= 4.00: IARECPE= 4.00]
02061# [SMIN= 31.81: SMAK=221.43: SK= 010]
02062# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02063# COMPUTE DIALYD 1.0 01:corr1 15.87 1.352 No_date 28:02 31.77 n/a 0.000
02064# Major System / 1.0 03:corr1-MJ 0.00 .000 No_date 0:00 .00 n/a 0.000
02065# Minor System / 1.0 03:corr1-MN 15.87 1.352 No_date 28:02 31.77 n/a 0.000
02066# [MjSysVol=00000-00, TotVolVol=00000-00, N-Ovrf= 0, TotDurOvf= 0 hrs]
02067# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02068# CONTINUOUS STANDBY 1.0 01:corr2 12.47 .100 No_date 29:12 14.83 136 0.000
02069# [CN= 77.0] N= 3.001 Tpe= 1.10]
02070# [IAREC= 4.00: SMIN= 31.15: SMAK=207.66: SK= 010]
02071# [LOSS= 2 CN= 75.0]
02072# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02073# CONTINUOUS STANDBY 1.0 01:corr1 15.75 .992 No_date 28:02 25.60 563 0.000
02074# [XMP= 42:TMP= 52]
02075# [LOSS= 2 CN= 75.0]
02076# [Previous area IArea= 4.67:SLP=1.00:LDP= 40.0:MP= 250:SCP= 0]
02077# [Impervious area IArea= 1.57:SLP=1.00:LDP= 324.0:MI= 013:SCI= 0]
02078# [IARECimp= 4.00: IARECPE= 4.00]
02079# [SMIN= 33.81: SMAK=221.43: SK= 010]
02080# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02081# COMPUTE DIALYD 1.0 01:corr1 15.75 .992 No_date 28:02 25.60 n/a 0.000
02082# Major System / 1.0 02:corr1-MJ 15.75 .992 No_date 28:02 25.60 n/a 0.000
02083# Minor System / 1.0 03:corr1-MN 15.75 .992 No_date 28:02 25.60 n/a 0.000
02084# [MjSysVol=00000-00, TotVolVol=00000-00, N-Ovrf= 0, TotDurOvf= 0 hrs]
02085# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02086# CONTINUOUS STANDBY 1.0 01:BL 2.77 .033 No_date 28:09 9.64 212 0.000
02087# [CN= 56.0] 1.00 Tpe= 1.20]
02088# [IAREC= 4.00: SMIN= 75.69: SMAK=531.24: SK= 010]
02089# [InterValTime= 12.00]
02090# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02091# CONTINUOUS STANDBY 1.0 01:AD 1.27 .116 No_date 28:01 32.20 707 0.000
02092# [XMP= 63:TMP= 63]
02093# [LOSS= 2 CN= 75.0]
02094# [Previous area IArea= 4.67:SLP=1.00:LDP= 40.0:MP= 250:SCP= 0]
02095# [Impervious area IArea= 1.57:SLP=1.00:LDP= 251.0:MI= 013:SCI= 0]
02096# [IARECimp= 4.00: IARECPE= 4.00]
02097# [SMIN= 31.81: SMAK=221.43: SK= 010]
02098# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02099# COMPUTE DIALYD 1.0 01:AD 1.27 .116 No_date 28:01 32.20 n/a 0.000
02100# Major System / 1.0 02:AD-MJ 1.27 .116 No_date 28:01 32.20 n/a 0.000
02101# Minor System / 1.0 03:AD-MN 1.27 .116 No_date 28:01 32.20 n/a 0.000
02102# [MjSysVol=00000-00, TotVolVol=00000-00, N-Ovrf= 0, TotDurOvf= 0 hrs]
02103# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02104# CONTINUOUS STANDBY 1.0 01:AD 48.13 2.497 No_date 28:02 24.10 n/a 0.000
02105# SAVE HYD
02106# *****
02107# # Continous Flows at Station 2462
02108# # *****
02109# # - To Corrigan Drain (south of the Jock)
02110# # - Primarily Developed (medium density)
02111# # - JFSA JAN 2021, add Corrigan subcatchments as per IRI, July 2008
02112# # *****
02113# # CONTINUOUS STANDBY 1.0 01:corr1 15.87 1.352 No_date 28:02 31.77 698 0.000
02114# [XMP= 63:TMP= 63]
02115# [LOSS= 2 CN= 77.0]
02116# [Previous area IArea= 4.67:SLP=1.00:LDP= 40.0:MP= 250:SCP= 0]
02117# [Impervious area IArea= 1.57:SLP=1.00:LDP= 325.0:MI= 013:SCI= 0]
02118# [IARECimp= 4.00: IARECPE= 4.00]
02119# [SMIN= 31.81: SMAK=221.43: SK= 010]
02120# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02121# COMPUTE DIALYD 1.0 01:corr1 15.87 1.352 No_date 28:02 31.77 n/a 0.000
02122# Major System / 1.0 03:corr1-MJ 0.00 .000 No_date 0:00 .00 n/a 0.000
02123# Minor System / 1.0 03:corr1-MN 15.87 1.352 No_date 28:02 31.77 n/a 0.000
02124# [MjSysVol=00000-00, TotVolVol=00000-00, N-Ovrf= 0, TotDurOvf= 0 hrs]
02125# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02126# CONTINUOUS STANDBY 1.0 01:corr2 12.47 .100 No_date 29:12 14.83 136 0.000
02127# [CN= 77.0] N= 3.001 Tpe= 1.10]
02128# [IAREC= 4.00: SMIN= 31.15: SMAK=207.66: SK= 010]
02129# [LOSS= 2 CN= 75.0]
02130# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02131# CONTINUOUS STANDBY 1.0 01:corr1 15.75 .992 No_date 28:02 25.60 563 0.000
02132# [XMP= 42:TMP= 52]
02133# [LOSS= 2 CN= 75.0]
02134# [Previous area IArea= 4.67:SLP=1.00:LDP= 40.0:MP= 250:SCP= 0]
02135# [Impervious area IArea= 1.57:SLP=1.00:LDP= 324.0:MI= 013:SCI= 0]
02136# [IARECimp= 4.00: IARECPE= 4.00]
02137# [SMIN= 33.81: SMAK=221.43: SK= 010]
02138# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02139# COMPUTE DIALYD 1.0 01:corr1 15.75 .992 No_date 28:02 25.60 n/a 0.000
02140# Major System / 1.0 02:corr1-MJ 15.75 .992 No_date 28:02 25.60 n/a 0.000
02141# Minor System / 1.0 03:corr1-MN 15.75 .992 No_date 28:02 25.60 n/a 0.000
02142# [MjSysVol=00000-00, TotVolVol=00000-00, N-Ovrf= 0, TotDurOvf= 0 hrs]
02143# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02144# CONTINUOUS STANDBY 1.0 01:BL 2.77 .033 No_date 28:09 9.64 212 0.000
02145# [CN= 56.0] 1.00 Tpe= 1.20]
02146# [IAREC= 4.00: SMIN= 75.69: SMAK=531.24: SK= 010]
02147# [InterValTime= 12.00]
02148# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02149# CONTINUOUS STANDBY 1.0 01:AD 1.27 .116 No_date 28:01 32.20 707 0.000
02150# [XMP= 63:TMP= 63]
02151# [LOSS= 2 CN= 75.0]
02152# [Previous area IArea= 4.67:SLP=1.00:LDP= 40.0:MP= 250:SCP= 0]
02153# [Impervious area IArea= 1.57:SLP=1.00:LDP= 251.0:MI= 013:SCI= 0]
02154# [IARECimp= 4.00: IARECPE= 4.00]
02155# [SMIN= 31.81: SMAK=221.43: SK= 010]
02156# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02157# COMPUTE DIALYD 1.0 01:AD 1.27 .116 No_date 28:01 32.20 n/a 0.000
02158# Major System / 1.0 02:AD-MJ 1.27 .116 No_date 28:01 32.20 n/a 0.000
02159# Minor System / 1.0 03:AD-MN 1.27 .116 No_date 28:01 32.20 n/a 0.000
02160# [MjSysVol=00000-00, TotVolVol=00000-00, N-Ovrf= 0, TotDurOvf= 0 hrs]
02161# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02162# CONTINUOUS STANDBY 1.0 01:AD 48.13 2.497 No_date 28:02 24.10 n/a 0.000
02163# SAVE HYD
02164# *****
02165# # Continous Flows at Station 2462
02166# # *****
02167# # - To Corrigan Drain (south of the Jock)
02168# # - Primarily Developed (medium density)
02169# # - JFSA JAN 2021, add Corrigan subcatchments as per IRI, July 2008
02170# # *****
02171# # CONTINUOUS STANDBY 1.0 01:corr1 15.87 1.352 No_date 28:02 31.77 698 0.000
02172# [XMP= 63:TMP= 63]
02173# [LOSS= 2 CN= 77.0]
02174# [Previous area IArea= 4.67:SLP=1.00:LDP= 40.0:MP= 250:SCP= 0]
02175# [Impervious area IArea= 1.57:SLP=1.00:LDP= 325.0:MI= 013:SCI= 0]
02176# [IARECimp= 4.00: IARECPE= 4.00]
02177# [SMIN= 31.81: SMAK=221.43: SK= 010]
02178# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02179# COMPUTE DIALYD 1.0 01:corr1 15.87 1.352 No_date 28:02 31.77 n/a 0.000
02180# Major System / 1.0 03:corr1-MJ 0.00 .000 No_date 0:00 .00 n/a 0.000
02181# Minor System / 1.0 03:corr1-MN 15.87 1.352 No_date 28:02 31.77 n/a 0.000
02182# [MjSysVol=00000-00, TotVolVol=00000-00, N-Ovrf= 0, TotDurOvf= 0 hrs]
02183# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02184# CONTINUOUS STANDBY 1.0 01:corr2 12.47 .100 No_date 29:12 14.83 136 0.000
02185# [CN= 77.0] N= 3.001 Tpe= 1.10]
02186# [IAREC= 4.00: SMIN= 31.15: SMAK=207.66: SK= 010]
02187# [LOSS= 2 CN= 75.0]
02188# AREHA=OPEAR=Cms=TPeakDate_hh:mm-----Rvm=R.C-----DWFFms
02189# CONTINUOUS STANDBY 1.0 01:corr1 15.75 .992 No_date 28:02 25.60 563 0.000
02190# [XMP= 42:TMP= 52]
02191# [LOSS= 2 CN= 75.0]
02192# [Previous area IArea= 4.67:SLP=1.00:LDP= 40.0:MP= 250:SCP= 0]
02193# [Impervious area IArea= 1.57:SLP=1.00:LDP= 324.0:MI= 013:SCI= 0]
02194# [IARECimp= 4.00: IARECPE= 4.00]
0219
```





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02619 overflow <= 1.0 03:20-0VDF 0.00 0.00 No.Date 0:00 0.00 n/a 0.00
02620 (MaxOvflow=3346.0) TotalOvflow=0.000E+00 83 0:00:00 0.0000000000
02621 R0025-CO0398-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02622 ADD HYD + 1.0 02:01:SM 55124.85 49.262 No.Date 38:53 13.26 n/a 0.00
02623 [I/Sm= 23.78 / 936 No.Date 28:03 19.26 n/a 0.00]
02624 + 1.0 02:30-0VDF 0.00 0.00 No.Date 0:00 0.00 n/a 0.00
02625 SUM= 1.0 02:30:0P 257.63 2.560 No.Date 29:05 26.85 n/a 0.00
02626 [I/Sm= 55476.26 / 49.619 No.Date 38:49 13.23 n/a 0.00]
02627 R0025-CO0397-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02628 SAVE HYD 1.0 01:SM_01 55476.26 49.619 No.Date 38:49 13.23 n/a 0.00
02629 name 'SML_DE_0022
02630 remark:Total Flows at Heart's Desire
02631 #
02632 # Hydrograph from Heart's Desire routed to Rideau River
02633 # Channel X-Section obtained from RWCA Hydraulic Model - Station 0
02634 #
02635 R0025-CO0398-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02636 ROUTE CHANNEL -> 1.0 02:SM_01 55476.26 49.619 No.Date 38:49 13.23 n/a 0.00
02637 [I/Sm= 1.0] out<= 1.0 01:SM 55476.26 49.617 No.Date 38:54 13.23 n/a 0.00
02638 [L/S/N= 563. / 367. / 045]
02639 (Vmax= 1.49 / Dmax= 0.01)
02640 #
02641 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02642 # of 1.65
02643 #
02644 # CONTINUOUS NASHVD 1.0 01:SM_01 55476.26 49.617 No.Date 38:54 13.23 n/a 0.00
02645 [I/Sm= 563. / 367. / 045]
02646 [I/Sm= 563. / 367. / 045]
02647 [I/Sm= 563. / 367. / 045]
02648 [I/Sm= 563. / 367. / 045]
02649 [I/Sm= 563. / 367. / 045]
02650 R0025-CO0400-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02651 ADD HYD + 1.0 02:SM 55476.26 49.617 No.Date 38:54 13.23 n/a 0.00
02652 + 1.0 02:SM_2 102.94 1.373 No.Date 28:20 13.01 n/a 0.00
02653 SUM= 1.0 02:SM_01 55476.26 49.617 No.Date 38:54 13.23 n/a 0.00
02654 R0025-CO0401-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02655 SAVE HYD 1.0 01:SM_01 55476.26 49.617 No.Date 38:54 13.23 n/a 0.00
02656 name 'SML_N1_0002
02657 remark:Total Flows at Rideau River
02658 #
02659 # ***** END OF RUN *****
02660 #
02661 #
02662 #
02663 #
02664 #
02665 #
02666 #
02667 R005-COMMANDS
02668 START
02669 [MTO= 0 hrs on 0]
02670 [MTO= 1]
02671 [MTO= 2 (1=Imperial, 2=metric output)]
02672 [MTO= 3]
02673 [MTO= 4]
02674 #
02675 # SWMNO Vers 5.02 (Jan 2001) ***** INPUT DATA FILE *****
02676 #
02677 # Project Name: (Good) Project Number: 1474-16
02678 #
02679 # Date 04-03-2021
02680 # Modeler JFS
02681 # Company JFSaInc
02682 # License # 254923
02683 #
02684 # CALIBRATION OF SUMMER MODEL PARAMETERS
02685 # USING CONTINUOUS SIMULATION
02686 # Mainfall data from OFSA rain gauge installed at site + other gauges by the City
02687 # Use data collected from May 1st to July 14, 2000
02688 # 2020-11-10 Change TMRPTO in COMPUTE POLYD TMRPTO = 0.1 instead of 0.2001
02689 # 2020-10-01 correct pond curve values
02690 # 2020-10-01 Change TMRPTO to 0.55, HLD(=0.5) (imperious slope), and LDT up to 700m
02691 # 2021-02-19 Change the slope for ROUTE CHANNEL Station 2462 (INHDD= 'M_70') ,MHVNI(= 'M_70') from 0.03 % (as per st
02692 # 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (INHDD= 'M_80') ,MHVNI(= 'M_80') from 0.01 % (as per st
02693 #
02694 R005-CO0002-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02695 READ STORM
02696 Filename = storm.001
02697 Comment = Pluie GCM de 24 hrs 1:5 ans pour Ottawa CDA
02698 [SD=10.00:SDUR= 24.00:PTD= 57.12]
02699 R005-CO0003
02700 MODIFY STORM
02701 [SFACT= 1.00:TMRPT= 96.00 min]
02702 [MTO= 10.00:SDUR= 24.00:PTD= 57.12]
02703 R005-CO0004-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02704 DEFAULT VALUES
02705 Filename = T:\PROJ\1474-16\Design\20210226-QuantityControlAnalysis\SWMNO\BNG-Model\Updated\Cl1CiteG.DEP
02706 ICAIRSD = 1 (read and print data)
02707 FileTitle File comments calibration exercises in Onta
02708 The FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDARD COM
02709 Horton's infiltration coefficient (F=0.1) [DCAV= 4.14 (hr) / (in .00 mm)
02710 [F= 76.20 mm/hr] [F=0.1] [DCAV= 4.14 (hr) / (in .00 mm)
02711 Parameters for IMPERVIOUS surfaces in STANWYVD
02712 [I/Sm= 4.67 mm] [LQ=50.00 min] [IMP= .250]
02713 Parameters for PERVIOUS surfaces in STANWYVD
02714 [I/Sm= 1.57 mm] [LQ= 1.50] [IMP= .033]
02715 Parameters used in NASHVD
02716 [I/Sm= 1.57 mm] [LQ= 1.50] [IMP= .033]
02717 Average monthly Pan Evaporation data in (mm)
02718 JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
02719 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
02720 Average monthly Potential Evapotranspiration in (mm)
02721 JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
02722 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
02723 R005-CO0005-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02724 COMPUTE API
02725 [API= 50.00:APIKdy= 8500:APIKdt= .9989]
02726 [API= 50.00:APIKdy= 8500:APIKdt= .9989]
02727 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02728 # of 1.32
02729 R005-CO0006-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02730 CONTINUOUS NASHVD 1.0 01:SM_01 3680.00 9.398 No.Date 37:02 16.41 287.00
02731 [I/Sm= 64.0 No. 3.00: Tp= 7.13]
02732 [I/Sm= 4.00: SMIN= 57.85: SMAX=380.32: SK= .010]
02733 [I/Sm= 64.0 No. 3.00: Tp= 7.13]
02734 #
02735 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02736 # of 1.32
02737 R005-CO0007-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02738 CONTINUOUS NASHVD 1.0 01:SM_01 971.00 3.405 No.Date 32:36 15.29 268.00
02739 [I/Sm= 64.0 No. 3.00: Tp= 7.13]
02740 [I/Sm= 4.00: SMIN= 64.50: SMAX=430.01: SK= .010]
02741 [I/Sm= 64.0 No. 3.00: Tp= 7.13]
02742 #
02743 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02744 # of 1.80
02745 R005-CO0008-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02746 CONTINUOUS NASHVD 1.0 01:SM_01 3074.00 4.682 No.Date 39:59 13.23 232.00
02747 [I/Sm= 64.0 No. 3.00: Tp= 11.33]
02748 [I/Sm= 4.00: SMIN= 54.96: SMAX=554.96: SK= .010]
02749 [I/Sm= 64.0 No. 3.00: Tp= 11.33]
02750 R005-CO0009-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02751 CONTINUOUS NASHVD 1.0 01:SM_01 1781.00 4.524 No.Date 39:49 13.23 232.00
02752 [I/Sm= 72.0 No. 3.00: Tp= 3.91]
02753 [I/Sm= 4.00: SMIN= 35.75: SMAX=264.99: SK= .010]
02754 [I/Sm= 72.0 No. 3.00: Tp= 3.91]
02755 R005-CO0010-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02756 CONTINUOUS NASHVD 1.0 01:SM_01 500.00 4.354 No.Date 39:22 17.18 301.00
02757 [I/Sm= 66.0 No. 3.00: Tp= 1.24]
02758 [I/Sm= 4.00: SMIN= 52.62: SMAX=350.79: SK= .010]
02759 [I/Sm= 66.0 No. 3.00: Tp= 1.24]
02760 #
02761 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02762 # of 1.80
02763 R005-CO0011-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02764 CONTINUOUS NASHVD 1.0 01:SM_01 1937.00 6.210 No.Date 34:31 17.18 301.00
02765 [I/Sm= 66.0 No. 3.00: Tp= 1.24]
02766 [I/Sm= 4.00: SMIN= 52.62: SMAX=350.79: SK= .010]
02767 [I/Sm= 66.0 No. 3.00: Tp= 1.24]
02768 #
02769 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02770 # of 1.52
02771 R005-CO0012-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02772 CONTINUOUS NASHVD 1.0 01:SM_01 5666.00 16.924 No.Date 38:02 20.12 352.00
02773 [I/Sm= 72.0 No. 3.00: Tp= 8.00]
02774 [I/Sm= 4.00: SMIN= 39.75: SMAX=264.99: SK= .010]
02775 [I/Sm= 72.0 No. 3.00: Tp= 8.00]
02776 #
02777 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02778 # of 1.75
02779 R005-CO0013-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02780 CONTINUOUS NASHVD 1.0 01:SM_01 8376.00 16.342 No.Date 39:59 17.18 301.00
02781 [I/Sm= 66.0 No. 3.00: Tp= 11.66]
02782 [I/Sm= 4.00: SMIN= 52.62: SMAX=350.79: SK= .010]
02783 [I/Sm= 66.0 No. 3.00: Tp= 11.66]
02784 #
02785 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02786 # of 1.68
02787 R005-CO0014-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02788 CONTINUOUS NASHVD 1.0 01:SM_01 1132.00 6.963 No.Date 30:55 19.24 337.00
02789 [I/Sm= 72.0 No. 3.00: Tp= 1.68]
02790 [I/Sm= 4.00: SMIN= 43.07: SMAX=287.10: SK= .010]
02791 [I/Sm= 72.0 No. 3.00: Tp= 1.68]
02792 #
02793 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02794 # of 1.52
02795 R005-CO0015-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02796 CONTINUOUS NASHVD 1.0 01:SM_01 5666.00 16.924 No.Date 38:02 20.12 352.00
02797 [I/Sm= 72.0 No. 3.00: Tp= 8.00]
02798 [I/Sm= 4.00: SMIN= 39.75: SMAX=264.99: SK= .010]
02799 [I/Sm= 72.0 No. 3.00: Tp= 8.00]
02800 #
02801 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02802 # of 1.80
02803 R005-CO0016-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02804 CONTINUOUS NASHVD 1.0 01:SM_01 131.00 1.298 No.Date 28:57 16.03 281.00
02805 [I/Sm= 63.0 No. 3.00: Tp= .90]
02806 #
02807 #
02808 #
02809 #
02810 #
02811 #
02812 #
02813 #
02814 #
02815 #
02816 #
02817 #
02818 #
02819 #
02820 #
02821 #
02822 #
02823 #
02824 #
02825 #
02826 #
02827 R005-CO0019-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02828 CONTINUOUS NASHVD 1.0 01:SM_01 1412.00 4.646 No.Date 37:53 21.98 385.00
02829 [I/Sm= 67.0 No. 3.00: Tp= 4.18]
02830 [I/Sm= 4.00: SMIN= 50.55: SMAX=336.97: SK= .010]
02831 [I/Sm= 67.0 No. 3.00: Tp= 4.18]
02832 #
02833 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02834 # of 1.67
02835 R005-CO0020-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02836 CONTINUOUS NASHVD 1.0 01:VGLDR 1332.00 4.803 No.Date 39:19 20.12 352.00
02837 [I/Sm= 72.0 No. 3.00: Tp= 5.93]
02838 [I/Sm= 4.00: SMIN= 39.75: SMAX=264.99: SK= .010]
02839 [I/Sm= 72.0 No. 3.00: Tp= 5.93]
02840 R005-CO0021-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02841 CONTINUOUS NASHVD 1.0 01:SM_01 224.00 4.100 No.Date 28:45 22.97 402.00
02842 [I/Sm= 77.0 No. 3.00: Tp= .75]
02843 [I/Sm= 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]
02844 [I/Sm= 77.0 No. 3.00: Tp= .75]
02845 #
02846 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02847 # of 1.23
02848 R005-CO0022-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02849 CONTINUOUS NASHVD 1.0 01:FLCK 4945.00 22.837 No.Date 33:22 21.04 368.00
02850 [I/Sm= 74.0 No. 3.00: Tp= 3.25]
02851 [I/Sm= 4.00: SMIN= 36.67: SMAX=244.49: SK= .010]
02852 [I/Sm= 74.0 No. 3.00: Tp= 3.25]
02853 R005-CO0023-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02854 CONTINUOUS NASHVD 1.0 01:SM_01 20.00 .489 No.Date 28:36 25.62 448.00
02855 [I/Sm= 81.0 No. 3.00: Tp= 1.23]
02856 [I/Sm= 4.00: SMIN= 25.21: SMAX=168.09: SK= .010]
02857 [I/Sm= 81.0 No. 3.00: Tp= 1.23]
02858 #
02859 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02860 # of 1.61
02861 R005-CO0024-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02862 CONTINUOUS NASHVD 1.0 01:SM_01 1412.00 4.646 No.Date 37:53 21.98 385.00
02863 [I/Sm= 75.0 No. 3.00: Tp= 8.00]
02864 [I/Sm= 4.00: SMIN= 31.15: SMAX=225.43: SK= .010]
02865 [I/Sm= 75.0 No. 3.00: Tp= 8.00]
02866 R005-CO0025-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02867 CONTINUOUS NASHVD 1.0 01:SM_01 585.00 6.688 No.Date 29:57 25.62 448.00
02868 [I/Sm= 81.0 No. 3.00: Tp= 1.75]
02869 [I/Sm= 4.00: SMIN= 25.21: SMAX=168.09: SK= .010]
02870 [I/Sm= 81.0 No. 3.00: Tp= 1.75]
02871 R005-CO0026-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02872 CONTINUOUS NASHVD 1.0 01:LMLCK 1021.00 8.861 No.Date 30:48 25.07 439.00
02873 [I/Sm= 80.0 No. 3.00: Tp= 2.46]
02874 [I/Sm= 4.00: SMIN= 24.12: SMAX=175.50: SK= .010]
02875 [I/Sm= 80.0 No. 3.00: Tp= 2.46]
02876 R005-CO0027-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02877 CONTINUOUS NASHVD 1.0 01:SM_01 177.00 3.240 No.Date 28:45 22.97 402.00
02878 [I/Sm= 77.0 No. 3.00: Tp= .75]
02879 [I/Sm= 4.00: SMIN= 31.15: SMAX=207.66: SK= .010]
02880 [I/Sm= 77.0 No. 3.00: Tp= .75]
02881 R005-CO0028-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02882 CONTINUOUS NASHVD 1.0 01:SM_01 1122.00 8.165 No.Date 31:48 25.62 448.00
02883 [I/Sm= 81.0 No. 3.00: Tp= 1.23]
02884 [I/Sm= 4.00: SMIN= 25.21: SMAX=168.09: SK= .010]
02885 [I/Sm= 81.0 No. 3.00: Tp= 1.23]
02886 R005-CO0029-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02887 CONTINUOUS NASHVD 1.0 01:SM_01 2737.00 17.859 No.Date 31:33 22.47 393.00
02888 [I/Sm= 76.0 No. 3.00: Tp= 1.81]
02889 [I/Sm= 4.00: SMIN= 32.46: SMAX=216.39: SK= .010]
02890 [I/Sm= 76.0 No. 3.00: Tp= 1.81]
02891 #
02892 # Routing hydrographs
02893 #
02894 # Starting with the addition of Jock River Headwater and Subwatershed 13
02895 #
02896 R005-CO0030-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02897 ADD HYD + 1.0 02:SM_01 3680.00 9.398 No.Date 37:02 16.41 287.00
02898 SUM= 1.0 02:SM_01 971.00 3.405 No.Date 32:36 15.29 n/a 0.00
02899 [I/Sm= 1.0] out<= 1.0 01:SM_01 4651.00 11.949 No.Date 39:33 16.17 n/a 0.00
02900 [I/Sm= 1.0] out<= 1.0 01:SM_01 4651.00 11.949 No.Date 39:33 16.17 n/a 0.00
02901 # Sum of hydrographs from Node 13 routed to Node 13A
02902 # (Approximated cross-section - see cross-section 258)
02903 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
02904 #
02905 R005-CO0031-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02906 ROUTE CHANNEL -> 1.0 02:SM_01 4651.00 11.949 No.Date 39:33 16.17 n/a 0.00
02907 [I/Sm= 1.0] out<= 1.0 01:SM_01 4651.00 11.949 No.Date 39:33 16.17 n/a 0.00
02908 [L/S/N= 9074. / 022. / 040]
02909 (Vmax= 478: Dmax= 3.020)
02910 #
02911 # Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
02912 R005-CO0032-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02913 ADD HYD + 1.0 02:SM_01 4651.00 9.514 No.Date 39:57 16.17 n/a 0.00
02914 SUM= 1.0 02:SM_01 3074.00 4.682 No.Date 39:59 13.23 n/a 0.00
02915 [I/Sm= 1.0] out<= 1.0 01:SM_01 7725.00 14.196 No.Date 39:59 15.00 n/a 0.00
02916 [I/Sm= 1.0] out<= 1.0 01:SM_01 7725.00 14.196 No.Date 39:59 15.00 n/a 0.00
02917 #
02918 # Insertion of a reservoir to simulate the effects of the Goodwood Marsh
02919 R005-CO0033-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02920 CONTINUOUS NASHVD 1.0 01:SM_01 7725.00 14.196 No.Date 39:59 15.00 n/a 0.00
02921 [I/Sm= 1.0] out<= 1.0 01:RES_GM 7725.00 3.149 No.Date 57:25 15.00 n/a 0.00
02922 [I/Sm= 1.0] out<= 1.0 01:RES_GM 7725.00 3.149 No.Date 57:25 15.00 n/a 0.00
02923 (MaxOvflow=6321.02 mm)
02924 #
02925 R005-CO0034-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02926 SAVE HYD 1.0 01:SM_01 7725.00 3.149 No.Date 57:25 15.00 n/a 0.00
02927 name 'HRES_GM
02928 remark:Outlet flow from Res GM
02929 # Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
02930 # (Approximated cross-section - see cross-section 258)
02931 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
02932 R005-CO0035-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02933 ROUTE CHANNEL -> 1.0 01:SM_01 7725.00 3.149 No.Date 57:25 15.00 n/a 0.00
02934 [I/Sm= 1.0] out<= 1.0 01:SM_01 7725.00 3.149 No.Date 57:25 15.00 n/a 0.00
02935 [I/Sm= 1.0] out<= 1.0 01:SM_01 7725.00 3.149 No.Date 57:25 15.00 n/a 0.00
02936 (Vmax= 527: Dmax= 1.429)
02937 #
02938 # Addition of Subwatershed Jock River at Ashton to Node 12
02939 R005-CO0036-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02940 ADD HYD + 1.0 02:H12 7725.00 3.137 No.Date 60:12 15.00 n/a 0.00
02941 SUM= 1.0 02:SM_01 1781.00 4.524 No.Date 39:49 13.23 232.00
02942 [I/Sm= 1.0] out<= 1.0 02:RASH 1781.00 4.524 No.Date 39:49 13.23 232.00
02943 [I/Sm= 1.0] out<= 1.0 02:H12 8506.00 10.498 No.Date 32:46 15.96 n/a 0.00
02944 R005-CO0037-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02945 SAVE HYD 1.0 01:SM_01 8506.00 10.498 No.Date 32:46 15.96 n/a 0.00
02946 name 'H_S12
02947 remark:flow at S_1212 near Ashton
02948 #
02949 # Sum of hydrographs from Node 12 routed to Node 11
02950 # (Approximated cross-section - see cross-section 258)
02951 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
02952 R005-CO0038-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02953 CONTINUOUS NASHVD 1.0 01:SM_01 9506.00 10.499 No.Date 32:46 15.96 n/a 0.00
02954 [I/Sm= 1.0] out<= 1.0 01:SM_01 9506.00 10.499 No.Date 32:46 15.96 n/a 0.00
02955 [I/Sm= 1.0] out<= 1.0 01:SM_01 9506.00 10.499 No.Date 32:46 15.96 n/a 0.00
02956 (Vmax= 648: Dmax= 2.408)
02957 #
02958 # Addition of Subwatershed 11 and No Name Creek to Node 11
02959 R005-CO0039-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02960 ADD HYD + 1.0 02:H11 11923.00 12.026 No.Date 38:02 17.18 n/a 0.00
02961 SUM= 1.0 02:SM_01 500.00 4.354 No.Date 39:22 17.18 n/a 0.00
02962 [I/Sm= 1.0] out<= 1.0 01:SM_01 12115.00 16.480 No.Date 38:02 17.18 n/a 0.00
02963 [I/Sm= 1.0] out<= 1.0 01:SM_01 11923.00 12.026 No.Date 38:02 17.18 n/a 0.00
02964 [I/Sm= 1.0] out<= 1.0 01:SM_01 11923.00 12.026 No.Date 38:02 17.18 n/a 0.00
02965 [I/Sm= 1.0] out<= 1.0 01:SM_01 11923.00 12.026 No.Date 38:02 17.18 n/a 0.00
02966 #
02967 # Sum of hydrographs from Node 11 routed to Node 10
02968 R005-CO0040-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02969 ADD HYD + 1.0 02:H10 11923.00 12.026 No.Date 38:02 17.18 n/a 0.00
02970 SUM= 1.0 01:SM_01 11923.00 12.026 No.Date 38:02 17.18 n/a 0.00
02971 [I/Sm= 1.0] out<= 1.0 01:SM_01 11923.00 12.026 No.Date 38:02 17.18 n/a 0.00
02972 R005-CO0041-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02973 ROUTE CHANNEL -> 1.0 01:R_01 11923.00 17.560 No.Date 31:03 16.21 n/a 0.00
02974 [I/Sm= 1.0] out<= 1.0 01:R_01 11923.00 17.560 No.Date 31:03 16.21 n/a 0.00
02975 [I/Sm= 14028. / 157. / 040]
02976 (Vmax= 461: Dmax= 1.087)
02977 #
02978 # Addition of Subwatershed 10 to Node 10
02979 R005-CO0042-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02980 ADD HYD + 1.0 02:H10 11923.00 12.026 No.Date 38:02 17.18 n/a 0.00
02981 SUM= 1.0 02:SM_01 5666.00 16.924 No.Date 38:02 20.12 n/a 0.00
02982 [I/Sm= 1.0] out<= 1.0 01:SM_01 17589.00 28.927 No.Date 38:09 17.47 n/a 0.00
02983 R005-CO0043-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02984 name 'H_S10
02985 remark:flow at S_1010 N10 + SK= 10
02986 # Addition of Kings Creek to S_10
02987 R005-CO0044-----DtnIn-ID:HYDF-----AREHA-QPEARComs-TpeakDate_hh:mm-----RvM-R.C-----DWFFms
02988 ADD HYD + 1.0 02:R_01 17589.00 28.927 No.Date 38:09 17.47 n/a 
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02993# SUM= 1.0 01:15:00 25965.00 44.722 No.Date 39:35 17.37 n/a .000
02994# #
02995# # Sum of hydrographs from Node 10 routed to Node 9
02996# # Section 2
02997# #
02998# ROUTE CHANNEL -> 1.0 02:15:00 25965.00 44.722 No.Date 39:35 17.37 n/a .000
02999# [RPT: 1.00] out<- 1.0 01:15:00 25965.00 43.534 No.Date 39:59 17.37 n/a .000
03000# [L/S= 3982./ .071/.051/.035]
03001# [Vmax: .664;Dmax: 1.502]
03002# #
03003# #
03004# # Addition of Subwatershed 9 and Nichols Creek to Node 9
03005# #
03006# ROUTES-CO0044-----DtnIn-ID:HYND-----AREHA-GPEARCS-TpeaDate_hh:mm-----Rvm-R-C-----DWFCms
03007# ADD HYD + 1.0 02:15:00 25965.00 43.534 No.Date 39:59 17.37 n/a .000
03008# + 1.0 02:15:00 1132.00 6.963 No.Date 30:55 19.24 n/a .000
03009# + 1.0 02:15:00 4464.00 8.109 No.Date 39:59 15.66 n/a .000
03010# SUM= 1.0 01:15:00 31661.00 53.366 No.Date 39:59 17.20 n/a .000
03011# [L/S= 2269./ .089/.040]
03012# [Vmax: .370;Dmax: 1.520]
03013# #
03014# # Sum of hydrographs from Node 9 routed to Node 8
03015# # Section 3
03016# ROUTES-CO0044-----DtnIn-ID:HYND-----AREHA-GPEARCS-TpeaDate_hh:mm-----Rvm-R-C-----DWFCms
03017# [RPT: 1.00] out<- 1.0 01:15:00 31661.00 49.404 No.Date 39:59 17.20 n/a .000
03018# [L/S= 2269./ .089/.040]
03019# [Vmax: .370;Dmax: 1.520]
03020# #
03021# # Addition of Subwatershed 8 and Hobbs' Drain to Node 8
03022# #
03023# ROUTES-CO0047-----DtnIn-ID:HYND-----AREHA-GPEARCS-TpeaDate_hh:mm-----Rvm-R-C-----DWFCms
03024# ADD HYD + 1.0 02:15:00 31661.00 49.404 No.Date 39:59 17.20 n/a .000
03025# + 1.0 02:15:00 131.00 1.298 No.Date 28:57 16.63 n/a .000
03026# + 1.0 02:15:00 3854.00 9.385 No.Date 38:41 17.18 n/a .000
03027# SUM= 1.0 01:15:00 35546.00 58.845 No.Date 39:59 17.19 n/a .000
03028# #
03029# # Sum of hydrographs from Node 8 routed to Node 7
03030# # Section 3
03031# ROUTES-CO0044-----DtnIn-ID:HYND-----AREHA-GPEARCS-TpeaDate_hh:mm-----Rvm-R-C-----DWFCms
03032# [RPT: 1.00] out<- 1.0 01:15:00 35546.00 48.127 No.Date 45:08 17.19 n/a .000
03033# [L/S= 2187./ .057/.037]
03034# [Vmax: .208;Dmax: 1.855]
03035# #
03036# #
03037# #
03038# # Addition of Subwatershed 7 to Node 7
03039# #
03040# ROUTES-CO0049-----DtnIn-ID:HYND-----AREHA-GPEARCS-TpeaDate_hh:mm-----Rvm-R-C-----DWFCms
03041# ADD HYD + 1.0 02:15:00 35546.00 48.127 No.Date 45:08 17.19 n/a .000
03042# + 1.0 02:15:00 3197.00 7.027 No.Date 36:28 13.49 n/a .000
03043# SUM= 1.0 01:15:00 38743.00 55.155 No.Date 44:14 16.92 n/a .000
03044# [L/S= 2187./ .057/.037]
03045# [Vmax: .208;Dmax: 1.855]
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06611	ADD HYD	1.0 0218_M5	31561.00	61.483 No.Date	39:57	21.20	n/a	.000
06612		1.0 0218_M5	131.00	1.689 No.Date	28:57	19.76	n/a	.000
06613		1.0 0218_DR	3854.00	11.811 No.Date	38:37	21.19	n/a	.000
06614	SUM	1.0 0121_M5	35546.00	73.344 No.Date	39:57	21.19	n/a	.000
06615								
06616	Sum of hydrographs from Node 8 routed to Node 7							
06617	Section 4							
06618	ROUTER CHANNEL	1.0 0218_M5	35546.00	73.344 No.Date	39:57	21.19	n/a	.000
06619	[RPT: 1.00] out<	1.0 0218_M5	3157.00	61.416 No.Date	45:01	21.19	n/a	.000
06620	[L/S= 306. / .057/.035]							
06621	[Vmax= .218/Dmax= 1.987]							
06622								
06623								
06624								
06625	Addition of Subwatershed 7 to Node 7							
06626								
06627	ROUTER CHANNEL	1.0 0218_M5	35546.00	73.344 No.Date	39:57	21.19	n/a	.000
06628	ADD HYD	1.0 0218_M5	35546.00	61.416 No.Date	45:01	21.19	n/a	.000
06629		1.0 0218_M5	3157.00	61.416 No.Date	45:01	21.19	n/a	.000
06630	SUM	1.0 0218_M5	38743.00	65.819 No.Date	44:06	20.85	n/a	.000
06631	ROUTER CHANNEL	1.0 0218_M5	38743.00	65.819 No.Date	44:06	20.85	n/a	.000
06632	SAVE HYD	1.0 0121_M7	38743.00	65.819 No.Date	44:06	20.85	n/a	.000
06633	fname_H_LNBT							
06634	remark:flow at 8_N7: M7 = SK 7							
06635	Insertion of a reservoir to simulate the effects of the Richmond Fen.							
06636	Storage area and volumes were estimated from available topo maps.							
06637	Release rate from fen was assumed to be controlled by the downstream							
06638	river cross-section for summer conditions. It is assumed that for up to							
06639	0.75 m of water, the main channel of the river provided the storage. Above							
06640	0.75 m this depth, the wetland starts to significantly store water.							
06641								
06642	ROUTER CHANNEL	1.0 0218_M5	38743.00	65.819 No.Date	44:06	20.85	n/a	.000
06643	ROUTER RESERVOIR	1.0 0218_M5	38743.00	65.819 No.Date	44:06	20.85	n/a	.000
06644	out <=	1.0 01218_RP	38743.00	31.796 No.Date	60:32	20.85	n/a	.000
06645	[NotToStore=.188E+02 m3, ToOVVol=.0000E+00 m3, N-ovr= 0.0, ToTurbDvF=.0 hrs]							
06646	ROUTER CHANNEL	1.0 0218_M5	38743.00	31.796 No.Date	60:32	20.85	n/a	.000
06647	SAVE HYD	1.0 01218_RP	38743.00	31.796 No.Date	60:32	20.85	n/a	.000
06648	fname_H_ResRF							
06649	remark:outflow of Richmond Fen							
06650								
06651	Sum of hydrographs from Node 7 routed to Node 6							
06652	Section 5							
06653								
06654	ROUTER CHANNEL	1.0 0218_M5	38743.00	31.796 No.Date	62:00	20.85	n/a	.000
06655	[RPT: 1.00] out<	1.0 01218_RP	38743.00	31.796 No.Date	62:00	20.85	n/a	.000
06656	[L/S= 306. / .087/.035]							
06657	[Vmax= .477/Dmax= .940]							
06658								
06659	Addition of Subwatershed 6 and Van Gaal Drain to Node 6							
06660								
06661	ROUTER CHANNEL	1.0 0218_M5	38743.00	31.796 No.Date	62:00	20.85	n/a	.000
06662	ADD HYD	1.0 0218_M5	38743.00	31.796 No.Date	62:00	20.85	n/a	.000
06663		1.0 0218_M5	1232.00	6.069 No.Date	35:17	24.81	n/a	.000
06664	SUM	1.0 0121_M5	1040.00	31.737 No.Date	62:00	20.85	n/a	.000
06665	ROUTER CHANNEL	1.0 0218_M5	38743.00	31.737 No.Date	62:00	20.85	n/a	.000
06666								
06667	Sum of hydrographs from Node 6 routed to Node 5							
06668	Section 5							
06669	ROUTER CHANNEL	1.0 0218_M5	38743.00	31.796 No.Date	62:00	20.85	n/a	.000
06670	[RPT: 1.00] out<	1.0 01218_RP	40240.00	31.737 No.Date	62:48	20.99	n/a	.000
06671	[L/S= 423. / .054/.035]							
06672	[Vmax= .412/Dmax= 1.069]							
06673								
06674	Addition of Subwatershed 5 and Flowing Creek to Node 5							
06675								
06676	ROUTER CHANNEL	1.0 0218_M5	40240.00	31.737 No.Date	62:48	20.99	n/a	.000
06677	ADD HYD	1.0 0218_M5	40240.00	31.737 No.Date	62:48	20.99	n/a	.000
06678		1.0 0218_M5	224.00	5.246 No.Date	28:45	24.81	n/a	.000
06679	SUM	1.0 0218_M5	4945.00	28.945 No.Date	33:21	25.91	n/a	.000
06680	ROUTER CHANNEL	1.0 0218_M5	4945.00	28.945 No.Date	33:21	25.91	n/a	.000
06681	SUM	1.0 0121_M5	45409.00	51.948 No.Date	34:54	21.86	n/a	.000
06682								
06683	Sum of hydrographs from Node 5 routed to Node 5A							
06684	Section 7							
06685	ROUTER CHANNEL	1.0 0218_M5	49409.00	51.948 No.Date	34:54	21.86	n/a	.000
06686	ROUTER RESERVOIR	1.0 0218_M5	45409.00	51.948 No.Date	35:12	21.56	n/a	.000
06687	[RPT: 1.00] out<	1.0 01218_RP	45409.00	51.948 No.Date	35:12	21.56	n/a	.000
06688	[L/S= 556. / .099/.040]							
06689	[Vmax= .485/Dmax= 1.331]							
06690	Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A							
06691								
06692	ROUTER CHANNEL	1.0 0218_M5	45409.00	51.948 No.Date	35:12	21.56	n/a	.000
06693	ADD HYD	1.0 0218_M5	45409.00	51.948 No.Date	35:12	21.56	n/a	.000
06694		1.0 0218_M5	1432.00	5.817 No.Date	37:54	27.06	n/a	.000
06695	SUM	1.0 0121_M5	46844.00	56.788 No.Date	35:22	21.73	n/a	.000
06696	ROUTER CHANNEL	1.0 0218_M5	46844.00	56.788 No.Date	35:22	21.73	n/a	.000
06697								
06698	Sum of hydrographs from Node 5A routed to Node 4							
06699	Section 8							
06700	ROUTER CHANNEL	1.0 0218_M5A	46844.00	56.788 No.Date	35:22	21.73	n/a	.000
06701	[RPT: 1.00] out<	1.0 0218_M5A	46841.00	54.943 No.Date	35:26	21.73	n/a	.000
06702	[L/S= 463.0 / .043/.035]							
06703	[Vmax= .793/Dmax= 3.295]							
06704								
06705	Addition of Subwatershed 4 and Leamy Creek to Node 4							
06706								
06707	ROUTER CHANNEL	1.0 0218_M5A	46841.00	54.943 No.Date	35:26	21.73	n/a	.000
06708	ADD HYD	1.0 0218_M4	46841.00	54.943 No.Date	35:26	21.73	n/a	.000
06709		1.0 0218_M4	1585.00	8.458 No.Date	29:57	31.37	n/a	.000
06710	SUM	1.0 0218_M5	1021.00	11.195 No.Date	30:48	30.72	n/a	.000
06711	ROUTER CHANNEL	1.0 0218_M5	48447.00	59.818 No.Date	36:12	22.03	n/a	.000
06712	SAVE HYD	1.0 0121_M5	48447.00	59.818 No.Date	36:12	22.03	n/a	.000
06713	fname_R_M4.0010							
06714	remark:flow at 8_M4							
06715	Sum of hydrographs from Node 4 routed to Node 2							
06716	Section 9							
06717	ROUTER CHANNEL	1.0 0218_M4	48447.00	59.818 No.Date	36:12	22.03	n/a	.000
06718	[RPT: 1.00] out<	1.0 01218_RP	48447.00	59.818 No.Date	36:12	22.03	n/a	.000
06719	[L/S= 1467. / .061/.040]							
06720	[Vmax= .824/Dmax= 3.325]							
06721								
06722	Addition of Subwatershed 2 with Monahan Drain and Smith Drain to Node 2							
06723								
06724	ROUTER CHANNEL	1.0 0218_M4	48447.00	59.818 No.Date	36:12	22.03	n/a	.000
06725	ADD HYD	1.0 0218_M4	48447.00	59.818 No.Date	36:12	22.03	n/a	.000
06726		1.0 0218_M4	177.00	4.146 No.Date	28:45	28.24	n/a	.000
06727	SUM	1.0 0218_M4	1122.00	10.275 No.Date	31:46	31.37	n/a	.000
06728	ROUTER CHANNEL	1.0 0218_M4	2377.00	22.669 No.Date	31:32	27.64	n/a	.000
06729	SUM	1.0 0121_M5	52483.00	83.235 No.Date	33:15	22.55	n/a	.000
06730	ROUTER CHANNEL	1.0 0218_M4	52483.00	83.235 No.Date	33:15	22.55	n/a	.000
06731	SAVE HYD	1.0 0121_M5	52483.00	83.235 No.Date	33:15	22.55	n/a	.000
06732	fname_H_N2							
06733	remark:flow at 8_N2 Joak River Gauge at Moodle Dr							
06734	Sum of hydrographs from Node 2 routed to Node 1							
06735	Section 10							
06736	ROUTER CHANNEL	1.0 0218_M4	52483.00	83.235 No.Date	33:15	22.55	n/a	.000
06737	[RPT: 1.00] out<	1.0 01218_RP	52483.00	83.235 No.Date	34:18	22.55	n/a	.000
06738	[L/S= 1237. / .050/.055]							
06739	[Vmax= .705/Dmax= 2.443]							
06740								
06741	Catchment SW-1A							
06742	Position of RWCA catchment SW-1 outside of Reach 3 subwatershed							
06743	Undeveloped agricultural land							
06744								
06745	ROUTER CHANNEL	1.0 0218_M5	536.42	3.888 No.Date	31:17	23.97	364	.000
06746	CONTINUOUS STANDED	[SW= 72.0] No. 3.001 Tpa= 2.91						
06747	[RPT: 1.00] out<	[SW= 72.0] No. 3.001 Tpa= 2.91						
06748	[L/S= 92. / .230/.043]							
06749	[Vmax= .592/Dmax= 1.002]							
06750								
06751	ROUTER CHANNEL	1.0 0218_M5	536.42	3.888 No.Date	31:17	23.97	364	.000
06752	CONTINUOUS STANDED	[SW= 46.3] No. 3.001 Tpa= 1.05						
06753	[RPT: 1.00] out<	[SW= 46.3] No. 3.001 Tpa= 1.05</						





06733	R0101C00225	-----DtmIn-ID:HYD-----	AREHA-GPEARMS-TPeakDate_hh:mm	-----RvM-R-C-----	DWPFMS	06920	#	PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (11808)), SWM Modeling Approach, NOVATECH Report June, 2020
06734	CONTINUOUS STANDHYD	Fw= 76.20(Fc= 13.20)DCAV4:1.44 Fw= 0.00	2.137	270	28:00	56.40	872	
06735	[XMP= 86(TIMP= 86)]							
06736	[Horizon parameters] Fw= 76.20(Fc= 13.20)DCAV4:1.44 Fw= 0.00							
06737	[Previous area] IArea= 4.67(SLPP= 2.00)LD= 40.IMP= 250(SIC= 0)							
06738	[Impervious area] IArea= 1.57(SLPP= 2.00)LD= 40.IMP= 250(SIC= 0)							
06739	[ISaIcImp= 4.00] IArea= 4.00							
06740	[Major system] / 1.0 01:PC-01-MJ	8.03	1.049	28:01	37.67	1.82	0.00	
06741	[Minor system] / 1.0 01:PC-02-MJ	16.05	1.159	28:02	39.94	0.00	0.00	
06742	[MjSysTot= 1270E= 0.0, TotVolVol= 0.000E= 0.0, N= 0.0, T= 0.0] (hrs)							
06743	ADD HYD	+ 1.0 01:PC-01-MJ	0.00	0.00	0:00	0.00	0.00	
06744	SUM	+ 1.0 01:PC-01-MJ	8.03	1.049	28:01	37.67	1.82	
06745	SUM	+ 1.0 01:PC-02-MJ	16.05	1.159	28:02	39.94	0.00	
06746	CONTINUOUS STANDHYD	1.0 01:PC-02	16.05	1.159	28:02	39.94	0.00	
06747	[XMP= 93(TIMP= 93)]							
06748	[Horizon parameters] Fw= 76.20(Fc= 13.20)DCAV4:1.44 Fw= 0.00							
06749	[Previous area] IArea= 4.67(SLPP= 2.00)LD= 40.IMP= 250(SIC= 0)							
06750	[Impervious area] IArea= 1.57(SLPP= 2.00)LD= 40.IMP= 250(SIC= 0)							
06751	[ISaIcImp= 4.00] IArea= 4.00							
06752	[Major system] / 1.0 01:PC-01-MJ	8.03	1.049	28:01	37.67	1.82	0.00	
06753	[Minor system] / 1.0 01:PC-02-MJ	16.05	1.159	28:02	39.94	0.00	0.00	
06754	[MjSysTot= 1407E= 0.0, TotVolVol= 0.000E= 0.0, N= 0.0, T= 0.0] (hrs)							
06755	ADD HYD	+ 1.0 01:PC-01-MJ	0.00	0.00	0:00	0.00	0.00	
06756	SUM	+ 1.0 01:PC-01-MJ	8.03	1.049	28:01	37.67	1.82	
06757	SUM	+ 1.0 01:PC-02-MJ	16.05	1.159	28:02	39.94	0.00	
06758	CONTINUOUS STANDHYD	1.0 01:PC-03	7.37	1.130	28:01	45.83	7.08	
06759	[XMP= 64(TIMP= 64)]							
06760	[Horizon parameters] Fw= 76.20(Fc= 13.20)DCAV4:1.44 Fw= 0.00							
06761	[Previous area] IArea= 4.67(SLPP= 2.00)LD= 40.IMP= 250(SIC= 0)							
06762	[Impervious area] IArea= 1.57(SLPP= 2.00)LD= 40.IMP= 250(SIC= 0)							
06763	[ISaIcImp= 4.00] IArea= 4.00							
06764	[Major system] / 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	0.00	
06765	[Minor system] / 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	0.00	
06766	[MjSysTot= 9380E= 0.0, TotVolVol= 0.000E= 0.0, N= 0.0, T= 0.0] (hrs)							
06767	ADD HYD	+ 1.0 01:PC-04-MJ	0.00	0.00	0:00	0.00	0.00	
06768	SUM	+ 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	
06769	SUM	+ 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	
06770	CONTINUOUS STANDHYD	1.0 01:PC-04	12.87	1.806	28:01	45.83	7.08	
06771	[XMP= 64(TIMP= 64)]							
06772	[Horizon parameters] Fw= 76.20(Fc= 13.20)DCAV4:1.44 Fw= 0.00							
06773	[Previous area] IArea= 4.67(SLPP= 2.00)LD= 40.IMP= 250(SIC= 0)							
06774	[Impervious area] IArea= 1.57(SLPP= 2.00)LD= 40.IMP= 250(SIC= 0)							
06775	[ISaIcImp= 4.00] IArea= 4.00							
06776	[Major system] / 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	0.00	
06777	[Minor system] / 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	0.00	
06778	[MjSysTot= 9380E= 0.0, TotVolVol= 0.000E= 0.0, N= 0.0, T= 0.0] (hrs)							
06779	ADD HYD	+ 1.0 01:PC-04-MJ	0.00	0.00	0:00	0.00	0.00	
06780	SUM	+ 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	
06781	SUM	+ 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	
06782	CONTINUOUS STANDHYD	1.0 01:PC-04	12.87	1.806	28:01	45.83	7.08	
06783	[XMP= 64(TIMP= 64)]							
06784	[Horizon parameters] Fw= 76.20(Fc= 13.20)DCAV4:1.44 Fw= 0.00							
06785	[Previous area] IArea= 4.67(SLPP= 2.00)LD= 40.IMP= 250(SIC= 0)							
06786	[Impervious area] IArea= 1.57(SLPP= 2.00)LD= 40.IMP= 250(SIC= 0)							
06787	[ISaIcImp= 4.00] IArea= 4.00							
06788	[Major system] / 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	0.00	
06789	[Minor system] / 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	0.00	
06790	[MjSysTot= 9380E= 0.0, TotVolVol= 0.000E= 0.0, N= 0.0, T= 0.0] (hrs)							
06791	ADD HYD	+ 1.0 01:PC-04-MJ	0.00	0.00	0:00	0.00	0.00	
06792	SUM	+ 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	
06793	SUM	+ 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	
06794	CONTINUOUS STANDHYD	1.0 01:PC-04	12.87	1.806	28:01	45.83	7.08	
06795	[XMP= 64(TIMP= 64)]							
06796	[Horizon parameters] Fw= 76.20(Fc= 13.20)DCAV4:1.44 Fw= 0.00							
06797	[Previous area] IArea= 4.67(SLPP= 2.00)LD= 40.IMP= 250(SIC= 0)							
06798	[Impervious area] IArea= 1.57(SLPP= 2.00)LD= 40.IMP= 250(SIC= 0)							
06799	[ISaIcImp= 4.00] IArea= 4.00							
06800	[Major system] / 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	0.00	
06801	[Minor system] / 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	0.00	
06802	[MjSysTot= 9380E= 0.0, TotVolVol= 0.000E= 0.0, N= 0.0, T= 0.0] (hrs)							
06803	ADD HYD	+ 1.0 01:PC-04-MJ	0.00	0.00	0:00	0.00	0.00	
06804	SUM	+ 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	
06805	SUM	+ 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	
06806	CONTINUOUS STANDHYD	1.0 01:PC-04	12.87	1.806	28:01	45.83	7.08	
06807	[XMP= 64(TIMP= 64)]							
06808	[Horizon parameters] Fw= 76.20(Fc= 13.20)DCAV4:1.44 Fw= 0.00							
06809	[Previous area] IArea= 4.67(SLPP= 2.00)LD= 40.IMP= 250(SIC= 0)							
06810	[Impervious area] IArea= 1.57(SLPP= 2.00)LD= 40.IMP= 250(SIC= 0)							
06811	[ISaIcImp= 4.00] IArea= 4.00							
06812	[Major system] / 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	0.00	
06813	[Minor system] / 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	0.00	
06814	[MjSysTot= 9380E= 0.0, TotVolVol= 0.000E= 0.0, N= 0.0, T= 0.0] (hrs)							
06815	ADD HYD	+ 1.0 01:PC-04-MJ	0.00	0.00	0:00	0.00	0.00	
06816	SUM	+ 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	
06817	SUM	+ 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	
06818	CONTINUOUS STANDHYD	1.0 01:PC-04	12.87	1.806	28:01	45.83	7.08	
06819	[XMP= 64(TIMP= 64)]							
06820	[Horizon parameters] Fw= 76.20(Fc= 13.20)DCAV4:1.44 Fw= 0.00							
06821	[Previous area] IArea= 4.67(SLPP= 2.00)LD= 40.IMP= 250(SIC= 0)							
06822	[Impervious area] IArea= 1.57(SLPP= 2.00)LD= 40.IMP= 250(SIC= 0)							
06823	[ISaIcImp= 4.00] IArea= 4.00							
06824	[Major system] / 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	0.00	
06825	[Minor system] / 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	0.00	
06826	[MjSysTot= 9380E= 0.0, TotVolVol= 0.000E= 0.0, N= 0.0, T= 0.0] (hrs)							
06827	ADD HYD	+ 1.0 01:PC-04-MJ	0.00	0.00	0:00	0.00	0.00	
06828	SUM	+ 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	
06829	SUM	+ 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	
06830	CONTINUOUS STANDHYD	1.0 01:PC-04	12.87	1.806	28:01	45.83	7.08	
06831	[XMP= 64(TIMP= 64)]							
06832	[Horizon parameters] Fw= 76.20(Fc= 13.20)DCAV4:1.44 Fw= 0.00							
06833	[Previous area] IArea= 4.67(SLPP= 2.00)LD= 40.IMP= 250(SIC= 0)							
06834	[Impervious area] IArea= 1.57(SLPP= 2.00)LD= 40.IMP= 250(SIC= 0)							
06835	[ISaIcImp= 4.00] IArea= 4.00							
06836	[Major system] / 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	0.00	
06837	[Minor system] / 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	0.00	
06838	[MjSysTot= 9380E= 0.0, TotVolVol= 0.000E= 0.0, N= 0.0, T= 0.0] (hrs)							
06839	ADD HYD	+ 1.0 01:PC-04-MJ	0.00	0.00	0:00	0.00	0.00	
06840	SUM	+ 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	
06841	SUM	+ 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	
06842	CONTINUOUS STANDHYD	1.0 01:PC-04	12.87	1.806	28:01	45.83	7.08	
06843	[XMP= 64(TIMP= 64)]							
06844	[Horizon parameters] Fw= 76.20(Fc= 13.20)DCAV4:1.44 Fw= 0.00							
06845	[Previous area] IArea= 4.67(SLPP= 2.00)LD= 40.IMP= 250(SIC= 0)							
06846	[Impervious area] IArea= 1.57(SLPP= 2.00)LD= 40.IMP= 250(SIC= 0)							
06847	[ISaIcImp= 4.00] IArea= 4.00							
06848	[Major system] / 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	0.00	
06849	[Minor system] / 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	0.00	
06850	[MjSysTot= 9380E= 0.0, TotVolVol= 0.000E= 0.0, N= 0.0, T= 0.0] (hrs)							
06851	ADD HYD	+ 1.0 01:PC-04-MJ	0.00	0.00	0:00	0.00	0.00	
06852	SUM	+ 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	
06853	SUM	+ 1.0 01:PC-04-MJ	12.87	1.806	28:01	45.83	0.00	
06854	CONTINUOUS STANDHYD	1.0 01:PC-04	12.87	1.806	28:01	45.83	7.08	
06855	[XMP= 64(TIMP= 64)]							
06856	[Horizon parameters] Fw= 76.20(Fc= 13.20							





07481# [Previous area Ipaer= 4.675LPP1.00LDP= 40.IMP=250:SCP= 0]
07482# [Impervious area Ipaer= 1.575LPI1.00LGI= 146.IMP= 013:SCI= 0]
07483# [ISaerClap= 4.00: IASaerP= 4.00]
07484# [SMIN= 31.81: SMAX=225.41: SK= 010]
07485# ROD01:CO0394-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07486# COMPUTE DUALHYD 1.0 01:AI3 3.29 .376 No.Date 28:00 41.19 n/a .000
07487# Major System / 1.0 01:AI3-MJ 3.29 .000 No.Date 0:00 .00 n/a .000
07488# Minor System \ 1.0 01:AI3-MN 3.29 .064 No.Date 27:00 41.22 n/a .000
07489# [MjSysStor=.5949E+03, TotOccVol=.0000E+00, N-Ofv= 0, TotDurOfv= 0 hrs]
07490# ROD01:CO0350-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07491# CONTINUOUS STANDHYD 1.0 01:AI3-LAND 32.50 3.367 No.Date 28:02 41.86 .647 .000
07492# [XIMP= 50:TIMP= 50]
07493# [LOGS= 2 C/M= 75.0]
07494# [Impervious area Ipaer= 4.675LPP1.00LDP= 40.IMP=250:SCP= 0]
07495# [ISaerClap= 4.00: IASaerP= 4.00]
07496# [SMIN= 36.67: SMAX=244.49: SK= 010]
07497# ROD01:CO0351-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07498# COMPUTE DUALHYD 1.0 01:AI3-LAND 32.50 3.367 No.Date 28:02 41.86 n/a .000
07499# Major System / 1.0 01:AI3-LAND-MJ 3.29 .000 No.Date 0:00 .00 n/a .000
07500# Minor System \ 1.0 01:AI3-LAND-MN 3.29 .064 No.Date 27:00 41.89 n/a .000
07501# [MjSysStor=.5949E+03, TotOccVol=.0000E+00, N-Ofv= 0, TotDurOfv= 0 hrs]
07502# ROD01:CO0352-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07503# ADD HYD 1.0 01:AI3-RM 3.29 .064 No.Date 0:00 .00 n/a .000
07504# + 1.0 01:AI3-LAND-MJ 3.29 .064 No.Date 0:00 .00 n/a .000
07505# + 1.0 01:AI3-LAND-MN 3.29 .064 No.Date 0:00 .00 n/a .000
07506# + 1.0 01:AI3-MJ 3.29 .064 No.Date 27:00 41.22 n/a .000
07507# + 1.0 01:AI3-MN 3.29 .064 No.Date 27:00 41.22 n/a .000
07508# + 1.0 01:AI3-MJ-86 3.29 .064 No.Date 0:00 .00 n/a .000
07509# + 1.0 01:AI3-MN-86 3.29 .064 No.Date 0:00 .00 n/a .000
07510# ROD01:CO0353-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07511# COMPUTE DUALHYD 1.0 01:AI3-RTEADM 3.29 .064 No.Date 27:00 41.22 n/a .000
07512# Major System / 1.0 01:AI3-RM 3.29 .064 No.Date 0:00 .00 n/a .000
07513# Minor System \ 1.0 01:AI3-RM 3.29 .064 No.Date 27:00 41.22 n/a .000
07514# [MjSysStor=.5949E+03, TotOccVol=.0000E+00, N-Ofv= 0, TotDurOfv= 0 hrs]
07515# ROD01:CO0354-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07516# ROUTE PIPE -> 1.0 01:AI3-MJ-106 106.90 3.008 No.Date 28:05 41.72 n/a .000
07517# [RTEP= 1.00] out<= 1.0 01:AI3-106A 106.90 3.008 No.Date 28:12 41.72 n/a .000
07518# [L/S= 1.00] [Dmax= 1.80]
07519# [Vmax= 1.57] [Dused= 1.80]
07520# [Din= 1.80] [Dused= 1.80]
07521# ROD01:CO0355-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07522# ADD HYD 1.0 01:AI3-106A 106.90 3.006 No.Date 28:12 41.72 n/a .000
07523# + 1.0 01:AI3-106A 106.90 3.006 No.Date 28:12 41.72 n/a .000
07524# + 1.0 01:AI3-MJ 3.29 .064 No.Date 27:00 41.22 n/a .000
07525# + 1.0 01:AI3-MN 3.29 .064 No.Date 27:00 41.22 n/a .000
07526# + 1.0 01:AI3-MJ-86 117.38 3.698 No.Date 28:11 41.68 n/a .000
07527# + 1.0 01:AI3-MN-86 117.38 3.698 No.Date 28:11 41.68 n/a .000
07528# ROD01:CO0356-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07529# SAVE HYD 1.0 01:AI3-106A 117.38 3.698 No.Date 28:11 41.68 n/a .000
07530# name: MH106A.0010
07531# remark:Total Flows at MH106A
07532# ROD01:CO0357-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07533# ROUTE PIPE -> 1.0 01:AI3-106A 117.38 3.698 No.Date 28:11 41.68 n/a .000
07534# [RTEP= 1.00] out<= 1.0 01:AI3-106A 117.38 3.698 No.Date 28:06 41.68 n/a .000
07535# [L/S= 1.00] [Dmax= 1.80]
07536# [Vmax= 1.57] [Dused= 1.80]
07537# [Din= 1.80] [Dused= 1.80]
07538# ROD01:CO0358-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07539# CONTINUOUS STANDHYD 1.0 01:AI3 2.44 .365 No.Date 28:00 51.11 .790 .000
07540# [XIMP= 71:TIMP= 71]
07541# [LOGS= 2 C/M= 75.0]
07542# [Impervious area Ipaer= 4.675LPP1.00LDP= 40.IMP=250:SCP= 0]
07543# [ISaerClap= 4.00: IASaerP= 4.00]
07544# [SMIN= 33.81: SMAX=225.41: SK= 010]
07545# ROD01:CO0359-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07546# COMPUTE DUALHYD 1.0 01:AI3 2.44 .365 No.Date 28:00 51.11 n/a .000
07547# Major System / 1.0 01:AI3-MJ 2.44 .000 No.Date 0:00 .00 n/a .000
07548# Minor System \ 1.0 01:AI3-MN 2.44 .365 No.Date 28:00 51.11 n/a .000
07549# [MjSysStor=.4172E+02, TotOccVol=.0000E+00, N-Ofv= 0, TotDurOfv= 0 hrs]
07550# ROD01:CO0360-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07551# ADD HYD 1.0 01:AI3-106 117.38 3.698 No.Date 28:12 41.68 n/a .000
07552# + 1.0 01:AI3-MJ 2.44 .365 No.Date 28:00 51.11 n/a .000
07553# + 1.0 01:AI3-MN 2.44 .365 No.Date 28:00 51.11 n/a .000
07554# ROD01:CO0361-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07555# SAVE HYD 1.0 01:AI3-106 117.38 3.698 No.Date 28:12 41.68 n/a .000
07556# name: MH106.0010
07557# remark:Total Flows at MH106
07558# ROD01:CO0362-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07559# ROUTE PIPE -> 1.0 01:AI3-106 119.82 3.992 No.Date 28:02 41.87 n/a .000
07560# [RTEP= 1.00] out<= 1.0 01:AI3-107 119.82 3.992 No.Date 28:03 41.87 n/a .000
07561# [L/S= 1.00] [Dmax= 1.80]
07562# [Vmax= 1.66] [Dused= 1.80]
07563# [Din= 1.80] [Dused= 1.80]
07564# ROD01:CO0363-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07565# CONTINUOUS STANDHYD 1.0 01:AI3 4.14 .416 No.Date 28:01 38.46 .595 .000
07566# [XIMP= 35:TIMP= 47]
07567# [LOGS= 2 C/M= 75.0]
07568# [Impervious area Ipaer= 4.675LPP1.00LDP= 40.IMP=250:SCP= 0]
07569# [ISaerClap= 4.00: IASaerP= 4.00]
07570# [SMIN= 31.81: SMAX=225.41: SK= 010]
07571# ROD01:CO0364-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07572# COMPUTE DUALHYD 1.0 01:AI3 4.14 .416 No.Date 28:01 38.46 n/a .000
07573# Major System / 1.0 01:AI3-MJ 4.14 .000 No.Date 0:00 .00 n/a .000
07574# Minor System \ 1.0 01:AI3-MN 4.14 .416 No.Date 28:00 38.48 n/a .000
07575# [MjSysStor=.4172E+02, TotOccVol=.0000E+00, N-Ofv= 0, TotDurOfv= 0 hrs]
07576# ROD01:CO0365-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07577# CONTINUOUS STANDHYD 1.0 01:AI3 10.61 1.251 No.Date 28:01 45.36 .701 .000
07578# [XIMP= 53:TIMP= 62]
07579# [LOGS= 2 C/M= 75.0]
07580# [Impervious area Ipaer= 4.675LPP1.00LDP= 40.IMP=250:SCP= 0]
07581# [ISaerClap= 4.00: IASaerP= 4.00]
07582# [SMIN= 31.81: SMAX=225.41: SK= 010]
07583# ROD01:CO0366-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07584# COMPUTE DUALHYD 1.0 01:AI3 10.61 1.251 No.Date 28:01 45.36 n/a .000
07585# Major System / 1.0 01:AI3-MJ 10.61 .000 No.Date 0:00 .00 n/a .000
07586# Minor System \ 1.0 01:AI3-MN 10.61 .993 No.Date 27:00 45.38 n/a .000
07587# [MjSysStor=.4172E+02, TotOccVol=.0000E+00, N-Ofv= 0, TotDurOfv= 0 hrs]
07588# ROD01:CO0367-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07589# ADD HYD 1.0 01:AI3-107 134.57 5.265 No.Date 28:03 42.04 n/a .000
07590# + 1.0 01:AI3-108 134.57 5.265 No.Date 27:00 42.04 n/a .000
07591# + 1.0 01:AI3-MJ 10.61 .993 No.Date 27:00 45.38 n/a .000
07592# + 1.0 01:AI3-MN 10.61 .993 No.Date 27:00 45.38 n/a .000
07593# ROD01:CO0368-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07594# SAVE HYD 1.0 01:AI3-107 134.57 5.265 No.Date 28:03 42.04 n/a .000
07595# name: MH107.0010
07596# remark:Total Flows at MH107
07597# ROD01:CO0369-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07598# ROUTE PIPE -> 1.0 01:AI3-107 134.57 5.265 No.Date 28:03 42.04 n/a .000
07599# [RTEP= 1.00] out<= 1.0 01:AI3-107-119 134.57 5.265 No.Date 28:03 42.04 n/a .000
07600# [L/S= 1.00] [Dmax= 1.80]
07601# [Vmax= 1.14] [Dused= 2.00]
07602# [Din= 1.80] [Dused= 2.00]
07603# ROD01:CO0370-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07604# ROUTE PIPE -> 1.0 01:AI3-119 134.57 5.248 No.Date 28:06 42.04 n/a .000
07605# [RTEP= 1.00] out<= 1.0 01:AI3-119-108 134.57 5.248 No.Date 28:06 42.04 n/a .000
07606# [L/S= 1.00] [Dmax= 1.639]
07607# [Vmax= 1.91] [Dused= 2.00]
07608# [Din= 1.80] [Dused= 2.00]
07609# ROD01:CO0371-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07610# CONTINUOUS STANDHYD 1.0 01:AI3 12.29 1.385 No.Date 28:01 41.19 .637 .000
07611# [XIMP= 41:TIMP= 54]
07612# [LOGS= 2 C/M= 75.0]
07613# [Impervious area Ipaer= 4.675LPP1.00LDP= 40.IMP=250:SCP= 0]
07614# [ISaerClap= 4.00: IASaerP= 4.00]
07615# [SMIN= 31.81: SMAX=225.41: SK= 010]
07616# ROD01:CO0372-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07617# COMPUTE DUALHYD 1.0 01:AI3 12.29 1.385 No.Date 28:01 41.19 n/a .000
07618# Major System / 1.0 01:AI3-MJ 12.29 .000 No.Date 0:00 .00 n/a .000
07619# Minor System \ 1.0 01:AI3-MN 12.29 1.029 No.Date 27:00 41.24 n/a .000
07620# [MjSysStor=.1401E+03, TotOccVol=.0000E+00, N-Ofv= 0, TotDurOfv= 0 hrs]
07621# ROD01:CO0373-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07622# CONTINUOUS STANDHYD 1.0 01:AI3 2.99 .568 No.Date 28:01 51.11 .790 .000
07623# [XIMP= 71:TIMP= 71]
07624# [LOGS= 2 C/M= 75.0]
07625# [Impervious area Ipaer= 4.675LPP1.00LDP= 40.IMP=250:SCP= 0]
07626# [ISaerClap= 4.00: IASaerP= 4.00]
07627# [SMIN= 33.81: SMAX=225.41: SK= 010]
07628# ROD01:CO0374-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07629# COMPUTE DUALHYD 1.0 01:AI3 2.99 .368 No.Date 28:01 51.11 n/a .000
07630# Major System / 1.0 01:AI3-MJ 2.99 .000 No.Date 0:00 .00 n/a .000
07631# Minor System \ 1.0 01:AI3-MN 2.99 .368 No.Date 28:01 51.11 n/a .000
07632# [MjSysStor=.1401E+03, TotOccVol=.0000E+00, N-Ofv= 0, TotDurOfv= 0 hrs]
07633# ROD01:CO0375-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07634# CONTINUOUS STANDHYD 1.0 01:AI3-Block 2.94 .369 No.Date 28:00 48.90 .601 .000
07635# [XIMP= 41:TIMP= 41]
07636# [LOGS= 2 C/M= 75.0]
07637# [Impervious area Ipaer= 4.675LPP1.00LDP= 40.IMP=250:SCP= 0]
07638# [ISaerClap= 4.00: IASaerP= 4.00]
07639# [SMIN= 33.81: SMAX=225.41: SK= 010]
07640# ROD01:CO0376-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07641# COMPUTE DUALHYD 1.0 01:AI3 2.94 .368 No.Date 28:01 51.11 n/a .000
07642# Major System / 1.0 01:AI3-MJ 2.94 .000 No.Date 0:00 .00 n/a .000
07643# Minor System \ 1.0 01:AI3-MN 2.94 .368 No.Date 28:01 51.11 n/a .000
07644# [MjSysStor=.1401E+03, TotOccVol=.0000E+00, N-Ofv= 0, TotDurOfv= 0 hrs]
07645# ROD01:CO0377-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07646# SAVE HYD 1.0 01:AI3-Block 2.94 .369 No.Date 28:04 42.14 n/a .000
07647# name: MH108.0010
07648# remark:Total Flows at MH108
07649# ROD01:CO0378-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07650# ROUTE PIPE -> 1.0 01:AI3-Block 149.45 6.990 No.Date 28:04 42.14 n/a .000
07651# [RTEP= 1.00] out<= 1.0 01:AI3-116 149.45 6.990 No.Date 28:05 42.14 n/a .000
07652# [L/S= 71.7] [Dmax= 1.75]
07653# [Vmax= 2.08] [Dused= 1.75]
07654# [Din= 1.80] [Dused= 1.75]
07655# ROD01:CO0379-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07656# ROUTE PIPE -> 1.0 01:AI3-Block 149.45 6.990 No.Date 28:04 42.14 n/a .000
07657# [RTEP= 1.00] out<= 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 38.90 n/a .000
07658# [L/S= 80.] [Dmax= 2.14]
07659# [Vmax= 1.84] [Dused= 2.14]
07660# [Din= 1.80] [Dused= 2.14]
07661# ROD01:CO0380-----DRAIN-ID-NHYD-----AREHA-OPEARCS-TpeakDate\_hh:mm-----RVM-R-C-----DWFCMS
07662# ADD HYD 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07663# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:00 38.90 n/a .000
07664# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07665# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07666# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07667# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07668# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07669# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07670# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07671# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07672# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07673# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07674# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07675# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07676# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07677# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07678# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07679# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07680# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07681# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07682# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07683# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07684# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07685# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07686# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07687# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07688# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07689# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07690# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07691# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07692# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07693# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07694# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07695# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07696# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07697# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07698# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07699# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07700# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07701# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07702# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07703# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07704# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07705# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07706# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07707# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07708# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07709# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07710# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07711# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07712# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07713# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07714# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07715# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07716# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07717# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07718# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07719# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07720# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07721# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07722# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07723# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07724# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07725# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07726# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07727# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07728# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07729# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07730# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07731# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07732# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07733# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07734# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07735# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07736# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07737# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07738# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07739# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07740# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07741# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07742# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07743# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07744# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07745# + 1.0 01:AI3-Block 149.45 6.990 No.Date 28:06 42.14 n/a .000
07746# + 1.0 01:AI3

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07855 # License # 254923
07856 *****
07857 # CALIBRATION OF SUMMER MODEL PARAMETERS
07858 # USING CONTINUOUS SIMULATIONS
07859 # Rainfall data from JFSA raingauge installed at site + other gauges by the City
07860 # Use data collected from May 1st to July 14, 2003
07861 # 2021-11-30 change TMRSD to COMPOSITE POLYMER (TMRSD = 0.1 instead of 0.0001)
07862 # 2021-11-01 correct pond curve values
07863 # 2020-11-01 change W_Clar_Break_XSD to 0.55, SLP1=[0.51] (impermeable slope), and LUT up to 700m
07864 # 2021-02-19 Change the slope for ROUTE CHANNEL Station 2462 (INVDout="N_TO", INVDin="SM_TO") from 0.033 t (as per S
07865 # 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (INVDout="R_MC", INVDin="SH_CK") from 0.01 t (as per S
07866 #
07867 R0225=C0002-----
07868 # HEAD STORM
07869 # Filename = storm.001
07870 # Comment = Pluie RCS de 24 heures 1125 ans pour Ottawa CDA
07871 # [SDT=10.00;SDCR= 24.00;POT= 74.39]
07872 R0225=C0003-----
07873 # MODIFY STORM
07874 # [SFACT= 1.00;TRHPT= 960.00 min]
07875 # [CMT=10.00;SDCR= 24.00;POT= 74.39]
07876 R0225=C0004-----
07877 # SPECIAL VALUES
07878 # Filename = T:\PROJ\1474\6\Design\2020\1026-QuantityControlAnalysis\SHMHO\SMS-Model\Updated\CltiDate.DEP
07879 # ICRSDev = 1 (read and print data)
07880 # FileTitle file comment: Based on various calibration exercises in Osta
07881 # THE FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDARD COM
07882 # Horton's infiltration equation parameters:
07883 # [Fw= 76.20 mm/hr] [Fw1=1.20 mm/hr] [DCAV= 4.14 hr] [P= .00 mm]
07884 # Parameters for IMPERVIOUS surfaces in STANDARD:
07885 # [Intr= 4.67 mm] [SDF=50.00 m] [DPR= .250]
07886 # Parameters for PERVIOUS surfaces in STANDARD:
07887 # [Intr= 1.87 mm] [CMT= 1.50] [DPR= .253]
07888 # Parameters used in NASHVD:
07889 # [a= 1.67 mm] [n= 1.00]
07890 # Average monthly pan Evaporation data in (mm)
07891 # JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
07892 # .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
07893 # Average monthly Potential Transpiration in (mm)
07894 # JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
07895 # .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
07896 # JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
07897 # .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
07898 R0225=C0005-----
07899 # COMPUTE API
07900 # [API=1.50.00; APIkty= .8500; APIktr= .998]
07901 # [APIktr=0.76; APIkty= 44.87]
07902 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
07903 # of 3.32
07904 R0225=C0006-----
07905 # CONTINUOUS NASHVD 1.0 01;SH_13 971.00 5.778_NashDate 32:34 24.02 233.000
07906 # [CMT= 61.0; N= 3.00; Tp= 1.13]
07907 # [IAREC= 4.00; SMIN= 33.00; SMAX=380.32; SK= .010]
07908 # [InterEventTime= 12.00]
07909 #
07910 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
07911 # of 3.32
07912 R0225=C0007-----
07913 # CONTINUOUS NASHVD 1.0 01;SH_13 971.00 5.778_NashDate 32:34 24.02 233.000
07914 # [CMT= 61.0; N= 3.00; Tp= 1.13]
07915 # [IAREC= 4.00; SMIN= 33.00; SMAX=430.01; SK= .010]
07916 # [InterEventTime= 12.00]
07917 #
07918 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
07919 # of 3.32
07920 R0225=C0008-----
07921 # CONTINUOUS NASHVD 1.0 01;SH_13 971.00 5.778_NashDate 32:34 24.02 233.000
07922 # [CMT= 61.0; N= 3.00; Tp= 1.13]
07923 # [IAREC= 4.00; SMIN= 33.24; SMAX=554.96; SK= .010]
07924 # [InterEventTime= 12.00]
07925 R0225=C0009-----
07926 # CONTINUOUS NASHVD 1.0 01;SH_10 5666.00 27.457_NashDate 37:54 31.50 423.000
07927 # [CMT= 72.0; N= 3.00; Tp= 3.91]
07928 # [IAREC= 4.00; SMIN= 39.75; SMAX=264.99; SK= .010]
07929 # [InterEventTime= 12.00]
07930 R0225=C0010-----
07931 # CONTINUOUS NASHVD 1.0 01;SH_10 5666.00 27.457_NashDate 37:54 31.50 423.000
07932 # [CMT= 66.0; N= 3.00; Tp= 1.24]
07933 # [IAREC= 4.00; SMIN= 52.62; SMAX=350.79; SK= .010]
07934 # [InterEventTime= 12.00]
07935 #
07936 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
07937 # of 3.32
07938 R0225=C0011-----
07939 # CONTINUOUS NASHVD 1.0 01;SH_10 5666.00 27.457_NashDate 37:54 31.50 423.000
07940 # [CMT= 66.0; N= 3.00; Tp= 1.24]
07941 # [IAREC= 4.00; SMIN= 52.62; SMAX=350.79; SK= .010]
07942 # [InterEventTime= 12.00]
07943 #
07944 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
07945 # of 3.32
07946 R0225=C0012-----
07947 # CONTINUOUS NASHVD 1.0 01;SH_10 5666.00 27.457_NashDate 37:54 31.50 423.000
07948 # [CMT= 72.0; N= 3.00; Tp= 3.91]
07949 # [IAREC= 4.00; SMIN= 39.75; SMAX=264.99; SK= .010]
07950 # [InterEventTime= 12.00]
07951 #
07952 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
07953 # of 3.75
07954 R0225=C0013-----
07955 # CONTINUOUS NASHVD 1.0 01;SH_10 5666.00 27.457_NashDate 37:54 31.50 423.000
07956 # [CMT= 66.0; N= 3.00; Tp= 1.16]
07957 # [IAREC= 4.00; SMIN= 52.62; SMAX=350.79; SK= .010]
07958 # [InterEventTime= 12.00]
07959 #
07960 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
07961 # of 3.68
07962 R0225=C0014-----
07963 # CONTINUOUS NASHVD 1.0 01;SH_9 1132.00 11.752_NashDate 30:54 30.18 406.000
07964 # [CMT= 72.0; N= 3.00; Tp= 4.00]
07965 # [IAREC= 4.00; SMIN= 41.07; SMAX=287.10; SK= .010]
07966 # [InterEventTime= 12.00]
07967 #
07968 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
07969 # of 3.62
07970 R0225=C0015-----
07971 # CONTINUOUS NASHVD 1.0 01;SH_9 1132.00 11.752_NashDate 30:54 30.18 406.000
07972 # [CMT= 62.0; N= 3.00; Tp= 1.32]
07973 # [IAREC= 4.00; SMIN= 61.90; SMAX=412.66; SK= .010]
07974 # [InterEventTime= 12.00]
07975 #
07976 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
07977 # of 3.60
07978 R0225=C0016-----
07979 # CONTINUOUS NASHVD 1.0 01;SH_8 131.00 2.266_NashDate 28:57 25.20 339.000
07980 # [CMT= 61.0; N= 3.00; Tp= .90]
07981 # [IAREC= 4.00; SMIN= 59.42; SMAX=396.11; SK= .010]
07982 # [InterEventTime= 12.00]
07983 #
07984 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
07985 # of 3.45
07986 R0225=C0017-----
07987 # CONTINUOUS NASHVD 1.0 01;SH_8R 3854.00 15.333_NashDate 38:34 27.01 363.000
07988 # [CMT= 66.0; N= 3.00; Tp= 1.81]
07989 # [IAREC= 4.00; SMIN= 52.62; SMAX=350.79; SK= .010]
07990 # [InterEventTime= 12.00]
07991 #
07992 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
07993 # of 3.42
07994 R0225=C0018-----
07995 # CONTINUOUS NASHVD 1.0 01;SH_8R 3854.00 15.333_NashDate 38:34 27.01 363.000
07996 # [CMT= 77.0; N= 3.00; Tp= 6.65]
07997 # [IAREC= 4.00; SMIN= 76.32; SMAX=508.81; SK= .010]
07998 # [InterEventTime= 12.00]
07999 #
08000 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
08001 # of 3.79
08002 R0225=C0019-----
08003 # CONTINUOUS NASHVD 1.0 01;SH_6 165.00 1.076_NashDate 33:03 27.63 371.000
08004 # [CMT= 67.0; N= 3.00; Tp= 1.81]
08005 # [IAREC= 4.00; SMIN= 50.55; SMAX=336.97; SK= .010]
08006 # [InterEventTime= 12.00]
08007 #
08008 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
08009 # of 4.41
08010 R0225=C0020-----
08011 # CONTINUOUS NASHVD 1.0 01;SH_6R 1332.00 7.882_NashDate 35:14 31.50 423.000
08012 # [CMT= 72.0; N= 3.00; Tp= 8.95]
08013 # [IAREC= 4.00; SMIN= 39.75; SMAX=264.99; SK= .010]
08014 # [InterEventTime= 12.00]
08015 R0225=C0021-----
08016 # CONTINUOUS NASHVD 1.0 01;SH_5 224.00 6.892_NashDate 28:45 35.66 479.000
08017 # [CMT= 77.0; N= 3.00; Tp= 1.00]
08018 # [IAREC= 4.00; SMIN= 31.15; SMAX=207.66; SK= .010]
08019 # [InterEventTime= 12.00]
08020 #
08021 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
08022 # of 3.20
08023 R0225=C0022-----
08024 # CONTINUOUS NASHVD 1.0 01;SH_5R 4945.00 17.464_NashDate 33:18 32.85 442.000
08025 # [CMT= 74.0; N= 3.00; Tp= 4.45]
08026 # [IAREC= 4.00; SMIN= 31.81; SMAX=225.43; SK= .010]
08027 # [InterEventTime= 12.00]
08028 R0225=C0023-----
08029 # CONTINUOUS NASHVD 1.0 01;SH_5A2 20.00 .798_NashDate 28:35 39.36 529.000
08030 # [CMT= 81.0; N= 3.00; Tp= .62]
08031 # [IAREC= 4.00; SMIN= 25.21; SMAX=168.09; SK= .010]
08032 # [InterEventTime= 12.00]
08033 #
08034 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
08035 # of 3.64
08036 R0225=C0024-----
08037 # CONTINUOUS NASHVD 1.0 01;SH_5A1 1422.00 7.480_NashDate 37:50 34.24 460.000
08038 # [CMT= 76.0; N= 3.00; Tp= 1.81]
08039 # [IAREC= 4.00; SMIN= 31.81; SMAX=225.43; SK= .010]
08040 # [InterEventTime= 12.00]
08041 R0225=C0025-----
08042 # CONTINUOUS NASHVD 1.0 01;SH_4 585.00 10.942_NashDate 29:56 39.36 529.000

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082229 ROUTES CO00051-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082230 ROUTE RESERVOIR -> 1.0 02:RES\_P 38743.00 86.333 No.Date 44:08 26.55 n/a .000
082231 out <= 1.0 01:RES\_FP 38743.00 42.032 No.Date 60:05 26.55 n/a .000
082232 [L/S= 3066./ .047/.035]
082233 ROUTES CO00052-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082234 SAVE HYD 1.0 01:RES\_FP 38743.00 42.032 No.Date 60:05 26.55 n/a .000
082235 fname\_H\_ResRF
082236 remark:outflow of Richmond Pen
082237 #
082238 # Sum of hydrographs from Node 7 routed to Node 6
082239 # Section 5
082240
082241 ROUTES CO00053-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082242 ROUTE CHANNEL -> 1.0 02:RES\_P 38743.00 42.032 No.Date 60:05 26.55 n/a .000
082243 [RPT= 1.00] out<= 1.0 01:RES 38743.00 41.826 No.Date 61:26 26.55 n/a .000
082244 [L/S= 3066./ .047/.035]
082245 [Vmax= .514]Dmax= 1.120]
082246 #
082247 # Addition of Subwatershed 6 and Van Gaal Drain to Node 6
082248 #
082249 ROUTES CO00054-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082250 ADD HYD + 1.0 02:RES 38743.00 41.826 No.Date 61:26 26.55 n/a .000
082251 + 1.0 02:RES\_S2 155.00 1.076 No.Date 33:03 27.63 n/a .000
082252 + 1.0 02:VLR\_DR 1332.00 7.882 No.Date 35:14 31.50 n/a .000
082253 SUM= 1.0 01:RES\_M6 40240.01 41.832 No.Date 61:20 26.72 n/a .000
082254 #
082255 # Sum of hydrographs from Node 6 routed to Node 5
082256 # Section 6
082257 #
082258 ROUTES CO00055-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082259 ROUTE CHANNEL -> 1.0 02:RES\_M 40240.01 41.832 No.Date 61:20 26.72 n/a .000
082260 [RPT= 1.00] out<= 1.0 01:RES 40240.01 41.717 No.Date 62:14 26.72 n/a .000
082261 [L/S= 1892./ .057/.035]
082262 [Vmax= .444]Dmax= 1.222]
082263 #
082264 # Addition of Subwatershed 5 and Flowing Creek to Node 5
082265 #
082266 ROUTES CO00056-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082267 ADD HYD + 1.0 02:RES 40240.01 41.717 No.Date 62:14 26.72 n/a .000
082268 + 1.0 02:RES\_S 224.00 6.892 No.Date 28:45 35.66 n/a .000
082269 + 1.0 02:RES\_S1 1612.00 7.480 No.Date 37:50 34.24 n/a .000
082270 SUM= 1.0 01:RES\_M5 45409.01 62.634 No.Date 34:27 27.43 n/a .000
082271 #
082272 # Sum of hydrographs from Node 5 routed to Node 5A
082273 # Section 7
082274 #
082275 ROUTES CO00057-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082276 ROUTE CHANNEL -> 1.0 02:RES\_M 45409.01 62.634 No.Date 34:27 27.43 n/a .000
082277 [RPT= 1.00] out<= 1.0 01:RES 45409.01 62.487 No.Date 34:43 27.43 n/a .000
082278 [L/S= 1892./ .097/.035]
082279 [Vmax= .511]Dmax= 1.222]
082280 #
082281 # Addition of Subwatershed S1 and Subwatershed S2 to Node 5A
082282 #
082283 ROUTES CO00058-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082284 ADD HYD + 1.0 02:RES 45409.01 62.487 No.Date 34:43 27.43 n/a .000
082285 + 1.0 02:RES\_S2 20.00 1.788 No.Date 28:35 39.36 n/a .000
082286 + 1.0 02:RES\_S1 1612.00 7.480 No.Date 37:50 34.24 n/a .000
082287 SUM= 1.0 01:RES\_M5 46441.01 69.334 No.Date 35:01 27.64 n/a .000
082288 #
082289 # Sum of hydrographs from Node 5A routed to Node 4
082290 # Section 8
082291 #
082292 ROUTES CO00059-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082293 ROUTE CHANNEL -> 1.0 02:RES\_M 46441.01 69.334 No.Date 35:01 27.64 n/a .000
082294 [RPT= 1.00] out<= 1.0 01:RES 46441.01 66.496 No.Date 36:27 27.64 n/a .000
082295 [L/S= 4630./ .041/.035]
082296 [Vmax= .840]Dmax= 3.530]
082297 #
082298 # Addition of Subwatershed 4 and Leamy Creek to Node 4
082299 #
082300 ROUTES CO00060-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082301 ADD HYD + 1.0 02:RES 46441.01 66.496 No.Date 36:27 27.64 n/a .000
082302 + 1.0 02:RES\_S 1885.00 10.942 No.Date 29:56 39.36 n/a .000
082303 + 1.0 02:RES\_S1 1021.00 14.476 No.Date 30:46 38.60 n/a .000
082304 SUM= 1.0 01:RES\_M 48447.01 73.819 No.Date 35:41 28.02 n/a .000
082305 ROUTES CO00061-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082306 SAVE HYD 1.0 01:RES\_M 48447.01 73.819 No.Date 35:41 28.02 n/a .000
082307 fname\_S\_M\_0025
082308 remark:flow at S\_M
082309 #
082310 # Sum of hydrographs from Node 4 routed to Node 2
082311 # Section 9
082312 #
082313 ROUTES CO00062-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082314 ROUTE CHANNEL -> 1.0 02:RES\_M 48447.01 73.819 No.Date 35:41 28.02 n/a .000
082315 [RPT= 1.00] out<= 1.0 01:RES 48447.01 73.485 No.Date 35:42 28.02 n/a .000
082316 [L/S= 1677./ .067/.035]
082317 [Vmax= .874]Dmax= 3.970]
082318 #
082319 # Addition of Subwatershed 2 with Monahan Drain and Smith Drain to Node 2
082320 #
082321 ROUTES CO00063-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082322 ADD HYD + 1.0 02:RES 48447.01 73.485 No.Date 35:42 28.02 n/a .000
082323 + 1.0 02:RES\_S 177.00 5.438 No.Date 28:45 35.66 n/a .000
082324 + 1.0 02:RES\_S1 1122.00 13.229 No.Date 31:45 39.36 n/a .000
082325 SUM= 1.0 01:RES\_M 50446.01 82.153 No.Date 34:41 28.02 n/a .000
082326 + 1.0 01:RES\_S2 52483.00 106.109 No.Date 33:07 28.64 n/a .000
082327 ROUTES CO00064-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082328 SAVE HYD 1.0 01:RES\_M 50446.01 106.109 No.Date 33:07 28.64 n/a .000
082329 fname\_H\_S2
082330 remark:total flow at R\_NJ Joek River Gauge at Moodle Dr
082331 #
082332 # Sum of hydrographs from Node 2 routed to Node 1
082333 # Section 10
082334 #
082335 ROUTES CO00065-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082336 ROUTE CHANNEL -> 1.0 02:RES\_M 50446.01 106.109 No.Date 33:07 28.64 n/a .000
082337 [RPT= 1.00] out<= 1.0 01:RES 50446.01 103.234 No.Date 34:03 28.64 n/a .000
082338 [L/S= 2327./ .057/.055]
082339 [Vmax= 1.568]Dmax= 2.111]
082340 #
082341 # Catchment SW-1a
082342 #
082343 # Position of RWCA catchment SW-1 outside of Reach 1 subwatershed
082344 # Undeveloped agricultural land
082345 #
082346 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082347 [CM= 72.0] N= 3.00] T= 2.79]
082348 [IAREC= 4.00] SMIN= 39.75] SMAX= 264.99] SK= .010]
082349 #
082350 ROUTES CO00067-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082351 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082352 [CM= 72.0] N= 3.00] T= 1.05]
082353 [IAREC= 4.00] SMIN= 31.15] SMAX= 207.66] SK= .010]
082354 #
082355 ROUTES CO00068-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082356 ADD HYD + 1.0 02:RES\_M 52483.00 106.109 No.Date 33:07 28.64 n/a .000
082357 + 1.0 02:RES\_S 536.42 5.154 No.Date 31:16 30.13 n/a .000
082358 + 1.0 02:RES\_S1 46.92 1.029 No.Date 29:07 34.14 459 .000
082359 SUM= 1.0 01:RES\_M 53064.36 107.224 No.Date 33:26 28.64 n/a .000
082360 #
082361 ROUTES CO00069-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082362 SAVE HYD 1.0 01:RES\_M 53064.36 107.224 No.Date 33:26 28.64 n/a .000
082363 fname\_S\_M\_416\_0025
082364 remark:total flow at Highway 416
082365 #
082366 # Hydrograph from Node 416 routed to Node 416
082367 # Channel X-Section obtained from RWCA Hydraulic Model - Station 9025
082368 #
082369 ROUTES CO00070-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082370 ROUTE CHANNEL -> 1.0 02:RES\_M 53064.36 107.224 No.Date 33:26 28.64 n/a .000
082371 [RPT= 1.00] out<= 1.0 01:RES 53064.36 107.200 No.Date 33:50 28.64 n/a .000
082372 [L/S= 497./ .302/.055]
082373 [Vmax= 1.568]Dmax= 2.111]
082374 #
082375 # Catchment OKEFEF
082376 #
082377 # 20-D-02 keefe drain (north of the Joek)
082378 #
082379 # 20-D-11 keefe drain (south of the Joek)
082380 #
082381 # 20-D-12 keefe drain (east of the Joek)
082382 #
082383 # 20-D-11-20 keefe drain (detailed model was added as per the NOVATEC SWMGMO model (Cili-Date 2014).
082384 #
082385 ROUTES CO00071-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082386 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082387 [CM= 61.0] N= 3.00] T= 1.00]
082388 [IAREC= 4.00] SMIN= 64.50] SMAX= 430.01] SK= .010]
082389 [InterEventTime= 12.00]
082390 ROUTES CO00072-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082391 ROUTE CHANNEL -> 1.0 02:RES\_M 63.72 .937 No.Date 28:58 22.21 n/a .000
082392 [RPT= 1.00] out<= 1.0 01:RES 63.72 .877 No.Date 29:15 22.21 n/a .000
082393 [L/S= 860./ .630/.043]
082394 #
082395 ROUTES CO00073-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082396 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082397 [CM= 61.0] N= 3.00] T= 1.00]
082398 [IAREC= 4.00] SMIN= 76.32] SMAX= 508.81] SK= .010]
082399 [InterEventTime= 12.00]
082400 ROUTES CO00074-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082401 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082402 [CM= 49.0] N= 3.00] T= .90]
082403 [IAREC= 4.00] SMIN= 104.59] SMAX= 697.25] SK= .010]
082404 #
082405 ROUTES CO00075-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082406 ADD HYD + 1.0 02:RES\_M 63.72 .937 No.Date 28:58 22.21 n/a .000
082407 + 1.0 02:RES\_S 28.61 .330 No.Date 29:13 20.55 n/a .000
082408 + 1.0 02:RES\_S1 46.94 .426 No.Date 29:00 15.62 n/a .000
082409 SUM= 1.0 01:DEF\_N 139.27 1.623 No.Date 29:11 19.65 n/a .000
082410 ROUTES CO00076-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
082411 ROUTE CHANNEL -> 1.0 01:DEF\_N 139.27 1.623 No.Date 29:14 19.65 n/a .000
082412 [RPT= 1.00] out<= 1.0 01:DEF\_N 139.27 1.620 No.Date 29:14 19.65 n/a .000
082413 [L/S= 710./ .047/.035]
082414 [Vmax= .998]Dmax= .685]
082415 #
082416 ROUTES CO00077-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08416 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08417 [CM= 63.0] N= 3.00] T= 1.00]
08418 [IAREC= 4.00] SMIN= 134.47] SMAX= 896.47] SK= .010]
08419 [InterEventTime= 12.00]
08420 ROUTES CO00078-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08421 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08422 [CM= 63.0] N= 3.00] T= 1.00]
08423 [IAREC= 4.00] SMIN= 134.47] SMAX= 896.47] SK= .010]
08424 #
08425 ROUTES CO00079-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08426 ROUTE CHANNEL -> 1.0 02:RES\_P 38743.00 86.333 No.Date 44:08 26.55 n/a .000
08427 [RPT= 1.00] out<= 1.0 01:RES 38743.00 42.032 No.Date 60:05 26.55 n/a .000
08428 [L/S= 3066./ .047/.035]
08429 [Vmax= .514]Dmax= 1.120]
08430 #
08431 ROUTES CO00080-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08432 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08433 [CM= 63.0] N= 3.00] T= 1.00]
08434 [IAREC= 4.00] SMIN= 134.47] SMAX= 896.47] SK= .010]
08435 #
08436 ROUTES CO00081-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08437 ADD HYD + 1.0 02:DEF\_N 139.27 1.620 No.Date 29:14 19.65 n/a .000
08438 + 1.0 02:DEF\_N 28.61 .330 No.Date 29:13 20.55 n/a .000
08439 + 1.0 02:DEF\_N 46.94 .426 No.Date 29:00 15.62 n/a .000
08440 SUM= 1.0 01:DEF\_N 139.27 1.623 No.Date 29:11 19.65 n/a .000
08441 #
08442 ROUTES CO00082-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08443 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08444 [CM= 64.0] N= 3.00] T= .60]
08445 [IAREC= 4.00] SMIN= 21.09] SMAX= 140.62] SK= .010]
08446 [InterEventTime= 12.00]
08447 ROUTES CO00083-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08448 ADD HYD + 1.0 02:DEF\_N 261.31 4.014 No.Date 28:28 21.91 n/a .000
08449 + 1.0 02:DEF\_N 2.50 .117 No.Date 28:22 58.43 n/a .000
08450 + 1.0 02:DEF\_N 1.17 .078 No.Date 28:12 37.38 n/a .000
08451 SUM= 1.0 01:DEF\_N 265.31 4.014 No.Date 28:28 21.91 n/a .000
08452 #
08453 ROUTES CO00084-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08454 ROUTE CHANNEL -> 1.0 02:DEF\_N 261.31 4.014 No.Date 28:28 21.91 n/a .000
08455 [RPT= 1.00] out<= 1.0 01:DEF\_N 261.31 4.014 No.Date 28:28 21.91 n/a .000
08456 [L/S= 302./ 1.000/.043]
08457 [Vmax= 74.0] Dmax= 715]
08458 #
08459 ROUTES CO00085-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08460 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08461 [CM= 84.0] N= 3.00] T= .28]
08462 [IAREC= 4.00] SMIN= 21.09] SMAX= 140.62] SK= .010]
08463 [InterEventTime= 12.00]
08464 ROUTES CO00086-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08465 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08466 [CM= 66.0] N= 3.00] T= .85]
08467 [IAREC= 4.00] SMIN= 21.09] SMAX= 140.62] SK= .010]
08468 [InterEventTime= 12.00]
08469 #
08470 ROUTES CO00087-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08471 ADD HYD + 1.0 02:DEF\_N 261.31 4.014 No.Date 28:28 21.91 n/a .000
08472 + 1.0 02:DEF\_N 2.50 .117 No.Date 28:22 58.43 n/a .000
08473 + 1.0 02:DEF\_N 1.17 .078 No.Date 28:12 37.38 n/a .000
08474 SUM= 1.0 01:DEF\_N 265.31 4.014 No.Date 28:28 21.91 n/a .000
08475 #
08476 ROUTES CO00088-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08477 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08478 [CM= 66.0] N= 3.00] T= .85]
08479 [IAREC= 4.00] SMIN= 21.09] SMAX= 140.62] SK= .010]
08480 [InterEventTime= 12.00]
08481 #
08482 ROUTES CO00089-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08483 ROUTE CHANNEL -> 1.0 02:DEF\_N 261.31 4.014 No.Date 28:28 21.91 n/a .000
08484 [RPT= 1.00] out<= 1.0 01:DEF\_N 261.31 4.014 No.Date 28:28 21.91 n/a .000
08485 [L/S= 335./ 100/.013]
08486 [Vmax= 1.178]Dmax= 540]
08487 [InterEventTime= 12.00]
08488 #
08489 ROUTES CO00090-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08490 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08491 [CM= 69.0] N= 3.00] T= 1.00]
08492 [IAREC= 4.00] SMIN= 21.09] SMAX= 140.62] SK= .010]
08493 [InterEventTime= 12.00]
08494 #
08495 ROUTES CO00091-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08496 ADD HYD + 1.0 02:DEF\_N 261.31 4.014 No.Date 28:28 21.91 n/a .000
08497 + 1.0 02:DEF\_N 2.50 .117 No.Date 28:22 58.43 n/a .000
08498 + 1.0 02:DEF\_N 1.17 .078 No.Date 28:12 37.38 n/a .000
08499 SUM= 1.0 01:DEF\_N 265.31 4.014 No.Date 28:28 21.91 n/a .000
08500 #
08501 ROUTES CO00092-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08502 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08503 [CM= 69.0] N= 3.00] T= 1.00]
08504 [IAREC= 4.00] SMIN= 21.09] SMAX= 140.62] SK= .010]
08505 [InterEventTime= 12.00]
08506 #
08507 ROUTES CO00093-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08508 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08509 [CM= 69.0] N= 3.00] T= 1.00]
08510 [IAREC= 4.00] SMIN= 21.09] SMAX= 140.62] SK= .010]
08511 [InterEventTime= 12.00]
08512 #
08513 ROUTES CO00094-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08514 ROUTE RESERVOIR -> 1.0 02:DEF\_N 3.51 .635 No.Date 28:01 58.43 n/a .000
08515 + 1.0 02:DEF\_N 2.50 .117 No.Date 28:22 58.43 n/a .000
08516 + 1.0 02:DEF\_N 1.17 .078 No.Date 28:12 37.38 n/a .000
08517 SUM= 1.0 01:DEF\_N 7.18 .830 No.Date 28:01 58.43 n/a .000
08518 #
08519 ROUTES CO00095-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08520 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08521 [CM= 66.0] N= 3.00] T= .85]
08522 [IAREC= 4.00] SMIN= 21.09] SMAX= 140.62] SK= .010]
08523 [InterEventTime= 12.00]
08524 #
08525 ROUTES CO00096-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08526 ROUTE RESERVOIR -> 1.0 02:DEF\_N 3.51 .635 No.Date 28:01 58.43 n/a .000
08527 + 1.0 02:DEF\_N 2.50 .117 No.Date 28:22 58.43 n/a .000
08528 + 1.0 02:DEF\_N 1.17 .078 No.Date 28:12 37.38 n/a .000
08529 SUM= 1.0 01:DEF\_N 7.18 .830 No.Date 28:01 58.43 n/a .000
08530 #
08531 ROUTES CO00097-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08532 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08533 [CM= 66.0] N= 3.00] T= .85]
08534 [IAREC= 4.00] SMIN= 21.09] SMAX= 140.62] SK= .010]
08535 [InterEventTime= 12.00]
08536 #
08537 ROUTES CO00098-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08538 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08539 [CM= 66.0] N= 3.00] T= .85]
08540 [IAREC= 4.00] SMIN= 21.09] SMAX= 140.62] SK= .010]
08541 [InterEventTime= 12.00]
08542 #
08543 ROUTES CO00099-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08544 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08545 [CM= 66.0] N= 3.00] T= .85]
08546 [IAREC= 4.00] SMIN= 21.09] SMAX= 140.62] SK= .010]
08547 [InterEventTime= 12.00]
08548 #
08549 ROUTES CO00100-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08550 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08551 [CM= 66.0] N= 3.00] T= .85]
08552 [IAREC= 4.00] SMIN= 21.09] SMAX= 140.62] SK= .010]
08553 [InterEventTime= 12.00]
08554 #
08555 ROUTES CO00101-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08556 ROUTE RESERVOIR -> 1.0 02:DEF\_N 3.51 .635 No.Date 28:01 58.43 n/a .000
08557 + 1.0 02:DEF\_N 2.50 .117 No.Date 28:22 58.43 n/a .000
08558 + 1.0 02:DEF\_N 1.17 .078 No.Date 28:12 37.38 n/a .000
08559 SUM= 1.0 01:DEF\_N 7.18 .830 No.Date 28:01 58.43 n/a .000
08560 #
08561 ROUTES CO00102-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08562 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08563 [CM= 66.0] N= 3.00] T= .85]
08564 [IAREC= 4.00] SMIN= 21.09] SMAX= 140.62] SK= .010]
08565 [InterEventTime= 12.00]
08566 #
08567 ROUTES CO00103-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08568 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08569 [CM= 66.0] N= 3.00] T= .85]
08570 [IAREC= 4.00] SMIN= 21.09] SMAX= 140.62] SK= .010]
08571 [InterEventTime= 12.00]
08572 #
08573 ROUTES CO00104-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08574 ROUTE RESERVOIR -> 1.0 02:DEF\_N 3.51 .635 No.Date 28:01 58.43 n/a .000
08575 + 1.0 02:DEF\_N 2.50 .117 No.Date 28:22 58.43 n/a .000
08576 + 1.0 02:DEF\_N 1.17 .078 No.Date 28:12 37.38 n/a .000
08577 SUM= 1.0 01:DEF\_N 7.18 .830 No.Date 28:01 58.43 n/a .000
08578 #
08579 ROUTES CO00105-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08580 CONTINUOUS STANDBY-----DtmIn:ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----RvM-R-C-----DWFCMS
08581 [CM= 66.0] N= 3.00] T= .85]
08582 [IAREC= 4.00] SMIN= 21

08603# CONTINUOUS STANDBYD 1.0 01:01: 3.41 .618 No.Date 28:01 58.43 .785 .000
08604# [XIMP:64:TIMP:85]
08605# [Horton parameters] Fw: 76.20:Fc: 13.20:DCAV:4.14: Fw: .00]
08606# [Previous area] IArea: 4.67:SLIP: 50:LDI: 50:MDM: 250:SPC: .0]
08607# [Impervious area] IAlmp: 1.57:SLIP: 50:LDI: 261:MMI: .013:SPC: .0]
08608# [Iscalc] area: 4.00: IArea: 4.00]
08609# ROUTE RESERVOIR -> 1.0 02:01: 3.41 .618 No.Date 28:01 58.43 n/a .000
08610# out <- 1.0 01:01:CTE 1.87 .354 No.Date 28:01 58.43 n/a .000
08611# overflow <- 1.0 03:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08612# [Msdto:oad=.2418E+01 n3, TotVol:Vol=.0000E+00 n3, N-Ofv: 0, TotDur:Dur=.0 hrs]
08613# 08614# ROUTES COU1101-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08615# CONTINUOUS STANDBYD 1.0 01:01: 4.55 .071 No.Date 28:00 45.54 .612 .000
08616# [XIMP:64:TIMP:87]
08617# [Horton parameters] Fw: 76.20:Fc: 13.20:DCAV:4.14: Fw: .00]
08618# [Previous area] IArea: 4.67:SLIP: 50:LDI: 50:MDM: 250:SPC: .0]
08619# [Impervious area] IAlmp: 1.57:SLIP: 50:LDI: 95:MMI: .013:SPC: .0]
08620# [Iscalc] area: 4.00: IArea: 4.00]
08621# ROUTES COU111-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08622# CONTINUOUS STANDBYD 1.0 01:01: 4.55 .071 No.Date 28:00 45.54 n/a .000
08623# out <- 1.0 02:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08624# overflow <- 1.0 03:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08625# [Msdto:oad=.2418E+01 n3, TotVol:Vol=.0000E+00 n3, N-Ofv: 0, TotDur:Dur=.0 hrs]
08626# 08627# ROUTES COU112-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08628# ADD HYD + 1.0 02:02:EAHNS 350.31 5.293 No.Date 29:13 25.77 n/a .000
08629# + 1.0 02:01:CTE 3.41 .159 No.Date 28:23 58.43 n/a .000
08630# + 1.0 02:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08631# + 1.0 02:01:STRT 45 .040 No.Date 28:07 45.54 n/a .000
08632# + 1.0 02:01:STRT 45 .040 No.Date 28:07 45.54 n/a .000
08633# + 1.0 02:01:STRT 45 .040 No.Date 28:07 45.54 n/a .000
08634# + 1.0 02:01:STRT 45 .040 No.Date 28:07 45.54 n/a .000
08635# SUM 356.68 .000 No.Date 29:11 26.21 n/a .000
08636# 08637# ROUTES COU113-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08638# CONTINUOUS STANDBYD 1.0 01:01: 5.19 .518 No.Date 28:10 57.02 .767 .000
08639# [XIMP:64:TIMP:88]
08640# [Horton parameters] Fw: 76.20:Fc: 13.20:DCAV:4.14: Fw: .00]
08641# [Previous area] IArea: 4.67:SLIP: 50:LDI: 50:MDM: 250:SPC: .0]
08642# [Impervious area] IAlmp: 1.57:SLIP: 50:LDI: 1230:MMI: .013:SPC: .0]
08643# [Iscalc] area: 4.00: IArea: 4.00]
08644# ROUTES COU114-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08645# CONTINUOUS STANDBYD 1.0 01:01: 7.59 .109 No.Date 29:19 57.02 n/a .000
08646# out <- 1.0 01:01:POD 7.59 .109 No.Date 29:19 57.02 n/a .000
08647# overflow <- 1.0 03:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08648# [Msdto:oad=.2418E+01 n3, TotVol:Vol=.0000E+00 n3, N-Ofv: 0, TotDur:Dur=.0 hrs]
08649# 08650# ROUTES COU115-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08651# ADD HYD + 1.0 02:01:POD 7.59 .109 No.Date 29:19 57.02 n/a .000
08652# + 1.0 02:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08653# + 1.0 02:01:STRT 364.27 5.889 No.Date 29:11 26.85 n/a .000
08654# SUM 364.27 5.889 No.Date 29:11 26.85 n/a .000
08655# 08656# ROUTES COU116-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08657# SAVE HYD + 1.0 01:01:SSAOT 364.27 5.889 No.Date 29:11 26.85 n/a .000
08658# frame :SSAOT:0025
08659# 08660# ROUTES COU117-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08661# CONTINUOUS STANDBYD 1.0 01:01: 66.75 7.879 No.Date 28:09 56.06 .754 .000
08662# [XIMP:64:TIMP:80]
08663# [Horton parameters] Fw: 76.20:Fc: 13.20:DCAV:4.14: Fw: .00]
08664# [Previous area] IArea: 4.67:SLIP: 50:LDI: 50:MDM: 250:SPC: .0]
08665# [Impervious area] IAlmp: 1.57:SLIP: 50:LDI: 1155:MMI: .013:SPC: .0]
08666# [Iscalc] area: 4.00: IArea: 4.00]
08667# ROUTES COU118-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08668# CONTINUOUS STANDBYD 1.0 01:01: 66.75 7.879 No.Date 28:09 56.06 n/a .000
08669# out <- 1.0 02:01:Area-A 66.75 7.879 No.Date 28:09 56.06 n/a .000
08670# overflow <- 1.0 03:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08671# [Msdto:oad=.2418E+01 n3, TotVol:Vol=.0000E+00 n3, N-Ofv: 0, TotDur:Dur=.0 hrs]
08672# 08673# ROUTES COU119-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08674# frame :SMPF:0025
08675# 08676# ROUTES COU120-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08677# CONTINUOUS STANDBYD 1.0 01:01: 66.75 7.879 No.Date 28:09 56.06 n/a .000
08678# [XIMP:64:TIMP:80]
08679# [Horton parameters] Fw: 76.20:Fc: 13.20:DCAV:4.14: Fw: .00]
08680# [Previous area] IArea: 4.67:SLIP: 50:LDI: 50:MDM: 250:SPC: .0]
08681# [Impervious area] IAlmp: 1.57:SLIP: 50:LDI: 1155:MMI: .013:SPC: .0]
08682# [Iscalc] area: 4.00: IArea: 4.00]
08683# ROUTES COU121-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08684# CONTINUOUS STANDBYD 1.0 01:01: 66.75 7.879 No.Date 28:09 56.06 n/a .000
08685# out <- 1.0 01:01:Area-A 66.75 7.879 No.Date 28:09 56.06 n/a .000
08686# overflow <- 1.0 03:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08687# [Msdto:oad=.2418E+01 n3, TotVol:Vol=.0000E+00 n3, N-Ofv: 0, TotDur:Dur=.0 hrs]
08688# 08689# CONTINUOUS STANDBYD 1.0 01:01: 1.62 .309 No.Date 28:01 58.43 .785 .000
08690# [XIMP:64:TIMP:85]
08691# [Horton parameters] Fw: 76.20:Fc: 13.20:DCAV:4.14: Fw: .00]
08692# [Previous area] IArea: 4.67:SLIP: 50:LDI: 50:MDM: 250:SPC: .0]
08693# [Impervious area] IAlmp: 1.57:SLIP: 50:LDI: 180:MMI: .013:SPC: .0]
08694# [Iscalc] area: 4.00: IArea: 4.00]
08695# ROUTE RESERVOIR -> 1.0 02:01: 1.87 .354 No.Date 28:01 58.43 n/a .000
08696# out <- 1.0 01:01:CTE 1.87 .354 No.Date 28:01 58.43 n/a .000
08697# overflow <- 1.0 03:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08698# [Msdto:oad=.5013E+01 n3, TotVol:Vol=.0000E+00 n3, N-Ofv: 0, TotDur:Dur=.0 hrs]
08699# 08700# CONTINUOUS STANDBYD 1.0 01:01: 1.62 .309 No.Date 28:01 58.43 .785 .000
08701# [XIMP:64:TIMP:85]
08702# [Horton parameters] Fw: 76.20:Fc: 13.20:DCAV:4.14: Fw: .00]
08703# [Previous area] IArea: 4.67:SLIP: 50:LDI: 50:MDM: 250:SPC: .0]
08704# [Impervious area] IAlmp: 1.57:SLIP: 50:LDI: 180:MMI: .013:SPC: .0]
08705# [Iscalc] area: 4.00: IArea: 4.00]
08706# ROUTE RESERVOIR -> 1.0 02:01: 1.62 .309 No.Date 28:01 58.43 n/a .000
08707# out <- 1.0 01:01:CTE 1.87 .354 No.Date 28:01 58.43 n/a .000
08708# overflow <- 1.0 03:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08709# [Msdto:oad=.5013E+01 n3, TotVol:Vol=.0000E+00 n3, N-Ofv: 0, TotDur:Dur=.0 hrs]
08710# 08711# ROUTES COU122-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08712# CONTINUOUS STANDBYD 1.0 01:01: 4.1 .036 No.Date 28:00 45.54 n/a .000
08713# out <- 1.0 01:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08714# overflow <- 1.0 03:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08715# [Msdto:oad=.2350E+02 n3, TotVol:Vol=.0000E+00 n3, N-Ofv: 0, TotDur:Dur=.0 hrs]
08716# 08717# ROUTES COU123-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08718# ADD HYD + 1.0 02:01:PT4T5 431.02 6.356 No.Date 29:13 31.37 n/a .000
08719# + 1.0 02:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08720# + 1.0 02:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08721# + 1.0 02:01:CTE 1.62 .077 No.Date 28:21 58.43 n/a .000
08722# + 1.0 02:01:CTE 1.62 .077 No.Date 28:21 58.43 n/a .000
08723# + 1.0 02:01:CTE 1.62 .077 No.Date 28:21 58.43 n/a .000
08724# + 1.0 02:01:CTE 1.62 .077 No.Date 28:21 58.43 n/a .000
08725# SUM 434.92 6.444 No.Date 29:12 31.60 n/a .000
08726# 08727# ROUTES COU124-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08728# ROUTE CHANNEL -> 1.0 02:01:PT4T5 434.92 6.444 No.Date 29:12 31.60 n/a .000
08729# [RDY:1.00] out <- 1.0 01:01:EAHNS 434.92 6.229 No.Date 29:21 31.60 n/a .000
08730# [L/S: 1.24 / 1.00]
08731# [Vmax: .475:Imax: 1.440]
08732# 08733# ROUTES COU125-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08734# CONTINUOUS NASHYD 1.0 01:01: 1.73 .082 No.Date 28:34 43.34 .183 .000
08735# [Ck: 80.0: N: 3.00: Tp: .69]
08736# [Iscalc: 4.00: SMIN: 14.94: SMAX: 99.61: SK: .010]
08737# [InterEventTime: 12.00]
08738# 08739# ROUTES COU131-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08740# CONTINUOUS STANDBYD 1.0 01:01: 24.04 3.916 No.Date 28:03 54.85 .737 .000
08741# [XIMP:64:TIMP:77]
08742# [Horton parameters] Fw: 76.20:Fc: 13.20:DCAV:4.14: Fw: .00]
08743# [Previous area] IArea: 4.67:SLIP: 50:LDI: 50:MDM: 250:SPC: .0]
08744# [Impervious area] IAlmp: 1.57:SLIP: 40:LDI: 693:MMI: .013:SPC: .0]
08745# [Iscalc] area: 4.00: IArea: 4.00]
08746# ROUTE RESERVOIR -> 1.0 02:01: 24.04 3.916 No.Date 28:03 54.85 n/a .000
08747# out <- 1.0 01:01:Area-A 24.04 3.916 No.Date 28:03 54.85 n/a .000
08748# overflow <- 1.0 03:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08749# [Msdto:oad=.8178E+00 n3, TotVol:Vol=.0000E+00 n3, N-Ofv: 0, TotDur:Dur=.0 hrs]
08750# 08751# ROUTES COU133-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08752# ADD HYD + 1.0 02:01:EAHNS 434.92 6.229 No.Date 29:21 31.60 n/a .000
08753# + 1.0 02:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08754# + 1.0 02:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08755# + 1.0 02:01:STRT 24.04 .492 No.Date 28:44 54.85 n/a .000
08756# + 1.0 02:01:STRT 24.04 .492 No.Date 28:44 54.85 n/a .000
08757# + 1.0 02:01:STRT 24.04 .492 No.Date 28:44 54.85 n/a .000
08758# + 1.0 02:01:STRT 24.04 .492 No.Date 28:44 54.85 n/a .000
08759# SUM 460.69 6.177 No.Date 29:21 32.86 n/a .000
08760# 08761# ROUTES COU134-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08762# CONTINUOUS STANDBYD 1.0 01:01: 460.69 6.177 No.Date 29:21 32.86 n/a .000
08763# [L/S: 423.7 / 160]
08764# [Vmax: .641:Imax: .984]
08765# 08766# ROUTES COU135-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08767# CONTINUOUS NASHYD 1.0 01:01: 1.90 .076 No.Date 28:41 40.67 .547 .000
08768# [Ck: 80.0: N: 3.00: Tp: .69]
08769# [Iscalc: 4.00: SMIN: 116.21: SK: .010]
08770# [InterEventTime: 12.00]
08771# 08772# ROUTES COU136-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08773# CONTINUOUS STANDBYD 1.0 01:01: 9.74 .487 No.Date 28:22 38.23 .514 .000
08774# [Ck: 81.0: N: 3.00: Tp: .43]
08775# [Iscalc: 4.00: SMIN: 14.94: SMAX: 168.09: SK: .010]
08776# [InterEventTime: 12.00]
08777# 08778# ROUTES COU137-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08779# CONTINUOUS STANDBYD 1.0 02:01: 9.74 .487 No.Date 28:22 38.23 n/a .000
08780# out <- 1.0 01:01:RDY 9.74 .052 No.Date 31:01 38.23 n/a .000
08781# overflow <- 1.0 03:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08782# [Msdto:oad=.2061E+00 n3, TotVol:Vol=.0000E+00 n3, N-Ofv: 0, TotDur:Dur=.0 hrs]
08783# 08784# ROUTES COU138-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08785# ADD HYD + 1.0 02:01:EAHNS 460.69 6.177 No.Date 29:21 32.86 n/a .000
08786# + 1.0 02:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08787# + 1.0 02:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08788# + 1.0 02:01:STRT 24.04 .492 No.Date 28:44 54.85 n/a .000
08789# + 1.0 02:01:STRT 24.04 .492 No.Date 28:44 54.85 n/a .000
08790# + 1.0 02:01:STRT 24.04 .492 No.Date 28:44 54.85 n/a .000
08791# + 1.0 02:01:STRT 24.04 .492 No.Date 28:44 54.85 n/a .000
08792# SUM 472.33 6.689 No.Date 29:35 33.00 n/a .000
08793# 08794# ROUTES COU139-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08795# CONTINUOUS NASHYD 1.0 01:01: 10.67 .668 No.Date 28:13 37.06 .498 .000
08796# [Ck: 80.0: N: 3.00: Tp: .69]
08797# [Iscalc: 4.00: SMIN: 23.09: SMAX: 153.94: SK: .010]
08798# [InterEventTime: 12.00]
08799# 08800# ROUTES COU140-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08801# CONTINUOUS NASHYD 1.0 01:01: 1.90 .076 No.Date 28:41 40.67 .547 .000
08802# [Ck: 80.0: N: 3.00: Tp: .69]
08803# [Iscalc: 4.00: SMIN: 116.21: SK: .010]
08804# [InterEventTime: 12.00]
08805# 08806# ROUTES COU141-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08807# ADD HYD + 1.0 02:01:PT4T5 431.02 6.356 No.Date 29:13 31.37 n/a .000
08808# + 1.0 02:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08809# + 1.0 02:01:OVF 0.00 .000 No.Date 0:00 .00 n/a .000
08810# + 1.0 02:01:CTE 1.62 .077 No.Date 28:21 58.43 n/a .000
08811# + 1.0 02:01:CTE 1.62 .077 No.Date 28:21 58.43 n/a .000
08812# + 1.0 02:01:CTE 1.62 .077 No.Date 28:21 58.43 n/a .000
08813# + 1.0 02:01:CTE 1.62 .077 No.Date 28:21 58.43 n/a .000
08814# SUM 434.92 6.444 No.Date 29:12 31.60 n/a .000
08815# 08816# ROUTES COU142-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08817# CONTINUOUS STANDBYD 1.0 01:01: 434.92 6.229 No.Date 29:21 31.60 n/a .000
08818# [L/S: 423.7 / 160]
08819# [Vmax: .475:Imax: 1.440]
08820# 08821# ROUTES COU143-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08822# CONTINUOUS NASHYD 1.0 01:01: 1.90 .076 No.Date 28:41 40.67 .547 .000
08823# [Ck: 80.0: N: 3.00: Tp: .69]
08824# [Iscalc: 4.00: SMIN: 116.21: SK: .010]
08825# [InterEventTime: 12.00]
08826# 08827# ROUTES COU144-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08828# CONTINUOUS STANDBYD 1.0 01:01: 1.90 .076 No.Date 28:41 40.67 .547 .000
08829# [Ck: 80.0: N: 3.00: Tp: .69]
08830# [Iscalc: 4.00: SMIN: 116.21: SK: .010]
08831# [InterEventTime: 12.00]
08832# 08833# ROUTES COU145-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08834# CONTINUOUS NASHYD 1.0 01:01: 1.90 .076 No.Date 28:41 40.67 .547 .000
08835# [Ck: 80.0: N: 3.00: Tp: .69]
08836# [Iscalc: 4.00: SMIN: 116.21: SK: .010]
08837# [InterEventTime: 12.00]
08838# 08839# ROUTES COU146-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08840# CONTINUOUS STANDBYD 1.0 01:01: 1.90 .076 No.Date 28:41 40.67 .547 .000
08841# [Ck: 80.0: N: 3.00: Tp: .69]
08842# [Iscalc: 4.00: SMIN: 116.21: SK: .010]
08843# [InterEventTime: 12.00]
08844# 08845# ROUTES COU147-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08846# CONTINUOUS NASHYD 1.0 01:01: 1.90 .076 No.Date 28:41 40.67 .547 .000
08847# [Ck: 80.0: N: 3.00: Tp: .69]
08848# [Iscalc: 4.00: SMIN: 116.21: SK: .010]
08849# [InterEventTime: 12.00]
08850# 08851# ROUTES COU148-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08852# CONTINUOUS STANDBYD 1.0 01:01: 1.90 .076 No.Date 28:41 40.67 .547 .000
08853# [Ck: 80.0: N: 3.00: Tp: .69]
08854# [Iscalc: 4.00: SMIN: 116.21: SK: .010]
08855# [InterEventTime: 12.00]
08856# 08857# ROUTES COU149-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08858# CONTINUOUS NASHYD 1.0 01:01: 1.90 .076 No.Date 28:41 40.67 .547 .000
08859# [Ck: 80.0: N: 3.00: Tp: .69]
08860# [Iscalc: 4.00: SMIN: 116.21: SK: .010]
08861# [InterEventTime: 12.00]
08862# 08863# ROUTES COU150-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08864# CONTINUOUS STANDBYD 1.0 01:01: 1.90 .076 No.Date 28:41 40.67 .547 .000
08865# [Ck: 80.0: N: 3.00: Tp: .69]
08866# [Iscalc: 4.00: SMIN: 116.21: SK: .010]
08867# [InterEventTime: 12.00]
08868# 08869# ROUTES COU151-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08870# CONTINUOUS NASHYD 1.0 01:01: 1.90 .076 No.Date 28:41 40.67 .547 .000
08871# [Ck: 80.0: N: 3.00: Tp: .69]
08872# [Iscalc: 4.00: SMIN: 116.21: SK: .010]
08873# [InterEventTime: 12.00]
08874# 08875# ROUTES COU152-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08876# CONTINUOUS STANDBYD 1.0 01:01: 1.90 .076 No.Date 28:41 40.67 .547 .000
08877# [Ck: 80.0: N: 3.00: Tp: .69]
08878# [Iscalc: 4.00: SMIN: 116.21: SK: .010]
08879# [InterEventTime: 12.00]
08880# 08881# ROUTES COU153-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08882# CONTINUOUS NASHYD 1.0 01:01: 1.90 .076 No.Date 28:41 40.67 .547 .000
08883# [Ck: 80.0: N: 3.00: Tp: .69]
08884# [Iscalc: 4.00: SMIN: 116.21: SK: .010]
08885# [InterEventTime: 12.00]
08886# 08887# ROUTES COU154-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08888# CONTINUOUS STANDBYD 1.0 01:01: 1.90 .076 No.Date 28:41 40.67 .547 .000
08889# [Ck: 80.0: N: 3.00: Tp: .69]
08890# [Iscalc: 4.00: SMIN: 116.21: SK: .010]
08891# [InterEventTime: 12.00]
08892# 08893# ROUTES COU155-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08894# CONTINUOUS NASHYD 1.0 01:01: 1.90 .076 No.Date 28:41 40.67 .547 .000
08895# [Ck: 80.0: N: 3.00: Tp: .69]
08896# [Iscalc: 4.00: SMIN: 116.21: SK: .010]
08897# [InterEventTime: 12.00]
08898# 08899# ROUTES COU156-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08900# CONTINUOUS STANDBYD 1.0 01:01: 1.90 .076 No.Date 28:41 40.67 .547 .000
08901# [Ck: 80.0: N: 3.00: Tp: .69]
08902# [Iscalc: 4.00: SMIN: 116.21: SK: .010]
08903# [InterEventTime: 12.00]
08904# 08905# ROUTES COU157-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08906# CONTINUOUS NASHYD 1.0 01:01: 1.90 .076 No.Date 28:41 40.67 .547 .000
08907# [Ck: 80.0: N: 3.00: Tp: .69]
08908# [Iscalc: 4.00: SMIN: 116.21: SK: .010]
08909# [InterEventTime: 12.00]
08910# 08911# ROUTES COU158-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08912# CONTINUOUS STANDBYD 1.0 01:01: 1.90 .076 No.Date 28:41 40.67 .547 .000
08913# [Ck: 80.0: N: 3.00: Tp: .69]
08914# [Iscalc: 4.00: SMIN: 116.21: SK: .010]
08915# [InterEventTime: 12.00]
08916# 08917# ROUTES COU159-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08918# CONTINUOUS NASHYD 1.0 01:01: 1.90 .076 No.Date 28:41 40.67 .547 .000
08919# [Ck: 80.0: N: 3.00: Tp: .69]
08920# [Iscalc: 4.00: SMIN: 116.21: SK: .010]
08921# [InterEventTime: 12.00]
08922# 08923# ROUTES COU160-----DRAIN-ID:HYD-----AREHA-QPEARCS-TPeakDate\_hh:mm-----Rvm-R.C-----DMFcms
08924# CONTINUOUS STANDBYD 1.0 01:01: 1.90 .076 No.Date 28:41 40.67 .547 .000
08925# [Ck: 80.0: N: 3.00: Tp: .69]
08926# [Iscalc: 4.00: SMIN: 116.21: SK: .010]
08927# [InterEventTime: 12.0











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10473# Parameters for IMPERVIOUS surfaces in STANDHYD:
10474# [kings 1.57 mm] [cru 1.50] [mhw .013]
10475# Parameters used in BASSETD:
10476# [a 0.00] [b 0.00]
10477# Average monthly Pan Evaporation data in (mm)
10478# JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
10479# .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
10480# Average monthly Potential Evapotranspiration in (mm)
10481# JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
10482# .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
10483#-----
10484# R0550/C0001
10485# COMPUTE API
10486# [APIIn=50.00; APIQty= .8500; APIDir=.9988]
10487# [APITime=11.33; APIVgs= 07.34; APIFmax=44.97]
10488#
10489# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10490# # of 1.32
10491# R0550/C0006-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10492# CONTINUOUS NASHVD 1.0 01:28_RM 3840.00 18.440_NoDate 36:55 30.33 372 .000
10493# [Cm 64.0i No 3.00i Tp 1.32]
10494# [IAREK 4.00i SMIN= 37.65; SMAX=350.32; EK=.010]
10495# [InterVntTime= 12.00]
10496#
10497# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10498# # of 1.32
10499# R0550/C0007-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10500# CONTINUOUS NASHVD 1.0 01:28_RM 371.00 6.937_NoDate 32:34 28.27 347 .000
10501# [Cm 61.0i No 3.00i Tp 1.32]
10502# [IAREK 4.00i SMIN= 64.55; SMAX=430.01; EK=.010]
10503# [InterVntTime= 12.00]
10504#
10505# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10506# # of 1.80
10507# R0550/C0008-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10508# CONTINUOUS NASHVD 1.0 01:28_RM 3074.00 8.912_NoDate 39:59 24.31 298 .000
10509# [Cm 55.0i No 3.00i Tp=1.33]
10510# [IAREK 4.00i SMIN= 83.24; SMAX=554.96; EK=.010]
10511# [InterVntTime= 12.00]
10512#
10513# R0550/C0009-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10514# CONTINUOUS NASHVD 1.0 01:28_RM 16434.00 16.434_NoDate 32:39 36.65 452 .000
10515# [Cm 72.0i No 3.00i Tp= 3.91]
10516# [IAREK 4.00i SMIN= 35.78; SMAX=264.99; EK=.010]
10517# [InterVntTime= 12.00]
10518#
10519# R0550/C0010-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10520# CONTINUOUS NASHVD 1.0 01:28_RM 972.00 9.061_NoDate 29:21 31.73 389 .000
10521# [Cm 66.0i No 3.00i Tp 1.24]
10522# [IAREK 4.00i SMIN= 44.50; SMAX=350.79; EK=.010]
10523# [InterVntTime= 12.00]
10524#
10525# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10526# # of 1.80
10527# R0550/C0011-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10528# CONTINUOUS NASHVD 1.0 01:28_RM 1917.00 12.342_NoDate 34:26 31.73 389 .000
10529# [Cm 66.0i No 3.00i Tp 1.24]
10530# [IAREK 4.00i SMIN= 52.62; SMAX=350.79; EK=.010]
10531# [InterVntTime= 12.00]
10532#
10533# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10534# # of 1.52
10535# R0550/C0012-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10536# CONTINUOUS NASHVD 1.0 01:28_RM 5666.00 32.402_NoDate 37:52 36.65 452 .000
10537# [Cm 72.0i No 3.00i Tp= 4.00]
10538# [IAREK 4.00i SMIN= 39.75; SMAX=264.99; EK=.010]
10539# [InterVntTime= 12.00]
10540#
10541# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10542# # of 1.75
10543# R0550/C0013-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10544# CONTINUOUS NASHVD 1.0 01:28_RM 8176.00 11.024_NoDate 39:59 31.73 389 .000
10545# [Cm 66.0i No 3.00i Tp=1.66]
10546# [IAREK 4.00i SMIN= 92.62; SMAX=350.79; EK=.010]
10547# [InterVntTime= 12.00]
10548#
10549# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10550# # of 1.68
10551# R0550/C0014-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10552# CONTINUOUS NASHVD 1.0 01:28_RM 1132.00 14.039_NoDate 30:53 35.35 434 .000
10553# [Cm 73.0i No 3.00i Tp 1.29]
10554# [IAREK 4.00i SMIN= 43.07; SMAX=287.10; EK=.010]
10555# [InterVntTime= 12.00]
10556#
10557# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10558# # of 1.82
10559# R0550/C0015-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10560# CONTINUOUS NASHVD 1.0 01:28_RM 4464.00 15.472_NoDate 39:59 28.95 355 .000
10561# [Cm 62.0i No 3.00i Tp=1.32]
10562# [IAREK 4.00i SMIN= 61.90; SMAX=412.66; EK=.010]
10563# [InterVntTime= 12.00]
10564#
10565# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10566# # of 1.80
10567# R0550/C0016-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10568# CONTINUOUS NASHVD 1.0 01:28_RM 131.00 2.740_NoDate 28:57 29.64 364 .000
10569# [Cm 63.0i No 3.00i Tp .90]
10570# [IAREK 4.00i SMIN= 58.42; SMAX=396.11; EK=.010]
10571# [InterVntTime= 12.00]
10572#
10573# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10574# # of 1.65
10575# R0550/C0017-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10576# CONTINUOUS NASHVD 1.0 01:28_RM 3854.00 18.180_NoDate 38:32 31.73 389 .000
10577# [Cm 64.0i No 3.00i Tp 1.42]
10578# [IAREK 4.00i SMIN= 52.62; SMAX=350.79; EK=.010]
10579# [InterVntTime= 12.00]
10580#
10581# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10582# # of 1.82
10583# R0550/C0018-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10584# CONTINUOUS NASHVD 1.0 01:28_RM 3197.00 13.937_NoDate 36:23 25.61 314 .000
10585# [Cm 57.0i No 3.00i Tp 6.65]
10586# [IAREK 4.00i SMIN= 35.78; SMAX=264.99; EK=.010]
10587# [InterVntTime= 12.00]
10588#
10589# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10590# # of 1.75
10591# R0550/C0019-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10592# CONTINUOUS NASHVD 1.0 01:28_RM 165.00 1.285_NoDate 33:02 32.44 398 .000
10593# [Cm 67.0i No 3.00i Tp 4.18]
10594# [IAREK 4.00i SMIN= 35.78; SMAX=264.99; EK=.010]
10595# [InterVntTime= 12.00]
10596#
10597# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10598# # of 1.41
10599# R0550/C0020-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10600# CONTINUOUS NASHVD 1.0 01:28_RM 1332.00 9.332_NoDate 35:12 36.85 452 .000
10601# [Cm 75.0i No 3.00i Tp= 1.98]
10602# [IAREK 4.00i SMIN= 39.75; SMAX=264.99; EK=.010]
10603# [InterVntTime= 12.00]
10604#
10605# R0550/C0021-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10606# CONTINUOUS NASHVD 1.0 01:28_RM 224.00 8.187_NoDate 28:45 41.51 509 .000
10607# [Cm 77.0i No 3.00i Tp .75]
10608# [IAREK 4.00i SMIN= 31.15; SMAX=207.66; EK=.010]
10609# [InterVntTime= 12.00]
10610#
10611# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10612# # of 1.80
10613# R0550/C0022-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10614# CONTINUOUS NASHVD 1.0 01:28_RM 4945.00 14.623_NoDate 31:18 38.77 471 .000
10615# [Cm 74.0i No 3.00i Tp 4.45]
10616# [IAREK 4.00i SMIN= 35.78; SMAX=264.99; EK=.010]
10617# [InterVntTime= 12.00]
10618#
10619# R0550/C0023-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10620# CONTINUOUS NASHVD 1.0 01:28_RM 24.00 .943_NoDate 28:35 45.60 560 .000
10621# [Cm 81.0i No 3.00i Tp .62]
10622# [IAREK 4.00i SMIN= 25.21; SMAX=168.09; EK=.010]
10623# [InterVntTime= 12.00]
10624#
10625# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10626# # of 1.61
10627# R0550/C0024-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10628# CONTINUOUS NASHVD 1.0 01:28_RM 1412.00 8.794_NoDate 37:48 39.93 490 .000
10629# [Cm 75.0i No 3.00i Tp 1.78]
10630# [IAREK 4.00i SMIN= 33.81; SMAX=225.43; EK=.010]
10631# [InterVntTime= 12.00]
10632#
10633# R0550/C0025-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10634# CONTINUOUS NASHVD 1.0 01:28_RM 585.00 12.896_NoDate 29:55 45.60 560 .000
10635# [Cm 81.0i No 3.00i Tp 1.78]
10636# [IAREK 4.00i SMIN= 25.21; SMAX=168.09; EK=.010]
10637# [InterVntTime= 12.00]
10638#
10639# R0550/C0026-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10640# CONTINUOUS NASHVD 1.0 01:28_RM 1021.00 17.059_NoDate 30:46 44.77 549 .000
10641# [Cm 80.0i No 3.00i Tp 1.40]
10642# [IAREK 4.00i SMIN= 26.32; SMAX=175.50; EK=.010]
10643# [InterVntTime= 12.00]
10644#
10645# R0550/C0027-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10646# CONTINUOUS NASHVD 1.0 01:28_RM 177.00 6.469_NoDate 28:45 41.51 509 .000
10647# [Cm 77.0i No 3.00i Tp .75]
10648# [IAREK 4.00i SMIN= 31.15; SMAX=207.66; EK=.010]
10649# [InterVntTime= 12.00]
10650#
10651# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10652# # of 1.80
10653# R0550/C0028-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10654# CONTINUOUS NASHVD 1.0 01:28_RM 2737.00 14.946_NoDate 31:29 40.72 500 .000
10655# [Cm 76.0i No 3.00i Tp 3.03]
10656# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10657# [InterVntTime= 12.00]
10658#
10659# Routing hydrographs
10660#
10661# Starting with the addition of Jock River Headwater and Subwatershed 13
10662#
10663# R0550/C0030-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10664# ADD HYD + 1.0 02:18_RM 3680.00 18.440_NoDate 36:55 30.33 n/a .000
10665# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10666# [InterVntTime= 12.00]
10667#
10668# R0550/C0031-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10669# ROUTE CHANNEL -> 1.0 02:18_RM 4651.00 23.559_NoDate 35:24 29.90 n/a .000
10670# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10671# [InterVntTime= 12.00]
10672#
10673# R0550/C0032-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10674# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10675# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10676# [InterVntTime= 12.00]
10677#
10678# R0550/C0033-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10679# INSERTION OF A RESERVOIR TO SIMULATE THE EFFECTS OF THE GOODWOOD MARSH
10680#
10681# R0550/C0034-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10682# ROUTE CHANNEL -> 1.0 02:18_RM 7725.00 27.939_NoDate 39:54 27.68 n/a .000
10683# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10684# [InterVntTime= 12.00]
10685#
10686# R0550/C0035-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10687# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10688# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10689# [InterVntTime= 12.00]
10690#
10691# R0550/C0036-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10692# INSERTION OF A RESERVOIR TO SIMULATE THE EFFECTS OF THE GOODWOOD MARSH
10693#
10694# R0550/C0037-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10695# ROUTE CHANNEL -> 1.0 02:18_RM 7725.00 27.939_NoDate 39:54 27.68 n/a .000
10696# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10697# [InterVntTime= 12.00]
10698#
10699# R0550/C0038-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10700# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10701# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10702# [InterVntTime= 12.00]
10703#
10704# R0550/C0039-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10705# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10706# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10707# [InterVntTime= 12.00]
10708#
10709# R0550/C0040-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10710# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10711# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10712# [InterVntTime= 12.00]
10713#
10714# R0550/C0041-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10715# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10716# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10717# [InterVntTime= 12.00]
10718#
10719# R0550/C0042-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10720# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10721# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10722# [InterVntTime= 12.00]
10723#
10724# R0550/C0043-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10725# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10726# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10727# [InterVntTime= 12.00]
10728#
10729# R0550/C0044-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10730# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10731# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10732# [InterVntTime= 12.00]
10733#
10734# R0550/C0045-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10735# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10736# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10737# [InterVntTime= 12.00]
10738#
10739# R0550/C0046-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10740# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10741# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10742# [InterVntTime= 12.00]
10743#
10744# R0550/C0047-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10745# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10746# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10747# [InterVntTime= 12.00]
10748#
10749# R0550/C0048-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10750# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10751# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10752# [InterVntTime= 12.00]
10753#
10754# R0550/C0049-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10755# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10756# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10757# [InterVntTime= 12.00]
10758#
10759# R0550/C0050-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10760# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10761# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10762# [InterVntTime= 12.00]
10763#
10764# R0550/C0051-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10765# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10766# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10767# [InterVntTime= 12.00]
10768#
10769# R0550/C0052-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10770# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10771# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10772# [InterVntTime= 12.00]
10773#
10774# R0550/C0053-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10775# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10776# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10777# [InterVntTime= 12.00]
10778#
10779# R0550/C0054-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10780# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10781# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10782# [InterVntTime= 12.00]
10783#
10784# R0550/C0055-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10785# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10786# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10787# [InterVntTime= 12.00]
10788#
10789# R0550/C0056-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10790# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10791# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10792# [InterVntTime= 12.00]
10793#
10794# R0550/C0057-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10795# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10796# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10797# [InterVntTime= 12.00]
10798#
10799# R0550/C0058-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10800# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10801# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10802# [InterVntTime= 12.00]
10803#
10804# R0550/C0059-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10805# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10806# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10807# [InterVntTime= 12.00]
10808#
10809# R0550/C0060-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10810# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10811# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10812# [InterVntTime= 12.00]
10813#
10814# R0550/C0061-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10815# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10816# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10817# [InterVntTime= 12.00]
10818#
10819# R0550/C0062-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10820# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10821# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10822# [InterVntTime= 12.00]
10823#
10824# R0550/C0063-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10825# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10826# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10827# [InterVntTime= 12.00]
10828#
10829# R0550/C0064-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10830# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10831# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10832# [InterVntTime= 12.00]
10833#
10834# R0550/C0065-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10835# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10836# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10837# [InterVntTime= 12.00]
10838#
10839# R0550/C0066-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10840# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10841# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10842# [InterVntTime= 12.00]
10843#
10844# R0550/C0067-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10845# ADD HYD + 1.0 02:18_RM 3074.00 8.912_NoDate 39:59 24.31 n/a .000
10846# [IAREK 4.00i SMIN= 1.01; SMAX=216.39; EK=.010]
10847# [InterVntTime= 12.00]
10848#
10849# R0550/C0068-----DtnIn-ID-NHYD-----AREAh-QPEArms-TpeakDate_hh:mm-----RvM-R-C-----DWPFms
10850# ADD HYD + 1.0 
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10847#	[RDP= 1.00] out<	1.0 01:35	40240.01	51.693	NoDate	61:06	31.37	n/a	.000	
10848#	[L/S= 852 / .051] .035									
10849#	[Vmax= .469] Dmax= 1.331									
10850#										
10851#	Addition of Subwatershed 5 and Flowing Creek to Node 5									
10852#										
10853#	R050/C00056	-----	UTrain-ID:HYD	-----	AREHA-QPEARCS	-----	TpeakDate_hh:mm	-----	Rvum-R.C.	-----
10854#	ADD HYD	+	1.0 02:18	40240.01	51.693	NoDate	61:06	31.37	n/a	.000
10855#										
10856#										
10857#	SUM	+	1.0 01:35	45409.01	44.623	NoDate	33:18	38.37	n/a	.000
10858#										
10859#	Sum of hydrographs from Node 5 routed to Node 5A									
10860#	Section 7									
10861#										
10862#	R050/C00057	-----	UTrain-ID:HYD	-----	AREHA-QPEARCS	-----	TpeakDate_hh:mm	-----	Rvum-R.C.	-----
10863#	ROUTE CHANNEL	->	1.0 01:35	45409.01	71.514	NoDate	34:20	32.18	n/a	.000
10864#	[RDP= 1.00] out<	1.0 01:35	45409.01	71.514	NoDate	34:20	32.18	n/a	.000	
10865#	[L/S= 856 / .091] .030									
10866#	[Vmax= .530] Dmax= 1.290									
10867#										
10868#	Addition of Subwatershed 5L and Subwatershed 5A2 to Node 5A									
10869#	R050/C00058	-----	UTrain-ID:HYD	-----	AREHA-QPEARCS	-----	TpeakDate_hh:mm	-----	Rvum-R.C.	-----
10870#	ADD HYD	+	1.0 02:18	45409.01	71.514	NoDate	34:15	32.18	n/a	.000
10871#										
10872#										
10873#	SUM	+	1.0 01:35	45409.01	71.514	NoDate	34:15	32.18	n/a	.000
10874#										
10875#										
10876#	Sum of hydrographs from Node 5A routed to Node 4									
10877#	Section 8									
10878#										
10879#	R050/C00059	-----	UTrain-ID:HYD	-----	AREHA-QPEARCS	-----	TpeakDate_hh:mm	-----	Rvum-R.C.	-----
10880#	ROUTE CHANNEL	->	1.0 01:35	46841.01	79.247	NoDate	34:46	32.42	n/a	.000
10881#	[RDP= 1.00] out<	1.0 01:35	46841.01	79.247	NoDate	34:46	32.42	n/a	.000	
10882#	[L/S= 4630 / .041] .035									
10883#	[Vmax= .874] Dmax= 3.702									
10884#										
10885#	Addition of Subwatershed 4 and Leamy Creek to Node 4									
10886#	R050/C00060	-----	UTrain-ID:HYD	-----	AREHA-QPEARCS	-----	TpeakDate_hh:mm	-----	Rvum-R.C.	-----
10887#	ADD HYD	+	1.0 02:18	46841.01	79.247	NoDate	34:46	32.42	n/a	.000
10888#										
10889#										
10890#	SUM	+	1.0 01:35	46841.01	79.247	NoDate	34:46	32.42	n/a	.000
10891#										
10892#	R050/C00061	-----	UTrain-ID:HYD	-----	AREHA-QPEARCS	-----	TpeakDate_hh:mm	-----	Rvum-R.C.	-----
10893#	SAVE HYD	+	1.0 01:35	46841.01	84.908	NoDate	35:20	32.84	n/a	.000
10894#	fname IS_M4.0050									
10895#	remark:flow at R_N4									
10896#										
10897#	Sum of hydrographs from Node 4 routed to Node 2									
10898#	Section 9									
10899#										
10900#	R050/C00062	-----	UTrain-ID:HYD	-----	AREHA-QPEARCS	-----	TpeakDate_hh:mm	-----	Rvum-R.C.	-----
10901#	ROUTE CHANNEL	->	1.0 01:35	48447.00	84.908	NoDate	35:20	32.84	n/a	.000
10902#	[RDP= 1.00] out<	1.0 01:35	48447.00	84.908	NoDate	35:20	32.84	n/a	.000	
10903#	[L/S= 1687 / .064] .030									
10904#	[Vmax= .909] Dmax= 3.749									
10905#										
10906#	Addition of Subwatershed 2 with Monon Drain and Smith Drain to Node 2									
10907#	R050/C00063	-----	UTrain-ID:HYD	-----	AREHA-QPEARCS	-----	TpeakDate_hh:mm	-----	Rvum-R.C.	-----
10908#	ADD HYD	+	1.0 02:18	48447.00	84.908	NoDate	35:20	32.84	n/a	.000
10909#										
10910#										
10911#										
10912#	SUM	+	1.0 01:35	48447.00	84.908	NoDate	35:20	32.84	n/a	.000
10913#										
10914#	R050/C00064	-----	UTrain-ID:HYD	-----	AREHA-QPEARCS	-----	TpeakDate_hh:mm	-----	Rvum-R.C.	-----
10915#	SAVE HYD	+	1.0 01:35	52483.00	124.249	NoDate	32:52	33.56	n/a	.000
10916#	fname IS_H2									
10917#	remark:flow at R_H2									
10918#										
10919#	Sum of hydrographs from Node 2 routed to Node 1									
10920#	Section 10									
10921#										
10922#										
10923#										
10924#	Hydrograph from Node 2 routed to Node 416									
10925#	Channel X-Section obtained from RWCA Hydraulic Model - Station 9025									
10926#										
10927#	R050/C00065	-----	UTrain-ID:HYD	-----	AREHA-QPEARCS	-----	TpeakDate_hh:mm	-----	Rvum-R.C.	-----
10928#	ROUTE CHANNEL	->	1.0 01:35	52483.00	124.249	NoDate	32:52	33.56	n/a	.000
10929#	[RDP= 1.00] out<	1.0 01:35	52483.00	124.249	NoDate	32:52	33.56	n/a	.000	
10930#	[L/S= 2327 / .050] .055									
10931#	[Vmax= 1.237] Dmax= 4.661									
10932#										
10933#	Catchment IS-1a									
10934#	Position of RWCA catchment IS-1 outside of Reach 1 subwatershed									
10935#	Undeveloped agricultural land									
10936#										
10937#	R050/C00066	-----	UTrain-ID:HYD	-----	AREHA-QPEARCS	-----	TpeakDate_hh:mm	-----	Rvum-R.C.	-----
10938#	CONTINUOUS NASHVD	1.0 01:35	536.42	6.175	NoDate	31:15	35.39	4.84	.000	
10939#	[RDP= 72.0] IN	3:00	7:39							
10940#	[AREC= 4.00] SMIN= 39.75									
10941#	[SMAX= 264.99] SK= .010									
10942#	R050/C00067	-----	UTrain-ID:HYD	-----	AREHA-QPEARCS	-----	TpeakDate_hh:mm	-----	Rvum-R.C.	-----
10943#	CONTINUOUS NASHVD	1.0 01:35	536.42	6.175	NoDate	29:06	39.31	4.90	.000	
10944#	[RDP= 77.0] IN	3:00	7:39							
10945#	[AREC= 4.00] SMIN= 31.55									
10946#	[SMAX= 207.66] SK= .010									
10947#	R050/C00068	-----	UTrain-ID:HYD	-----	AREHA-QPEARCS	-----	TpeakDate_hh:mm	-----	Rvum-R.C.	-----
10948#	ADD HYD	+	1.0 01:35	52483.00	124.249	NoDate	32:52	33.56	n/a	.000
10949#										
10950#										
10951#	SUM	+	1.0 01:35	52483.00	124.249	NoDate	32:52	33.56	n/a	.000
10952#										
10953#	R050/C00069	-----	UTrain-ID:HYD	-----	AREHA-QPEARCS	-----	TpeakDate_hh:mm	-----	Rvum-R.C.	-----
10954#	SAVE HYD	+	1.0 01:35	53064.36	125.484	NoDate	33:19	33.88	n/a	.000
10955#	fname IS_H1.0050									
10956#	remark:flow at Highway 416									
10957#										
10958#	Hydrograph from Node 416 routed to Node at Office drain									
10959#	Channel X-Section obtained from RWCA Hydraulic Model - Station 7245									
10960#	R050/C00070	-----	UTrain-ID:HYD	-----	AREHA-QPEARCS	-----	TpeakDate_hh:mm	-----	Rvum-R.C.	-----
10961#	ROUTE CHANNEL	->	1.0 01:35	53064.36	125.484	NoDate	33:19	33.88	n/a	.000
10962#	[RDP= 1.00] out<	1.0 01:35	53064.36	125.484	NoDate	33:19	33.88	n/a	.000	
10963#	[L/S= 497 / .302] .055									
10964#	[Vmax= 1.649] Dmax= 3.358									
10965#										
10966#	Catchment OKEFE									
10967#	To Office drain (north of the Jack's office)									
10968#	Developed with assumed 43% imp									
10969#	2020-11-20 Okeefe detailed model was added as per the NOVATEC SIMMIND model (C111-date 2014).									
10970#	R050/C00071	-----	UTrain-ID:HYD	-----	AREHA-QPEARCS	-----	TpeakDate_hh:mm	-----	Rvum-R.C.	-----
10971#	CONTINUOUS NASHVD	1.0 01:35	63.72	1.147	NoDate	28:58	26.31	1.23	.000	
10972#	[RDP= 40.0] IN	3:00	7:39							
10973#	[AREC= 4.00] SMIN= 64.50									
10974#	[SMAX= 430.01] SK= .010									
10975#	R050/C00072	-----	UTrain-ID:HYD	-----	AREHA-QPEARCS	-----	TpeakDate_hh:mm	-----	Rvum-R.C.	-----
10976#	ROUTE CHANNEL	->	1.0 02:01	63.72	1.147	NoDate	28:58	26.31	n/a	.000
10977#	[RDP= 1.00] out<	1.0 02:01	63.72	1.147	NoDate	28:58	26.31	n/a	.000	
10978#	[L/S= 960 / .630] .043									
10979#	[Vmax= .807] Dmax= .445									
10980#										
10981#	R050/C00073	-----	UTrain-ID:HYD	-----	AREHA-QPEARCS	-----	TpeakDate_hh:mm	-----	Rvum-R.C.	-----
10982#	CONTINUOUS NASHVD	1.0 01:35	28.61	.404	NoDate	29:13	24.30	2.98	.000	
10983#	[RDP= 40.0] IN	3:00	7:39							
10984#	[AREC= 4.00] SMIN= 76.32									
10985#	[SMAX= 508.81] SK= .010									
10986#	R050/C00074	-----	UTrain-ID:HYD	-----	AREHA-QPEARCS	-----	TpeakDate_hh:mm	-----	Rvum-R.C.	-----
10987#	CONTINUOUS NASHVD	1.0 01:35	46.94	.933	NoDate	29:00	18.95	2.28	.000	
10988#	[RDP= 40.0] IN	3:00	7:39							
10989#	[AREC= 4.00] SMIN= 104.59									
10990#	[SMAX= 697.25] SK= .010									
10991#	R050/C00075	-----	UTrain-ID:HYD	-----	AREHA-QPEARCS	-----	TpeakDate_hh:mm	-----	Rvum-R.C.	-----













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13091 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13092 # of 1.80
13093 CONTINUOUS HASHYD 1.0 01:01:00 3074.00 10.428 No.Date 39:59 28.29 319 .000
13094 [Cm 55.0: No 3.00: Tp=11.33]
13095 [I&Rc 4.00: SMIN: 81.24: SMAX=554.96: Hk: .010]
13096 [InterVntTime= 12.00]
13097 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13098 CONTINUOUS HASHYD 1.0 01:01:00 1781.00 19.695 No.Date 32:38 42.49 480 .000
13099 [Cm 72.0: No 3.00: Tp= 3.91]
13100 [I&Rc 4.00: SMIN: 81.24: SMAX=264.99: Hk: .010]
13101 [InterVntTime= 12.00]
13102 CONTINUOUS HASHYD 1.0 01:01:00 8176.00 36.418 No.Date 39:59 36.76 415 .000
13103 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13104 CONTINUOUS HASHYD 1.0 01:01:00 1781.00 19.695 No.Date 32:38 42.49 480 .000
13105 [Cm 66.0: No 3.00: Tp= 1.24]
13106 [I&Rc 4.00: SMIN: 81.24: SMAX=350.79: Hk: .010]
13107 [InterVntTime= 12.00]
13108 #
13109 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13110 # of 1.80
13111 CONTINUOUS HASHYD 1.0 01:01:00 1917.00 14.496 No.Date 34:24 36.76 415 .000
13112 [Cm 66.0: No 3.00: Tp= 1.24]
13113 [I&Rc 4.00: SMIN: 81.24: SMAX=350.79: Hk: .010]
13114 [InterVntTime= 12.00]
13115 #
13116 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13117 # of 1.80
13118 CONTINUOUS HASHYD 1.0 01:01:00 1917.00 14.496 No.Date 34:24 36.76 415 .000
13119 [Cm 72.0: No 3.00: Tp= 4.00]
13120 [I&Rc 4.00: SMIN: 39.75: SMAX=264.99: Hk: .010]
13121 [InterVntTime= 12.00]
13122 #
13123 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13124 # of 1.75
13125 CONTINUOUS HASHYD 1.0 01:01:00 8176.00 36.418 No.Date 39:59 36.76 415 .000
13126 [Cm 66.0: No 3.00: Tp= 1.66]
13127 [I&Rc 4.00: SMIN: 81.24: SMAX=350.79: Hk: .010]
13128 [InterVntTime= 12.00]
13129 #
13130 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13131 # of 1.68
13132 CONTINUOUS HASHYD 1.0 01:01:00 1132.00 16.501 No.Date 30:52 40.82 461 .000
13133 [Cm 72.0: No 3.00: Tp= 8.00]
13134 [I&Rc 4.00: SMIN: 41.07: SMAX=287.10: Hk: .010]
13135 [InterVntTime= 12.00]
13136 #
13137 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13138 # of 1.82
13139 CONTINUOUS HASHYD 1.0 01:01:00 5666.00 37.663 No.Date 37:48 42.49 480 .000
13140 [Cm 72.0: No 3.00: Tp= 4.00]
13141 [I&Rc 4.00: SMIN: 61.90: SMAX=412.66: Hk: .010]
13142 [InterVntTime= 12.00]
13143 #
13144 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13145 # of 1.80
13146 CONTINUOUS HASHYD 1.0 01:01:00 131.00 3.259 No.Date 28:57 34.39 388 .000
13147 [Cm 63.0: No 3.00: Tp= .90]
13148 [I&Rc 4.00: SMIN: 59.42: SMAX=396.11: Hk: .010]
13149 [InterVntTime= 12.00]
13150 #
13151 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13152 # of 1.65
13153 CONTINUOUS HASHYD 1.0 01:01:00 3854.00 21.238 No.Date 38:28 36.76 415 .000
13154 [Cm 66.0: No 3.00: Tp= 1.42]
13155 [I&Rc 4.00: SMIN: 52.62: SMAX=350.79: Hk: .010]
13156 [InterVntTime= 12.00]
13157 #
13158 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13159 # of 1.82
13160 CONTINUOUS HASHYD 1.0 01:01:00 4948.00 32.056 No.Date 33:16 44.17 499 .000
13161 [Cm 57.0: No 3.00: Tp= 6.65]
13162 [I&Rc 4.00: SMIN: 59.42: SMAX=508.81: Hk: .010]
13163 [InterVntTime= 12.00]
13164 #
13165 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13166 # of 1.79
13167 CONTINUOUS HASHYD 1.0 01:01:00 165.00 1.511 No.Date 33:01 37.57 424 .000
13168 [Cm 67.0: No 3.00: Tp= 4.18]
13169 [I&Rc 4.00: SMIN: 61.90: SMAX=333.97: Hk: .010]
13170 [InterVntTime= 12.00]
13171 #
13172 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13173 # of 1.67
13174 CONTINUOUS HASHYD 1.0 01:01:00 224.00 9.576 No.Date 28:44 47.62 538 .000
13175 [Cm 77.0: No 3.00: Tp= 7.5]
13176 [I&Rc 4.00: SMIN: 31.15: SMAX=207.66: Hk: .010]
13177 [InterVntTime= 12.00]
13178 #
13179 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13180 # of 1.20
13181 CONTINUOUS HASHYD 1.0 01:01:00 4948.00 32.056 No.Date 33:16 44.17 499 .000
13182 [Cm 74.0: No 3.00: Tp= 4.45]
13183 [I&Rc 4.00: SMIN: 25.21: SMAX=244.49: Hk: .010]
13184 [InterVntTime= 12.00]
13185 #
13186 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13187 # of 1.61
13188 CONTINUOUS HASHYD 1.0 01:01:00 1412.00 10.184 No.Date 37:44 45.88 518 .000
13189 [Cm 72.0: No 3.00: Tp= 5.95]
13190 [I&Rc 4.00: SMIN: 39.75: SMAX=264.99: Hk: .010]
13191 [InterVntTime= 12.00]
13192 #
13193 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13194 # of 1.20
13195 CONTINUOUS HASHYD 1.0 01:01:00 585.00 14.953 No.Date 29:55 52.06 588 .000
13196 [Cm 81.0: No 3.00: Tp= .62]
13197 [I&Rc 4.00: SMIN: 25.21: SMAX=168.09: Hk: .010]
13198 [InterVntTime= 12.00]
13199 #
13200 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13201 # of 1.61
13202 CONTINUOUS HASHYD 1.0 01:01:00 1021.00 19.792 No.Date 30:45 51.16 578 .000
13203 [Cm 80.0: No 3.00: Tp= 4.46]
13204 [I&Rc 4.00: SMIN: 26.32: SMAX=175.50: Hk: .010]
13205 [InterVntTime= 12.00]
13206 #
13207 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13208 # of 1.20
13209 CONTINUOUS HASHYD 1.0 01:01:00 177.00 7.567 No.Date 28:44 47.62 538 .000
13210 [Cm 77.0: No 3.00: Tp= .75]
13211 [I&Rc 4.00: SMIN: 31.15: SMAX=207.66: Hk: .010]
13212 [InterVntTime= 12.00]
13213 #
13214 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13215 # of 1.20
13216 CONTINUOUS HASHYD 1.0 01:01:00 2977.00 40.130 No.Date 31:28 46.75 528 .000
13217 [Cm 76.0: No 3.00: Tp= 1.01]
13218 [I&Rc 4.00: SMIN: 31.15: SMAX=216.39: Hk: .010]
13219 [InterVntTime= 12.00]
13220 #
13221 # Starting with the addition of Jock River Headwater and Subwatershed 13
13222 #
13223 ROUTE CHANNEL -> 1.0 02:RSH_GM 3970.00 21.616 No.Date 36:52 35.18 n/a .000
13224 ADD HYD + 1.0 02:RSH_GM 3970.00 21.616 No.Date 36:52 35.18 n/a .000
13225 CONTINUOUS HASHYD 1.0 01:01:00 3974.00 8.203 No.Date 32:33 32.84 n/a .000
13226 [Cm 81.0: No 3.00: Tp= 3.25]
13227 [I&Rc 4.00: SMIN: 25.21: SMAX=168.09: Hk: .010]
13228 [InterVntTime= 12.00]
13229 #
13230 # Routing hydrographs
13231 #
13232 ROUTE CHANNEL -> 1.0 02:RSH_GM 3970.00 21.616 No.Date 36:52 35.18 n/a .000
13233 ADD HYD + 1.0 02:RSH_GM 3970.00 21.616 No.Date 36:52 35.18 n/a .000
13234 CONTINUOUS HASHYD 1.0 01:01:00 3974.00 8.203 No.Date 32:33 32.84 n/a .000
13235 [Cm 81.0: No 3.00: Tp= 3.25]
13236 [I&Rc 4.00: SMIN: 25.21: SMAX=168.09: Hk: .010]
13237 [InterVntTime= 12.00]
13238 #
13239 # Insertion of a reservoir to simulate the effects of the Goodwood Marsh
13240 #
13241 ROUTE RESERVOIR -> 1.0 02:RSH_GM 7725.00 32.845 No.Date 39:44 34.24 n/a .000
13242 [MstOfsed= 1.796E+03 m]
13243 [InterVntTime= 12.00]
13244 #
13245 # Sum of hydrographs from Node 13 routed to Node 13A
13246 # (Approximated cross-section - see cross-section 258)
13247 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
13248 #
13249 ROUTE CHANNEL -> 1.0 02:RSH_GM 3974.00 8.203 No.Date 32:33 32.84 n/a .000
13250 [I/S/n= 592.2/.076/.040]
13251 [Vmax= 589.0/Dmax= 4.178]
13252 #
13253 # Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
13254 #
13255 ROUTE CHANNEL -> 1.0 02:RSH_GM 3974.00 8.203 No.Date 32:33 32.84 n/a .000
13256 [I/S/n= 592.2/.076/.040]
13257 [Vmax= 589.0/Dmax= 4.178]
13258 #
13259 # Addition of Subwatershed Jock River at Ashton to Node 12
13260 #
13261 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13262 [I/S/n= 592.2/.076/.040]
13263 [Vmax= 589.0/Dmax= 4.178]
13264 #
13265 # Sum of hydrographs from Node 12 routed to Node 11
13266 # (Approximated cross-section - see cross-section 258)
13267 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
13268 #
13269 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13270 [I/S/n= 592.2/.076/.040]
13271 [Vmax= 589.0/Dmax= 4.178]
13272 #
13273 # Sum of hydrographs from Node 11 routed to Node 10
13274 #
13275 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13276 [I/S/n= 592.2/.076/.040]
13277 [Vmax= 589.0/Dmax= 4.178]
13278 #
13279 # Addition of Subwatershed 11 and No Name Creek to Node 11
13280 #
13281 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13282 [I/S/n= 592.2/.076/.040]
13283 [Vmax= 589.0/Dmax= 4.178]
13284 #
13285 # Sum of hydrographs from Node 11 routed to Node 10
13286 #
13287 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13288 [I/S/n= 592.2/.076/.040]
13289 [Vmax= 589.0/Dmax= 4.178]
13290 #
13291 # Addition of Subwatershed 11 and No Name Creek to Node 11
13292 #
13293 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13294 [I/S/n= 592.2/.076/.040]
13295 [Vmax= 589.0/Dmax= 4.178]
13296 #
13297 # Sum of hydrographs from Node 11 routed to Node 10
13298 #
13299 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13300 [I/S/n= 592.2/.076/.040]
13301 [Vmax= 589.0/Dmax= 4.178]
13302 #
13303 # Addition of Subwatershed 11 and No Name Creek to Node 11
13304 #
13305 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13306 [I/S/n= 592.2/.076/.040]
13307 [Vmax= 589.0/Dmax= 4.178]
13308 #
13309 # Sum of hydrographs from Node 11 routed to Node 10
13310 #
13311 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13312 [I/S/n= 592.2/.076/.040]
13313 [Vmax= 589.0/Dmax= 4.178]
13314 #
13315 # Addition of Subwatershed 11 and No Name Creek to Node 11
13316 #
13317 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13318 [I/S/n= 592.2/.076/.040]
13319 [Vmax= 589.0/Dmax= 4.178]
13320 #
13321 # Sum of hydrographs from Node 11 routed to Node 10
13322 #
13323 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13324 [I/S/n= 592.2/.076/.040]
13325 [Vmax= 589.0/Dmax= 4.178]
13326 #
13327 # Addition of Subwatershed 11 and No Name Creek to Node 11
13328 #
13329 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13330 [I/S/n= 592.2/.076/.040]
13331 [Vmax= 589.0/Dmax= 4.178]
13332 #
13333 # Sum of hydrographs from Node 11 routed to Node 10
13334 #
13335 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13336 [I/S/n= 592.2/.076/.040]
13337 [Vmax= 589.0/Dmax= 4.178]
13338 #
13339 # Addition of Subwatershed 11 and No Name Creek to Node 11
13340 #
13341 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13342 [I/S/n= 592.2/.076/.040]
13343 [Vmax= 589.0/Dmax= 4.178]
13344 #
13345 # Sum of hydrographs from Node 11 routed to Node 10
13346 #
13347 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13348 [I/S/n= 592.2/.076/.040]
13349 [Vmax= 589.0/Dmax= 4.178]
13350 #
13351 # Addition of Subwatershed 11 and No Name Creek to Node 11
13352 #
13353 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13354 [I/S/n= 592.2/.076/.040]
13355 [Vmax= 589.0/Dmax= 4.178]
13356 #
13357 # Sum of hydrographs from Node 11 routed to Node 10
13358 #
13359 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13360 [I/S/n= 592.2/.076/.040]
13361 [Vmax= 589.0/Dmax= 4.178]
13362 #
13363 # Addition of Subwatershed 11 and No Name Creek to Node 11
13364 #
13365 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13366 [I/S/n= 592.2/.076/.040]
13367 [Vmax= 589.0/Dmax= 4.178]
13368 #
13369 # Sum of hydrographs from Node 11 routed to Node 10
13370 #
13371 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13372 [I/S/n= 592.2/.076/.040]
13373 [Vmax= 589.0/Dmax= 4.178]
13374 #
13375 # Addition of Subwatershed 11 and No Name Creek to Node 11
13376 #
13377 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13378 [I/S/n= 592.2/.076/.040]
13379 [Vmax= 589.0/Dmax= 4.178]
13380 #
13381 # Sum of hydrographs from Node 11 routed to Node 10
13382 #
13383 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13384 [I/S/n= 592.2/.076/.040]
13385 [Vmax= 589.0/Dmax= 4.178]
13386 #
13387 # Addition of Subwatershed 11 and No Name Creek to Node 11
13388 #
13389 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13390 [I/S/n= 592.2/.076/.040]
13391 [Vmax= 589.0/Dmax= 4.178]
13392 #
13393 # Sum of hydrographs from Node 11 routed to Node 10
13394 #
13395 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13396 [I/S/n= 592.2/.076/.040]
13397 [Vmax= 589.0/Dmax= 4.178]
13398 #
13399 # Addition of Subwatershed 11 and No Name Creek to Node 11
13400 #
13401 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13402 [I/S/n= 592.2/.076/.040]
13403 [Vmax= 589.0/Dmax= 4.178]
13404 #
13405 # Sum of hydrographs from Node 11 routed to Node 10
13406 #
13407 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13408 [I/S/n= 592.2/.076/.040]
13409 [Vmax= 589.0/Dmax= 4.178]
13410 #
13411 # Addition of Subwatershed 11 and No Name Creek to Node 11
13412 #
13413 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13414 [I/S/n= 592.2/.076/.040]
13415 [Vmax= 589.0/Dmax= 4.178]
13416 #
13417 # Sum of hydrographs from Node 11 routed to Node 10
13418 #
13419 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13420 [I/S/n= 592.2/.076/.040]
13421 [Vmax= 589.0/Dmax= 4.178]
13422 #
13423 # Addition of Subwatershed 11 and No Name Creek to Node 11
13424 #
13425 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13426 [I/S/n= 592.2/.076/.040]
13427 [Vmax= 589.0/Dmax= 4.178]
13428 #
13429 # Sum of hydrographs from Node 11 routed to Node 10
13430 #
13431 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13432 [I/S/n= 592.2/.076/.040]
13433 [Vmax= 589.0/Dmax= 4.178]
13434 #
13435 # Addition of Subwatershed 11 and No Name Creek to Node 11
13436 #
13437 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13438 [I/S/n= 592.2/.076/.040]
13439 [Vmax= 589.0/Dmax= 4.178]
13440 #
13441 # Sum of hydrographs from Node 11 routed to Node 10
13442 #
13443 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13444 [I/S/n= 592.2/.076/.040]
13445 [Vmax= 589.0/Dmax= 4.178]
13446 #
13447 # Addition of Subwatershed 11 and No Name Creek to Node 11
13448 #
13449 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13450 [I/S/n= 592.2/.076/.040]
13451 [Vmax= 589.0/Dmax= 4.178]
13452 #
13453 # Sum of hydrographs from Node 11 routed to Node 10
13454 #
13455 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13456 [I/S/n= 592.2/.076/.040]
13457 [Vmax= 589.0/Dmax= 4.178]
13458 #
13459 # Addition of Subwatershed 11 and No Name Creek to Node 11
13460 #
13461 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13462 [I/S/n= 592.2/.076/.040]
13463 [Vmax= 589.0/Dmax= 4.178]
13464 #
13465 # Sum of hydrographs from Node 11 routed to Node 10
13466 #
13467 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13468 [I/S/n= 592.2/.076/.040]
13469 [Vmax= 589.0/Dmax= 4.178]
13470 #
13471 # Addition of Subwatershed 11 and No Name Creek to Node 11
13472 #
13473 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13474 [I/S/n= 592.2/.076/.040]
13475 [Vmax= 589.0/Dmax= 4.178]
13476 #
13477 # Sum of hydrographs from Node 11 routed to Node 10
13478 #
13479 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13480 [I/S/n= 592.2/.076/.040]
13481 [Vmax= 589.0/Dmax= 4.178]
13482 #
13483 # Addition of Subwatershed 11 and No Name Creek to Node 11
13484 #
13485 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13486 [I/S/n= 592.2/.076/.040]
13487 [Vmax= 589.0/Dmax= 4.178]
13488 #
13489 # Sum of hydrographs from Node 11 routed to Node 10
13490 #
13491 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13492 [I/S/n= 592.2/.076/.040]
13493 [Vmax= 589.0/Dmax= 4.178]
13494 #
13495 # Addition of Subwatershed 11 and No Name Creek to Node 11
13496 #
13497 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13498 [I/S/n= 592.2/.076/.040]
13499 [Vmax= 589.0/Dmax= 4.178]
13500 #
13501 # Sum of hydrographs from Node 11 routed to Node 10
13502 #
13503 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13504 [I/S/n= 592.2/.076/.040]
13505 [Vmax= 589.0/Dmax= 4.178]
13506 #
13507 # Addition of Subwatershed 11 and No Name Creek to Node 11
13508 #
13509 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13510 [I/S/n= 592.2/.076/.040]
13511 [Vmax= 589.0/Dmax= 4.178]
13512 #
13513 # Sum of hydrographs from Node 11 routed to Node 10
13514 #
13515 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13516 [I/S/n= 592.2/.076/.040]
13517 [Vmax= 589.0/Dmax= 4.178]
13518 #
13519 # Addition of Subwatershed 11 and No Name Creek to Node 11
13520 #
13521 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13522 [I/S/n= 592.2/.076/.040]
13523 [Vmax= 589.0/Dmax= 4.178]
13524 #
13525 # Sum of hydrographs from Node 11 routed to Node 10
13526 #
13527 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13528 [I/S/n= 592.2/.076/.040]
13529 [Vmax= 589.0/Dmax= 4.178]
13530 #
13531 # Addition of Subwatershed 11 and No Name Creek to Node 11
13532 #
13533 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13534 [I/S/n= 592.2/.076/.040]
13535 [Vmax= 589.0/Dmax= 4.178]
13536 #
13537 # Sum of hydrographs from Node 11 routed to Node 10
13538 #
13539 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13540 [I/S/n= 592.2/.076/.040]
13541 [Vmax= 589.0/Dmax= 4.178]
13542 #
13543 # Addition of Subwatershed 11 and No Name Creek to Node 11
13544 #
13545 ROUTE CHANNEL -> 1.0 02:RSH_GM 1781.00 19.695 No.Date 32:38 42.49 480 .000
13546 [I/S/n= 592.2/.076/.040]
13547 [Vmax=
```

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13465# #
13466# ROUTE CHANNEL -> 1.0 02:18_NSA 4684.01 89.756_Date 34:38 37.51 n/a .000
13467# [RDP: 1.00] out< 1.0 01:82 4684.01 89.756_Date 34:38 37.51 n/a .000
13468# [L/S/n: 4630./ .043/.055]
13470# [Vmax: .904/Dmax: 3.866]
13471#
13472# # Addition of Subwatershed 4 and Leamy Creek to Node 4
13473#
13474# ROUTE CHANNEL -> 1.0 02:18_NSA 4684.01 89.756_Date 34:38 37.51 n/a .000
13475# ADD HYD + 1.0 02:18 4684.01 89.756_Date 29:55 37.51 n/a .000
13476# [L/S/n: 4630./ .043/.055]
13477# [Vmax: .904/Dmax: 3.866]
13478#
13479# ROUTE CHANNEL -> 1.0 02:18_NSA 4684.01 89.756_Date 34:38 37.51 n/a .000
13480# ADD HYD + 1.0 02:18 4684.01 89.756_Date 29:55 37.51 n/a .000
13481# [L/S/n: 4630./ .043/.055]
13482# [Vmax: .904/Dmax: 3.866]
13483#
13484# # Sum of hydrographs from Node 4 routed to Node 2
13485# # Section 9
13486# #
13487# ROUTE CHANNEL -> 1.0 02:18_NSA 4847.00 96.618_Date 35:12 37.97 n/a .000
13488# [RDP: 1.00] out< 1.0 01:82 4847.00 96.618_Date 35:12 37.97 n/a .000
13489# [L/S/n: 1867./ .067/.080]
13491# [Vmax: .944/Dmax: 3.929]
13492#
13493# # Addition of Subwatershed 2 with Monahan Drain and Smith Drain to Node 2
13494#
13495# ROUTE CHANNEL -> 1.0 02:18_NSA 4847.00 96.618_Date 35:12 37.97 n/a .000
13496# ADD HYD + 1.0 02:18 4847.00 96.618_Date 35:12 37.97 n/a .000
13497# [L/S/n: 1867./ .067/.080]
13498# [Vmax: .944/Dmax: 3.929]
13499#
13500# # Sum of hydrographs from Node 2 routed to Node 1
13501# # Section 10
13502# #
13503# ROUTE CHANNEL -> 1.0 02:18_NSA 52483.00 143.580_Date 32:59 38.76 n/a .000
13504# [RDP: 1.00] out< 1.0 01:82 52483.00 143.580_Date 32:59 38.76 n/a .000
13505# [L/S/n: 2127./ .050/.055]
13507# [Vmax: .833/Dmax: .797]
13508#
13509# # Sum of hydrographs from Node 2 routed to Node 416
13510# #
13511# # Hydrograph from Node 2 routed to Node 416
13512# # Channel X-Section obtained from RYCA Hydraulic Model - Station 9025
13513#
13514# ROUTE CHANNEL -> 1.0 02:18_NSA 52483.00 143.580_Date 32:59 38.76 n/a .000
13515# [RDP: 1.00] out< 1.0 01:82 52483.00 143.580_Date 32:59 38.76 n/a .000
13516# [L/S/n: 2127./ .050/.055]
13518# [Vmax: .833/Dmax: .797]
13519#
13520# # Catchment SM-1a
13521# # Portion of RYCA catchment SM_1 outside of Reach 3 subwatershed
13522# # Undeveloped agricultural land
13523# #
13524# CONTINUOUS STANDBY 1.0 01:01-4 536.42 7.274_Date 31:14 40.95 .462 .000
13525# [RDP: 1.00] out< 1.0 01:01-4 536.42 7.274_Date 31:14 40.95 .462 .000
13526# [L/S/n: 3.00] Tm: 1.05]
13527# [Vmax: 4.00] SMIN: 39.75; SMAX:264.99; SK: .010]
13528# [InterEventTime: 12.00]
13529# [Previous area: IArea: 4.67;SLDP: .32;LDL:50.0;NDP: .250;SDCP: .0]
13530# [Impervious area: IArea: 1.57;SLDP: .50;LDL:1.18;NMI: .013;ICI: .0]
13531# [ISa: 4.00] IArea: 4.00]
13532# [Sump: 1.0]
13533# [Sump: 1.0]
13534# ROUTE RESERVOIR -> 1.0 02:18-8 52483.00 143.580_Date 32:59 38.76 n/a .000
13535# out< 1.0 01:17-STR 3.51 .240_Date 28:18 70.42 n/a .000
13536# overfill over 1.0 01:17-STR 3.51 .240_Date 28:18 70.42 n/a .000
13537# [NstOfsed:1.056E+00 m3, TokOfVol:0.000E+00 m3, N-ovf: 0, TotOfDrfV: 0.hrs]
13538# [L/S/n: 592./ .230/.043]
13539# [Vmax: 611/Dmax: 1.215]
13540#
13541# CONTINUOUS STANDBY 1.0 01:17-3 71 .138_Date 28:00 55.78 630 .000
13542# [RDP: 1.00] out< 1.0 01:17-3 71 .138_Date 28:00 55.78 630 .000
13543# [L/S/n: 592./ .230/.043]
13544# [Vmax: 611/Dmax: 1.215]
13545#
13546# # Hydrograph from Node 416 routed to Node 4 at Office drain
13547# # Channel X-Section obtained from RYCA Hydraulic Model - Station 7245
13548# #
13549# ROUTE CHANNEL -> 1.0 02:18_NSA 53064.36 145.020_Date 33:31 38.79 n/a .000
13550# [RDP: 1.00] out< 1.0 01:82 53064.36 145.020_Date 33:31 38.79 n/a .000
13551# [L/S/n: 497./ .302/.055]
13553# [Vmax: 1.728/Dmax: 3.267]
13554#
13555# # Catchment OKRFEF
13556# # To V-Office drain (north of the Site)
13557# # - Developed with assumed 43 imp.
13558# # - 2020-12-01 add Okrfele model (Area 513.02 HA) instead of current Okrfele (Area 513.02 HA)
13559# # - 2020-11-20 Okrfele model was added as per the NOVATEC SWMM2D model (Cili-Date 2014).
13560# #
13561# CONTINUOUS STANDBY 1.0 01:01-4 63.72 1.380_Date 28:58 30.74 347 .000
13562# [RDP: 1.00] out< 1.0 01:01-4 63.72 1.380_Date 28:58 30.74 347 .000
13563# [L/S/n: 3.00] Tm: 1.05]
13564# [Vmax: 4.00] SMIN: 64.50; SMAX:430.01; SK: .010]
13565# [InterEventTime: 12.00]
13566# [Previous area: IArea: 4.67;SLDP: .32;LDL:50.0;NDP: .250;SDCP: .0]
13567# [Impervious area: IArea: 1.57;SLDP: .50;LDL:1.18;NMI: .013;ICI: .0]
13568# [ISa: 4.00] IArea: 4.00]
13569# [Sump: 1.0]
13570# [Sump: 1.0]
13571# ROUTE RESERVOIR -> 1.0 02:18-8 46.94 .650_Date 28:59 21.79 .246 .000
13572# out< 1.0 01:17-STR 4.51 .240_Date 28:18 70.42 n/a .000
13573# overfill over 1.0 01:17-STR 4.51 .240_Date 28:18 70.42 n/a .000
13574# [NstOfsed:1.056E+00 m3, TokOfVol:0.000E+00 m3, N-ovf: 0, TotOfDrfV: 0.hrs]
13575# [L/S/n: 960./ .630/.043]
13576# [Vmax: 928./ .230/.043]
13577#
13578# CONTINUOUS STANDBY 1.0 01:17-4 35 .069_Date 28:00 55.78 630 .000
13579# [RDP: 1.00] out< 1.0 01:17-4 35 .069_Date 28:00 55.78 630 .000
13580# [L/S/n: 960./ .630/.043]
13581# [Vmax: 928./ .230/.043]
13582#
13583# # Catchment OKRFEF
13584# # To V-Office drain (north of the Site)
13585# # - Developed with assumed 43 imp.
13586# # - 2020-12-01 add Okrfele model (Area 513.02 HA) instead of current Okrfele (Area 513.02 HA)
13587# # - 2020-11-20 Okrfele model was added as per the NOVATEC SWMM2D model (Cili-Date 2014).
13588# #
13589# CONTINUOUS STANDBY 1.0 01:01-4 63.72 1.380_Date 28:58 30.74 347 .000
13590# [RDP: 1.00] out< 1.0 01:01-4 63.72 1.380_Date 28:58 30.74 347 .000
13591# [L/S/n: 3.00] Tm: 1.05]
13592# [Vmax: 4.00] SMIN: 64.50; SMAX:430.01; SK: .010]
13593# [InterEventTime: 12.00]
13594# [Previous area: IArea: 4.67;SLDP: .32;LDL:50.0;NDP: .250;SDCP: .0]
13595# [Impervious area: IArea: 1.57;SLDP: .50;LDL:1.18;NMI: .013;ICI: .0]
13596# [ISa: 4.00] IArea: 4.00]
13597# [Sump: 1.0]
13598# [Sump: 1.0]
13599# ROUTE RESERVOIR -> 1.0 02:18-8 46.94 .650_Date 28:59 21.79 .246 .000
13600# out< 1.0 01:17-STR 4.51 .240_Date 28:18 70.42 n/a .000
13601# overfill over 1.0 01:17-STR 4.51 .240_Date 28:18 70.42 n/a .000
13602# [NstOfsed:1.056E+00 m3, TokOfVol:0.000E+00 m3, N-ovf: 0, TotOfDrfV: 0.hrs]
13603# [L/S/n: 960./ .630/.043]
13604# [Vmax: 928./ .230/.043]
13605#
13606# CONTINUOUS STANDBY 1.0 01:17-4 35 .069_Date 28:00 55.78 630 .000
13607# [RDP: 1.00] out< 1.0 01:17-4 35 .069_Date 28:00 55.78 630 .000
13608# [L/S/n: 960./ .630/.043]
13609# [Vmax: 928./ .230/.043]
13610#
13611# # Hydrograph from Node 416 routed to Node 4 at Office drain
13612# # Channel X-Section obtained from RYCA Hydraulic Model - Station 7245
13613# #
13614# ROUTE CHANNEL -> 1.0 02:18_NSA 53064.36 145.020_Date 33:31 38.79 n/a .000
13615# [RDP: 1.00] out< 1.0 01:82 53064.36 145.020_Date 33:31 38.79 n/a .000
13616# [L/S/n: 497./ .302/.055]
13618# [Vmax: 1.728/Dmax: 3.267]
13619#
13620# # Catchment OKRFEF
13621# # To V-Office drain (north of the Site)
13622# # - Developed with assumed 43 imp.
13623# # - 2020-12-01 add Okrfele model (Area 513.02 HA) instead of current Okrfele (Area 513.02 HA)
13624# # - 2020-11-20 Okrfele model was added as per the NOVATEC SWMM2D model (Cili-Date 2014).
13625# #
13626# CONTINUOUS STANDBY 1.0 01:01-4 63.72 1.380_Date 28:58 30.74 347 .000
13627# [RDP: 1.00] out< 1.0 01:01-4 63.72 1.380_Date 28:58 30.74 347 .000
13628# [L/S/n: 3.00] Tm: 1.05]
13629# [Vmax: 4.00] SMIN: 64.50; SMAX:430.01; SK: .010]
13630# [InterEventTime: 12.00]
13631# [Previous area: IArea: 4.67;SLDP: .32;LDL:50.0;NDP: .250;SDCP: .0]
13632# [Impervious area: IArea: 1.57;SLDP: .50;LDL:1.18;NMI: .013;ICI: .0]
13633# [ISa: 4.00] IArea: 4.00]
13634# [Sump: 1.0]
13635# [Sump: 1.0]
13636# ROUTE RESERVOIR -> 1.0 02:18-8 46.94 .650_Date 28:59 21.79 .246 .000
13637# out< 1.0 01:17-STR 4.51 .240_Date 28:18 70.42 n/a .000
13638# overfill over 1.0 01:17-STR 4.51 .240_Date 28:18 70.42 n/a .000
13639# [NstOfsed:1.056E+00 m3, TokOfVol:0.000E+00 m3, N-ovf: 0, TotOfDrfV: 0.hrs]
13640# [L/S/n: 960./ .630/.043]
13641# [Vmax: 928./ .230/.043]
13642#
13643# CONTINUOUS STANDBY 1.0 01:17-4 35 .069_Date 28:00 55.78 630 .000
13644# [RDP: 1.00] out< 1.0 01:17-4 35 .069_Date 28:00 55.78 630 .000
13645# [L/S/n: 960./ .630/.043]
13646# [Vmax: 928./ .230/.043]
13647#
13648# # Hydrograph from Node 416 routed to Node 4 at Office drain
13649# # Channel X-Section obtained from RYCA Hydraulic Model - Station 7245
13650# #
13651# ROUTE CHANNEL -> 1.0 02:18_NSA 53064.36 145.020_Date 33:31 38.79 n/a .000
13652# [RDP: 1.00] out< 1.0 01:82 53064.36 145.020_Date 33:31 38.79 n/a .000
13653# [L/S/n: 497./ .302/.055]
13655# [Vmax: 1.728/Dmax: 3.267]
13656#
13657# # Catchment OKRFEF
13658# # To V-Office drain (north of the Site)
13659# # - Developed with assumed 43 imp.
13660# # - 2020-12-01 add Okrfele model (Area 513.02 HA) instead of current Okrfele (Area 513.02 HA)
13661# # - 2020-11-20 Okrfele model was added as per the NOVATEC SWMM2D model (Cili-Date 2014).
13662# #
13663# CONTINUOUS STANDBY 1.0 01:01-4 63.72 1.380_Date 28:58 30.74 347 .000
13664# [RDP: 1.00] out< 1.0 01:01-4 63.72 1.380_Date 28:58 30.74 347 .000
13665# [L/S/n: 3.00] Tm: 1.05]
13666# [Vmax: 4.00] SMIN: 64.50; SMAX:430.01; SK: .010]
13667# [InterEventTime: 12.00]
13668# [Previous area: IArea: 4.67;SLDP: .32;LDL:50.0;NDP: .250;SDCP: .0]
13669# [Impervious area: IArea: 1.57;SLDP: .50;LDL:1.18;NMI: .013;ICI: .0]
13670# [ISa: 4.00] IArea: 4.00]
13671# [Sump: 1.0]
13672# [Sump: 1.0]
13673# ROUTE RESERVOIR -> 1.0 02:18-8 46.94 .650_Date 28:59 21.79 .246 .000
13674# out< 1.0 01:17-STR 4.51 .240_Date 28:18 70.42 n/a .000
13675# overfill over 1.0 01:17-STR 4.51 .240_Date 28:18 70.42 n/a .000
13676# [NstOfsed:1.056E+00 m3, TokOfVol:0.000E+00 m3, N-ovf: 0, TotOfDrfV: 0.hrs]
13677# [L/S/n: 960./ .630/.043]
13678# [Vmax: 928./ .230/.043]
13679#
13680# CONTINUOUS STANDBY 1.0 01:17-4 35 .069_Date 28:00 55.78 630 .000
13681# [RDP: 1.00] out< 1.0 01:17-4 35 .069_Date 28:00 55.78 630 .000
13682# [L/S/n: 960./ .630/.043]
13683# [Vmax: 928./ .230/.043]
13684#
13685# # Hydrograph from Node 416 routed to Node 4 at Office drain
13686# # Channel X-Section obtained from RYCA Hydraulic Model - Station 7245
13687# #
13688# ROUTE CHANNEL -> 1.0 02:18_NSA 53064.36 145.020_Date 33:31 38.79 n/a .000
13689# [RDP: 1.00] out< 1.0 01:82 53064.36 145.020_Date 33:31 38.79 n/a .000
13690# [L/S/n: 497./ .302/.055]
13692# [Vmax: 1.728/Dmax: 3.267]
13693#
13694# # Catchment OKRFEF
13695# # To V-Office drain (north of the Site)
13696# # - Developed with assumed 43 imp.
13697# # - 2020-12-01 add Okrfele model (Area 513.02 HA) instead of current Okrfele (Area 513.02 HA)
13698# # - 2020-11-20 Okrfele model was added as per the NOVATEC SWMM2D model (Cili-Date 2014).
13699# #
13700# CONTINUOUS STANDBY 1.0 01:01-4 63.72 1.380_Date 28:58 30.74 347 .000
13701# [RDP: 1.00] out< 1.0 01:01-4 63.72 1.380_Date 28:58 30.74 347 .000
13702# [L/S/n: 3.00] Tm: 1.05]
13703# [Vmax: 4.00] SMIN: 64.50; SMAX:430.01; SK: .010]
13704# [InterEventTime: 12.00]
13705# [Previous area: IArea: 4.67;SLDP: .32;LDL:50.0;NDP: .250;SDCP: .0]
13706# [Impervious area: IArea: 1.57;SLDP: .50;LDL:1.18;NMI: .013;ICI: .0]
13707# [ISa: 4.00] IArea: 4.00]
13708# [Sump: 1.0]
13709# [Sump: 1.0]
13710# ROUTE RESERVOIR -> 1.0 02:18-8 46.94 .650_Date 28:59 21.79 .246 .000
13711# out< 1.0 01:17-STR 4.51 .240_Date 28:18 70.42 n/a .000
13712# overfill over 1.0 01:17-STR 4.51 .240_Date 28:18 70.42 n/a .000
13713# [NstOfsed:1.056E+00 m3, TokOfVol:0.000E+00 m3, N-ovf: 0, TotOfDrfV: 0.hrs]
13714# [L/S/n: 960./ .630/.043]
13715# [Vmax: 928./ .230/.043]
13716#
13717# CONTINUOUS STANDBY 1.0 01:17-4 35 .069_Date 28:00 55.78 630 .000
13718# [RDP: 1.00] out< 1.0 01:17-4 35 .069_Date 28:00 55.78 630 .000
13719# [L/S/n: 960./ .630/.043]
13720# [Vmax: 928./ .230/.043]
13721#
13722# # Hydrograph from Node 416 routed to Node 4 at Office drain
13723# # Channel X-Section obtained from RYCA Hydraulic Model - Station 7245
13724# #
13725# ROUTE CHANNEL -> 1.0 02:18_NSA 53064.36 145.020_Date 33:31 38.79 n/a .000
13726# [RDP: 1.00] out< 1.0 01:82 53064.36 145.020_Date 33:31 38.79 n/a .000
13727# [L/S/n: 497./ .302/.055]
13729# [Vmax: 1.728/Dmax: 3.267]
13730#
13731# # Catchment OKRFEF
13732# # To V-Office drain (north of the Site)
13733# # - Developed with assumed 43 imp.
13734# # - 2020-12-01 add Okrfele model (Area 513.02 HA) instead of current Okrfele (Area 513.02 HA)
13735# # - 2020-11-20 Okrfele model was added as per the NOVATEC SWMM2D model (Cili-Date 2014).
13736# #
13737# CONTINUOUS STANDBY 1.0 01:01-4 63.72 1.380_Date 28:58 30.74 347 .000
13738# [RDP: 1.00] out< 1.0 01:01-4 63.72 1.380_Date 28:58 30.74 347 .000
13739# [L/S/n: 3.00] Tm: 1.05]
13740# [Vmax: 4.00] SMIN: 64.50; SMAX:430.01; SK: .010]
13741# [InterEventTime: 12.00]
13742# [Previous area: IArea: 4.67;SLDP: .32;LDL:50.0;NDP: .250;SDCP: .0]
13743# [Impervious area: IArea: 1.57;SLDP: .50;LDL:1.18;NMI: .013;ICI: .0]
13744# [ISa: 4.00] IArea: 4.00]
13745# [Sump: 1.0]
13746# [Sump: 1.0]
13747# ROUTE RESERVOIR -> 1.0 02:18-8 46.94 .650_Date 28:59 21.79 .246 .000
13748# out< 1.0 01:17-STR 4.51 .240_Date 28:18 70.42 n/a .000
13749# overfill over 1.0 01:17-STR 4.51 .240_Date 28:18 70.42 n/a .000
13750# [NstOfsed:1.056E+00 m3, TokOfVol:0.000E+00 m3, N-ovf: 0, TotOfDrfV: 0.hrs]
13751# [L/S/n: 960./ .630/.043]
13752# [Vmax: 928./ .230/.043]
13753#
13754# CONTINUOUS STANDBY 1.0 01:17-4 35 .069_Date 28:00 55.78 630 .000
13755# [RDP: 1.00] out< 1.0 01:17-4 35 .069_Date 28:00 55.78 630 .000
13756# [L/S/n: 960./ .630/.043]
13757# [Vmax: 928./ .230/.043]
13758#
13759# # Hydrograph from Node 416 routed to Node 4 at Office drain
13760# # Channel X-Section obtained from RYCA Hydraulic Model - Station 7245
13761# #
13762# ROUTE CHANNEL -> 1.0 02:18_NSA 53064.36 145.020_Date 33:31 38.79 n/a .000
13763# [RDP: 1.00] out< 1.0 01:82 53064.36 145.020_Date 33:31 38.79 n/a .000
13764# [L/S/n: 497./ .302/.055]
13766# [Vmax: 1.728/Dmax: 3.267]
13767#
13768# # Catchment OKRFEF
13769# # To V-Office drain (north of the Site)
13770# # - Developed with assumed 43 imp.
13771# # - 2020-12-01 add Okrfele model (Area 513.02 HA) instead of current Okrfele (Area 513.02 HA)
13772# # - 2020-11-20 Okrfele model was added as per the NOVATEC SWMM2D model (Cili-Date 2014).
13773# #
13774# CONTINUOUS STANDBY 1.0 01:01-4 63.72 1.380_Date 28:58 30.74 347 .000
13775# [RDP: 1.00] out< 1.0 01:01-4 63.72 1.380_Date 28:58 30.74 347 .000
13776# [L/S/n: 3.00] Tm: 1.05]
13777# [Vmax: 4.00] SMIN: 64.50; SMAX:430.01; SK: .010]
13778# [InterEventTime: 12.00]
13779# [Previous area: IArea: 4.67;SLDP: .32;LDL:50.0;NDP: .250;SDCP: .0]
13780# [Impervious area: IArea: 1.57;SLDP: .50;LDL:1.18;NMI: .013;ICI: .0]
13781# [ISa: 4.00] IArea: 4.00]
13782# [Sump: 1.0]
13783# [Sump: 1.0]
13784# ROUTE RESERVOIR -> 1.0 02:18-8 46.94 .650_Date 28:59 21.79 .246 .000
13785# out< 1.0 01:17-STR 4.51 .240_Date 28:18 70.42 n/a .000
13786# overfill over 1.0 01:17-STR 4.51 .240_Date 28:18 70.42 n/a .000
13787# [NstOfsed:1.056E+00 m3, TokOfVol:0.000E+00 m3, N-ovf: 0, TotOfDrfV: 0.hrs]
13788# [L/S/n: 960./ .630/.043]
13789# [Vmax: 928./ .230/.043]
13790#
13791# CONTINUOUS STANDBY 1.0 01:17-4 35 .069_Date 28:00 55.78 630 .000
13792# [RDP: 1.00] out< 1.0 01:17-4 35 .069_Date 28:00 55.78 630 .000
13793# [L/S/n: 960./ .630/.043]
13794# [Vmax: 928./ .230/.043]
13795#
13796# # Hydrograph from Node 416 routed to Node 4 at Office drain
13797# # Channel X-Section obtained from RYCA Hydraulic Model - Station 7245
13798# #
13799# ROUTE CHANNEL -> 1.0 02:18_NSA 53064.36 145.020_Date 33:31 38.79 n/a .000
13800# [RDP: 1.00] out< 1.0 01:82 53064.36 145.020_Date 33:31 38.79 n/a .000
13801# [L/S/n: 497./ .302/.055]
13803# [Vmax: 1.728/Dmax: 3.267]
13804#
13805# # Catchment OKRFEF
13806# # To V-Office drain (north of the Site)
13807# # - Developed with assumed 43 imp.
13808# # - 2020-12-01 add Okrfele model (Area 513.02 HA) instead of current Okrfele (Area 513.02 HA)
13809# # - 2020-11-20 Okrfele model was added as per the NOVATEC SWMM2D model (Cili-Date 2014).
13810# #
13811# CONTINUOUS STANDBY 1.0 01:01-4 63.72 1.380_Date 28:58 30.74 347 .000
13812# [RDP: 1.00] out< 1.0 01:01-4 63.72 1.380_Date 28:58 30.74 347 .000
13813# [L/S/n: 3.00] Tm: 1.05]
13814# [Vmax: 4.00] SMIN: 64.50; SMAX:430.01; SK: .010]
13815# [InterEventTime: 12.00]
13816# [Previous area: IArea: 4.67;SLDP: .32;LDL:50.0;NDP: .250;SDCP: .0]
13817# [Impervious area: IArea: 1.57;SLDP: .50;LDL:1.18;NMI: .013;ICI: .0]
13818# [ISa: 4.00] IArea: 4.00]
13819# [Sump: 1.0]
13820# [Sump: 1.0]
13821# ROUTE RESERVOIR -> 1.0 02:18-8 46.94 .650_Date 28:59 21.79 .246 .000
13822# out< 1.0 01:17-STR 4.51 .240_Date 28:18 70.42 n/a .000
13823# overfill over 1.0 01:17-STR 4.51 .240_Date 28:18 70.42 n/a .000
13824# [NstOfsed:1.056E+00 m3, TokOfVol:0.000E+00 m3, N-ovf: 0, TotOfDrfV: 0.hrs]
13825# [L/S/n: 960./ .630/.043]
13826# [Vmax: 928./ .230/.043]
13827#
13828# CONTINUOUS STANDBY 1.0 01:17-4 35 .069_Date 28:00 55.78 630 .000
13829# [RDP: 1.00] out< 1.0 01:17-4 35 .069_Date 28:00 55.78 630 .000
13830# [L/S/n: 960./ .630/.043]
13831# [Vmax: 928./ .230/.043]
13832#
13833# # Hydrograph from Node 416 routed to Node 4 at Office drain
13834# # Channel X-Section obtained from RYCA Hydraulic Model - Station 7245
13835# #
13836# ROUTE CHANNEL -> 1.0 02:18_NSA 53064.36 145.020_Date 33:31 38.79 n/a .000
13837# [RDP: 1.00] out< 1.0 01:82 53064.36 145.020_Date 33:31 38.79 n/a .000
13838# [L/S/n: 497./ .302/.055]
13840# [Vmax: 1.728/Dmax: 3.267]
13841#
13842# # Catchment OKRFEF
13843# # To V-Office drain (north of the Site)
13844# # - Developed with assumed 43 imp.
13845# # - 2020-12-01 add Okrfele model (Area 513.02 HA) instead of current Okrfele (Area 5
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14587 # remark:Total Flows at KB second pond
14588 R0100-C00241-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14589 CONTINIOUS STANDEYD 1.0 01:38-16.1 2.80 486.00 Date 28:00 72.68 821.000
14590 [XIMP: 75:TIMP: 75]
14591 [Horton parameters] Fw = 76.20Pc= 13.20:DCOV4:1.4 P= .00]
14592 [Previous area IArea: 4.67:SLP=2.00:LD= 40.0:MD= 250:ISCP= .0]
14593 [Impervious area IArea: 1.61:SLP=1.00:LD= 137.0:MD= 0:ISCP= .0]
14594 [ISaIcImp: 4.00: ISaIcP= 4.00]
14595 R0100-C00242-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14596 ADD HYD + 1.0 02:18-Pond3 254.24 24.84 Date 28:06 51.59 n/a .000
14597 + 1.0 02:18-P1 2.80 486.00 Date 28:06 72.68 n/a .000
14598 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14599 [SUM]
14600 R0100-C00243-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14601 COMPUTE DUALHDYD 1.0 01:38-02 12.87 1.769 Date 28:03 82.69 n/a .000
14602 Major System / 1.0 02:18-04-MJ 4.0 0.00 Date 28:00 64.86 n/a .000
14603 Minor System \ 1.0 03:18-03-MN 7.03 .358 Date 27:41 64.90 n/a .000
14604 [MjSysTot= 1794E+03, TotVolVol= 2828E+03, N-Ofv= 1, TotDurOfv= 0 hrs]
14605 ADD HYD + 1.0 02:18-04-MJ 4.0 0.00 Date 28:00 64.86 n/a .000
14606 + 1.0 02:18-03-MN 7.03 .358 Date 27:41 64.90 n/a .000
14607 [SUM]
14608 R0100-C00244-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14609 ADD HYD + 1.0 02:18-04-MJ 4.0 0.00 Date 28:00 64.86 n/a .000
14610 + 1.0 02:18-03-MN 7.03 .358 Date 27:41 64.90 n/a .000
14611 [SUM]
14612 R0100-C00245-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14613 SAVE HYD frame :SBN_0100 54681.21 147.52 Date 28:07 51.82 n/a .000
14614 # TO FRASER-CORNER DRAIN
14615 # KXITIMP / PROPOSED Subcatchments (Kennedy-Burnett SNN Facility (11800)), SNN Modeling Approach, NOVATECH Report Ju
14616 #
14617 R0100-C00246-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14618 CONTINIOUS STANDEYD 1.0 01:38-01 8.03 1.446 Date 28:01 64.40 614.000
14619 [XIMP: 47:TIMP: 47]
14620 [Horton parameters] Fw = 76.20Pc= 13.20:DCOV4:1.4 P= .00]
14621 [Previous area IArea: 4.67:SLP=2.00:LD= 40.0:MD= 250:ISCP= .0]
14622 [Impervious area IArea: 1.57:SLP=1.00:LD= 231.0:MD= 0:ISCP= .0]
14623 [ISaIcImp: 4.00: ISaIcP= 4.00]
14624 R0100-C00247-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14625 COMPUTE DUALHDYD 1.0 01:38-02 12.87 1.769 Date 28:03 82.69 n/a .000
14626 Major System / 1.0 02:18-04-MJ 4.0 0.00 Date 28:00 64.86 n/a .000
14627 Minor System \ 1.0 03:18-03-MN 7.03 .358 Date 27:41 64.90 n/a .000
14628 [MjSysTot= 6274E+03, TotVolVol= 0.000E+00, N-Ofv= 0, TotDurOfv= 0 hrs]
14629 R0100-C00248-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14630 ADD HYD + 1.0 02:18-04-MJ 4.0 0.00 Date 28:00 64.86 n/a .000
14631 + 1.0 02:18-03-MN 7.03 .358 Date 27:41 64.90 n/a .000
14632 [SUM]
14633 R0100-C00249-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14634 CONTINIOUS STANDEYD 1.0 01:38-02 12.87 1.769 Date 28:00 82.69 732.000
14635 [XIMP: 93:TIMP: 93]
14636 [Horton parameters] Fw = 76.20Pc= 13.20:DCOV4:1.4 P= .00]
14637 [Previous area IArea: 4.67:SLP=2.00:LD= 40.0:MD= 250:ISCP= .0]
14638 [Impervious area IArea: 1.57:SLP=1.00:LD= 327.0:MD= 0:ISCP= .0]
14639 [ISaIcImp: 4.00: ISaIcP= 4.00]
14640 R0100-C00250-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14641 COMPUTE DUALHDYD 1.0 01:38-02 12.87 1.769 Date 28:03 82.69 n/a .000
14642 Major System / 1.0 02:18-04-MJ 4.0 0.00 Date 28:00 64.86 n/a .000
14643 Minor System \ 1.0 03:18-03-MN 7.03 .358 Date 27:41 64.90 n/a .000
14644 [MjSysTot= 2385E+03, TotVolVol= 0.000E+00, N-Ofv= 0, TotDurOfv= 0 hrs]
14645 ADD HYD + 1.0 02:18-04-MJ 4.0 0.00 Date 28:00 64.86 n/a .000
14646 + 1.0 02:18-03-MN 7.03 .358 Date 27:41 64.90 n/a .000
14647 [SUM]
14648 R0100-C00251-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14649 CONTINIOUS STANDEYD 1.0 01:38-02 12.87 1.769 Date 28:00 82.69 732.000
14650 [XIMP: 93:TIMP: 93]
14651 [Horton parameters] Fw = 76.20Pc= 13.20:DCOV4:1.4 P= .00]
14652 [Previous area IArea: 4.67:SLP=2.00:LD= 40.0:MD= 250:ISCP= .0]
14653 [Impervious area IArea: 1.57:SLP=1.00:LD= 222.0:MD= 0:ISCP= .0]
14654 [ISaIcImp: 4.00: ISaIcP= 4.00]
14655 R0100-C00252-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14656 COMPUTE DUALHDYD 1.0 01:38-03 7.37 1.717 Date 28:00 64.86 n/a .000
14657 Major System / 1.0 02:18-04-MJ 4.0 0.00 Date 28:00 64.86 n/a .000
14658 Minor System \ 1.0 03:18-03-MN 7.03 .358 Date 27:41 64.90 n/a .000
14659 [MjSysTot= 1131E+03, TotVolVol= 218E+03, N-Ofv= 1, TotDurOfv= 0 hrs]
14660 R0100-C00253-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14661 ADD HYD + 1.0 02:18-04-MJ 4.0 0.00 Date 28:00 64.86 n/a .000
14662 + 1.0 02:18-03-MN 7.03 .358 Date 27:41 64.90 n/a .000
14663 [SUM]
14664 R0100-C00254-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14665 CONTINIOUS STANDEYD 1.0 01:38-04 8.24 2.884 Date 28:01 64.86 732.000
14666 [XIMP: 64:TIMP: 64]
14667 [Horton parameters] Fw = 76.20Pc= 13.20:DCOV4:1.4 P= .00]
14668 [Previous area IArea: 4.67:SLP=2.00:LD= 40.0:MD= 250:ISCP= .0]
14669 [Impervious area IArea: 1.57:SLP=1.00:LD= 293.0:MD= 0:ISCP= .0]
14670 [ISaIcImp: 4.00: ISaIcP= 4.00]
14671 R0100-C00255-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14672 COMPUTE DUALHDYD 1.0 01:38-04 12.87 2.884 Date 28:01 64.86 n/a .000
14673 Major System / 1.0 02:18-04-MJ 4.0 0.00 Date 28:00 64.86 n/a .000
14674 Minor System \ 1.0 03:18-04-MN 12.43 1.743 Date 28:00 64.86 n/a .000
14675 [MjSysTot= 1794E+04, TotVolVol= 2828E+03, N-Ofv= 1, TotDurOfv= 0 hrs]
14676 R0100-C00256-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14677 ADD HYD + 1.0 02:18-04-MJ 4.0 0.00 Date 28:00 64.86 n/a .000
14678 + 1.0 02:18-03-MN 12.43 1.743 Date 28:00 64.86 n/a .000
14679 [SUM]
14680 R0100-C00257-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14681 CONTINIOUS STANDEYD 1.0 01:38-02 12.87 1.719 Date 28:07 65.10 n/a .000
14682 # TO JOCK RIVER
14683 # PROPOSED Subcatchments (Kennedy-Burnett SNN Facility (11800)), SNN Modeling Approach, NOVATECH Report June, 2020]
14684 #
14685 R0100-C00258-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14686 CONTINIOUS STANDEYD 1.0 01:38-02 12.87 1.719 Date 28:00 64.86 732.000
14687 [XIMP: 64:TIMP: 64]
14688 [Horton parameters] Fw = 76.20Pc= 13.20:DCOV4:1.4 P= .00]
14689 [Previous area IArea: 4.67:SLP=2.00:LD= 40.0:MD= 250:ISCP= .0]
14690 [Impervious area IArea: 1.57:SLP=1.00:LD= 234.0:MD= 0:ISCP= .0]
14691 [ISaIcImp: 4.00: ISaIcP= 4.00]
14692 R0100-C00259-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14693 COMPUTE DUALHDYD 1.0 01:38-01 8.24 1.891 Date 28:00 64.86 n/a .000
14694 Major System / 1.0 02:18-04-MJ 4.0 0.00 Date 28:00 64.86 n/a .000
14695 Minor System \ 1.0 03:18-03-MN 8.04 .563 Date 27:44 64.95 n/a .000
14696 [MjSysTot= 1040E+03, TotVolVol= 1.000E+00, N-Ofv= 1, TotDurOfv= 0 hrs]
14697 R0100-C00260-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14698 ADD HYD + 1.0 02:18-04-MJ 4.0 0.00 Date 28:00 64.86 n/a .000
14699 + 1.0 02:18-03-MN 8.04 .563 Date 27:44 64.95 n/a .000
14700 [SUM]
14701 R0100-C00261-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14702 CONTINIOUS STANDEYD 1.0 01:38-02 1.59 1.034 Date 28:00 64.86 732.000
14703 [XIMP: 64:TIMP: 64]
14704 [Horton parameters] Fw = 76.20Pc= 13.20:DCOV4:1.4 P= .00]
14705 [Previous area IArea: 4.67:SLP=2.00:LD= 40.0:MD= 250:ISCP= .0]
14706 [Impervious area IArea: 1.57:SLP=1.00:LD= 193.0:MD= 0:ISCP= .0]
14707 [ISaIcImp: 4.00: ISaIcP= 4.00]
14708 R0100-C00262-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14709 COMPUTE DUALHDYD 1.0 01:38-02 1.59 1.034 Date 28:00 64.86 n/a .000
14710 Major System / 1.0 02:18-04-MJ 4.0 0.00 Date 28:00 64.86 n/a .000
14711 Minor System \ 1.0 03:18-02-MN 1.57 .153 Date 27:44 65.24 n/a .000
14712 [MjSysTot= 1930E+03, TotVolVol= 1735E+02, N-Ofv= 1, TotDurOfv= 0 hrs]
14713 R0100-C00263-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14714 ADD HYD + 1.0 02:18-02-MN 1.57 .153 Date 28:03 64.85 n/a .000
14715 + 1.0 02:18-02-MN 1.57 .153 Date 28:03 64.85 n/a .000
14716 [SUM]
14717 R0100-C00264-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14718 CONTINIOUS STANDEYD 1.0 01:38-02 1.59 1.034 Date 28:00 64.86 732.000
14719 [XIMP: 64:TIMP: 64]
14720 # TO FRASER-CLARKE drain (north of the Jock)
14721 # Developing land with 35% impervious (Nashby)
14722 # - 2020-12-17 Change Fraser area to be 35.1 as measured from GIS
14723 #
14724 R0100-C00265-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14725 CONTINIOUS NASHYD 1.0 01:38-02 1.59 1.034 Date 28:00 64.86 732.000
14726 [XIMP: 7.0: N 3.00: T= 43]
14727 [Area: 4.00: SNN: 31.15: SMA: 207.66: SK= 0:0]
14728 [InterEventTime: 12.00]
14729 R0100-C00266-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14730 CONTINIOUS NASHYD 1.0 01:38-02 21.61 .559 Date 28:00 45.95 519.000
14731 [XIMP: 7.0: N 3.00: T= 67]
14732 [Area: 4.00: SNN: 31.15: SMA: 207.66: SK= 0:0]
14733 [InterEventTime: 12.00]
14734 R0100-C00267-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14735 ADD HYD + 1.0 02:18-Pond3 257.04 24.70 Date 28:07 51.82 n/a .000
14736 + 1.0 02:18-P1 2.80 486.00 Date 28:06 72.68 n/a .000
14737 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14738 # TO FRASER-DRAIN
14739 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14740 + 1.0 02:18-P1 2.80 486.00 Date 28:06 72.68 n/a .000
14741 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14742 + 1.0 02:18-P1 2.80 486.00 Date 28:06 72.68 n/a .000
14743 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14744 + 1.0 02:18-P1 2.80 486.00 Date 28:06 72.68 n/a .000
14745 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14746 + 1.0 02:18-P1 2.80 486.00 Date 28:06 72.68 n/a .000
14747 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14748 + 1.0 02:18-P1 2.80 486.00 Date 28:06 72.68 n/a .000
14749 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14750 + 1.0 02:18-P1 2.80 486.00 Date 28:06 72.68 n/a .000
14751 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14752 + 1.0 02:18-P1 2.80 486.00 Date 28:06 72.68 n/a .000
14753 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14754 + 1.0 02:18-P1 2.80 486.00 Date 28:06 72.68 n/a .000
14755 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14756 + 1.0 02:18-P1 2.80 486.00 Date 28:06 72.68 n/a .000
14757 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14758 + 1.0 02:18-P1 2.80 486.00 Date 28:06 72.68 n/a .000
14759 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14760 + 1.0 02:18-P1 2.80 486.00 Date 28:06 72.68 n/a .000
14761 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14762 + 1.0 02:18-P1 2.80 486.00 Date 28:06 72.68 n/a .000
14763 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14764 + 1.0 02:18-P1 2.80 486.00 Date 28:06 72.68 n/a .000
14765 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14766 + 1.0 02:18-P1 2.80 486.00 Date 28:06 72.68 n/a .000
14767 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14768 + 1.0 02:18-P1 2.80 486.00 Date 28:06 72.68 n/a .000
14769 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14770 + 1.0 02:18-P1 2.80 486.00 Date 28:06 72.68 n/a .000
14771 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14772 + 1.0 02:18-P1 2.80 486.00 Date 28:06 72.68 n/a .000
14773 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14774 + 1.0 02:18-P1 2.80 486.00 Date 28:06 72.68 n/a .000
14775 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14776 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14777 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14778 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14779 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14780 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14781 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14782 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14783 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14784 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14785 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14786 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14787 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14788 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14789 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14790 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14791 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14792 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14793 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14794 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14795 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14796 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14797 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14798 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14799 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000
14800 + 1.0 02:18-P3 257.04 24.93 Date 28:06 52.82 n/a .000

```

```

14776 # Catchment Greenbank
14777 # To Greenbank Drain (south of the Jock)
14778 # JFS 2021-01-19 Greenbank pond as per JFS, P598(06)-15, June 2016
14779 # JFS 2021-01-19 update area from 37.475 ha to 36.6 ha based on GIS measurements
14780 #
14781 R0100-C00272-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14782 CONTINIOUS STANDEYD 1.0 01:Greenbank 36.60 7.069 Date 28:01 71.80 811.000
14783 [XIMP: 64:TIMP: 68]
14784 [ISS: 2 :CN: 77.0]
14785 [Previous area IArea: 4.67:SLP=1.00:LD= 40.0:MD= 250:ISCP= .0]
14786 [Impervious area IArea: 1.57:SLP=1.00:LD= 494.0:MD= 0:ISCP= .0]
14787 [ISaIcImp: 4.00: ISaIcP= 4.00]
14788 [SMA: 31.15: SMA: 207.66: SK= 0:0]
14789 R0100-C00273-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14790 ROUTE RESERVOIR out <= 1.0 01:Greenbank 36.60 5.350 Date 28:07 71.80 n/a .000
14791 [MjSysTot= 2834E+01, TotVolVol= 0.000E+00, N-Ofv= 0, TotDurOfv= 0 hrs]
14792 overflow <= 1.0 01:Greenbank 36.60 5.350 Date 28:07 71.80 n/a .000
14793 [MjSysTot= 2834E+01, TotVolVol= 0.000E+00, N-Ofv= 0, TotDurOfv= 0 hrs]
14794 R0100-C00274-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14795 ADD HYD + 1.0 02:Greenbank 54681.21 147.52 Date 28:07 51.82 n/a .000
14796 + 1.0 02:Greenbank 54681.21 147.52 Date 28:07 51.82 n/a .000
14797 [SUM]
14798 R0100-C00275-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14799 SAVE HYD frame :SBN_0100 54717.82 147.488 Date 28:03 35.49 39.25 n/a .000
14800 # remark:Total Flows at Greenbank Drain
14801 #
14802 # Catchment TODD
14803 # To Todd Drain (south of the Jock)
14804 # Subdivision with 4% imp. as per Barrhaven South MSS
14805 # - 2020-11-30 Increase imp. based on P598(04)-11
14806 # - 2020-11-30 update TODD Tributary Drainage Area to = 146.015 ha based on P598(04)-11
14807 # - 2020-11-30 update TODD Tributary Drainage Area to = 146.015 ha based on P598(04)-11
14808 #
14809 R0100-C00276-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14810 CONTINIOUS STANDEYD 1.0 01:TODD_M2 2.10 428 Date 28:00 66.78 754.000
14811 [XIMP: 53:TIMP: 57]
14812 [ISS: 2 :CN: 77.0]
14813 [Previous area IArea: 4.67:SLP=1.00:LD= 40.0:MD= 250:ISCP= .0]
14814 [Impervious area IArea: 1.57:SLP=1.00:LD= 118.0:MD= 0:ISCP= .0]
14815 [ISaIcImp: 4.00: ISaIcP= 4.00]
14816 [SMA: 31.15: SMA: 207.66: SK= 0:0]
14817 R0100-C00277-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14818 COMPUTE DUALHDYD 1.0 01:TODD_M3 12 .025 Date 28:00 66.78 754.000
14819 Major System / 1.0 02:TODD_M3 12 .025 Date 28:00 66.78 754.000
14820 Minor System \ 1.0 03:TODD_M3 12 .025 Date 28:00 66.78 754.000
14821 [MjSysTot= 53:TIMP: 57]
14822 [ISS: 2 :CN: 77.0]
14823 [Previous area IArea: 4.67:SLP=1.00:LD= 40.0:MD= 250:ISCP= .0]
14824 [Impervious area IArea: 1.57:SLP=1.00:LD= 28.0:MD= 0:ISCP= .0]
14825 [ISaIcImp: 4.00: ISaIcP= 4.00]
14826 [SMA: 31.15: SMA: 207.66: SK= 0:0]
14827 R0100-C00278-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14828 CONTINIOUS STANDEYD 1.0 01:TODD_MJ 30.23 5.210 Date 28:02 68.65 775.000
14829 [XIMP: 52:TIMP: 64]
14830 [ISS: 2 :CN: 77.0]
14831 [Previous area IArea: 4.67:SLP=1.00:LD= 40.0:MD= 250:ISCP= .0]
14832 [Impervious area IArea: 1.57:SLP=1.00:LD= 449.0:MD= 0:ISCP= .0]
14833 [ISaIcImp: 4.00: ISaIcP= 4.00]
14834 [SMA: 31.15: SMA: 207.66: SK= 0:0]
14835 R0100-C00279-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14836 CONTINIOUS STANDEYD 1.0 01:TODD_ALL 112.91 17.286 Date 28:04 66.60 752.000
14837 [XIMP: 53:TIMP: 57]
14838 [ISS: 2 :CN: 77.0]
14839 [Previous area IArea: 4.67:SLP=1.00:LD= 40.0:MD= 250:ISCP= .0]
14840 [Impervious area IArea: 1.57:SLP=1.00:LD= 868.0:MD= 0:ISCP= .0]
14841 [ISaIcImp: 4.00: ISaIcP= 4.00]
14842 [SMA: 31.15: SMA: 207.66: SK= 0:0]
14843 R0100-C00280-----AREA-A-GPARC-Area-TpeakDate_hh:mm-----RvM-R-C-----DWPFM
14844 COMPUTE DUALHDYD 1.0 01:TODD_P 1.00 669 Date 28:00 70.28 794.000
14845 Major System / 1.0 02:TODD_P 1.00 669 Date 28:00 70.28 794.000
14846 Minor System \ 1.0 03:TODD_P 1.00 669 Date 28:00 70.28 794.000
14847 [MjSysTot= 63:TIMP: 63]
14848 [ISS: 2 :CN: 77.0]
14849 [Previous area IArea: 4.67:SLP=1.00:LD= 40.0:MD= 250:ISCP= .0]
14850 [Impervious area IArea: 1.57:SLP=1.00:LD= 143.0:MD= 0:ISCP= .0]
14851 [ISaIcImp: 4.00: ISaIcP= 4.00]
14852 [SMA: 31.
```





```
15709> *** WARNING: New pipe size used for routing.
15710> RO100:C00370 ROUTE PIPE ->
15711> *** WARNING: New pipe size used for routing.
15712> RO100:C00378 ROUTE PIPE ->
15713> *** WARNING: New pipe size used for routing.
15714> RO100:C00379 ROUTE PIPE ->
15715> *** WARNING: New pipe size used for routing.
15716> RO100:C00303 ROUTE PIPE ->
15717> *** WARNING: New pipe size used for routing.
15718> RO100:C00309 ROUTE PIPE ->
15719> *** WARNING: New pipe size used for routing.
15720> RO100:C00325 ROUTE PIPE ->
15721> *** WARNING: New pipe size used for routing.
15722> RO100:C00326 ROUTE PIPE ->
15723> *** WARNING: New pipe size used for routing.
15724> RO100:C00334 ROUTE PIPE ->
15725> *** WARNING: New pipe size used for routing.
15726> RO100:C00342 DIVERT HYD ->
15727> *** NOTE: Inflow hyd. is dry and cannot be diverted.
15728> RO100:C00357 ROUTE PIPE ->
15729> *** WARNING: New pipe size used for routing.
15730> RO100:C00362 ROUTE PIPE ->
15731> *** WARNING: New pipe size used for routing.
15732> RO100:C00369 ROUTE PIPE ->
15733> *** WARNING: New pipe size used for routing.
15734> RO100:C00370 ROUTE PIPE ->
15735> *** WARNING: New pipe size used for routing.
15736> RO100:C00378 ROUTE PIPE ->
15737> *** WARNING: New pipe size used for routing.
15738> RO100:C00379 ROUTE PIPE ->
15739> *** WARNING: New pipe size used for routing.
15740> Simulation ended on 2021-03-04 at 11:53:36
15741> .....
15742>
15743>
```



# Attachment D

Model 4A – Jock River Reach One Future Conditions – Without SWM controls

JFSA, 2021

SWMHYMO Input & Summary files

```

1  20  Metric units / ID numbers OFF
2  *#*****
3  *# SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
4  *#*****
5  *# Project Name: [Jock River] Project Number: [1474-16]
6  *# Date : 04-03-2021
7  *# Modeller : [M.M.]
8  *# Company : JFSAinc.
9  *# License # : 2549237
10 *#*****
11 *# CALIBRATION OF SUMMER MODEL PARAMETERS
12 *# USING CONTINUOUS SIMULATIONS
13 *# Rainfall data from JFSA raingauge installed at site + other gauges by the City
14 *# Use data collected from May 1st to July 14, 2003
15 *# 2020-11-30 change TMJSTO in COMPUTE DUALHYD (TMJSTO = 0.1 instead of 0.0001)
16 *# 2020-12-01 correct pond curve values
17 *# 2020-12-01 change W_CLAR_BRAZ XIMP to 0.55, SLPI=[0.5](%) (impervious slope), and
LGI up to 700m
18 *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 2462 (NHYDout=["N_TO"]
,NHYDin=["SN_TO"]) from 0.033 % (as per Stantec Report 2007) to 0.05 % so the model
will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELs
aren't well suited to really flat slopes.
19 *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHYDout=["N_WC"]
,NHYDin=["SN_CE"]) from 0.01 % (as per Stantec Report 2007) to 0.0255 % so the model
will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELs
aren't well suited to really flat slopes.
20 *
21 * Calibrated parameters for Summer 2003 data: APII=50, APIK=0.85, CN=varies,
22 * SK=0.01, InterEventTime=12,
23 * GWResk=0.96, VHydCond=0.055
24 *
25 *# -----
26 *
27 *START TZERO=[2003.0501], METOUT=[2], NSTORM=[1], NRUN=[001]
28 * ["XAVG0315.STM"] average storm data a 15 minute time step
29 * The above rainf file is an average of the JFSA gauge data
30 * with the City of Ottawa rainfall data collected during
31 * the same period.
32 *% 2 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
33 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[2]
34 ["C24SC002.stm"] <--storm filename, one per line for NSTORM time
35 *%-----|-----|
36 *%-----|-----|
37 READ STORM STORM_FILENAME=["storm.001"]
38 *%-----|-----|
39 MODIFY STORM ICASEms=[1], NSHIFT=[96],
40 RedFACT=[1],
41 *%-----|-----|
42 DEFAULT VALUES ICASEdef=[1], read and print values
43 DEFVAL_FILENAME=["CitiGate.DEF"]
44 *%-----|-----|
45 COMPUTE API APII=[50], APIK=[.85]/day
46 *%-----|-----|
47 *%-----|-----|
48 *#
49 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
50 *# of 1.32
51 *%-----|-----|
52 CONTINUOUS NASHYD NHYD=["JR_HW"], DT=[1]min, AREA=[3680](ha),
53 DWF=[0](cms), CN/C=[64], IA=[2.5](mm),
54 N=[3.0], TP=[7.13]hrs,
55 Continuous simulation parameters:
56 IaRECper=[4](hrs),
57 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
58 InterEventTime=[12](hrs)
59 Baseflow simulation parameters:

```

```

60         BaseFlowOption=[1] ,
61         InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
62         VHydCond=[0.055](mm/hr),   END=-1
63     *%-----|-----
64     *#
65     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
66     *# of 1.32
67     *%-----|-----
68     CONTINUOUS NASHYD  NHYD=["SW_13"], DT=[1]min, AREA=[971](ha),
69                        DWF=[0](cms),  CN/C=[61], IA=[2.5](mm),
70                        N=[3.0], TP=[3.76]hrs,
71                        Continuous simulation parameters:
72                        IaRECper=[4](hrs),
73                        SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
74                        InterEventTime=[12](hrs)
75                        Baseflow simulation parameters:
76                        BaseFlowOption=[1] ,
77                        InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
78                        VHydCond=[0.055](mm/hr),   END=-1
79     *%-----|-----
80     *#
81     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
82     *# of 1.80
83     *%-----|-----
84     CONTINUOUS NASHYD  NHYD=["JR_GWM"], DT=[1]min, AREA=[3074](ha),
85                        DWF=[0](cms),  CN/C=[55], IA=[2.5](mm),
86                        N=[3], TP=[11.33]hrs,
87                        Continuous simulation parameters:
88                        IaRECper=[4](hrs),
89                        SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
90                        InterEventTime=[12](hrs)
91                        Baseflow simulation parameters:
92                        BaseFlowOption=[1] ,
93                        InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
94                        VHydCond=[0.055](mm/hr),   END=-1
95     *%-----|-----
96     CONTINUOUS NASHYD  NHYD=["JR_ASH"], DT=[1]min, AREA=[1781](ha),
97                        DWF=[0](cms),  CN/C=[72], IA=[2.5](mm),
98                        N=[3.0], TP=[3.91]hrs,
99                        Continuous simulation parameters:
100                       IaRECper=[4](hrs),
101                       SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
102                       InterEventTime=[12](hrs)
103                       Baseflow simulation parameters:
104                       BaseFlowOption=[1] ,
105                       InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
106                       VHydCond=[0.055](mm/hr),   END=-1
107     *%-----|-----
108     CONTINUOUS NASHYD  NHYD=["SW_11"], DT=[1]min, AREA=[500](ha),
109                        DWF=[0](cms),  CN/C=[66], IA=[2.5](mm),
110                        N=[3.0], TP=[1.24]hrs,
111                        Continuous simulation parameters:
112                        IaRECper=[4](hrs),
113                        SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
114                        InterEventTime=[12](hrs)
115                        Baseflow simulation parameters:
116                        BaseFlowOption=[1] ,
117                        InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
118                        VHydCond=[0.055](mm/hr),   END=-1
119     *%-----|-----
120     *#
121     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
122     *# of 1.80
123     *%-----|-----
124     CONTINUOUS NASHYD  NHYD=["NN_CK"], DT=[1]min, AREA=[1917](ha),
125                        DWF=[0](cms),  CN/C=[66], IA=[2.5](mm),

```

```

126 N=[3.0], TP=[5.29]hrs,
127 Continuous simulation parameters:
128 IaREcper=[4](hrs),
129 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
130 InterEventTime=[12](hrs)
131 Baseflow simulation parameters:
132 BaseFlowOption=[1] ,
133 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
134 VHydCond=[0.055](mm/hr), END=-1
135 *%-----|-----
136 *#
137 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
138 *# of 1.52
139 *%-----|-----
140 CONTINUOUS NASHYD NHYD=["SW_10"], DT=[1]min, AREA=[5666](ha),
141 DWF=[0](cms), CN/C=[72], IA=[2.5](mm),
142 N=[3.0], TP=[8.00]hrs,
143 Continuous simulation parameters:
144 IaREcper=[4](hrs),
145 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
146 InterEventTime=[12](hrs)
147 Baseflow simulation parameters:
148 BaseFlowOption=[1] ,
149 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
150 VHydCond=[0.055](mm/hr), END=-1
151 *%-----|-----
152 *#
153 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
154 *# of 1.75
155 *%-----|-----
156 CONTINUOUS NASHYD NHYD=["KG CK"], DT=[1]min, AREA=[8376](ha),
157 DWF=[0](cms), CN/C=[66], IA=[2.5](mm),
158 N=[3.0], TP=[11.66]hrs,
159 Continuous simulation parameters:
160 IaREcper=[4](hrs),
161 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
162 InterEventTime=[12](hrs)
163 Baseflow simulation parameters:
164 BaseFlowOption=[1] ,
165 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
166 VHydCond=[0.055](mm/hr), END=-1
167 *%-----|-----
168 *#
169 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
170 *# of 1.68
171 *%-----|-----
172 CONTINUOUS NASHYD NHYD=["SW_9"], DT=[1]min, AREA=[1132](ha),
173 DWF=[0](cms), CN/C=[70], IA=[2.5](mm),
174 N=[3.0], TP=[2.51]hrs,
175 Continuous simulation parameters:
176 IaREcper=[4](hrs),
177 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
178 InterEventTime=[12](hrs)
179 Baseflow simulation parameters:
180 BaseFlowOption=[1] ,
181 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
182 VHydCond=[0.055](mm/hr), END=-1
183 *%-----|-----
184 *#
185 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
186 *# of 1.82
187 *%-----|-----
188 CONTINUOUS NASHYD NHYD=["NC CK"], DT=[1]min, AREA=[4464](ha),
189 DWF=[0](cms), CN/C=[62], IA=[2.5](mm),
190 N=[3.0], TP=[11.32]hrs,
191 Continuous simulation parameters:

```

```

192         IaREcper=[4](hrs),
193         SMIN=[-1](mm),  SMAx=[-1](mm), SK=[0.010]/(mm),
194         InterEventTime=[12](hrs)
195         Baseflow simulation parameters:
196         BaseFlowOption=[1] ,
197         InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
198         VHydCond=[0.055](mm/hr),  END=-1
199     *%-----|-----
200     *#
201     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
202     *# of 1.80
203     *%-----|-----
204     CONTINUOUS NASHYD  NHYD=["SW_8"], DT=[1]min, AREA=[131](ha),
205                       DWF=[0](cms),  CN/C=[63], IA=[2.5](mm),
206                       N=[3.0], TP=[0.90]hrs,
207                       Continuous simulation parameters:
208                       IaREcper=[4](hrs),
209                       SMIN=[-1](mm),  SMAx=[-1](mm), SK=[0.010]/(mm),
210                       InterEventTime=[12](hrs)
211                       Baseflow simulation parameters:
212                       BaseFlowOption=[1] ,
213                       InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
214                       VHydCond=[0.055](mm/hr),  END=-1
215     *%-----|-----
216     *#
217     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
218     *# of 1.65
219     *%-----|-----
220     CONTINUOUS NASHYD  NHYD=["HB_DR"], DT=[1]min, AREA=[3854](ha),
221                       DWF=[0](cms),  CN/C=[66], IA=[2.5](mm),
222                       N=[3.0], TP=[8.42]hrs,
223                       Continuous simulation parameters:
224                       IaREcper=[4](hrs),
225                       SMIN=[-1](mm),  SMAx=[-1](mm), SK=[0.010]/(mm),
226                       InterEventTime=[12](hrs)
227                       Baseflow simulation parameters:
228                       BaseFlowOption=[1] ,
229                       InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
230                       VHydCond=[0.055](mm/hr),  END=-1
231     *%-----|-----
232     *#
233     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
234     *# of 1.82
235     *%-----|-----
236     CONTINUOUS NASHYD  NHYD=["SW_7"], DT=[1]min, AREA=[3197](ha),
237                       DWF=[0](cms),  CN/C=[57], IA=[2.5](mm),
238                       N=[3.0], TP=[6.65]hrs,
239                       Continuous simulation parameters:
240                       IaREcper=[4](hrs),
241                       SMIN=[-1](mm),  SMAx=[-1](mm), SK=[0.010]/(mm),
242                       InterEventTime=[12](hrs)
243                       Baseflow simulation parameters:
244                       BaseFlowOption=[1] ,
245                       InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
246                       VHydCond=[0.055](mm/hr),  END=-1
247     *%-----|-----
248     *#
249     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
250     *# of 1.75
251     *%-----|-----
252     CONTINUOUS NASHYD  NHYD=["SW_6"], DT=[1]min, AREA=[165](ha),
253                       DWF=[0](cms),  CN/C=[67], IA=[2.5](mm),
254                       N=[3.0], TP=[4.18]hrs,
255                       Continuous simulation parameters:
256                       IaREcper=[4](hrs),
257                       SMIN=[-1](mm),  SMAx=[-1](mm), SK=[0.010]/(mm),

```

```

258 InterEventTime=[12](hrs)
259 Baseflow simulation parameters:
260 BaseFlowOption=[1] ,
261 InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
262 VHydCond=[0.055](mm/hr) , END=-1
263 *%-----|-----
264 *#
265 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
266 *# of 1.67
267 *%-----|-----
268 CONTINUOUS NASHYD NHYD=["VG_DR"] , DT=[1]min , AREA=[1332](ha) ,
269 DWF=[0](cms) , CN/C=[72] , IA=[2.5](mm) ,
270 N=[3.0] , TP=[5.95]hrs ,
271 Continuous simulation parameters:
272 IaREcper=[4](hrs) ,
273 SMIN=[-1](mm) , SMAX=[-1](mm) , SK=[0.010]/(mm) ,
274 InterEventTime=[12](hrs)
275 Baseflow simulation parameters:
276 BaseFlowOption=[1] ,
277 InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
278 VHydCond=[0.055](mm/hr) , END=-1
279 *%-----|-----
280 CONTINUOUS NASHYD NHYD=["SW_5"] , DT=[1]min , AREA=[224](ha) ,
281 DWF=[0](cms) , CN/C=[77] , IA=[2.5](mm) ,
282 N=[3.0] , TP=[0.75]hrs ,
283 Continuous simulation parameters:
284 IaREcper=[4](hrs) ,
285 SMIN=[-1](mm) , SMAX=[-1](mm) , SK=[0.010]/(mm) ,
286 InterEventTime=[12](hrs)
287 Baseflow simulation parameters:
288 BaseFlowOption=[1] ,
289 InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
290 VHydCond=[0.055](mm/hr) , END=-1
291 *%-----|-----
292 *#
293 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
294 *# of 1.20
295 *%-----|-----
296 CONTINUOUS NASHYD NHYD=["FL_CK"] , DT=[1]min , AREA=[4945](ha) ,
297 DWF=[0](cms) , CN/C=[74] , IA=[2.5](mm) ,
298 N=[3.0] , TP=[4.45]hrs ,
299 Continuous simulation parameters:
300 IaREcper=[4](hrs) ,
301 SMIN=[-1](mm) , SMAX=[-1](mm) , SK=[0.010]/(mm) ,
302 InterEventTime=[12](hrs)
303 Baseflow simulation parameters:
304 BaseFlowOption=[1] ,
305 InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
306 VHydCond=[0.055](mm/hr) , END=-1
307 *%-----|-----
308 CONTINUOUS NASHYD NHYD=["SW_5A2"] , DT=[1]min , AREA=[20](ha) ,
309 DWF=[0](cms) , CN/C=[81] , IA=[2.5](mm) ,
310 N=[3.0] , TP=[0.62]hrs ,
311 Continuous simulation parameters:
312 IaREcper=[4](hrs) ,
313 SMIN=[-1](mm) , SMAX=[-1](mm) , SK=[0.010]/(mm) ,
314 InterEventTime=[12](hrs)
315 Baseflow simulation parameters:
316 BaseFlowOption=[1] ,
317 InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
318 VHydCond=[0.055](mm/hr) , END=-1
319 *%-----|-----
320 *#
321 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
322 *# of 1.61
323 *%-----|-----

```



```

324 CONTINUOUS NASHYD NHYD=["SW_5A1"], DT=[1]min, AREA=[1412](ha),
325 DWF=[0](cms), CN/C=[75], IA=[2.5](mm),
326 N=[3.0], TP=[8.00]hrs,
327 Continuous simulation parameters:
328 IaREcper=[4](hrs),
329 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
330 InterEventTime=[12](hrs)
331 Baseflow simulation parameters:
332 BaseFlowOption=[1] ,
333 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
334 VHydCond=[0.055](mm/hr), END=-1
335 *%-----|
336 CONTINUOUS NASHYD NHYD=["SW_4"], DT=[1]min, AREA=[585](ha),
337 DWF=[0](cms), CN/C=[81], IA=[2.5](mm),
338 N=[3.0], TP=[1.75]hrs,
339 Continuous simulation parameters:
340 IaREcper=[4](hrs),
341 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
342 InterEventTime=[12](hrs)
343 Baseflow simulation parameters:
344 BaseFlowOption=[1] ,
345 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
346 VHydCond=[0.055](mm/hr), END=-1
347 *%-----|
348 CONTINUOUS NASHYD NHYD=["LM_CK"], DT=[1]min, AREA=[1021](ha),
349 DWF=[0](cms), CN/C=[80], IA=[2.5](mm),
350 N=[3.0], TP=[2.46]hrs,
351 Continuous simulation parameters:
352 IaREcper=[4](hrs),
353 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
354 InterEventTime=[12](hrs)
355 Baseflow simulation parameters:
356 BaseFlowOption=[1] ,
357 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
358 VHydCond=[0.055](mm/hr), END=-1
359 *%-----|
360 CONTINUOUS NASHYD NHYD=["SW_2"], DT=[1]min, AREA=[177](ha),
361 DWF=[0](cms), CN/C=[77], IA=[2.5](mm),
362 N=[3.0], TP=[0.75]hrs,
363 Continuous simulation parameters:
364 IaREcper=[4](hrs),
365 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
366 InterEventTime=[12](hrs)
367 Baseflow simulation parameters:
368 BaseFlowOption=[1] ,
369 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
370 VHydCond=[0.055](mm/hr), END=-1
371 *%-----|
372 CONTINUOUS NASHYD NHYD=["SM_DR"], DT=[1]min, AREA=[1122](ha),
373 DWF=[0](cms), CN/C=[81], IA=[2.5](mm),
374 N=[3.0], TP=[3.25]hrs,
375 Continuous simulation parameters:
376 IaREcper=[4](hrs),
377 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
378 InterEventTime=[12](hrs)
379 Baseflow simulation parameters:
380 BaseFlowOption=[1] ,
381 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
382 VHydCond=[0.055](mm/hr), END=-1
383 *%-----|
384 CONTINUOUS NASHYD NHYD=["MO_DR"], DT=[1]min, AREA=[2737](ha),
385 DWF=[0](cms), CN/C=[76], IA=[2.5](mm),
386 N=[3.0], TP=[3.03]hrs,
387 Continuous simulation parameters:
388 IaREcper=[4](hrs),
389 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),

```

```

390 InterEventTime=[12](hrs)
391 Baseflow simulation parameters:
392 BaseFlowOption=[1] ,
393 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
394 VHydCond=[0.055](mm/hr), END=-1
395 *%-----|-----
396 * -JFSA 2020 replaced SW_1 with a detailed model from Stantec Report 2007
397 *CONTINUOUS NASHYD NHYD=["SW_1"], DT=[1]min, AREA=[3176](ha),
398 * DWF=[0](cms), CN/C=[78], IA=[2.5](mm),
399 * N=[3.0], TP=[3.56]hrs,
400 * Continuous simulation parameters:
401 * IaRECper=[4](hrs),
402 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
403 * InterEventTime=[12](hrs)
404 * Baseflow simulation parameters:
405 * BaseFlowOption=[1] ,
406 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
407 * VHydCond=[0.055](mm/hr), END=-1
408 *%-----|-----
409 *#
410 *# Routing hydrographs
411 *#
412 *# Starting with the addition of Jock River Headwater and Subwatershed 13
413 *#
414 ADD HYD NHYDsum=["S_N13"], NHYDs to add=["JR_HW"+"SW_13"]
415 *%-----|-----
416 *#
417 *# Sum of hydrographs from Node 13 routed to Node 13A
418 *# (Approximated cross-section - see cross-section 258)
419 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
420 *#
421 ROUTE CHANNEL NHYDout=["N13A"] ,NHYDin=["S_N13"],
422 RDT=[1](min),
423 CHLGTH=[9074](m), CHSLOPE=[0.0220](%),
424 FPSLOPE=[0.0220](%),
425 SECNUM=[1.0], NSEG=[1]
426 ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
427 ( DISTANCE (m), ELEVATION (m))=
428 [-40, 132.5]
429 [-30, 132]
430 [-25, 131.5]
431 [-13, 130]
432 [-8, 127.00]
433 [-7, 126.50]
434 [-6, 126]
435 [-5.5, 125.50]
436 [0, 123.75]
437 [4.5, 125.50]
438 [6, 126]
439 [7.5, 126.5]
440 [9, 127]
441 [10, 127.5]
442 [11.5, 128.0]
443 [15.5, 129.5]
444 *%-----|-----
445 *#
446 *# Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
447 *#
448 ADD HYD NHYDsum=["SN13A"], NHYDs to add=["N13A"+"JR_GWM"]
449 *%-----|-----
450 *#
451 *# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
452 *#
453 ROUTE RESERVOIR NHYDout=["RES_GM"] ,NHYDin=["SN13A"],
454 RDT=[1](min),
455 TABLE of ( OUTFLOW-STORAGE ) values

```

```

456 (cms) - (ha-m)
457 [ 0.0 , 0.0 ]
458 [1.991, 2.144 ]
459 [2.693, 39.826 ]
460 [3.509, 81.697 ]
461 [4.578, 318.774 ]
462 [5.647, 594.947 ]
463 [7.109, 910.219 ]
464 [8.616, 1264.589 ]
465 [10.371, 1658.057 ]
466 [12.402, 2090.622 ]
467 [22.056, 3462.487 ]
468 [ -1 , -1 ] (max twenty pts)
469

```

```
NHYDovf=[ " " ] ,
```

```

470 *%-----|-----
471 *#
472 SAVE HYD          NHYD=["RES_GM"], # OF PCYCLES=[-1], ICASEsh=[-1]
473                   HYD_FILENAME=["H_RESGM"]
474                   HYD_COMMENT=["Outflow from Res GM"]
475 *%-----|-----

```

```

476 *# Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
477 *# (Approximated cross-section - see cross-section 258)
478 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions

```

```

479 ROUTE CHANNEL   NHYDout=["N12"] ,NHYDin=["RES_GM"] ,
480                   RDT=[1](min),
481                   CHLGTH=[5926](m),  CHSLOPE=[0.0759](%),
482                                     FPSLOPE=[0.0759](%),
483                   SECNUM=[1.0],      NSEG=[1]
484                   ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
485                   ( DISTANCE (m), ELEVATION (m))=
486                     [-40, 132.5]
487                     [-30, 132]
488                     [-25, 131.5]
489                     [-13, 130]
490                     [-8, 127.00]
491                     [-7, 126.50]
492                     [-6, 126]
493                     [-5.5, 125.50]
494                     [0, 123.75]
495                     [4.5, 125.50]
496                     [6, 126]
497                     [7.5, 126.5]
498                     [9, 127]
499                     [10, 127.5]
500                     [11.5, 128.00]
501                     [15.5, 129.5]

```

```

502 *%-----|-----
503 *#
504 *# Addition of Subwatershed Jock River at Ashton to Node 12
505 *#
506 ADD HYD          NHYDsum=["S_N12"], NHYDs to add=["N12"+"JR_ASH"]
507 SAVE HYD          NHYD=["S_N12"], # OF PCYCLES=[-1], ICASEsh=[-1]
508                   HYD_FILENAME=["H_SN12"]
509                   HYD_COMMENT=["flow at S_N12 near Ashton"]

```

```

510 *%-----|-----
511 *#
512 *# Sum of hydrographs from Node 12 routed to Node 11
513 *# (Approximated cross-section - see cross-section 258)
514 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
515 *ROUTE CHANNEL   NHYDout=["N11"] ,NHYDin=["S_N12"] ,
516 *               RDT=[1](min),
517 *               CHLGTH=[972](m),  CHSLOPE=[0.0514](%),
518 *                                     FPSLOPE=[0.0514](%),
519 *               SECNUM=[1.0],      NSEG=[1]
520 *               ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
521 *               ( DISTANCE (m), ELEVATION (m))=

```

```

522 * [-40, 132.5]
523 * [-30, 132]
524 * [-25, 131.5]
525 * [-13, 130]
526 * [-8, 127.00]
527 * [-7, 126.50]
528 * [-6, 126]
529 * [-5.5, 125.50]
530 * [0, 123.75]
531 * [4.5, 125.50]
532 * [6, 126]
533 * [7.5, 126.5]
534 * [9, 127]
535 * [10, 127.5]
536 * [11.5, 128.00]
537 * [15.5, 129.5]
538 *%-----|-----
539 *#
540 *# Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
541 *#
542 ROUTE CHANNEL NHYDout=["Dum11"] ,NHYDin=["S_N12"] ,
543 RDT=[1](min),
544 CHLGTH=[972](m), CHSLOPE=[0.054](%),
545 FPSLOPE=[0.054](%),
546 SECNUM=[1.0], NSEG=[1]
547 ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
548 ( DISTANCE (m), ELEVATION (m))=
549 [-40, 132.5]
550 [-30, 132]
551 [-25, 131.5]
552 [-13, 130]
553 [-8, 127.00]
554 [-7, 126.50]
555 [-6, 126]
556 [-5.5, 125.50]
557 [0, 123.75]
558 [4.5, 125.50]
559 [6, 126]
560 [7.5, 126.5]
561 [9, 127]
562 [10, 127.5]
563 [11.5, 128.00]
564 [15.5, 129.5]
565 *%-----|-----
566 *#
567 *# Addition of Subwatershed 11 and No Name Creek to Node 11
568 *#
569 ADD HYD NHYDsum=["S_N11"], NHYDs to add=["Dum11"+"SW_11"+"NN_CK"]
570 *%-----|-----
571 *#
572 *# Sum of hydrographs from Node 11 routed to Node 10
573 *# Section 1
574 *#
575 ROUTE CHANNEL NHYDout=["N10"] ,NHYDin=["S_N11"] ,
576 RDT=[1](min),
577 CHLGTH=[14028](m), CHSLOPE=[0.1568](%),
578 FPSLOPE=[0.1568](%),
579 SECNUM=[1.0], NSEG=[5]
580 ( SEGROUGH, SEGDIST (m))=
581 [0.04,-52.82
582 0.1,-6.47
583 -0.05,6.47
584 0.1,45.36
585 0.04,423.88] NSEG times
586 ( DISTANCE (m), ELEVATION (m))=
587 [-226.24 ,112.50]

```

```

588 [-167.50 ,111.50]
589 [-106.81 ,111.00]
590 [-92.37 ,110.00]
591 [-52.82 ,109.00]
592 [-24.90, 109.00]
593 [-17.02, 108.50]
594 [-6.47, 108.00]
595 [6.47, 108.00]
596 [15.67, 108.50]
597 [18.95, 109.00]
598 [45.36, 109.50]
599 [120.79, 110.00]
600 [145.72, 111.00]
601 [181.56, 111.50]
602 [423.88, 112.50]
603 *%-----|-----|
604 *#
605 *# Addition of Subwatershed 10 to Node 10
606 *#
607 ADD HYD          NHYDsum=["S_N10"], NHYDs to add=["N10"+"SW_10"]
608 *%-----|-----|
609 SAVE HYD       NHYD=["S_N10"], # OF PCYCLES=[-1], ICASEsh=[-1]
610                   HYD_FILENAME=["H_SN10"]
611                   HYD_COMMENT=["flow at S_N10: N10 + SW_10"]
612 *%-----|-----|
613 *# Addition of Kings Creek to S_N10
614 *#
615 ADD HYD          NHYDsum=["S_N10A"], NHYDs to add=["S_N10"+"KG_CK"]
616 *%-----|-----|
617 *#
618 *# Sum of hydrographs from Node 10 routed to Node 9
619 *# Section 2
620 *#
621 ROUTE CHANNEL   NHYDout=["N9"] ,NHYDin=["S_N10A"] ,
622                   RDT=[1](min),
623                   CHLGTH=[3982](m),  CHSLOPE=[0.0753](%),
624                                           FPSLOPE=[0.0753](%),
625                   SECNUM=[1.0],      NSEG=[4]
626                   ( SEGROUGH, SEGDIST (m))=
627                     [0.04,-30.27
628                      0.05,-18.42
629                      -0.05,18.42
630                      0.04,131.58] NSEG times
631                   ( DISTANCE (m), ELEVATION (m))=
632                     [-446.74, 106.00]
633                     [-415.68, 105.50]
634                     [-285.40, 105.00]
635                     [-173.77, 104.50]
636                     [-144.95, 104.00]
637                     [-111.18, 103.50]
638                     [-94.06, 103.00]
639                     [-71.02, 102.50]
640                     [-30.27, 102.00]
641                     [-19.33, 100.00]
642                     [-18.42, 99.50]
643                     [18.42, 99.50]
644                     [20.77, 100.00]
645                     [27.93, 101.00]
646                     [52.29, 101.00]
647                     [68.80, 101.50]
648                     [79.66, 103.00]
649                     [91.50, 103.50]
650                     [131.58, 104.00]
651 *%-----|-----|
652 *#
653 *# Addition of Subwatershed 9 and Nichols Creek to Node 9

```

```

654  *#
655  ADD HYD          NHYDsum=["S_N9"], NHYDs to add=["N9"+"SW_9"+"NC_CK"]
656  *%-----|-----
657  *#
658  *# Sum of hydrographs from Node 9 routed to Node 8
659  *# Section 3
660  *#
661  ROUTE CHANNEL    NHYDout=["N8"] ,NHYDin=["S_N9"] ,
662                  RDT=[1](min),
663                  CHLGTH=[2269](m),  CHSLOPE=[0.0882](%),
664                                          FPSLOPE=[0.0882](%),
665                  SECNUM=[1.0],      NSEG=[3]
666                  ( SEGROUGH, SEGDIST (m))=
667                    [0.1,-17.99
668                    -0.045,17.31
669                    0.1,456.58] NSEG times
670                  ( DISTANCE (m), ELEVATION (m))=
671                    [-201.19,100.50]
672                    [-135.21, 100.00]
673                    [-94.83, 99.50]
674                    [-67.05, 99.00]
675                    [-17.99, 98.50]
676                    [-16.02, 98.00]
677                    [-13.95, 97.50]
678                    [13.95, 97.50]
679                    [15.64, 98.00]
680                    [17.31, 98.50]
681                    [162.02, 98.50]
682                    [172.89 ,99.00]
683                    [314.38, 99.00]
684                    [343.78, 99.50]
685                    [365.67, 100.00]
686                    [376.68, 100.00 ]
687                    [393.11, 99.50]
688                    [404.97, 99.50]
689                    [431.70, 100.00]
690                    [456.58, 100.50 ]
691  *%-----|-----
692  *#
693  *# Addition of Subwatershed 8 and Hobb's Drain to Node 8
694  *#
695  ADD HYD          NHYDsum=["S_N8"], NHYDs to add=["N8"+"SW_8"+"HB_DR"]
696  *%-----|-----
697  *#
698  *# Sum of hydrographs from Node 8 routed to Node 7
699  *# Section 4
700  *#
701  ROUTE CHANNEL    NHYDout=["N7"] ,NHYDin=["S_N8"],
702                  RDT=[1](min),
703                  CHLGTH=[3750](m),  CHSLOPE=[0.0533](%),
704                                          FPSLOPE=[0.0533](%),
705                  SECNUM=[1.0],      NSEG=[3]
706                  ( SEGROUGH, SEGDIST (m))=
707                    [0.12,-18.11
708                    -0.07,17.22
709                    0.12,590.05] NSEG times
710                  ( DISTANCE (m), ELEVATION (m))=
711                    [-433.21, 102.00]
712                    [-425.34, 101.50]
713                    [-377.56, 101.50]
714                    [-366.23, 101.00]
715                    [-202.60, 100.50]
716                    [-96.25, 99.50]
717                    [-68.36 99.00]
718                    [-18.11, 98.50]
719                    [-13.81, 97.50]

```



```

720             [13.81, 97.50]
721             [17.22, 98.50]
722             [161.95, 98.50]
723             [173.11, 99.00]
724             [314.05, 99.00]
725             [365.52, 100.00]
726             [404.70, 99.50]
727             [476.74, 100.50]
728             [502.31, 101.00]
729             [584.69, 101.00]
730             [585.79, 101.00]
731             [590.05, 102.00]
732 *%-----|-----
733 *#
734 *# Addition of Subwatershed 7 to Node 7
735 *#
736 ADD HYD           NHYDsum=["S_N7"], NHYDs to add=["N7"+"SW_7"]
737 *%-----|-----
738 SAVE HYD         NHYD=["S_N7"], # OF PCYCLES=[-1], ICASEsh=[-1]
739                   HYD_FILENAME=["H_SN7"]
740                   HYD_COMMENT=["flow at S_N7: N7 + SW_7"]
741 *%-----|-----
742 *# Insertion of a reservoir to simulate the effects of the Richmond Fen.
743 *# Storage area and volumes were estimated from available topo maps.
744 *# Release rate from fen was assumed to be controlled by the downstream
745 *# river cross-section for summer conditions. It is was assumed that for up to
746 *# 0.75 m of water, the main channel of the river provided the storage. Above
747 *# this depth, the wetland starts to signigicantly store water.
748 *#
749 ROUTE RESERVOIR  NHYDout=["RES_RF"] ,NHYDin=["S_N7"] ,
750                   RDT=[1](min),
751                   TABLE of ( OUTFLOW-STORAGE ) values
752                             (cms) - (ha-m)
753                   TABLE of ( OUTFLOW-STORAGE ) values
754                             (cms) - (ha-m)
755                             [ 0.0 , 0.0 ]
756                             [0.9051, 2.40]
757                             [2.907, 4.13]
758                             [9.744, 9.18]
759                             [20.304, 14.96]
760                             [34.167, 310.21]
761                             [74.993, 605.46]
762                             [104.876, 900.71]
763                             [140.56, 2892.00]
764                             [225.00, 3615.63]
765                             [ -1 , -1 ] (max twenty pts)
766                   NHYDovf=[" " ] ,
767 *%-----|-----
768 SAVE HYD         NHYD=["RES_RF"], # OF PCYCLES=[-1], ICASEsh=[-1]
769                   HYD_FILENAME=["H_ResRF"]
770                   HYD_COMMENT=["outflow of Richmond Fen"]
771 *%-----|-----
772 *#
773 *# Sum of hydrographs from Node 7 routed to Node 6
774 *# Section 5
775 *#
776 ROUTE CHANNEL  NHYDout=["N6"] ,NHYDin=["RES_RF"] ,
777                   RDT=[1](min),
778                   CHLGTH=[3056](m), CHSLOPE=[0.0818](%),
779                   FPSLOPE=[0.0818](%),
780                   SECNUM=[1.0], NSEG=[5]
781                   ( SEGROUGH, SEGDIST (m))=
782                   [0.025,-70.8
783                   0.1,-23.9
784                   -0.05,23.9
785                   0.06,39.8

```

```

786             0.05,96.3] NSEG times
787             ( DISTANCE (m), ELEVATION (m))=
788                 [-100.8, 97.00]
789                 [-70.8, 96.50]
790                 [-52.0, 96.00]
791                 [-35.1, 95.50]
792                 [-30.6, 95.00]
793                 [-23.9, 94.54]
794                 [23.9, 94.54]
795                 [39.8, 95.00]
796                 [50.4, 95.50]
797                 [93.5, 96.00]
798                 [94.9, 96.50]
799                 [96.3, 97.00]
800 *%-----|-----
801 *#
802 *# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
803 *#
804 ADD HYD             NHYDsum=["S_N6"], NHYDs to add=["N6"+"SW_6"+"VG_DR"]
805 *%-----|-----
806 *#
807 *# Sum of hydrographs from Node 6 routed to Node 5
808 *# Section 6
809 *#
810 ROUTE CHANNEL     NHYDout=["N5"] ,NHYDin=["S_N6"] ,
811                     RDT=[1](min),
812                     CHLGTH=[1852](m),   CHSLOPE=[0.0540](%),
813                                     FPSLOPE=[0.0540](%),
814                     SECNUM=[1.0],       NSEG=[3]
815                     ( SEGROUGH, SEGDIST (m))=
816                         [0.035,-131.59
817                         -0.045,48.96
818                         0.1,239.04] NSEG times
819                     ( DISTANCE (m), ELEVATION (m))=
820                         [-686.30, 94.50]
821                         [-675.70, 94.00]
822                         [-492.52, 93.00]
823                         [-467.28, 94.00]
824                         [-131.59, 94.00]
825                         [-92.79, 92.50]
826                         [-18.06, 91.00]
827                         [18.06, 91.00]
828                         [43.47, 92.50]
829                         [48.96, 94.00]
830                         [177.43, 94.00]
831                         [239.04,94.50]
832 *%-----|-----
833 *#
834 *# Addition of Subwatershed 5 and Flowing Creek to Node 5
835 *#
836 ADD HYD             NHYDsum=["S_N5"], NHYDs to add=["N5"+"SW_5"+"FL_CK"]
837 *%-----|-----
838 *#
839 *# Sum of hydrographs from Node 5 routed to Node 5A
840 *# Section 7
841 *#
842 ROUTE CHANNEL     NHYDout=["N5A"] ,NHYDin=["S_N5"] ,
843                     RDT=[1](min),
844                     CHLGTH=[556](m),   CHSLOPE=[0.0900](%),
845                                     FPSLOPE=[0.0900](%),
846                     SECNUM=[1.0],       NSEG=[4]
847                     ( SEGROUGH, SEGDIST (m))=
848                         [0.04,-41.5
849                         0.1,-14.0
850                         -0.045,14.0
851                         0.1,41.1] NSEG times

```

```

852          ( DISTANCE (m), ELEVATION (m))=
853              [-275.8, 93.00]
854              [-248.6, 92.50]
855              [-237.0, 92.00]
856              [-219.3, 91.50]
857              [-202.1, 91.50]
858              [-186.0, 92.00]
859              [-129.2, 92.00]
860              [-117.6, 91.50]
861              [-100.6, 91.00]
862              [-41.5, 91.00]
863              [-20.0, 91.00]
864              [-14.0, 90.54]
865              [14.0, 90.54]
866              [15.3, 91.00]
867              [17.3, 91.50]
868              [38.4, 92.00]
869              [39.8, 92.50]
870              [41.1, 93.00]
871  *%-----|-----
872  *#
873  *# Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
874  *#
875  ADD HYD          NHYDsum=["S_N5A"], NHYDs to add=["N5A"+"SW_5A2"+"SW_5A1"]
876  *%-----|-----
877  *#
878  *# Sum of hydrographs from Node 5A routed to Node 4
879  *# Section 8
880  *#
881  ROUTE CHANNEL    NHYDout=["N4"] ,NHYDin=["S_N5A"] ,
882                  RDT=[1](min),
883                  CHLGTH=[4630](m),  CHSLOPE=[0.0432](%),
884                                          FPSLOPE=[0.0432](%),
885                  SECNUM=[1.0],      NSEG=[3]
886                  ( SEGROUGH, SEGDIST (m))=
887                      [0.05,-28.2
888                      -0.035,28.2
889                      0.05,173.1] NSEG times
890                  ( DISTANCE (m), ELEVATION (m))=
891                      [-38.9, 92.00]
892                      [-35.8, 91.50]
893                      [-33.3, 91.00]
894                      [-28.2, 90.50]
895                      [-15.0, 87.48]
896                      [-5.0, 88.34]
897                      [5.0, 86.20]
898                      [15.0, 88.55]
899                      [28.2, 90.50]
900                      [29.7, 91.00]
901                      [46.5, 91.00]
902                      [127.8, 91.00]
903                      [148.7, 91.50]
904                      [173.1, 92.00]
905  *%-----|-----
906  *#
907  *# Addition of Subwatershed 4 and Leamy Creek to Node 4
908  *#
909  ADD HYD          NHYDsum=["S_N4"], NHYDs to add=["N4"+"SW_4"+"LM_CK"]
910  SAVE HYD         NHYD=["S_N4"], # OF PCYCLES=[-1], ICASEsh=[1]
911                  HYD_COMMENT=["flow at S_N4"]
912  *%-----|-----
913  *#
914  *# Sum of hydrographs from Node 4 routed to Node 2
915  *# Section 9
916  *#
917  ROUTE CHANNEL    NHYDout=["N2"] ,NHYDin=["S_N4"] ,

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918 RDT=[1](min),
919 CHLGTH=[1667](m), CHSLOPE=[0.0600](%),
920 FPSLOPE=[0.0600](%),
921 SECNUM=[1.0], NSEG=[4]
922 ( SEGROUGH, SEGDIST (m))=
923 [0.1,-28.0
924 -0.04,28.4
925 0.06,31.7
926 0.04,80.2] NSEG times
927 ( DISTANCE (m), ELEVATION (m))=
928 [-36.3, 92.00]
929 [-32.6, 91.50]
930 [-30.2, 91.00]
931 [-28.0, 90.45]
932 [-15.0, 87.48]
933 [-5.0, 88.34]
934 [5.0, 86.20]
935 [15.0, 88.55]
936 [28.0, 90.45]
937 [28.4, 90.50]
938 [30.4, 91.00]
939 [31.7, 91.50]
940 [80.2, 92.00]
941 *%-----|-----
942 *#
943 *# Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2
944 *#
945 ADD HYD NHYDsum=["S_N2"], NHYDs to add=["N2"+"SW_2"+"SM_DR"+"MO_DR"]
946 *%-----|-----
947 SAVE HYD NHYD=["S_N2"], # OF PCYCLES=[-1], ICASEsh=[-1]
948 HYD_FILENAME=["H_SN2"]
949 HYD_COMMENT=["flow at S_N2 Jock River Gauge at Moodie Dr."]
950 *%-----|-----
951 *#
952 *# Sum of hydrographs from Node 2 routed to Node 1
953 *# Section 10
954 *#
955 *#*****
956 *%READ HYD NHYD=["S_N2"],
957 *% HYD_FILENAME=["H-S_N2"]
958 *%-----|-----
959 *#
960 *# Hydrograph from Node 2 routed to Node 416
961 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 9025
962 *#
963 ROUTE CHANNEL NHYDout=["N_416"] ,NHYDin=["S_N2"] ,
964 RDT=[1](min),
965 CHLGTH=[2327](m), CHSLOPE=[0.0498](%),
966 FPSLOPE=[0.0498](%),
967 SECNUM=[1.0], NSEG=[3]
968 ( SEGROUGH, SEGDIST (m))=
969 [0.075,-23.96
970 -0.055,23.96
971 0.075,157.38] NSEG times
972 ( DISTANCE (m), ELEVATION (m))=
973 [-336.97,93.5]
974 [-318.85,93]
975 [-259,92.5]
976 [-133.18,92]
977 [-33.17,92]
978 [-27.21,92]
979 [-26.14,91.5]
980 [-24.99,91]
981 [-23.96,90.5]
982 [-14.33,88.26]
983 [-0.68,88.12]

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984 [14.33,88.26]
985 [23.96,90.5]
986 [32.12,91]
987 [43.74,91.5]
988 [57.09,92]
989 [73.53,92.5]
990 [108.27,93]
991 [125.88,93.5]
992 [144.81,94]
993 [157.38,94.5]
994 *%-----|-----|
995 *#*****|
996 *# Catchment SW-1a
997 *# - Portion of RVCA catchment SW_1 outside of Reach 1 subwatershed
998 *# - Undeveloped agricultural land
999 *#*****|
1000 CONTINUOUS NASHYD NHYD=["SW_1a"], DT=[1]min, AREA=[536.42](ha),
1001 DWF=[0](cms), CN/C=[72], IA=[4.67](mm),
1002 N=[3], TP=[2.79]hrs,
1003 Continuous simulation parameters:
1004 IaREcper=[4](hrs),
1005 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1006 InterEventTime=[12](hrs)
1007 Baseflow simulation parameters:
1008 BaseFlowOption=[1],
1009 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1010 VHydCond=[0.055](mm/hr), END=-1
1011 *%-----|-----|
1012 * -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
before station 7245 on Jock River
1013 CONTINUOUS STANDHYD NHYD=["S-1-Okeefe"], DT=[1](min), AREA=[44.93](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
1014 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
IAPER=[4.67](mm), SLPP=[2.0](%),
1015 LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
1016 LGI=[547.296](m), MNI=[0.013], SCI=[0](min),
1017 Continuous simulation parameters:
1018 IaREcper=[4](hrs), IaREcimp=[4](hrs),
1019 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1020 InterEventTime=[12](hrs), END=-1
1021 *%-----|-----|
1022 *COMPUTE DUALHYD NHYDin=["S-1-Okeefe"], CINLET=[4.796](cms), NINLET=[1],
1023 * MajNHYD=["S-1-OkMJ"]
1024 * MinNHYD=["S-1-OkMN"]
1025 * TMJSTO=[9999999](cu-m)
1026 *%-----|-----|
1027 *ADD HYD NHYDsum=["S-1-OkS"], NHYDs to add=["S-1-OkMJ"+"S-1-OkMN"]
1028 *%-----|-----|
1029 *ROUTE RESERVOIR NHYDout=["S-1-OkSR"],NHYDin=["S-1-OkS"],
1030 * RDT=[1](min),
1031 * TABLE of ( OUTFLOW-STORAGE ) values
1032 * (cms) - (ha-m)
1033 * [ 0.0 , 0.0 ]
1034 * [ 0.5370, 1.7917 ]
1035 * [ -1 , -1 ] (max twenty pts)
1036 * NHYDovf=["S-1-OkSovf"]
1037 *%-----|-----|
1038 ADD HYD NHYDsum=["SN_416"], NHYDs to add=["N_416"+"SW_1a"+"S-1-Okeefe"]
1039 *%-----|-----|
1040 SAVE HYD NHYD=["SN_416"], # OF PCYCLES=[-1], ICASEsh=[1]
1041 HYD_COMMENT=["Total Flows at Highway 416"]
1042 *%-----|-----|
1043 *#
1044 *# Hydrograph from Node 416 routed to Node at Okeefe drain
1045 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 7245

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1046 *#
1047 ROUTE CHANNEL      NHYDout=["N_OK"] ,NHYDin=["SN_416"] ,
1048                   RDT=[1](min),
1049                   CHLGTH=[497](m),  CHSLOPE=[0.3018](%),
1050                                     FPSLOPE=[0.3018](%),
1051                   SECNUM=[1.0],      NSEG=[3]
1052                   ( SEGROUGH, SEGDIST (m))=
1053                   [0.075,-19.40
1054                   -0.055,19.40
1055                   0.075,377.02] NSEG times
1056                   ( DISTANCE (m), ELEVATION (m))=
1057                   [-1061.41, 92.50]
1058                   [-945.91, 92.00]
1059                   [-783.64, 91.50]
1060                   [-136.74, 91.00]
1061                   [-86.04, 91.00]
1062                   [-20.86, 91.00]
1063                   [-20.18, 90.50]
1064                   [-19.40, 90.00]
1065                   [-11.68, 86.89]
1066                   [0.00, 86.10]
1067                   [12.09, 86.81]
1068                   [19.40, 90.00]
1069                   [34.68, 90.50]
1070                   [60.56, 91.00]
1071                   [170.14, 91.00]
1072                   [175.05, 90.50]
1073                   [180.29, 90.00]
1074                   [193.41, 90.00]
1075                   [195.98, 90.50]
1076                   [377.02, 92.50]
1077 *%-----|-----|
1078 *#*****|
1079 *#   Catchment OKEEFE
1080 *#   - To O'Keefe drain (north of the Jock)
1081 *#   - Developed with assumed 43% imp.
1082 *#   - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area
1083 *#   - 2020-11-20 Okeefe detailed model was added as per the NOVATECH SWMHYMO model
1084 *#   (Citi-Gate 2014).
1085 *%-----|-----|
1086 *POST DEVELOPMENT CONDITIONS
1087 *%-----|-----|
1088 *#*****|
1089 CONTINUOUS NASHYD  NHYD=["O-1"], DT=[1]min, AREA=[63.72](ha),
1090                   DWF=[0](cms), CN/C=[61], IA=[6.2](mm), N=[3], TP=[.9]hrs,
1091                   Continuous simulation parameters:
1092                   IaRECPper=[4](hrs),
1093                   SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
1094                   InterEventTime=[12](hrs)
1095                   Baseflow simulation parameters:
1096                   BaseFlowOption=[1] ,
1097                   InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1098                   VHydCond=[0.055](mm/hr),  END=-1
1099 *%-----|-----|
1100 *ROUTE FLOW THROUGH AREA 0-2
1101 ROUTE CHANNEL      NHYDout=["O-1R"], NHYDin=["O-1"], RDT=[1](min),
1102                   CHLGTH=[960](m), CHSLOPE=[0.63](%), FPSLOPE=[0.63](%),
1103                   SECNUM=[1], NSEG=[3]
1104                   ( SEGROUGH, SEGDIST (m))=[0.06,4 -.043,6 0.06,10] NSEG times
1105                   ( DISTANCE (m), ELEVATION (m))=[0.00, 2.0]
1106                   [0.0, 2.0]
1107                   [4.0, 0.0]
1108                   [6.0, 0.0]
1109                   [10.0, 2.0]

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1109 *%-----|-----
1110 CONTINUOUS NASHYD NHYD=["O-2"], DT=[1]min, AREA=[28.61](ha),
1111 DWF=[0](cms), CN/C=[57], IA=[5.2](mm), N=[3], TP=[1.1]hrs,
1112 Continuous simulation parameters:
1113 IaREcper=[4](hrs),
1114 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1115 InterEventTime=[12](hrs)
1116 Baseflow simulation parameters:
1117 BaseFlowOption=[1] ,
1118 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1119 VHydCond=[0.055](mm/hr), END=-1
1120 *%-----|-----
1121 CONTINUOUS NASHYD NHYD=["O-4"], DT=[1]min, AREA=[46.94](ha),
1122 DWF=[0](cms), CN/C=[49], IA=[9.2](mm), N=[3], TP=[0.9]hrs,
1123 Continuous simulation parameters:
1124 IaREcper=[4](hrs),
1125 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1126 InterEventTime=[12](hrs)
1127 Baseflow simulation parameters:
1128 BaseFlowOption=[1] ,
1129 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1130 VHydCond=[0.055](mm/hr), END=-1
1131 *%-----|-----
1132 *TOTAL EXTERNAL FLOW NORTH OF O'KEEFE CT. CROSSING
1133 ADD HYD NHYDsum=["OKF-N"], NHYDs to add=["O-1R"+"O-2"+"O-4"]
1134 *%-----|-----
1135 *ROUTE FLOW THROUGH AREA O-6
1136 ROUTE CHANNEL ROUTE CHANNEL NHYDout=["OKF-NR"], NHYDin=["OKF-N"], RDT=[1](min),
1137 CHLGTH=[210](m), CHSLOPE=[.81](%), FPSLOPE=[.81](%),
1138 SECNUM=[1], NSEG=[3]
1139 ( SEGROUGH, SEGDIST (m))=[0.043,22.43 -0.043,25.07
1140 0.043,45.54] NSEG times
1141 ( DISTANCE (m), ELEVATION (m))=[0.00, 3.73]
1142 (14.62, 1.56)
1143 (18.41, 1.44)
1144 (22.43, 0.00)
1145 (25.07, 0.70)
1146 (29.10, 1.79)
1147 (33.73, 2.71)
1148 (45.54, 3.58)
1149 *%-----|-----
1150 CONTINUOUS NASHYD NHYD=["O-6"], DT=[1]min, AREA=[16.46](ha),
1151 DWF=[0](cms), CN/C=[43], IA=[9.2](mm), N=[3], TP=[0.7]hrs,
1152 Continuous simulation parameters:
1153 IaREcper=[4](hrs),
1154 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1155 InterEventTime=[12](hrs)
1156 Baseflow simulation parameters:
1157 BaseFlowOption=[1] ,
1158 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1159 VHydCond=[0.055](mm/hr), END=-1
1160 *%-----|-----
1161 CONTINUOUS STANDHYD NHYD=["O-3"], DT=[1](min), AREA=[39.67](ha), XIMP=[0.15],
1162 TIMP=[0.30], DWF=[0](cms),
1163 LOSS=[2], SCS curve number CN=[50], Pervious surfaces:
1164 IAper=[4.67](mm), SLPP=[0.32](%),
1165 LGP=[440](m), MNP=[0.035], SCP=[0](min), Impervious surfaces:
1166 IAimp=[1.57](mm), SLPI=[0.32](%),
1167 LGI=[1880](m), MNI=[0.013], SCI=[0](min),
1168 Continuous simulation parameters:
1169 IaREcper=[4](hrs), IaREcimp=[4](hrs),
1170 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1171 InterEventTime=[12](hrs), END=-1
1172 *%-----|-----
1173 CONTINUOUS STANDHYD NHYD=["O-5"], DT=[1](min), AREA=[60.63](ha), XIMP=[0.13],
1174 TIMP=[0.26], DWF=[0](cms),

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1171      LOSS=[2], SCS curve number CN=[61],
1172      Pervious surfaces: IAPER=[4.67](mm), SLPP=[1.38](%),
1173      LGP=[550](m), MNP=[0.035], SCP=[0](min), Impervious surfaces:
1174      IAimp=[1.57](mm), SLPI=[1.38](%),
1175      LGI=[1450](m), MNI=[0.013], SCI=[0](min),
1176      Continuous simulation parameters:
1177      IaREcper=[4](hrs), IaREcimp=[4](hrs),
1178      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1179      InterEventTime=[12](hrs), END=-1
1180 *%-----|-----|
1181 *TOTAL EXTERNAL FLOWS WEST OF THE SITE AND NORTH OF O'KEEFE CRT
1182 *%-----|-----|
1183 ADD HYD      NHYDsum=["PT1"], NHYDs to add=["OKF-NR"+"O-3"+"O-5"+"O-6"]
1184 *%-----|-----|
1185 CONTINUOUS NASHYD      NHYD=["O-7"], DT=[1]min, AREA=[5.28](ha),
1186      DWF=[0](cms), CN/C=[54], IA=[7.5](mm), N=[3], TP=[0.6]hrs,
1187      Continuous simulation parameters:
1188      IaREcper=[4](hrs),
1189      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1190      InterEventTime=[12](hrs)
1191      Baseflow simulation parameters:
1192      BaseFlowOption=[1] ,
1193      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1194      VHydCond=[0.055](mm/hr), END=-1
1195 *%-----|-----|
1196 *ANALYSIS POINT 1 - TOTAL FLOW NORTH OF FALLOWFIELD DR. AND O'KEEFE CRT.
1197 ADD HYD      NHYDsum=["FF"], NHYDs to add=["PT1"+"O-7"]
1198 *%-----|-----|
1199 *ROUTE FLOW through O'Keefe Drain 1
1200 ROUTE CHANNEL      NHYDout=["DRAIN1"], NHYDin=["FF"], RDT=[1](min),
1201      CHLGTH=[302]{m}, CHSLOPE=[1.00](%), FPSLOPE=[1.00](%),
1202      SECNUM=[1], NSEG=[3]
1203      ( SEGROUGH, SEGDIST (m))=[0.07,13.45 -0.043,16.55 0.07,30.00] NSEG
1204      times
1205      ( DISTANCE (m), ELEVATION (m))=[0.00, 1.70]
1206      (3.45, 0.60)
1207      (13.45, 0.50)
1208      (14.45, 0.00)
1209      (15.55, 0.00)
1210      (16.55, 0.50)
1211      (26.55, 0.60)
1212      (30.00, 1.70)
1213 *%-----|-----|
1214 CONTINUOUS NASHYD      NHYD=["D1"], DT=[1]min, AREA=[1.17](ha),
1215      DWF=[0](cms), CN/C=[84], IA=[9.0](mm), N=[3], TP=[0.28]hrs,
1216      Continuous simulation parameters:
1217      IaREcper=[4](hrs),
1218      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1219      InterEventTime=[12](hrs)
1220      Baseflow simulation parameters:
1221      BaseFlowOption=[1] ,
1222      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1223      VHydCond=[0.055](mm/hr), END=-1
1224 *%-----|-----|
1225 CONTINUOUS STANDHYD      NHYD=["A1"], DT=[1]min, AREA=[2.50](ha), XIMP=[0.68], TIMP=[0.85],
1226      DWF=[0](cms), LOSS=[1]:
1227      Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1228      F=[0.00](mm),
1229      Pervious areas: IAPER=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1230      MNP=[0.250], SCP=[0](min),
1231      Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
1232      LGI=[223.607](m), MNI=[0.013], SCI=[0](min),
1233      Continuous simulation parameters:
1234      IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
1235      END=-1
1236 *%-----|-----|

```

```

1230 ROUTE RESERVOIR      NHYDout=["A1-STR"], NHYDin=["A1"], RDT=[1](min),
1231                      TABLE of ( OUTFLOW-STORAGE ) values
1232                      (cms) - (ha-m)
1233                      [ 0.000 , 0.000 ]
1234                      [ 0.035 , 0.038 ]
1235                      [ 0.072 , 0.051 ]
1236                      [ 0.100 , 0.059 ]
1237                      [ 0.125 , 0.070 ]
1238                      [ 0.160 , 0.074 ]
1239                      [ 0.185 , 0.081 ]
1240                      [ -1 , -1 ] (max twenty pts)
1241                      NHYDovf=["A1-OVF"]
1242 *%-----|-----|
1243 CONTINUOUS STANDHYD NHYD=["ST-2"], DT=[1]min, AREA=[0.59](ha), XIMP=[0.46],
TIMP=[0.57], DWF=[0](cms), LOSS=[1]:
1244 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1245 Pervious areas: IAPER=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1246 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[108.628](m), MNI=[0.013], SCI=[0](min),
1247 Continuous simulation parameters:
1248 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1249 *%-----|-----|
1250 ROUTE RESERVOIR      NHYDout=["ST2STR"], NHYDin=["ST-2"], RDT=[1](min),
1251                      TABLE of ( OUTFLOW-STORAGE ) values
1252                      (cms) - (ha-m)
1253                      [ 0.000 , 0.0000 ]
1254                      [ 0.052 , 0.0010 ]
1255                      [ 0.053 , 0.0080 ]
1256                      [ -1 , -1 ] (max twenty pts)
1257                      NHYDovf=["ST2OVF"]
1258 *%-----|-----|
1259 *%-----|-----|
1260 *TOTAL FLOW NORTH OF STRANDHERD DR. (EAST BRANCH) CROSSING
1261 *%-----|-----|
1262 CONTINUOUS NASHYD    NHYD=["O-8"], DT=[1]min, AREA=[60.55](ha),
1263 DWF=[0](cms), CN/C=[69], IA=[4.0](mm), N=[3], TP=[1.0]hrs,
1264 Continuous simulation parameters:
1265 IaRECper=[4](hrs),
1266 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1267 InterEventTime=[12](hrs)
1268 Baseflow simulation parameters:
1269 BaseFlowOption=[1] ,
1270 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1271 VHydCond=[0.055](mm/hr), END=-1
1272 *%-----|-----|
1273 ROUTE PIPE           PTYPE=[2]rect, NHYDout=["O8PIPE"], RNUMBER=[1], PWIDTH=[1800](mm),
PHEIGHT=[1200](mm), PLNGTH=[335.1](m),
1274 PROUGH=[0.013], PSLOPE=[0.001](m/m), NHYDin=["O-8"], RDT=[1](min)
1275 *%-----|-----|
1276 *%-----|-----|
1277 ADD HYD              NHYDsum=["ST2-IN"], NHYDs to
add=["DRAIN1"+"D1"+"A1-STR"+"A1-OVF"+"ST2STR"+"ST2OVF"+"O8PIPE"]
1278 *%-----|-----|
1279 CONTINUOUS STANDHYD NHYD=["A7"], DT=[1]min, AREA=[3.51](ha), XIMP=[0.68], TIMP=[0.85],
DWF=[0](cms), LOSS=[1]:
1280 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1281 Pervious areas: IAPER=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1282 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[264.953](m), MNI=[0.013], SCI=[0](min),
1283 Continuous simulation parameters:
1284 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),

```

END=-1

```

1285 *%-----|-----|
1286 ROUTE RESERVOIR NHYDout=["A7-STR"], NHYDin=["A7"], RDT=[1](min),
1287             TABLE of ( OUTFLOW-STORAGE ) values
1288             (cms) - (ha-m)
1289             [ 0.000 , 0.000 ]
1290             [ 0.049 , 0.054 ]
1291             [ 0.102 , 0.072 ]
1292             [ 0.140 , 0.082 ]
1293             [ 0.175 , 0.099 ]
1294             [ 0.225 , 0.105 ]
1295             [ 0.260 , 0.114 ]
1296             [ -1 , -1 ] (max twenty pts)
1297             NHYDovf=["A7-OVF"]

```

```

1298 *%-----|-----|
1299 CONTINUOUS STANDHYD NHYD=["ST-3"], DT=[1]min, AREA=[0.71](ha), XIMP=[0.46],
TIMP=[0.57], DWF=[0](cms), LOSS=[1]:
1300 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1301 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1302 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[119.164](m), MNI=[0.013], SCI=[0](min),
1303 Continuous simulation parameters:
1304 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1

```

```

1305 *%-----|-----|
1306 ROUTE RESERVOIR NHYDout=["ST3STR"], NHYDin=["ST-3"], RDT=[1](min),
1307             TABLE of ( OUTFLOW-STORAGE ) values
1308             (cms) - (ha-m)
1309             [ 0.000 , 0.0000 ]
1310             [ 0.063 , 0.0010 ]
1311             [ 0.064 , 0.0094 ]
1312             [ -1 , -1 ] (max twenty pts)
1313             NHYDovf=["ST3OVF"]

```

```

1314 *%-----|-----|
1315 *ANALYSIS POINT 2 - TOTAL FLOW AT OUTLET OF STREET 2/3 INTERSECTION
1316 *%-----|-----|

```

```

1317 ADD HYD NHYDsum=["PT2ST3"], NHYDs to
add=["ST2-IN"+"A7-STR"+"A7-OVF"+"ST3STR"+"ST3OVF"]

```

```

1318 *%-----|-----|
1319 *ROUTE FLOW through O'Keefe Drain 2

```

```

1320 ROUTE CHANNEL NHYDout=["DRAIN2"], NHYDin=["PT2ST3"], RDT=[1](min),
1321             CHLGTH=[592]{m}, CHSLOPE=[.23](%), FPSLOPE=[.23](%),
1322             SECNUM=[1], NSEG=[3]
1323             ( SEGROUGH, SEGDIST (m))=[0.07,12.60 -0.043,17.40 0.07,30.00] NSEG
times
1324             ( DISTANCE (m), ELEVATION (m))=[0.00, 1.70]
1325             (2.60, 0.95)
1326             (12.60, 0.75)
1327             (14.10, 0.00)
1328             (15.90, 0.00)
1329             (17.40, 0.75)
1330             (27.40, 0.95)
1331             (30.00, 1.70)

```

```

1332 *%-----|-----|
1333 CONTINUOUS NASHYD NHYD=["D2"], DT=[1]min, AREA=[2.28](ha), DWF=[0](cms), CN/C=[84],
IA=[9.0](mm),
1334 N=[3], TP=[0.99]hrs,
1335 Continuous simulation parameters:
1336 IaREcper=[4](hrs),
1337 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1338 InterEventTime=[12](hrs)
1339 Baseflow simulation parameters:
1340 BaseFlowOption=[1] ,
1341 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)

```

```

1342          VHydCond=[0.055](mm/hr),   END=-1
1343  *%-----|-----|
1344  CONTINUOUS STANDHYD NHYD=["A17"], DT=[1]min, AREA=[12.04](ha), XIMP=[0.68],
1345  TIMP=[0.85], DWF=[0](cms), LOSS=[1]:
1346  Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1347  F=[0.00](mm),
1348  Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1349  MNP=[0.250], SCP=[0](min),
1350  Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
1351  LGI=[490.714](m), MNI=[0.013], SCI=[0](min),
1352  Continuous simulation parameters:
1353  IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
1354  END=-1
1355  *%-----|-----|
1356  ROUTE RESERVOIR NHYDout=["A17STR"], NHYDin=["A17"], RDT=[1](min),
1357  TABLE of ( OUTFLOW-STORAGE ) values
1358  (cms) - (ha-m)
1359  [ 0.000 , 0.000 ]
1360  [ 0.169 , 0.185 ]
1361  [ 0.349 , 0.248 ]
1362  [ 0.482 , 0.283 ]
1363  [ 0.602 , 0.338 ]
1364  [ 0.771 , 0.359 ]
1365  [ 0.891 , 0.391 ]
1366  [ -1 , -1 ] (max twenty pts)
1367  NHYDovf=["A17OVF"]
1368  *%-----|-----|
1369  CONTINUOUS STANDHYD NHYD=["ST-4"], DT=[1]min, AREA=[0.35](ha), XIMP=[0.46],
1370  TIMP=[0.57], DWF=[0](cms), LOSS=[1]:
1371  Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1372  F=[0.00](mm),
1373  Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1374  MNP=[0.250], SCP=[0](min),
1375  Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[83.666](m),
1376  MNI=[0.013], SCI=[0](min),
1377  Continuous simulation parameters:
1378  IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
1379  END=-1
1380  *%-----|-----|
1381  ROUTE RESERVOIR NHYDout=["ST4STR"], NHYDin=["ST-4"], RDT=[1](min),
1382  TABLE of ( OUTFLOW-STORAGE ) values
1383  (cms) - (ha-m)
1384  [ 0.000 , 0.0000 ]
1385  [ 0.031 , 0.0010 ]
1386  [ 0.032 , 0.0050 ]
1387  [ -1 , -1 ] (max twenty pts)
1388  NHYDovf=["ST4OVF"]
1389  *%-----|-----|
1390  CONTINUOUS STANDHYD NHYD=["A18"], DT=[1]min, AREA=[5.30](ha), XIMP=[0.68], TIMP=[0.85],
1391  DWF=[0](cms), LOSS=[1]:
1392  Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1393  F=[0.00](mm),
1394  Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1395  MNP=[0.250], SCP=[0](min),
1396  Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
1397  LGI=[325.576](m), MNI=[0.013], SCI=[0](min),
1398  Continuous simulation parameters:
1399  IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
1400  END=-1
1401  *%-----|-----|
1402  ROUTE RESERVOIR NHYDout=["A18STR"], NHYDin=["A18"], RDT=[1](min),
1403  TABLE of ( OUTFLOW-STORAGE ) values
1404  (cms) - (ha-m)
1405  [ 0.000 , 0.000 ]
1406  [ 0.074 , 0.082 ]
1407  [ 0.154 , 0.109 ]

```

```

1393         [ 0.212 , 0.125 ]
1394         [ 0.265 , 0.149 ]
1395         [ 0.339 , 0.158 ]
1396         [ 0.392 , 0.172 ]
1397         [ -1 , -1 ] (max twenty pts)
1398         NHYDovf=["A18OVF"]
1399 *%-----|-----|
1400 *ANALYSIS POINT 3 - TOTAL FLOW AT OUTLET OF STREET 4
1401 *%-----|-----|
1402 ADD HYD          NHYDsum=["PT3ST4"], NHYDs to
add=["DRAIN2"+"D2"+"A17STR"+"A17OVF"+"ST4STR"+"ST4OVF"+"A18STR"+"A18OVF"]
1403 *%-----|-----|
1404 *ROUTE FLOW through O'Keefe Drain 3
1405 ROUTE CHANNEL   NHYDout=["DRAIN3"], NHYDin=["PT3ST4"], RDT=[1](min),
1406                 CHLGTH=[525]{m}, CHSLOPE=[.23](%), FPSLOPE=[.23](%),
1407                 SECNUM=[1], NSEG=[3]
1408                 ( SEGROUGH, SEGDIST (m))=[0.07,12.50 -0.043,17.50 0.07,30.00] NSEG
times
1409                 ( DISTANCE (m), ELEVATION (m))=[0.00, 1.70]
1410                 (2.50, 1.00)
1411                 (12.50, 0.80)
1412                 (14.10, 0.00)
1413                 (15.90, 0.00)
1414                 (17.50, 0.80)
1415                 (27.50, 1.00)
1416                 (30.00, 1.70)
1417 *%-----|-----|
1418 CONTINUOUS NASHYD NHYD=["D3"], DT=[1]min, AREA=[2.51](ha),
1419                 DWF=[0](cms), CN/C=[86], IA=[8.7](mm), N=[3], TP=[0.73]hrs,
1420                 Continuous simulation parameters:
1421                 IaRECper=[4](hrs),
1422                 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1423                 InterEventTime=[12](hrs)
1424                 Baseflow simulation parameters:
1425                 BaseFlowOption=[1] ,
1426                 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1427                 VHydCond=[0.055](mm/hr), END=-1
1428 *%-----|-----|
1429 CONTINUOUS STANDHYD NHYD=["C1"], DT=[1]min, AREA=[3.41](ha), XIMP=[0.68], TIMP=[0.85],
DWF=[0](cms), LOSS=[1]:
1430                 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1431                 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1432                 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[261.151](m), MNI=[0.013], SCI=[0](min),
1433                 Continuous simulation parameters:
1434                 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1435 *%-----|-----|
1436 ROUTE RESERVOIR  NHYDout=["C1-STR"], NHYDin=["C1"], RDT=[1](min),
1437                 TABLE of ( OUTFLOW-STORAGE ) values
1438                 (cms) - (ha-m)
1439                 [ 0.000 , 0.000 ]
1440                 [ 0.048 , 0.052 ]
1441                 [ 0.099 , 0.070 ]
1442                 [ 0.136 , 0.080 ]
1443                 [ 0.170 , 0.096 ]
1444                 [ 0.218 , 0.102 ]
1445                 [ 0.252 , 0.111 ]
1446                 [ -1 , -1 ] (max twenty pts)
1447                 NHYDovf=["C1-OVF"]
1448 *%-----|-----|
1449 CONTINUOUS STANDHYD NHYD=["ST-5"], DT=[1]min, AREA=[0.45](ha), XIMP=[0.46],
TIMP=[0.57], DWF=[0](cms), LOSS=[1]:
1450                 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),

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1451           F=[0.00](mm),
1452           Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1453           MNP=[0.250], SCP=[0](min),
1454           Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[94.868](m),
1455           MNI=[0.013], SCI=[0](min),
1456           Continuous simulation parameters:
1457           IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
1458           END=-1
1459
1460 *%-----|-----|
1461 ROUTE RESERVOIR NHYDout=["ST5STR"], NHYDin=["ST-5"], RDT=[1](min),
1462           TABLE of ( OUTFLOW-STORAGE ) values
1463           (cms) - (ha-m)
1464           [ 0.000 , 0.0000 ]
1465           [ 0.040 , 0.0010 ]
1466           [ 0.041 , 0.0062 ]
1467           [ -1 , -1 ] (max twenty pts)
1468           NHYDovf=["ST5OVF"]
1469
1470 *%-----|-----|
1471 ADD HYD NHYDsum=["ST5-E"], NHYDs to
1472 add=["DRAIN3"+"D3"+"C1-STR"+"C1-OVF"+"ST5STR"+"ST5OVF"]
1473
1474 *%-----|-----|
1475 CONTINUOUS STANDHYD NHYD=["STRAND"], DT=[1](min), AREA=[7.59](ha),
1476 XIMP=[0.64], TIMP=[0.85], DWF=[0](cms), LOSS=[1]:
1477 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1478 F=[0.00](mm),
1479 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[40](m),
1480 MNP=[0.250], SCP=[0](min),
1481 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[1230](m),
1482 MNI=[0.013], SCI=[0](min),
1483 Continuous simulation parameters:
1484 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
1485 END=-1
1486
1487 *%-----|-----|
1488 ROUTE RESERVOIR NHYDout=["S-POND"], NHYDin=["STRAND"], RDT=[1](min),
1489           TABLE of ( OUTFLOW-STORAGE ) values
1490           (cms) - (ha-m)
1491           [ 0.000 , 0.000 ]
1492           [ 0.033 , 0.188 ]
1493           [ 0.057 , 0.253 ]
1494           [ 0.104 , 0.287 ]
1495           [ 0.160 , 0.336 ]
1496           [ 0.340 , 0.346 ]
1497           [ 0.471 , 0.360 ]
1498           [ 0.824 , 0.390 ]
1499           [ -1 , -1 ] (max twenty pts)
1500           NHYDovf=["S-OVF"]
1501
1502 *%-----|-----|
1503 ADD HYD NHYDsum=["SSAOUT"], NHYDs to add=["ST5-E"+"S-POND"+"S-OVF"]
1504
1505 *%-----|-----|
1506 SAVE HYD NHYD=["SSAOUT"], # OF PCYCLES=[5], ICASEsh=[1]
1507 HYD_COMMENT=["SSAOUT"]
1508
1509 *%-----|-----|
1510 CONTINUOUS STANDHYD NHYD=["Area-A"], DT=[1]min, AREA=[66.75](ha), XIMP=[0.64],
1511 TIMP=[0.80], DWF=[0](cms), LOSS=[1]:
1512 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1513 F=[0.00](mm),
1514 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1515 MNP=[0.250], SCP=[0](min),
1516 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
1517 LGI=[1155.422](m), MNI=[0.013], SCI=[0](min),
1518 Continuous simulation parameters:
1519 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
1520 END=-1
1521
1522 *%-----|-----|
1523 SAVE HYD NHYD=["Area-A"], # OF PCYCLES=[1], ICASEsh=[1]
1524 HYD_COMMENT=["SMWF-A Inflow"]

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1503 *%-----|-----|
1504 ROUTE RESERVOIR NHYDout=["SWMF-A"], NHYDin=["Area-A"], RDT=[1](min),
1505             TABLE of ( OUTFLOW-STORAGE ) values
1506             (cms) - (ha-m)
1507             [ 0.000 , 0.000 ]
1508             [ 0.103 , 1.077 ]
1509             [ 0.128 , 1.749 ]
1510             [ 0.382 , 2.282 ]
1511             [ 0.703 , 2.582 ]
1512             [ 1.256 , 2.978 ]
1513             [ 1.567 , 3.202 ]
1514             [ 1.955 , 3.493 ]
1515             [ 2.100 , 3.600 ]
1516             [ -1 , -1 ] (max twenty pts)
1517             NHYDovf=["SWMAOV"]
1518 *%-----|-----|
1519 SAVE HYD NHYD=["SWMF-A"], # OF PCYCLES=[1], ICASEsh=[1]
1520 HYD_COMMENT=["SMWF-A Outflow"]
1521 *%-----|-----|
1522 *ANALYSIS POINT 4 - TOTAL FLOW AT OUTLET OF STREET 5
1523 *%-----|-----|
1524 ADD HYD NHYDsum=["PT4ST5"], NHYDs to add=["SSAOUT"+"SWMF-A"+"SWMAOV"]
1525 *%-----|-----|
1526 CONTINUOUS STANDHYD NHYD=["C6"], DT=[1]min, AREA=[1.87](ha), XIMP=[0.68], TIMP=[0.85],
DWF=[0](cms), LOSS=[1]:
1527 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1528 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1529 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[193.391](m), MNI=[0.013], SCI=[0](min),
1530 Continuous simulation parameters:
1531 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1532 *%-----|-----|
1533 ROUTE RESERVOIR NHYDout=["C6-STR"], NHYDin=["C6"], RDT=[1](min),
1534             TABLE of ( OUTFLOW-STORAGE ) values
1535             (cms) - (ha-m)
1536             [ 0.000 , 0.000 ]
1537             [ 0.026 , 0.029 ]
1538             [ 0.054 , 0.038 ]
1539             [ 0.075 , 0.044 ]
1540             [ 0.093 , 0.052 ]
1541             [ 0.120 , 0.056 ]
1542             [ 0.138 , 0.061 ]
1543             [ -1 , -1 ] (max twenty pts)
1544             NHYDovf=["C6-OVF"]
1545 *%-----|-----|
1546 CONTINUOUS STANDHYD NHYD=["C7"], DT=[1]min, AREA=[1.62](ha), XIMP=[0.68], TIMP=[0.85],
DWF=[0](cms), LOSS=[1]:
1547 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1548 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1549 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[180.000](m), MNI=[0.013], SCI=[0](min),
1550 Continuous simulation parameters:
1551 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1552 *%-----|-----|
1553 ROUTE RESERVOIR NHYDout=["C7-STR"], NHYDin=["C7"], RDT=[1](min),
1554             TABLE of ( OUTFLOW-STORAGE ) values
1555             (cms) - (ha-m)
1556             [ 0.000 , 0.000 ]
1557             [ 0.023 , 0.025 ]
1558             [ 0.047 , 0.033 ]

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1559         [ 0.065 , 0.038 ]
1560         [ 0.081 , 0.045 ]
1561         [ 0.104 , 0.048 ]
1562         [ 0.120 , 0.053 ]
1563         [ -1 , -1 ] (max twenty pts)
1564         NHYDovf=["C7-OVF"]
1565 *%-----|-----|
1566 CONTINUOUS STANDHYD NHYD=["ST-6"], DT=[1]min, AREA=[0.41](ha),XIMP=[0.46], TIMP=[0.57],
DWF=[0](cms), LOSS=[1]:
1567         Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1568         Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1569         Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[90.554](m),
MNI=[0.013], SCI=[0](min),
1570         Continuous simulation parameters:
1571         IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1572 *%-----|-----|
1573 ROUTE RESERVOIR NHYDout=["ST6STR"], NHYDin=["ST-6"], RDT=[1](min),
1574         TABLE of ( OUTFLOW-STORAGE ) values
1575         (cms) - (ha-m)
1576         [ 0.000 , 0.0000 ]
1577         [ 0.036 , 0.0010 ]
1578         [ 0.037 , 0.0058 ]
1579         [ -1 , -1 ] (max twenty pts)
1580         NHYDovf=["ST6OVF"]
1581 *%-----|-----|
1582 *ANALYSIS POINT 5 - TOTAL FLOW AT OUTLET OF STREET 6
1583 *%-----|-----|
1584 ADD HYD NHYDsum=["PT5ST6"], NHYDs to
add=["PT4ST5"+"C6-STR"+"C6-OVF"+"C7-STR"+"C7-OVF"+"ST6STR"+"ST6OVF"]
1585 *%-----|-----|
1586 *ROUTE FLOW through O'Keefe Drain 4
1587 ROUTE CHANNEL NHYDout=["DRAIN4"], NHYDin=["PT5ST6"], RDT=[1](min),
1588         CHLGTH=[324]{m}, CHSLOPE=[.10](%), FPSLOPE=[.10](%),
1589         SECNUM=[1], NSEG=[3]
1590         ( SEGROUGH, SEGDIST (m))=[0.07,12.00 -0.043,18.00 0.07,30.00] NSEG
times
1591         ( DISTANCE (m), ELEVATION (m))=[0.00, 2.00]
1592         (2.00, 1.20)
1593         (12.00, 1.00)
1594         (14.00, 0.00)
1595         (16.00, 0.00)
1596         (18.00, 1.00)
1597         (28.00, 1.20)
1598         (30.00, 2.00)
1599 *%-----|-----|
1600 CONTINUOUS NASHYD NHYD=["D4"], DT=[1]min, AREA=[1.73](ha), DWF=[0](cms), CN/C=[88],
IA=[8.4](mm),
1601         N=[3], TP=[0.60]hrs,
1602         Continuous simulation parameters:
1603         IaRECper=[4](hrs),
1604         SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1605         InterEventTime=[12](hrs)
1606         Baseflow simulation parameters:
1607         BaseFlowOption=[1] ,
1608         InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1609         VHydCond=[0.055](mm/hr), END=-1
1610 *%-----|-----|
1611 CONTINUOUS STANDHYD NHYD=["Area-B"], DT=[1]min, AREA=[24.04](ha), XIMP=[0.62],
TIMP=[0.77], DWF=[0](cms), LOSS=[1]:
1612         Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1613         Pervious areas: IAper=[4.67](mm), SLPP=[1.4](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),

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1614      Impervious areas: IAimp=[1.57](mm), SLPI=[1.4](%),
1615      LGI=[693.397](m), MNI=[0.013], SCI=[0](min),
1616      Continuous simulation parameters:
1617      IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
1618      END=-1
1619  *%-----|-----|
1620  ROUTE RESERVOIR      NHYDout=["SWMF-B"], NHYDin=["Area-B"], RDT=[1](min),
1621      TABLE of ( OUTFLOW-STORAGE ) values
1622      (cms) - (ha-m)
1623      [ 0.000 , 0.000 ]
1624      [ 0.025 , 0.090 ]
1625      [ 0.175 , 0.510 ]
1626      [ 0.350 , 0.710 ]
1627      [ 0.495 , 0.820 ]
1628      [ 0.648 , 0.980 ]
1629      [ 0.965 , 1.045 ]
1630      [ 1.072 , 1.140 ]
1631      [ -1 , -1 ] (max twenty pts)
1632      NHYDovf=["SWMBOVF"]
1633  *%-----|-----|
1634  ADD HYD              NHYDsum=["D4-EX"], NHYDs to add=["DRAIN4"+"D4"+"SWMF-B"+"SWMBOVF"]
1635  *%-----|-----|
1636  *ROUTE FLOW THROUGH O'Keefe Drain 5
1637  * JFSA: Nov. 2020, added en points to close X-Section
1638  ROUTE CHANNEL      NHYDout=["DRAIN5"], NHYDin=["D4-EX"], RDT=[1](min),
1639      CHLGTH=[413.0](m), CHSLOPE=[0.16](%), FPSLOPE=[0.16](%),
1640      SECNUM=[1], NSEG=[3]
1641      ( SEGROUGH, SEGDIST (m))=[0.043,12.29 -0.033,17.97
1642      0.043,32.84] NSEG times
1643      ( DISTANCE (m), ELEVATION (m))=(-0.01, 2.50)
1644      [0.00, 1.41]
1645      [6.13, 0.97]
1646      [12.29, 0.89]
1647      [15.71, 0.00]
1648      [17.97, 0.39]
1649      [23.04, 0.35]
1650      [32.83, 0.96]
1651      (32.84, 2.50)
1652  *%-----|-----|
1653  CONTINUOUS NASHYD   NHYD=["D5"], DT=[1]min, AREA=[1.90](ha),
1654      DWF=[0](cms), CN/C=[86], IA=[8.7](mm), N=[3], TP=[0.69]hrs,
1655      Continuous simulation parameters:
1656      IaREcper=[4](hrs),
1657      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1658      InterEventTime=[12](hrs)
1659      Baseflow simulation parameters:
1660      BaseFlowOption=[1] ,
1661      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1662      VHydCond=[0.055](mm/hr), END=-1
1663  *%-----|-----|
1664  *EXTERNAL FLOWS SOUTHEAST OF THE SITE NORTH OF MCKENNA CASEY DR.
1665  CONTINUOUS NASHYD   NHYD=["O-13SDF"], DT=[1]min, AREA=[9.74](ha),
1666      DWF=[0](cms), CN/C=[81], IA=[4.0](mm), N=[3], TP=[.43]hrs,
1667      Continuous simulation parameters:
1668      IaREcper=[4](hrs),
1669      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1670      InterEventTime=[12](hrs)
1671      Baseflow simulation parameters:
1672      BaseFlowOption=[1] ,
1673      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1674      VHydCond=[0.055](mm/hr), END=-1
1675  *%-----|-----|
1676  *SNOW DISPOSAL FACILITY
1677  *PARAMETERS BASED ON ROBINSON 2006 MODEL
1678  ROUTE RESERVOIR      NHYDout=["SDF"], NHYDin=["O-13SDF"], RDT=[1](min),
1679      TABLE of ( OUTFLOW-STORAGE ) values

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1678             (cms) - (ha-m)
1679             [0.000,0.000]
1680             [0.150,0.600]
1681             (0.200,1.500)
1682             [ -1 , -1 ] (max twenty pts)
1683             NHYDovf=["OVFSDF"]
1684 *%-----|-----|
1685 *ANALYSIS POINT 6 - McKenna Casey Dr.
1686 *%-----|-----|
1687 ADD HYD      NHYDsum=["PT6MC"], NHYDs to add=["DRAIN5"+"D5"+"SDF"]
1688 *%-----|-----|
1689 CONTINUOUS NASHYD NHYD=["O-15"], DT=[1]min, AREA=[10.67](ha),
1690 DWF=[0](cms), CN/C=[82], IA=[7.5](mm), N=[3], TP=[0.30]hrs,
1691 Continuous simulation parameters:
1692 IaRECper=[4](hrs),
1693 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1694 InterEventTime=[12](hrs)
1695 Baseflow simulation parameters:
1696 BaseFlowOption=[1] ,
1697 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1698 VHydCond=[0.055](mm/hr), END=-1
1699 *%-----|-----|
1700 *TOTAL FLOW NORTH OF McKENNA CASEY DR.
1701 ADD HYD      NHYDsum=["M-C"], NHYDs to add=["PT6MC"+"O-15"]
1702 *%-----|-----|
1703 *ROUTE FLOW THROUGH AREA O-14
1704 * JFSA: Nov. 2020, added end points to close X-section
1705 ROUTE CHANNEL NHYDout=["O-14Ch"], NHYDin=["M-C"], RDT=[1](min),
1706 CHLGTH=[845.3](m), CHSLOPE=[0.10](%), FPSLOPE=[0.10](%),
1707 SECNUM=[1], NSEG=[3]
1708 ( SEGROUGH, SEGDIST (m))=[0.06,15.00 -0.033,18.04 0.06,31.85] NSEG
times
1709 ( DISTANCE (m), ELEVATION (m))=[-0.01, 2.5
1710 (0.00, 1.53]
1711 (5.56, 1.47)
1712 (9.21, 1.45)
1713 (12.45, 1.53)
1714 (13.70, 1.50)
1715 (15.00, 0.69)
1716 (15.34, 0.00)
1717 (16.51, 0.05)
1718 (17.30, 0.17)
1719 (18.04, 0.74)
1720 (19.29, 1.32)
1721 (22.73, 1.47)
1722 (31.84, 1.41)
1723 (31.85, 2.50)
1724 *%-----|-----|
1725 *% -Change O-14 from NASHYD to STANDHYD, name it "S-1-Okeefe" and add it to S-1
subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
1726 *% -JFSA 2021-02-16, add detailed subcatchment drainage area for each subcatchment
in Corrigan sub-catchment. After adding part of O-14 to S_1 sub-catchment so O-14
becomes 5 ha instead of 30.02 ha and TP becomes 0.133 (5*0.8/30.02) instead of 0.8
1727 CONTINUOUS NASHYD NHYD=["O-14"], DT=[1]min, AREA=[5](ha),
1728 DWF=[0](cms), CN/C=[82], IA=[7.5](mm), N=[3], TP=[0.133]hrs,
1729 Continuous simulation parameters:
1730 IaRECper=[4](hrs),
1731 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1732 InterEventTime=[12](hrs)
1733 Baseflow simulation parameters:
1734 BaseFlowOption=[1] ,
1735 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1736 VHydCond=[0.055](mm/hr), END=-1
1737 *
1738 *%-----|-----|
1739 *ANALYSIS POINT 7 - JOCK RIVER

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1740 * 2020-12-01 To Foster Drain
1741 * 2020-12-01 replace ("PT7JR") by ("OKEEFE")
1742 *%-----|-----
1743 ADD HYD          NHYDsum=["OKEEFE"], NHYDs to add=["O-14Ch"+"O-14"]
1744 *%-----|-----
1745 *CONTINUOUS STANDHYD NHYD=["OKEEFE"], DT=[1](min), AREA=[448](ha),
1746 *                XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
1747 *                SCS curve number CN=[77],
1748 *                Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
1749 *                LGP=[40](m), MNP=[0.25], SCP=[0](min),
1750 *                Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
1751 *                LGI=[1728](m), MNI=[0.013], SCI=[0](min),
1752 *                Continuous simulation parameters:
1753 *                IaRECper=[4](hrs), IaRECimp=[4](hrs),
1754 *                SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1755 *                InterEventTime=[18](hrs), END=-1
1756 *#*****
1757 *#      Okeefe Pond
1758 *#      - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1759 *#      and a ratio of the catchment area to the West Clarke pond rating curve
1760 *#      from the MSS for the next coordinates
1761 *#*****
1762 *ROUTE RESERVOIR  NHYDout=["P_OKE"], NHYDin=["OKEEFE"],
1763 *                RDT=[1](min),
1764 *                TABLE of ( OUTFLOW-STORAGE ) values
1765 *                (cms) - (ha-m)
1766 *                [  0.0 ,  0.0]
1767 *                [ 14.13 , 13.0]
1768 *                [  -1 ,  -1 ] (maximum one hundred pairs of points)
1769 *                NHYDovf=["ok-OVF"],
1770 *%-----|-----
1771 * -JFSA 2021-02-25 "S-1-D2" and "S-1-D3" are part of S-1 sub-catchment. They are
1772 * moved to drain before station 6215 on Jock River
1773 *CONTINUOUS STANDHYD NHYD=["S-1-D2"], DT=[1](min), AREA=[18.67](ha), XIMP=[0.65],
1774 *                TIMP=[0.65], DWF=[0](cms),
1775 *                LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
1776 *                IAper=[4.67](mm), SLPP=[2.0](%),
1777 *                LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
1778 *                IAimp=[1.57](mm), SLPI=[0.75](%),
1779 *                LGI=[352.798](m), MNI=[0.013], SCI=[0](min),
1780 *                Continuous simulation parameters:
1781 *                IaRECper=[4](hrs), IaRECimp=[4](hrs),
1782 *                SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1783 *                InterEventTime=[12](hrs), END=-1
1784 *%-----|-----
1785 *CONTINUOUS NASHYD  NHYD=["S-1-D2"], DT=[1]min, AREA=[18.67](ha),
1786 *                DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
1787 *                N=[3], TP=[1.120]hrs,
1788 *                Continuous simulation parameters:
1789 *                IaRECper=[4](hrs),
1790 *                SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1791 *                InterEventTime=[12](hrs)
1792 *                Baseflow simulation parameters:
1793 *                BaseFlowOption=[1] ,
1794 *                InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1795 *                VHydCond=[0.055](mm/hr), END=-1
1796 *%-----|-----
1797 *COMPUTE DUALHYD   NHYDin=["S-1-D2"], CINLET=[2.062](cms), NINLET=[1],
1798 *                MajNHYD=["S-1-D2J"]
1799 *                MinNHYD=["S-1-D2N"]
1800 *                TMJSTO=[9999999](cu-m)
1801 *%-----|-----
1802 *ADD HYD           NHYDsum=["S-1-D2S"], NHYDs to add=["S-1-D2J"+"S-1-D2N"]
1803 *%-----|-----
1804 *ROUTE RESERVOIR  NHYDout=["S-1-D2R"] ,NHYDin=["S-1-D2S"] ,

```



```

1801 *           RDT=[1](min),
1802 *           TABLE of ( OUTFLOW-STORAGE ) values
1803 *                 (cms) - (ha-m)
1804 *                 [ 0.0      , 0.0 ]
1805 *                 [ 0.2231, 0.7445 ]
1806 *                 [   -1   ,  -1   ] (max twenty pts)
1807 *           NHYDovf=["S-1-D2Rovf"]
1808 *%-----|-----
1809 CONTINUOUS STANDHYD NHYD=["S-1-D3"], DT=[1](min), AREA=[6.79](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
1810 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
IAper=[4.67](mm), SLPP=[2.0](%),
1811 LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
1812 LGI=[212.760](m), MNI=[0.013], SCI=[0](min),
1813 Continuous simulation parameters:
1814 IaREcper=[4](hrs), IaREcimp=[4](hrs),
1815 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1816 InterEventTime=[12](hrs), END=-1
1817 *%-----|-----
1818 *CONTINUOUS NASHYD NHYD=["S-1-D3"], DT=[1]min, AREA=[6.79](ha),
1819 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
1820 * N=[3], TP=[1.281]hrs,
1821 * Continuous simulation parameters:
1822 * IaREcper=[4](hrs),
1823 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1824 * InterEventTime=[12](hrs)
1825 * Baseflow simulation parameters:
1826 * BaseFlowOption=[1] ,
1827 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1828 * VHydCond=[0.055](mm/hr), END=-1
1829 *%-----|-----
1830 *COMPUTE DUALHYD NHYDin=["S-1-D3"], CINLET=[0.719](cms), NINLET=[1],
1831 * MajNHYD=["S-1-D3J"]
1832 * MinNHYD=["S-1-D3N"]
1833 * TMJSTO=[9999999](cu-m)
1834 *%-----|-----
1835 *ADD HYD NHYDsum=["S-1-D3S"], NHYDs to add=["S-1-D3J"+"S-1-D3N"]
1836 *%-----|-----
1837 *ROUTE RESERVOIR NHYDout=["S-1-D3R"] ,NHYDin=["S-1-D3S"] ,
1838 * RDT=[1](min),
1839 *           TABLE of ( OUTFLOW-STORAGE ) values
1840 *                 (cms) - (ha-m)
1841 *                 [ 0.0      , 0.0 ]
1842 *                 [ 0.0811, 0.2708 ]
1843 *                 [   -1   ,  -1   ] (max twenty pts)
1844 *           NHYDovf=["S-1-D3Rovf"]
1845 *%-----|-----
1846 ADD HYD NHYDsum=["SN_OK"], NHYDs to add=["N_OK"+"OKEEFE"+"S-1-D2"+"S-1-D3"]
1847 *%-----|-----
1848 SAVE HYD NHYD=["SN_OK"], # OF PCYCLES=[-1], ICASEsh=[1]
1849 HYD_COMMENT=["Total Flows at Okeefe Drain"]
1850 *%-----|-----
1851 *#
1852 *# Hydrograph from Node Okeefe routed to Node at Foster Drain
1853 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
1854 *#
1855 ROUTE CHANNEL NHYDout=["N_FO"] ,NHYDin=["SN_OK"] ,
1856 RDT=[1](min),
1857 CHLGTH=[1183](m), CHSLOPE=[0.0761](%),
1858 FPSLOPE=[0.0761](%),
1859 SECNUM=[1.0], NSEG=[3]
1860 ( SEGROUGH, SEGDIST (m))=
1861 [0.050,-33.89
1862 -0.035,31.59
1863 0.050,34.41] NSEG times

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```

1864      ( DISTANCE (m), ELEVATION (m))=
1865      [-794.18, 91.00]
1866      [-775.41, 91.50]
1867      [-702.63, 91.50]
1868      [-546.19, 91.50]
1869      [-529.54, 91.50]
1870      [-323.44, 91.00]
1871      [-320.71, 91.00]
1872      [-183.59, 91.00]
1873      [-182.54, 90.50]
1874      [-181.36, 90.00]
1875      [-177.37, 90.00]
1876      [-87.70, 90.00]
1877      [-33.89, 90.00]
1878      [-18.52, 86.88]
1879      [0.00,85.20]
1880      [16.20, 86.83]
1881      [31.59, 90.00]
1882      [33.03, 90.50]
1883      [34.41, 91.00]
1884      *%-----|-----|
1885      *#*****|
1886      *#      Catchment FOSTER
1887      *#      - To Foster ditch (north of the Jock)
1888      *#      - Partially developed (medium density); remaining agricultural
1889      *#      - 2020-12-01 JFSA Foster area is 332 as per Foster SWMF Environmental Study
1890      *#      - 2020-12-01 decrease Foster drainage area from (373 HA) to (307.98 HA) after
1891      *#      - 2021-02-12 update Foster area to 325.44 ha as measured from QGIS
1892      *#*****|
1893      CONTINUOUS STANDHYD NHYD=["FOSTER"], DT=[1]min, AREA=[325.44](ha),
1894      XIMP=[0.55], TIMP=[0.55], DWF=[0](cms), LOSS=[2],
1895      SCS curve number CN=[74],
1896      Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
1897      LGP=[40](m), MNP=[0.25], SCP=[0](min),
1898      Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
1899      LGI=[1472.956](m), MNI=[0.013], SCI=[0](min),
1900      Continuous simulation parameters:
1901      IaRECper=[4](hrs), IaRECimp=[4](hrs),
1902      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1903      InterEventTime=[18](hrs), END=-1
1904      *#*****|
1905      *#      Foster Pond
1906      *#      - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1907      *#      and a ratio of the catchment area to the West Clarke pond rating curve
1908      *#      from the MSS for the next coordinates
1909      *#*****|
1910      ROUTE RESERVOIR      NHYDout=["P_FOS"], NHYDin=["FOSTER"],
1911      RDT=[1](min),
1912      TABLE of ( OUTFLOW-STORAGE ) values
1913      (cms) - (ha-m)
1914      [ 0.0 , 0.0 ]
1915      [ 10.34 , 10]
1916      [ -1 , -1 ] (max twenty pts)
1917      NHYDovf=["FO-OVF"]
1918      *%-----|-----|
1919      ADD HYD      NHYDsum=["FOSTER-OUT"], NHYDs to add=["P_FOS"+"FO-OVF"]
1920      *%-----|-----|
1921      *#*****|
1922      *      -Brazeau area from P 1800-19 =[71.751], change to 63.59 ha based on GIS measurements
1923      *      -JFSA, 2021-01-19 update "W_CLAR_BRAZ" to 73.29 ha based on GIS measurements
1924      *      -JFSA, 2021-01-22 Brazeau ("MS_P10"+"P10-OVF")brazeau pond discharges directly
1925      to the jock river through a road side ditch on the west side of Borrisokane road
1926      (station 6016)

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1925 CONTINUOUS STANDHYD NHYD=["W_CLAR_BRAZ"], DT=[1]min, AREA=[73.29](ha),
1926 XIMP=[0.6], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
1927 SCS curve number CN=[77],
1928 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
1929 LGP=[40](m), MNP=[0.25], SCP=[0](min),
1930 Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
1931 LGI=[699.00](m), MNI=[0.013], SCI=[0](min),
1932 Continuous simulation parameters:
1933 IaRECper=[4](hrs), IaRECimp=[4](hrs),
1934 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1935 InterEventTime=[18](hrs), END=-1
1936 *%-----|-----
1937 * 2020-12-01 correct pond curve values
1938 ROUTE RESERVOIR NHYDout=["MS_P10"], NHYDin=["W_CLAR_BRAZ"],
1939 RDT=[1](min),
1940 TABLE of ( OUTFLOW-STORAGE ) values
1941 ( cms ) - ( ha-m )
1942 [ 0.0 , 0.0 ]
1943 [ 0.068 , 0.001 ]
1944 [ 0.271 , 0.022 ]
1945 [ 0.379 , 0.051 ]
1946 [ 0.48 , 0.091 ]
1947 [ 0.853 , 0.341 ]
1948 [ 1.005 , 0.61 ]
1949 [ 1.128 , 1.231 ]
1950 [ 1.155 , 1.592 ]
1951 [ 1.194 , 1.876 ]
1952 [ 1.2 , 1.921 ]
1953 [ 1.259 , 2.369 ]
1954 [ 1.3 , 2.665 ]
1955 [ 1.349 , 2.813 ]
1956 [ -1 , -1 ] (max twenty pts)
1957 NHYDovf=["P10-OVF"]
1958 *%-----|-----
1959 * -JFSA 2021-02-26 "S-1-FO-D2" is a part of S-1 sub-catchment. It is moved to drain
before station 980 on Foster Drain
1960 CONTINUOUS STANDHYD NHYD=["S-1-FO-D2"], DT=[1]min, AREA=[4.94](ha),
1961 XIMP=[0.55], TIMP=[0.55], DWF=[0](cms), LOSS=[2],
1962 SCS curve number CN=[74],
1963 Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
1964 LGP=[40](m), MNP=[0.25], SCP=[0](min),
1965 Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
1966 LGI=[181.475](m), MNI=[0.013], SCI=[0](min),
1967 Continuous simulation parameters:
1968 IaRECper=[4](hrs), IaRECimp=[4](hrs),
1969 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1970 InterEventTime=[18](hrs), END=-1
1971 *%-----|-----
1972 *CONTINUOUS NASHYD NHYD=["S-1-FO-D2"], DT=[1]min, AREA=[4.94](ha),
1973 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
1974 * N=[3], TP=[1.10]hrs,
1975 * Continuous simulation parameters:
1976 * IaRECper=[4](hrs),
1977 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1978 * InterEventTime=[12](hrs)
1979 * Baseflow simulation parameters:
1980 * BaseFlowOption=[1] ,
1981 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1982 * VHydCond=[0.055](mm/hr), END=-1
1983 *%-----|-----
1984 *COMPUTE DUALHYD NHYDin=["S-1-FO-D2"], CINLET=[0.508](cms), NINLET=[1],
1985 * MajNHYD=["S-1-FO-D2J"]
1986 * MinNHYD=["S-1-FO-D2N"]
1987 * TMJSTO=[9999999](cu-m)
1988 *%-----|-----
1989 *ADD HYD NHYDsum=["S-1-FO-D2S"], NHYDs to add=["S-1-FO-D2J"+"S-1-FO-D2N"]

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1990  *%-----|-----|
1991  *ROUTE RESERVOIR      NHYDout=["S-1-FO-D2R"] ,NHYDin=["S-1-FO-D2S"] ,
1992  *                      RDT=[1](min),
1993  *                      TABLE of ( OUTFLOW-STORAGE ) values
1994  *                      (cms) - (ha-m)
1995  *                      [ 0.0      , 0.0 ]
1996  *                      [ 0.0590, 0.1970 ]
1997  *                      [   -1   ,  -1   ] (max twenty pts)
1998  *                      NHYDovf=["S-1FOD2ovf"]
1999  *%-----|-----|
2000  ADD HYD                NHYDsum=["980"], NHYDs to add=["FOSTER-OUT"+"S-1-FO-D2"]
2001  *%-----|-----|
2002  SAVE HYD               NHYD=["980"], # OF PCYCLES=[-1], ICASEsh=[1]
2003  HYD_COMMENT=["Total Flows at Station 980 on Foster Drain"]
2004  *%-----|-----|
2005  *#
2006  *# Hydrograph from Node Foster SWM (Station 980)to Node at station 520
2007  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 980
2008  *#
2009  ROUTE CHANNEL          NHYDout=["980-out"] ,NHYDin=["980"] ,
2010  RDT=[1](min),
2011  CHLGTH=[460](m),    CHSLOPE=[0.04348](%),
2012  FPSLOPE=[0.04348](%),
2013  SECNUM=[1.0],      NSEG=[3]
2014  ( SEGROUGH, SEGDIST (m))=
2015  [0.050,45.90
2016  -0.035,53.30
2017  0.050,100] NSEG times
2018  ( DISTANCE (m), ELEVATION (m))=
2019  [0, 91.75 ]
2020  [42.4, 92.18 ]
2021  [43.5, 92.16 ]
2022  [44.1, 92.1 ]
2023  [44.6, 92 ]
2024  [44.8, 91.86 ]
2025  [45.9, 91.04 ]
2026  [46.4, 90.65 ]
2027  [46.8, 90.36 ]
2028  [47.9, 90.32 ]
2029  [48.7, 90.35 ]
2030  [50.7, 90.33 ]
2031  [52.2, 90.38 ]
2032  [52.5, 90.59 ]
2033  [53.3, 91.28 ]
2034  [54, 91.83 ]
2035  [54.3, 92 ]
2036  [54.8, 92.08 ]
2037  [55.4, 92.12 ]
2038  [100, 91.84 ]
2039  *%-----|-----|
2040  * -JFSA 2021-02-26 "S-1-FO-D1" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2041  CONTINUOUS STANDHYD NHYD=["S-1-FO-D1"], DT=[1]min, AREA=[5.11](ha),
2042  XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2043  SCS curve number CN=[74],
2044  Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2045  LGP=[40](m), MNP=[0.25], SCP=[0](min),
2046  Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2047  LGI=[184.572](m), MNI=[0.013], SCI=[0](min),
2048  Continuous simulation parameters:
2049  IaRECper=[4](hrs), IaRECimp=[4](hrs),
2050  SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2051  InterEventTime=[18](hrs), END=-1
2052  *%-----|-----|
2053  *COMPUTE DUALHYD      NHYDin=["S-1-FO-D1"], CINLET=[0.605](cms), NINLET=[1],
2054  *                      MajNHYD=["S-1-FO-D1J"]

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2055 *                               MinNHYD=["S-1-FO-D1N"]
2056 *                               TMJSTO=[9999999](cu-m)
2057 *%-----|-----|
2058 *ADD HYD                               NHYDsum=["S-1-FO-D1S"], NHYDs to add=["S-1-FO-D1N"+"S-1-FO-D1J"]
2059 *%-----|-----|
2060 *ROUTE RESERVOIR                       NHYDout=["S-1-FO-D1R"] ,NHYDin=["S-1-FO-D1S"] ,
2061 *                               RDT=[1](min),
2062 *                               TABLE of ( OUTFLOW-STORAGE ) values
2063 *                               (cms) - (ha-m)
2064 *                               [ 0.0      , 0.0 ]
2065 *                               [ 0.0611, 0.2038 ]
2066 *                               [   -1   ,  -1   ] (max twenty pts)
2067 *                               NHYDovf=["S-1FOD1ovf"]
2068 *%-----|-----|
2069 ADD HYD                               NHYDsum=["520"], NHYDs to add=["980-out"+"S-1-FO-D1"]
2070 *%-----|-----|
2071 SAVE HYD                             NHYD=["520"], # OF PCYCLES=[-1], ICASEsh=[1]
2072                               HYD_COMMENT=["Total Flows at Sation 520 on Foster Drain"]
2073 *%-----|-----|
2074 *# Hydrograph from Node at Station 520 (Foster Drain) to Node at station 6016 (Jock
River)
2075 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 520
2076 *#
2077 ROUTE CHANNEL                       NHYDout=["520-out"] ,NHYDin=["520"] ,
2078                               RDT=[1](min),
2079                               CHLGTH=[860](m), CHSLOPE=[0.5872](%),
2080                               FPSLOPE=[0.5872](%),
2081                               SECNUM=[1.0], NSEG=[3]
2082                               ( SEGROUGH, SEGDIST (m))=
2083                               [0.050,45.90
2084                               -0.035,54.3
2085                               0.050,100.1097] NSEG times
2086                               ( DISTANCE (m), ELEVATION (m))=
2087                               [0, 91.26 ]
2088                               [44.9, 91.46 ]
2089                               [45.1, 91.37 ]
2090                               [45.9, 90.84 ]
2091                               [47, 90.32 ]
2092                               [47.5, 90.22 ]
2093                               [48, 90.17 ]
2094                               [50.7, 90.19 ]
2095                               [51.5, 90.17 ]
2096                               [52.2, 90.13 ]
2097                               [52.7, 90.12 ]
2098                               [53.3, 90.14 ]
2099                               [53.5, 90.31 ]
2100                               [53.9, 90.59 ]
2101                               [54.3, 90.87 ]
2102                               [54.7, 91.04 ]
2103                               [55.3, 91.24 ]
2104                               [55.5, 91.26 ]
2105                               [63.7, 91.37 ]
2106                               [100.1097, 91.43 ]
2107 *%-----|-----|
2108 * -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2109 CONTINUOUS STANDHYD NHYD=["S-1-FO-F-D"], DT=[1]min, AREA=[14.96](ha),
2110                               XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2111                               SCS curve number CN=[74],
2112                               Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2113                               LGP=[40](m), MNP=[0.25], SCP=[0](min),
2114                               Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2115                               LGI=[315.806](m), MNI=[0.013], SCI=[0](min),
2116                               Continuous simulation parameters:
2117                               IaREcper=[4](hrs), IaREcimp=[4](hrs),
2118                               SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),

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2119 InterEventTime=[18](hrs), END=-1
2120 *%-----|-----|
2121 *CONTINUOUS NASHYD NHYD=["S-1-FO-F-D"], DT=[1]min, AREA=[14.96](ha),
2122 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2123 * N=[3], TP=[1.007]hrs,
2124 * Continuous simulation parameters:
2125 * IaRECper=[4](hrs),
2126 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2127 * InterEventTime=[12](hrs)
2128 * Baseflow simulation parameters:
2129 * BaseFlowOption=[1] ,
2130 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2131 * VHydCond=[0.055](mm/hr), END=-1
2132 *%-----|-----|
2133 *COMPUTE DUALHYD NHYDin=["S-1-FO-F-D"], CINLET=[1.749](cms), NINLET=[1],
2134 * MajNHYD=["S-1FO-F-DJ"]
2135 * MinNHYD=["S-1FO-F-DN"]
2136 * TMJSTO=[9999999](cu-m)
2137 *%-----|-----|
2138 *ADD HYD NHYDsum=["S-1FO-F-DS"], NHYDs to add=["S-1FO-F-DJ"+"S-1FO-F-DN"]
2139 *%-----|-----|
2140 *ROUTE RESERVOIR NHYDout=["S-1FO-F-DR"],NHYDin=["S-1FO-F-DS"] ,
2141 * RDT=[1](min),
2142 * TABLE of ( OUTFLOW-STORAGE ) values
2143 * (cms) - (ha-m)
2144 * [ 0.0 , 0.0 ]
2145 * [ 0.1788, 0.5966 ]
2146 * [ -1 , -1 ] (max twenty pts)
2147 * NHYDovf=["S-1FoFDovf"]
2148 *%-----|-----|
2149 * -JFSA 2021-02-26 "S-1-D8" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2150 CONTINUOUS STANDHYD NHYD=["S-1-D8"], DT=[1]min, AREA=[5.27](ha), XIMP=[0.325],
TIMP=[0.65], DWF=[0](cms), LOSS=[1]:
2151 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
2152 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
2153 Impervious areas: IAimp=[0.785](mm), SLPI=[0.75](%),
LGI=[187.439](m), MNI=[0.013], SCI=[0](min),
2154 Continuous simulation parameters:
2155 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
2156 *%-----|-----|
2157 *CONTINUOUS NASHYD NHYD=["S-1-D8"], DT=[1]min, AREA=[5.27](ha),
2158 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2159 * N=[3], TP=[1.10]hrs,
2160 * Continuous simulation parameters:
2161 * IaRECper=[4](hrs),
2162 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2163 * InterEventTime=[12](hrs)
2164 * Baseflow simulation parameters:
2165 * BaseFlowOption=[1] ,
2166 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2167 * VHydCond=[0.055](mm/hr), END=-1
2168 *%-----|-----|
2169 *COMPUTE DUALHYD NHYDin=["S-1-D8"], CINLET=[2.279](cms), NINLET=[1],
2170 * MajNHYD=["S-1-D8J"]
2171 * MinNHYD=["S-1-D8N"]
2172 * TMJSTO=[9999999](cu-m)
2173 *%-----|-----|
2174 *ADD HYD NHYDsum=["S-1-D8S"], NHYDs to add=["S-1-D8J"+"S-1-D8N"]
2175 *%-----|-----|
2176 *ADD HYD NHYDsum=["S-1-D"], NHYDs to add=["S-1-Okeefe"+"S-1"+"S-1-Post"]
2177 *%-----|-----|
2178 *COMPUTE DUALHYD NHYDin=["S-1-D"], CINLET=[11.616](cms), NINLET=[1],

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2179 *           MajNHYD=["S-1-D-MJ"]
2180 *           MinNHYD=["S-1-D-MN"]
2181 *           TMJSTO=[5974](cu-m)
2182 *%-----|-----|
2183 *ADD HYD           NHYDsum=["S-1-DEV"], NHYDs to add=["S-1-D-MJ"+"S-1-D-MN"]
2184 *%-----|-----|
2185 *ROUTE RESERVOIR  NHYDout=["S-1-D8R"], NHYDin=["S-1-D8S"],
2186 *           RDT=[1](min),
2187 *           TABLE of ( OUTFLOW-STORAGE ) values
2188 *                   (cms) - (ha-m)
2189 *                   [ 0.0      , 0.0 ]
2190 *                   [ 0.0630, 0.2102 ]
2191 *                   [   -1   ,  -1   ] (max twenty pts)
2192 *           NHYDovf=["S-1-D8Rovf"]
2193 *%-----|-----|
2194 *   -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2195 CONTINUOUS NASHYD NHYD=["S-1-A"], DT=[1]min, AREA=[75.88](ha),
2196 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2197 N=[3], TP=[0.619]hrs,
2198 Continuous simulation parameters:
2199 IaREcper=[4](hrs),
2200 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2201 InterEventTime=[12](hrs)
2202 Baseflow simulation parameters:
2203 BaseFlowOption=[1],
2204 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2205 VHydCond=[0.055](mm/hr), END=-1
2206 *%-----|-----|
2207 *   -JFSA, 2021-01-22 "W_CLAR_UNDE" (west of Clarke sub-catchment) discharges
directly to the jock river through a road side ditch on the west side of Borrisokane
road (station 6016)
2208 CONTINUOUS NASHYD NHYD=["W_CLAR_UNDE"], DT=[1]min, AREA=[35.65](ha),
2209 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2210 N=[3], TP=[1.10]hrs,
2211 Continuous simulation parameters:
2212 IaREcper=[4](hrs),
2213 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2214 InterEventTime=[12](hrs)
2215 Baseflow simulation parameters:
2216 BaseFlowOption=[1],
2217 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2218 VHydCond=[0.055](mm/hr), END=-1
2219 *%-----|-----|
2220 ADD HYD           NHYDsum=["SN_FO"], NHYDs to
add=["N_FO"+"520-out"+"MS_P10"+"P10-OVF"+"W_CLAR_UNDE"+"S-1-FO-F-D"+"S-1-D8"+"S-1-A"]
2221 *%-----|-----|
2222 SAVE HYD         NHYD=["SN_FO"], # OF PCYCLES=[-1], ICASEsh=[1]
2223 HYD_COMMENT=["Total Flows at Foster Drain"]
2224 *%-----|-----|
2225 *# Hydrograph from Node Foster routed to Node at Cedarview Road
2226 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6016
2227 *#
2228 ROUTE CHANNEL   NHYDout=["N_CE"], NHYDin=["SN_FO"],
2229 RDT=[1](min),
2230 CHLGTH=[159](m), CHSLOPE=[0.0818](%),
2231 FPSLOPE=[0.0818](%),
2232 SECNUM=[1.0], NSEG=[3]
2233 ( SEGROUGH, SEGDIST (m))=
2234 [0.050,-15.46
2235 -0.035,26.55
2236 0.050,116.76] NSEG times
2237 ( DISTANCE (m), ELEVATION (m))=
2238 [-645.23, 91.50]
2239 [-391.20, 91.50]
2240 [-91.00, 91.50]

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2241          [-85.52, 91.50]
2242          [-15.46, 89.40]
2243          [-9.79, 89.31]
2244          [-3.22, 86.24]
2245          [3.22, 85.07]
2246          [10.96, 85.79]
2247          [16.44, 86.49]
2248          [26.55, 89.45]
2249          [29.03, 90.27]
2250          [35.76, 90.67]
2251          [36.67, 91.00]
2252          [108.08, 91.00]
2253          [109.82, 90.50]
2254          [112.04, 90.50]
2255          [114.62, 91.00]
2256          [116.76, 91.50]
2257  *%-----|-----|
2258  *#*****|*****|
2259  *#      Catchment S-1
2260  *#      - To Jock River (north and south of Jock)
2261  *#      - Primarily agricultural fields; portion of sand quarry
2262  *%-----|-----|
2263  *%      -2020-12-17 "S-1-Undev" and "S-1-Fost" was a part of Foster drain, they are below
the foster pond. Now they are added to S-1 subcatchment based on Project 1474-BCDC,
JFSA, Nov. 2020
2264  *%      -2020-12-17 Change O-14 (it was part of Okeefe drain) to "S-1-Okeefe" and add it
to S-1 subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
2265  *%      -2020-12-17 Add "S-1-BCDC" as NASHYD
2266  *%      -2020-12-17 all other S-1 subcatchment as STANDHYD with DUALHYD and ROUTE RESERVOIR
2267  *%-----|-----|
2268  *#*****|*****|
2269  *      -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2270  *CONTINUOUS NASHYD  NHYD=["S-1-A"], DT=[1]min, AREA=[75.88](ha),
2271  *                    DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2272  *                    N=[3], TP=[0.619]hrs,
2273  *                    Continuous simulation parameters:
2274  *                    IaRECper=[4](hrs),
2275  *                    SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2276  *                    InterEventTime=[12](hrs)
2277  *                    Baseflow simulation parameters:
2278  *                    BaseFlowOption=[1] ,
2279  *                    InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2280  *                    VHydCond=[0.055](mm/hr), END=-1
2281  *%-----|-----|
2282  CONTINUOUS NASHYD  NHYD=["S-1-B"], DT=[1]min, AREA=[55.36](ha),
2283  *                    DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2284  *                    N=[3], TP=[0.451]hrs,
2285  *                    Continuous simulation parameters:
2286  *                    IaRECper=[4](hrs),
2287  *                    SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2288  *                    InterEventTime=[12](hrs)
2289  *                    Baseflow simulation parameters:
2290  *                    BaseFlowOption=[1] ,
2291  *                    InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2292  *                    VHydCond=[0.055](mm/hr), END=-1
2293  *%-----|-----|
2294  *#      - JFSA 2021-02-24 change the name from S-1-BCDC to S-1-A and S-1-B. Change their
TP values based on the new areas compared to the old ones.
2295  *CONTINUOUS NASHYD  NHYD=["S-1-BCDC"], DT=[1]min, AREA=[134.9](ha),
2296  *                    DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2297  *                    N=[3], TP=[1.10]hrs,
2298  *                    Continuous simulation parameters:
2299  *                    IaRECper=[4](hrs),
2300  *                    SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2301  *                    InterEventTime=[12](hrs)

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2302 *           Baseflow simulation parameters:
2303 *           BaseFlowOption=[1] ,
2304 *           InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2305 *           VHydCond=[0.055](mm/hr),   END=-1
2306 *%-----|-----|
2307 *# - JFSA 2021-02-24 "S-1-BCDC-1" and "S-1-BCDC-2" are not existing anymore.
      "S-1-BCDC-1" is part of "S-1-FO-D2" and "S-1-BCDC-2" is part of "S-1-D2" and "S-1-D3"
2308 *CONTINUOUS NASHYD  NHYD=["S-1-BCDC-1"], DT=[1]min, AREA=[0.3](ha),
2309 *           DWF=[0](cms), CN/C=[77],   IA=[4.67](mm),
2310 *           N=[3], TP=[1.10]hrs,
2311 *           Continuous simulation parameters:
2312 *           IaRECper=[4](hrs),
2313 *           SMIN=[-1](mm),   SMAX=[-1](mm), SK=[0.010]/(mm),
2314 *           InterEventTime=[12](hrs)
2315 *           Baseflow simulation parameters:
2316 *           BaseFlowOption=[1] ,
2317 *           InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2318 *           VHydCond=[0.055](mm/hr),   END=-1
2319 *%-----|-----|
2320 *CONTINUOUS NASHYD  NHYD=["S-1-BCDC-2"], DT=[1]min, AREA=[1.3](ha),
2321 *           DWF=[0](cms), CN/C=[77],   IA=[4.67](mm),
2322 *           N=[3], TP=[1.10]hrs,
2323 *           Continuous simulation parameters:
2324 *           IaRECper=[4](hrs),
2325 *           SMIN=[-1](mm),   SMAX=[-1](mm), SK=[0.010]/(mm),
2326 *           InterEventTime=[12](hrs)
2327 *           Baseflow simulation parameters:
2328 *           BaseFlowOption=[1] ,
2329 *           InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2330 *           VHydCond=[0.055](mm/hr),   END=-1
2331 *%-----|-----|
2332 *# - JFSA 2021-01-19, after adding Greenbank pond, "S-1-BCDC-3" is not existing
      anymore
2333 *CONTINUOUS NASHYD  NHYD=["S-1-BCDC-3"], DT=[1]min, AREA=[3.9](ha),
2334 *           DWF=[0](cms), CN/C=[77],   IA=[4.67](mm),
2335 *           N=[3], TP=[1.10]hrs,
2336 *           Continuous simulation parameters:
2337 *           IaRECper=[4](hrs),
2338 *           SMIN=[-1](mm),   SMAX=[-1](mm), SK=[0.010]/(mm),
2339 *           InterEventTime=[12](hrs)
2340 *           Baseflow simulation parameters:
2341 *           BaseFlowOption=[1] ,
2342 *           InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2343 *           VHydCond=[0.055](mm/hr),   END=-1
2344 *%-----|-----|
2345 * -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
      before station 7245 on Jock River
2346 *CONTINUOUS STANDHYD NHYD=["S-1-Okeefe"], DT=[1](min), AREA=[44.93](ha), XIMP=[0.65],
      TIMP=[0.65], DWF=[0](cms),
2347 *           LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
      IAper=[4.67](mm), SLPP=[2.0](%),
2348 *           LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
      IAimp=[1.57](mm), SLPI=[0.75](%),
2349 *           LGI=[547.296](m), MNI=[0.013], SCI=[0](min),
2350 *           Continuous simulation parameters:
2351 *           IaRECper=[4](hrs), IaRECimp=[4](hrs),
2352 *           SMIN=[-1](mm),   SMAX=[-1](mm), SK=[0.010]/(mm),
2353 *           InterEventTime=[12](hrs),   END=-1
2354 *%-----|-----|
2355 *COMPUTE DUALHYD  NHYDin=["S-1-Okeefe"], CINLET=[4.796](cms), NINLET=[1],
2356 *           MajNHYD=["S-1-OkMJ"]
2357 *           MinNHYD=["S-1-OkMN"]
2358 *           TMJSTO=[9999999](cu-m)
2359 *%-----|-----|
2360 *ADD HYD  NHYDsum=["S-1-OkS"], NHYDs to add=["S-1-OkMJ"+"S-1-OkMN"]
2361 *%-----|-----|

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2362 *ROUTE RESERVOIR      NHYDout=["S-1-OksR" ] ,NHYDin=["S-1-Oks" ] ,
2363 *                      RDT=[1](min),
2364 *                      TABLE of ( OUTFLOW-STORAGE ) values
2365 *                      (cms) - (ha-m)
2366 *                      [ 0.0      , 0.0 ]
2367 *                      [ 0.5370, 1.7917 ]
2368 *                      [   -1   ,  -1   ] (max twenty pts)
2369 *                      NHYDovf=["S-1-OkSovf" ]
2370 *%-----|-----|
2371 *CONTINUOUS NASHYD     NHYD=["S-1-Okeefe"], DT=[1]min, AREA=[44.93](ha),
2372 *                      DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2373 *                      N=[3], TP=[1.049]hrs,
2374 *                      Continuous simulation parameters:
2375 *                      IaRECper=[4](hrs),
2376 *                      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2377 *                      InterEventTime=[12](hrs)
2378 *                      Baseflow simulation parameters:
2379 *                      BaseFlowOption=[1] ,
2380 *                      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2381 *                      VHydCond=[0.055](mm/hr), END=-1
2382 *%-----|-----|
2383 * -JFSA 2021-02-26 "S-1-FO-D1" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2384 *CONTINUOUS STANDHYD NHYD=["S-1-FO-D1"], DT=[1]min, AREA=[5.11](ha),
2385 *                      XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2386 *                      SCS curve number CN=[74],
2387 *                      Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2388 *                      LGP=[40](m), MNP=[0.25], SCP=[0](min),
2389 *                      Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2390 *                      LGI=[184.572](m), MNI=[0.013], SCI=[0](min),
2391 *                      Continuous simulation parameters:
2392 *                      IaRECper=[4](hrs), IaRECimp=[4](hrs),
2393 *                      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2394 *                      InterEventTime=[18](hrs), END=-1
2395 *%-----|-----|
2396 *COMPUTE DUALHYD      NHYDin=["S-1-FO-D1"], CINLET=[0.605](cms), NINLET=[1],
2397 *                      MajNHYD=["S-1-FO-D1J"]
2398 *                      MinNHYD=["S-1-FO-D1N"]
2399 *                      TMJSTO=[9999999](cu-m)
2400 *%-----|-----|
2401 *ADD HYD               NHYDsum=["S-1-FO-D1S"], NHYDs to add=["S-1-FO-D1N"+"S-1-FO-D1J"]
2402 *%-----|-----|
2403 *ROUTE RESERVOIR      NHYDout=["S-1-FO-D1R" ] ,NHYDin=["S-1-FO-D1S" ] ,
2404 *                      RDT=[1](min),
2405 *                      TABLE of ( OUTFLOW-STORAGE ) values
2406 *                      (cms) - (ha-m)
2407 *                      [ 0.0      , 0.0 ]
2408 *                      [ 0.0611, 0.2038 ]
2409 *                      [   -1   ,  -1   ] (max twenty pts)
2410 *                      NHYDovf=["S-1FOD1ovf" ]
2411 *%-----|-----|
2412 *CONTINUOUS NASHYD     NHYD=["S-1-FO-D1"], DT=[1]min, AREA=[5.11](ha),
2413 *                      DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2414 *                      N=[3], TP=[1.10]hrs,
2415 *                      Continuous simulation parameters:
2416 *                      IaRECper=[4](hrs),
2417 *                      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2418 *                      InterEventTime=[12](hrs)
2419 *                      Baseflow simulation parameters:
2420 *                      BaseFlowOption=[1] ,
2421 *                      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2422 *                      VHydCond=[0.055](mm/hr), END=-1
2423 *%-----|-----|
2424 * -JFSA 2021-02-26 "S-1-FO-D2" is a part of S-1 sub-catchment. It is moved to drain
before station 980 on Foster Drain
2425 *CONTINUOUS STANDHYD NHYD=["S-1-FO-D2"], DT=[1]min, AREA=[4.94](ha),

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2426 * XIMP=[0.55], TIMP=[0.55], DWF=[0](cms), LOSS=[2],
2427 * SCS curve number CN=[74],
2428 * Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2429 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
2430 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2431 * LGI=[181.475](m), MNI=[0.013], SCI=[0](min),
2432 * Continuous simulation parameters:
2433 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
2434 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2435 * InterEventTime=[18](hrs), END=-1
2436 *%-----|-----
2437 *CONTINUOUS NASHYD NHYD=["S-1-FO-D2"], DT=[1]min, AREA=[4.94](ha),
2438 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2439 * N=[3], TP=[1.10]hrs,
2440 * Continuous simulation parameters:
2441 * IaRECper=[4](hrs),
2442 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2443 * InterEventTime=[12](hrs)
2444 * Baseflow simulation parameters:
2445 * BaseFlowOption=[1] ,
2446 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2447 * VHydCond=[0.055](mm/hr), END=-1
2448 *%-----|-----
2449 *COMPUTE DUALHYD NHYDin=["S-1-FO-D2"], CINLET=[0.508](cms), NINLET=[1],
2450 * MaJNHYD=["S-1-FO-D2J"]
2451 * MinNHYD=["S-1-FO-D2N"]
2452 * TMJSTO=[9999999](cu-m)
2453 *%-----|-----
2454 *ADD HYD NHYDsum=["S-1-FO-D2S"], NHYDs to add=["S-1-FO-D2J"+"S-1-FO-D2N"]
2455 *%-----|-----
2456 *ROUTE RESERVOIR NHYDout=["S-1-FO-D2R"],NHYDin=["S-1-FO-D2S"] ,
2457 * RDT=[1](min),
2458 * TABLE of ( OUTFLOW-STORAGE ) values
2459 * (cms) - (ha-m)
2460 * [ 0.0 , 0.0 ]
2461 * [ 0.0590, 0.1970 ]
2462 * [ -1 , -1 ] (max twenty pts)
2463 * NHYDovf=["S-1FOD2ovf"]
2464 *%-----|-----
2465 * -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2466 *CONTINUOUS STANDHYD NHYD=["S-1-FO-F-D"], DT=[1]min, AREA=[14.96](ha),
2467 * XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2468 * SCS curve number CN=[74],
2469 * Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2470 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
2471 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2472 * LGI=[315.806](m), MNI=[0.013], SCI=[0](min),
2473 * Continuous simulation parameters:
2474 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
2475 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2476 * InterEventTime=[18](hrs), END=-1
2477 *%-----|-----
2478 *CONTINUOUS NASHYD NHYD=["S-1-FO-F-D"], DT=[1]min, AREA=[14.96](ha),
2479 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2480 * N=[3], TP=[1.007]hrs,
2481 * Continuous simulation parameters:
2482 * IaRECper=[4](hrs),
2483 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2484 * InterEventTime=[12](hrs)
2485 * Baseflow simulation parameters:
2486 * BaseFlowOption=[1] ,
2487 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2488 * VHydCond=[0.055](mm/hr), END=-1
2489 *%-----|-----
2490 *COMPUTE DUALHYD NHYDin=["S-1-FO-F-D"], CINLET=[1.749](cms), NINLET=[1],

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2491 *           MajNHYD=["S-1FO-F-DJ"]
2492 *           MinNHYD=["S-1FO-F-DN"]
2493 *           TMJSTO=[9999999](cu-m)
2494 *%-----|-----|
2495 *ADD HYD           NHYDsum=["S-1FO-F-DS"], NHYDs to add=["S-1FO-F-DJ"+"S-1FO-F-DN"]
2496 *%-----|-----|
2497 *ROUTE RESERVOIR  NHYDout=["S-1FO-F-DR"], NHYDin=["S-1FO-F-DS"],
2498 *                 RDT=[1](min),
2499 *                 TABLE of ( OUTFLOW-STORAGE ) values
2500 *                 (cms) - (ha-m)
2501 *                 [ 0.0      , 0.0 ]
2502 *                 [ 0.1788, 0.5966 ]
2503 *                 [   -1   ,  -1   ] (max twenty pts)
2504 *                 NHYDovf=["S-1FoFDovf"]
2505 *%-----|-----|
2506 CONTINUOUS STANDHYD NHYD=["S-1-D1"], DT=[1](min), AREA=[21.67](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
2507 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
IAper=[4.67](mm), SLPP=[2.0](%),
2508 LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
2509 LGI=[380.088](m), MNI=[0.013], SCI=[0](min),
2510 Continuous simulation parameters:
2511 IaRECper=[4](hrs), IaRECimp=[4](hrs),
2512 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2513 InterEventTime=[12](hrs), END=-1
2514 *%-----|-----|
2515 *CONTINUOUS NASHYD NHYD=["S-1-D1"], DT=[1]min, AREA=[21.67](ha),
2516 *                 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2517 *                 N=[3], TP=[1.066]hrs,
2518 *                 Continuous simulation parameters:
2519 *                 IaRECper=[4](hrs),
2520 *                 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2521 *                 InterEventTime=[12](hrs)
2522 *                 Baseflow simulation parameters:
2523 *                 BaseFlowOption=[1],
2524 *                 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2525 *                 VHydCond=[0.055](mm/hr), END=-1
2526 *%-----|-----|
2527 *COMPUTE DUALHYD  NHYDin=["S-1-D1"], CINLET=[2.482](cms), NINLET=[1],
2528 *                 MajNHYD=["S-1-D1J"]
2529 *                 MinNHYD=["S-1-D1N"]
2530 *                 TMJSTO=[9999999](cu-m)
2531 *%-----|-----|
2532 *ADD HYD           NHYDsum=["S-1-D1S"], NHYDs to add=["S-1-D1J"+"S-1-D1N"]
2533 *%-----|-----|
2534 *ROUTE RESERVOIR  NHYDout=["S-1-D1R"], NHYDin=["S-1-D1S"],
2535 *                 RDT=[1](min),
2536 *                 TABLE of ( OUTFLOW-STORAGE ) values
2537 *                 (cms) - (ha-m)
2538 *                 [ 0.0      , 0.0 ]
2539 *                 [ 0.2590, 0.8642 ]
2540 *                 [   -1   ,  -1   ] (max twenty pts)
2541 *                 NHYDovf=["S-1-D1Rovf"]
2542 *%-----|-----|
2543 * -JFSA 2021-02-25 "S-1-D2" and "S-1-D3" are part of S-1 sub-catchment. They are
moved to drain before station 6215 on Jock River
2544 *CONTINUOUS STANDHYD NHYD=["S-1-D2"], DT=[1](min), AREA=[18.67](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
2545 *                 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
IAper=[4.67](mm), SLPP=[2.0](%),
2546 *                 LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
2547 *                 LGI=[352.798](m), MNI=[0.013], SCI=[0](min),
2548 *                 Continuous simulation parameters:
2549 *                 IaRECper=[4](hrs), IaRECimp=[4](hrs),

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2550 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2551 * InterEventTime=[12](hrs), END=-1
2552 *%-----|-----
2553 *CONTINUOUS NASHYD NHYD=["S-1-D2"], DT=[1]min, AREA=[18.67](ha),
2554 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2555 * N=[3], TP=[1.120]hrs,
2556 * Continuous simulation parameters:
2557 * IaRECper=[4](hrs),
2558 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2559 * InterEventTime=[12](hrs)
2560 * Baseflow simulation parameters:
2561 * BaseFlowOption=[1] ,
2562 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2563 * VHydCond=[0.055](mm/hr), END=-1
2564 *%-----|-----
2565 *COMPUTE DUALHYD NHYDin=["S-1-D2"], CINLET=[2.062](cms), NINLET=[1],
2566 * MajNHYD=["S-1-D2J"]
2567 * MinNHYD=["S-1-D2N"]
2568 * TMJSTO=[9999999](cu-m)
2569 *%-----|-----
2570 *ADD HYD NHYDsum=["S-1-D2S"], NHYDs to add=["S-1-D2J"+"S-1-D2N"]
2571 *%-----|-----
2572 *ROUTE RESERVOIR NHYDout=["S-1-D2R"],NHYDin=["S-1-D2S"] ,
2573 * RDT=[1](min),
2574 * TABLE of ( OUTFLOW-STORAGE ) values
2575 * (cms) - (ha-m)
2576 * [ 0.0 , 0.0 ]
2577 * [ 0.2231, 0.7445 ]
2578 * [ -1 , -1 ] (max twenty pts)
2579 * NHYDovf=["S-1-D2Rovf"]
2580 *%-----|-----
2581 *CONTINUOUS STANDHYD NHYD=["S-1-D3"], DT=[1](min), AREA=[6.79](ha), XIMP=[0.65],
2582 * TIMP=[0.65], DWF=[0](cms),
2583 * LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
2584 * IAper=[4.67](mm), SLPP=[2.0](%),
2585 * LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
2586 * IAimp=[1.57](mm), SLPI=[0.75](%),
2587 * LGI=[212.760](m), MNI=[0.013], SCI=[0](min),
2588 * Continuous simulation parameters:
2589 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
2590 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2591 * InterEventTime=[12](hrs), END=-1
2592 *%-----|-----
2593 *CONTINUOUS NASHYD NHYD=["S-1-D3"], DT=[1]min, AREA=[6.79](ha),
2594 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2595 * N=[3], TP=[1.281]hrs,
2596 * Continuous simulation parameters:
2597 * IaRECper=[4](hrs),
2598 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2599 * InterEventTime=[12](hrs)
2600 * Baseflow simulation parameters:
2601 * BaseFlowOption=[1] ,
2602 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2603 * VHydCond=[0.055](mm/hr), END=-1
2604 *%-----|-----
2605 *COMPUTE DUALHYD NHYDin=["S-1-D3"], CINLET=[0.719](cms), NINLET=[1],
2606 * MajNHYD=["S-1-D3J"]
2607 * MinNHYD=["S-1-D3N"]
2608 * TMJSTO=[9999999](cu-m)
2609 *%-----|-----
2610 *ADD HYD NHYDsum=["S-1-D3S"], NHYDs to add=["S-1-D3J"+"S-1-D3N"]
2611 *%-----|-----
2612 *ROUTE RESERVOIR NHYDout=["S-1-D3R"],NHYDin=["S-1-D3S"] ,
2613 * RDT=[1](min),
2614 * TABLE of ( OUTFLOW-STORAGE ) values
2615 * (cms) - (ha-m)

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2613 * [ 0.0 , 0.0 ]
2614 * [ 0.0811, 0.2708 ]
2615 * [ -1 , -1 ] (max twenty pts)
2616 * NHYDovf=["S-1-D3Rovf"]
2617 *%-----|-----|
2618 CONTINUOUS STANDHYD NHYD=["S-1-D4"], DT=[1](min), AREA=[3.28](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
2619 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
IAper=[4.67](mm), SLPP=[2.0](%),
2620 LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
2621 LGI=[147.874](m), MNI=[0.013], SCI=[0](min),
2622 Continuous simulation parameters:
IaRECper=[4](hrs), IaRECimp=[4](hrs),
2623 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2624 InterEventTime=[12](hrs), END=-1
2625
2626 *%-----|-----|
2627 *CONTINUOUS NASHYD NHYD=["S-1-D4"], DT=[1]min, AREA=[3.28](ha),
2628 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2629 * N=[3], TP=[1.10]hrs,
2630 * Continuous simulation parameters:
2631 * IaRECper=[4](hrs),
2632 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2633 * InterEventTime=[12](hrs)
2634 * Baseflow simulation parameters:
2635 * BaseFlowOption=[1] ,
2636 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2637 * VHydCond=[0.055](mm/hr), END=-1
2638 *%-----|-----|
2639 *COMPUTE DUALHYD NHYDin=["S-1-D4"], CINLET=[0.373](cms), NINLET=[1],
2640 * MajNHYD=["S-1-D4J"]
2641 * MinNHYD=["S-1-D4N"]
2642 * TMJSTO=[9999999](cu-m)
2643 *%-----|-----|
2644 *ADD HYD NHYDsum=["S-1-D4S"], NHYDs to add=["S-1-D4J"+"S-1-D4N"]
2645 *%-----|-----|
2646 *ROUTE RESERVOIR NHYDout=["S-1-D4R"],NHYDin=["S-1-D4S"],
2647 * RDT=[1](min),
2648 * TABLE of ( OUTFLOW-STORAGE ) values
2649 * (cms) - (ha-m)
2650 * [ 0.0 , 0.0 ]
2651 * [ 0.0392, 0.1308 ]
2652 * [ -1 , -1 ] (max twenty pts)
2653 * NHYDovf=["S-1-D4Rovf"]
2654 *%-----|-----|
2655 CONTINUOUS STANDHYD NHYD=["S-1-D5"], DT=[1](min), AREA=[12.84](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
2656 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
IAper=[4.67](mm), SLPP=[2.0](%),
2657 LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
2658 LGI=[292.57](m), MNI=[0.013], SCI=[0](min),
2659 Continuous simulation parameters:
IaRECper=[4](hrs), IaRECimp=[4](hrs),
2660 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2661 InterEventTime=[12](hrs), END=-1
2662
2663 *%-----|-----|
2664 *CONTINUOUS NASHYD NHYD=["S-1-D5"], DT=[1]min, AREA=[12.84](ha),
2665 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2666 * N=[3], TP=[1.10]hrs,
2667 * Continuous simulation parameters:
2668 * IaRECper=[4](hrs),
2669 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2670 * InterEventTime=[12](hrs)
2671 * Baseflow simulation parameters:
2672 * BaseFlowOption=[1] ,

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2673 *          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2674 *          VHydCond=[0.055](mm/hr),   END=-1
2675 *%-----|-----
2676 *COMPUTE DUALHYD  NHYDin=["S-1-D5"], CINLET=[1.395](cms), NINLET=[1],
2677 *                  MajNHYD=["S-1-D5J"]
2678 *                  MinNHYD=["S-1-D5N"]
2679 *                  TMJSTO=[9999999](cu-m)
2680 *%-----|-----
2681 *ADD HYD          NHYDsum=["S-1-D5S"], NHYDs to add=["S-1-D5J"+"S-1-D5N"]
2682 *%-----|-----
2683 *ROUTE RESERVOIR NHYDout=["S-1-D5R"],NHYDin=["S-1-D5S"],
2684 *                  RDT=[1](min),
2685 *                  TABLE of ( OUTFLOW-STORAGE ) values
2686 *                  (cms) - (ha-m)
2687 *                  [ 0.0      , 0.0 ]
2688 *                  [ 0.1535, 0.5120 ]
2689 *                  [   -1   ,  -1   ] (max twenty pts)
2690 *                  NHYDovf=["S-1-D5Rovf"]
2691 *%-----|-----
2692 CONTINUOUS STANDHYD NHYD=["S-1-D6"], DT=[1](min), AREA=[1.75](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
2693 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
2694 IAper=[4.67](mm), SLPP=[2.0](%),
LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
2695 IAimp=[1.57](mm), SLPI=[0.75](%),
2696 LGI=[108.01](m), MNI=[0.013], SCI=[0](min),
2697 Continuous simulation parameters:
2698 IaRECper=[4](hrs), IaRECimp=[4](hrs),
2699 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
InterEventTime=[12](hrs),   END=-1
2700 *%-----|-----
2701 *CONTINUOUS NASHYD  NHYD=["S-1-D6"], DT=[1]min, AREA=[1.75](ha),
2702 *                  DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2703 *                  N=[3], TP=[1.10]hrs,
2704 *                  Continuous simulation parameters:
2705 *                  IaRECper=[4](hrs),
2706 *                  SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2707 *                  InterEventTime=[12](hrs)
2708 *                  Baseflow simulation parameters:
2709 *                  BaseFlowOption=[1],
2710 *                  InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2711 *                  VHydCond=[0.055](mm/hr),   END=-1
2712 *%-----|-----
2713 *COMPUTE DUALHYD  NHYDin=["S-1-D6"], CINLET=[0.218](cms), NINLET=[1],
2714 *                  MajNHYD=["S-1-D6J"]
2715 *                  MinNHYD=["S-1-D6N"]
2716 *                  TMJSTO=[9999999](cu-m)
2717 *%-----|-----
2718 *ADD HYD          NHYDsum=["S-1-D6S"], NHYDs to add=["S-1-D6J"+"S-1-D6N"]
2719 *%-----|-----
2720 *ROUTE RESERVOIR NHYDout=["S-1-D6R"],NHYDin=["S-1-D6S"],
2721 *                  RDT=[1](min),
2722 *                  TABLE of ( OUTFLOW-STORAGE ) values
2723 *                  (cms) - (ha-m)
2724 *                  [ 0.0      , 0.0 ]
2725 *                  [ 0.0209, 0.0698 ]
2726 *                  [   -1   ,  -1   ] (max twenty pts)
2727 *                  NHYDovf=["S-1-D6Rovf"]
2728 *%-----|-----
2729 CONTINUOUS STANDHYD NHYD=["S-1-D7"], DT=[1](min), AREA=[2.03](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
2730 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
2731 IAper=[4.67](mm), SLPP=[2.0](%),
LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
2732 IAimp=[1.57](mm), SLPI=[0.75](%),
LGI=[116.33](m), MNI=[0.013], SCI=[0](min),

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2733 Continuous simulation parameters:
2734 IaREcper=[4](hrs), IaREcimp=[4](hrs),
2735 SMIN=[-1](mm), SMAx=[-1](mm), SK=[0.010]/(mm),
2736 InterEventTime=[12](hrs), END=-1
2737 *%-----|-----|
2738 *CONTINUOUS NASHYD NHYD=["S-1-D7"], DT=[1]min, AREA=[2.03](ha),
2739 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2740 * N=[3], TP=[1.10]hrs,
2741 * Continuous simulation parameters:
2742 * IaREcper=[4](hrs),
2743 * SMIN=[-1](mm), SMAx=[-1](mm), SK=[0.010]/(mm),
2744 * InterEventTime=[12](hrs)
2745 * Baseflow simulation parameters:
2746 * BaseFlowOption=[1] ,
2747 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2748 * VHydCond=[0.055](mm/hr), END=-1
2749 *%-----|-----|
2750 *COMPUTE DUALHYD NHYDin=["S-1-D7"], CINLET=[2.279](cms), NINLET=[1],
2751 * MajNHYD=["S-1-D7J"]
2752 * MinNHYD=["S-1-D7N"]
2753 * TMJSTO=[9999999](cu-m)
2754 *%-----|-----|
2755 *ADD HYD NHYDsum=["S-1-D7S"], NHYDs to add=["S-1-D7J"+"S-1-D7N"]
2756 *%-----|-----|
2757 *ROUTE RESERVOIR NHYDout=["S-1-D7R"], NHYDin=["S-1-D7S"] ,
2758 * RDT=[1](min),
2759 * TABLE of ( OUTFLOW-STORAGE ) values
2760 * (cms) - (ha-m)
2761 * [ 0.0 , 0.0 ]
2762 * [ 0.0243, 0.0810 ]
2763 * [ -1 , -1 ] (max twenty pts)
2764 * NHYDovf=["S-1-D8Rovf"]
2765 *%-----|-----|
2766 * -JFSA 2021-02-26 "S-1-D8" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2767 *CONTINUOUS STANDHYD NHYD=["S-1-D8"], DT=[1](min), AREA=[5.27](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
2768 * LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
IAper=[4.67](mm), SLPP=[2.0](%),
2769 * LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
2770 * LGI=[187.439](m), MNI=[0.013], SCI=[0](min),
2771 * Continuous simulation parameters:
2772 * IaREcper=[4](hrs), IaREcimp=[4](hrs),
2773 * SMIN=[-1](mm), SMAx=[-1](mm), SK=[0.010]/(mm),
2774 * InterEventTime=[12](hrs), END=-1
2775 *%-----|-----|
2776 *CONTINUOUS NASHYD NHYD=["S-1-D8"], DT=[1]min, AREA=[5.27](ha),
2777 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2778 * N=[3], TP=[1.10]hrs,
2779 * Continuous simulation parameters:
2780 * IaREcper=[4](hrs),
2781 * SMIN=[-1](mm), SMAx=[-1](mm), SK=[0.010]/(mm),
2782 * InterEventTime=[12](hrs)
2783 * Baseflow simulation parameters:
2784 * BaseFlowOption=[1] ,
2785 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2786 * VHydCond=[0.055](mm/hr), END=-1
2787 *%-----|-----|
2788 *COMPUTE DUALHYD NHYDin=["S-1-D8"], CINLET=[2.279](cms), NINLET=[1],
2789 * MajNHYD=["S-1-D8J"]
2790 * MinNHYD=["S-1-D8N"]
2791 * TMJSTO=[9999999](cu-m)
2792 *%-----|-----|
2793 *ADD HYD NHYDsum=["S-1-D8S"], NHYDs to add=["S-1-D8J"+"S-1-D8N"]
2794 *%-----|-----|

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2795 *ADD HYD NHYDsum=["S-1-D"], NHYDs to add=["S-1-Okeefe"+"S-1"+"S-1-Post"]
2796 *%-----|-----|
2797 *COMPUTE DUALHYD NHYDin=["S-1-D"], CINLET=[11.616](cms), NINLET=[1],
2798 * MajNHYD=["S-1-D-MJ"]
2799 * MinNHYD=["S-1-D-MN"]
2800 * TMJSTO=[5974](cu-m)
2801 *%-----|-----|
2802 *ADD HYD NHYDsum=["S-1-DEV"], NHYDs to add=["S-1-D-MJ"+"S-1-D-MN"]
2803 *%-----|-----|
2804 *ROUTE RESERVOIR NHYDout=["S-1-D8R"] ,NHYDin=["S-1-D8S"] ,
2805 * RDT=[1](min),
2806 * TABLE of ( OUTFLOW-STORAGE ) values
2807 * (cms) - (ha-m)
2808 * [ 0.0 , 0.0 ]
2809 * [ 0.0630, 0.2102 ]
2810 * [ -1 , -1 ] (max twenty pts)
2811 * NHYDovf=["S-1-D8Rovf"]
2812 *%-----|-----|
2813 *%-----|-----|
2814 * -JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
(W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
2815 *# Catchment W_CLAR
2816 *# - To West Clarke Drain (south of the Jock)
2817 *# - Subdivision with 43% imp. as per Barrhaven South MSS
2818 *# - 2020-11-30 update CLARKE Tributary Drainage Area to = 121 ha based on
P598(04)-11
2819 *# - 2020-11-30 split CLARKE Drainage Area to MAJOR and ALL
2820 *#*****
2821 CONTINUOUS STANDHYD NHYD=["W_CLAR_MJ"], DT=[1]min, AREA=[1.772](ha),
2822 XIMP=[0.46], TIMP=[0.59], DWF=[0](cms), LOSS=[2],
2823 SCS curve number CN=[77],
2824 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
2825 LGP=[40](m), MNP=[0.25], SCP=[0](min),
2826 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
2827 LGI=[109](m), MNI=[0.013], SCI=[0](min),
2828 Continuous simulation parameters:
2829 IaREcper=[4](hrs), IaREcimp=[4](hrs),
2830 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2831 InterEventTime=[18](hrs), END=-1
2832 *%-----|-----|
2833 *COMPUTE DUALHYD NHYDin=["W_CLAR_MJ"], CINLET=[0.213](cms), NINLET=[1],
2834 * MajNHYD=["W_CLAR_MJj"]
2835 * MinNHYD=["W_CLAR_MJn"]
2836 * TMJSTO=[0.1](cu-m)
2837 *%-----|-----|
2838 *# 5-Year + 12% Capture
2839 ROUTE RESERVOIR NHYDout=["W_CLAR_MJn"] ,NHYDin=["W_CLAR_MJ"] ,
2840 RDT=[1](min),
2841 TABLE of ( OUTFLOW-STORAGE ) values
2842 (cms) - (ha-m)
2843 [ 0.0 , 0.0 ]
2844 [ 0.213 , 0.0001 ]
2845 [ -1 , -1 ] (max twenty pts)
2846 NHYDovf=["W_CLAR_MJj"] ,
2847 *%-----|-----|
2848 * -Clarke_All area from P 598(04)-11 = 120.207 ha, change to 127.298 ha based on
GIS measurements,
2849 * -JFSA, 2021-01-19 update W_CLAR_ALL to (121.17-1.772=119.398) ha based on GIS
measurements W_CLAR is 121.17 ha and W_CLAR_MJ is 1.772 ha
2850 CONTINUOUS STANDHYD NHYD=["W_CLAR_ALL"], DT=[1]min, AREA=[119.398](ha),
2851 XIMP=[0.60], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2852 SCS curve number CN=[77],
2853 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
2854 LGP=[40](m), MNP=[0.25], SCP=[0](min),
2855 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
2856 LGI=[892.18](m), MNI=[0.013], SCI=[0](min),

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2857 Continuous simulation parameters:
2858 IaRECper=[4](hrs), IaRECimp=[4](hrs),
2859 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2860 InterEventTime=[18](hrs), END=-1
2861 *%-----|-----|
2862 ADD HYD NHYDsum=["W_CLAR"], NHYDs to add=["W_CLAR_ALL"+"W_CLAR_MJj"]
2863 *%-----|-----|
2864 SAVE HYD NHYD=["W_CLAR"], # OF PCYCLES=[-1], ICASEsh=[1]
2865 HYD_COMMENT=["Total Flows to West Clarke"]
2866 *#*****
2867 *# West Clarke Pond 2
2868 *# - Rating curve obtained from Barrhaven South MSS modeling
2869 *# - Tributary Drainage Area to MSS Pond 2 = 241 ha
2870 *#*****
2871 ROUTE RESERVOIR NHYDout=["MS_P2"], NHYDin=["W_CLAR"],
2872 RDT=[1](min),
2873 TABLE of ( OUTFLOW-STORAGE ) values
2874 (cms) - (ha-m)
2875 [ 0.0 , 0.0 ]
2876 [ 0.128 , 0.161 ]
2877 [ 0.138 , 0.409 ]
2878 [ 0.148 , 0.68 ]
2879 [ 0.227 , 0.931 ]
2880 [ 0.354 , 1.223 ]
2881 [ 0.505 , 1.52 ]
2882 [ 0.666 , 1.821 ]
2883 [ 0.831 , 2.123 ]
2884 [ 0.995 , 2.434 ]
2885 [ 1.069 , 2.583 ]
2886 [ 1.51 , 2.647 ]
2887 [ 4.904 , 2.861 ]
2888 [ 13.048 , 3.188 ]
2889 [ 23.745 , 3.523 ]
2890 [ 36.474 , 3.871 ]
2891 [ 45.938 , 4.127 ]
2892 [ 61.652 , 4.539 ]
2893 [ -1 , -1 ] (max twenty pts)
2894 NHYDovf=["P2-OVF"]
2895 *%-----|-----|
2896 *#*****
2897 * -JFSA, 2021-01-22 "W_CLAR_UNDE" (west of Clarke sub-catchment) discharges
directly to the jock river through a road side ditch on the west side of Borrisokane
road (station 6016)
2898 *CONTINUOUS NASHYD NHYD=["W_CLAR_UNDE"], DT=[1]min, AREA=[35.65](ha),
2899 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2900 * N=[3], TP=[1.10]hrs,
2901 * Continuous simulation parameters:
2902 * IaRECper=[4](hrs),
2903 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2904 * InterEventTime=[12](hrs)
2905 * Baseflow simulation parameters:
2906 * BaseFlowOption=[1] ,
2907 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2908 * VHydCond=[0.055](mm/hr), END=-1
2909 *%-----|-----|
2910 ADD HYD NHYDsum=["SN_CE"], NHYDs to
add=["N_CE"+"S-1-D4"+"S-1-D5"+"MS_P2"+"P2-OVF"]
2911 *%-----|-----|
2912 SAVE HYD NHYD=["SN_CE"], # OF PCYCLES=[-1], ICASEsh=[1]
2913 HYD_COMMENT=["Total Flows before Station 5737 on Jock River"]
2914 *%-----|-----|
2915 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5737
2916 *# 2021-02-25 add station 5737 before station 5002. Station 5737 was extracted from the
HEC-RAS model
T:\PROJ\1474-16\Design\20201026-QuantityControlAnalysis\HEC-RAS\JockLidar2005
2917 *# JFSA 2021-03-02 change the slope to 0.0175% instead of 0.02593 to stabilize the model

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2918 ROUTE CHANNEL      NHYDout=["5737"] ,NHYDin=["SN_CE" ] ,
2919                      RDT=[1](min),
2920                      CHLGTH=[270](m),   CHSLOPE=[0.0175](%),
2921                      FPSLOPE=[0.0175](%),
2922                      SECNUM=[1.0],      NSEG=[3]
2923                      ( SEGROUGH, SEGDIST (m))=
2924                      [0.050,-24.04
2925                      -0.035,23.92
2926                      0.050,1130.8] NSEG times
2927                      ( DISTANCE (m), ELEVATION (m))=
2928                      [-1060.52, 94 ]
2929                      [-268.6, 91.5 ]
2930                      [-259.43, 91.5 ]
2931                      [-179.48, 91.5 ]
2932                      [-67.9, 91.5 ]
2933                      [-59.21, 91.5 ]
2934                      [-33.19, 91 ]
2935                      [-26.08, 90.5 ]
2936                      [-24.04, 90 ]
2937                      [-13.14, 86.77 ]
2938                      [0, 85 ]
2939                      [14.68, 86.74 ]
2940                      [23.92, 90 ]
2941                      [25.78, 90.5 ]
2942                      [31.91, 91 ]
2943                      [91.95, 91.5 ]
2944                      [772.15, 92 ]
2945                      [961.49, 92.5 ]
2946                      [1044.69, 93 ]
2947                      [1130.8, 95 ]
2948 *%-----|-----|
2949 ADD HYD      NHYDsum=["5002"], NHYDs to add=["5737"+"S-1-D1"+"S-1-D6"+"S-1-D7"]
2950 *%-----|-----|
2951 SAVE HYD     NHYD=["5002"], # OF PCYCLES=[-1], ICASEsh=[1]
2952             HYD_COMMENT=["Total Flows before Station 5002 on Jock River"]
2953 *%-----|-----|
2954 *# Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain
2955 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5002
2956 *# JFSA 2021-02-19 Change the slope from 0.01 % (as per Stantec Report 2007) to 0.0255
% so the model will be more stable and give reasonable results. It is justifiable as
ROUTE CHANNELs aren't well suited to really flat slopes.
2957 *# JFSA 2021-02-19 Change to three ROUTE CHANNEL with length 275 m each instead of one
with 825 m length so the model will be more stable
2958 *# JFSA 2021-02-26 change the length of 5002 route channel from 825 m to 736 m. That is
because of adding station 5737 between station 6016 and station 5002. Then the length
from station 5737 to station 5002 is 736 m. Change the slope from 0.0255 % to 0.09511 %
2959 *
2960 ROUTE CHANNEL      NHYDout=["N_WCa"] ,NHYDin=["5002"] ,
2961                      RDT=[1](min),
2962                      CHLGTH=[245.33333](m),   CHSLOPE=[0.09511](%),
2963                      FPSLOPE=[0.09511](%),
2964                      SECNUM=[1.0],      NSEG=[3]
2965                      ( SEGROUGH, SEGDIST (m))=
2966                      [0.050,-37.5
2967                      -0.035,37.50
2968                      0.050,157.05] NSEG times
2969                      ( DISTANCE (m), ELEVATION (m))=
2970                      [-601.81, 91.5 ]
2971                      [-37.50, 90.00]
2972                      [-19.61, 87.04]
2973                      [0.00, 85.70]
2974                      [14.87, 86.93]
2975                      [37.50, 90.00]
2976                      [38.54, 90.50]
2977                      [42.23, 91]
2978                      [157.05,91.50]

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2979 * [161.44, 91.50]
2980 * [236.48, 93.00]
2981 * [385.47, 92.50]
2982 * [390.78, 92.50]
2983 *%-----|-----
2984 ROUTE CHANNEL NHYDout=["N_WCb"] ,NHYDin=["N_WCa"] ,
2985 RDT=[1](min),
2986 CHLGTH=[245.33333](m), CHSLOPE=[0.09511](%),
2987 FPSLOPE=[0.09511](%),
2988 SECNUM=[1.0], NSEG=[3]
2989 ( SEGROUGH, SEGDIST (m))=
2990 [0.050,-37.5
2991 -0.035,37.50
2992 0.050,157.05] NSEG times
2993 ( DISTANCE (m), ELEVATION (m))=
2994 [-601.81, 91.5]
2995 [-37.50, 90.00]
2996 [-19.61, 87.04]
2997 [0.00, 85.70]
2998 [14.87, 86.93]
2999 [37.50, 90.00]
3000 [38.54, 90.50]
3001 [42.23, 91]
3002 [157.05,91.50]
3003 *%-----|-----
3004 ROUTE CHANNEL NHYDout=["N_WC"] ,NHYDin=["N_WCb"] ,
3005 RDT=[1](min),
3006 CHLGTH=[245.33333](m), CHSLOPE=[0.09511](%),
3007 FPSLOPE=[0.09511](%),
3008 SECNUM=[1.0], NSEG=[3]
3009 ( SEGROUGH, SEGDIST (m))=
3010 [0.050,-37.5
3011 -0.035,37.50
3012 0.050,157.05] NSEG times
3013 ( DISTANCE (m), ELEVATION (m))=
3014 [-601.81, 91.5]
3015 [-37.50, 90.00]
3016 [-19.61, 87.04]
3017 [0.00, 85.70]
3018 [14.87, 86.93]
3019 [37.50, 90.00]
3020 [38.54, 90.50]
3021 [42.23, 91]
3022 [157.05,91.50]
3023 *#*****
3024 * -JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
(W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
3025 *ADD HYD NHYDsum=["SN_WC"], NHYDs to
add=["MS_P2"+"P2-OVF"+"N_WC"+"W_CLAR_UNDE"]
3026 *%-----|-----
3027 *SAVE HYD NHYD=["SN_WC"], # OF PCYCLES=[-1], ICASEsh=[1]
3028 * HYD_COMMENT=["Total Flows at West Clarke Pond Outlet"]
3029 *%-----|-----
3030 *# Hydrograph from Node West Clarke routed to Node at Kennedy - Burnett Drain
3031 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4534
3032 *#
3033 ROUTE CHANNEL NHYDout=["N_KB"] ,NHYDin=["N_WC"] ,
3034 RDT=[1](min),
3035 CHLGTH=[1020](m), CHSLOPE=[0.0498](%),
3036 FPSLOPE=[0.0498](%),
3037 SECNUM=[1.0], NSEG=[3]
3038 ( SEGROUGH, SEGDIST (m))=
3039 [0.050,-23.63
3040 -0.035,23.63
3041 0.050,728.3] NSEG times
3042 ( DISTANCE (m), ELEVATION (m))=

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3043 [-1082.01,94]
3044 [-1028.17,92.5]
3045 [-992.3,93.5]
3046 [-279.34,90]
3047 [-23.63,90]
3048 [-13.45,87.13]
3049 [-0.07,86.24]
3050 [10.54,87.15]
3051 [23.63,90]
3052 [24.86,90.5]
3053 [26.72,91]
3054 [45.07,91.5]
3055 [128.17,91.5]
3056 [270.7,92.5]
3057 [728.3,95]
3058 *%-----|-----|
3059 *#*****|
3060 *# Catchment KEN_BU
3061 *# - To Kennedy-Burnett SWM Facility
3062 *# - Outlets to Fraser-Clarke drain (north of the Jock)
3063 *# - Medium density residential subdivision
3064 * - Add Kennedy Burnett model (Convert PCSWMM from NOVATECH June, 2020 to SWMHYMO)
3065 *#*****|
3066 *CONTINUOUS STANDHYD NHYD=["KEN_BU"], DT=[1]min, AREA=[281](ha),
3067 * XIMP=[0.55], TIMP=[0.55], DWF=[0](cms), LOSS=[2],
3068 * SCS curve number CN=[71],
3069 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3070 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3071 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3072 * LGI=[1369](m), MNI=[0.013], SCI=[0](min),
3073 * Continuous simulation parameters:
3074 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
3075 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3076 * InterEventTime=[18](hrs), END=-1
3077 *%-----|-----|
3078 *#*****|
3079 *# Existing Kennedy-Burnett SWM Facility
3080 *# - Rating curve obtained from URTKBP
3081 *# - Tributary Drainage Area to Pond = 160 ha
3082 *#*****|
3083 *ROUTE RESERVOIR NHYDout=["KEN_P"], NHYDin=["KEN_BU"],
3084 * RDT=[1](min),
3085 * TABLE of ( OUTFLOW-STORAGE ) values
3086 * (cms) - (ha-m)
3087 * [ 0.0 , 0.0 ]
3088 * [ 0.13 , 0.26]
3089 * [ 0.43 , 0.56]
3090 * [ 0.67 , 0.90]
3091 * [ 0.86 , 1.32]
3092 * [ 1.01 , 1.79]
3093 * [ 1.15 , 2.33]
3094 * [ -1 , -1 ] (max twenty pts)
3095 * NHYDovf=["KEN-OV"]
3096 *%-----|-----|
3097 * -JFSA, 2021-01-19 update all KEN_BU areas based on GIS measurements
3098 CONTINUOUS STANDHYD NHYD=["KB-01A"], DT=[1]min, AREA=[40.82](ha), XIMP=[0.097],
3099 TIMP=[0.4], DWF=[0](cms), LOSS=[1]:
3099 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3100 F=[0.00](mm),
3100 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[40](m),
3101 MNP=[0.250], SCP=[0](min),
3101 Impervious areas: IAimp=[0.785](mm), SLPI=[0.5](%),
3102 LGI=[521.664](m), MNI=[0.013], SCI=[0](min),
3102 Continuous simulation parameters:
3103 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
3103 END=-1

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3104 *%-----|-----|
3105 COMPUTE DUALHYD NHYDin=["KB-01A"], CINLET=[3.6](cms), NINLET=[1],
3106 MajNHYD=["KB-01A-MJ"]
3107 MinNHYD=["KB-01A-MN"]
3108 TMJSTO=[4995](cu-m)
3109 *%-----|-----|
3110 ADD HYD NHYDsum=["KB-01A-S"], NHYDs to add=["KB-01A-MJ"+"KB-01A-MN"]
3111 *%-----|-----|
3112 CONTINUOUS STANDHYD NHYD=["KB-01B"], DT=[1]min, AREA=[31.1](ha), XIMP=[0.1875],
TIMP=[0.375], DWF=[0](cms), LOSS=[1]:
3113 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3114 Pervious areas: IAper=[4.67](mm), SLPP=[0.42](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3115 Impervious areas: IAimp=[0.785](mm), SLPI=[0.42](%),
LGI=[455.339](m), MNI=[0.013], SCI=[0](min),
3116 Continuous simulation parameters:
3117 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3118 *%-----|-----|
3119 COMPUTE DUALHYD NHYDin=["KB-01B"], CINLET=[1.585](cms), NINLET=[1],
3120 MajNHYD=["KB-01B-MJ"]
3121 MinNHYD=["KB-01B-MN"]
3122 TMJSTO=[6075](cu-m)
3123 *%-----|-----|
3124 ADD HYD NHYDsum=["KB-01B-S"], NHYDs to add=["KB-01B-MJ"+"KB-01B-MN"]
3125 *%-----|-----|
3126 CONTINUOUS STANDHYD NHYD=["KB-01C"], DT=[1]min, AREA=[13.78](ha), XIMP=[0.2045],
TIMP=[0.409], DWF=[0](cms), LOSS=[1]:
3127 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3128 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3129 Impervious areas: IAimp=[0.785](mm), SLPI=[0.5](%),
LGI=[303.095](m), MNI=[0.013], SCI=[0](min),
3130 Continuous simulation parameters:
3131 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3132 *%-----|-----|
3133 COMPUTE DUALHYD NHYDin=["KB-01C"], CINLET=[1.35](cms), NINLET=[1],
3134 MajNHYD=["KB-01C-MJ"]
3135 MinNHYD=["KB-01C-MN"]
3136 TMJSTO=[1880](cu-m)
3137 *%-----|-----|
3138 ADD HYD NHYDsum=["KB-01C-S"], NHYDs to add=["KB-01C-MJ"+"KB-01C-MN"]
3139 *%-----|-----|
3140 CONTINUOUS STANDHYD NHYD=["KB-03"], DT=[1]min, AREA=[84.78](ha), XIMP=[0.197],
TIMP=[0.394], DWF=[0](cms), LOSS=[1]:
3141 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3142 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3143 Impervious areas: IAimp=[0.785](mm), SLPI=[0.63](%),
LGI=[751.798](m), MNI=[0.013], SCI=[0](min),
3144 Continuous simulation parameters:
3145 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3146 *%-----|-----|
3147 COMPUTE DUALHYD NHYDin=["KB-03"], CINLET=[5.27](cms), NINLET=[1],
3148 MajNHYD=["KB-03-MJ"]
3149 MinNHYD=["KB-03-MN"]
3150 TMJSTO=[15500](cu-m)
3151 *%-----|-----|
3152 ADD HYD NHYDsum=["KB-03-S"], NHYDs to add=["KB-03-MJ"+"KB-03-MN"]
3153 *%-----|-----|
3154 CONTINUOUS STANDHYD NHYD=["KB-04"], DT=[1]min, AREA=[6.95](ha), XIMP=[0.85],

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TIMP=[0.85], DWF=[0](cms), LOSS=[1]:
3155 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3156 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3157 Impervious areas: IAimp=[0.942](mm), SLPI=[0.5](%),
LGI=[215.252](m), MNI=[0.013], SCI=[0](min),
3158 Continuous simulation parameters:
3159 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3160 *%-----|-----|
3161 COMPUTE DUALHYD NHYDin=["KB-04"], CINLET=[0.503](cms), NINLET=[1],
3162 MaJNHYD=["KB-04-MJ"]
3163 MinNHYD=["KB-04-MN"]
3164 TMJSTO=[1972](cu-m)
3165 *%-----|-----|
3166 ADD HYD NHYDsum=["KB-04-S"], NHYDs to add=["KB-04-MJ"+"KB-04-MN"]
3167 *%-----|-----|
3168 CONTINUOUS STANDHYD NHYD=["KB-05"], DT=[1]min, AREA=[5.19](ha), XIMP=[0.93],
TIMP=[0.93], DWF=[0](cms), LOSS=[1]:
3169 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3170 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3171 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[186.011](m), MNI=[0.013], SCI=[0](min),
3172 Continuous simulation parameters:
3173 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3174 *%-----|-----|
3175 *%-----|-----|
3176 CONTINUOUS STANDHYD NHYD=["KB-06"], DT=[1]min, AREA=[12.93](ha), XIMP=[0.873],
TIMP=[0.873], DWF=[0](cms), LOSS=[1]:
3177 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3178 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3179 Impervious areas: IAimp=[0.942](mm), SLPI=[4.75](%),
LGI=[293.598](m), MNI=[0.013], SCI=[0](min),
3180 Continuous simulation parameters:
3181 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3182 *%-----|-----|
3183 COMPUTE DUALHYD NHYDin=["KB-06"], CINLET=[2.262](cms), NINLET=[1],
3184 MaJNHYD=["KB-06-MJ"]
3185 MinNHYD=["KB-06-MN"]
3186 TMJSTO=[1950](cu-m)
3187 *%-----|-----|
3188 ADD HYD NHYDsum=["KB-06-S"], NHYDs to add=["KB-06-MJ"+"KB-06-MN"]
3189 *%-----|-----|
3190 CONTINUOUS STANDHYD NHYD=["KB-11"], DT=[1]min, AREA=[4.03](ha), XIMP=[0.675],
TIMP=[0.675], DWF=[0](cms), LOSS=[1]:
3191 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3192 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3193 Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%),
LGI=[163.911](m), MNI=[0.013], SCI=[0](min),
3194 Continuous simulation parameters:
3195 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3196 *%-----|-----|
3197 COMPUTE DUALHYD NHYDin=["KB-11"], CINLET=[0.5773](cms), NINLET=[1],
3198 MaJNHYD=["KB-11-MJ"]
3199 MinNHYD=["KB-11-MN"]
3200 TMJSTO=[597](cu-m)

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3201  *%-----|-----|
3202  ADD HYD      NHYDsum=["KB-11-S"], NHYDs to add=["KB-11-MJ"+"KB-11-MN"]
3203  *%-----|-----|
3204  CONTINUOUS STANDHYD NHYD=["S1"], DT=[1]min, AREA=[4.99](ha), XIMP=[0.93], TIMP=[0.93],
DWF=[0](cms), LOSS=[1]:
3205      Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3206      Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3207      Impervious areas: IAimp=[1.57](mm), SLPI=[2.0](%),
LGI=[182.392](m), MNI=[0.013], SCI=[0](min),
3208      Continuous simulation parameters:
3209      IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3210  *%-----|-----|
3211  CONTINUOUS STANDHYD NHYD=["KB-15"], DT=[1]min, AREA=[2.15](ha), XIMP=[0.79],
TIMP=[0.79], DWF=[0](cms), LOSS=[1]:
3212      Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3213      Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3214      Impervious areas: IAimp=[0.157](mm), SLPI=[0.3](%),
LGI=[119.722](m), MNI=[0.013], SCI=[0](min),
3215      Continuous simulation parameters:
3216      IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3217  *%-----|-----|
3218  *%-----|-----|
3219  ADD HYD      NHYDsum=["KB-P1"], NHYDs to
add=["KB-01A-S"+"KB-01B-S"+"KB-01C-S"+"KB-03-S"+"KB-04-S"+"KB-05"+"KB-06-S"+"KB-11-S"+"KB
-15"+"S1"]
3220  *%-----|-----|
3221  ROUTE RESERVOIR NHYDout=["KB-P1R"], NHYDin=["KB-P1"],
3222      RDT=[1](min),
3223      TABLE of ( OUTFLOW-STORAGE ) values
3224      (cms) - (ha-m)
3225      [ 0.0 , 0.0 ]
3226      [0.076,0.003]
3227      [0.088,0.006]
3228      [0.136,0.011]
3229      [0.301,0.017]
3230      [0.454,0.027]
3231      [0.631,0.041]
3232      [1.173,0.068]
3233      [1.91,0.111]
3234      [4.847,0.231]
3235      [9.813,0.436]
3236      [12.134,0.617]
3237      [12.438,0.732]
3238      [12.424,0.811]
3239      [12.425,0.894]
3240      [ -1 , -1 ] (max twenty pts)
3241      NHYDovf=["KB-P1ovf"]
3242  *%-----|-----|
3243  ADD HYD      NHYDsum=["KB-Pond1"], NHYDs to add=["KB-P1R"+"KB-P1ovf"]
3244  *%-----|-----|
3245  SAVE HYD     NHYD=["KB-Pond1"], # OF PCYCLES=[-1], ICASEsh=[1]
3246      HYD_COMMENT=["Total Flows at KB first pond"]
3247  *%-----|-----|
3248  CONTINUOUS STANDHYD NHYD=["KB-07"], DT=[1]min, AREA=[10.86](ha), XIMP=[0.86],
TIMP=[0.86], DWF=[0](cms), LOSS=[1]:
3249      Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3250      Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3251      Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%),

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LGI=[269.072](m), MNI=[0.013], SCI=[0](min),
3252 Continuous simulation parameters:
3253 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3254 *%-----|-----|
3255 COMPUTE DUALHYD NHYDin=["KB-07"], CINLET=[2.094](cms), NINLET=[1],
3256 MajNHYD=["KB-07-MJ"]
3257 MinNHYD=["KB-07-MN"]
3258 TMJSTO=[1378](cu-m)
3259 *%-----|-----|
3260 ADD HYD NHYDsum=["KB-07-S"], NHYDs to add=["KB-07-MJ"+"KB-07-MN"]
3261 *%-----|-----|
3262 CONTINUOUS STANDHYD NHYD=["KB-08"], DT=[1]min, AREA=[6.61](ha), XIMP=[0.64],
TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3263 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3264 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3265 Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%),
LGI=[209.921](m), MNI=[0.013], SCI=[0](min),
3266 Continuous simulation parameters:
3267 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3268 *%-----|-----|
3269 COMPUTE DUALHYD NHYDin=["KB-08"], CINLET=[1.058](cms), NINLET=[1],
3270 MajNHYD=["KB-08-MJ"]
3271 MinNHYD=["KB-08-MN"]
3272 TMJSTO=[787](cu-m)
3273 *%-----|-----|
3274 ADD HYD NHYDsum=["KB-08-S"], NHYDs to add=["KB-08-MJ"+"KB-08-MN"]
3275 *%-----|-----|
3276 CONTINUOUS STANDHYD NHYD=["KB-09"], DT=[1]min, AREA=[2.6](ha), XIMP=[0.86],
TIMP=[0.86], DWF=[0](cms), LOSS=[1]:
3277 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3278 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3279 Impervious areas: IAimp=[1.57](mm), SLPI=[2.0](%),
LGI=[131.656](m), MNI=[0.013], SCI=[0](min),
3280 Continuous simulation parameters:
3281 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3282 *%-----|-----|
3283 *%-----|-----|
3284 CONTINUOUS STANDHYD NHYD=["KB-10_1"], DT=[1]min, AREA=[2.37](ha), XIMP=[0.86],
TIMP=[0.86], DWF=[0](cms), LOSS=[1]:
3285 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3286 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3287 Impervious areas: IAimp=[1.57](mm), SLPI=[2.0](%),
LGI=[125.698](m), MNI=[0.013], SCI=[0](min),
3288 Continuous simulation parameters:
3289 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3290 *%-----|-----|
3291 CONTINUOUS STANDHYD NHYD=["KB-10_2"], DT=[1]min, AREA=[1.14](ha), XIMP=[0.86],
TIMP=[0.86], DWF=[0](cms), LOSS=[1]:
3292 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3293 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3294 Impervious areas: IAimp=[1.57](mm), SLPI=[2.0](%), LGI=[87.178](m),
MNI=[0.013], SCI=[0](min),
3295 Continuous simulation parameters:
3296 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),

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END=-1
3297 *%-----|-----|
3298 *%-----|-----|
3299 CONTINUOUS STANDHYD NHYD=["KB-12"], DT=[1]min, AREA=[4.86](ha), XIMP=[0.79],
TIMP=[0.79], DWF=[0](cms), LOSS=[1]:
3300 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3301 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3302 Impervious areas: IAimp=[1.099](mm), SLPI=[2.0](%),
LGI=[180.000](m), MNI=[0.013], SCI=[0](min),
3303 Continuous simulation parameters:
3304 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3305 *%-----|-----|
3306 COMPUTE DUALHYD NHYDin=["KB-12"], CINLET=[0.8665](cms), NINLET=[1],
3307 MajNHYD=["KB-12-MJ"]
3308 MinNHYD=["KB-12-MN"]
3309 TMJSTO=[632](cu-m)
3310 *%-----|-----|
3311 ADD HYD NHYDsum=["KB-12-S"], NHYDs to add=["KB-12-MJ"+"KB-12-MN"]
3312 *%-----|-----|
3313 CONTINUOUS STANDHYD NHYD=["KB-13"], DT=[1]min, AREA=[10.19](ha), XIMP=[0.64],
TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3314 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3315 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3316 Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%),
LGI=[260.640](m), MNI=[0.013], SCI=[0](min),
3317 Continuous simulation parameters:
3318 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3319 *%-----|-----|
3320 COMPUTE DUALHYD NHYDin=["KB-13"], CINLET=[1.722](cms), NINLET=[1],
3321 MajNHYD=["KB-13-MJ"]
3322 MinNHYD=["KB-13-MN"]
3323 TMJSTO=[1077](cu-m)
3324 *%-----|-----|
3325 ADD HYD NHYDsum=["KB-13-S"], NHYDs to add=["KB-13-MJ"+"KB-13-MN"]
3326 *%-----|-----|
3327 CONTINUOUS STANDHYD NHYD=["KB-14"], DT=[1]min, AREA=[5.47](ha), XIMP=[0.64],
TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3328 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3329 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3330 Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%),
LGI=[190.962](m), MNI=[0.013], SCI=[0](min),
3331 Continuous simulation parameters:
3332 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3333 *%-----|-----|
3334 COMPUTE DUALHYD NHYDin=["KB-14"], CINLET=[0.8734](cms), NINLET=[1],
3335 MajNHYD=["KB-14-MJ"]
3336 MinNHYD=["KB-14-MN"]
3337 TMJSTO=[631](cu-m)
3338 *%-----|-----|
3339 ADD HYD NHYDsum=["KB-14-S"], NHYDs to add=["KB-14-MJ"+"KB-14-MN"]
3340 *%-----|-----|
3341 *%-----|-----|
3342 CONTINUOUS STANDHYD NHYD=["KB-16_2"], DT=[1]min, AREA=[3.42](ha), XIMP=[0.71],
TIMP=[0.71], DWF=[0](cms), LOSS=[1]:
3343 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3344 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),

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3345 MNP=[0.250], SCP=[0](min),
Impervious areas: IAimp=[0.157](mm), SLPI=[0.3](%),
3346 LGI=[150.997](m), MNI=[0.013], SCI=[0](min),
3347 Continuous simulation parameters:
IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3348 *%-----|-----|
3349 ADD HYD NHYDsum=["KB-P2"], NHYDs to
add=["KB-Pond1"+"KB-07-S"+"KB-08-S"+"KB-09"+"KB-10_1"+"KB-10_2"+"KB-12-S"+"KB-13-S"+"KB-1
4-S"+"KB-16_2"]
3350 *%-----|-----|
3351 ROUTE RESERVOIR NHYDout=["KB-P2R"], NHYDin=["KB-P2"],
3352 RDT=[1](min),
3353 TABLE of ( OUTFLOW-STORAGE ) values
3354 (cms) - (ha-m)
3355 [ 0.0 , 0.0 ]
3356 [0.053,0.005]
3357 [0.132,0.009]
3358 [0.269,0.014]
3359 [0.455,0.023]
3360 [0.699,0.037]
3361 [0.947,0.056]
3362 [1.853,0.09]
3363 [2.712,0.146]
3364 [6.626,0.287]
3365 [11.228,0.515]
3366 [14.885,0.738]
3367 [16.473,0.893]
3368 [17.311,0.998]
3369 [17.633,1.063]
3370 [17.634,1.112]
3371 [ -1 , -1 ] (max twenty pts)
3372 NHYDovf=["KB-P2ovf"]
3373 *%-----|-----|
3374 ADD HYD NHYDsum=["KB-Pond2"], NHYDs to add=["KB-P2R"+"KB-P2ovf"]
3375 *%-----|-----|
3376 SAVE HYD NHYD=["KB-Pond2"], # OF PCYCLES=[-1], ICASEsh=[1]
3377 HYD_COMMENT=["Total Flows at KB second pond"]
3378 *%-----|-----|
3379 CONTINUOUS STANDHYD NHYD=["KB-16_1"], DT=[1]min, AREA=[2.8](ha), XIMP=[0.75],
TIMP=[0.75], DWF=[0](cms), LOSS=[1]:
3380 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3381 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3382 Impervious areas: IAimp=[0.157](mm), SLPI=[0.3](%),
LGI=[136.626](m), MNI=[0.013], SCI=[0](min),
3383 Continuous simulation parameters:
3384 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3385 *%-----|-----|
3386 ADD HYD NHYDsum=["KB-P3"], NHYDs to add=["KB-Pond2"+"KB-16_1"]
3387 *%-----|-----|
3388 *%-----|-----|
3389 * One inflow node from pond 3 is added to the model (ROUTE RESERVOIR)
3390 * Another inflow node from right side of pond 3 is not added to the model
3391 ROUTE RESERVOIR NHYDout=["KB-P3R"], NHYDin=["KB-P3"],
3392 RDT=[1](min),
3393 TABLE of ( OUTFLOW-STORAGE ) values
3394 (cms) - (ha-m)
3395 [ 0.0 , 0.0 ]
3396 [0.051,0.002]
3397 [0.048,0.003]
3398 [0.057,0.029]
3399 [0.089,0.045]
3400 [0.133,0.069]

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3401 [0.199,0.106]
3402 [0.321,0.172]
3403 [1.029,0.306]
3404 [4.036,0.527]
3405 [8.332,0.761]
3406 [11.727,0.941]
3407 [14.125,1.067]
3408 [15.675,1.149]
3409 [16.555,1.196]
3410 [16.911,1.214]
3411 [ -1 , -1 ] (max twenty pts)
3412 NHYDovf=["KB-P3ovf"]
3413 *%-----|-----|
3414 ADD HYD NHYDsum=["KB-Pond3"], NHYDs to add=["KB-P3R"+"KB-P3ovf"]
3415 *%-----|-----|
3416 SAVE HYD NHYD=["KB-Pond3"], # OF PCYCLES=[-1], ICASEsh=[1]
3417 HYD_COMMENT=["Total Flows at KB third pond"]
3418 *%-----|-----|
3419 *#*****|
3420 *# EXISTING / PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118080), SWM
3421 Modeling Approach, NOVATECH Report June, 2020)
3422 *# - TO FRASER-CLARKE DRAIN
3423 *#*****|
3424 CONTINUOUS STANDHYD NHYD=["FC-01"], DT=[1]min, AREA=[8.03](ha), XIMP=[0.47],
3425 TIMP=[0.47], DWF=[0](cms), LOSS=[1]:
3426 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3427 F=[0.00](mm),
3428 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3429 MNP=[0.250], SCP=[0](min),
3430 Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
3431 LGI=[231.373](m), MNI=[0.013], SCI=[0](min),
3432 Continuous simulation parameters:
3433 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
3434 END=-1
3435 *%-----|-----|
3436 COMPUTE DUALHYD NHYDin=["FC-01"], CINLET=[0.756](cms), NINLET=[1],
3437 MajNHYD=["FC-01-MJ"]
3438 MinNHYD=["FC-01-MN"]
3439 TMJSTO=[714](cu-m)
3440 *%-----|-----|
3441 ADD HYD NHYDsum=["FC-01-S"], NHYDs to add=["FC-01-MJ"+"FC-01-MN"]
3442 *%-----|-----|
3443 CONTINUOUS STANDHYD NHYD=["FC-02"], DT=[1]min, AREA=[16.05](ha), XIMP=[0.93],
3444 TIMP=[0.93], DWF=[0](cms), LOSS=[1]:
3445 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3446 F=[0.00](mm),
3447 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3448 MNP=[0.250], SCP=[0](min),
3449 Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
3450 LGI=[327.109](m), MNI=[0.013], SCI=[0](min),
3451 Continuous simulation parameters:
3452 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
3453 END=-1
3454 *%-----|-----|
3455 COMPUTE DUALHYD NHYDin=["FC-02"], CINLET=[1.159](cms), NINLET=[1],
3456 MajNHYD=["FC-02-MJ"]
3457 MinNHYD=["FC-02-MN"]
3458 TMJSTO=[2385](cu-m)
3459 *%-----|-----|
3460 ADD HYD NHYDsum=["FC-02-S"], NHYDs to add=["FC-02-MJ"+"FC-02-MN"]
3461 *%-----|-----|
3462 CONTINUOUS STANDHYD NHYD=["FC-03"], DT=[1]min, AREA=[7.37](ha), XIMP=[0.64],
3463 TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3464 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3465 F=[0.00](mm),
3466 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),

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3454 MNP=[0.250], SCP=[0](min),
Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
LGI=[221.660](m), MNI=[0.013], SCI=[0](min),
3455 Continuous simulation parameters:
3456 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3457 *%-----|-----|
3458 COMPUTE DUALHYD NHYDin=["FC-03"], CINLET=[0.358](cms), NINLET=[1],
3459 MajNHYD=["FC-03-MJ"]
3460 MinNHYD=["FC-03-MN"]
3461 TMJSTO=[1131](cu-m)
3462 *%-----|-----|
3463 ADD HYD NHYDsum=["FC-03-S"], NHYDs to add=["FC-03-MJ"+"FC-03-MN"]
3464 *%-----|-----|
3465 CONTINUOUS STANDHYD NHYD=["FC-04"], DT=[1]min, AREA=[12.87](ha), XIMP=[0.64],
TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3466 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3467 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3468 Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
LGI=[292.916](m), MNI=[0.013], SCI=[0](min),
3469 Continuous simulation parameters:
3470 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3471 *%-----|-----|
3472 COMPUTE DUALHYD NHYDin=["FC-04"], CINLET=[0.741](cms), NINLET=[1],
3473 MajNHYD=["FC-04-MJ"]
3474 MinNHYD=["FC-04-MN"]
3475 TMJSTO=[1794](cu-m)
3476 *%-----|-----|
3477 ADD HYD NHYDsum=["FC-04-S"], NHYDs to add=["FC-04-MJ"+"FC-04-MN"]
3478 *%-----|-----|
3479 *#*****
3480 *# PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118080), SWM Modeling
Approach, NOVATECH Report June, 2020)
3481 *# - TO JOCK RIVER
3482 *#*****
3483 CONTINUOUS STANDHYD NHYD=["JR-01"], DT=[1]min, AREA=[8.24](ha), XIMP=[0.64],
TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3484 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3485 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3486 Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
LGI=[234.379](m), MNI=[0.013], SCI=[0](min),
3487 Continuous simulation parameters:
3488 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3489 *%-----|-----|
3490 COMPUTE DUALHYD NHYDin=["JR-01"], CINLET=[0.563](cms), NINLET=[1],
3491 MajNHYD=["JR-01-MJ"]
3492 MinNHYD=["JR-01-MN"]
3493 TMJSTO=[1040](cu-m)
3494 *%-----|-----|
3495 ADD HYD NHYDsum=["JR-01-S"], NHYDs to add=["JR-01-MJ"+"JR-01-MN"]
3496 *%-----|-----|
3497 CONTINUOUS STANDHYD NHYD=["JR-02"], DT=[1]min, AREA=[1.59](ha), XIMP=[0.64],
TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3498 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3499 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3500 Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
LGI=[102.956](m), MNI=[0.013], SCI=[0](min),
3501 Continuous simulation parameters:

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3502 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
      END=-1
3503 *%-----|-----|
3504 COMPUTE DUALHYD NHYDin=["JR-02"], CINLET=[0.153](cms), NINLET=[1],
3505 MajNHYD=["JR-02-MJ"]
3506 MinNHYD=["JR-02-MN"]
3507 TMJSTO=[153](cu-m)
3508 *%-----|-----|
3509 ADD HYD NHYDsum=["JR-02-S"], NHYDs to add=["JR-02-MJ"+"JR-02-MN"]
3510 *%-----|-----|
3511 *#*****|*****|
3512 *# Catchment FRASER
3513 *# - To Fraser-Clarke drain (north of the Jock)
3514 *# - Developed land with assumed 43% imp.
3515 *# - 2020-12-17 Change Fraser area to be 35.1 as measured from QGIS
3516 *# - 2020-12-17 All Fraser is undeveloped (Nashyd)
3517 *#*****|*****|
3518 CONTINUOUS NASHYD NHYD=["FRASER-DRN"], DT=[1]min, AREA=[13.65](ha),
3519 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
3520 N=[3], TP=[0.4258]hrs,
3521 Continuous simulation parameters:
3522 IaREcper=[4](hrs),
3523 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3524 InterEventTime=[12](hrs)
3525 Baseflow simulation parameters:
3526 BaseFlowOption=[1],
3527 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
3528 VHydCond=[0.055](mm/hr), END=-1
3529 *
3530 CONTINUOUS STANDHYD NHYD=["FRASER-D"], DT=[1]min, AREA=[21.61](ha),
3531 XIMP=[0.585], TIMP=[0.585], DWF=[0](cms), LOSS=[2],
3532 SCS curve number CN=[80],
3533 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3534 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3535 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3536 LGI=[379.561](m), MNI=[0.013], SCI=[0](min),
3537 Continuous simulation parameters:
3538 IaREcper=[4](hrs), IaREcimp=[4](hrs),
3539 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3540 InterEventTime=[18](hrs), END=-1
3541 *%-----|-----|
3542 COMPUTE DUALHYD NHYDin=["FRASER-D"], CINLET=[2.281](cms), NINLET=[1],
3543 MajNHYD=["FRASER-J"]
3544 MinNHYD=["FRASER-N"]
3545 TMJSTO=[9999999](cu-m)
3546 *%-----|-----|
3547 ADD HYD NHYDsum=["FRASER-S"], NHYDs to add=["FRASER-J"+"FRASER-N"]
3548 *%-----|-----|
3549 *ROUTE RESERVOIR NHYDout=["MS_P20"], NHYDin=["FRASER"],
3550 * RDT=[1](min),
3551 * TABLE of ( OUTFLOW-STORAGE ) values
3552 * (cms) - (ha-m)
3553 * [ 0.0 , 0.0 ]
3554 * [ 0.04 , 0.36 ]
3555 * [ -1 , -1 ] (max twenty pts)
3556 * NHYDovf=["P20-OVF"]
3557 *%-----|-----|
3558 ADD HYD NHYDsum=["4241"], NHYDs to
add=["KB-Pond3"+"S-1-B"+"FRASER-DRN"+"FRASER-S"+"N_KB"+"FC-01-S"+"FC-02-S"+"FC-03-S"]
3559 *%-----|-----|
3560 SAVE HYD NHYD=["4241"], # OF PCYCLES=[-1], ICASEsh=[1]
3561 HYD_COMMENT=["Total Flows at Ken-Burnett Outlet"]
3562 *%-----|-----|
3563 *# Hydrograph from Node Ken-Burnett to station 3633
3564 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4241
3565 *#

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3566 ROUTE CHANNEL      NHYDout=["4241-out"],NHYDin=["4241"], RDT=[1](min),
3567 CHLGTH=[294](m), CHSLOPE=[0.1088](%), FPSLOPE=[0.1088](%),
3568 SECNUM=[1.0], NSEG=[3]
3569 ( SEGROUGH, SEGDIST (m))=[0.05, -20.12
3570 -0.035, 45.26
3571 0.05, 403.84] NSEG times
3572 ( DISTANCE (m), ELEVATION (m))=[]
3573 [-909.72, 95 ]
3574 [-907.09, 94.5 ]
3575 [-904.65, 94 ]
3576 [-902.26, 93.5 ]
3577 [-44.51, 91.5 ]
3578 [-25.1, 91.5 ]
3579 [-20.98, 91 ]
3580 [-20.61, 90.5 ]
3581 [-20.12, 90 ]
3582 [-6.13, 87.26 ]
3583 [17.51, 86.56 ]
3584 [31.37, 87.2 ]
3585 [45.26, 90 ]
3586 [50.41, 90.5 ]
3587 [63.06, 91 ]
3588 [134.5, 91.5 ]
3589 [190.63, 92 ]
3590 [251.98, 92.5 ]
3591 [321.32, 93.5 ]
3592 [403.84, 95 ]
3593 *%-----|-----
3594 ADD HYD          NHYDsum=["SN_KB"], NHYDs to
add=["4241-out"+"FC-04-S"+"JR-01-S"+"JR-02-S"]
3595 *%-----|-----
3596 SAVE HYD        NHYD=["SN_KB"], # OF PCYCLES=[-1], ICASEsh=[1]
3597 HYD_COMMENT=["Total Flows before Station 3633"]
3598 *%-----|-----
3599 *# Hydrograph from Station 3633 to Node Todd
3600 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 3633
3601 *# JFSA 2021-02-26 change the channel length (at station 3633) from 650m to 608m and
change the slope from 0.0498% to 0.24671%. That is because of adding station 4241
between station 4534 and station 3633
3602 *#
3603 ROUTE CHANNEL   NHYDout=["N_TO"], NHYDin=["SN_KB"], RDT=[1](min),
3604 CHLGTH=[608](m), CHSLOPE=[0.24671](%), FPSLOPE=[0.24671](%),
3605 SECNUM=[1.0], NSEG=[3]
3606 ( SEGROUGH, SEGDIST (m))=[0.05, -23.74
3607 -0.035, 23.74
3608 0.05, 26.50] NSEG times
3609 ( DISTANCE (m), ELEVATION (m))=[]
3610 -29.24, 91.0
3611 -27.41, 90.5
3612 -25.64, 90
3613 -23.74, 89.5
3614 -22, 89.26
3615 -20, 88.51
3616 -19, 88.32
3617 -15, 88.1
3618 -10, 88.11
3619 -5, 88.17
3620 0, 88.27
3621 5, 88.19
3622 10, 88.06
3623 15, 88.48
3624 16, 88.7
3625 23.74, 89.5
3626 24.68, 90
3627 25.57, 90.5
3628 26.50, 91.0

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3629 * [-29.24, 91]
3630 * [-27.41, 90.5]
3631 * [-25.64, 90]
3632 * [-23.74, 89.5]
3633 * [-22, 89.26]
3634 * [-20, 88.51]
3635 * [-19, 88.32]
3636 * [-15, 88.1]
3637 * [-10, 88.11]
3638 * [-5, 88.17]
3639 * [0, 88.27]
3640 * [5, 88.19]
3641 * [10, 88.06]
3642 * [15, 88.48]
3643 * [16, 88.7]
3644 * [23.74, 89.5]
3645 * [24.68, 90]
3646 * [25.57, 90.5]
3647 *%-----|-----|
3648 *#*****|*****|
3649 *# Catchment Greenbank
3650 *# - To Greenbank Drain (south of the Jock)
3651 *# - JFSA 2021-01-18 add Greenbank pond as per JFSA, P598(06)-15, June 2016
3652 *# - JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GIS measurements
3653 *#*****|*****|
3654 CONTINUOUS STANDHYD NHYD=["Greenbank"], DT=[1]min, AREA=[36.6](ha),
3655 XIMP=[0.639], TIMP=[0.682], DWF=[0](cms), LOSS=[2],
3656 SCS curve number CN=[77],
3657 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3658 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3659 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3660 LGI=[493.96](m), MNI=[0.013], SCI=[0](min),
3661 Continuous simulation parameters:
3662 IaRECper=[4](hrs), IaRECimp=[4](hrs),
3663 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3664 InterEventTime=[18](hrs), END=-1
3665 *%-----|-----|
3666 ROUTE RESERVOIR NHYDout=["GreenB_MN"], NHYDin=["Greenbank"],
3667 RDT=[1](min),
3668 TABLE of ( OUTFLOW-STORAGE ) values
3669 (cms) - (ha-m)
3670 [ 0.0 , 0.0 ]
3671 [ 0.033 , 0.084 ]
3672 [ 0.039 , 0.201 ]
3673 [ 0.113 , 0.292 ]
3674 [ 0.237 , 0.386 ]
3675 [ 0.382 , 0.484 ]
3676 [ 0.539 , 0.585 ]
3677 [ 0.7 , 0.692 ]
3678 [ 0.86 , 0.804 ]
3679 [ 4.684 , 0.922 ]
3680 [ 11.539 , 1.052 ]
3681 [ 20.867 , 1.168 ]
3682 [ 103.616 , 1.974 ]
3683 [ -1 , -1 ] (max twenty pts)
3684 NHYDovf=["GreenB_MJ"],
3685 *%-----|-----|
3686 *%-----|-----|
3687 ADD HYD NHYDsum=["GreenB"], NHYDs to add=["N_TO"+"GreenB_MJ"+"GreenB_MN"]
3688 *%-----|-----|
3689 SAVE HYD NHYD=["GreenB"], # OF PCYCLES=[-1], ICASEsh=[1]
3690 HYD_COMMENT=["Total Flows at Greenbank Drain"]
3691 *%-----|-----|
3692 *#*****|*****|
3693 *# Catchment TODD
3694 *# - To Todd Drain (south of the Jock)

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3695 *# - Subdivision with 43% imp. as per Barrhaven South MSS
3696 *# - 2020-11-30 increase imp. based on P598(04)-11
3697 *# - 2020-11-30 update TODD Tributary Drainage Area to = 146.015 ha based on
P598(04)-11
3698 *# - 2020-11-30 split TODD Drainage Area to MAJOR, MINOR, POND and ALL
3699 *#*****
3700 *# - JFSA 2021-01-19 add "TODD_MN1" as part of Clarke("W_CLAR_MJ") and remove it
from Todd
3701 *CONTINUOUS STANDHYD NHYD=["TODD_MN1"], DT=[1]min, AREA=[1.772](ha),
3702 * XIMP=[0.53], TIMP=[0.57], DWF=[0](cms), LOSS=[2],
3703 * SCS curve number CN=[77],
3704 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3705 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3706 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3707 * LGI=[108.689](m), MNI=[0.013], SCI=[0](min),
3708 * Continuous simulation parameters:
3709 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
3710 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3711 * InterEventTime=[18](hrs), END=-1
3712 *%-----|-----
3713 CONTINUOUS STANDHYD NHYD=["TODD_MN2"], DT=[1]min, AREA=[2.1](ha),
3714 XIMP=[0.53], TIMP=[0.57], DWF=[0](cms), LOSS=[2],
3715 SCS curve number CN=[77],
3716 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3717 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3718 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3719 LGI=[118.322](m), MNI=[0.013], SCI=[0](min),
3720 Continuous simulation parameters:
3721 IaRECper=[4](hrs), IaRECimp=[4](hrs),
3722 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3723 InterEventTime=[18](hrs), END=-1
3724 *%-----|-----
3725 CONTINUOUS STANDHYD NHYD=["TODD_MN3"], DT=[1]min, AREA=[0.117](ha),
3726 XIMP=[0.53], TIMP=[0.57], DWF=[0](cms), LOSS=[2],
3727 SCS curve number CN=[77],
3728 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3729 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3730 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3731 LGI=[27.928](m), MNI=[0.013], SCI=[0](min),
3732 Continuous simulation parameters:
3733 IaRECper=[4](hrs), IaRECimp=[4](hrs),
3734 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3735 InterEventTime=[18](hrs), END=-1
3736 *%-----|-----
3737 CONTINUOUS STANDHYD NHYD=["TODD_MJ"], DT=[1]min, AREA=[30.230](ha),
3738 XIMP=[0.52], TIMP=[0.64], DWF=[0](cms), LOSS=[2],
3739 SCS curve number CN=[77],
3740 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3741 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3742 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3743 LGI=[448.925](m), MNI=[0.013], SCI=[0](min),
3744 Continuous simulation parameters:
3745 IaRECper=[4](hrs), IaRECimp=[4](hrs),
3746 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3747 InterEventTime=[18](hrs), END=-1
3748 *%-----|-----
3749 * -JFSA, 2021-01-19 update "TODD_ALL" area from 108.741 ha to 112.908 ha based on
GIS measurements (148.41-30.23-0.117-2.1-3.055=112.908 ha)
3750 CONTINUOUS STANDHYD NHYD=["TODD_ALL"], DT=[1]min, AREA=[112.908](ha),
3751 XIMP=[0.52], TIMP=[0.57], DWF=[0](cms), LOSS=[2],
3752 SCS curve number CN=[77],
3753 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3754 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3755 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3756 LGI=[867.594](m), MNI=[0.013], SCI=[0](min),
3757 Continuous simulation parameters:

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3758 IaREcper=[4](hrs), IaREcimp=[4](hrs),
3759 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3760 InterEventTime=[18](hrs), END=-1
3761 *%-----|-----
3762 CONTINUOUS STANDHYD NHYD=["TODD_P"], DT=[1]min, AREA=[3.055](ha),
3763 XIMP=[0.63], TIMP=[0.63], DWF=[0](cms), LOSS=[2],
3764 SCS curve number CN=[77],
3765 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3766 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3767 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3768 LGI=[142.712](m), MNI=[0.013], SCI=[0](min),
3769 Continuous simulation parameters:
3770 IaREcper=[4](hrs), IaREcimp=[4](hrs),
3771 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3772 InterEventTime=[18](hrs), END=-1
3773 *%-----|-----
3774 *%-----|-----
3775 * -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"
and its parameters remain the same.
3776 *CONTINUOUS STANDHYD NHYD=["TODD_DEVL"], DT=[1]min, AREA=[15.87](ha),
3777 * XIMP=[0.63], TIMP=[0.63], DWF=[0](cms), LOSS=[2],
3778 * SCS curve number CN=[77],
3779 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3780 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3781 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3782 * LGI=[325.27](m), MNI=[0.013], SCI=[0](min),
3783 * Continuous simulation parameters:
3784 * IaREcper=[4](hrs), IaREcimp=[4](hrs),
3785 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3786 * InterEventTime=[18](hrs), END=-1
3787 *%-----|-----
3788 * -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
is called "corr2" and its parameters remain the same.
3789 *CONTINUOUS NASHYD NHYD=["TODD_UnD"], DT=[1]min, AREA=[12.47](ha),
3790 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
3791 * N=[3], TP=[1.10]hrs,
3792 * Continuous simulation parameters:
3793 * IaREcper=[4](hrs),
3794 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3795 * InterEventTime=[12](hrs)
3796 * Baseflow simulation parameters:
3797 * BaseFlowOption=[1] ,
3798 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
3799 * VHydCond=[0.055](mm/hr), END=-1
3800 *%-----|-----
3801 *# 5-Year + 12% Capture
3802 *COMPUTE DUALHYD NHYDin=["TODD_MJ"], CINLET=[3.314](cms), NINLET=[1],
3803 * MajNHYD=["TODD_MJj"]
3804 * MinNHYD=["TODD_MJn"]
3805 * TMJSTO=[0.1](cu-m)
3806 ROUTE RESERVOIR NHYDout=["TODD_MJn"],NHYDin=["TODD_MJ"] ,
3807 RDT=[1](min),
3808 TABLE of ( OUTFLOW-STORAGE ) values
3809 (cms) - (ha-m)
3810 [ 0.0 , 0.0 ]
3811 [ 3.314 , 0.0001 ]
3812 [ -1 , -1 ] (max twenty pts)
3813 NHYDovf=["TODD_MJj"] ,
3814 *%-----|-----
3815 *# 5-Year + 12% Capture
3816 *COMPUTE DUALHYD NHYDin=["TODD_MN1"], CINLET=[0.227](cms), NINLET=[1],
3817 * MajNHYD=["TODD_MN1j"]
3818 * MinNHYD=["TODD_MN1n"]
3819 * TMJSTO=[0.1](cu-m)
3820 *ROUTE RESERVOIR NHYDout=["TODD_MN1n"],NHYDin=["TODD_MN1"] ,

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3821 *          RDT=[1](min),
3822 *          TABLE of ( OUTFLOW-STORAGE ) values
3823 *              (cms) - (ha-m)
3824 *              [ 0.0 , 0.0 ]
3825 *              [ 0.227 , 0.0001 ]
3826 *              [ -1 , -1 ] (max twenty pts)
3827 *          NHYDovf=["TODD_MN1j"] ,
3828 *%-----|-----|
3829 *COMPUTE DUALHYD  NHYDin=["TODD_MN2"], CINLET=[0.268](cms), NINLET=[1],
3830 *              MajNHYD=["TODD_MN2j"]
3831 *              MinNHYD=["TODD_MN2n"]
3832 *              TMJSTO=[0.1](cu-m)
3833 ROUTE RESERVOIR NHYDout=["TODD_MN2n"] ,NHYDin=["TODD_MN2"] ,
3834 RDT=[1](min),
3835          TABLE of ( OUTFLOW-STORAGE ) values
3836              (cms) - (ha-m)
3837              [ 0.0 , 0.0 ]
3838              [ 0.268 , 0.0001 ]
3839              [ -1 , -1 ] (max twenty pts)
3840          NHYDovf=["TODD_MN2j"] ,
3841 *%-----|-----|
3842 *COMPUTE DUALHYD  NHYDin=["TODD_MN3"], CINLET=[0.016](cms), NINLET=[1],
3843 *              MajNHYD=["TODD_MN3j"]
3844 *              MinNHYD=["TODD_MN3n"]
3845 *              TMJSTO=[0.1](cu-m)
3846 ROUTE RESERVOIR NHYDout=["TODD_MN3n"] ,NHYDin=["TODD_MN3"] ,
3847 RDT=[1](min),
3848          TABLE of ( OUTFLOW-STORAGE ) values
3849              (cms) - (ha-m)
3850              [ 0.0 , 0.0 ]
3851              [ 0.016 , 0.0001 ]
3852              [ -1 , -1 ] (max twenty pts)
3853          NHYDovf=["TODD_MN3j"] ,
3854 *%-----|-----|
3855 *          -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
major system from A2 can be added to Todd
3856 CONTINUOUS STANDHYD NHYD=["A2"], DT=[1]min, AREA=[25.5](ha),
3857 XIMP=[0.42], TIMP=[0.52], DWF=[0](cms), LOSS=[2],
3858 SCS curve number CN=[75],
3859 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3860 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3861 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3862 LGI=[566](m), MNI=[0.013], SCI=[0](min),
3863 Continuous simulation parameters:
3864 IaRECper=[4](hrs), IaRECimp=[4](hrs),
3865 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3866 InterEventTime=[18](hrs), END=-1
3867 *%-----|-----|
3868 COMPUTE DUALHYD NHYDin=["A2"], CINLET=[1.818](cms), NINLET=[1],
3869 MajNHYD=["A2-MJ"]
3870 MinNHYD=["A2-MN"]
3871 TMJSTO=[924](cu-m)
3872 *%-----|-----|
3873 ADD HYD NHYDsum=["TODD"], NHYDs to
add=["TODD_MN2n"+"TODD_MN3n"+"TODD_MJj"+"TODD_P"+"TODD_ALL"+"W_CLAR_MJn"]
3874 *%-----|-----|
3875 SAVE HYD NHYD=["TODD"], # OF PCYCLES=[-1], ICASEsh=[1]
3876 HYD_COMMENT=["Total Flows at Todd Drain"]
3877 *%-----|-----|
3878 *#*****
3879 *# Todd Pond 3
3880 *# - Rating curve obtained from Barrhaven South MSS modeling
3881 *# - stantec 2007, Tributary Drainage Area to MSS Pond 3 = 193 ha
3882 *#*****
3883 ROUTE RESERVOIR NHYDout=["MS_P3"], NHYDin=["TODD"],
3884 RDT=[1](min),

```

```

3885             TABLE of ( OUTFLOW-STORAGE ) values
3886                 (cms) - (ha-m)
3887                 [ 0.0 , 0.0 ]
3888                 [ 0.014 , 0.155 ]
3889                 [ 0.048 , 0.394 ]
3890                 [ 0.061 , 0.56 ]
3891                 [ 0.08 , 0.909 ]
3892                 [ 0.088 , 1.089 ]
3893                 [ 0.109 , 1.652 ]
3894                 [ 0.118 , 1.952 ]
3895                 [ 0.122 , 2.099 ]
3896                 [ 1.972 , 2.269 ]
3897                 [ 9.135 , 2.598 ]
3898                 [ 15.608 , 2.826 ]
3899                 [ 19.256 , 2.942 ]
3900                 [ 27.282 , 3.181 ]
3901                 [ 40.957 , 3.55 ]
3902                 [ 56.372 , 3.929 ]
3903                 [ 73.349 , 4.317 ]
3904                 [ 85.469 , 4.579 ]
3905                 [ 104.771 , 4.977 ]
3906                 [ -1 , -1 ] (max twenty pts)
3907             NHYDovf=["P3-OVF"]
3908 *%-----|-----|
3909 ADD HYD           NHYDsum=["SN_TO"], NHYDs to
add=["GreenB"+"MS_P3"+"P3-OVF"+"TODD_MN2j"+"A2-MJ"]
3910 *%-----|-----|
3911 SAVE HYD        NHYD=["SN_TO"], # OF PCYCLES=[-1], ICASEsh=[1]
3912             HYD_COMMENT=["Total Flows at Todd Drain"]
3913 *%-----|-----|
3914 *#
3915 *# Hydrograph from Todd Drain routed to Corrigan Drain
3916 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
3917 *# 2021-02-19 Change the slope from 0.033 % (as per Stantec Report 2007) to 0.05 % so
the model will be more stable and give reasonable results. It is justifiable as ROUTE
CHANNELs aren't well suited to really flat slopes.
3918 *
3919 ROUTE CHANNEL   NHYDout=["N_TO"] ,NHYDin=["SN_TO"] ,
3920             RDT=[1](min),
3921             CHLGTH=[280](m),  CHSLOPE=[0.05](%),
3922             FPSLOPE=[0.05](%),
3923             SECNUM=[1.0],      NSEG=[3]
3924             ( SEGROUGH, SEGDIST (m))=
3925             [0.075,-17.72
3926             -0.045,17.72
3927             0.075,80.62] NSEG times
3928             ( DISTANCE (m), ELEVATION (m))=
3929             [-83.32, 90.00]
3930             [-81.36, 89.50]
3931             [-79.12, 89.00]
3932             [-76.13, 88.50]
3933             [-20.46, 88.00]
3934             [-19.36, 87.50]
3935             [-18.51, 87.00]
3936             [-17.72, 86.50]
3937             [-11.95, 85.24]
3938             [-0.11, 85.12]
3939             [11.49, 85.20]
3940             [17.72, 86.50]
3941             [19.74, 87.00]
3942             [21.22, 87.50]
3943             [22.68, 88.00]
3944             [24.28, 88.50]
3945             [26.79, 89.00]
3946             [71.98, 90.00]
3947             [80.62, 90.50]

```



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3948 *%-----|-----|
3949 SAVE HYD NHYD=["N_TO"], # OF PCYCLES=[-1], ICASEsh=[1]
3950 HYD_COMMENT=["Total inflows at Station 2462"]
3951 *%-----|-----|
3952 *#*****|-----|
3953 *# Catchment CORRIG
3954 *# - To Corrigan Drain (south of the Jock)
3955 *# - Primarily Developed (medium density)
3956 *# - JFSA JAN 2021, add Corrigan subcatchments as per IBI, July 2008
3957 *#*****|-----|
3958 *ROUTE RESERVOIR NHYDout=["MS_P1"], NHYDin=["CORRIG"],
3959 * RDT=[1](min),
3960 * TABLE of ( OUTFLOW-STORAGE ) values
3961 * (cms) - (ha-m)
3962 * [ 0.0 , 0.0 ]
3963 * [ 0.06 , 0.58]
3964 * [ -1 , -1 ] (max twenty pts)
3965 * NHYDovf=["P1-OVF"]
3966 *%-----|-----|
3967 *ADD HYD NHYDsum=["SN_CO"], NHYDs to add=["N_TO"+"P1-OVF"+"MS_P1"]
3968 *%-----|-----|
3969 *SAVE HYD NHYD=["SN_CO"], # OF PCYCLES=[-1], ICASEsh=[1]
3970 * HYD_COMMENT=["Total Flows at Corrigan Drain"]
3971 *%-----|-----|
3972 * -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"
and its parameters remain the same.
3973 CONTINUOUS STANDHYD NHYD=["corr1"], DT=[1]min, AREA=[15.87](ha),
3974 XIMP=[0.63], TIMP=[0.63], DWF=[0](cms), LOSS=[2],
3975 SCS curve number CN=[77],
3976 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3977 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3978 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3979 LGI=[325.27](m), MNI=[0.013], SCI=[0](min),
3980 Continuous simulation parameters:
3981 IaRECper=[4](hrs), IaRECimp=[4](hrs),
3982 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3983 InterEventTime=[18](hrs), END=-1
3984 *%-----|-----|
3985 * -JFSA 2021-02-23 add DUALHYD for "corr1". "corr1" DUALHYD Parameters are the
same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to "corr1".
3986 * At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for
Al-Corrig
3987 COMPUTE DUALHYD NHYDin=["corr1"], CINLET=[1.818](cms), NINLET=[1],
3988 MaJNHYD=["corr1-MJ"]
3989 MinNHYD=["corr1-MN"]
3990 TMJSTO=[924](cu-m)
3991 *%-----|-----|
3992 * -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
is called "corr2" and its parameters remain the same.
3993 CONTINUOUS NASHYD NHYD=["corr2"], DT=[1]min, AREA=[12.47](ha),
3994 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
3995 N=[3], TP=[1.10]hrs,
3996 Continuous simulation parameters:
3997 IaRECper=[4](hrs),
3998 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3999 InterEventTime=[12](hrs)
4000 Baseflow simulation parameters:
4001 BaseFlowOption=[1] ,
4002 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4003 VHydCond=[0.055](mm/hr), END=-1
4004 *%-----|-----|
4005 * -JFSA 2021-01-19 change Al-Corrig to be developed as per geottawa website and
apply the parameters of A2, the nearest sub-catchment to Al-Corrig, LGI is calculated
based on Al-Corrig area
4006 * -JFSA 2021-01-19 update all Corrigan areas based on GIS measurements, and keep

```

LGI as it is from Corrigan Report, IBI Group, 2008 because LGI calculated is less than LGI from the Corrigan Report

```
4007 CONTINUOUS STANDHYD NHYD=["A1-Corrig"], DT=[1]min, AREA=[15.75](ha),
4008 XIMP=[0.42], TIMP=[0.52], DWF=[0](cms), LOSS=[2],
4009 SCS curve number CN=[75],
4010 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4011 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4012 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4013 LGI=[324.037](m), MNI=[0.013], SCI=[0](min),
4014 Continuous simulation parameters:
4015 IaREcper=[4](hrs), IaREcimp=[4](hrs),
4016 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4017 InterEventTime=[18](hrs), END=-1
4018 *
4019 * -JFSA 2021-01-25 add DUALHYD for A1-Corrig. A1-Corrig DUALHYD Parameters are the
4020 * same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to A1-Corrig.
4021 * At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for
4022 A1-Corrig
4023 COMPUTE DUALHYD NHYDin=["A1-Corrig"], CINLET=[1.818](cms), NINLET=[1],
4024 MajNHYD=["A1-MJ"]
4025 MinNHYD=["A1-MN"]
4026 TMJSTO=[924](cu-m)
4027 *%-----|-----|
4028 *CONTINUOUS NASHYD NHYD=["A1-Corrig"], DT=[1]min, AREA=[15.75](ha),
4029 * DWF=[0](cms), CN/C=[66], IA=[2.5](mm),
4030 * N=[3.0], TP=[0.36]hrs,
4031 * Continuous simulation parameters:
4032 * IaREcper=[4](hrs),
4033 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4034 * InterEventTime=[12](hrs)
4035 * Baseflow simulation parameters:
4036 * BaseFlowOption=[1] ,
4037 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4038 * VHydCond=[0.055](mm/hr), END=-1
4039 *%-----|-----|
4040 CONTINUOUS NASHYD NHYD=["B1"], DT=[1]min, AREA=[2.77](ha),
4041 DWF=[0](cms), CN/C=[56], IA=[2.5](mm),
4042 N=[3.0], TP=[0.23]hrs,
4043 Continuous simulation parameters:
4044 IaREcper=[4](hrs),
4045 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4046 InterEventTime=[12](hrs)
4047 Baseflow simulation parameters:
4048 BaseFlowOption=[1] ,
4049 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4050 VHydCond=[0.055](mm/hr), END=-1
4051 *%-----|-----|
4052 CONTINUOUS STANDHYD NHYD=["A4"], DT=[1]min, AREA=[1.27](ha),
4053 XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
4054 SCS curve number CN=[75],
4055 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4056 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4057 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4058 LGI=[253](m), MNI=[0.013], SCI=[0](min),
4059 Continuous simulation parameters:
4060 IaREcper=[4](hrs), IaREcimp=[4](hrs),
4061 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4062 InterEventTime=[18](hrs), END=-1
4063 *%-----|-----|
4064 COMPUTE DUALHYD NHYDin=["A4"], CINLET=[0.405](cms), NINLET=[1],
4065 MajNHYD=["A4-MJ"]
4066 MinNHYD=["A4-MN"]
4067 TMJSTO=[68](cu-m)
4068 *%-----|-----|
4069 ADD HYD NHYDsum=["MH101"], NHYDs to
4070 add=["A1-MJ"+"A1-MN"+"corr1-MJ"+"corr1-MN"+"corr2"+"B1"+"A4-MN"]
```

```

4068 *%-----|-----|
4069 SAVE HYD      NHYD=["MH101"], # OF PCYCLES=[-1], ICASEsh=[1]
4070              HYD_COMMENT=["Total Flows at MH101"]
4071 *%-----|-----|
4072 ROUTE PIPE    PTYPE=[1]circ, NHYDout=["101-102"], RNUMBER=[1.0], PDIAM=[1050](mm),
4073              PLNGTH=[368](m), PROUGH=[0.013], PSLOPE=[0.0054](m/m),
              NHYDin=["MH101"], RDT=[1]
4074 *%-----|-----|
4075 *      -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
major system from A2 can be added to Todd
4076 *CONTINUOUS STANDHYD NHYD=["A2"], DT=[1]min, AREA=[25.5](ha),
4077 *              XIMP=[0.42], TIMP=[0.52], DWF=[0](cms), LOSS=[2],
4078 *              SCS curve number CN=[75],
4079 *              Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4080 *              LGP=[40](m), MNP=[0.25], SCP=[0](min),
4081 *              Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4082 *              LGI=[566](m), MNI=[0.013], SCI=[0](min),
4083 *              Continuous simulation parameters:
4084 *              IaRECper=[4](hrs), IaRECimp=[4](hrs),
4085 *              SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4086 *              InterEventTime=[18](hrs), END=-1
4087 *%-----|-----|
4088 *COMPUTE DUALHYD  NHYDin=["A2"], CINLET=[1.818](cms), NINLET=[1],
4089 *              MaJNHYD=["A2-MJ"]
4090 *              MinNHYD=["A2-MN"]
4091 *              TMJSTO=[924](cu-m)
4092 *%-----|-----|
4093 ADD HYD      NHYDsum=["MH102"], NHYDs to add=["A2-MN"+"101-102"]
4094 *%-----|-----|
4095 SAVE HYD      NHYD=["MH102"], # OF PCYCLES=[-1], ICASEsh=[1]
4096              HYD_COMMENT=["Total Flows at MH102"]
4097 *%-----|-----|
4098 CONTINUOUS STANDHYD NHYD=["A5"], DT=[1]min, AREA=[1.6](ha),
4099 *              XIMP=[0.71], TIMP=[0.71], DWF=[0](cms), LOSS=[2],
4100 *              SCS curve number CN=[75],
4101 *              Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4102 *              LGP=[40](m), MNP=[0.25], SCP=[0](min),
4103 *              Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4104 *              LGI=[300](m), MNI=[0.013], SCI=[0](min),
4105 *              Continuous simulation parameters:
4106 *              IaRECper=[4](hrs), IaRECimp=[4](hrs),
4107 *              SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4108 *              InterEventTime=[18](hrs), END=-1
4109 *%-----|-----|
4110 ADD HYD      NHYDsum=["A5T"], NHYDs to add=["A4-MJ"+"A5"]
4111 *%-----|-----|
4112 COMPUTE DUALHYD  NHYDin=["A5T"], CINLET=[0.357](cms), NINLET=[1],
4113 *              MaJNHYD=["A5-MJ"]
4114 *              MinNHYD=["A5-MN"]
4115 *              TMJSTO=[60](cu-m)
4116 *%-----|-----|
4117 *      -JFSA Jan. 2021, A3 is a part of Todd so it is removed
4118 *      -JFSA Jan. 2021, "A2-MJ" added to "Todd"
4119 *CONTINUOUS STANDHYD NHYD=["A3"], DT=[1]min, AREA=[18.4](ha),
4120 *              XIMP=[0.58], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
4121 *              SCS curve number CN=[75],
4122 *              Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4123 *              LGP=[40](m), MNP=[0.25], SCP=[0](min),
4124 *              Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4125 *              LGI=[450](m), MNI=[0.013], SCI=[0](min),
4126 *              Continuous simulation parameters:
4127 *              IaRECper=[4](hrs), IaRECimp=[4](hrs),
4128 *              SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4129 *              InterEventTime=[18](hrs), END=-1
4130 *%-----|-----|
4131 *ADD HYD      NHYDsum=["A3-A2MJ"], NHYDs to add=["A2-MJ"+"A3"]

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```

4132 *%-----|-----|
4133 *COMPUTE DUALHYD   NHYDin=["A3-A2MJ"], CINLET=[2.208](cms), NINLET=[1],
4134 *                   MajNHYD=["A3R-MJ"]
4135 *                   MinNHYD=["A3R-MN"]
4136 *                   TMJSTO=[908](cu-m)
4137 *%-----|-----|
4138 ROUTE PIPE         PTYPE=[1]circ, NHYDout=["102-103"], RNUMBER=[1.0], PDIAM=[1500](mm),
4139                   PLNGTH=[504](m), PROUGH=[0.013], PSLOPE=[0.0028](m/m),
                   NHYDin=["MH102"], RDT=[1]
4140 *%-----|-----|
4141 ADD HYD            NHYDsum=["MH103"], NHYDs to add=["102-103"+"A5-MN"]
4142 *%-----|-----|
4143 SAVE HYD          NHYD=["MH103"], # OF PCYCLES=[-1], ICASEsh=[1]
4144                   HYD_COMMENT=["Total Flows at MH103"]
4145 *%-----|-----|
4146 ROUTE PIPE         PTYPE=[1]circ, NHYDout=["103-104"], RNUMBER=[1.0], PDIAM=[1650](mm),
4147                   PLNGTH=[438](m), PROUGH=[0.013], PSLOPE=[0.0046](m/m),
                   NHYDin=["MH103"], RDT=[1]
4148 *%-----|-----|
4149 CONTINUOUS STANDHYD NHYD=["A6"], DT=[1]min, AREA=[1.56](ha),
4150                   XIMP=[0.71], TIMP=[0.71], DWF=[0](cms), LOSS=[2],
4151                   SCS curve number CN=[75],
4152                   Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4153                   LGP=[40](m), MNP=[0.25], SCP=[0](min),
4154                   Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4155                   LGI=[280](m), MNI=[0.013], SCI=[0](min),
4156                   Continuous simulation parameters:
4157                   IaRECper=[4](hrs), IaRECimp=[4](hrs),
4158                   SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4159                   InterEventTime=[18](hrs), END=-1
4160 *%-----|-----|
4161 ADD HYD            NHYDsum=["A6T"], NHYDs to add=["A5-MJ"+"A6"]
4162 *%-----|-----|
4163 COMPUTE DUALHYD   NHYDin=["A6T"], CINLET=[0.357](cms), NINLET=[1],
4164 *                   MajNHYD=["A6-MJ"]
4165 *                   MinNHYD=["A6-MN"]
4166 *                   TMJSTO=[60](cu-m)
4167 *%-----|-----|
4168 *   -JFSA Jan. 2021, A7-corrig is a part of Todd so it is removed
4169 *CONTINUOUS STANDHYD NHYD=["A7-corrig"], DT=[1]min, AREA=[11.8](ha),
4170 *                   XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4171 *                   SCS curve number CN=[75],
4172 *                   Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4173 *                   LGP=[40](m), MNP=[0.25], SCP=[0](min),
4174 *                   Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4175 *                   LGI=[438](m), MNI=[0.013], SCI=[0](min),
4176 *                   Continuous simulation parameters:
4177 *                   IaRECper=[4](hrs), IaRECimp=[4](hrs),
4178 *                   SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4179 *                   InterEventTime=[18](hrs), END=-1
4180 *%-----|-----|
4181 *ADD HYD            NHYDsum=["A7-A3RMJ"], NHYDs to add=["A3R-MJ"+"A7-corrig"]
4182 *%-----|-----|
4183 *COMPUTE DUALHYD   NHYDin=["A7-A3RMJ"], CINLET=[1.003](cms), NINLET=[1],
4184 *                   MajNHYD=["A7R-MJ"]
4185 *                   MinNHYD=["A7R-MN"]
4186 *                   TMJSTO=[496](cu-m)
4187 *%-----|-----|
4188 ADD HYD            NHYDsum=["MH104"], NHYDs to add=["A6-MN"+"103-104"+"TODD_MJn"]
4189 *%-----|-----|
4190 SAVE HYD          NHYD=["MH104"], # OF PCYCLES=[-1], ICASEsh=[1]
4191                   HYD_COMMENT=["Total Flows at MH104"]
4192 *%-----|-----|
4193 CONTINUOUS STANDHYD NHYD=["B2"], DT=[1]min, AREA=[12.31](ha),
4194                   XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4195                   SCS curve number CN=[75],

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4196 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4197 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4198 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4199 LGI=[417](m), MNI=[0.013], SCI=[0](min),
4200 Continuous simulation parameters:
4201 IaREcper=[4](hrs), IaREcimp=[4](hrs),
4202 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4203 InterEventTime=[18](hrs), END=-1
4204 *%-----|
4205 COMPUTE DUALHYD NHYDin=["B2"], CINLET=[1.029](cms), NINLET=[1],
4206 MajNHYD=["B2-MJ"]
4207 MinNHYD=["B2-MN"]
4208 TMJSTO=[508](cu-m)
4209 *%-----|
4210 ROUTE PIPE PTYPE=[1]circ, NHYDout=["315-333"], RNUMBER=[1.0], PDIAM=[1200](mm),
4211 PLNGTH=[254](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["B2-MN"], RDT=[1]
4212 *%-----|
4213 CONTINUOUS STANDHYD NHYD=["B3"], DT=[1]min, AREA=[5.59](ha),
4214 XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4215 SCS curve number CN=[75],
4216 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4217 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4218 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4219 LGI=[345](m), MNI=[0.013], SCI=[0](min),
4220 Continuous simulation parameters:
4221 IaREcper=[4](hrs), IaREcimp=[4](hrs),
4222 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4223 InterEventTime=[18](hrs), END=-1
4224 *%-----|
4225 COMPUTE DUALHYD NHYDin=["B3"], CINLET=[0.459](cms), NINLET=[1],
4226 MajNHYD=["B3-MJ"]
4227 MinNHYD=["B3-MN"]
4228 TMJSTO=[227](cu-m)
4229 *%-----|
4230 ADD HYD NHYDsum=["MH333"], NHYDs to add=["B3-MN"+"315-333"]
4231 *%-----|
4232 SAVE HYD NHYD=["MH333"], # OF PCYCLES=[-1], ICASEsh=[1]
4233 HYD_COMMENT=["Total Flows at MH333"]
4234 *%-----|
4235 ROUTE PIPE PTYPE=[1]circ, NHYDout=["333-335"], RNUMBER=[1.0], PDIAM=[1200](mm),
4236 PLNGTH=[251](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["MH333"], RDT=[1]
4237 *%-----|
4238 ROUTE PIPE PTYPE=[1]circ, NHYDout=["335-338"], RNUMBER=[1.0], PDIAM=[1200](mm),
4239 PLNGTH=[185](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["333-335"], RDT=[1]
4240 *%-----|
4241 ROUTE PIPE PTYPE=[1]circ, NHYDout=["338-340"], RNUMBER=[1.0], PDIAM=[1350](mm),
4242 PLNGTH=[233](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["335-338"], RDT=[1]
4243 *%-----|
4244 CONTINUOUS STANDHYD NHYD=["B4"], DT=[1]min, AREA=[7.6](ha),
4245 XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4246 SCS curve number CN=[75],
4247 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4248 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4249 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4250 LGI=[388](m), MNI=[0.013], SCI=[0](min),
4251 Continuous simulation parameters:
4252 IaREcper=[4](hrs), IaREcimp=[4](hrs),
4253 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4254 InterEventTime=[18](hrs), END=-1
4255 *%-----|
4256 COMPUTE DUALHYD NHYDin=["B4"], CINLET=[0.655](cms), NINLET=[1],
4257 MajNHYD=["B4-MJ"]

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4258 MinNHYD=["B4-MN"]
4259 TMJSTO=[323](cu-m)
4260 *%-----|-----|
4261 ADD HYD NHYDsum=["MH340"], NHYDs to add=["338-340"+"B4-MN"]
4262 *%-----|-----|
4263 SAVE HYD NHYD=["MH340"], # OF PCYCLES=[-1], ICASEsh=[1]
4264 HYD_COMMENT=["Total Flows at MH340"]
4265 *%-----|-----|
4266 ROUTE PIPE PTYPE=[1]circ, NHYDout=["340-104"], RNUMBER=[1.0], PDIAM=[1650](mm),
4267 PLNGTH=[240](m), PROUGH=[0.013], PSLOPE=[0.0015](m/m),
NHYDin=["MH340"], RDT=[1]
4268 *%-----|-----|
4269 ADD HYD NHYDsum=["MH104T"], NHYDs to add=["340-104"+"MH104"]
4270 *%-----|-----|
4271 ROUTE PIPE PTYPE=[2]rect, NHYDout=["104-105"], RNUMBER=[1.0],
4272 PWIDTH=[2400](mm) by PHEIGHT=[2100](mm),
PLNGTH=[380](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["MH104T"], RDT=[1]
4273 *%-----|-----|
4274 CONTINUOUS STANDHYD NHYD=["B5"], DT=[1]min, AREA=[2.2](ha),
4275 XIMP=[0.57], TIMP=[0.57], DWF=[0](cms), LOSS=[2],
4276 SCS curve number CN=[75],
4277 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4278 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4279 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4280 LGI=[187](m), MNI=[0.013], SCI=[0](min),
4281 Continuous simulation parameters:
4282 IaREcper=[4](hrs), IaREcimp=[4](hrs),
4283 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4284 InterEventTime=[18](hrs), END=-1
4285 *%-----|-----|
4286 COMPUTE DUALHYD NHYDin=["B5"], CINLET=[0.260](cms), NINLET=[1],
4287 MajNHYD=["B5-MJ"]
4288 MinNHYD=["B5-MN"]
4289 TMJSTO=[250](cu-m)
4290 *%-----|-----|
4291 CONTINUOUS STANDHYD NHYD=["A8"], DT=[1]min, AREA=[0.96](ha),
4292 XIMP=[0.71], TIMP=[0.71], DWF=[0](cms), LOSS=[2],
4293 SCS curve number CN=[75],
4294 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4295 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4296 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4297 LGI=[186](m), MNI=[0.013], SCI=[0](min),
4298 Continuous simulation parameters:
4299 IaREcper=[4](hrs), IaREcimp=[4](hrs),
4300 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4301 InterEventTime=[18](hrs), END=-1
4302 *%-----|-----|
4303 ADD HYD NHYDsum=["A8T"], NHYDs to add=["A6-MJ"+"A8"]
4304 *%-----|-----|
4305 COMPUTE DUALHYD NHYDin=["A8T"], CINLET=[0.238](cms), NINLET=[1],
4306 MajNHYD=["A8-MJ"]
4307 MinNHYD=["A8-MN"]
4308 TMJSTO=[40](cu-m)
4309 *%-----|-----|
4310 ADD HYD NHYDsum=["MH105"], NHYDs to
add=["104-105"+"B5-MN"+"A8-MN"+"TODD_MN3j"]
4311 *%-----|-----|
4312 SAVE HYD NHYD=["MH105"], # OF PCYCLES=[-1], ICASEsh=[1]
4313 HYD_COMMENT=["Total Flows at MH105"]
4314 *%-----|-----|
4315 DIVERT HYD NHYDin=["A8-MJ"] NIDout=[2]max five,
4316 outflow hydrographs (NHYDs)=["A8-MJ-JR" "A8-MJ-B6"]
4317 flow distribution table: (modify as necessary)
4318 Note: all flows are in (cms)

```



```

4319          QIDi + QIDii = QTOTAL
4320          [ 0 + 0 = 0 ]
4321          [ 50 + 50 = 100 ] end
4322  *%-----|-----
|
4323  DIVERT HYD      NHYDin=["MH105"] NIDout=[2]max five,
4324                  outflow hydrographs (NHYDs)=["MH105-JR" "MH105-B6"]
4325                  flow distribution table: (modify as necessary)
4326                  Note: all flows are in (cms)
4327                  QIDi + QIDii = QTOTAL
4328                  [ 0 + 0 = 0 ]
4329                  [ 0 + 3.0 = 3.0 ]
4330                  [ 96.9+ 3.1 = 100 ] end
4331  *%-----|-----
|
4332  CONTINUOUS STANDHYD NHYD=["B7"], DT=[1]min, AREA=[7.19](ha),
4333                  XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4334                  SCS curve number CN=[75],
4335                  Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4336                  LGP=[40](m), MNP=[0.25], SCP=[0](min),
4337                  Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4338                  LGI=[211](m), MNI=[0.013], SCI=[0](min),
4339                  Continuous simulation parameters:
4340                  IaRECper=[4](hrs), IaRECimp=[4](hrs),
4341                  SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4342                  InterEventTime=[18](hrs), END=-1
4343  *%-----|-----
4344  ADD HYD        NHYDsum=["B7-B4MJ"], NHYDs to add=["B4-MJ"+"B7"]
4345  *%-----|-----
4346  COMPUTE DUALHYD NHYDin=["B7-B4MJ"], CINLET=[0.629](cms), NINLET=[1],
4347                  MajNHYD=["B7R-MJ"]
4348                  MinNHYD=["B7R-MN"]
4349                  TMJSTO=[311](cu-m)
4350  *%-----|-----
4351  ROUTE PIPE    PTYPE=[1]circ, NHYDout=["360-106A"], RNUMBER=[1.0], PDIAM=[1050](mm),
4352                  PLNGTH=[167](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
4353                  NHYDin=["B7R-MN"], RDT=[1]
4354  *%-----|-----
4355  * -JFSA 2021-01-19 change B6 to be developed as per geottawa website and apply the
4356  parameters of A7, the nearest sub-catchment to B6, LGI is calculated based on B6 area
4357  CONTINUOUS STANDHYD NHYD=["B6"], DT=[1]min, AREA=[3.29](ha),
4358                  XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4359                  SCS curve number CN=[75],
4360                  Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4361                  LGP=[40](m), MNP=[0.25], SCP=[0](min),
4362                  Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4363                  LGI=[148.099](m), MNI=[0.013], SCI=[0](min),
4364                  Continuous simulation parameters:
4365                  IaRECper=[4](hrs), IaRECimp=[4](hrs),
4366                  SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4367                  InterEventTime=[18](hrs), END=-1
4368  *%-----|-----
4369  * -JFSA 2021-01-25 add B1 DUALHYD as per Corrigan Report, IBI Group, 2008
4370  COMPUTE DUALHYD NHYDin=["B6"], CINLET=[0.064](cms), NINLET=[1],
4371                  MajNHYD=["B6-MJ"]
4372                  MinNHYD=["B6-MN"]
4373                  TMJSTO=[5484](cu-m)
4374  *%-----|-----
4375  * CONTINUOUS NASHHYD NHYD=["B6"], DT=[1]min, AREA=[3.29](ha),
4376                  * DWF=[0](cms), CN/C=[75], IA=[2.5](mm),
4377                  * N=[3.0], TP=[0.36]hrs,
4378                  * Continuous simulation parameters:
4379                  * IaRECper=[4](hrs),
4380                  * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4381                  * InterEventTime=[12](hrs)
4382                  * Baseflow simulation parameters:

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4381 *           BaseFlowOption=[1] ,
4382 *           InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4383 *           VHydCond=[0.055](mm/hr),   END=-1
4384 *%-----|-----
4385 *%   -EX-LAND is external land. It is a part of JOCKVA sub-catchment as per Corrigan
Report, IBI Group, 2008
4386 CONTINUOUS STANDHYD NHYD=["EX-LAND"], DT=[1]min, AREA=[32.5](ha),
4387 XIMP=[0.50], TIMP=[0.50], DWF=[0](cms), LOSS=[2],
4388 SCS curve number CN=[74],
4389 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4390 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4391 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4392 LGI=[465.475](m), MNI=[0.013], SCI=[0](min),
4393 Continuous simulation parameters:
4394 IaRECper=[4](hrs), IaRECimp=[4](hrs),
4395 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4396 InterEventTime=[18](hrs),   END=-1
4397 *%-----|-----
4398 COMPUTE DUALHYD NHYDin=["EX-LAND"], CINLET=[2.275](cms), NINLET=[1],
4399 MajNHYD=["EX-LAND-MJ"]
4400 MinNHYD=["EX-LAND-MN"]
4401 TMJSTO=[1365](cu-m)
4402 *%-----|-----
4403 ADD HYD NHYDsum=["B6-B7ExMJ"], NHYDs to
add=["B7R-MJ"+"EX-LAND-MJ"+"B5-MJ"+"B6-MJ"+"B6-MN"+"A8-MJ-B6"]
4404 *%-----|-----
4405 COMPUTE DUALHYD NHYDin=["B6-B7ExMJ"], CINLET=[0.064](cms), NINLET=[1],
4406 MajNHYD=["B6R-MJ"]
4407 MinNHYD=["B6R-MN"]
4408 TMJSTO=[5484](cu-m)
4409 *%-----|-----
4410 ROUTE PIPE PTYPE=[1]circ, NHYDout=["105-106A"], RNUMBER=[1.0], PDIAM=[1800](mm),
4411 PLNGTH=[208](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["MH105-B6"], RDT=[1]
4412 *%-----|-----
4413 ADD HYD NHYDsum=["MH106A"], NHYDs to
add=["360-106A"+"105-106A"+"B6R-MN"+"B6R-MJ"]
4414 *%-----|-----
4415 SAVE HYD NHYD=["MH106A"], # OF PCYCLES=[-1], ICASEsh=[1]
4416 HYD_COMMENT=["Total Flows at MH106A"]
4417 *%-----|-----
4418 *%   -JFSA 2021-01-12 THE MANHOLE MH106 is called MH117/106 in Corrigan Report, IBI
Group, July 2008
4419 *%
4420 ROUTE PIPE PTYPE=[1]circ, NHYDout=["106A-106"], RNUMBER=[1.0], PDIAM=[1800](mm),
4421 PLNGTH=[190](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["MH106A"], RDT=[1]
4422 *%-----|-----
4423 CONTINUOUS STANDHYD NHYD=["A9"], DT=[1]min, AREA=[2.44](ha),
4424 XIMP=[0.71], TIMP=[0.71], DWF=[0](cms), LOSS=[2],
4425 SCS curve number CN=[75],
4426 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4427 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4428 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4429 LGI=[262](m), MNI=[0.013], SCI=[0](min),
4430 Continuous simulation parameters:
4431 IaRECper=[4](hrs), IaRECimp=[4](hrs),
4432 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4433 InterEventTime=[18](hrs),   END=-1
4434 *%-----|-----
4435 COMPUTE DUALHYD NHYDin=["A9"], CINLET=[0.547](cms), NINLET=[1],
4436 MajNHYD=["A9-MJ"]
4437 MinNHYD=["A9-MN"]
4438 TMJSTO=[0](cu-m)
4439 *%-----|-----
4440 ADD HYD NHYDsum=["MH106"], NHYDs to add=["106A-106"+"A9-MN"]

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4441  *%-----|-----|
4442  SAVE HYD      NHYD=["MH106"], # OF PCYCLES=[-1], ICASEsh=[1]
4443              HYD_COMMENT=["Total Flows at MH106"]
4444  *%-----|-----|
4445  *%    -JFSA 2021-01-12 THE MANHOLE MH107 is called MH118/107 in Corrigan Report, IBI
Group, July 2008
4446  *%
4447  ROUTE PIPE    PTYPE=[1]circ, NHYDout=["106-107"], RNUMBER=[1.0], PDIAM=[1800](mm),
4448              PLNGTH=[122.5](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
              NHYDin=["MH106"], RDT=[1]
4449  *%-----|-----|
4450  CONTINUOUS STANDHYD NHYD=["A10"], DT=[1]min, AREA=[4.14](ha),
4451              XIMP=[0.35], TIMP=[0.47], DWF=[0](cms), LOSS=[2],
4452              SCS curve number CN=[75],
4453              Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4454              LGP=[40](m), MNP=[0.25], SCP=[0](min),
4455              Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4456              LGI=[183](m), MNI=[0.013], SCI=[0](min),
4457              Continuous simulation parameters:
4458              IaRECper=[4](hrs), IaRECimp=[4](hrs),
4459              SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4460              InterEventTime=[18](hrs), END=-1
4461  *%-----|-----|
4462  COMPUTE DUALHYD NHYDin=["A10"], CINLET=[0.310](cms), NINLET=[1],
4463              MajNHYD=["A10-MJ"]
4464              MinNHYD=["A10-MN"]
4465              TMJSTO=[228](cu-m)
4466  *%-----|-----|
4467  CONTINUOUS STANDHYD NHYD=["A11"], DT=[1]min, AREA=[10.61](ha),
4468              XIMP=[0.53], TIMP=[0.62], DWF=[0](cms), LOSS=[2],
4469              SCS curve number CN=[75],
4470              Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4471              LGP=[40](m), MNP=[0.25], SCP=[0](min),
4472              Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4473              LGI=[379](m), MNI=[0.013], SCI=[0](min),
4474              Continuous simulation parameters:
4475              IaRECper=[4](hrs), IaRECimp=[4](hrs),
4476              SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4477              InterEventTime=[18](hrs), END=-1
4478  *%-----|-----|
4479  COMPUTE DUALHYD NHYDin=["A11"], CINLET=[0.993](cms), NINLET=[1],
4480              MajNHYD=["A11-MJ"]
4481              MinNHYD=["A11-MN"]
4482              TMJSTO=[556](cu-m)
4483  *%-----|-----|
4484  ADD HYD       NHYDsum=["MH107"], NHYDs to add=["106-107"+"A10-MN"+"A11-MN"]
4485  *%-----|-----|
4486  SAVE HYD      NHYD=["MH107"], # OF PCYCLES=[-1], ICASEsh=[1]
4487              HYD_COMMENT=["Total Flows at MH107"]
4488  *%-----|-----|
4489  ROUTE PIPE    PTYPE=[1]circ, NHYDout=["107-119"], RNUMBER=[1.0], PDIAM=[1800](mm),
4490              PLNGTH=[114](m), PROUGH=[0.013], PSLOPE=[0.0012](m/m),
              NHYDin=["MH107"], RDT=[1]
4491  *%-----|-----|
4492  *%    -JFSA 2021-01-12 THE MANHOLE MH108 is called MH120/108 in Corrigan Report, IBI
Group, July 2008
4493  *%
4494  ROUTE PIPE    PTYPE=[1]circ, NHYDout=["119-108"], RNUMBER=[1.0], PDIAM=[1800](mm),
4495              PLNGTH=[65.8](m), PROUGH=[0.013], PSLOPE=[0.0012](m/m),
              NHYDin=["107-119"], RDT=[1]
4496  *%-----|-----|
4497  CONTINUOUS STANDHYD NHYD=["A12"], DT=[1]min, AREA=[12.29](ha),
4498              XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4499              SCS curve number CN=[75],
4500              Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4501              LGP=[40](m), MNP=[0.25], SCP=[0](min),

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4502      Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4503      LGI=[183](m), MNI=[0.013], SCI=[0](min),
4504      Continuous simulation parameters:
4505      IaREcper=[4](hrs), IaREcimp=[4](hrs),
4506      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4507      InterEventTime=[18](hrs), END=-1
4508  *%-----|-----|
4509  COMPUTE DUALHYD  NHYDin=["A12"], CINLET=[1.029](cms), NINLET=[1],
4510      MajNHYD=["A12-MJ"]
4511      MinNHYD=["A12-MN"]
4512      TMJSTO=[672](cu-m)
4513  *%-----|-----|
4514  CONTINUOUS STANDHYD  NHYD=["A13"], DT=[1]min, AREA=[2.59](ha),
4515      XIMP=[0.71], TIMP=[0.71], DWF=[0](cms), LOSS=[2],
4516      SCS curve number CN=[75],
4517      Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4518      LGP=[40](m), MNP=[0.25], SCP=[0](min),
4519      Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4520      LGI=[379](m), MNI=[0.013], SCI=[0](min),
4521      Continuous simulation parameters:
4522      IaREcper=[4](hrs), IaREcimp=[4](hrs),
4523      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4524      InterEventTime=[18](hrs), END=-1
4525  *%-----|-----|
4526  COMPUTE DUALHYD  NHYDin=["A13"], CINLET=[0.571](cms), NINLET=[1],
4527      MajNHYD=["A13-MJ"]
4528      MinNHYD=["A13-MN"]
4529      TMJSTO=[0](cu-m)
4530  *%-----|-----|
4531  * -JFSA 2021-01-22 add the Corrigan pond area ("Pond-Block")
4532  CONTINUOUS STANDHYD  NHYD=["Pond-Block"], DT=[1]min, AREA=[2.94](ha),
4533      XIMP=[0.415], TIMP=[0.415], DWF=[0](cms), LOSS=[2],
4534      SCS curve number CN=[75],
4535      Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4536      LGP=[40](m), MNP=[0.25], SCP=[0](min),
4537      Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4538      LGI=[183](m), MNI=[0.013], SCI=[0](min),
4539      Continuous simulation parameters:
4540      IaREcper=[4](hrs), IaREcimp=[4](hrs),
4541      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4542      InterEventTime=[18](hrs), END=-1
4543  *%-----|-----|
4544  ADD HYD  NHYDsum=["MH108"], NHYDs to add=["119-108"+"A13-MN"+"A12-MN"]
4545  *%-----|-----|
4546  SAVE HYD  NHYD=["MH108"], # OF PCYCLES=[-1], ICASEsh=[1]
4547      HYD_COMMENT=["Total Flows at MH108"]
4548  *%-----|-----|
4549  ROUTE PIPE  PTYPE=[1]circ, NHYDout=["108-116"], RNUMBER=[1.0], PDIAM=[1800](mm),
4550      PLNGTH=[76.6](m), PROUGH=[0.013], PSLOPE=[0.0013](m/m),
      NHYDin=["MH108"], RDT=[1]
4551  *%-----|-----|
4552  ROUTE PIPE  PTYPE=[1]circ, NHYDout=["116-corrig"], RNUMBER=[1.0],
      PDIAM=[1800](mm),
4553      PLNGTH=[79.5](m), PROUGH=[0.013], PSLOPE=[0.0013](m/m),
      NHYDin=["108-116"], RDT=[1]
4554  *%-----|-----|
4555  ADD HYD  NHYDsum=["Corrigan"], NHYDs to add=["116-corrig"+"Pond-Block"]
4556  *%-----|-----|
4557  SAVE HYD  NHYD=["Corrigan"], # OF PCYCLES=[-1], ICASEsh=[1]
4558      HYD_COMMENT=["Total Flows at Corrigan Pond"]
4559  *%-----|-----|
4560  ROUTE RESERVOIR  NHYDout=["Co-P"], NHYDin=["Corrigan"],
4561      RDT=[1](min),
4562      TABLE of ( OUTFLOW-STORAGE ) values
4563      (cms) - (ha-m)
4564      [ 0.0 , 0.0 ]

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```

4565 [ 0.015 , 0.04118]
4566 [ 0.030 , 0.08297]
4567 [ 0.045 , 0.12537]
4568 [ 0.060 , 0.16837]
4569 [ 0.075 , 0.21199]
4570 [ 0.090 , 0.27545]
4571 [ 0.105 , 0.34650]
4572 [ 0.120 , 0.42049]
4573 [ 0.135 , 0.50188]
4574 [ 0.186 , 0.60307]
4575 [ 2.110 , 0.79083]
4576 [ 5.874 , 1.00271]
4577 [ 11.395 , 1.29643]
4578 [ 18.770 , 1.62054]
4579 [ 28.143 , 1.97516]
4580 [ -1 , -1 ] (max twenty pts)
4581 NHYDovf=[ "Co-P-OVF" ]
4582 *%-----|-----|
4583 ADD HYD NHYDsum=["corrig"], NHYDs to
add=["Co-P-OVF"+"Co-P"+"N_TO"+"MH105-JR"+"A8-MJ-JR"+"A9-MJ"+"A10-MJ"+"A11-MJ"+"A12-MJ"+"A
13-MJ" ]
4584 *%-----|-----|
4585 SAVE HYD NHYD=["corrig"], # OF PCYCLES=[-1], ICASEsh=[1]
4586 HYD_COMMENT=["Total Flows at Corrigan Pond"]
4587 *%-----|-----|
4588 *#*****|
4589 *# Corrigan Pond 1
4590 *# - Rating curve obtained from Barrhaven South MSS modeling
4591 *# - Tributary Drainage Area to MSS Pond 1 = 145 ha
4592 *#*****|
4593 *ROUTE RESERVOIR NHYDout=["MS_P1"], NHYDin=["CORRIG"],
4594 * RDT=[1](min),
4595 * TABLE of ( OUTFLOW-STORAGE ) values
4596 * (cms) - (ha-m)
4597 * [ 0.0 , 0.0 ]
4598 * [ 0.06 , 0.58]
4599 * [ -1 , -1 ] (max twenty pts)
4600 * NHYDovf=["P1-OVF" ]
4601 *%-----|-----|
4602 *ADD HYD NHYDsum=["SN_CO"], NHYDs to add=["N_TO"+"P1-OVF"+"MS_P1" ]
4603 *%-----|-----|
4604 *SAVE HYD NHYD=["SN_CO"], # OF PCYCLES=[-1], ICASEsh=[1]
4605 * HYD_COMMENT=["Total Flows at Corrigan Drain" ]
4606 *%-----|-----|
4607 *#
4608 *# Hydrograph from Corrigan Drain routed to Jockvale Road
4609 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
4610 *#
4611 ROUTE CHANNEL NHYDout=["N_MI" ] ,NHYDin=["corrig" ] ,
4612 RDT=[1](min),
4613 CHLGTH=[580](m), CHSLOPE=[0.4448](%),
4614 FPSLOPE=[0.4448](%),
4615 SECNUM=[1.0], NSEG=[3]
4616 ( SEGROUGH, SEGDIST (m))=
4617 [0.075,-17.72
4618 -0.045,17.72
4619 0.075,80.62] NSEG times
4620 ( DISTANCE (m), ELEVATION (m))=
4621 [-83.32, 90.00]
4622 [-81.36, 89.50]
4623 [-79.12, 89.00]
4624 [-76.13, 88.50]
4625 [-20.46, 88.00]
4626 [-19.36, 87.50]
4627 [-18.51, 87.00]
4628 [-17.72, 86.50]

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4629 [-11.95, 85.24]  
4630 [-0.11, 85.12]  
4631 [11.49, 85.20]  
4632 [17.72, 86.50]  
4633 [19.74, 87.00]  
4634 [21.22, 87.50]  
4635 [22.68, 88.00]  
4636 [24.28, 88.50]  
4637 [26.79, 89.00]  
4638 [71.98, 90.00]  
4639 [80.62, 90.50]

4640 \*%-----|-----|  
4641 \*#\*\*\*\*\*|  
4642 \*# Catchment MILLS  
4643 \*# - To SWM Facility north of the Jock  
4644 \*# - Primarily residential development  
4645 \*#\*\*\*\*\*|  
4646 **CONTINUOUS STANDHYD** NHYD=["MILLS"], DT=[1]min, AREA=[175.99](ha),  
4647 XIMP=[0.38], TIMP=[0.38], DWF=[0](cms), LOSS=[2],  
4648 SCS curve number CN=[74],  
4649 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),  
4650 LGP=[40](m), MNP=[0.25], SCP=[0](min),  
4651 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),  
4652 LGI=[1118.123](m), MNI=[0.013], SCI=[0](min),  
4653 Continuous simulation parameters:  
4654 IaRECper=[4](hrs), IaRECimp=[4](hrs),  
4655 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),  
4656 InterEventTime=[18](hrs), END=-1

4657 \*%-----|-----|  
4658 \*#\*\*\*\*\*|  
4659 \*# Chapman Mills SWM Pond  
4660 \*# - Rating curve obtained from CCL hydraulic modeling  
4661 \*#\*\*\*\*\*|

4662 **ROUTE RESERVOIR** NHYDout=["MILL\_P"], NHYDin=["MILLS"],  
4663 RDT=[1](min),  
4664 TABLE of ( OUTFLOW-STORAGE ) values  
4665 (cms) - (ha-m)  
4666 [ 0.0 , 0.0 ]  
4667 [ 0.01 , 0.01 ]  
4668 [ 0.05 , 0.06 ]  
4669 [ 0.09 , 0.11 ]  
4670 [ 0.13 , 0.15 ]  
4671 [ 0.18 , 0.19 ]  
4672 [ 0.28 , 0.28 ]  
4673 [ 0.37 , 0.34 ]  
4674 [ 0.45 , 0.40 ]  
4675 [ 0.51 , 0.44 ]  
4676 [ 0.56 , 0.47 ]  
4677 [ 0.64 , 0.52 ]  
4678 [ 0.76 , 0.59 ]  
4679 [ 0.86 , 0.65 ]  
4680 [ 1.09 , 0.78 ]  
4681 [ 1.44 , 0.96 ]  
4682 [ 3.18 , 1.84 ]  
4683 [ 4.05 , 2.31 ]  
4684 [ -1 , -1 ] (max twenty pts)

4685 NHYDovf=["MIL-OV"]  
4686 \*%-----|-----|  
4687 **ADD HYD** NHYDsum=["SN\_MI"], NHYDs to add=["N\_MI"+"MIL-OV"+"MILL\_P"]  
4688 \*%-----|-----|  
4689 **SAVE HYD** NHYD=["SN\_MI"], # OF PCYCLES=[-1], ICASEsh=[1]  
4690 HYD\_COMMENT=["Total Flows at Jockvale Road"]  
4691 \*%-----|-----|  
4692 \*#  
4693 \*# Hydrograph from Jockvale Road routed to Heart's Desire  
4694 \*# Channel X-Section obtained from RVCA Hydraulic Model - Station 689



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4695 *#
4696 ROUTE CHANNEL NHYDout=["N_DE"] ,NHYDin=["SN_MI"] ,
4697 RDT=[1](min),
4698 CHLGTH=[1962](m), CHSLOPE=[0.2227](%),
4699 FPSLOPE=[0.2227](%),
4700 SECNUM=[1.0], NSEG=[3]
4701 ( SEGROUGH, SEGDIST (m))=
4702 [0.075,-17.56
4703 -0.045,18.27
4704 0.075,32.51] NSEG times
4705 ( DISTANCE (m), ELEVATION (m))=
4706 [-54.07, 85.00]
4707 [-39.43, 84.50]
4708 [-28.30, 84.00]
4709 [-24.12, 83.50]
4710 [-22.30, 83.00]
4711 [-20.55, 82.50]
4712 [-17.56, 82.00]
4713 [-12.63, 81.22]
4714 [-0.11, 80.75]
4715 [11.55, 81.22]
4716 [18.27, 82.00]
4717 [19.82, 82.50]
4718 [22.48, 83.00]
4719 [27.90, 83.50]
4720 [29.31, 84.00]
4721 [30.81, 84.50]
4722 [32.51, 85.00]
4723 *%-----|-----|
4724 *#*****|
4725 *# Catchment DESIRE
4726 *# - To Jock River (north of the Jock)
4727 *# - Rural-estate subdivision (Heart's Desire Community)
4728 *#*****|
4729 CONTINUOUS STANDHYD NHYD=["DESIRE"], DT=[1]min, AREA=[23.78](ha),
4730 XIMP=[0.25], TIMP=[0.25], DWF=[0](cms), LOSS=[2],
4731 SCS curve number CN=[77],
4732 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4733 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4734 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4735 LGI=[400](m), MNI=[0.013], SCI=[0](min),
4736 Continuous simulation parameters:
4737 IaRECper=[4](hrs), IaRECimp=[4](hrs),
4738 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4739 InterEventTime=[18](hrs), END=-1
4740 *%-----|-----|
4741 *#*****|
4742 *# Catchment JOCKVA
4743 *# - To Jockvale SWM Facility
4744 *# - Residential development & golf course
4745 *# - JFSA 2021-01-11 update JOCKVA after updating CORRIG as per IBI GROUP, July 2008.
4746 *# JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two
areas JOCKVA and EX-LAND 32.5 ha as per IBI GROUP, July 2008.
4747 *#*****|
4748 CONTINUOUS STANDHYD NHYD=["JOCKVA"], DT=[1]min, AREA=[225.13](ha),
4749 XIMP=[0.50], TIMP=[0.50], DWF=[0](cms), LOSS=[2],
4750 SCS curve number CN=[74],
4751 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4752 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4753 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4754 LGI=[1310.55](m), MNI=[0.013], SCI=[0](min),
4755 Continuous simulation parameters:
4756 IaRECper=[4](hrs), IaRECimp=[4](hrs),
4757 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4758 InterEventTime=[18](hrs), END=-1
4759 *%-----|-----|

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4760 ADD HYD          NHYDsum=["JOCKVA-TO"], NHYDs to
add=["EX-LAND-MN"+"JOCKVA"+"B2-MJ"+"B3-MJ"]
4761 *%-----|-----|
4762 SAVE HYD          NHYD=["JOCKVA-TO"], # OF PCYCLES=[-1], ICASEsh=[1]
4763 HYD_COMMENT=["Total Flows at KB first pond"]
4764 *%-----|-----|
4765 *#*****|
4766 *#   Jockvale SWM Facility
4767 *#   - Rating curve obtained from Jockvale Servicing Study (CCL 1999)
4768 *#*****|
4769 ROUTE RESERVOIR  NHYDout=["JOCK_P"], NHYDin=["JOCKVA-TO"],
4770 RDT=[1](min),
4771             TABLE of ( OUTFLOW-STORAGE ) values
4772             (cms) - (ha-m)
4773             [ 0.0 , 0.0 ]
4774             [ 0.27 , 0.03]
4775             [ 0.28 , 0.55]
4776             [ 0.29 , 1.14]
4777             [ 0.30 , 1.80]
4778             [ 0.31 , 2.32]
4779             [ 1.12 , 2.87]
4780             [ 2.92 , 3.45]
4781             [ 4.64 , 4.07]
4782             [ 6.69 , 4.72]
4783             [ 9.02 , 5.39]
4784             [ 11.62 , 6.10]
4785             [ 14.42 , 6.85]
4786             [ 17.45 , 7.62]
4787             [ 20.69 , 8.44]
4788             [ 24.08 , 9.28]
4789             [ 27.68 , 10.17]
4790             [ -1 , -1 ] (max twenty pts)
4791             NHYDovf=["JO-OVF"]
4792 *%-----|-----|
4793 ADD HYD          NHYDsum=["SN_DE"], NHYDs to add=["N_DE"+"DESIRE"+"JO-OVF"+"JOCK_P"]
4794 *%-----|-----|
4795 SAVE HYD          NHYD=["SN_DE"], # OF PCYCLES=[-1], ICASEsh=[1]
4796 HYD_COMMENT=["Total Flows at Heart's Desire"]
4797 *%-----|-----|
4798 *#
4799 *# Hydrograph from Heart's Desire routed to Rideau River
4800 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 0
4801 *#
4802 ROUTE CHANNEL    NHYDout=["N1"] ,NHYDin=["SN_DE"] ,
4803 RDT=[1](min),
4804 CHLGTH=[563](m), CHSLOPE=[0.9668](%),
4805             FPSLOPE=[0.9668](%),
4806 SECNUM=[1.0], NSEG=[3]
4807 ( SEGROUGH, SEGDIST (m))=
4808 [0.075,-30.20
4809 -0.045,30.20
4810 0.075,48.48] NSEG times
4811 ( DISTANCE (m), ELEVATION (m))=
4812 [-98.46, 81.50]
4813 [-92.24, 81.00]
4814 [-86.88, 80.50]
4815 [-81.54, 80.00]
4816 [-74.36, 79.50]
4817 [-63.54, 79.00]
4818 [-39.23, 78.50]
4819 [-34.51, 78.00]
4820 [-33.01, 77.50]
4821 [-30.20, 77.00]
4822 [-13.42, 76.18]
4823 [-1.14, 76.09]
4824 [17.06, 76.18]

```

```

4825          [30.20, 77.00]
4826          [32.95, 77.50]
4827          [34.06, 78.00]
4828          [35.11, 78.50]
4829          [36.32, 79.00]
4830          [37.74, 79.50]
4831          [48.48, 81.50]
4832  *%-----|-----|
4833  *#*****|*****|
4834  *#   Catchment S-2
4835  *#   - To Jock River (north and south)
4836  *#   - Undeveloped floodplain and river
4837  *#*****|*****|
4838  CONTINUOUS NASHYD  NHYD=["S-2"], DT=[1]min, AREA=[102.94](ha),
4839                    DWF=[0](cms), CN/C=[72], IA=[4.67](mm),
4840                    N=[3], TP=[0.40]hrs,
4841                    Continuous simulation parameters:
4842                    IaREcper=[4](hrs),
4843                    SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4844                    InterEventTime=[12](hrs)
4845                    Baseflow simulation parameters:
4846                    BaseFlowOption=[1] ,
4847                    InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4848                    VHydCond=[0.055](mm/hr), END=-1
4849  *%-----|-----|
4850  ADD HYD            NHYDsum=["SN_N1"], NHYDs to add=["N1"+"S-2"]
4851  *%-----|-----|
4852  SAVE HYD          NHYD=["SN_N1"], # OF PCYCLES=[-1], ICASEsh=[1]
4853                    HYD_COMMENT=["Total Flows at Rideau River"]
4854  *%-----|-----|
4855  *#####|#####|
4856  *% 5 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4857  START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[5]
4858  *%              ["C24SC005.stm"] <--storm filename, one per line for NSTORM time
4859  *%-----|-----|
4860  *% 10 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4861  START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[10]
4862  *%              ["C24SC010.stm"] <--storm filename, one per line for NSTORM time
4863  *%-----|-----|
4864  *% 25 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4865  START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[25]
4866  *%              ["C24SC025.stm"] <--storm filename, one per line for NSTORM time
4867  *%-----|-----|
4868  *% 50 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4869  START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[50]
4870  *%              ["C24SC050.stm"] <--storm filename, one per line for NSTORM time
4871  *%-----|-----|
4872  *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4873  *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4874  *%              ["100YC3H.STM"] <--storm filename, one per line for NSTORM time
4875  *%-----|-----|
4876  *% 100 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4877  START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4878  *%              ["C24SC100.stm"] <--storm filename, one per line for NSTORM time
4879  *%-----|-----|
4880  *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4881  *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4882  *%              ["C24SC100.stm"] <--storm filename, one per line for NSTORM time
4883  *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[101]
4884  *%              ["A24SC100.stm"] <--storm filename, one per line for NSTORM time
4885  *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[102]
4886  *%              ["A24SC100_60.stm"] <--storm filename, one per line for NSTORM time
4887  FINISH
4888

```

```

00001 .....
00002 .....
00003 SSSSS W W M M H H Y Y V V M M OOO 222 000 11 5555 .....
00004 S W W M M H H T T M M M O O 2 0 0 11 5 .....
00005 SSSSS W W M M M H H H H H Y Y M M M O O 2 0 0 11 5 Ver 5.800
00006 S W W M M H H Y Y M M O O 222 0 0 11 555 PRE 2015
00007 SSSSS W W M M H H Y Y M M O O 2 0 0 11 5 .....
00008 .....
00009 Stormwater Management Hydrologic Model 222 0 0 11 5 *****
00010 .....
00011 .....
00012 ***** SWHYMO Ver 5.800 *****
00013 .....
00014 ..... A single event and continuous hydrologic simulation model .....
00015 ..... based on the principles of HMO and its successors .....
00016 ***** OTHYMO=83 and OTHYMO=89 .....
00017 .....
00018 ***** Distributed by: J.F. Sabourin and Associates Inc. *****
00019 .....
00020 ***** Ottawa, Ontario: (613) 886-8884 .....
00021 ***** Gatineau, Quebec: (819) 243-6858 .....
00022 ***** E-Mail: swmhy@jfsa.com .....
00023 .....
00024 ***** Licensed user: JFSaInc. *****
00025 ***** Ottawa SERIAL#:2549237 *****
00026 *****
00027 .....
00028 *****
00029 ***** PROGRAM ARRAY DIMENSIONS *****
00030 ***** Maximum value for ID numbers : 11 *****
00031 ***** Max. number of rainfall points: 105408 *****
00032 ***** Max. number of flow points : 105408 *****
00033 *****
00034 *****
00035 ***** SUMMARY OUTPUT *****
00036 *****
00037 ***** RUN DATE: 2021-03-04 TIME: 11:54:16 RUN COUNTER: 020283 *****
00038 *****
00039 ***** Input file: T:\PROJ\1474-16\Design\20210226-QuantityControlAnalysis\SWHYMO\SMH-Model\Updated\
00040 ***** 3\SMR_1-3-F_Sf_Sd.dat *****
00041 *****
00042 ***** Output file: T:\PROJ\1474-16\Design\20210226-QuantityControlAnalysis\SWHYMO\SMH-Model\Updated\
00043 ***** 3\SMR_1-3-F_Sf_Sd.dat *****
00044 ***** Summary file: T:\PROJ\1474-16\Design\20210226-QuantityControlAnalysis\SWHYMO\SMH-Model\Updated\
00045 ***** 3\SMR_1-3-F_Sf_Sd.dat *****
00046 ***** User comment: *****
00047 ***** 1: *****
00048 ***** 2: *****
00049 ***** 3: *****
00050 ***** *****
00051 *****
00052 *****
00053 *****
00054 ***** SWHYMO Ver 5.800 INPUT DATA FILE *****
00055 *****
00056 ***** Project Name: [Jock River] Project Number: [1474-16] *****
00057 ***** Date [04-03-2021] *****
00058 ***** Modeller [J.F.M.] *****
00059 ***** Company [JFSaInc.] *****
00060 ***** License # [2549237] *****
00061 *****
00062 ***** CALIBRATION OF SUMMER MODEL PARAMETERS *****
00063 ***** USING CONTINUOUS SIMULATIONS *****
00064 ***** Rainfall data from JFSA rain gauge installed at site + other gauges by the City *****
00065 ***** Use data collected from May 1st to July 14, 2003 *****
00066 ***** 2020-11-30 change WMPROD to 0.55, SLPD=[0.5*(1+)] (impervious slope), and LGT up to 700m *****
00067 ***** 2020-12-01 correct pond curve values *****
00068 ***** 2020-12-01 change W_CLEAR_SLOPE to 0.55, SLPD=[0.5*(1+)] (impervious slope), and LGT up to 700m *****
00069 ***** 2021-02-19 Change the slope for ROUTE CHANNEL STATION 2462 (HNYDout="R_MC") ,HNYDin("SM_MC") from 0.033 k (as per st *****
00070 ***** 2021-02-19 Change the slope for ROUTE CHANNEL STATION 5002 (HNYDout="R_MC") ,HNYDin("SM_MC") from 0.01 k (as per st *****
00071 ***** *****
00072 ***** ** END OF RUN : 1 *****
00073 *****
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00188 [InterEventTime= 12.00]
00189 #
00190 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
00191 # of 1.32
00192 R0021C00013-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00193 CONTINUOUS NASHVD 1.0 01:SR_CK 8376.00 11.072 No.date 39:59 11.98 263 .000
00194 [Cm: 70.0; H: 3.00; Tp: 2.51]
00195 [IAREC: 4.00; SMIN: 52.62; SMAX:350.79; SK: .010]
00196 [InterEventTime= 12.00]
00197 #
00198 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
00199 # of 1.68
00200 R0021C00014-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00201 CONTINUOUS NASHVD 1.0 01:SR_B 1132.00 4.434 No.date 39:59 11.98 293 .000
00202 [Cm: 70.0; H: 3.00; Tp: 2.51]
00203 [IAREC: 4.00; SMIN: 43.07; SMAX:287.10; SK: .010]
00204 [InterEventTime= 12.00]
00205 #
00206 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
00207 # of 1.62
00208 R0021C00015-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00209 CONTINUOUS NASHVD 1.0 01:SR_CK 4664.00 5.504 No.date 39:59 10.98 241 .000
00210 [Cm: 62.0; H: 3.00; Tp: 1.32]
00211 [IAREC: 4.00; SMIN: 61.90; SMAX:412.66; SK: .010]
00212 [InterEventTime= 12.00]
00213 #
00214 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
00215 # of 1.80
00216 R0021C00016-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00217 CONTINUOUS NASHVD 1.0 01:SR_B 131.00 .805 No.date 28:57 11.22 247 .000
00218 [Cm: 63.0; H: 3.00; Tp: .93]
00219 [IAREC: 4.00; SMIN: 59.42; SMAX:396.11; SK: .010]
00220 [InterEventTime= 12.00]
00221 #
00222 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
00223 # of 1.65
00224 R0021C00017-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00225 CONTINUOUS NASHVD 1.0 01:SR_B 348.00 4.242 No.date 38:46 11.98 263 .000
00226 [Cm: 66.0; H: 3.00; Tp: 8.42]
00227 [IAREC: 4.00; SMIN: 51.81; SMAX:350.79; SK: .010]
00228 [InterEventTime= 12.00]
00229 #
00230 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
00231 # of 1.82
00232 R0021C00018-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00233 CONTINUOUS NASHVD 1.0 01:SR_7 3397.00 4.651 No.date 36:31 9.85 217 .000
00234 [Cm: 69.0; H: 3.00; Tp: .93]
00235 [IAREC: 4.00; SMIN: 76.32; SMAX:508.81; SK: .010]
00236 [InterEventTime= 12.00]
00237 #
00238 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
00239 # of 1.75
00240 R0021C00019-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00241 CONTINUOUS NASHVD 1.0 01:SR_B 165.00 .413 No.date 33:07 12.24 269 .000
00242 [Cm: 67.0; H: 3.00; Tp: 4.18]
00243 [IAREC: 4.00; SMIN: 60.55; SMAX:336.97; SK: .010]
00244 [InterEventTime= 12.00]
00245 #
00246 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
00247 # of 1.67
00248 R0021C00020-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00249 CONTINUOUS NASHVD 1.0 01:VDR 1332.00 3.148 No.date 35:23 13.94 306 .000
00250 [Cm: 72.0; H: 3.00; Tp: 5.93]
00251 [IAREC: 4.00; SMIN: 39.75; SMAX:264.99; SK: .010]
00252 [InterEventTime= 12.00]
00253 R0021C00021-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00254 CONTINUOUS NASHVD 1.0 01:SR_5 224.00 2.597 No.date 28:45 15.91 350 .000
00255 [Cm: 77.0; H: 3.00; Tp: .78]
00256 [IAREC: 4.00; SMIN: 38.15; SMAX:207.66; SK: .010]
00257 [InterEventTime= 12.00]
00258 #
00259 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
00260 # of 1.23
00261 R0021C00022-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00262 CONTINUOUS NASHVD 1.0 01:FL_CK 4945.00 14.839 No.date 33:25 14.57 320 .000
00263 [Cm: 74.0; H: 3.00; Tp: 4.63]
00264 [IAREC: 4.00; SMIN: 36.67; SMAX:244.49; SK: .010]
00265 [InterEventTime= 12.00]
00266 R0021C00023-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00267 CONTINUOUS NASHVD 1.0 01:SR_S 20.00 .309 No.date 28:36 17.79 391 .000
00268 [Cm: 81.0; H: 3.00; Tp: .21]
00269 [IAREC: 4.00; SMIN: 25.21; SMAX:168.09; SK: .010]
00270 [InterEventTime= 12.00]
00271 #
00272 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
00273 # of 1.61
00274 R0021C00024-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00275 CONTINUOUS NASHVD 1.0 01:SR_B 1413.00 3.090 No.date 39:04 15.22 334 .000
00276 [Cm: 75.0; H: 3.00; Tp: 8.00]
00277 [IAREC: 4.00; SMIN: 33.81; SMAX:225.43; SK: .010]
00278 [InterEventTime= 12.00]
00279 R0021C00025-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00280 CONTINUOUS NASHVD 1.0 01:SR_4 585.00 4.325 No.date 29:58 17.79 391 .000
00281 [Cm: 81.0; H: 3.00; Tp: 1.75]
00282 [IAREC: 4.00; SMIN: 25.21; SMAX:168.09; SK: .010]
00283 [InterEventTime= 12.00]
00284 R0021C00026-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00285 CONTINUOUS NASHVD 1.0 01:LM_CK 1021.00 5.747 No.date 30:50 17.39 382 .000
00286 [Cm: 80.0; H: 3.00; Tp: .86]
00287 [IAREC: 4.00; SMIN: 38.32; SMAX:175.50; SK: .010]
00288 [InterEventTime= 12.00]
00289 R0021C00027-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00290 CONTINUOUS NASHVD 1.0 01:SR_2 177.00 2.052 No.date 28:45 15.91 350 .000
00291 [Cm: 77.0; H: 3.00; Tp: .78]
00292 [IAREC: 4.00; SMIN: 31.15; SMAX:207.66; SK: .010]
00293 [InterEventTime= 12.00]
00294 R0021C00028-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00295 CONTINUOUS NASHVD 1.0 01:SR_B 1122.00 5.337 No.date 31:50 17.79 391 .000
00296 [Cm: 81.0; H: 3.00; Tp: 3.25]
00297 [IAREC: 4.00; SMIN: 25.21; SMAX:168.09; SK: .010]
00298 [InterEventTime= 12.00]
00299 R0021C00029-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00300 CONTINUOUS NASHVD 1.0 01:SR_D 2737.00 11.528 No.date 31:35 15.56 342 .000
00301 [Cm: 76.0; H: 3.00; Tp: .93]
00302 [IAREC: 4.00; SMIN: 32.46; SMAX:216.39; SK: .010]
00303 [InterEventTime= 12.00]
00304 #
00305 # Routing hydrographs
00306 #
00307 # Starting with the addition of Jock River Headwater and Subwatershed 13
00308 #
00309 R0021C00030-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00310 ADD HYD 3680.00 6.204 No.date 37:06 11.47 n/a .000
00311 [IAREC: 4.00; SMIN: 31.15; SMAX:207.66; SK: .010]
00312 [IAREC: 4.00; SMIN: 31.15; SMAX:207.66; SK: .010]
00313 #
00314 # Sum of hydrographs from Node 13 routed to Node 13A
00315 # (Approximated cross-section - see cross-section 258)
00316 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
00317 #
00318 R0021C00031-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00319 ROUTE CHANNEL -> 1.0 02:R_M13 4651.00 7.871 No.date 39:37 11.32 n/a .000
00320 [IAREC: 4.00; SMIN: 31.15; SMAX:207.66; SK: .010]
00321 [I/S/N= 9074./ .022/.040]
00322 [Wmax= 429;Dmax= 2.557]
00323 #
00324 # Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
00325 #
00326 R0021C00032-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00327 ADD HYD 4651.00 6.208 No.date 39:59 11.32 n/a .000
00328 [IAREC: 4.00; SMIN: 31.15; SMAX:207.66; SK: .010]
00329 [IAREC: 4.00; SMIN: 31.15; SMAX:207.66; SK: .010]
00330 #
00331 # Insertion of a reservoir to simulate the effects of the Goodwood Marsh
00332 #
00333 R0021C00033-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00334 ROUTE CHANNEL -> 1.0 02:SR13A 7725.00 9.475 No.date 39:59 10.97 n/a .000
00335 [IAREC: 4.00; SMIN: 31.15; SMAX:207.66; SK: .010]
00336 [IAREC: 4.00; SMIN: 31.15; SMAX:207.66; SK: .010]
00337 #
00338 R0021C00034-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00339 frme H_RESUM 7725.00 2.619 No.date 55:07 10.97 n/a .000
00340 [IAREC: 4.00; SMIN: 31.15; SMAX:207.66; SK: .010]
00341 [IAREC: 4.00; SMIN: 31.15; SMAX:207.66; SK: .010]
00342 # Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
00343 # (Approximated cross-section - see cross-section 258)
00344 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
00345 #
00346 R0021C00035-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00347 ROUTE CHANNEL -> 1.0 02:SR12 7725.00 2.619 No.date 55:07 10.97 n/a .000
00348 [IAREC: 4.00; SMIN: 31.15; SMAX:207.66; SK: .010]
00349 [IAREC: 4.00; SMIN: 31.15; SMAX:207.66; SK: .010]
00350 #
00351 # Addition of Subwatershed Jock River at Ashton to Node 12
00352 #
00353 R0021C00036-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00354 ADD HYD 7725.00 2.609 No.date 58:08 10.57 n/a .000
00355 [IAREC: 4.00; SMIN: 31.15; SMAX:207.66; SK: .010]
00356 [IAREC: 4.00; SMIN: 31.15; SMAX:207.66; SK: .010]
00357 R0021C00037-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00358 frme H_RESUM 7725.00 2.619 No.date 55:07 10.97 n/a .000
00359 [IAREC: 4.00; SMIN: 31.15; SMAX:207.66; SK: .010]
00360 [IAREC: 4.00; SMIN: 31.15; SMAX:207.66; SK: .010]
00361 #
00362 # Sum of hydrographs from Node 12 routed to Node 11
00363 # (Approximated cross-section - see cross-section 258)
00364 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
00365 #
00366 # Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
00367 #
00368 R0021C00038-----Dtn-ID:HNYD-----AREHA-GPEAKCms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
00369 ROUTE CHANNEL -> 1.0 02:R_M11 9506.00 7.458 No.date 32:50 11.20 n/a .000
00370 [IAREC: 4.00; SMIN: 31.15; SMAX:207.66; SK: .010]
00371 [I/S/N= 972./ .014/.040]
00372 [Wmax= 591;Dmax= 2.108]
00373 #
00374 # Addition of Subwatershed 11 and No Name Creek to Node 11

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00375# #
00376# R002/C00039-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00377# ADD HYD + 1.0 02:01M1 9506.00 7.472_MoDate 33:12 11.20 n/a .000
00378# ROUTE CHANNEL -> 1.0 02:01M1 500.00 2.720_MoDate 29:22 11.98 n/a .000
00379# + 1.0 02:01M2 1917.00 4.042_MoDate 34:34 11.98 n/a .000
00380# SUM= 1.0 01:01M1 11923.00 12.077_MoDate 33:14 11.36 n/a .000
00381#
00382# Sum of hydrographs from Node 11 routed to Node 10
00383# Section 1
00384#
00385# R002/C00040-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00386# ROUTE CHANNEL -> 1.0 02:01M1 11923.00 12.077_MoDate 33:14 11.36 n/a .000
00387# [RDP= 1.00] out<= 1.0 01:01M0 11923.00 8.276_MoDate 39:46 11.36 n/a .000
00388# [L/S= 2429 / .057/.040]
00389# [Vmax=.462;Dmax=.886]
00390#
00391# Addition of Subwatershed 10 to Node 10
00392#
00393# R002/C00041-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00394# ADD HYD + 1.0 02:01M0 11923.00 8.276_MoDate 39:46 11.36 n/a .000
00395# + 1.0 02:01M1 5646.00 11.228_MoDate 38:07 13.94 n/a .000
00396# + 1.0 01:01M0 17589.00 19.451_MoDate 38:31 12.19 n/a .000
00397# SUM= 1.0 01:01M0 17589.00 19.451_MoDate 38:31 12.19 n/a .000
00398# SAVE HYD + 1.0 01:01M0 17589.00 19.451_MoDate 38:31 12.19 n/a .000
00399# frame_H_SMI0
00400# remark:flow at_N10: M10 + SW_10
00401# Addition of Kings Creek to S_M10
00402#
00403# R002/C00043-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00404# ADD HYD + 1.0 02:01M0 17589.00 19.451_MoDate 38:31 12.19 n/a .000
00405# + 1.0 02:01M1 8376.00 11.072_MoDate 39:59 11.98 n/a .000
00406# SUM= 1.0 01:01M0A 25965.00 30.328_MoDate 39:58 12.12 n/a .000
00407#
00408# Sum of hydrographs from Node 10 routed to Node 9
00409# Section 2
00410#
00411# R002/C00044-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00412# ROUTE CHANNEL -> 1.0 02:01M0A 25965.00 30.328_MoDate 39:58 12.12 n/a .000
00413# [RDP= 1.00] out<= 1.0 01:01M9 25965.00 29.579_MoDate 39:59 12.12 n/a .000
00414# [L/S= 3942 / .075/.040]
00415# [Vmax=.595;Dmax=1.208]
00416#
00417# Addition of Subwatershed 9 and Nichols Creek to Node 9
00418#
00419# R002/C00045-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00420# ADD HYD + 1.0 02:01M9 25965.00 29.579_MoDate 39:59 12.12 n/a .000
00421# + 1.0 02:01M9 1132.00 4.484_MoDate 39:59 12.12 n/a .000
00422# + 1.0 02:01M2 4464.00 5.504_MoDate 39:59 10.98 n/a .000
00423# SUM= 1.0 01:01M9 31561.00 36.313_MoDate 39:59 12.00 n/a .000
00424#
00425# Sum of hydrographs from Node 9 routed to Node 8
00426# Section 3
00427#
00428# R002/C00046-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00429# ROUTE CHANNEL -> 1.0 02:01M9 31561.00 36.313_MoDate 39:59 12.00 n/a .000
00430# [RDP= 1.00] out<= 1.0 01:01M8 31561.00 34.173_MoDate 39:59 12.00 n/a .000
00431# [L/S= 4028 / .087/.040]
00432# [Vmax=.418;Dmax=1.281]
00433#
00434# Addition of Subwatershed 8 and Bobb's Drain to Node 8
00435#
00436# R002/C00047-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00437# ADD HYD + 1.0 02:01M8 31561.00 34.173_MoDate 39:59 12.00 n/a .000
00438# + 1.0 02:01M8 3197.00 4.651_MoDate 36:31 9.45 n/a .000
00439# + 1.0 02:01M2 3854.00 6.242_MoDate 38:46 11.98 n/a .000
00440# SUM= 1.0 01:01M8 38546.00 40.474_MoDate 39:59 12.00 n/a .000
00441#
00442# Sum of hydrographs from Node 8 routed to Node 7
00443# Section 4
00444#
00445# R002/C00048-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00446# ROUTE CHANNEL -> 1.0 02:01M8 38546.00 40.474_MoDate 39:59 12.00 n/a .000
00447# [RDP= 1.00] out<= 1.0 01:01M7 38546.00 32.892_MoDate 44:30 12.00 n/a .000
00448# [L/S= 3750 / .053/.070]
00449# [Vmax=.208;Dmax=1.651]
00450#
00451# Addition of Subwatershed 7 to Node 7
00452#
00453# R002/C00049-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00454# ADD HYD + 1.0 02:01M7 38546.00 32.892_MoDate 44:30 12.00 n/a .000
00455# + 1.0 02:01M7 3197.00 4.651_MoDate 36:31 9.45 n/a .000
00456# + 1.0 01:01M7 38743.00 35.071_MoDate 43:33 11.82 n/a .000
00457# SUM= 1.0 01:01M7 38743.00 35.071_MoDate 43:33 11.82 n/a .000
00458# SAVE HYD + 1.0 01:01M7 38743.00 35.071_MoDate 43:33 11.82 n/a .000
00459# frame_H_LBPT
00460# remark:flow at_R7: M7 + SW_7
00461# Insertion of a Reservoir to simulate the effects of the Richmond Fen.
00462# Storage area and volumes were estimated from available topo maps.
00463# Release rate from Fen was assumed to be controlled by the downstream
00464# a river cross-section for which it is assumed that for up to
00465# 0.75 m of water, the main channel of the river provided the storage. Above
00466# this depth, the wetland starts to significantly store water.
00467#
00468# R002/C00051-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00469# ROUTE CHANNEL -> 1.0 02:01M7 38743.00 35.071_MoDate 43:33 11.82 n/a .000
00470# out<= 1.0 01:RES_RP 38743.00 23.265_MoDate 55:09 11.82 n/a .000
00471# [MedSto=7001.0;V=0]
00472# R002/C00052-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00473# SAVE HYD + 1.0 01:RES_RP 38743.00 23.265_MoDate 55:09 11.82 n/a .000
00474# frame_H_ResFp
00475# remark:outflow of Richmond Fen
00476#
00477# Sum of hydrographs from Node 7 routed to Node 6
00478# Section 5
00479#
00480# R002/C00053-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00481# ROUTE CHANNEL -> 1.0 02:01M7 38743.00 23.265_MoDate 55:09 11.82 n/a .000
00482# [RDP= 1.00] out<= 1.0 01:01M6 38743.00 23.228_MoDate 56:38 11.82 n/a .000
00483# [L/S= 3036 / .081/.040]
00484# [Vmax=.432;Dmax=.808]
00485#
00486# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
00487#
00488# R002/C00054-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00489# ADD HYD + 1.0 02:01M6 38743.00 23.228_MoDate 56:38 11.82 n/a .000
00490# + 1.0 02:01M6 1455.00 4.412_MoDate 28:12 11.94 n/a .000
00491# + 1.0 02:01M2 1332.00 3.148_MoDate 35:23 13.94 n/a .000
00492# SUM= 1.0 01:01M6 40949.00 23.318_MoDate 39:59 11.89 n/a .000
00493#
00494# Sum of hydrographs from Node 6 routed to Node 5
00495# Section 6
00496#
00497# R002/C00055-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00498# ROUTE CHANNEL -> 1.0 02:01M6 40949.00 23.318_MoDate 39:59 11.89 n/a .000
00499# [RDP= 1.00] out<= 1.0 01:01M5 40949.00 23.285_MoDate 56:09 11.89 n/a .000
00500# [L/S= 3036 / .057/.040]
00501# [Vmax=.378;Dmax=.917]
00502#
00503# Addition of Subwatershed 5 and Flowing Creek to Node 5
00504#
00505# R002/C00056-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00506# ADD HYD + 1.0 02:01M5 40949.00 23.285_MoDate 56:09 11.89 n/a .000
00507# + 1.0 02:01M5 224.94 2.587_MoDate 28:12 11.94 n/a .000
00508# + 1.0 02:01M2 4949.00 14.839_MoDate 33:25 14.57 n/a .000
00509# SUM= 1.0 01:01M5 45408.00 31.366_MoDate 37:08 12.20 n/a .000
00510#
00511# Sum of hydrographs from Node 5 routed to Node 5A
00512# Section 7
00513#
00514# R002/C00057-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00515# ROUTE CHANNEL -> 1.0 02:01M5 45409.00 31.366_MoDate 37:08 12.20 n/a .000
00516# [RDP= 1.00] out<= 1.0 01:01M5A 45409.00 31.335_MoDate 37:20 12.20 n/a .000
00517# [L/S= 556 / .090/.040]
00518# [Vmax=.443;Dmax=.937]
00519#
00520# Addition of Subwatershed 5A and Subwatershed 5A2 to Node 5A
00521#
00522# R002/C00058-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00523# ADD HYD + 1.0 02:01M5A 45409.00 31.335_MoDate 37:20 12.20 n/a .000
00524# + 1.0 02:01M5A 20.00 0.509_MoDate 28:16 12.20 n/a .000
00525# + 1.0 02:01M5A 1622.00 3.090_MoDate 38:04 15.22 n/a .000
00526# SUM= 1.0 01:01M5A 46841.00 36.236_MoDate 37:28 12.30 n/a .000
00527#
00528# Sum of hydrographs from Node 5A routed to Node 4
00529# Section 8
00530#
00531# R002/C00059-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00532# ROUTE CHANNEL -> 1.0 02:01M5A 46841.00 36.236_MoDate 37:28 12.30 n/a .000
00533# [RDP= 1.00] out<= 1.0 01:01M4 46841.00 35.288_MoDate 37:28 12.30 n/a .000
00534# [L/S= 4630 / .043/.035]
00535# [Vmax=.695;Dmax=2.444]
00536#
00537# Addition of Subwatershed 4 and Leamy Creek to Node 4
00538#
00539# R002/C00060-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00540# ADD HYD + 1.0 02:01M4 46841.00 35.288_MoDate 37:28 12.30 n/a .000
00541# + 1.0 02:01M4 585.00 4.325_MoDate 29:58 17.79 n/a .000
00542# + 1.0 02:01M2 1022.00 5.747_MoDate 30:50 17.39 n/a .000
00543# SUM= 1.0 01:01M4 48447.00 37.581_MoDate 38:13 12.47 n/a .000
00544# R002/C00061-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00545# SAVE HYD + 1.0 01:01M4 48447.00 37.581_MoDate 38:13 12.47 n/a .000
00546# frame_R_4.0002
00547# remark:flow at_R_4
00548#
00549# Sum of hydrographs from Node 4 routed to Node 2
00550# Section 9
00551#
00552# R002/C00062-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00553# ROUTE CHANNEL -> 1.0 02:01M4 48447.00 37.581_MoDate 38:13 12.47 n/a .000
00554# [RDP= 1.00] out<= 1.0 01:01M2 48447.00 37.455_MoDate 38:49 12.47 n/a .000
00555# [L/S= 1467 / .060/.040]
00556# [Vmax=.715;Dmax=2.485]
00557#
00558# Addition of Subwatershed 2 with Monahan Drain and Smith Drain to Node 2
00559#
00560# R002/C00063-----DtmIn-ID:HYD-----AREAh-QPEARcMs-TPeakDate,h:mm-----RvM-R,C-----DWPFms
00561# ADD HYD + 1.0 02:01M2 48447.00 37.455_MoDate 38:49 12.47 n/a .000

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018171 SAVE HYD 1.0 01:01:00 54681.13 48.551 NoDate 39:29 13.09 n/a .000
018172 # frame 'SN_KB_0002
018173 # remark 'HYD_COMMENT('Total Flows before Station 3633')
018174 # Hydrograph from Station 3633 to Node Todd
018175 # Channel X-Section obtained from RWCA Hydraulic Model - Station 3633
018176 # JFSA 2021-01-26 change the channel length (at station 3633) from 650m to 608m and change the slope from 0.0498 to 0.2
018177 #
018178 ROUTE CHANNEL --> 1.0 01:01:00 54681.13 48.552 NoDate 37:57 13.09 n/a .000
018180 # [L/S=] 608 / 247 / 0.01:01:00
018182 # [Max= 1.291Dmax= 1.13]
018183 #
018184 # Catchment CORRID
018185 # - To Greenbank Drain (south of the Jock)
018186 # - JFSA 2021-01-18 as per Greenbank pond as per JFSA_P598(04)-11 June 2016
018187 # - JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GIS measurements
018188 #
018189 R0002:CO0274 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018190 # CONTINUOUS STANDBY 1.0 01:01:00 36.60 2.954 NoDate 28:02 32.54 715 .000
018192 # [XMP= 64:7TMD= 64]
018193 # [LOSS= 2 CEN 77.0]
018194 # [Previous area: IArea= 4.67:SLP=1.00:LIG= 40.IMP= 250:SCP= 0]
018195 # [Impervious area: IArea= 1.57:SLP=1.00:LIG= 494.IMP= 0.13:SCI= 0]
018196 # [IARCSimp= 4.00: IARCCover= 4.00]
018197 # [SMIN= 31.15: SMAX=207.66: SK= 0.10]
018198 R0002:CO0275 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018199 # ROUTE RESERVOIR --> 1.0 01:01:00 36.60 2.954 NoDate 28:02 32.54 n/a .000
018200 # out <= 1.0 01:01:00 36.60 2.954 NoDate 28:02 32.54 n/a .000
018201 # [MxToStd= 4.05E+00 n3, TotVolVol= 0.000E+00 n3, N-ovf= 0, TotDurDv= 0 hrs]
018202 R0002:CO0276 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018203 # ADD HYD + 1.0 01:01:00 54681.13 48.552 NoDate 37:57 13.09 n/a .000
018204 # + 1.0 01:01:00 54681.13 48.552 NoDate 37:57 13.09 n/a .000
018205 # + 1.0 01:01:00 54681.13 48.552 NoDate 37:57 13.09 n/a .000
018206 # SIM= 1.0 01:01:00 54681.13 48.552 NoDate 37:57 13.09 n/a .000
018207 R0002:CO0277 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018208 # SAVE HYD 1.0 01:01:00 54681.13 48.552 NoDate 37:57 13.09 n/a .000
018209 # frame 'Green0002
018210 # remark 'Total Flows at Greenbank Drain
018211 #
018212 # Catchment CORRID
018213 # - To Todd Drain (south of the Jock)
018214 # - Subdivision with 438 imp as per Barrowhen South MSS
018215 # - 2020-11-30 increase area based on P598(04)-11
018216 # - 2020-11-30 update TODD Tributary Drainage area to 146.015 ha based on P598(04)-11
018217 #
018218 # JFSA 2021-01-19 add 'TODD_MH1' as part of clake('M.CLAM1') and remove it from Todd
018219 R0002:CO0278 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018220 # CONTINUOUS STANDBY 1.0 01:01:00 146.015 1.79 NoDate 28:00 28.91 635 .000
018222 # [LOSS= 2 CEN 77.0]
018223 # [Previous area: IArea= 4.67:SLP=1.00:LIG= 40.IMP= 250:SCP= 0]
018224 # [Impervious area: IArea= 1.57:SLP=1.00:LIG= 118.IMP= 0.13:SCI= 0]
018225 # [IARCSimp= 4.00: IARCCover= 4.00]
018226 # [SMIN= 31.15: SMAX=207.66: SK= 0.10]
018227 R0002:CO0279 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018228 # CONTINUOUS STANDBY 1.0 01:01:00 146.015 1.79 NoDate 28:00 28.91 635 .000
018229 # [XMP= 53:TMD= 57]
018230 # [LOSS= 2 CEN 77.0]
018231 # [Previous area: IArea= 4.67:SLP=1.00:LIG= 40.IMP= 250:SCP= 0]
018232 # [Impervious area: IArea= 1.57:SLP=1.00:LIG= 28.IMP= 0.13:SCI= 0]
018233 # [IARCSimp= 4.00: IARCCover= 4.00]
018234 # [SMIN= 31.15: SMAX=207.66: SK= 0.10]
018235 R0002:CO0280 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018236 # CONTINUOUS STANDBY 1.0 01:01:00 30.23 2.154 NoDate 28:03 29.64 651 .000
018238 # [XMP= 52:TMD= 64]
018239 # [LOSS= 2 CEN 77.0]
018240 # [Previous area: IArea= 4.67:SLP=1.00:LIG= 40.IMP= 250:SCP= 0]
018241 # [Impervious area: IArea= 1.57:SLP=1.00:LIG= 449.IMP= 0.13:SCI= 0]
018242 # [IARCSimp= 4.00: IARCCover= 4.00]
018243 # [SMIN= 31.15: SMAX=207.66: SK= 0.10]
018244 R0002:CO0281 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018245 # CONTINUOUS STANDBY 1.0 01:01:00 112.91 6.553 NoDate 28:06 28.70 631 .000
018246 # [XMP= 64:7TMD= 64]
018247 # [LOSS= 2 CEN 77.0]
018248 # [Previous area: IArea= 4.67:SLP=1.00:LIG= 40.IMP= 250:SCP= 0]
018249 # [Impervious area: IArea= 1.57:SLP=1.00:LIG= 868.IMP= 0.13:SCI= 0]
018250 # [IARCSimp= 4.00: IARCCover= 4.00]
018251 # [SMIN= 31.15: SMAX=207.66: SK= 0.10]
018252 R0002:CO0282 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018253 # CONTINUOUS STANDBY 1.0 01:01:00 9.06 1.198 NoDate 28:00 31.76 658 .000
018254 # [XMP= 63:TMD= 63]
018255 # [LOSS= 2 CEN 77.0]
018256 # [Previous area: IArea= 4.67:SLP=1.00:LIG= 40.IMP= 250:SCP= 0]
018257 # [Impervious area: IArea= 1.57:SLP=1.00:LIG= 143.IMP= 0.13:SCI= 0]
018258 # [IARCSimp= 4.00: IARCCover= 4.00]
018259 # [SMIN= 31.15: SMAX=207.66: SK= 0.10]
018260 # 5-Year + 12h Capture
018261 R0002:CO0283 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018262 # ROUTE RESERVOIR --> 1.0 01:01:00 30.23 2.154 NoDate 28:03 29.64 n/a .000
018263 # out <= 1.0 01:01:00 30.23 2.154 NoDate 28:03 29.64 n/a .000
018264 # [MxToStd= 6.761E+04 n3, TotVolVol= 0.000E+00 n3, N-ovf= 0, TotDurDv= 0 hrs]
018265 # [MxToStd= 6.761E+04 n3, TotVolVol= 0.000E+00 n3, N-ovf= 0, TotDurDv= 0 hrs]
018266 # 5-Year + 12h Capture
018267 R0002:CO0284 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018268 # ROUTE RESERVOIR --> 1.0 01:01:00 2.10 1.79 NoDate 28:00 28.91 n/a .000
018269 # out <= 1.0 01:01:00 2.10 1.79 NoDate 28:00 28.91 n/a .000
018270 # [MxToStd= 6.761E+04 n3, TotVolVol= 0.000E+00 n3, N-ovf= 0, TotDurDv= 0 hrs]
018271 # [MxToStd= 6.761E+04 n3, TotVolVol= 0.000E+00 n3, N-ovf= 0, TotDurDv= 0 hrs]
018272 R0002:CO0285 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018273 # ROUTE RESERVOIR --> 1.0 01:01:00 12.00 1.00 NoDate 28:00 28.91 n/a .000
018274 # out <= 1.0 01:01:00 12.00 1.00 NoDate 28:00 28.91 n/a .000
018275 # [MxToStd= 6.666E+04 n3, TotVolVol= 0.000E+00 n3, N-ovf= 0, TotDurDv= 0 hrs]
018276 # [MxToStd= 6.666E+04 n3, TotVolVol= 0.000E+00 n3, N-ovf= 0, TotDurDv= 0 hrs]
018277 R0002:CO0286 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018278 # CONTINUOUS STANDBY 1.0 01:01:00 25.50 1.427 NoDate 28:04 25.60 563 .000
018279 # [XMP= 77:0]
018280 # [LOSS= 2 CEN 75.0]
018281 # [Previous area: IArea= 4.67:SLP=1.00:LIG= 40.IMP= 250:SCP= 0]
018282 # [Impervious area: IArea= 1.57:SLP=1.00:LIG= 566.IMP= 0.13:SCI= 0]
018283 # [IARCSimp= 4.00: IARCCover= 4.00]
018284 # [SMIN= 31.15: SMAX=207.66: SK= 0.10]
018285 R0002:CO0287 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018286 # COMPUTE DIALYD + 1.0 01:01:00 2.10 1.79 NoDate 28:00 28.91 n/a .000
018287 # Major System / 1.0 01:01:00 2.10 1.79 NoDate 28:00 28.91 n/a .000
018288 # Minor System / 1.0 01:01:00 2.10 1.79 NoDate 28:00 28.91 n/a .000
018289 # [MjSysSto= 0.000E+00, TotVolVol= 0.000E+00, N-ovf= 0, TotDurDv= 0 hrs]
018290 # [MjSysSto= 0.000E+00, TotVolVol= 0.000E+00, N-ovf= 0, TotDurDv= 0 hrs]
018291 R0002:CO0288 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018292 # ADD HYD + 1.0 01:01:00 54681.13 48.552 NoDate 37:57 13.09 n/a .000
018293 # + 1.0 01:01:00 54681.13 48.552 NoDate 37:57 13.09 n/a .000
018294 # + 1.0 01:01:00 54681.13 48.552 NoDate 37:57 13.09 n/a .000
018295 # SIM= 1.0 01:01:00 54681.13 48.552 NoDate 37:57 13.09 n/a .000
018296 R0002:CO0289 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018297 # SAVE HYD 1.0 01:01:00 54681.13 48.552 NoDate 37:57 13.09 n/a .000
018298 # frame 'TDD_0002
018299 # remark 'Total Flows at Todd Drain
018300 #
018301 # Todd Drain 3
018302 # - Rating curve obtained from Barrowhen South MSS modeling
018303 # - atnatic 2007, Tributary Drainage Area to WES Round 3 = 193 ha
018304 #
018305 R0002:CO0290 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018306 # ROUTE RESERVOIR --> 1.0 01:01:00 119.95 6.882 NoDate 28:05 28.77 n/a .000
018307 # out <= 1.0 01:01:00 119.95 6.882 NoDate 28:05 28.76 n/a .000
018308 # [MxToStd= 2.183E+01 n3, TotVolVol= 0.000E+00 n3, N-ovf= 0, TotDurDv= 0 hrs]
018309 # [MxToStd= 2.183E+01 n3, TotVolVol= 0.000E+00 n3, N-ovf= 0, TotDurDv= 0 hrs]
018310 R0002:CO0291 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018311 # ADD HYD + 1.0 01:01:00 54681.13 48.552 NoDate 37:57 13.09 n/a .000
018312 # + 1.0 01:01:00 54681.13 48.552 NoDate 37:57 13.09 n/a .000
018313 # + 1.0 01:01:00 54681.13 48.552 NoDate 37:57 13.09 n/a .000
018314 # SIM= 1.0 01:01:00 54681.13 48.552 NoDate 37:57 13.09 n/a .000
018315 R0002:CO0292 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018316 # SAVE HYD 1.0 01:01:00 54681.13 48.552 NoDate 37:57 13.09 n/a .000
018317 # frame 'SN_TO_0002
018318 # remark 'Total Flows at Todd Drain
018319 #
018320 # Hydrograph from Todd Drain routed to Corrigan Drain
018321 # Channel X-Section obtained from RWCA Hydraulic Model - Station 2462
018322 # 2021-02-19 Change the slope from 0.033 % (as per Stantec Report 2007) to 0.05 % so the model will be more stable and g
018323 R0002:CO0293 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018324 # ROUTE CHANNEL --> 1.0 01:01:00 54837.69 48.739 NoDate 37:56 13.13 n/a .000
018325 # [L/S=] 280 / 0.50 / 0.45]
018326 # [Max= 1.727Dmax= 1.13]
018327 R0002:CO0294 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018328 # CONTINUOUS STANDBY 1.0 01:01:00 54837.69 48.720 NoDate 38:09 13.13 n/a .000
018329 # [XMP= 63:TMD= 63]
018330 # [LOSS= 2 CEN 77.0]
018331 # [Previous area: IArea= 4.67:SLP=1.00:LIG= 40.IMP= 250:SCP= 0]
018332 # [Impervious area: IArea= 1.57:SLP=1.00:LIG= 325.IMP= 0.13:SCI= 0]
018333 # [IARCSimp= 4.00: IARCCover= 4.00]
018334 # [SMIN= 31.15: SMAX=207.66: SK= 0.10]
018335 R0002:CO0295 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018336 # COMPUTE DIALYD + 1.0 01:01:00 15.87 1.352 NoDate 28:02 31.77 n/a .000
018337 # Major System / 1.0 01:01:00 15.87 1.352 NoDate 28:02 31.77 n/a .000
018338 # Minor System / 1.0 01:01:00 15.87 1.352 NoDate 28:02 31.77 n/a .000
018339 # [MjSysSto= 0.000E+00, TotVolVol= 0.000E+00, N-ovf= 0, TotDurDv= 0 hrs]
018340 # [MjSysSto= 0.000E+00, TotVolVol= 0.000E+00, N-ovf= 0, TotDurDv= 0 hrs]
018341 R0002:CO0296 -----DRAIN-ID:HYD-----AREHA-QPEARCS-TpeakeDate_hh:mm-----Rvwm-R.C-----DWPFCS
018342 # CONTINUOUS STANDBY 1.0 01:01:00 12.47 1.00 NoDate 29:12 14.83 326 .000
018343 # [CN 77.0] N= 3.00] Tpe= 1.0]
018344 # [Previous area: IArea= 4.67:SLP=1.00:LIG= 40.IMP= 250:SCP= 0]
018345 # [Impervious area: IArea= 1.57:SLP=1.00:LIG= 388.IMP= 0.13:SCI= 0]

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026139 # Catchment DESIRE
026140 # - To Jock River (north of the Jock)
026141 # - Rural-estate subdivision (Heart's Desire Community)
02622 # *****
02623 # R0002-C00393-----DtmIn-ID:HYD-----AREAhA-GPEAKCms-TpeakDate_hh:mm-----RvM-R.C-----DWFCms
02624 # CONTINUOUS NASHVD 1.0 01:SR_25 23.78 .936 NoDate 28:03 19:26 423 .000
02625 # [XMP=50;TMD=50]
02626 # [LQ8= 2;CN= 77.0]
02627 # [IperV= 4.67;SLP=1.00;LDP= 40.0;NMP=250;SCP= .0]
02628 # [IperV= 4.00;IAlp= 1.57;SLP=1.00;LDP= 40.0;NMP=250;SCP= .0]
02629 # [IAREC= 4.00;EMIM= 39.75;SMAX=264.99;SK= .010]
02630 # [SMIN= 31.15;SMAX=264.99;SK= .010]
02631 # [InterVTime= 12.00]
02632 # *****
02633 # Catchment Jockvale
02634 # - To Jockvale RM Facility
02635 # - Residential development & golf course
02636 # - JPSA 2021-01 update JOCKVA after updating CORRIE as per IRI CORREP, July 2008.
02637 # - JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX-LAND 32.5 ha as
02638 # *****
02639 # R0002-C00394-----DtmIn-ID:HYD-----AREAhA-GPEAKCms-TpeakDate_hh:mm-----RvM-R.C-----DWFCms
02640 # CONTINUOUS NASHVD 1.0 01:SR_25 225.13 10.636 NoDate 28:10 26:45 430 .000
02641 # [XMP=50;TMD=50]
02642 # [LQ8= 2;CN= 74.0]
02643 # [IperV= 4.67;SLP=1.00;LDP= 40.0;NMP=250;SCP= .0]
02644 # [IperV= 4.00;IAlp= 1.57;SLP=1.00;LDP= 40.0;NMP=250;SCP= .0]
02645 # [IAREC= 4.00;EMIM= 39.75;SMAX=264.99;SK= .010]
02646 # [SMIN= 36.67;SMAX=264.99;SK= .010]
02647 # AREAhA-GPEAKCms-TpeakDate_hh:mm-----RvM-R.C-----DWFCms
02648 # ADD HYD 1.0 02:IR-LAND-NM 32.50 2.093 NoDate 28:02 26:85 n/a .000
02649 # + 1.0 02:JOCKVA 225.13 10.636 NoDate 28:10 26:85 n/a .000
02650 # + 1.0 02:IR-NM .00 .000 NoDate 0:00 .00 n/a .000
02651 # SUM= 1.0 02:IR-NM 287.63 12.214 NoDate 28:07 26:85 n/a .000
02652 # R0002-C00396-----DtmIn-ID:HYD-----AREAhA-GPEAKCms-TpeakDate_hh:mm-----RvM-R.C-----DWFCms
02653 # SAVE HYD 1.0 01:JOCKVA-TO_0002 257.63 12.214 NoDate 28:07 26:85 n/a .000
02654 # fname JOCKVA-TO_0002
02655 # remark Total Flows at KB first pond
02656 # *****
02657 # Jockvale RM Facility
02658 # Rating curve obtained from Jockvale Servicing Study (OCL 1999)
02659 # *****
02660 # R0002-C00399-----DtmIn-ID:HYD-----AREAhA-GPEAKCms-TpeakDate_hh:mm-----RvM-R.C-----DWFCms
02661 # ROUTE RESERVOIR -> 1.0 02:JOCKVA-TO 257.63 12.214 NoDate 28:07 26:85 n/a .000
02662 # out <= 1.0 01:JOCK_P 257.63 2.660 NoDate 29:05 26:85 n/a .000
02663 # overFlow= 1.0 02:OWF 102.94 1.373 NoDate 28:20 13:01 n/a .000
02664 # [MstUsed= .333AE=0;L;TotDvVol=0.000;N3=N;Dv= 0;TotDvOv= 0;hrr]
02665 # R0002-C00398-----DtmIn-ID:HYD-----AREAhA-GPEAKCms-TpeakDate_hh:mm-----RvM-R.C-----DWFCms
02666 # ADD HYD 1.0 02:IR_DE 55194.85 49.114 NoDate 38:33 13:21 n/a .000
02667 # + 1.0 02:DESIRE 23.78 .936 NoDate 28:03 19:26 n/a .000
02668 # + 1.0 02:OWF 102.94 1.373 NoDate 28:20 13:01 n/a .000
02669 # + 1.0 02:JOCK_P 257.63 2.660 NoDate 29:05 26:85 n/a .000
02670 # SUM= 1.0 01:RES_RM 55476.26 49.482 NoDate 38:27 13:27 n/a .000
02671 # R0002-C00399-----DtmIn-ID:HYD-----AREAhA-GPEAKCms-TpeakDate_hh:mm-----RvM-R.C-----DWFCms
02672 # SAVE HYD 1.0 01:IR_DE 55476.26 49.482 NoDate 38:27 13:27 n/a .000
02673 # fname IR_DE_0002
02674 # remark Total Flows at Heart's Desire
02675 # *****
02676 # Hydrograph from Heart's Desire routed to Rideau River
02677 # Channel X-section obtained from RPS Hydrologic Model - Station 0
02678 # *****
02679 # R0002-C00400-----DtmIn-ID:HYD-----AREAhA-GPEAKCms-TpeakDate_hh:mm-----RvM-R.C-----DWFCms
02680 # ROUTE CHANNEL -> 1.0 02:IR_DE 55476.26 49.482 NoDate 38:27 13:27 n/a .000
02681 # [RFD= 1.00] out<= 1.0 01:RM 55476.26 49.482 NoDate 38:33 13:27 n/a .000
02682 # [L/S= 563; / 967;0.65]
02683 # [Vmax= 1.489;Dmax= .800]
02684 # [InterVTime= 12.00]
02685 # *****
02686 # Catchment S-2
02687 # - To Jock River (north and south)
02688 # - Undeveloped floodplain
02689 # *****
02690 # R0002-C00401-----DtmIn-ID:HYD-----AREAhA-GPEAKCms-TpeakDate_hh:mm-----RvM-R.C-----DWFCms
02691 # CONTINUOUS NASHVD 1.0 01:SR_2 102.94 1.373 NoDate 28:20 13:01 286 .000
02692 # [CN= 72.0;N= 3.00;T= 1.5]
02693 # [IAREC= 4.00;EMIM= 39.75;SMAX=264.99;SK= .010]
02694 # [InterVTime= 12.00]
02695 # *****
02696 # R0002-C00402-----DtmIn-ID:HYD-----AREAhA-GPEAKCms-TpeakDate_hh:mm-----RvM-R.C-----DWFCms
02697 # ADD HYD 1.0 02:IR 55476.26 49.480 NoDate 38:33 13:27 n/a .000
02698 # + 1.0 02:SR_2 102.94 1.373 NoDate 28:20 13:01 n/a .000
02699 # + 1.0 02:IR_NM 55579.20 49.578 NoDate 38:33 13:27 n/a .000
02700 # R0002-C00403-----DtmIn-ID:HYD-----AREAhA-GPEAKCms-TpeakDate_hh:mm-----RvM-R.C-----DWFCms
02701 # SAVE HYD 1.0 01:IR_NM 55579.20 49.578 NoDate 38:33 13:27 n/a .000
02702 # fname IR_NM_0002
02703 # remark Total Flows at Rideau River
02704 # *****
02705 # *****
02706 # *****
02707 # *****
02708 # *****
02709 # *****
02710 # *****
02711 # RIN=COMMANDS
02712 # *****
02713 # START
02714 # [TZERO = .00 hrs on 0]
02715 # [INST02 = 1 (1=imperial, 2=metric output)]
02716 # [INST06 = 1]
02717 # [RIN = 0005 ]
02718 # *****
02719 # SMMHYD Ver:02/Jan 2001 <SETA> / INPUT DATA FILE
02720 # *****
02721 # Project Name [Jock River] Project Number: [1474-16]
02722 # Date [01-01-2021]
02723 # Modeller [M.M.]
02724 # Company [JFSaInc.]
02725 # License # [284923]
02726 # *****
02727 # CALIBRATION & VALIDATION SUMMARY
02728 # USING CONTINUOUS SIMULATIONS
02729 # Rainfall data from FRS rain gauge installed at site + other gauges by City
02730 # See data collect from May 1st to July 14, 2003
02731 # 2010-11-30 change TMDSTO IN COMPUTE DUALYD (TMDSTO = 0.1 instead of 0.0001)
02732 # 2020-11-01 correct total curve
02733 # 2020-11-01 change W_LAR_SBR_XIMP to 0.55, SLP([0.5]) (impervious slope), and LDI up to 70m
02734 # 2021-02-18 change the slope for ROUTE CHANNEL (MSTO="R_001") from 0.033 to 0.033 & (as per 03)
02735 # 2021-02-19 Change the slope for ROUTE CHANNEL ST002 (INHVD="H_NM_C") from 0.01 & (as per 03)
02736 # *****
02737 # R0005-C00002-----DtmIn-ID:HYD-----AREAhA-GPEAKCms-TpeakDate_hh:mm-----RvM-R.C-----DWFCms
02738 # READ STORM
02739 # filename storm.001
02740 # Comment # pluie SCS de 24 hrs 1:5 ans pour Ottawa CDA
02741 # [LQ8= 2;CN= 24.00;TMD= 97.12]
02742 # [RFD= 1.00]
02743 # *****
02744 # MODIFY STORM
02745 # [IAREC= 1.00;TMD= 96.00 min]
02746 # [RFD= 1.00;SDR= 40.00;PFD= 57.12]
02747 # *****
02748 # R0005-C00004-----DtmIn-ID:HYD-----AREAhA-GPEAKCms-TpeakDate_hh:mm-----RvM-R.C-----DWFCms
02749 # DEFAULT VALUES
02750 # filename = T:\WORK\1474-16\Design\20201026-QuantityControlAnalysis\SMMHYD\SRM-Model\updated\Citigade.DEP
02751 # [CORREV = 1 (read and print data)]
02752 # FileTitle File comment: [Based on various calibration exercises in Ont]
02753 # [USE THE USER PARAMETERS ARE USED BY THE REGION STANDARD COM]
02754 # Horton's infiltration equation parameters:
02755 # [F= 76.20 mm/hr] [F=12.20 mm/hr] [COCY= 4.14 /hr] [F= .00 mm]
02756 # Parameters for DEVI008 surfaces in STANHYD:
02757 # [IperV= 4.67 mm] [LQ8=50.00] [NMP= .250]
02758 # Parameters for IMPREV008 surfaces in STANHYD:
02759 # [IAlp= 1.57 mm] [CL=1.50] [NMP= .013]
02760 # Parameters used in NASHVD:
02761 # [Ia= 4.67 mm] [N= 3.00]
02762 # Average monthly Pan Evaporation data in (mm)
02763 # JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
02764 # 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00
02765 # Average monthly Potential Evapotranspiration in (mm)
02766 # JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
02767 # 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00
02768 # R0005-C00005-----DtmIn-ID:HYD-----AREAhA-GPEAKCms-TpeakDate_hh:mm-----RvM-R.C-----DWFCms
02769 # COMPUTE AP
02770 # [Iare= 50.00; AP1kty= .8500; AP1kty= .9989]
02771 # [AP1kty= 90.83; AP1kty= 60.09; AP1kty= 44.87]
02772 # *****
02773 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02774 # of 1.32
02775 # R0005-C00006-----DtmIn-ID:HYD-----AREAhA-GPEAKCms-TpeakDate_hh:mm-----RvM-R.C-----DWFCms
02776 # CONTINUOUS NASHVD 1.0 01:SR_RM 3680.00 9.398 NoDate 37:02 16.41 287 .000
02777 # [CN= 60.0;N= 3.00;T= 1.5]
02778 # [IAREC= 4.00;EMIM= 39.75;SMAX=380.32;SK= .010]
02779 # [InterVTime= 12.00]
02780 # *****
02781 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02782 # of 1.32
02783 # R0005-C00007-----DtmIn-ID:HYD-----AREAhA-GPEAKCms-TpeakDate_hh:mm-----RvM-R.C-----DWFCms
02784 # CONTINUOUS NASHVD 1.0 01:SR_RM 3680.00 9.398 NoDate 37:02 16.41 287 .000
02785 # [CN= 60.0;N= 3.00;T= 1.76]
02786 # [IAREC= 4.00;EMIM= 39.75;SMAX=430.01;SK= .010]
02787 # [InterVTime= 12.00]
02788 # *****
02789 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02790 # of 1.32
02791 # R0005-C00008-----DtmIn-ID:HYD-----AREAhA-GPEAKCms-TpeakDate_hh:mm-----RvM-R.C-----DWFCms
02792 # CONTINUOUS NASHVD 1.0 01:SR_RM 3074.00 4.682 NoDate 39:59 13.23 232 .000
02793 # [CN= 60.0;N= 3.00;T= 1.24]
02794 # [IAREC= 4.00;EMIM= 39.75;SMAX=554.96;SK= .010]
02795 # [InterVTime= 12.00]
02796 # *****
02797 # R0005-C00009-----DtmIn-ID:HYD-----AREAhA-GPEAKCms-TpeakDate_hh:mm-----RvM-R.C-----DWFCms
02798 # CONTINUOUS NASHVD 1.0 01:SR_ASH 1781.00 8.521 NoDate 32:43 20.12 352 .000
02799 # [CN= 72.0;N= 3.00;T= 1.83]
02800 # [IAREC= 4.00;EMIM= 39.75;SMAX=264.99;SK= .010]
02801 # [InterVTime= 12.00]
02802 # *****
02803 # R0005-C00010-----DtmIn-ID:HYD-----AREAhA-GPEAKCms-TpeakDate_hh:mm-----RvM-R.C-----DWFCms
02804 # CONTINUOUS NASHVD 1.0 01:SR_M1 500.00 4.354 NoDate 29:22 17.18 301 .000
02805 # [CN= 60.0;N= 3.00;T= 1.24]
02806 # [IAREC= 4.00;EMIM= 39.75;SMAX=350.79;SK= .010]
02807 # [InterVTime= 12.00]
02808 # *****
02809 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)

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052377 SAVE HYD 1.0 01:SN_MI 55194.85 70.602 NoDate 37:03 18.87 n/a .000
052384 frame :SN_MI_0005
052385 remark:Total Flows at Jockvale Road
052400 #
052410 # Hydrograph from Jockvale Road routed to Heart's Desire
052420 # Channel X-Section obtained from RWCA Hydraulic Model - Station 689
052430 #
052440 R005:CO0393-----Dtain-ID:HYD-----AREHA-OPEARcMs-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
052450 ROUTE CHANNEL -> 1.0 01:SN_MI 55194.85 70.676 NoDate 27:57 18.87 n/a .000
052460 [RDT=1.00] out<- 1.0 01:SN_DE 55194.85 70.452 NoDate 37:20 18.87 n/a .000
052470 [L/S=1967. / 2217. / 0.02]
052480 [Wmax=1.101Dmax=1.891]
052490 #
052500 # Catchment OVERVIEW
052510 # - To Jock River (north of the Jock)
052520 # Rural (Heart's Desire Community)
052530 #
052540 R005:CO0393-----Dtain-ID:HYD-----AREHA-OPEARcMs-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
052550 CONTINUOUS STANNYD
052560 [XIMP=25:TIMP=25]
052570 [L0S=2:CM=77.0]
052580 [Previous area IArea:4.67:SLPP=1.00:LDW=40:RMD=250:RCP=0]
052590 [Impervious area IArea:1.57:SLPP=1.00:LDW=400:RMD=013:RCP=0]
052600 [IareCimp=4.00:IareCp=4.00]
052610 [SMIN=31.15:SMAX=207.66:SK=010]
052620 #
052630 # Catchment JOCKVA
052640 # - To Jockvale SWM Facility
052650 # - Residential development & golf course
052660 # - JFRA 2021-01-11 update JOCKVA after updating CORRID as per IRI GROUP, July 2008.
052670 # JOCKVA area becomes 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX-LAND 32.5 ha as
052680 #
052690 R005:CO0394-----Dtain-ID:HYD-----AREHA-OPEARcMs-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
052700 CONTINUOUS STANNYD 1.0 01:JOCKVA 225.13 14.675 NoDate 28:09 35.73 4.26 .000
052710 [XIMP=50:TIMP=50]
052720 [L0S=2:CM=74.0]
052730 [Previous area IArea:4.67:SLPP=1.00:LDW=40:RMD=250:RCP=0]
052740 [Impervious area IArea:1.57:SLPP=1.00:LDW=400:RMD=013:RCP=0]
052750 [IareCimp=4.00:IareCp=4.00]
052760 [SMIN=26.67:SMAX=264.99:SK=010]
052770 R005:CO0395-----Dtain-ID:HYD-----AREHA-OPEARcMs-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
052780 ADD HYD + 1.0 02:JOCKVA 225.13 14.675 NoDate 28:09 35.73 n/a .000
052790 + 1.0 02:JOCKVA 225.13 14.675 NoDate 28:09 35.73 n/a .000
052800 + 1.0 02:R2-DM 0.00 0.00 NoDate 0:00 0.00 n/a .000
052810 + 1.0 02:R2-DM 0.00 0.00 NoDate 0:00 0.00 n/a .000
052820 SUM= 1.0 01:JOCKVA 257.63 16.950 NoDate 28:09 35.73 n/a .000
052830 R005:CO0396-----Dtain-ID:HYD-----AREHA-OPEARcMs-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
052840 SAVE HYD 1.0 01:JOCKVA 257.63 16.950 NoDate 28:09 35.73 n/a .000
052850 frame :JOCKVA_TO_0005
052860 remark:Total Flows at KB first pond
052870 #
052880 # Jockvale SWM Facility
052890 # - Rating curve obtained from Jockvale Servicing Study (CCL 1999)
052900 #
052910 R005:CO0397-----Dtain-ID:HYD-----AREHA-OPEARcMs-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
052920 ROUTE RESERVOIR -> 1.0 02:JOCKVA 257.63 16.950 NoDate 28:09 35.73 n/a .000
052930 [RDT=1.00] out<- 1.0 01:JOCK_P 257.63 4.781 NoDate 28:48 35.73 n/a .000
052940 [overflow=0.0 03:20:OVF 0.00 0.00 NoDate 0:00 0.00 n/a .000]
052950 [MaxOutflow=10:SL0=1.0:TotOutflow=0.0005:0=0.63:R=0:V=0:TotInflow=0.0]
052960 R005:CO0398-----Dtain-ID:HYD-----AREHA-OPEARcMs-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
052970 ADD HYD + 1.0 02:DE 55194.85 70.452 NoDate 37:20 18.87 n/a .000
052980 + 1.0 02:RESERVE 23.78 1.359 NoDate 28:09 35.73 n/a .000
052990 + 1.0 02:OVF 0.00 0.00 NoDate 0:00 0.00 n/a .000
053000 + 1.0 02:JOCK_P 257.63 4.781 NoDate 28:48 35.73 n/a .000
053010 SUM= 1.0 01:SN_DE 55476.26 71.017 NoDate 37:17 18.95 n/a .000
053020 R005:CO0399-----Dtain-ID:HYD-----AREHA-OPEARcMs-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
053030 SAVE HYD 1.0 01:SN_DE 55476.26 71.017 NoDate 37:17 18.95 n/a .000
053040 frame :SN_DE_0005
053050 remark:Total Flows at Heart's Desire
053060 #
053070 # Hydrograph from Heart's Desire routed to Rideau River
053080 # Channel X-Section obtained from RWCA Hydraulic Model - Station 0
053090 #
053100 R005:CO0400-----Dtain-ID:HYD-----AREHA-OPEARcMs-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
053110 ROUTE CHANNEL -> 1.0 02:SN_DE 55476.26 71.017 NoDate 37:17 18.95 n/a .000
053120 [RDT=1.00] out<- 1.0 01:SN_DE 55476.26 71.028 NoDate 37:08 18.95 n/a .000
053130 [L/S=963. / 967. / 0.05]
053140 [Wmax=1.676:Max=1.676]
053150 #
053160 # Catchment S-2
053170 # - To Jock River (north and south)
053180 # Undeveloped floodplain and river
053190 #
053200 R005:CO0401-----Dtain-ID:HYD-----AREHA-OPEARcMs-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
053210 CONTINUOUS STANNYD 1.0 01:SN_DE 102.94 2.262 NoDate 28:20 19.00 .333 .000
053220 [IareC=4.00:SMIN=39.75:SMAX=264.99:SK=010]
053230 #
053240 R005:CO0402-----Dtain-ID:HYD-----AREHA-OPEARcMs-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
053250 ADD HYD + 1.0 02:R2-DM 102.94 2.262 NoDate 28:20 19.00 n/a .000
053260 + 1.0 02:R2-DM 102.94 2.262 NoDate 28:20 19.00 n/a .000
053270 SUM= 1.0 01:SN_DE 102.94 2.262 NoDate 28:20 19.00 n/a .000
053280 R005:CO0403-----Dtain-ID:HYD-----AREHA-OPEARcMs-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
053290 SAVE HYD 1.0 01:SN_MI 55579.20 71.168 NoDate 37:08 18.95 n/a .000
053300 frame :SN_MI_0005
053310 remark:Total Flows at Rideau River
053320 ***** END OF RUN *****
053330 ** END OF RUN **
053340 #
053350 #
053360 #
053370 #
053380 #
053390 #
053400 #
053410 #
053420 R005:CO0404-----Dtain-ID:HYD-----AREHA-OPEARcMs-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
053430 START
053440 [TZERO=0:00:00]
053450 [MFCOEF=2:1:Imperial,2:metric output]
053460 [MFCOEF=2:1:Imperial,2:metric output]
053470 [MFCOEF=2:1:Imperial,2:metric output]
053480 [MFCOEF=2:1:Imperial,2:metric output]
053490 #
053500 # SWMM6 User's Manual 2003: INPUT DATA FILE
053510 #
053520 # Project Name: (Project Name) Project Number: (1474-16)
053530 # Date: 04-03-2021
053540 # Modeler: (J.F.S.)
053550 # Company: JFSaInc.
053560 # License #: 2549237
053570 #
053580 # CALIBRATION OF SUMMER MODEL PARAMETERS
053590 # USING CONSERVATION SUMMER MODEL
053600 # Rainfall data from JFRA range to installed at site + other gauges by 0.001
053610 # Use data collected from May 1st to July 14, 2001
053620 # 2020-11-10 Change TRNPD in CONSERVATION TRNPD=0.3 instead of 0.2001
053630 # 2020-11-01 correct pond curve values
053640 # 2020-11-01 Change the slope for ROUTE CHANNEL Station 2442 (Impervious slope), and LID up to 700m
053650 # 2021-02-19 Change the slope for ROUTE CHANNEL Station 2442 (Impervious slope), and LID up to 700m
053660 # 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (Impervious slope), and LID up to 700m
053670 #
053680 #
053690 #
053700 #
053710 #
053720 #
053730 #
053740 #
053750 #
053760 #
053770 #
053780 #
053790 #
053800 #
053810 #
053820 #
053830 #
053840 #
053850 #
053860 #
053870 #
053880 #
053890 #
053900 #
053910 #
053920 #
053930 #
053940 #
053950 #
053960 #
053970 #
053980 #
053990 #
054000 #
054010 #
054020 #
054030 #
054040 #
054050 #
054060 #
054070 #
054080 #
054090 #
054100 #
054110 #
054120 #
054130 #
054140 #
054150 #
054160 #
054170 #
054180 #
054190 #
054200 #
054210 #
054220 #
054230 #
054240 #
054250 #
054260 #
054270 #
054280 #
054290 #
054300 #
054310 #
054320 #
054330 #
054340 #
054350 #
054360 #
054370 #
054380 #
054390 #
054400 #
054410 #
054420 #
054430 #
054440 #
054450 #
054460 #
054470 #
054480 #
054490 #
054500 #
054510 #
054520 #
054530 #
054540 #
054550 #
054560 #
054570 #
054580 #
054590 #
054600 #
054610 #
054620 #
054630 #
054640 #
054650 #
054660 #
054670 #
054680 #
054690 #
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056080 #
056090 #
056100 #

```



05611 # (Vmax :.546;Dmax:1.499)
05612 #
05613 # Addition of Subwatershed Jock River at Ashton to Node 12
05614 #
05615 R0101:C00036 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05616 ADD HYD + 1.0 02:18:12 7725.00 3.619\_NDate 61:53 18.46 n/a .000
05617 + 1.0 02:18:28 1781.00 10.819\_NDate 32:42 24.81 n/a .000
05618 SUM= 1.0 01:18:12 9506.00 12.834\_NDate 32:45 19.65 n/a .000
05619 DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05620 SAVE HYD 1.0 01:18:12 9506.00 12.834\_NDate 32:45 19.65 n/a .000
05621 frame\_H\_RHS10
05622 remark:flow at\_RHS1 near Ashton
05623 #
05624 # Sum of hydrographs from Node 12 routed to Node 11
05625 # [Approximated cross-section - see cross-section 258]
05626 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
05627 #
05628 # Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
05629 #
05630 R0101:C00038 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05631 ROUTE CHANNEL -> 1.0 02:18:M10 25965.00 12.316\_NDate 32:45 19.65 n/a .000
05632 [RDY 1.00] out<= 1.0 01:18:M11 11923.00 12.710\_NDate 33:02 19.65 n/a .000
05633 [L/S= 3056. / .057 / .845]
05634 (Vmax :.680;Dmax:2.598)
05635 #
05636 # Addition of Subwatershed 11 and No Name Creek to Node 11
05637 #
05638 R0101:C00039 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05639 ADD HYD + 1.0 02:18:M10 9506.00 12.710\_NDate 33:02 19.65 n/a .000
05640 + 1.0 02:18:M11 5656.00 9.639\_NDate 29:22 21.19 n/a .000
05641 SUM= 1.0 02:18:M10 15162.00 21.813\_NDate 33:05 19.96 n/a .000
05642 + 1.0 01:18:M11 11923.00 21.813\_NDate 33:05 19.96 n/a .000
05643 #
05644 # Sum of hydrographs from Node 11 routed to Node 10
05645 # Section 1
05646 #
05647 R0101:C00040 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05648 ROUTE CHANNEL -> 1.0 02:18:M11 11923.00 21.813\_NDate 33:05 19.96 n/a .000
05649 [RDY 1.00] out<= 1.0 01:M10 11923.00 14.761\_NDate 39:58 19.96 n/a .000
05650 [L/S= 14028. / .157 / .845]
05651 (Vmax :.452;Dmax:1.212)
05652 #
05653 # Addition of Subwatershed 10 to Node 10
05654 #
05655 R0101:C00041 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05656 ADD HYD + 1.0 02:18:M10 11923.00 14.761\_NDate 39:58 19.96 n/a .000
05657 + 1.0 02:18:M10 5656.00 21.255\_NDate 37:58 24.81 n/a .000
05658 SUM= 1.0 01:18:M10 17579.00 35.808\_NDate 38:35 21.52 n/a .000
05659 R0101:C00042 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05660 SAVE HYD 1.0 01:18:M10 17579.00 35.808\_NDate 38:35 21.52 n/a .000
05661 frame\_H\_RHS10
05662 remark:flow at\_RHS10 M10 + SK\_10
05663 #
05664 # Addition of Kings Creek to S\_M10
05665 #
05666 R0101:C00043 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05667 ADD HYD + 1.0 02:18:M10 17579.00 35.808\_NDate 38:35 21.52 n/a .000
05668 + 1.0 02:18:M10 8176.00 20.398\_NDate 39:59 21.19 n/a .000
05669 SUM= 1.0 01:18:M10 25965.00 55.807\_NDate 39:58 21.41 n/a .000
05670 #
05671 # Sum of hydrographs from Node 10 routed to Node 9
05672 # Section 2
05673 #
05674 R0101:C00044 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05675 ROUTE CHANNEL -> 1.0 02:18:M10 25965.00 55.807\_NDate 39:58 21.41 n/a .000
05676 [RDY 1.00] out<= 1.0 01:18:R 25965.00 54.076\_NDate 39:59 21.41 n/a .000
05677 [L/S= 2750. / .075 / .845]
05678 (Vmax :.682;Dmax:1.695)
05679 #
05680 # Addition of Subwatershed 9 and Nichols Creek to Node 9
05681 #
05682 R0101:C00045 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05683 ADD HYD + 1.0 02:18:R 31561.00 61.483\_NDate 39:57 21.20 n/a .000
05684 + 1.0 02:18:R 31561.00 61.483\_NDate 39:57 21.20 n/a .000
05685 SUM= 1.0 02:18:R 63122.00 123.966\_NDate 39:59 21.19 n/a .000
05686 + 1.0 01:18:R 31561.00 61.483\_NDate 39:57 21.19 n/a .000
05687 #
05688 # Sum of hydrographs from Node 9 routed to Node 8
05689 # Section 3
05690 #
05691 R0101:C00046 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05692 ROUTE CHANNEL -> 1.0 02:18:R 31561.00 61.483\_NDate 39:57 21.20 n/a .000
05693 [RDY 1.00] out<= 1.0 01:18:R 31561.00 61.483\_NDate 39:57 21.20 n/a .000
05694 [L/S= 1822. / .057 / .845]
05695 (Vmax :.363;Dmax:1.619)
05696 #
05697 # Addition of Subwatershed 8 and Bobb's Drain to Node 8
05698 #
05699 R0101:C00047 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05700 ADD HYD + 1.0 02:18:R 31561.00 61.483\_NDate 39:57 21.19 n/a .000
05701 + 1.0 02:18:R 31561.00 61.483\_NDate 39:57 21.19 n/a .000
05702 SUM= 1.0 02:18:R 63122.00 123.966\_NDate 39:57 21.19 n/a .000
05703 + 1.0 01:18:R 31561.00 61.483\_NDate 39:57 21.19 n/a .000
05704 #
05705 # Sum of hydrographs from Node 8 routed to Node 7
05706 # Section 4
05707 #
05708 R0101:C00048 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05709 ROUTE CHANNEL -> 1.0 02:18:R 31561.00 61.483\_NDate 39:57 21.19 n/a .000
05710 [RDY 1.00] out<= 1.0 01:18:R 31561.00 61.483\_NDate 39:57 21.19 n/a .000
05711 [L/S= 2750. / .057 / .845]
05712 (Vmax :.218;Dmax:1.987)
05713 #
05714 # Addition of Subwatershed 7 to Node 7
05715 #
05716 R0101:C00049 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05717 ADD HYD + 1.0 02:18:R 31561.00 61.483\_NDate 39:57 21.19 n/a .000
05718 + 1.0 02:18:R 31561.00 61.483\_NDate 39:57 21.19 n/a .000
05719 SUM= 1.0 02:18:R 63122.00 123.966\_NDate 39:57 21.19 n/a .000
05720 + 1.0 01:18:R 31561.00 61.483\_NDate 39:57 21.19 n/a .000
05721 #
05722 # Insertion of a reservoir to simulate the effects of the Richmond Fen
05723 # Storage area and volumes were obtained from available topo maps
05724 # Release rate from Fen was assumed to be controlled by the downstream
05725 # river cross-section for summer conditions. It is assumed that for up to
05726 # 0.75 m of water, the main channel of the river provided the storage. Above
05727 # this depth, the wetland starts to significantly store water.
05728 #
05729 R0101:C00051 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05730 ROUTE CHANNEL -> 1.0 02:18:R 38743.00 65.819\_NDate 44:06 20.85 n/a .000
05731 [RDY 1.00] out<= 1.0 01:RES\_RP 38743.00 31.796\_NDate 60:32 20.85 n/a .000
05732 [L/S= 25965. / .057 / .845]
05733 (Vmax :.477;Dmax:.960)
05734 #
05735 # Addition of Subwatershed 6 and Van Gaal Drain to Node 6
05736 #
05737 R0101:C00052 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05738 ADD HYD + 1.0 02:18:R 38743.00 65.819\_NDate 44:06 20.85 n/a .000
05739 + 1.0 02:18:R 38743.00 65.819\_NDate 44:06 20.85 n/a .000
05740 SUM= 1.0 02:18:R 77486.00 131.638\_NDate 44:06 20.85 n/a .000
05741 + 1.0 01:18:R 38743.00 65.819\_NDate 44:06 20.85 n/a .000
05742 #
05743 # Sum of hydrographs from Node 6 routed to Node 5
05744 # Section 5
05745 #
05746 R0101:C00053 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05747 ROUTE CHANNEL -> 1.0 02:18:R 38743.00 65.819\_NDate 44:06 20.85 n/a .000
05748 [RDY 1.00] out<= 1.0 01:18:R 38743.00 31.797\_NDate 62:00 20.85 n/a .000
05749 [L/S= 3056. / .057 / .845]
05750 (Vmax :.477;Dmax:.960)
05751 #
05752 # Addition of Subwatershed 5 and Flowing Creek to Node 5
05753 #
05754 R0101:C00054 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05755 ADD HYD + 1.0 02:18:R 38743.00 31.797\_NDate 62:00 20.85 n/a .000
05756 + 1.0 02:18:R 38743.00 31.797\_NDate 62:00 20.85 n/a .000
05757 SUM= 1.0 02:18:R 77486.00 63.594\_NDate 62:00 20.85 n/a .000
05758 + 1.0 01:18:R 38743.00 31.797\_NDate 62:00 20.85 n/a .000
05759 #
05760 # Sum of hydrographs from Node 5 routed to Node 4
05761 # Section 6
05762 #
05763 R0101:C00055 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05764 ROUTE CHANNEL -> 1.0 02:18:R 38743.00 31.797\_NDate 62:00 20.85 n/a .000
05765 [RDY 1.00] out<= 1.0 01:18:R 38743.00 31.797\_NDate 62:00 20.85 n/a .000
05766 [L/S= 3056. / .057 / .845]
05767 (Vmax :.412;Dmax:1.069)
05768 #
05769 # Addition of Subwatershed 4 and Leamy Creek to Node 4
05770 #
05771 R0101:C00056 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05772 ADD HYD + 1.0 02:18:R 38743.00 31.797\_NDate 62:00 20.85 n/a .000
05773 + 1.0 02:18:R 38743.00 31.797\_NDate 62:00 20.85 n/a .000
05774 SUM= 1.0 02:18:R 77486.00 63.594\_NDate 62:00 20.85 n/a .000
05775 + 1.0 01:18:R 38743.00 31.797\_NDate 62:00 20.85 n/a .000
05776 #
05777 # Sum of hydrographs from Node 4 routed to Node 3
05778 # Section 7
05779 #
05780 R0101:C00057 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05781 ROUTE CHANNEL -> 1.0 02:18:R 38743.00 31.797\_NDate 62:00 20.85 n/a .000
05782 [RDY 1.00] out<= 1.0 01:18:R 38743.00 31.797\_NDate 62:00 20.85 n/a .000
05783 [L/S= 3056. / .057 / .845]
05784 (Vmax :.485;Dmax:1.331)
05785 #
05786 # Addition of Subwatershed 3 and Subwatershed 3A2 to Node 3A
05787 #
05788 R0101:C00058 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05789 ADD HYD + 1.0 02:18:R 38743.00 31.797\_NDate 62:00 20.85 n/a .000
05790 + 1.0 02:18:R 38743.00 31.797\_NDate 62:00 20.85 n/a .000
05791 SUM= 1.0 02:18:R 77486.00 63.594\_NDate 62:00 20.85 n/a .000
05792 + 1.0 01:18:R 38743.00 31.797\_NDate 62:00 20.85 n/a .000
05793 #
05794 # Sum of hydrographs from Node 3A routed to Node 2
05795 # Section 8
05796 #
05797 R0101:C00059 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05798 ROUTE CHANNEL -> 1.0 02:18:R 38743.00 31.797\_NDate 62:00 20.85 n/a .000
05799 [RDY 1.00] out<= 1.0 01:18:R 38743.00 31.797\_NDate 62:00 20.85 n/a .000
05800 [L/S= 4630. / .043 / .035]
05801 (Vmax :.793;Dmax:3.295)
05802 #
05803 # Addition of Subwatershed 2 with Monahan Drain and Smith Drain to Node 2
05804 #
05805 R0101:C00060 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05806 ADD HYD + 1.0 02:18:R 48447.00 59.698\_NDate 36:12 22.03 n/a .000
05807 + 1.0 02:18:R 48447.00 59.698\_NDate 36:12 22.03 n/a .000
05808 SUM= 1.0 02:18:R 96894.00 119.396\_NDate 36:12 22.03 n/a .000
05809 + 1.0 01:18:R 48447.00 59.698\_NDate 36:12 22.03 n/a .000
05810 #
05811 # Sum of hydrographs from Node 4 routed to Node 2
05812 # Section 9
05813 #
05814 R0101:C00062 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05815 ROUTE CHANNEL -> 1.0 02:18:R 48447.00 59.698\_NDate 36:12 22.03 n/a .000
05816 [RDY 1.00] out<= 1.0 01:18:R 48447.00 59.698\_NDate 36:12 22.03 n/a .000
05817 [L/S= 1667. / .050 / .040]
05818 (Vmax :.546;Dmax:1.499)
05819 #
05820 # Addition of Subwatershed 2 with Monahan Drain and Smith Drain to Node 2
05821 #
05822 R0101:C00063 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05823 ADD HYD + 1.0 02:18:R 48447.00 59.698\_NDate 36:12 22.03 n/a .000
05824 + 1.0 02:18:R 48447.00 59.698\_NDate 36:12 22.03 n/a .000
05825 SUM= 1.0 02:18:R 96894.00 119.396\_NDate 36:12 22.03 n/a .000
05826 + 1.0 02:18:R 48447.00 59.698\_NDate 36:12 22.03 n/a .000
05827 #
05828 R0101:C00064 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05829 SAVE HYD 1.0 01:18:R 96894.00 119.396\_NDate 36:12 22.03 n/a .000
05830 frame\_H\_RHS10
05831 remark:flow at\_RHS2 Jock River Gauged at Moodie Dr.
05832 #
05833 # Sum of hydrographs from Node 2 routed to Node 1
05834 # Section 10
05835 #
05836 R0101:C00065 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05837 ROUTE CHANNEL -> 1.0 02:18:R 48447.00 59.698\_NDate 36:12 22.03 n/a .000
05838 [RDY 1.00] out<= 1.0 01:18:R 48447.00 59.698\_NDate 36:12 22.03 n/a .000
05839 [L/S= 1667. / .050 / .040]
05840 (Vmax :.705;Dmax:2.943)
05841 #
05842 # Hydrograph from Node 2 routed to Node 416
05843 # Channel X-Section obtained from RWCA Hydraulic Model - Station 9025
05844 #
05845 R0101:C00066 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05846 ROUTE CHANNEL -> 1.0 02:18:R 48447.00 59.698\_NDate 36:12 22.03 n/a .000
05847 [RDY 1.00] out<= 1.0 01:18:R 48447.00 59.698\_NDate 36:12 22.03 n/a .000
05848 [L/S= 1667. / .050 / .040]
05849 (Vmax :.705;Dmax:2.943)
05850 #
05851 # Catchment SM-1a
05852 # - Portion of RWCA catchment SM-1a outside of Reach 1 subwatershed
05853 # - Underlain by artificial aquifer
05854 #
05855 R0101:C00067 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05856 CONTINUOUS NASHYD 1.0 01:18:R 536.42 3.888\_NDate 31:17 23.57 364 .000
05857 [Cm: 72.0; H: 3.00; Tm: 2.9]
05858 [Imperv: area: IArea= 4.67;SLDp= 1.32;LSD= 440.0;IMP= .035;ICP= .0]
05859 [L/S= 4.00; IArea= 4.67;SLDp= 1.32;LSD= 440.0;IMP= .035;ICP= .0]
05860 [Vmax :.75;Dmax:2.943]
05861 #
05862 # Catchment SM-1a
05863 # - Portion of RWCA catchment SM-1a outside of Reach 1 subwatershed
05864 # - Underlain by artificial aquifer
05865 #
05866 R0101:C00068 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05867 ADD HYD + 1.0 02:18:R 536.42 3.888\_NDate 31:17 23.57 364 .000
05868 + 1.0 02:18:R 536.42 3.888\_NDate 31:17 23.57 364 .000
05869 SUM= 1.0 02:18:R 1072.84 7.776\_NDate 31:17 23.57 364 .000
05870 + 1.0 01:18:R 536.42 3.888\_NDate 31:17 23.57 364 .000
05871 #
05872 # Hydrograph from Node 416 routed to Node 2 at Okeefe drain
05873 # Channel X-Section obtained from RWCA Hydraulic Model - Station 7245
05874 #
05875 R0101:C00069 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05876 ROUTE CHANNEL -> 1.0 02:18:R 536.42 3.888\_NDate 31:17 23.57 364 .000
05877 [RDY 1.00] out<= 1.0 01:18:R 536.42 3.888\_NDate 31:17 23.57 364 .000
05878 [L/S= 4.00; IArea= 4.67;SLDp= 1.32;LSD= 440.0;IMP= .035;ICP= .0]
05879 (Vmax :.450;Dmax:2.495)
05880 #
05881 # Catchment OKEEFE
05882 # - To O'Keefe drain (north of the Jock)
05883 # - Developed with assumed 416 imp
05884 # - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area 513.02 HA)
05885 # - 2020-12-01 Okeefe model was added as per the NOVATECH BROWNO model (Cell-426 2041).
05886 #
05887 R0101:C00070 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05888 CONTINUOUS NASHYD 1.0 01:18:R 63.72 684\_NDate 28:58 17.24 266 .000
05889 [Cm: 61.0; H: 3.00; Tm: .90]
05890 [Imperv: area: IArea= 4.67;SLDp= 1.32;LSD= 440.0;IMP= .035;ICP= .0]
05891 [L/S= 4.00; IArea= 4.67;SLDp= 1.32;LSD= 440.0;IMP= .035;ICP= .0]
05892 [Vmax :.75;Dmax:2.943]
05893 #
05894 # Catchment OKEEFE
05895 # - To O'Keefe drain (north of the Jock)
05896 # - Developed with assumed 416 imp
05897 # - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area 513.02 HA)
05898 # - 2020-12-01 Okeefe model was added as per the NOVATECH BROWNO model (Cell-426 2041).
05899 #
05900 R0101:C00071 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05901 CONTINUOUS NASHYD 1.0 01:18:R 63.72 684\_NDate 28:58 17.24 266 .000
05902 [Cm: 61.0; H: 3.00; Tm: .90]
05903 [Imperv: area: IArea= 4.67;SLDp= 1.32;LSD= 440.0;IMP= .035;ICP= .0]
05904 [L/S= 4.00; IArea= 4.67;SLDp= 1.32;LSD= 440.0;IMP= .035;ICP= .0]
05905 [Vmax :.75;Dmax:2.943]
05906 #
05907 # Catchment OKEEFE
05908 # - To O'Keefe drain (north of the Jock)
05909 # - Developed with assumed 416 imp
05910 # - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area 513.02 HA)
05911 # - 2020-12-01 Okeefe model was added as per the NOVATECH BROWNO model (Cell-426 2041).
05912 #
05913 R0101:C00072 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05914 CONTINUOUS NASHYD 1.0 01:18:R 63.72 684\_NDate 28:58 17.24 266 .000
05915 [Cm: 61.0; H: 3.00; Tm: .90]
05916 [Imperv: area: IArea= 4.67;SLDp= 1.32;LSD= 440.0;IMP= .035;ICP= .0]
05917 [L/S= 4.00; IArea= 4.67;SLDp= 1.32;LSD= 440.0;IMP= .035;ICP= .0]
05918 [Vmax :.75;Dmax:2.943]
05919 #
05920 # Catchment OKEEFE
05921 # - To O'Keefe drain (north of the Jock)
05922 # - Developed with assumed 416 imp
05923 # - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area 513.02 HA)
05924 # - 2020-12-01 Okeefe model was added as per the NOVATECH BROWNO model (Cell-426 2041).
05925 #
05926 R0101:C00073 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05927 CONTINUOUS NASHYD 1.0 01:18:R 63.72 684\_NDate 28:58 17.24 266 .000
05928 [Cm: 61.0; H: 3.00; Tm: .90]
05929 [Imperv: area: IArea= 4.67;SLDp= 1.32;LSD= 440.0;IMP= .035;ICP= .0]
05930 [L/S= 4.00; IArea= 4.67;SLDp= 1.32;LSD= 440.0;IMP= .035;ICP= .0]
05931 [Vmax :.75;Dmax:2.943]
05932 #
05933 # Catchment OKEEFE
05934 # - To O'Keefe drain (north of the Jock)
05935 # - Developed with assumed 416 imp
05936 # - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area 513.02 HA)
05937 # - 2020-12-01 Okeefe model was added as per the NOVATECH BROWNO model (Cell-426 2041).
05938 #
05939 R0101:C00074 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05940 CONTINUOUS NASHYD 1.0 01:18:R 63.72 684\_NDate 28:58 17.24 266 .000
05941 [Cm: 61.0; H: 3.00; Tm: .90]
05942 [Imperv: area: IArea= 4.67;SLDp= 1.32;LSD= 440.0;IMP= .035;ICP= .0]
05943 [L/S= 4.00; IArea= 4.67;SLDp= 1.32;LSD= 440.0;IMP= .035;ICP= .0]
05944 [Vmax :.75;Dmax:2.943]
05945 #
05946 # Catchment OKEEFE
05947 # - To O'Keefe drain (north of the Jock)
05948 # - Developed with assumed 416 imp
05949 # - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area 513.02 HA)
05950 # - 2020-12-01 Okeefe model was added as per the NOVATECH BROWNO model (Cell-426 2041).
05951 #
05952 R0101:C00075 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05953 CONTINUOUS NASHYD 1.0 01:18:R 63.72 684\_NDate 28:58 17.24 266 .000
05954 [Cm: 61.0; H: 3.00; Tm: .90]
05955 [Imperv: area: IArea= 4.67;SLDp= 1.32;LSD= 440.0;IMP= .035;ICP= .0]
05956 [L/S= 4.00; IArea= 4.67;SLDp= 1.32;LSD= 440.0;IMP= .035;ICP= .0]
05957 [Vmax :.75;Dmax:2.943]
05958 #
05959 # Catchment OKEEFE
05960 # - To O'Keefe drain (north of the Jock)
05961 # - Developed with assumed 416 imp
05962 # - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area 513.02 HA)
05963 # - 2020-12-01 Okeefe model was added as per the NOVATECH BROWNO model (Cell-426 2041).
05964 #
05965 R0101:C00076 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05966 CONTINUOUS NASHYD 1.0 01:18:R 63.72 684\_NDate 28:58 17.24 266 .000
05967 [Cm: 61.0; H: 3.00; Tm: .90]
05968 [Imperv: area: IArea= 4.67;SLDp= 1.32;LSD= 440.0;IMP= .035;ICP= .0]
05969 [L/S= 4.00; IArea= 4.67;SLDp= 1.32;LSD= 440.0;IMP= .035;ICP= .0]
05970 [Vmax :.75;Dmax:2.943]
05971 #
05972 # Catchment OKEEFE
05973 # - To O'Keefe drain (north of the Jock)
05974 # - Developed with assumed 416 imp
05975 # - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area 513.02 HA)
05976 # - 2020-12-01 Okeefe model was added as per the NOVATECH BROWNO model (Cell-426 2041).
05977 #
05978 R0101:C00077 -----DtnIn-ID:HYD-----AREHA-QPEARcm-TpeakDate\_hh:mm-----Rvm-R.C-----DWfcm
05979 CONTINUOUS NASHYD 1.0 01:18:R 63.72 684\_NDate 28:58 17.24 266 .000
05980 [Cm: 61.0; H: 3.00; Tm: .90]
05981 [Imperv: area: IArea= 4.67;SLDp= 1.32;LSD=



06359 # [Impervious area IAlp=1.57SLP1-50.1MI=1473.NMI-.013:SCI-.0]
06360 # [ISRC= 4.00 IAREP= 4.00]
06361 # [SMIN=36.67I SMAK=244.49I SK=.010]
06362 #
06363 # Poster Pond
06364 # - Rating curve obtained assuming 4003/ha in 24 hours for quality control
06365 # and a ratio of the catchment area to the West Clarke pond rating curve
06366 # from the MSF for the next coordinates
06367 #
06368 #
06369 #
06370 #
06371 #
06372 # [MsfTotAed=.1341E+03 TotVolVol=.000E+00 N=0.0V=0.0 TotDurDv=0.0 hrs]
06373 #
06374 # ADD HYD + 1.0 0.018E-007 325.44 6.061 NoDate 29:06 43.99 n/a .000
06375 #
06376 # SUM= 1.0 0.018E-007 325.44 6.061 NoDate 29:06 43.99 n/a .000
06377 #
06378 #
06379 #
06380 #
06381 #
06382 #
06383 # [Impervious area IAlp=4.67SLP1-50.1MI=699.NMI-.013:SCI-.0]
06384 # [ISRC= 4.00 IAREP= 4.00]
06385 # [SMIN=31.15I SMAK=207.66I SK=.010]
06386 #
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082229 # (MxStoUsed=.1192E+03)
082230 #
082231 ROUTES+CO0034-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082232 SAVE HYD + 1.0 01:RES_DM 7725.00 3.678_MoDate 60:27 23.92 n/a .000
082233 #
082234 # name_H_RESUM
082235 #
082236 # remark:Outflow from Res Q
082237 #
082238 # Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
082239 # [Approximated cross-section - see cross-section 258]
082240 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
082241 #
082242 ROUTE CHANNEL --> 1.0 02:RES_DM 7725.00 3.678_MoDate 60:27 23.92 n/a .000
082243 [RPT= 1.00] out-< 1.0 01:RES_DM 7725.00 3.678_MoDate 63:05 23.92 n/a .000
082244 [L/S/n= 5926./ / .076/.040]
082245 [Vmax=.592/Dmax= 1.204]
082246 #
082247 # Addition of Subwatershed Jock River at Ashton to Node 12
082248 #
082249 ROUTES+CO0036-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082250 ADD HYD + 1.0 01:RES_DM 7725.00 3.678_MoDate 63:05 23.92 n/a .000
082251 #
082252 # name_H_RESUM
082253 #
082254 # remark:flow at S_M12 near Ashton
082255 #
082256 # Sum of hydrographs from Node 12 routed to Node 11
082257 # [Approximated cross-section - see cross-section 258]
082258 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
082259 #
082260 # Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
082261 #
082262 ROUTES+CO0038-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082263 ADD HYD + 1.0 01:RES_DM 7725.00 3.678_MoDate 63:05 23.92 n/a .000
082264 #
082265 # name_H_RESUM
082266 #
082267 # remark:flow at S_M12 near Ashton
082268 #
082269 # Addition of Subwatershed 11 and No Name Creek to Node 11
082270 #
082271 ROUTES+CO0039-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082272 ADD HYD + 1.0 01:RES_DM 9000.00 16.007_MoDate 33:02 25.02 n/a .000
082273 #
082274 # name_H_RESUM
082275 #
082276 # remark:flow at S_M10 N10 = S_M10
082277 #
082278 # Sum of hydrographs from Node 11 routed to Node 10
082279 #
082280 ROUTES+CO0040-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082281 ADD HYD + 1.0 02:RES_DM 11923.00 27.908_MoDate 33:04 25.01 n/a .000
082282 #
082283 # name_H_RESUM
082284 #
082285 # remark:flow at S_M10 N10 = S_M10
082286 #
082287 # Addition of Subwatershed 10 to Node 10
082288 #
082289 ROUTES+CO0041-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082290 ADD HYD + 1.0 02:RES_DM 11923.00 27.908_MoDate 33:04 25.01 n/a .000
082291 #
082292 # name_H_RESUM
082293 #
082294 # remark:flow at S_M10 N10 = S_M10
082295 #
082296 # Sum of hydrographs from Node 10 routed to Node 9
082297 #
082298 ROUTES+CO0042-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082299 ADD HYD + 1.0 02:RES_DM 17859.00 45.026_MoDate 38:35 27.38 n/a .000
082300 #
082301 # name_H_RESUM
082302 #
082303 # remark:flow at S_M10 N10 = S_M10
082304 #
082305 # Addition of Kings Creek to S_M10
082306 #
082307 ROUTES+CO0043-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082308 ADD HYD + 1.0 02:RES_DM 17859.00 45.026_MoDate 38:35 27.38 n/a .000
082309 #
082310 # name_H_RESUM
082311 #
082312 # remark:flow at S_M10 N10 = S_M10
082313 #
082314 # Addition of Subwatershed 9 and Nichols Creek to Node 9
082315 #
082316 ROUTES+CO0044-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082317 ADD HYD + 1.0 02:RES_DM 25965.00 70.812_MoDate 39:59 27.26 n/a .000
082318 #
082319 # name_H_RESUM
082320 #
082321 # remark:flow at S_M10 N10 = S_M10
082322 #
082323 # Sum of hydrographs from Node 9 routed to Node 8
082324 #
082325 ROUTES+CO0045-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082326 ADD HYD + 1.0 02:RES_DM 25965.00 70.812_MoDate 39:59 27.26 n/a .000
082327 #
082328 # name_H_RESUM
082329 #
082330 # remark:flow at S_M10 N10 = S_M10
082331 #
082332 # Addition of Subwatershed 8 and Robb's Drain to Node 8
082333 #
082334 ROUTES+CO0046-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082335 ADD HYD + 1.0 02:RES_DM 31561.00 84.684_MoDate 39:59 26.99 n/a .000
082336 #
082337 # name_H_RESUM
082338 #
082339 # remark:flow at S_M10 N10 = S_M10
082340 #
082341 # Sum of hydrographs from Node 8 routed to Node 7
082342 #
082343 ROUTES+CO0047-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082344 ADD HYD + 1.0 02:RES_DM 31561.00 84.684_MoDate 39:59 26.99 n/a .000
082345 #
082346 # name_H_RESUM
082347 #
082348 # remark:flow at S_M10 N10 = S_M10
082349 #
082350 # Insertion of a reservoir to simulate the effects of the Richmond Fen.
082351 # Storage area and volumes were estimated from available top maps.
082352 # Release rates were assumed to be controlled by the downstream
082353 # river cross-section for summer conditions. It is assumed that for up to
082354 # 18.75 m of water, the main channel of the river provided the storage. Above
082355 # this depth, the wetland starts to significantly store water.
082356 #
082357 ROUTES+CO0048-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082358 ADD HYD + 1.0 02:RES_DM 31561.00 84.684_MoDate 39:59 26.99 n/a .000
082359 #
082360 # name_H_RESUM
082361 #
082362 # remark:flow at S_M10 N10 = S_M10
082363 #
082364 # Addition of Subwatershed 7 to Node 7
082365 #
082366 ROUTES+CO0049-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082367 ADD HYD + 1.0 02:RES_DM 31561.00 84.684_MoDate 39:59 26.99 n/a .000
082368 #
082369 # name_H_RESUM
082370 #
082371 # remark:flow at S_M10 N10 = S_M10
082372 #
082373 # Sum of hydrographs from Node 7 routed to Node 6
082374 #
082375 ROUTES+CO0050-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082376 ADD HYD + 1.0 02:RES_DM 31561.00 84.684_MoDate 39:59 26.99 n/a .000
082377 #
082378 # name_H_RESUM
082379 #
082380 # remark:flow at S_M10 N10 = S_M10
082381 #
082382 # Addition of Subwatershed 6 and Van Gaal Drain to Node 6
082383 #
082384 ROUTES+CO0051-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082385 ADD HYD + 1.0 02:RES_DM 31561.00 84.684_MoDate 39:59 26.99 n/a .000
082386 #
082387 # name_H_RESUM
082388 #
082389 # remark:flow at S_M10 N10 = S_M10
082390 #
082391 # Sum of hydrographs from Node 6 routed to Node 5
082392 #
082393 ROUTES+CO0052-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082394 ADD HYD + 1.0 02:RES_DM 31561.00 84.684_MoDate 39:59 26.99 n/a .000
082395 #
082396 # name_H_RESUM
082397 #
082398 # remark:flow at S_M10 N10 = S_M10
082399 #
082400 # Addition of Subwatershed 5 and Flowing Creek to Node 5
082401 #
082402 ROUTES+CO0053-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082403 ADD HYD + 1.0 02:RES_DM 31561.00 84.684_MoDate 39:59 26.99 n/a .000
082404 #
082405 # name_H_RESUM
082406 #
082407 # remark:flow at S_M10 N10 = S_M10
082408 #
082409 # Sum of hydrographs from Node 5 routed to Node 5A
082410 #
082411 ROUTES+CO0054-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082412 ADD HYD + 1.0 02:RES_DM 31561.00 84.684_MoDate 39:59 26.99 n/a .000
082413 #
082414 # name_H_RESUM
082415 #
082416 # remark:flow at S_M10 N10 = S_M10
082417 #
082418 # Addition of Subwatershed 5A and Subwatershed 5A2 to Node 5A
082419 #
082420 ROUTES+CO0055-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082421 ADD HYD + 1.0 02:RES_DM 31561.00 84.684_MoDate 39:59 26.99 n/a .000
082422 #
082423 # name_H_RESUM
082424 #
082425 # remark:flow at S_M10 N10 = S_M10
082426 #
082427 # Sum of hydrographs from Node 5A routed to Node 5
082428 #
082429 ROUTES+CO0056-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082430 ADD HYD + 1.0 02:RES_DM 31561.00 84.684_MoDate 39:59 26.99 n/a .000
082431 #
082432 # name_H_RESUM
082433 #
082434 # remark:flow at S_M10 N10 = S_M10
082435 #
082436 # Addition of Subwatershed 4 and Leamy Creek to Node 4
082437 #
082438 ROUTES+CO0057-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082439 ADD HYD + 1.0 02:RES_DM 31561.00 84.684_MoDate 39:59 26.99 n/a .000
082440 #
082441 # name_H_RESUM
082442 #
082443 # remark:flow at S_M4
082444 #
082445 # Sum of hydrographs from Node 4 routed to Node 2
082446 #
082447 ROUTES+CO0058-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082448 ADD HYD + 1.0 02:RES_DM 31561.00 84.684_MoDate 39:59 26.99 n/a .000
082449 #
082450 # name_H_RESUM
082451 #
082452 # remark:flow at S_M4
082453 #
082454 # Addition of Subwatershed 2 with Monahan Drain and Smith Drain to Node 2
082455 #
082456 ROUTES+CO0059-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082457 ADD HYD + 1.0 02:RES_DM 31561.00 84.684_MoDate 39:59 26.99 n/a .000
082458 #
082459 # name_H_RESUM
082460 #
082461 # remark:flow at S_M2 Jock River Gauge at Mondie Dr.
082462 #
082463 # Sum of hydrographs from Node 2 routed to Node 1
082464 #
082465 ROUTES+CO0060-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082466 ADD HYD + 1.0 02:RES_DM 31561.00 84.684_MoDate 39:59 26.99 n/a .000
082467 #
082468 # name_H_RESUM
082469 #
082470 # remark:flow at S_M2 Jock River Gauge at Mondie Dr.
082471 #
082472 # Hydrograph from Node 2 routed to Node 416
082473 # Channel X-Section obtained from RVCA Hydraulic Model - Station 9025
082474 #
082475 ROUTES+CO0061-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082476 ADD HYD + 1.0 02:RES_DM 31561.00 84.684_MoDate 39:59 26.99 n/a .000
082477 #
082478 # name_H_RESUM
082479 #
082480 # remark:flow at S_M2 Jock River Gauge at Mondie Dr.
082481 #
082482 # Catchment SW-1a
082483 # Portion of RVCA catchment SW_1 outside of Reach 1 subwatershed
082484 # Undeveloped agricultural land
082485 #
082486 ROUTES+CO0062-----DTrain-ID:HYD-----AREHA-QPEARCS+TpeaDate_hh:mm-----RvM-R-C-----DWFCms
082487 ADD HYD + 1.0 02:RES_DM 31561.00 84.684_MoDate 39:59 26.99 n/a .000
082488 #
082489 # name_H_RESUM
082490 #
082491 # remark:flow at S_M2 Jock River Gauge at Mondie Dr.
082492 #
082493 # CONTINUOUS STANDBY
082494 # [Area= 4.00] [IM= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082495 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082496 # [XIMP= 65] [TIMP= 65]
082497 # [LOSS= 2] [C= 75.0]
082498 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082499 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082500 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082501 # [XIMP= 65] [TIMP= 65]
082502 # [LOSS= 2] [C= 75.0]
082503 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082504 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082505 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082506 # [XIMP= 65] [TIMP= 65]
082507 # [LOSS= 2] [C= 75.0]
082508 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082509 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082510 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082511 # [XIMP= 65] [TIMP= 65]
082512 # [LOSS= 2] [C= 75.0]
082513 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082514 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082515 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082516 # [XIMP= 65] [TIMP= 65]
082517 # [LOSS= 2] [C= 75.0]
082518 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082519 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082520 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082521 # [XIMP= 65] [TIMP= 65]
082522 # [LOSS= 2] [C= 75.0]
082523 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082524 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082525 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082526 # [XIMP= 65] [TIMP= 65]
082527 # [LOSS= 2] [C= 75.0]
082528 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082529 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082530 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082531 # [XIMP= 65] [TIMP= 65]
082532 # [LOSS= 2] [C= 75.0]
082533 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082534 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082535 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082536 # [XIMP= 65] [TIMP= 65]
082537 # [LOSS= 2] [C= 75.0]
082538 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082539 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082540 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082541 # [XIMP= 65] [TIMP= 65]
082542 # [LOSS= 2] [C= 75.0]
082543 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082544 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082545 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082546 # [XIMP= 65] [TIMP= 65]
082547 # [LOSS= 2] [C= 75.0]
082548 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082549 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082550 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082551 # [XIMP= 65] [TIMP= 65]
082552 # [LOSS= 2] [C= 75.0]
082553 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082554 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082555 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082556 # [XIMP= 65] [TIMP= 65]
082557 # [LOSS= 2] [C= 75.0]
082558 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082559 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082560 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082561 # [XIMP= 65] [TIMP= 65]
082562 # [LOSS= 2] [C= 75.0]
082563 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082564 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082565 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082566 # [XIMP= 65] [TIMP= 65]
082567 # [LOSS= 2] [C= 75.0]
082568 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082569 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082570 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082571 # [XIMP= 65] [TIMP= 65]
082572 # [LOSS= 2] [C= 75.0]
082573 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082574 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082575 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082576 # [XIMP= 65] [TIMP= 65]
082577 # [LOSS= 2] [C= 75.0]
082578 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082579 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082580 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082581 # [XIMP= 65] [TIMP= 65]
082582 # [LOSS= 2] [C= 75.0]
082583 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082584 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082585 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082586 # [XIMP= 65] [TIMP= 65]
082587 # [LOSS= 2] [C= 75.0]
082588 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082589 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082590 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082591 # [XIMP= 65] [TIMP= 65]
082592 # [LOSS= 2] [C= 75.0]
082593 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082594 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082595 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082596 # [XIMP= 65] [TIMP= 65]
082597 # [LOSS= 2] [C= 75.0]
082598 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082599 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082600 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082601 # [XIMP= 65] [TIMP= 65]
082602 # [LOSS= 2] [C= 75.0]
082603 # [Previous area: IArea= 4.67] [SLO= 2.00] [LDP= 40.0] [MNP= 250] [SCP= 0]
082604 # [Impervious area: IArea= 1.57] [SLO= 75.10] [MNI= 0.01] [SCT= 0]
082605 # [SMD= 31.81] [SMX= 225.43] [SK= 0.10]
082606 # [XIMP= 65] [TIMP= 65]

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10473 # - To SWM Facility north of the Jock
10474 # Primarily residential development
10475 #*****
10476 #*****
10477 CONTINUOUS STANBYD 1.0 01:01:00 175.99 15.275 No_date 28:07 44.62 600 000
10478 [XIMP=38.7IMP=38]
10479 [LDRS=2 C/M 74.0]
10480 [Previous area IArea=4.675SLPP=1.00IDP=40.IMP=250:SNCP=0]
10481 [Impervious area IArea=1.575SLPP=1.00IDP=40.IMP=250:SNCP=0]
10482 [Impervious area IArea=1.575SLPP=1.00IDP=40.IMP=250:SNCP=0]
10483 [Impervious area IArea=1.575SLPP=1.00IDP=40.IMP=250:SNCP=0]
10484 [Impervious area IArea=1.575SLPP=1.00IDP=40.IMP=250:SNCP=0]
10485 # Chapman Mills SWM Pond
10486 # Rating curve obtained from CCL hydraulic modeling
10487 #*****
10488 #*****
10489 ROUTE RESERVOIR -> 1.0 01:01:00 175.99 15.275 No_date 28:07 44.62 n/a 000
10490 out -> 1.0 01:01:00 162.60 4.050 No_date 28:16 44.62 n/a 000
10491 overflow <= 1.0 01:01:00 53.39 8.160 No_date 28:16 44.62 n/a 000
10492 [Mstr=2310:0:0, TotVol=59738:0:0, N=0, V=2, TotDur=1.1hrs]
10493 #*****
10494 ADD HYD + 1.0 02:IR_LAND_MI 55194.86 104.478 No_date 38:54 29.33 n/a 000
10495 + 1.0 02:IR_LAND_MI 55194.86 104.478 No_date 38:54 29.33 n/a 000
10496 + 1.0 02:IR_LAND_MI 162.60 4.050 No_date 28:16 44.62 n/a 000
10497 SUM= 1.0 01:01:00 55194.86 104.478 No_date 38:54 29.33 n/a 000
10498 #*****
10499 SAVE HYD 1.0 01:01:00 55194.86 104.478 No_date 38:54 29.33 n/a 000
10500 #*****
10501 #*****
10502 #*****
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10660 COMBUTE API
10661 [APIMax=52.00:APIKdy=8500:APIKdt=9999]
10662 [APIMax=113.33:APIAve=67.14:APIMin=44.87]
10663 #*****
10664 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10665 # of 1.32
10666 #*****
10667 CONTINUOUS NASHVD 1.0 01:1R_JN 3680.00 18.440 No_date 36:55 30.33 372 000
10668 [C/M 61.0: N=3.00: Tp=3.76]
10669 [IAREC=4.00:IMIN=57.05:IMAX=380.32:SK=0.010]
10670 [InterEventTime=12.00]
10671 #*****
10672 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10673 # of 1.32
10674 #*****
10675 CONTINUOUS NASHVD 1.0 01:1R_JN 971.00 6.937 No_date 33:34 28.27 347 000
10676 [C/M 61.0: N=3.00: Tp=3.76]
10677 [IAREC=4.00:IMIN=64.50:IMAX=430.01:SK=0.010]
10678 [InterEventTime=12.00]
10679 #*****
10680 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10681 # of 1.80
10682 #*****
10683 CONTINUOUS NASHVD 1.0 01:1R_GWN 3074.00 8.912 No_date 39:59 24.31 298 000
10684 [C/M 55.0: N=3.00: Tp=11.33]
10685 [IAREC=4.00:IMIN=83.24:IMAX=554.96:SK=0.010]
10686 [InterEventTime=12.00]
10687 #*****
10688 CONTINUOUS NASHVD 1.0 01:1R_ASH 1781.00 16.834 No_date 32:39 36.85 452 000
10689 [C/M 72.0: N=3.00: Tp=3.21]
10690 [IAREC=4.00:IMIN=39.75:IMAX=264.99:SK=0.010]
10691 [InterEventTime=12.00]
10692 #*****
10693 CONTINUOUS NASHVD 1.0 01:1R_ML 500.00 9.061 No_date 29:21 31.73 389 000
10694 [C/M 66.0: N=3.00: Tp=5.29]
10695 [IAREC=4.00:IMIN=52.62:IMAX=350.79:SK=0.010]
10696 [InterEventTime=12.00]
10697 #*****
10698 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10699 # of 1.80
10700 #*****
10701 CONTINUOUS NASHVD 1.0 01:1R_CK 1917.00 12.342 No_date 34:26 31.73 389 000
10702 [C/M 66.0: N=3.00: Tp=5.29]
10703 [IAREC=4.00:IMIN=52.62:IMAX=350.79:SK=0.010]
10704 [InterEventTime=12.00]
10705 #*****
10706 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10707 # of 1.52
10708 #*****
10709 CONTINUOUS NASHVD 1.0 01:1R_ML 5666.00 32.402 No_date 37:52 36.85 452 000
10710 [C/M 72.0: N=3.00: Tp=8.00]
10711 [IAREC=4.00:IMIN=39.75:IMAX=264.99:SK=0.010]
10712 [InterEventTime=12.00]
10713 #*****
10714 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10715 # of 1.71
10716 #*****
10717 CONTINUOUS NASHVD 1.0 01:1R_CK 8376.00 31.024 No_date 39:59 31.73 389 000
10718 [C/M 66.0: N=3.00: Tp=5.29]
10719 [IAREC=4.00:IMIN=52.62:IMAX=350.79:SK=0.010]
10720 [InterEventTime=12.00]
10721 #*****
10722 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10723 # of 1.68
10724 #*****
10725 CONTINUOUS NASHVD 1.0 01:1R_CK 1332.00 14.039 No_date 30:53 35.35 434 000
10726 [C/M 70.0: N=3.00: Tp=2.51]
10727 [IAREC=4.00:IMIN=63.07:IMAX=287.10:SK=0.010]
10728 [InterEventTime=12.00]
10729 #*****
10730 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10731 # of 1.82
10732 #*****
10733 CONTINUOUS NASHVD 1.0 01:1R_CK 4464.00 15.472 No_date 39:59 28.95 355 000
10734 [C/M 62.0: N=3.00: Tp=11.32]
10735 [IAREC=4.00:IMIN=81.90:IMAX=412.66:SK=0.010]
10736 [InterEventTime=12.00]
10737 #*****
10738 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10739 # of 1.80
10740 #*****
10741 CONTINUOUS NASHVD 1.0 01:1R_ML 131.00 2.740 No_date 28:57 29.64 364 000
10742 [C/M 66.0: N=3.00: Tp=5.29]
10743 [IAREC=4.00:IMIN=52.62:IMAX=350.79:SK=0.010]
10744 [InterEventTime=12.00]
10745 #*****
10746 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10747 # of 1.65
10748 #*****
10749 CONTINUOUS NASHVD 1.0 01:1R_ML 384.00 18.380 No_date 38:32 31.73 389 000
10750 [C/M 66.0: N=3.00: Tp=8.42]
10751 [IAREC=4.00:IMIN=52.62:IMAX=350.79:SK=0.010]
10752 [InterEventTime=12.00]
10753 #*****
10754 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10755 # of 1.82
10756 #*****
10757 CONTINUOUS NASHVD 1.0 01:1R_W 3397.00 13.937 No_date 36:23 25.61 314 000
10758 [C/M 57.0: N=3.00: Tp=4.81]
10759 [IAREC=4.00:IMIN=76.32:IMAX=508.81:SK=0.010]
10760 [InterEventTime=12.00]
10761 #*****
10762 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10763 # of 1.73
10764 #*****
10765 CONTINUOUS NASHVD 1.0 01:1R_W 165.00 1.285 No_date 31:02 32.44 398 000
10766 [C/M 67.0: N=3.00: Tp=4.81]
10767 [IAREC=4.00:IMIN=50.55:IMAX=336.97:SK=0.010]
10768 [InterEventTime=12.00]
10769 #*****
10770 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10771 # of 1.67
10772 #*****
10773 CONTINUOUS NASHVD 1.0 01:1R_W 1332.00 9.332 No_date 35:12 36.85 452 000
10774 [C/M 72.0: N=3.00: Tp=5.95]
10775 [IAREC=4.00:IMIN=39.75:IMAX=264.99:SK=0.010]
10776 [InterEventTime=12.00]
10777 #*****
10778 CONTINUOUS NASHVD 1.0 01:1R_W 224.00 8.187 No_date 28:45 41.51 509 000
10779 [C/M 77.0: N=3.00: Tp=7.51]
10780 [IAREC=4.00:IMIN=31.15:IMAX=207.66:SK=0.010]
10781 [InterEventTime=12.00]
10782 #*****
10783 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10784 # of 1.20
10785 #*****
10786 CONTINUOUS NASHVD 1.0 01:1R_CK 4945.00 44.623 No_date 31:18 38.37 471 000
10787 [C/M 74.0: N=3.00: Tp=4.81]
10788 [IAREC=4.00:IMIN=36.67:IMAX=244.49:SK=0.010]
10789 [InterEventTime=12.00]
10790 #*****
10791 CONTINUOUS NASHVD 1.0 01:1R_W 20.00 .943 No_date 28:35 45.60 560 000
10792 [C/M 81.0: N=3.00: Tp=3.02]
10793 [IAREC=4.00:IMIN=25.21:IMAX=168.09:SK=0.010]
10794 [InterEventTime=12.00]
10795 #*****
10796 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
10797 # of 1.61
10798 #*****
10799 CONTINUOUS NASHVD 1.0 01:1R_W 141.00 8.794 No_date 37:48 39.93 480 000
10800 [C/M 75.0: N=3.00: Tp=8.00]
10801 [IAREC=4.00:IMIN=33.81:IMAX=225.43:SK=0.010]
10802 [InterEventTime=12.00]
10803 #*****
10804 CONTINUOUS NASHVD 1.0 01:1R_W 983.00 12.896 No_date 39:59 45.60 560 000
10805 [C/M 81.0: N=3.00: Tp=1.75]
10806 [IAREC=4.00:IMIN=35.21:IMAX=168.09:SK=0.010]
10807 [InterEventTime=12.00]
10808 #*****
10809 CONTINUOUS NASHVD 1.0 01:1R_CK 1021.00 17.059 No_date 31:46 44.77 549 000
10810 [C/M 80.0: N=3.00: Tp=2.46]
10811 [IAREC=4.00:IMIN=36.38:IMAX=175.50:SK=0.010]
10812 [InterEventTime=12.00]
10813 #*****
10814 CONTINUOUS NASHVD 1.0 01:1R_W 177.00 6.469 No_date 28:45 41.51 509 000
10815 [C/M 77.0: N=3.00: Tp=7.51]
10816 [IAREC=4.00:IMIN=31.15:IMAX=207.66:SK=0.010]
10817 [InterEventTime=12.00]
10818 #*****
10819 CONTINUOUS NASHVD 1.0 01:1R_DR 1122.00 15.544 No_date 31:43 45.60 560 000
10820 [C/M 81.0: N=3.00: Tp=3.21]
10821 [IAREC=4.00:IMIN=35.21:IMAX=168.09:SK=0.010]
10822 [InterEventTime=12.00]
10823 #*****
10824 CONTINUOUS NASHVD 1.0 01:1R_DR 2737.00 34.946 No_date 31:29 40.72 500 000
10825 [C/M 81.0: N=3.00: Tp=3.02]
10826 [IAREC=4.00:IMIN=32.46:IMAX=216.39:SK=0.010]
10827 [InterEventTime=12.00]
10828 #*****
10829 #*****
10830 #*****
10831 #*****
10832 #*****
10833 #*****
10834 #*****
10835 #*****
10836 #*****
10837 #*****
10838 #*****
10839 #*****
10840 #*****
10841 #*****
10842 #*****
10843 #*****
10844 #*****
10845 #*****
10846 #*****

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10847#
10848# Addition of Subwatershed Jock River at Goodwood Marsh to Node 13a
10849#
10850# RO505-C00032 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
10851# ADD HYD + 1.0 021813A 4651.00 19.136_MoDate 39:06 29.90 n/a .000
10852# [RDT= 1.00] out<- 1.0 021813M 3074.00 8.912_MoDate 39:59 24.31 n/a .000
10853# [L/S= 5242. / 0.567 / 0.80] [Vmax= 7725. / 27.539 / 39.54 27.68 n/a .000
10854#
10855# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
10856#
10857# RO505-C00033 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
10858# ROUTE RESERVOIR -> 1.0 021813A 7725.00 27.539_MoDate 39:54 27.68 n/a .000
10859# out<- 1.0 01RES_OH 7725.00 3.808_MoDate 61:35 27.67 n/a .000
10860# [M/S= 5242. / 0.567 / 0.80] [Vmax= 7725. / 27.539 / 39.54 27.68 n/a .000
10861#
10862# RO505-C00034 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
10863# SAVE HYD 1.0 01RES_OH 7725.00 3.808_MoDate 61:35 27.67 n/a .000
10864# name_H_RESOH
10865# remark:outflow from Res OH
10866# Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
10867# (Approximated cross-section - see cross-section 258)
10868# Use n=0.04 for summer conditions and n=0.025 for spring conditions
10869# RO505-C00035 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
10870# ROUTE CHANNEL -> 1.0 021813M 7725.00 3.808_MoDate 61:35 27.67 n/a .000
10871# [RDT= 1.00] out<- 1.0 01RES_OH 7725.00 3.804_MoDate 64:19 27.68 n/a .000
10872# [L/S= 5242. / 0.567 / 0.80] [Vmax= 7725. / 27.539 / 39.54 27.68 n/a .000
10873# [Vmax= 556. / 0.90 / 0.40]
10874#
10875# Addition of Subwatershed Jock River at Ashton to Node 12
10876#
10877# RO505-C00036 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
10878# ADD HYD + 1.0 021812 7725.00 3.804_MoDate 64:19 27.68 n/a .000
10879# [L/S= 1428. / 1.51 / 0.25] [Vmax= 1781.00 16.818_MoDate 32:39 36.85 n/a .000
10880# SUM= 1.0 01S_M12 9506.00 18.867_MoDate 32:42 29.39 n/a .000
10881#
10882# RO505-C00037 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
10883# SAVE HYD 1.0 01S_M12 9506.00 18.867_MoDate 32:42 29.39 n/a .000
10884# name_H_S12
10885# remark:flow at S_M12 near Ashton
10886#
10887# Sum of hydrographs from Node 12 routed to Node 11
10888# (Approximated cross-section - see cross-section 258)
10889# Use n=0.04 for summer conditions and n=0.025 for spring conditions
10890# Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
10891#
10892# RO505-C00038 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
10893# ROUTE CHANNEL -> 1.0 021812 9506.00 18.867_MoDate 32:42 29.39 n/a .000
10894# [RDT= 1.00] out<- 1.0 01Dum11 9506.00 18.867_MoDate 32:59 29.39 n/a .000
10895# [L/S= 972. / 0.54 / 0.40] [Vmax= 781 / Dmax= 3.09]
10896#
10897# Addition of Subwatershed 11 and No Name Creek to Node 11
10898#
10899# RO505-C00039 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
10900# ADD HYD + 1.0 021Dum11 9506.00 18.867_MoDate 32:59 29.39 n/a .000
10901# [RDT= 1.00] out<- 1.0 021811 500.00 9.061_MoDate 29:21 31.73 n/a .000
10902# [L/S= 1517. / 1.34 / 0.25] [Vmax= 1937.00 12.342_MoDate 34:26 31.73 n/a .000
10903# SUM= 1.0 01S_M11 11923.00 32.851_MoDate 33:00 29.87 n/a .000
10904#
10905# Sum of hydrographs from Node 11 routed to Node 10
10906# Section 1
10907#
10908# RO505-C00040 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
10909# ROUTE CHANNEL -> 1.0 021811 11923.00 20.490_MoDate 40:02 29.87 n/a .000
10910# [RDT= 1.00] out<- 1.0 01S_M10 11923.00 20.490_MoDate 40:02 29.87 n/a .000
10911# [L/S= 1517. / 1.34 / 0.25] [Vmax= 474 / Dmax= 1.423]
10912#
10913# Addition of Subwatershed 10 to Node 10
10914#
10915# RO505-C00041 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
10916# ADD HYD + 1.0 021810 11923.00 20.490_MoDate 40:02 29.87 n/a .000
10917# [L/S= 1517. / 1.34 / 0.25] [Vmax= 5646.00 52.600_MoDate 37:52 36.85 n/a .000
10918# SUM= 1.0 01S_M10 11923.00 20.490_MoDate 40:02 29.87 n/a .000
10919#
10920# RO505-C00042 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
10921# SAVE HYD 1.0 01S_M10 11923.00 20.490_MoDate 40:02 29.87 n/a .000
10922# name_H_S10
10923# remark:flow at S_M10 - SW_10
10924#
10925# Addition of Kings Creek to S_M10
10926#
10927# RO505-C00043 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
10928# ADD HYD + 1.0 021810 17859.00 52.600_MoDate 38:19 32.12 n/a .000
10929# [L/S= 8776. / 1.024 / 0.25] [Vmax= 8776.00 52.600_MoDate 38:19 32.12 n/a .000
10930# SUM= 1.0 01S_M10A 25965.00 82.746_MoDate 39:45 31.99 n/a .000
10931#
10932# Sum of hydrographs from Node 10 routed to Node 9
10933# Section 2
10934#
10935# RO505-C00044 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
10936# ROUTE CHANNEL -> 1.0 021810A 25965.00 82.746_MoDate 39:45 31.99 n/a .000
10937# [RDT= 1.00] out<- 1.0 01S_N9 25965.00 80.980_MoDate 39:59 31.99 n/a .000
10938# [L/S= 3982. / 0.70 / 0.25] [Vmax= 7441 / Dmax= 2.015]
10939#
10940# Addition of Subwatershed 9 and Nichols Creek to Node 9
10941#
10942# RO505-C00045 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
10943# ADD HYD + 1.0 02189 25965.00 80.980_MoDate 39:59 31.99 n/a .000
10944# [L/S= 1132. / 1.043 / 0.25] [Vmax= 4464.00 15.472_MoDate 39:59 28.95 n/a .000
10945# SUM= 1.0 01S_N9 31561.00 99.424_MoDate 39:59 31.68 n/a .000
10946#
10947# Sum of hydrographs from Node 9 routed to Node 8
10948# Section 3
10949#
10950# RO505-C00046 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
10951# ROUTE CHANNEL -> 1.0 02189 31561.00 99.424_MoDate 39:59 31.68 n/a .000
10952# [RDT= 1.00] out<- 1.0 01S_N8 31561.00 93.665_MoDate 39:59 31.68 n/a .000
10953# [L/S= 1882. / 0.81 / 0.25] [Vmax= 3671 / Dmax= 1.834]
10954#
10955# Addition of Subwatershed 8 and Bobb's Drain to Node 8
10956#
10957# RO505-C00047 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
10958# ADD HYD + 1.0 02188 31561.00 93.665_MoDate 39:59 31.68 n/a .000
10959# [L/S= 1882. / 0.81 / 0.25] [Vmax= 3854.00 18.180_MoDate 38:32 31.73 n/a .000
10960# SUM= 1.0 01S_N8 38546.00 111.843_MoDate 39:59 31.68 n/a .000
10961#
10962# Sum of hydrographs from Node 8 routed to Node 7
10963# Section 4
10964#
10965# RO505-C00048 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
10966# ROUTE CHANNEL -> 1.0 02188 35446.00 111.843_MoDate 39:59 31.68 n/a .000
10967# [RDT= 1.00] out<- 1.0 01S_M7 35446.00 95.475_MoDate 44:55 31.68 n/a .000
10968# [L/S= 1882. / 0.57 / 0.25] [Vmax= 2311 / Dmax= 2.290]
10969#
10970# Addition of Subwatershed 7 to Node 7
10971#
10972# RO505-C00049 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
10973# ADD HYD + 1.0 02187 35446.00 95.475_MoDate 44:55 31.68 n/a .000
10974# [L/S= 3197. / 1.33 / 0.25] [Vmax= 3197.00 102.892_MoDate 43:46 31.18 n/a .000
10975# SUM= 1.0 01S_M7 38743.00 102.892_MoDate 43:46 31.18 n/a .000
10976#
10977# RO505-C00050 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
10978# SAVE HYD 1.0 01S_M7 38743.00 102.892_MoDate 43:46 31.18 n/a .000
10979# name_H_S07
10980# remark:flow at S_M7 - SW_7
10981# Insertion of a reservoir to simulate the effects of the Richmond Fen.
10982# Storage area and volume were estimated from available topo maps.
10983# Release rate from fen was assumed to be controlled by the downstream
10984# river cross-section for summer conditions. It is assumed that for up to
10985# 0.75 m of water, the main channel of the river provided the storage. Above
10986# this depth, the wetland starts to significantly store water.
10987#
10988# RO505-C00051 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
10989# ROUTE RESERVOIR -> 1.0 021S_M7 38743.00 102.892_MoDate 43:46 31.18 n/a .000
10990# out<- 1.0 01RES_RF 38743.00 52.029_MoDate 59:07 31.18 n/a .000
10991# [Hydrology: 4394E+03] [Vmax= 1321.00 1132.00 39.132 36.85 n/a .000
10992#
10993# RO505-C00052 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
10994# SAVE HYD 1.0 01RES_RF 38743.00 52.029_MoDate 59:07 31.18 n/a .000
10995# name_H_RESRF
10996# remark:outflow of Richmond Fen
10997#
10998# Sum of hydrographs from Node 7 routed to Node 6
10999# Section 5
11000#
11001# RO505-C00053 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
11002# ROUTE CHANNEL -> 1.0 02186 38743.00 52.029_MoDate 59:07 31.18 n/a .000
11003# [RDT= 1.00] out<- 1.0 01S_M6 38743.00 51.784_MoDate 60:27 31.18 n/a .000
11004# [L/S= 3086. / 0.82 / 0.25] [Vmax= 5301 / Dmax= 1.253]
11005#
11006# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
11007#
11008# RO505-C00054 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
11009# ADD HYD + 1.0 02186 38743.00 51.784_MoDate 60:27 31.18 n/a .000
11010# [L/S= 1242. / 0.82 / 0.25] [Vmax= 4945.00 44.623_MoDate 33:18 38.37 n/a .000
11011# SUM= 1.0 01S_M6 40240.01 51.810_MoDate 60:20 31.44 n/a .000
11012#
11013# Sum of hydrographs from Node 6 routed to Node 5
11014# Section 6
11015#
11016# RO505-C00055 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
11017# ROUTE CHANNEL -> 1.0 02185 40240.01 51.810_MoDate 60:20 31.37 n/a .000
11018# [RDT= 1.00] out<- 1.0 01S_M5 40240.01 51.693_MoDate 61:06 31.37 n/a .000
11019# [L/S= 1882. / 0.57 / 0.25] [Vmax= 469 / Dmax= 1.351]
11020#
11021# Addition of Subwatershed 5 and Flowing Creek to Node 5
11022#
11023# RO505-C00056 -----Dtn-ID-NHYD-----AREHA-QPEAFcMs-TpeakDate_hh:mm-----RvM-R-C-----DWfCms
11024# ADD HYD + 1.0 02185 40240.01 51.693_MoDate 61:06 31.37 n/a .000
11025# [L/S= 1242. / 0.82 / 0.25] [Vmax= 4945.00 44.623_MoDate 33:18 38.37 n/a .000
11026# SUM= 1.0 01S_M5 45409.01 71.514_MoDate 34:20 32.38 n/a .000

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11221 (Vmax :822;Dmax: 759)
11222 RO550-C01094-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11223 CONTINUOUS HANDED 1.0 01:01 1.17 094_MoDate 28:12 43.70 1536 .000
11224 [InterEventTime=12.00]
11225 [Cm: 84.0 M: 3.00 Tm: .99]
11226 [IARcLimp= 4.00; IARcEper= 4.00]
11227 RO550-C01095-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11228 CONTINUOUS STANDBY 1.0 01:1A1 2.50 .517_MoDate 28:01 64.42 790 .000
11229 [XMP: 68;TMD: 85]
11230 (Horton parameters) Fw: 76.20;Fc: 13.20;DCAY:4.14; Pa: .00]
11231 (Previous area: IArea: 4.67;SLDP: .50;LDP: .50;MHP: .250;SDCP: .0]
11232 (Impervious area: IAlmp: 1.57;SLDp: .50;LdI: 199.9MI-.013;SCL: .0]
11233 [IARcLimp= 4.00; IARcEper= 4.00]
11234 RO550-C01096-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11235 ROUTE RESERVOIR -> 1.0 02:1A 2.50 .517_MoDate 28:01 64.42 n/a .000
11236 overlow out <= 1.0 01:1A7STB 2.50 .146_MoDate 28:19 64.42 n/a .000
11237 overlow <= 1.0 01:1A7OVF .00 .000_MoDate 0:00 .00 n/a .000
11238 (MstUsed: 1.741E-02 m3, TotDvVol: .0000E+00 m3, N-OvF= 0, TotDvOvF= 0.hrs)
11239 RO550-C01097-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11240 CONTINUOUS HANDED 1.0 01:ST-2 .59 .103_MoDate 28:00 50.67 622 .000
11241 [XMP: 46;TMD: 57]
11242 (Horton parameters) Fw: 76.20;Fc: 13.20;DCAY:4.14; Pa: .00]
11243 (Previous area: IArea: 4.67;SLDP: .50;LDP: .50;MHP: .250;SDCP: .0]
11244 (Impervious area: IAlmp: 1.57;SLDp: .50;LdI: 199.9MI-.013;SCL: .0]
11245 [IARcLimp= 4.00; IARcEper= 4.00]
11246 RO550-C01098-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11247 ROUTE RESERVOIR -> 1.0 02:1ST 2.59 .103_MoDate 28:00 50.67 n/a .000
11248 overlow out <= 1.0 01:1A7STB 2.59 .052_MoDate 28:11 50.67 n/a .000
11249 overlow <= 1.0 01:1A7OVF .00 .000_MoDate 0:00 .00 n/a .000
11250 (MstUsed: .1952E-02 m3, TotDvVol: .0000E+00 m3, N-OvF= 0, TotDvOvF= 0.hrs)
11251 RO550-C01099-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11252 CONTINUOUS HANDED 1.0 01:01-8 60.55 1.383_MoDate 29:04 33.66 413 .000
11253 [Cm: 84.0 M: 3.00 Tm: .99]
11254 [IARc: 4.00; SMIN: 44.82; SMAX: 298.82; SK: .010]
11255 [InterEventTime=12.00]
11256 RO550-C01100-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11257 ROUTE PIPE -> 1.0 02:01-8 60.55 1.383_MoDate 29:04 33.66 n/a .000
11258 (RDP: 1.00) out<= 1.0 01:01-8 60.55 1.376_MoDate 29:07 33.66 n/a .000
11259 [L/S/ra: 335./ 100./ 0.13]
11260 (Vmax :1.24;Dmax: 1.80)
11261 [RTP: 1.20;WDB: 1.80]
11262 RO550-C01101-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11263 ADD RTD + 1.0 02:01 261.31 4.883_MoDate 28:25 25.81 n/a .000
11264 + 1.0 02:01 1.17 094_MoDate 28:12 43.70 n/a .000
11265 + 1.0 02:01-STR 2.50 .146_MoDate 28:19 64.42 n/a .000
11266 + 1.0 02:01-TOVF .00 .000_MoDate 0:00 .00 n/a .000
11267 + 1.0 01:1A7STB 3.51 .199_MoDate 28:21 64.42 n/a .000
11268 + 1.0 01:1A7OVF .00 .000_MoDate 0:00 .00 n/a .000
11269 + 1.0 01:1A7STB 3.51 .199_MoDate 28:21 64.42 n/a .000
11270 (MstUsed: .1019E+00 m3, TotDvVol: .0000E+00 m3, N-OvF= 0, TotDvOvF= 0.hrs)
11271 RO550-C01102-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11272 CONTINUOUS STANDBY 1.0 01:01-8 60.55 1.376_MoDate 29:07 33.66 n/a .000
11273 [XMP: 68;TMD: 85]
11274 (Horton parameters) Fw: 76.20;Fc: 13.20;DCAY:4.14; Pa: .00]
11275 (Previous area: IArea: 4.67;SLDP: .50;LDP: .50;MHP: .250;SDCP: .0]
11276 (Impervious area: IAlmp: 1.57;SLDp: .50;LdI: 199.9MI-.013;SCL: .0]
11277 [IARcLimp= 4.00; IARcEper= 4.00]
11278 RO550-C01103-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11279 ROUTE RESERVOIR -> 1.0 02:1A 3.51 .199_MoDate 28:21 64.42 n/a .000
11280 overlow out <= 1.0 01:1A7STB 3.51 .199_MoDate 28:21 64.42 n/a .000
11281 overlow <= 1.0 01:1A7OVF .00 .000_MoDate 0:00 .00 n/a .000
11282 (MstUsed: .1019E+00 m3, TotDvVol: .0000E+00 m3, N-OvF= 0, TotDvOvF= 0.hrs)
11283 RO550-C01104-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11284 CONTINUOUS STANDBY 1.0 01:01-8 60.55 1.376_MoDate 29:07 33.66 n/a .000
11285 [XMP: 46;TMD: 57]
11286 (Horton parameters) Fw: 76.20;Fc: 13.20;DCAY:4.14; Pa: .00]
11287 (Previous area: IArea: 4.67;SLDP: .50;LDP: .50;MHP: .250;SDCP: .0]
11288 (Impervious area: IAlmp: 1.57;SLDp: .50;LdI: 199.9MI-.013;SCL: .0]
11289 [IARcLimp= 4.00; IARcEper= 4.00]
11290 RO550-C01105-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11291 ROUTE RESERVOIR -> 1.0 02:1A 3.51 .199_MoDate 28:21 64.42 n/a .000
11292 overlow out <= 1.0 01:1A7STB 3.51 .199_MoDate 28:21 64.42 n/a .000
11293 overlow <= 1.0 01:1A7OVF .00 .000_MoDate 0:00 .00 n/a .000
11294 (MstUsed: .4527E-02 m3, TotDvVol: .0000E+00 m3, N-OvF= 0, TotDvOvF= 0.hrs)
11295 RO550-C01106-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11296 ADD RTD + 1.0 02:1A 3.51 .199_MoDate 28:21 64.42 n/a .000
11297 + 1.0 02:1A 6.00 12.00_MoDate 28:19 64.42 n/a .000
11298 + 1.0 02:1A7STB 3.51 .199_MoDate 28:21 64.42 n/a .000
11299 + 1.0 02:1A7OVF .00 .000_MoDate 0:00 .00 n/a .000
11300 + 1.0 01:1A7STB 3.51 .199_MoDate 28:21 64.42 n/a .000
11301 + 1.0 01:1A7OVF .00 .000_MoDate 0:00 .00 n/a .000
11302 (MstUsed: 6.289 M: 330.34, TotDvVol: 28:23 28.11 n/a .000)
11303 RO550-C01107-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11304 CONTINUOUS HANDED 1.0 01:01-8 330.34 5.789_MoDate 28:58 28.11 n/a .000
11305 [L/S/ra: 335./ 100./ 0.13]
11306 (Vmax :593;Dmax: 1.152)
11307 RO550-C01108-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11308 CONTINUOUS HANDED 1.0 01:01-8 330.34 5.789_MoDate 28:58 28.11 n/a .000
11309 [Cm: 84.0 M: 3.00 Tm: .99]
11310 [IARc: 4.00; SMIN: 44.82; SMAX: 298.82; SK: .010]
11311 [InterEventTime=12.00]
11312 RO550-C01109-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11313 CONTINUOUS STANDBY 1.0 01:1A1 12.04 2.163_MoDate 28:03 64.42 790 .000
11314 [XMP: 68;TMD: 85]
11315 (Horton parameters) Fw: 76.20;Fc: 13.20;DCAY:4.14; Pa: .00]
11316 (Previous area: IArea: 4.67;SLDP: .50;LDP: .50;MHP: .250;SDCP: .0]
11317 (Impervious area: IAlmp: 1.57;SLDp: .50;LdI: 199.9MI-.013;SCL: .0]
11318 [IARcLimp= 4.00; IARcEper= 4.00]
11319 RO550-C01110-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11320 ROUTE RESERVOIR -> 1.0 02:1A 12.04 2.163_MoDate 28:03 64.42 n/a .000
11321 overlow out <= 1.0 01:1A7STB 12.04 .654_MoDate 28:27 64.42 n/a .000
11322 overlow <= 1.0 01:1A7OVF .00 .000_MoDate 0:00 .00 n/a .000
11323 (MstUsed: .1445E+00 m3, TotDvVol: .0000E+00 m3, N-OvF= 0, TotDvOvF= 0.hrs)
11324 RO550-C01111-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11325 CONTINUOUS STANDBY 1.0 01:ST-4 .35 .663_MoDate 28:00 50.67 622 .000
11326 [XMP: 46;TMD: 57]
11327 (Horton parameters) Fw: 76.20;Fc: 13.20;DCAY:4.14; Pa: .00]
11328 (Previous area: IArea: 4.67;SLDP: .50;LDP: .50;MHP: .250;SDCP: .0]
11329 (Impervious area: IAlmp: 1.57;SLDp: .50;LdI: 199.9MI-.013;SCL: .0]
11330 [IARcLimp= 4.00; IARcEper= 4.00]
11331 RO550-C01112-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11332 ROUTE RESERVOIR -> 1.0 02:1A 3.5 .663_MoDate 28:00 50.67 n/a .000
11333 overlow out <= 1.0 01:1A7STB 3.5 .031_MoDate 28:10 50.67 n/a .000
11334 overlow <= 1.0 01:1A7OVF .00 .000_MoDate 0:00 .00 n/a .000
11335 (MstUsed: .2719E-02 m3, TotDvVol: .0000E+00 m3, N-OvF= 0, TotDvOvF= 0.hrs)
11336 RO550-C01113-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11337 CONTINUOUS HANDED 1.0 01:1A8 1.30 1.036_MoDate 28:01 64.42 790 .000
11338 [XMP: 68;TMD: 85]
11339 (Horton parameters) Fw: 76.20;Fc: 13.20;DCAY:4.14; Pa: .00]
11340 (Previous area: IArea: 4.67;SLDP: .50;LDP: .50;MHP: .250;SDCP: .0]
11341 (Impervious area: IAlmp: 1.57;SLDp: .50;LdI: 199.9MI-.013;SCL: .0]
11342 [IARcLimp= 4.00; IARcEper= 4.00]
11343 RO550-C01114-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11344 ROUTE RESERVOIR -> 1.0 02:1A 5.30 1.036_MoDate 28:01 64.42 n/a .000
11345 overlow out <= 1.0 01:1A7STB 5.30 .300_MoDate 28:22 64.42 n/a .000
11346 overlow <= 1.0 01:1A7OVF .00 .000_MoDate 0:00 .00 n/a .000
11347 (MstUsed: .1532E+00 m3, TotDvVol: .0000E+00 m3, N-OvF= 0, TotDvOvF= 0.hrs)
11348 RO550-C01115-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11349 ADD RTD + 1.0 02:1A 330.34 5.789_MoDate 28:58 28.11 n/a .000
11350 + 1.0 01:1A7STB 12.04 .074_MoDate 28:27 64.42 n/a .000
11351 + 1.0 01:1A7STB 12.04 .074_MoDate 28:27 64.42 n/a .000
11352 + 1.0 01:1A7OVF .00 .000_MoDate 0:00 .00 n/a .000
11353 + 1.0 01:1A7STB 12.04 .074_MoDate 28:27 64.42 n/a .000
11354 + 1.0 01:1A7OVF .00 .000_MoDate 0:00 .00 n/a .000
11355 + 1.0 01:1A7STB 5.30 .300_MoDate 28:22 64.42 n/a .000
11356 + 1.0 01:1A7OVF .00 .000_MoDate 0:00 .00 n/a .000
11357 (MstUsed: .7719E-02 m3, TotDvVol: .0000E+00 m3, N-OvF= 0, TotDvOvF= 0.hrs)
11358 RO550-C01116-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11359 ROUTE CHANNEL -> 1.0 02:1P374 350.31 6.632_MoDate 28:55 30.03 n/a .000
11360 (RDP: 1.00) out<= 1.0 01:1A7STB 350.31 6.350_MoDate 29:11 30.03 n/a .000
11361 [L/S/ra: 525./ 230./ 0.43]
11362 (Vmax :613;Dmax: 1.197)
11363 RO550-C01117-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11364 CONTINUOUS HANDED 1.0 01:013 2.51 .113_MoDate 28:43 47.27 580 .000
11365 [Cm: 84.0 M: 3.00 Tm: .99]
11366 [IARc: 4.00; SMIN: 17.43; SMAX: 116.21; SK: .010]
11367 [InterEventTime=12.00]
11368 RO550-C01118-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11369 CONTINUOUS STANDBY 1.0 01:01-1 3.41 .690_MoDate 28:01 64.42 790 .000
11370 [XMP: 68;TMD: 85]
11371 (Horton parameters) Fw: 76.20;Fc: 13.20;DCAY:4.14; Pa: .00]
11372 (Previous area: IArea: 4.67;SLDP: .50;LDP: .50;MHP: .250;SDCP: .0]
11373 (Impervious area: IAlmp: 1.57;SLDp: .50;LdI: 199.9MI-.013;SCL: .0]
11374 [IARcLimp= 4.00; IARcEper= 4.00]
11375 RO550-C01119-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11376 ROUTE RESERVOIR -> 1.0 02:1C 3.41 .690_MoDate 28:01 64.42 n/a .000
11377 overlow out <= 1.0 01:1A7STB 3.41 .194_MoDate 28:10 64.42 n/a .000
11378 overlow <= 1.0 01:1A7OVF .00 .000_MoDate 0:00 .00 n/a .000
11379 (MstUsed: .1532E+00 m3, TotDvVol: .0000E+00 m3, N-OvF= 0, TotDvOvF= 0.hrs)
11380 RO550-C01120-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11381 CONTINUOUS STANDBY 1.0 01:ST-5 .45 .079_MoDate 28:00 50.67 622 .000
11382 [XMP: 46;TMD: 57]
11383 (Horton parameters) Fw: 76.20;Fc: 13.20;DCAY:4.14; Pa: .00]
11384 (Previous area: IArea: 4.67;SLDP: .50;LDP: .50;MHP: .250;SDCP: .0]
11385 (Impervious area: IAlmp: 1.57;SLDp: .50;LdI: 199.9MI-.013;SCL: .0]
11386 [IARcLimp= 4.00; IARcEper= 4.00]
11387 RO550-C01121-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11388 ROUTE RESERVOIR -> 1.0 02:1ST 4.5 .079_MoDate 28:00 50.67 n/a .000
11389 overlow out <= 1.0 01:1A7STB 4.5 .079_MoDate 28:10 50.67 n/a .000
11390 overlow <= 1.0 01:1A7OVF .00 .000_MoDate 0:00 .00 n/a .000
11391 (MstUsed: .1532E+00 m3, TotDvVol: .0000E+00 m3, N-OvF= 0, TotDvOvF= 0.hrs)
11392 RO550-C01122-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11393 ADD RTD + 1.0 02:013 2.51 .113_MoDate 28:43 47.27 n/a .000
11394 + 1.0 02:013 3.41 .194_MoDate 28:20 64.42 n/a .000
11395 + 1.0 02:013-STR 3.41 .194_MoDate 28:20 64.42 n/a .000
11396 + 1.0 02:013-TOVF .00 .000_MoDate 0:00 .00 n/a .000
11397 + 1.0 02:013-STR 3.41 .194_MoDate 28:20 64.42 n/a .000
11398 (MstUsed: .1532E+00 m3, TotDvVol: .0000E+00 m3, N-OvF= 0, TotDvOvF= 0.hrs)
11399 RO550-C01123-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11400 CONTINUOUS STANDBY 1.0 01:ST-5 356.68 6.575_MoDate 29:09 30.51 n/a .000
11401 [XMP: 64;TMD: 85]
11402 (Horton parameters) Fw: 76.20;Fc: 13.20;DCAY:4.14; Pa: .00]
11403 (Previous area: IArea: 4.67;SLDP: .50;LDP: .50;MHP: .250;SDCP: .0]
11404 (Impervious area: IAlmp: 1.57;SLDp: .50;LdI: 1230.7MI-.013;SCL: .0]
11405 [IARcLimp= 4.00; IARcEper= 4.00]
11406 RO550-C01124-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11407 ROUTE RESERVOIR -> 1.0 02:1STAND 7.59 1.036_MoDate 28:09 62.95 n/a .000
11408 (MstUsed: .1532E+00 m3, TotDvVol: .0000E+00 m3, N-OvF= 0, TotDvOvF= 0.hrs)
11409 [IARcLimp= 4.00; IARcEper= 4.00]
11410 [IARc: 4.00; SMIN: 17.43; SMAX: 116.21; SK: .010]
11411 [InterEventTime=12.00]
11412 RO550-C01125-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11413 ADD RTD + 1.0 02:1ST 356.68 6.575_MoDate 29:09 30.51 n/a .000
11414 + 1.0 02:1ST 7.59 1.036_MoDate 28:09 62.95 n/a .000
11415 + 1.0 02:1ST-STR 356.68 6.575_MoDate 29:09 30.51 n/a .000
11416 + 1.0 02:1ST-TOVF .00 .000_MoDate 0:00 .00 n/a .000
11417 (MstUsed: .1532E+00 m3, TotDvVol: .0000E+00 m3, N-OvF= 0, TotDvOvF= 0.hrs)
11418 RO550-C01126-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11419 SAVE RTD + 1.0 01:1SADT 364.27 6.711_MoDate 29:09 31.19 n/a .000
11420 [IARc: 4.00; SMIN: 17.43; SMAX: 116.21; SK: .010]
11421 [InterEventTime=12.00]
11422 RO550-C01127-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11423 CONTINUOUS STANDBY 1.0 01:Area-A 66.75 8.917_MoDate 28:08 61.83 759 .000
11424 [XMP: 64;TMD: 85]
11425 (Horton parameters) Fw: 76.20;Fc: 13.20;DCAY:4.14; Pa: .00]
11426 (Previous area: IArea: 4.67;SLDP: .50;LDP: .50;MHP: .250;SDCP: .0]
11427 (Impervious area: IAlmp: 1.57;SLDp: .50;LdI: 199.9MI-.013;SCL: .0]
11428 [IARcLimp= 4.00; IARcEper= 4.00]
11429 RO550-C01128-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11430 SAVE RTD + 1.0 01:Area-A 66.75 8.917_MoDate 28:08 61.83 n/a .000
11431 [IARc: 4.00; SMIN: 17.43; SMAX: 116.21; SK: .010]
11432 [InterEventTime=12.00]
11433 RO550-C01129-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11434 ROUTE RESERVOIR -> 1.0 02:1Area-A 66.75 8.917_MoDate 28:08 61.83 n/a .000
11435 overlow out <= 1.0 01:1SADT 66.75 1.070_MoDate 29:16 61.83 n/a .000
11436 overlow <= 1.0 01:1SADT .00 .000_MoDate 0:00 .00 n/a .000
11437 (MstUsed: .2845E+01 m3, TotDvVol: .0000E+00 m3, N-OvF= 0, TotDvOvF= 0.hrs)
11438 RO550-C01130-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11439 SAVE RTD + 1.0 01:Area-A 66.75 8.917_MoDate 28:08 61.83 n/a .000
11440 [IARc: 4.00; SMIN: 17.43; SMAX: 116.21; SK: .010]
11441 [InterEventTime=12.00]
11442 RO550-C01131-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11443 ADD RTD + 1.0 02:1Area-A 66.75 8.917_MoDate 29:16 61.83 n/a .000
11444 + 1.0 02:1Area-A 66.75 1.070_MoDate 29:16 61.83 n/a .000
11445 + 1.0 02:1Area-A 66.75 1.070_MoDate 29:16 61.83 n/a .000
11446 + 1.0 02:1Area-A 66.75 1.070_MoDate 29:16 61.83 n/a .000
11447 (MstUsed: .2845E+01 m3, TotDvVol: .0000E+00 m3, N-OvF= 0, TotDvOvF= 0.hrs)
11448 RO550-C01132-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11449 SAVE RTD + 1.0 01:Area-A 66.75 8.917_MoDate 29:16 61.83 n/a .000
11450 [IARc: 4.00; SMIN: 17.43; SMAX: 116.21; SK: .010]
11451 [InterEventTime=12.00]
11452 RO550-C01133-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11453 ROUTE RESERVOIR -> 1.0 02:1Area-A 66.75 8.917_MoDate 29:16 61.83 n/a .000
11454 overlow out <= 1.0 01:1SADT 66.75 1.070_MoDate 29:16 61.83 n/a .000
11455 overlow <= 1.0 01:1SADT .00 .000_MoDate 0:00 .00 n/a .000
11456 (MstUsed: .2845E+01 m3, TotDvVol: .0000E+00 m3, N-OvF= 0, TotDvOvF= 0.hrs)
11457 RO550-C01134-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11458 SAVE RTD + 1.0 01:Area-A 66.75 8.917_MoDate 29:16 61.83 n/a .000
11459 [IARc: 4.00; SMIN: 17.43; SMAX: 116.21; SK: .010]
11460 [InterEventTime=12.00]
11461 RO550-C01135-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11462 CONTINUOUS STANDBY 1.0 01:Area-A 66.75 8.917_MoDate 29:16 61.83 n/a .000
11463 [XMP: 68;TMD: 85]
11464 (Horton parameters) Fw: 76.20;Fc: 13.20;DCAY:4.14; Pa: .00]
11465 (Previous area: IArea: 4.67;SLDP: .50;LDP: .50;MHP: .250;SDCP: .0]
11466 (Impervious area: IAlmp: 1.57;SLDp: .50;LdI: 193.9MI-.013;SCL: .0]
11467 [IARcLimp= 4.00; IARcEper= 4.00]
11468 RO550-C01136-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11469 ROUTE RESERVOIR -> 1.0 02:1Area-A 66.75 8.917_MoDate 29:16 61.83 n/a .000
11470 overlow out <= 1.0 01:1SADT 66.75 1.070_MoDate 29:16 61.83 n/a .000
11471 overlow <= 1.0 01:1SADT .00 .000_MoDate 0:00 .00 n/a .000
11472 (MstUsed: .4452E-01 m3, TotDvVol: .0000E+00 m3, N-OvF= 0, TotDvOvF= 0.hrs)
11473 RO550-C01137-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11474 SAVE RTD + 1.0 01:Area-A 66.75 8.917_MoDate 29:16 61.83 n/a .000
11475 [IARc: 4.00; SMIN: 17.43; SMAX: 116.21; SK: .010]
11476 [InterEventTime=12.00]
11477 RO550-C01138-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11478 ROUTE RESERVOIR -> 1.0 02:1Area-A 66.75 8.917_MoDate 29:16 61.83 n/a .000
11479 overlow out <= 1.0 01:1SADT 66.75 1.070_MoDate 29:16 61.83 n/a .000
11480 overlow <= 1.0 01:1SADT .00 .000_MoDate 0:00 .00 n/a .000
11481 (MstUsed: .3103E-02 m3, TotDvVol: .0000E+00 m3, N-OvF= 0, TotDvOvF= 0.hrs)
11482 RO550-C01139-DT-INDY-----AREHA-OP-AREAS-TeakDate_hh:mm-----Rvm-R-C-----DWPMs
11483 ADD RTD + 1.0 02:1C6-STR 1.87 .110_MoDate 28:18 64.42 n/a .000
11484 + 1.0 02:1C6-STR 1.87 .110_MoDate 28:18 64.42 n/a .000
11485 + 1.0 02:1C6-STR 1.87 .110_MoDate 28:18 64.42 n/a .000
11486 + 1.0 02:1C6-STR 1.87 .110_MoDate 28:18 64.42 n/a .000
11487 + 1.0 02:1C6-STR 1.87 .110_MoDate 28:18 64.42 n/a .000
11488 + 1.0 02:1C6-STR 1.87 .110_MoDate 28:18 64.42 n/a .000
11489 (MstUsed: .4698E-01 m3, TotDvVol: .0000E+00 m3
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13091 # Tributary Drainage Area to MSS Pond = 145 ha
13092 *****
13093 #
13094 # Hydrograph from Curriam Drain routed to Jockvale Road
13095 # Channel X-Section obtained from RWCA Hydraulic Model - Station 2462
13096 #
13097 R050-C00387-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13098 ROUTE CHANNEL -> 1.0 02:COVRI 55019.59 126.926 NoDate 36:27 34.22 n/a .000
13099 [RDV: 1.00] out-< 1.0 01:MI_DE 55019.59 126.908 NoDate 36:31 34.22 n/a .000
13100 [L/S= 580./ 445./ 945.]
13101 [Vmax: 0.065/0.061]
13102 *****
13103 # Catchment MILLS
13104 # To SWM Facility north of the Jock
13105 # - Primarily residential development
13106 #
13107 R050-C00388-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13108 CONTINUOUS STANHYD 1.0 01:MILLS 175.99 17.756 NoDate 28:06 50.66 .622 .000
13109 [XIMG= 2:TMP= 38]
13110 [LOSS: 2 :CN 74.0]
13111 [Impervious area: IArea: 4.67:SDP1:0.0:LD: 400 :HMD: 250:SCP: 0]
13112 [Impervious area: IArea: 1.57:SDP1:0.0:LD: 400 :HMD: 250:SCP: 0]
13113 [SMin: 4.00 :SMax: 4.00]
13114 [SMin: 36.67 :SMax: 244.49 :Sk: 0.10]
13115 *****
13116 # Chapman Mills SWM Pond
13117 # - Rating curve obtained from CCL hydraulic modeling
13118 #
13119 R050-C00389-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13120 ROUTE RESERVOIR 1.0 02:MILLS 179.99 17.756 NoDate 28:06 50.66 n/a .000
13121 [RDV: 1.00] out-< 1.0 01:MI_DE 153.87 4.050 NoDate 28:11 50.66 n/a .000
13122 overflow <= 1.0 03:MI-UV 22.12 12.440 NoDate 28:11 50.66 n/a .000
13123 [MxTotVol: 59288.0 m3, TotVol: 11212.0 m3, M-ovr: 2, TotDur: 0.7 hrs]
13124 R050-C00390-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13125 ADD HYD + 1.0 02:DESIRE 55019.59 126.926 NoDate 36:31 34.22 n/a .000
13126 [L/S= 580./ 445./ 945.]
13127 [Vmax: 0.065/0.061]
13128 *****
13129 R050-C00391-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13130 SAVE HYD 1.0 01:MI_DE 55019.59 126.926 NoDate 36:30 34.27 n/a .000
13131 [L/S= 580./ 445./ 945.]
13132 *****
13133 # remark:Total Flows at Jockvale Road
13134 #
13135 # Hydrograph from Jockvale Road routed to Heart's Desire
13136 # Channel X-Section obtained from RWCA Hydraulic Model - Station 689
13137 #
13138 R050-C00392-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13139 ROUTE CHANNEL -> 1.0 02:MI_DE 55019.59 126.926 NoDate 36:30 34.27 n/a .000
13140 [RDV: 1.00] out-< 1.0 01:MI_DE 55019.59 126.926 NoDate 36:43 34.27 n/a .000
13141 [L/S= 1942./ 2271./ 2271.]
13142 [Vmax: 1.577/2.000/2.490]
13143 *****
13144 # Catchment DESIRE
13145 # To Jock River (north of the Jock)
13146 # - Rural-estate subdivision (Heart's Desire Community)
13147 #
13148 R050-C00393-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13149 CONTINUOUS STANHYD 1.0 01:DESIRE 23.78 2.563 NoDate 28:03 46.85 5.75 .000
13150 [XIMG= 2:TMP= 25]
13151 [LOSS: 2 :CN 77.0]
13152 [Impervious area: IArea: 4.67:SDP1:0.0:LD: 400 :HMD: 250:SCP: 0]
13153 [Impervious area: IArea: 1.57:SDP1:0.0:LD: 400 :HMD: 250:SCP: 0]
13154 [SMin: 4.00 :SMax: 4.00]
13155 *****
13156 # Jockvale SWM Facility
13157 # - Residential development & golf course
13158 # - JFSA 2021-01-11 update: After updating CORGIS as per IRI CORGIS, July 2008.
13159 # Jockvale Area became 235.13 ha instead of 257.61 ha. JockVA separated into two areas JockVA and EX-LAND 32.5 ha as
13160 #
13161 R050-C00394-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13162 CONTINUOUS STANHYD 1.0 01:JOCKVA 225.13 25.253 NoDate 28:07 56.33 6.91 .000
13163 [XIMG= 5:TMP= 50]
13164 [LOSS: 2 :CN 74.0]
13165 [Impervious area: IArea: 4.67:SDP1:0.0:LD: 400 :HMD: 250:SCP: 0]
13166 [Impervious area: IArea: 1.57:SDP1:0.0:LD: 400 :HMD: 250:SCP: 0]
13167 [SMin: 4.00 :SMax: 4.00]
13168 [SMin: 36.67 :SMax: 244.49 :Sk: 0.10]
13169 *****
13170 R050-C00395-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13171 ADD HYD + 1.0 02:JOCKVA 225.13 25.253 NoDate 28:07 56.33 n/a .000
13172 [L/S= 1942./ 2271./ 2271.]
13173 [Vmax: 1.577/2.000/2.490]
13174 *****
13175 R050-C00396-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13176 SAVE HYD 1.0 01:JOCKVA 225.13 25.253 NoDate 28:07 56.36 n/a .000
13177 [L/S= 1942./ 2271./ 2271.]
13178 *****
13179 # remark:Total Flows at KB first pond
13180 #
13181 # Jockvale SWM Facility
13182 # - Rating curve obtained from Jockvale Servicing Study (CCL 1998)
13183 #
13184 R050-C00397-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13185 ROUTE CHANNEL -> 1.0 02:JOCKVA 225.13 25.253 NoDate 28:07 56.36 n/a .000
13186 [RDV: 1.00] out-< 1.0 01:JOCK_P 225.13 25.253 NoDate 28:07 56.36 n/a .000
13187 overflow <= 1.0 03:JOCK_P 225.13 25.253 NoDate 28:07 56.36 n/a .000
13188 [MxTotVol: 59288.0 m3, TotVol: 11212.0 m3, M-ovr: 0, TotDur: 0.7 hrs]
13189 R050-C00398-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13190 ADD HYD + 1.0 02:DESIRE 23.78 2.563 NoDate 28:03 46.85 n/a .000
13191 [L/S= 1942./ 2271./ 2271.]
13192 [Vmax: 1.577/2.000/2.490]
13193 *****
13194 R050-C00399-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13195 SAVE HYD 1.0 01:MI_DE 55019.59 126.926 NoDate 36:42 34.38 n/a .000
13196 [L/S= 580./ 445./ 945.]
13197 *****
13198 # remark:Total Flows at Heart's Desire
13199 #
13200 # Hydrograph from Heart's Desire routed to Rideau River
13201 # Channel X-Section obtained from RWCA Hydraulic Model - Station 0
13202 #
13203 R050-C00400-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13204 ROUTE CHANNEL -> 1.0 02:MI_DE 55019.59 126.926 NoDate 36:42 34.38 n/a .000
13205 [RDV: 1.00] out-< 1.0 01:MI 55476.26 128.180 NoDate 36:45 34.38 n/a .000
13206 [L/S= 1942./ 2271./ 2271.]
13207 [Vmax: 2.123/2.000/2.248]
13208 *****
13209 # Catchment S-2
13210 # To Jock River (north and south)
13211 # - Undeveloped floodplain
13212 #
13213 R050-C00401-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13214 CONTINUOUS NASHVD 1.0 01:S-2 102.94 4.795 NoDate 28:20 35.39 4.34 .000
13215 [CN: 72.0 :N: 3.00 :Tp: 4.0]
13216 [AREC: 4.00 :SMin: 39.75 :SMax: 264.99 :Sk: 0.10]
13217 [InterEventTime: 12.00]
13218 R050-C00402-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13219 ADD HYD + 1.0 02:MI 55476.26 128.180 NoDate 36:45 34.38 n/a .000
13220 [L/S= 1942./ 2271./ 2271.]
13221 [Vmax: 2.123/2.000/2.248]
13222 *****
13223 R050-C00403-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13224 SAVE HYD 1.0 01:MI_DE 55476.26 128.174 NoDate 36:42 34.38 n/a .000
13225 [L/S= 1942./ 2271./ 2271.]
13226 *****
13227 # remark:Total Flows at Rideau River
13228 *****
13229 # END OF RUN : 99
13230 *****
13231 #
13232 #
13233 #
13234 *****
13235 #
13236 *****
13237 *****
13238 *****
13239 *****
13240 *****
13241 *****
13242 *****
13243 *****
13244 *****
13245 *****
13246 *****
13247 *****
13248 *****
13249 *****
13250 *****
13251 *****
13252 *****
13253 *****
13254 *****
13255 *****
13256 *****
13257 *****
13258 *****
13259 *****
13260 *****
13261 *****
13262 *****
13263 *****
13264 *****
13265 *****
13266 *****
13267 *****
13268 *****
13269 *****
13270 *****
13271 *****
13272 *****
13273 *****
13274 *****
13275 *****
13276 *****
13277 *****

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Parameters for PREVIOUS surfaces in STANHYD:
[Area: 4.67 mm [LQ=55.00 m] [Wp: 253]
Parameters for IMPERVIOUS surfaces in STANHYD:
[Area: 1.57 mm [LQ= 1.50] [Wp: 013]
Parameters used in NASHVD:
[tau: 4.67 mm [W: 3.00]
Average monthly Pan Evaporation data in (mm)
13285: JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
13286: 00 00 00 00 00 00 00 00 00 00 00 00
13287: Average monthly Potential Evapotranspiration in (mm)
13288: JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
13289: 00 00 00 00 00 00 00 00 00 00 00 00
13290: R010-C00005-----
13291: *****
13292: [ADPIn: 50.00 :ADPIdy: 8500 :ADPIdt: 9999]
13293: [ADPMax:19.84 :ADPMax: 69.19 :ADPMin: 44.87]
13294: #
13295: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13296: # of 1.32
13297: R010-C00006-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13298: CONTINUOUS NASHVD 1.0 01:R_SW 3683.00 21.616 NoDate 35:52 35.18 397 .000
13299: [CN: 64.0 :N: 3.00 :Tp: 7.13]
13300: [AREC: 4.00 :SMin: 37.65 :SMax: 380.32 :Sk: 0.10]
13301: [InterEventTime: 12.00]
13302: #
13303: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13304: # of 1.32
13305: R010-C00007-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13306: CONTINUOUS NASHVD 1.0 01:R_SW 971.00 8.203 NoDate 32:33 32.84 371 .000
13307: [CN: 61.0 :N: 3.00 :Tp: 3.98]
13308: [AREC: 4.00 :SMin: 64.50 :SMax: 430.01 :Sk: 0.10]
13309: [InterEventTime: 12.00]
13310: #
13311: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13312: # of 1.32
13313: R010-C00008-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13314: CONTINUOUS NASHVD 1.0 01:R_SW 3074.00 10.428 NoDate 39:59 28.29 319 .000
13315: [CN: 67.0 :N: 3.00 :Tp: 3.13]
13316: [AREC: 4.00 :SMin: 83.24 :SMax: 554.96 :Sk: 0.10]
13317: [InterEventTime: 12.00]
13318: R010-C00009-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13319: CONTINUOUS NASHVD 1.0 01:R_SW 1781.00 19.695 NoDate 33:38 42.49 480 .000
13320: [CN: 72.0 :N: 3.00 :Tp: 3.91]
13321: [AREC: 4.00 :SMin: 39.75 :SMax: 264.99 :Sk: 0.10]
13322: [InterEventTime: 12.00]
13323: R010-C00010-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13324: CONTINUOUS NASHVD 1.0 01:R_SW 500.00 10.735 NoDate 29:21 36.76 415 .000
13325: [CN: 66.0 :N: 3.00 :Tp: 1.24]
13326: [AREC: 4.00 :SMin: 52.62 :SMax: 350.79 :Sk: 0.10]
13327: [InterEventTime: 12.00]
13328: #
13329: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13330: # of 1.80
13331: R010-C00011-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13332: CONTINUOUS NASHVD 1.0 01:NNLCK 1917.00 14.496 NoDate 34:24 36.76 415 .000
13333: [CN: 66.0 :N: 3.00 :Tp: 5.29]
13334: [AREC: 4.00 :SMin: 52.62 :SMax: 350.79 :Sk: 0.10]
13335: [InterEventTime: 12.00]
13336: #
13337: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13338: # of 1.32
13339: R010-C00012-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13340: CONTINUOUS NASHVD 1.0 01:SW_0 5666.00 37.663 NoDate 37:48 42.49 480 .000
13341: [CN: 72.0 :N: 3.00 :Tp: 3.91]
13342: [AREC: 4.00 :SMin: 39.75 :SMax: 264.99 :Sk: 0.10]
13343: [InterEventTime: 12.00]
13344: #
13345: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13346: # of 1.75
13347: R010-C00013-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13348: CONTINUOUS NASHVD 1.0 01:SW_0 879.00 16.218 NoDate 39:59 36.76 415 .000
13349: [CN: 66.0 :N: 3.00 :Tp: 11.66]
13350: [AREC: 4.00 :SMin: 52.62 :SMax: 350.79 :Sk: 0.10]
13351: [InterEventTime: 12.00]
13352: #
13353: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13354: # of 1.68
13355: R010-C00014-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13356: CONTINUOUS NASHVD 1.0 01:SW_0 1132.00 16.501 NoDate 30:52 40.82 461 .000
13357: [CN: 70.0 :N: 3.00 :Tp: 2.11]
13358: [AREC: 4.00 :SMin: 43.07 :SMax: 287.10 :Sk: 0.10]
13359: [InterEventTime: 12.00]
13360: #
13361: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13362: # of 1.32
13363: R010-C00015-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13364: CONTINUOUS NASHVD 1.0 01:NNLCK 4464.00 18.060 NoDate 39:59 33.61 380 .000
13365: [CN: 62.0 :N: 3.00 :Tp: 1.21]
13366: [AREC: 4.00 :SMin: 61.90 :SMax: 412.66 :Sk: 0.10]
13367: [InterEventTime: 12.00]
13368: #
13369: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13370: # of 1.80
13371: R010-C00016-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13372: CONTINUOUS NASHVD 1.0 01:SW_0 31.00 3.255 NoDate 28:57 34.99 388 .000
13373: [CN: 63.0 :N: 3.00 :Tp: 5.0]
13374: [AREC: 4.00 :SMin: 55.63 :SMax: 396.11 :Sk: 0.10]
13375: [InterEventTime: 12.00]
13376: #
13377: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13378: # of 1.65
13379: R010-C00017-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13380: CONTINUOUS NASHVD 1.0 01:HLDR 1854.00 21.238 NoDate 38:28 36.76 415 .000
13381: [CN: 68.0 :N: 3.00 :Tp: 8.62]
13382: [AREC: 4.00 :SMin: 52.62 :SMax: 350.79 :Sk: 0.10]
13383: [InterEventTime: 12.00]
13384: #
13385: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13386: # of 1.82
13387: R010-C00018-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13388: CONTINUOUS NASHVD 1.0 01:SW_0 3197.00 16.421 NoDate 36:21 29.79 336 .000
13389: [CN: 57.0 :N: 3.00 :Tp: 6.65]
13390: [AREC: 4.00 :SMin: 76.32 :SMax: 508.81 :Sk: 0.10]
13391: [InterEventTime: 12.00]
13392: #
13393: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13394: # of 1.75
13395: R010-C00019-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13396: CONTINUOUS NASHVD 1.0 01:SW_6 165.00 1.511 NoDate 33:01 37.57 424 .000
13397: [CN: 67.0 :N: 3.00 :Tp: 4.18]
13398: [AREC: 4.00 :SMin: 60.85 :SMax: 336.97 :Sk: 0.10]
13399: [InterEventTime: 12.00]
13400: #
13401: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13402: # of 1.6
13403: R010-C00020-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13404: CONTINUOUS NASHVD 1.0 01:VLDR 1332.00 10.882 NoDate 35:10 42.49 480 .000
13405: [CN: 70.0 :N: 3.00 :Tp: 5.93]
13406: [AREC: 4.00 :SMin: 39.75 :SMax: 264.99 :Sk: 0.10]
13407: [InterEventTime: 12.00]
13408: R010-C00021-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13409: CONTINUOUS NASHVD 1.0 01:SW_5 224.00 9.576 NoDate 28:44 47.62 538 .000
13410: [CN: 77.0 :N: 3.00 :Tp: 7.9]
13411: [AREC: 4.00 :SMin: 31.15 :SMax: 207.66 :Sk: 0.10]
13412: [InterEventTime: 12.00]
13413: #
13414: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13415: # of 1.20
13416: R010-C00022-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13417: CONTINUOUS NASHVD 1.0 01:FL_CK 4943.00 52.056 NoDate 33:52 44.47 459 .000
13418: [CN: 74.0 :N: 3.00 :Tp: 4.45]
13419: [AREC: 4.00 :SMin: 36.67 :SMax: 244.49 :Sk: 0.10]
13420: [InterEventTime: 12.00]
13421: R010-C00023-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13422: CONTINUOUS NASHVD 1.0 01:FL_CK 20.00 1.097 NoDate 28:39 52.06 588 .000
13423: [CN: 81.0 :N: 3.00 :Tp: 6.2]
13424: [AREC: 4.00 :SMin: 35.21 :SMax: 168.09 :Sk: 0.10]
13425: [InterEventTime: 12.00]
13426: #
13427: # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
13428: # of 1.61
13429: R010-C00024-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13430: CONTINUOUS NASHVD 1.0 01:SW_SAI 1412.00 10.184 NoDate 37:44 45.88 518 .000
13431: [CN: 75.0 :N: 3.00 :Tp: 8.00]
13432: [AREC: 4.00 :SMin: 33.81 :SMax: 225.43 :Sk: 0.10]
13433: [InterEventTime: 12.00]
13434: R010-C00025-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13435: CONTINUOUS NASHVD 1.0 01:SW_4 585.00 14.953 NoDate 29:55 52.06 588 .000
13436: [CN: 69.0 :N: 3.00 :Tp: 7.9]
13437: [AREC: 4.00 :SMin: 25.21 :SMax: 168.09 :Sk: 0.10]
13438: [InterEventTime: 12.00]
13439: R010-C00026-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13440: CONTINUOUS NASHVD 1.0 01:MLCK 1021.00 19.782 NoDate 30:45 51.16 578 .000
13441: [CN: 83.0 :N: 3.00 :Tp: 4.61]
13442: [AREC: 4.00 :SMin: 26.32 :SMax: 175.50 :Sk: 0.10]
13443: [InterEventTime: 12.00]
13444: R010-C00027-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13445: CONTINUOUS NASHVD 1.0 01:SW_2 177.00 7.567 NoDate 28:44 47.62 538 .000
13446: [CN: 77.0 :N: 3.00 :Tp: 7.9]
13447: [AREC: 4.00 :SMin: 31.15 :SMax: 207.66 :Sk: 0.10]
13448: [InterEventTime: 12.00]
13449: R010-C00028-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13450: CONTINUOUS NASHVD 1.0 01:FLDR 7373.00 40.730 NoDate 31:28 46.75 528 .000
13451: [CN: 81.0 :N: 3.00 :Tp: 3.25]
13452: [AREC: 4.00 :SMin: 25.21 :SMax: 168.09 :Sk: 0.10]
13453: [InterEventTime: 12.00]
13454: R010-C00029-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms
13455: CONTINUOUS NASHVD 1.0 01:SW_0 7373.00 40.730 NoDate 31:28 46.75 528 .000
13456: [CN: 76.0 :N: 3.00 :Tp: 3.03]
13457: [AREC: 4.00 :SMin: 32.46 :SMax: 216.39 :Sk: 0.10]
13458: [InterEventTime: 12.00]
13459: #
13460: # Routing hydrographs
13461: #
13462: # Starting with the addition of Jock River Headwater and Subwatershed 13
13463: #
13464: R010-C00030-----Dtn-ID-NHVD-----AREAh-QPEARms-TpeakDate_hh:mm-----Rvm-R-C-----DWPFms

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13465#	ADD HYD	1.0 02:R_W3	3680.0	21.616 No.Date	36:52	35.18	n/a	.000
13466#		1.0 02:R_W3	3711.8	8.203 No.Date	32:33	32.84	n/a	.000
13467#	SUM#	1.0 01:R_M13	4651.0	27.660 No.Date	35:21	34.69	n/a	.000
13469#	Sum of hydrographs from Node 13 routed to Node 13A							
13470#	[Approximated cross-section - see cross-section 258]							
13471#	Use n=0.04 for summer conditions and n=0.025 for spring conditions							
13472#								
13473#	ROUTER CHANNEL ->	1.0 02:R_M13	4651.0	27.660 No.Date	35:21	34.69	n/a	.000
13474#	[R/S= 1.00] out->	1.0 02:R_W3	4651.0	10.428 No.Date	38:56	34.69	n/a	.000
13476#	[L/S= 807.4 / .027(.040)]							
13477#	[Vmax= .598;Dmax= 4.178]							
13478#								
13479#	Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A							
13480#								
13481#	ROUTER CHANNEL ->	1.0 02:R_W3	4651.0	27.660 No.Date	38:56	34.69	n/a	.000
13482#	ADD HYD	1.0 02:R_W3	3074.0	10.428 No.Date	39:59	28.29	n/a	.000
13483#		1.0 02:R_W3	3074.0	10.428 No.Date	39:59	28.29	n/a	.000
13484#	SUM#	1.0 01:R_M13A	7725.0	32.845 No.Date	39:44	32.14	n/a	.000
13485#								
13486#	Insertion of a reservoir to simulate the effects of the Goodwood Marsh							
13488#	ROUTER CHANNEL ->	1.0 02:R_W3	7725.0	32.845 No.Date	39:44	32.14	n/a	.000
13489#	ROUTER RESERVOIR ->	1.0 02:R_M13A	7725.0	32.845 No.Date	39:44	32.14	n/a	.000
13490#	out->	1.0 01:R_W3	7725.0	3.950 No.Date	62:26	32.14	n/a	.000
13491#	[Mdt=0.025; .1796E+03 m]							
13492#								
13493#	ROUTER CHANNEL ->	1.0 02:R_W3	7725.0	3.950 No.Date	62:26	32.14	n/a	.000
13494#	SAVE HYD	1.0 01:R_W3	7725.0	3.950 No.Date	62:26	32.14	n/a	.000
13495#	fname_H_R25M							
13496#	remark:flow at Res Out							
13497#	Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12							
13498#	[Approximated cross-section - see cross-section 258]							
13499#	Use n=0.04 for summer conditions and n=0.025 for spring conditions							
13500#								
13501#	ROUTER CHANNEL ->	1.0 02:R_W3	7725.0	3.950 No.Date	62:26	32.14	n/a	.000
13502#	[R/S= 1.00] out->	1.0 02:R_W3	7725.0	3.947 No.Date	64:43	32.14	n/a	.000
13503#	[L/S= 5926. / .076(.040)]							
13504#	[Vmax= .560;Dmax= 3.194]							
13505#								
13506#	Addition of Subwatershed Jock River at Ashton to Node 12							
13507#								
13508#	ROUTER CHANNEL ->	1.0 02:R_W3	7725.0	3.947 No.Date	64:43	32.14	n/a	.000
13509#	ADD HYD	1.0 02:R_W3	1781.0	19.695 No.Date	32:38	42.49	n/a	.000
13510#		1.0 02:R_W3	1781.0	19.695 No.Date	32:38	42.49	n/a	.000
13511#	SUM#	1.0 01:R_M12	9506.0	21.745 No.Date	32:41	34.08	n/a	.000
13512#								
13513#	ROUTER CHANNEL ->	1.0 02:R_W3	9506.0	21.745 No.Date	32:41	34.08	n/a	.000
13514#	SAVE HYD	1.0 01:R_M12	9506.0	21.745 No.Date	32:41	34.08	n/a	.000
13515#	fname_H_R22							
13516#	remark:flow at R_M12 near Ashton							
13517#	Sum of hydrographs from Node 12 routed to Node 11							
13518#	[Approximated cross-section - see cross-section 258]							
13519#	Use n=0.04 for summer conditions and n=0.025 for spring conditions							
13520#								
13521#	Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248							
13522#								
13523#	ROUTER CHANNEL ->	1.0 02:R_W3	9506.0	21.745 No.Date	32:41	34.08	n/a	.000
13524#	ROUTER CHANNEL ->	1.0 02:R_M12	9506.0	21.745 No.Date	32:41	34.08	n/a	.000
13525#	[R/S= 1.00] out->	1.0 01:R_M12	9506.0	21.522 No.Date	32:57	34.08	n/a	.000
13526#	[L/S= 97. / .054(.040)]							
13527#	[Vmax= .777;Dmax= 3.194]							
13528#								
13529#	Addition of Subwatershed 11 and No Name Creek to Node 11							
13530#								
13531#	ROUTER CHANNEL ->	1.0 02:R_W3	9506.0	21.522 No.Date	32:57	34.08	n/a	.000
13532#	ADD HYD	1.0 02:R_M12	9506.0	21.522 No.Date	32:57	34.08	n/a	.000
13533#		1.0 02:R_M12	9506.0	21.522 No.Date	32:57	34.08	n/a	.000
13534#	SUM#	1.0 01:R_M12	11923.0	39.138 No.Date	32:59	34.62	n/a	.000
13535#								
13536#	Sum of hydrographs from Node 11 routed to Node 10							
13537#	Section 1							
13538#								
13539#								
13540#	ROUTER CHANNEL ->	1.0 02:R_M11	11923.0	39.138 No.Date	32:59	34.62	n/a	.000
13541#	ROUTER CHANNEL ->	1.0 02:R_M11	11923.0	39.138 No.Date	32:59	34.62	n/a	.000
13542#	[R/S= 1.00] out->	1.0 01:R_M10	11923.0	23.609 No.Date	39:19	34.62	n/a	.000
13543#	[L/S= 14028. / .157(.040)]							
13544#	[Vmax= .486;Dmax= 1.492]							
13545#								
13546#	Addition of Subwatershed 10 to Node 10							
13547#								
13548#	ADD HYD	1.0 02:R_M10	5666.0	37.663 No.Date	37:48	42.49	n/a	.000
13549#		1.0 02:R_M10	5666.0	37.663 No.Date	37:48	42.49	n/a	.000
13550#	SUM#	1.0 01:R_M10	17899.0	61.058 No.Date	38:16	37.16	n/a	.000
13551#								
13552#	ROUTER CHANNEL ->	1.0 02:R_W3	17899.0	61.058 No.Date	38:16	37.16	n/a	.000
13553#	SAVE HYD	1.0 01:R_M10	17899.0	61.058 No.Date	38:16	37.16	n/a	.000
13554#	fname_H_R210							
13555#	remark:flow at R_M10 N10 + R_M10							
13556#	Addition of Kings Creek to S_M10							
13557#								
13558#	ROUTER CHANNEL ->	1.0 02:R_M10	17899.0	61.058 No.Date	38:16	37.16	n/a	.000
13559#	ADD HYD	1.0 02:R_M10	17899.0	61.058 No.Date	38:16	37.16	n/a	.000
13560#		1.0 02:R_W3	8376.0	36.118 No.Date	39:59	36.68	n/a	.000
13561#	SUM#	1.0 01:R_M10A	25865.0	96.054 No.Date	39:40	37.03	n/a	.000
13562#								
13563#	Sum of hydrographs from Node 10 routed to Node 9							
13564#	Section 2							
13565#								
13566#	ROUTER CHANNEL ->	1.0 02:R_M10A	25865.0	96.054 No.Date	39:40	37.03	n/a	.000
13567#	ROUTER CHANNEL ->	1.0 02:R_M10A	25865.0	96.054 No.Date	39:40	37.03	n/a	.000
13568#	[R/S= 1.00] out->	1.0 01:R_M9	25865.0	94.262 No.Date	39:59	37.03	n/a	.000
13569#	[L/S= 3982. / .075(.040)]							
13570#	[Vmax= .775;Dmax= 2.151]							
13571#								
13572#	Addition of Subwatershed 9 and Nichols Creek to Node 9							
13573#								
13574#	ROUTER CHANNEL ->	1.0 02:R_W3	25865.0	94.262 No.Date	39:59	36.68	n/a	.000
13575#	ADD HYD	1.0 02:R_M9	1132.0	16.201 No.Date	30:52	40.83	n/a	.000
13576#		1.0 02:R_M9	1132.0	16.201 No.Date	30:52	40.83	n/a	.000
13577#	SUM#	1.0 02:R_W3	4464.0	18.060 No.Date	39:59	33.61	n/a	.000
13578#		1.0 01:R_M9	31561.0	115.481 No.Date	39:59	36.68	n/a	.000
13579#								
13580#	Sum of hydrographs from Node 9 routed to Node 8							
13581#	Section 3							
13582#								
13583#	ROUTER CHANNEL ->	1.0 02:R_W3	31561.0	115.481 No.Date	39:59	36.68	n/a	.000
13584#	ROUTER CHANNEL ->	1.0 02:R_W3	31561.0	115.481 No.Date	39:59	36.68	n/a	.000
13585#	[R/S= 1.00] out->	1.0 01:R_M8	31561.0	109.395 No.Date	39:59	36.68	n/a	.000
13586#	[L/S= 2269. / .088(.045)]							
13587#	[Vmax= .374;Dmax= 1.924]							
13588#								
13589#	Addition of Subwatershed 8 and Bobb's drain to Node 8							
13590#								
13591#	ROUTER CHANNEL ->	1.0 02:R_W3	31561.0	109.395 No.Date	39:59	36.68	n/a	.000
13592#	ADD HYD	1.0 02:R_M8	131.0	1.259 No.Date	28:57	34.39	n/a	.000
13593#		1.0 02:R_M8	131.0	1.259 No.Date	28:57	34.39	n/a	.000
13594#	SUM#	1.0 01:R_M8	31692.0	111.218 No.Date	39:58	36.68	n/a	.000
13595#		1.0 01:R_M8	31692.0	111.218 No.Date	39:58	36.68	n/a	.000
13596#								
13597#	Sum of hydrographs from Node 8 routed to Node 7							
13598#	Section 4							
13599#								
13600#	ROUTER CHANNEL ->	1.0 02:R_W3	31692.0	111.218 No.Date	39:58	36.68	n/a	.000
13601#	ROUTER CHANNEL ->	1.0 02:R_W3	31692.0	111.218 No.Date	39:58	36.68	n/a	.000
13602#	[R/S= 1.00] out->	1.0 01:R_M7	31692.0	111.942 No.Date	44:52	36.68	n/a	.000
13603#	[L/S= 3750. / .053(.070)]							
13604#	[Vmax= .237;Dmax= 2.112]							
13605#								
13606#	Addition of Subwatershed 7 to Node 7							
13607#								
13608#	ROUTER CHANNEL ->	1.0 02:R_W3	31692.0	111.942 No.Date	44:52	36.68	n/a	.000
13609#	ADD HYD	1.0 02:R_M7	3197.0	16.421 No.Date	36:21	29.79	n/a	.000
13610#								















# Attachment E

Model 4B – Jock River Reach One Future Conditions – With SWM controls

JFSA, 2021

SWMHYMO Input & Summary files

```

1  20  Metric units / ID numbers OFF
2  *#*****
3  *# SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
4  *#*****
5  *# Project Name: [Jock River] Project Number: [1474-16]
6  *# Date : 04-03-2021
7  *# Modeller : [M.M.]
8  *# Company : JFSAinc.
9  *# License # : 2549237
10 *#*****
11 *# CALIBRATION OF SUMMER MODEL PARAMETERS
12 *# USING CONTINUOUS SIMULATIONS
13 *# Rainfall data from JFSA raingauge installed at site + other gauges by the City
14 *# Use data collected from May 1st to July 14, 2003
15 *# 2020-11-30 change TMJSTO in COMPUTE DUALHYD (TMJSTO = 0.1 instead of 0.0001)
16 *# 2020-12-01 correct pond curve values
17 *# 2020-12-01 change W_CLAR_BRAZ XIMP to 0.55, SLPI=[0.5](%) (impervious slope), and
LGI up to 700m
18 *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 2462 (NHYDout=["N_TO"]
,NHYDin=["SN_TO"]) from 0.033 % (as per Stantec Report 2007) to 0.05 % so the model
will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELs
aren't well suited to really flat slopes.
19 *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHYDout=["N_WC"]
,NHYDin=["SN_CE"]) from 0.01 % (as per Stantec Report 2007) to 0.0255 % so the model
will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELs
aren't well suited to really flat slopes.
20 *
21 * Calibrated parameters for Summer 2003 data: APII=50, APIK=0.85, CN=varies,
22 * SK=0.01, InterEventTime=12,
23 * GWResk=0.96, VHydCond=0.055
24 *
25 *# -----
26 *
27 *START TZERO=[2003.0501], METOUT=[2], NSTORM=[1], NRUN=[001]
28 * ["XAVG0315.STM"] average storm data a 15 minute time step
29 * The above rainf file is an average of the JFSA gauge data
30 * with the City of Ottawa rainfall data collected during
31 * the same period.
32 *% 2 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
33 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[2]
34 ["C24SC002.stm"] <--storm filename, one per line for NSTORM time
35 *%-----|-----|
36 *%-----|-----|
37 READ STORM STORM_FILENAME=["storm.001"]
38 *%-----|-----|
39 MODIFY STORM ICASEms=[1], NSHIFT=[96],
40 RedFACT=[1],
41 *%-----|-----|
42 DEFAULT VALUES ICASEdef=[1], read and print values
43 DEFVAL_FILENAME=["CitiGate.DEF"]
44 *%-----|-----|
45 COMPUTE API APII=[50], APIK=[.85]/day
46 *%-----|-----|
47 *%-----|-----|
48 *#
49 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
50 *# of 1.32
51 *%-----|-----|
52 CONTINUOUS NASHYD NHYD=["JR_HW"], DT=[1]min, AREA=[3680](ha),
53 DWF=[0](cms), CN/C=[64], IA=[2.5](mm),
54 N=[3.0], TP=[7.13]hrs,
55 Continuous simulation parameters:
56 IaRECper=[4](hrs),
57 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
58 InterEventTime=[12](hrs)
59 Baseflow simulation parameters:

```



```

60         BaseFlowOption=[1] ,
61         InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
62         VHydCond=[0.055](mm/hr),   END=-1
63     *%-----|-----
64     *#
65     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
66     *# of 1.32
67     *%-----|-----
68     CONTINUOUS NASHYD  NHYD=["SW_13"], DT=[1]min, AREA=[971](ha),
69                        DWF=[0](cms),  CN/C=[61], IA=[2.5](mm),
70                        N=[3.0], TP=[3.76]hrs,
71                        Continuous simulation parameters:
72                        IaRECper=[4](hrs),
73                        SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
74                        InterEventTime=[12](hrs)
75                        Baseflow simulation parameters:
76                        BaseFlowOption=[1] ,
77                        InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
78                        VHydCond=[0.055](mm/hr),   END=-1
79     *%-----|-----
80     *#
81     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
82     *# of 1.80
83     *%-----|-----
84     CONTINUOUS NASHYD  NHYD=["JR_GWM"], DT=[1]min, AREA=[3074](ha),
85                        DWF=[0](cms),  CN/C=[55], IA=[2.5](mm),
86                        N=[3], TP=[11.33]hrs,
87                        Continuous simulation parameters:
88                        IaRECper=[4](hrs),
89                        SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
90                        InterEventTime=[12](hrs)
91                        Baseflow simulation parameters:
92                        BaseFlowOption=[1] ,
93                        InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
94                        VHydCond=[0.055](mm/hr),   END=-1
95     *%-----|-----
96     CONTINUOUS NASHYD  NHYD=["JR_ASH"], DT=[1]min, AREA=[1781](ha),
97                        DWF=[0](cms),  CN/C=[72], IA=[2.5](mm),
98                        N=[3.0], TP=[3.91]hrs,
99                        Continuous simulation parameters:
100                       IaRECper=[4](hrs),
101                       SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
102                       InterEventTime=[12](hrs)
103                       Baseflow simulation parameters:
104                       BaseFlowOption=[1] ,
105                       InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
106                       VHydCond=[0.055](mm/hr),   END=-1
107     *%-----|-----
108     CONTINUOUS NASHYD  NHYD=["SW_11"], DT=[1]min, AREA=[500](ha),
109                        DWF=[0](cms),  CN/C=[66], IA=[2.5](mm),
110                        N=[3.0], TP=[1.24]hrs,
111                        Continuous simulation parameters:
112                        IaRECper=[4](hrs),
113                        SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
114                        InterEventTime=[12](hrs)
115                        Baseflow simulation parameters:
116                        BaseFlowOption=[1] ,
117                        InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
118                        VHydCond=[0.055](mm/hr),   END=-1
119     *%-----|-----
120     *#
121     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
122     *# of 1.80
123     *%-----|-----
124     CONTINUOUS NASHYD  NHYD=["NN_CK"], DT=[1]min, AREA=[1917](ha),
125                        DWF=[0](cms),  CN/C=[66], IA=[2.5](mm),

```

```

126 N=[3.0], TP=[5.29]hrs,
127 Continuous simulation parameters:
128 IaREcper=[4](hrs),
129 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
130 InterEventTime=[12](hrs)
131 Baseflow simulation parameters:
132 BaseFlowOption=[1] ,
133 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
134 VHydCond=[0.055](mm/hr), END=-1
135 *%-----|-----
136 *#
137 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
138 *# of 1.52
139 *%-----|-----
140 CONTINUOUS NASHYD NHYD=["SW_10"], DT=[1]min, AREA=[5666](ha),
141 DWF=[0](cms), CN/C=[72], IA=[2.5](mm),
142 N=[3.0], TP=[8.00]hrs,
143 Continuous simulation parameters:
144 IaREcper=[4](hrs),
145 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
146 InterEventTime=[12](hrs)
147 Baseflow simulation parameters:
148 BaseFlowOption=[1] ,
149 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
150 VHydCond=[0.055](mm/hr), END=-1
151 *%-----|-----
152 *#
153 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
154 *# of 1.75
155 *%-----|-----
156 CONTINUOUS NASHYD NHYD=["KG_CK"], DT=[1]min, AREA=[8376](ha),
157 DWF=[0](cms), CN/C=[66], IA=[2.5](mm),
158 N=[3.0], TP=[11.66]hrs,
159 Continuous simulation parameters:
160 IaREcper=[4](hrs),
161 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
162 InterEventTime=[12](hrs)
163 Baseflow simulation parameters:
164 BaseFlowOption=[1] ,
165 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
166 VHydCond=[0.055](mm/hr), END=-1
167 *%-----|-----
168 *#
169 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
170 *# of 1.68
171 *%-----|-----
172 CONTINUOUS NASHYD NHYD=["SW_9"], DT=[1]min, AREA=[1132](ha),
173 DWF=[0](cms), CN/C=[70], IA=[2.5](mm),
174 N=[3.0], TP=[2.51]hrs,
175 Continuous simulation parameters:
176 IaREcper=[4](hrs),
177 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
178 InterEventTime=[12](hrs)
179 Baseflow simulation parameters:
180 BaseFlowOption=[1] ,
181 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
182 VHydCond=[0.055](mm/hr), END=-1
183 *%-----|-----
184 *#
185 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
186 *# of 1.82
187 *%-----|-----
188 CONTINUOUS NASHYD NHYD=["NC_CK"], DT=[1]min, AREA=[4464](ha),
189 DWF=[0](cms), CN/C=[62], IA=[2.5](mm),
190 N=[3.0], TP=[11.32]hrs,
191 Continuous simulation parameters:

```

```

192         IaREcper=[4](hrs),
193         SMIN=[-1](mm),  SMAx=[-1](mm), SK=[0.010]/(mm),
194         InterEventTime=[12](hrs)
195         Baseflow simulation parameters:
196         BaseFlowOption=[1] ,
197         InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
198         VHydCond=[0.055](mm/hr),  END=-1
199     *%-----|-----
200     *#
201     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
202     *# of 1.80
203     *%-----|-----
204     CONTINUOUS NASHYD  NHYD=["SW_8"], DT=[1]min, AREA=[131](ha),
205                       DWF=[0](cms),  CN/C=[63], IA=[2.5](mm),
206                       N=[3.0], TP=[0.90]hrs,
207                       Continuous simulation parameters:
208                       IaREcper=[4](hrs),
209                       SMIN=[-1](mm),  SMAx=[-1](mm), SK=[0.010]/(mm),
210                       InterEventTime=[12](hrs)
211                       Baseflow simulation parameters:
212                       BaseFlowOption=[1] ,
213                       InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
214                       VHydCond=[0.055](mm/hr),  END=-1
215     *%-----|-----
216     *#
217     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
218     *# of 1.65
219     *%-----|-----
220     CONTINUOUS NASHYD  NHYD=["HB_DR"], DT=[1]min, AREA=[3854](ha),
221                       DWF=[0](cms),  CN/C=[66], IA=[2.5](mm),
222                       N=[3.0], TP=[8.42]hrs,
223                       Continuous simulation parameters:
224                       IaREcper=[4](hrs),
225                       SMIN=[-1](mm),  SMAx=[-1](mm), SK=[0.010]/(mm),
226                       InterEventTime=[12](hrs)
227                       Baseflow simulation parameters:
228                       BaseFlowOption=[1] ,
229                       InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
230                       VHydCond=[0.055](mm/hr),  END=-1
231     *%-----|-----
232     *#
233     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
234     *# of 1.82
235     *%-----|-----
236     CONTINUOUS NASHYD  NHYD=["SW_7"], DT=[1]min, AREA=[3197](ha),
237                       DWF=[0](cms),  CN/C=[57], IA=[2.5](mm),
238                       N=[3.0], TP=[6.65]hrs,
239                       Continuous simulation parameters:
240                       IaREcper=[4](hrs),
241                       SMIN=[-1](mm),  SMAx=[-1](mm), SK=[0.010]/(mm),
242                       InterEventTime=[12](hrs)
243                       Baseflow simulation parameters:
244                       BaseFlowOption=[1] ,
245                       InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
246                       VHydCond=[0.055](mm/hr),  END=-1
247     *%-----|-----
248     *#
249     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
250     *# of 1.75
251     *%-----|-----
252     CONTINUOUS NASHYD  NHYD=["SW_6"], DT=[1]min, AREA=[165](ha),
253                       DWF=[0](cms),  CN/C=[67], IA=[2.5](mm),
254                       N=[3.0], TP=[4.18]hrs,
255                       Continuous simulation parameters:
256                       IaREcper=[4](hrs),
257                       SMIN=[-1](mm),  SMAx=[-1](mm), SK=[0.010]/(mm),

```

```

258 InterEventTime=[12](hrs)
259 Baseflow simulation parameters:
260 BaseFlowOption=[1] ,
261 InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
262 VHydCond=[0.055](mm/hr) , END=-1
263 *%-----|-----
264 *#
265 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
266 *# of 1.67
267 *%-----|-----
268 CONTINUOUS NASHYD NHYD=["VG_DR"] , DT=[1]min , AREA=[1332](ha) ,
269 DWF=[0](cms) , CN/C=[72] , IA=[2.5](mm) ,
270 N=[3.0] , TP=[5.95]hrs ,
271 Continuous simulation parameters:
272 IaREcper=[4](hrs) ,
273 SMIN=[-1](mm) , SMAX=[-1](mm) , SK=[0.010]/(mm) ,
274 InterEventTime=[12](hrs)
275 Baseflow simulation parameters:
276 BaseFlowOption=[1] ,
277 InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
278 VHydCond=[0.055](mm/hr) , END=-1
279 *%-----|-----
280 CONTINUOUS NASHYD NHYD=["SW_5"] , DT=[1]min , AREA=[224](ha) ,
281 DWF=[0](cms) , CN/C=[77] , IA=[2.5](mm) ,
282 N=[3.0] , TP=[0.75]hrs ,
283 Continuous simulation parameters:
284 IaREcper=[4](hrs) ,
285 SMIN=[-1](mm) , SMAX=[-1](mm) , SK=[0.010]/(mm) ,
286 InterEventTime=[12](hrs)
287 Baseflow simulation parameters:
288 BaseFlowOption=[1] ,
289 InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
290 VHydCond=[0.055](mm/hr) , END=-1
291 *%-----|-----
292 *#
293 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
294 *# of 1.20
295 *%-----|-----
296 CONTINUOUS NASHYD NHYD=["FL_CK"] , DT=[1]min , AREA=[4945](ha) ,
297 DWF=[0](cms) , CN/C=[74] , IA=[2.5](mm) ,
298 N=[3.0] , TP=[4.45]hrs ,
299 Continuous simulation parameters:
300 IaREcper=[4](hrs) ,
301 SMIN=[-1](mm) , SMAX=[-1](mm) , SK=[0.010]/(mm) ,
302 InterEventTime=[12](hrs)
303 Baseflow simulation parameters:
304 BaseFlowOption=[1] ,
305 InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
306 VHydCond=[0.055](mm/hr) , END=-1
307 *%-----|-----
308 CONTINUOUS NASHYD NHYD=["SW_5A2"] , DT=[1]min , AREA=[20](ha) ,
309 DWF=[0](cms) , CN/C=[81] , IA=[2.5](mm) ,
310 N=[3.0] , TP=[0.62]hrs ,
311 Continuous simulation parameters:
312 IaREcper=[4](hrs) ,
313 SMIN=[-1](mm) , SMAX=[-1](mm) , SK=[0.010]/(mm) ,
314 InterEventTime=[12](hrs)
315 Baseflow simulation parameters:
316 BaseFlowOption=[1] ,
317 InitGWResVol=[50](mm) , GWResK=[0.96](mm/day/mm)
318 VHydCond=[0.055](mm/hr) , END=-1
319 *%-----|-----
320 *#
321 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
322 *# of 1.61
323 *%-----|-----

```

```

324 CONTINUOUS NASHYD NHYD=["SW_5A1"], DT=[1]min, AREA=[1412](ha),
325 DWF=[0](cms), CN/C=[75], IA=[2.5](mm),
326 N=[3.0], TP=[8.00]hrs,
327 Continuous simulation parameters:
328 IaREcper=[4](hrs),
329 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
330 InterEventTime=[12](hrs)
331 Baseflow simulation parameters:
332 BaseFlowOption=[1] ,
333 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
334 VHydCond=[0.055](mm/hr), END=-1
335 *%-----|
336 CONTINUOUS NASHYD NHYD=["SW_4"], DT=[1]min, AREA=[585](ha),
337 DWF=[0](cms), CN/C=[81], IA=[2.5](mm),
338 N=[3.0], TP=[1.75]hrs,
339 Continuous simulation parameters:
340 IaREcper=[4](hrs),
341 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
342 InterEventTime=[12](hrs)
343 Baseflow simulation parameters:
344 BaseFlowOption=[1] ,
345 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
346 VHydCond=[0.055](mm/hr), END=-1
347 *%-----|
348 CONTINUOUS NASHYD NHYD=["LM_CK"], DT=[1]min, AREA=[1021](ha),
349 DWF=[0](cms), CN/C=[80], IA=[2.5](mm),
350 N=[3.0], TP=[2.46]hrs,
351 Continuous simulation parameters:
352 IaREcper=[4](hrs),
353 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
354 InterEventTime=[12](hrs)
355 Baseflow simulation parameters:
356 BaseFlowOption=[1] ,
357 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
358 VHydCond=[0.055](mm/hr), END=-1
359 *%-----|
360 CONTINUOUS NASHYD NHYD=["SW_2"], DT=[1]min, AREA=[177](ha),
361 DWF=[0](cms), CN/C=[77], IA=[2.5](mm),
362 N=[3.0], TP=[0.75]hrs,
363 Continuous simulation parameters:
364 IaREcper=[4](hrs),
365 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
366 InterEventTime=[12](hrs)
367 Baseflow simulation parameters:
368 BaseFlowOption=[1] ,
369 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
370 VHydCond=[0.055](mm/hr), END=-1
371 *%-----|
372 CONTINUOUS NASHYD NHYD=["SM_DR"], DT=[1]min, AREA=[1122](ha),
373 DWF=[0](cms), CN/C=[81], IA=[2.5](mm),
374 N=[3.0], TP=[3.25]hrs,
375 Continuous simulation parameters:
376 IaREcper=[4](hrs),
377 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
378 InterEventTime=[12](hrs)
379 Baseflow simulation parameters:
380 BaseFlowOption=[1] ,
381 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
382 VHydCond=[0.055](mm/hr), END=-1
383 *%-----|
384 CONTINUOUS NASHYD NHYD=["MO_DR"], DT=[1]min, AREA=[2737](ha),
385 DWF=[0](cms), CN/C=[76], IA=[2.5](mm),
386 N=[3.0], TP=[3.03]hrs,
387 Continuous simulation parameters:
388 IaREcper=[4](hrs),
389 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),

```

```

390 InterEventTime=[12](hrs)
391 Baseflow simulation parameters:
392 BaseFlowOption=[1] ,
393 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
394 VHydCond=[0.055](mm/hr), END=-1
395 *%-----|-----
396 * -JFSA 2020 replaced SW_1 with a detailed model from Stantec Report 2007
397 *CONTINUOUS NASHYD NHYD=["SW_1"], DT=[1]min, AREA=[3176](ha),
398 * DWF=[0](cms), CN/C=[78], IA=[2.5](mm),
399 * N=[3.0], TP=[3.56]hrs,
400 * Continuous simulation parameters:
401 * IaRECper=[4](hrs),
402 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
403 * InterEventTime=[12](hrs)
404 * Baseflow simulation parameters:
405 * BaseFlowOption=[1] ,
406 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
407 * VHydCond=[0.055](mm/hr), END=-1
408 *%-----|-----
409 *#
410 *# Routing hydrographs
411 *#
412 *# Starting with the addition of Jock River Headwater and Subwatershed 13
413 *#
414 ADD HYD NHYDsum=["S_N13"], NHYDs to add=["JR_HW"+"SW_13"]
415 *%-----|-----
416 *#
417 *# Sum of hydrographs from Node 13 routed to Node 13A
418 *# (Approximated cross-section - see cross-section 258)
419 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
420 *#
421 ROUTE CHANNEL NHYDout=["N13A"] ,NHYDin=["S_N13"],
422 RDT=[1](min),
423 CHLGTH=[9074](m), CHSLOPE=[0.0220](%),
424 FPSLOPE=[0.0220](%),
425 SECNUM=[1.0], NSEG=[1]
426 ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
427 ( DISTANCE (m), ELEVATION (m))=
428 [-40, 132.5]
429 [-30, 132]
430 [-25, 131.5]
431 [-13, 130]
432 [-8, 127.00]
433 [-7, 126.50]
434 [-6, 126]
435 [-5.5, 125.50]
436 [0, 123.75]
437 [4.5, 125.50]
438 [6, 126]
439 [7.5, 126.5]
440 [9, 127]
441 [10, 127.5]
442 [11.5, 128.0]
443 [15.5, 129.5]
444 *%-----|-----
445 *#
446 *# Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
447 *#
448 ADD HYD NHYDsum=["SN13A"], NHYDs to add=["N13A"+"JR_GWM"]
449 *%-----|-----
450 *#
451 *# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
452 *#
453 ROUTE RESERVOIR NHYDout=["RES_GM"] ,NHYDin=["SN13A"],
454 RDT=[1](min),
455 TABLE of ( OUTFLOW-STORAGE ) values

```



```

456 (cms) - (ha-m)
457 [ 0.0 , 0.0 ]
458 [1.991, 2.144 ]
459 [2.693, 39.826 ]
460 [3.509, 81.697 ]
461 [4.578, 318.774 ]
462 [5.647, 594.947 ]
463 [7.109, 910.219 ]
464 [8.616, 1264.589 ]
465 [10.371, 1658.057 ]
466 [12.402, 2090.622 ]
467 [22.056, 3462.487 ]
468 [ -1 , -1 ] (max twenty pts)
469

```

```

NHYDovf=[ " " ] ,

```

```

470 *%-----|-----
471 *#
472 SAVE HYD          NHYD=["RES_GM"], # OF PCYCLES=[-1], ICASEsh=[-1]
473                   HYD_FILENAME=["H_RESGM"]
474                   HYD_COMMENT=["Outflow from Res GM"]
475 *%-----|-----

```

```

476 *# Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
477 *# (Approximated cross-section - see cross-section 258)
478 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions

```

```

479 ROUTE CHANNEL   NHYDout=["N12"] ,NHYDin=["RES_GM"] ,
480                   RDT=[1](min),
481                   CHLGTH=[5926](m),  CHSLOPE=[0.0759](%),
482                                     FPSLOPE=[0.0759](%),
483                   SECNUM=[1.0],      NSEG=[1]
484                   ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
485                   ( DISTANCE (m), ELEVATION (m))=
486                       [-40, 132.5]
487                       [-30, 132]
488                       [-25, 131.5]
489                       [-13, 130]
490                       [-8, 127.00]
491                       [-7, 126.50]
492                       [-6, 126]
493                       [-5.5, 125.50]
494                       [0, 123.75]
495                       [4.5, 125.50]
496                       [6, 126]
497                       [7.5, 126.5]
498                       [9, 127]
499                       [10, 127.5]
500                       [11.5, 128.00]
501                       [15.5, 129.5]

```

```

502 *%-----|-----
503 *#
504 *# Addition of Subwatershed Jock River at Ashton to Node 12
505 *#

```

```

506 ADD HYD          NHYDsum=["S_N12"], NHYDs to add=["N12"+"JR_ASH"]
507 SAVE HYD        NHYD=["S_N12"], # OF PCYCLES=[-1], ICASEsh=[-1]
508                   HYD_FILENAME=["H_SN12"]
509                   HYD_COMMENT=["flow at S_N12 near Ashton"]

```

```

510 *%-----|-----
511 *#
512 *# Sum of hydrographs from Node 12 routed to Node 11
513 *# (Approximated cross-section - see cross-section 258)
514 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
515 *ROUTE CHANNEL   NHYDout=["N11"] ,NHYDin=["S_N12"] ,
516 *               RDT=[1](min),
517 *               CHLGTH=[972](m),  CHSLOPE=[0.0514](%),
518 *                                     FPSLOPE=[0.0514](%),
519 *               SECNUM=[1.0],      NSEG=[1]
520 *               ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
521 *               ( DISTANCE (m), ELEVATION (m))=

```

```

522 * [-40, 132.5]
523 * [-30, 132]
524 * [-25, 131.5]
525 * [-13, 130]
526 * [-8, 127.00]
527 * [-7, 126.50]
528 * [-6, 126]
529 * [-5.5, 125.50]
530 * [0, 123.75]
531 * [4.5, 125.50]
532 * [6, 126]
533 * [7.5, 126.5]
534 * [9, 127]
535 * [10, 127.5]
536 * [11.5, 128.00]
537 * [15.5, 129.5]
538 *%-----|-----
539 *#
540 *# Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
541 *#
542 ROUTE CHANNEL NHYDout=["Dum11"] ,NHYDin=["S_N12"] ,
543 RDT=[1](min),
544 CHLGTH=[972](m), CHSLOPE=[0.054](%),
545 FPSLOPE=[0.054](%),
546 SECNUM=[1.0], NSEG=[1]
547 ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
548 ( DISTANCE (m), ELEVATION (m))=
549 [-40, 132.5]
550 [-30, 132]
551 [-25, 131.5]
552 [-13, 130]
553 [-8, 127.00]
554 [-7, 126.50]
555 [-6, 126]
556 [-5.5, 125.50]
557 [0, 123.75]
558 [4.5, 125.50]
559 [6, 126]
560 [7.5, 126.5]
561 [9, 127]
562 [10, 127.5]
563 [11.5, 128.00]
564 [15.5, 129.5]
565 *%-----|-----
566 *#
567 *# Addition of Subwatershed 11 and No Name Creek to Node 11
568 *#
569 ADD HYD NHYDsum=["S_N11"], NHYDs to add=["Dum11"+"SW_11"+"NN_CK"]
570 *%-----|-----
571 *#
572 *# Sum of hydrographs from Node 11 routed to Node 10
573 *# Section 1
574 *#
575 ROUTE CHANNEL NHYDout=["N10"] ,NHYDin=["S_N11"] ,
576 RDT=[1](min),
577 CHLGTH=[14028](m), CHSLOPE=[0.1568](%),
578 FPSLOPE=[0.1568](%),
579 SECNUM=[1.0], NSEG=[5]
580 ( SEGROUGH, SEGDIST (m))=
581 [0.04,-52.82
582 0.1,-6.47
583 -0.05,6.47
584 0.1,45.36
585 0.04,423.88] NSEG times
586 ( DISTANCE (m), ELEVATION (m))=
587 [-226.24 ,112.50]

```

```

588 [-167.50 ,111.50]
589 [-106.81 ,111.00]
590 [-92.37 ,110.00]
591 [-52.82 ,109.00]
592 [-24.90, 109.00]
593 [-17.02, 108.50]
594 [-6.47, 108.00]
595 [6.47, 108.00]
596 [15.67, 108.50]
597 [18.95, 109.00]
598 [45.36, 109.50]
599 [120.79, 110.00]
600 [145.72, 111.00]
601 [181.56, 111.50]
602 [423.88, 112.50]
603 *%-----|-----|
604 *#
605 *# Addition of Subwatershed 10 to Node 10
606 *#
607 ADD HYD NHYDsum=["S_N10"], NHYDs to add=["N10"+"SW_10"]
608 *%-----|-----|
609 SAVE HYD NHYD=["S_N10"], # OF PCYCLES=[-1], ICASEsh=[-1]
610 HYD_FILENAME=["H_SN10"]
611 HYD_COMMENT=["flow at S_N10: N10 + SW_10"]
612 *%-----|-----|
613 *# Addition of Kings Creek to S_N10
614 *#
615 ADD HYD NHYDsum=["S_N10A"], NHYDs to add=["S_N10"+"KG_CK"]
616 *%-----|-----|
617 *#
618 *# Sum of hydrographs from Node 10 routed to Node 9
619 *# Section 2
620 *#
621 ROUTE CHANNEL NHYDout=["N9"] ,NHYDin=["S_N10A"] ,
622 RDT=[1](min),
623 CHLGTH=[3982](m), CHSLOPE=[0.0753](%),
624 FPSLOPE=[0.0753](%),
625 SECNUM=[1.0], NSEG=[4]
626 ( SEGROUGH, SEGDIST (m))=
627 [0.04,-30.27
628 0.05,-18.42
629 -0.05,18.42
630 0.04,131.58] NSEG times
631 ( DISTANCE (m), ELEVATION (m))=
632 [-446.74, 106.00]
633 [-415.68, 105.50]
634 [-285.40, 105.00]
635 [-173.77, 104.50]
636 [-144.95, 104.00]
637 [-111.18, 103.50]
638 [-94.06, 103.00]
639 [-71.02, 102.50]
640 [-30.27, 102.00]
641 [-19.33, 100.00]
642 [-18.42, 99.50]
643 [18.42, 99.50]
644 [20.77, 100.00]
645 [27.93, 101.00]
646 [52.29, 101.00]
647 [68.80, 101.50]
648 [79.66, 103.00]
649 [91.50, 103.50]
650 [131.58, 104.00]
651 *%-----|-----|
652 *#
653 *# Addition of Subwatershed 9 and Nichols Creek to Node 9

```

```

654  *#
655  ADD HYD           NHYDsum=["S_N9"], NHYDs to add=["N9"+"SW_9"+"NC_CK"]
656  *%-----|-----
657  *#
658  *# Sum of hydrographs from Node 9 routed to Node 8
659  *# Section 3
660  *#
661  ROUTE CHANNEL     NHYDout=["N8"] ,NHYDin=["S_N9"] ,
662                   RDT=[1](min),
663                   CHLGTH=[2269](m),  CHSLOPE=[0.0882](%),
664                                     FPSLOPE=[0.0882](%),
665                   SECNUM=[1.0],      NSEG=[3]
666                   ( SEGROUGH, SEGDIST (m))=
667                     [0.1,-17.99
668                     -0.045,17.31
669                     0.1,456.58] NSEG times
670                   ( DISTANCE (m), ELEVATION (m))=
671                     [-201.19,100.50]
672                     [-135.21, 100.00]
673                     [-94.83, 99.50]
674                     [-67.05, 99.00]
675                     [-17.99, 98.50]
676                     [-16.02, 98.00]
677                     [-13.95, 97.50]
678                     [13.95, 97.50]
679                     [15.64, 98.00]
680                     [17.31, 98.50]
681                     [162.02, 98.50]
682                     [172.89 ,99.00]
683                     [314.38, 99.00]
684                     [343.78, 99.50]
685                     [365.67, 100.00]
686                     [376.68, 100.00 ]
687                     [393.11, 99.50]
688                     [404.97, 99.50]
689                     [431.70, 100.00]
690                     [456.58, 100.50 ]
691  *%-----|-----
692  *#
693  *# Addition of Subwatershed 8 and Hobb's Drain to Node 8
694  *#
695  ADD HYD           NHYDsum=["S_N8"], NHYDs to add=["N8"+"SW_8"+"HB_DR"]
696  *%-----|-----
697  *#
698  *# Sum of hydrographs from Node 8 routed to Node 7
699  *# Section 4
700  *#
701  ROUTE CHANNEL     NHYDout=["N7"] ,NHYDin=["S_N8"],
702                   RDT=[1](min),
703                   CHLGTH=[3750](m),  CHSLOPE=[0.0533](%),
704                                     FPSLOPE=[0.0533](%),
705                   SECNUM=[1.0],      NSEG=[3]
706                   ( SEGROUGH, SEGDIST (m))=
707                     [0.12,-18.11
708                     -0.07,17.22
709                     0.12,590.05] NSEG times
710                   ( DISTANCE (m), ELEVATION (m))=
711                     [-433.21, 102.00]
712                     [-425.34, 101.50]
713                     [-377.56, 101.50]
714                     [-366.23, 101.00]
715                     [-202.60, 100.50]
716                     [-96.25, 99.50]
717                     [-68.36 99.00]
718                     [-18.11, 98.50]
719                     [-13.81, 97.50]

```

```

720             [13.81, 97.50]
721             [17.22, 98.50]
722             [161.95, 98.50]
723             [173.11, 99.00]
724             [314.05, 99.00]
725             [365.52, 100.00]
726             [404.70, 99.50]
727             [476.74, 100.50]
728             [502.31, 101.00]
729             [584.69, 101.00]
730             [585.79, 101.00]
731             [590.05, 102.00]
732 *%-----|-----
733 *#
734 *# Addition of Subwatershed 7 to Node 7
735 *#
736 ADD HYD           NHYDsum=["S_N7"], NHYDs to add=["N7"+"SW_7"]
737 *%-----|-----
738 SAVE HYD         NHYD=["S_N7"], # OF PCYCLES=[-1], ICASEsh=[-1]
739                   HYD_FILENAME=["H_SN7"]
740                   HYD_COMMENT=["flow at S_N7: N7 + SW_7"]
741 *%-----|-----
742 *# Insertion of a reservoir to simulate the effects of the Richmond Fen.
743 *# Storage area and volumes were estimated from available topo maps.
744 *# Release rate from fen was assumed to be controlled by the downstream
745 *# river cross-section for summer conditions. It is was assumed that for up to
746 *# 0.75 m of water, the main channel of the river provided the storage. Above
747 *# this depth, the wetland starts to signigicantly store water.
748 *#
749 ROUTE RESERVOIR  NHYDout=["RES_RF"] ,NHYDin=["S_N7"] ,
750                   RDT=[1](min),
751                   TABLE of ( OUTFLOW-STORAGE ) values
752                             (cms) - (ha-m)
753                   TABLE of ( OUTFLOW-STORAGE ) values
754                             (cms) - (ha-m)
755                             [ 0.0 , 0.0 ]
756                             [0.9051, 2.40]
757                             [2.907, 4.13]
758                             [9.744, 9.18]
759                             [20.304, 14.96]
760                             [34.167, 310.21]
761                             [74.993, 605.46]
762                             [104.876, 900.71]
763                             [140.56, 2892.00]
764                             [225.00, 3615.63]
765                             [ -1 , -1 ] (max twenty pts)
766                   NHYDovf=[" " ] ,
767 *%-----|-----
768 SAVE HYD         NHYD=["RES_RF"], # OF PCYCLES=[-1], ICASEsh=[-1]
769                   HYD_FILENAME=["H_ResRF"]
770                   HYD_COMMENT=["outflow of Richmond Fen"]
771 *%-----|-----
772 *#
773 *# Sum of hydrographs from Node 7 routed to Node 6
774 *# Section 5
775 *#
776 ROUTE CHANNEL   NHYDout=["N6"] ,NHYDin=["RES_RF"] ,
777                   RDT=[1](min),
778                   CHLGTH=[3056](m), CHSLOPE=[0.0818](%),
779                   FPSLOPE=[0.0818](%),
780                   SECNUM=[1.0], NSEG=[5]
781                   ( SEGROUGH, SEGDIST (m))=
782                   [0.025,-70.8
783                   0.1,-23.9
784                   -0.05,23.9
785                   0.06,39.8

```

```

786             0.05,96.3] NSEG times
787             ( DISTANCE (m), ELEVATION (m))=
788                 [-100.8, 97.00]
789                 [-70.8, 96.50]
790                 [-52.0, 96.00]
791                 [-35.1, 95.50]
792                 [-30.6, 95.00]
793                 [-23.9, 94.54]
794                 [23.9, 94.54]
795                 [39.8, 95.00]
796                 [50.4, 95.50]
797                 [93.5, 96.00]
798                 [94.9, 96.50]
799                 [96.3, 97.00]
800 *%-----|-----
801 *#
802 *# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
803 *#
804 ADD HYD             NHYDsum=["S_N6"], NHYDs to add=["N6"+"SW_6"+"VG_DR"]
805 *%-----|-----
806 *#
807 *# Sum of hydrographs from Node 6 routed to Node 5
808 *# Section 6
809 *#
810 ROUTE CHANNEL     NHYDout=["N5"] ,NHYDin=["S_N6"] ,
811                     RDT=[1](min),
812                     CHLGTH=[1852](m),   CHSLOPE=[0.0540](%),
813                                     FPSLOPE=[0.0540](%),
814                     SECNUM=[1.0],       NSEG=[3]
815                     ( SEGROUGH, SEGDIST (m))=
816                         [0.035,-131.59
817                         -0.045,48.96
818                         0.1,239.04] NSEG times
819                     ( DISTANCE (m), ELEVATION (m))=
820                         [-686.30, 94.50]
821                         [-675.70, 94.00]
822                         [-492.52, 93.00]
823                         [-467.28, 94.00]
824                         [-131.59, 94.00]
825                         [-92.79, 92.50]
826                         [-18.06, 91.00]
827                         [18.06, 91.00]
828                         [43.47, 92.50]
829                         [48.96, 94.00]
830                         [177.43, 94.00]
831                         [239.04,94.50]
832 *%-----|-----
833 *#
834 *# Addition of Subwatershed 5 and Flowing Creek to Node 5
835 *#
836 ADD HYD             NHYDsum=["S_N5"], NHYDs to add=["N5"+"SW_5"+"FL_CK"]
837 *%-----|-----
838 *#
839 *# Sum of hydrographs from Node 5 routed to Node 5A
840 *# Section 7
841 *#
842 ROUTE CHANNEL     NHYDout=["N5A"] ,NHYDin=["S_N5"] ,
843                     RDT=[1](min),
844                     CHLGTH=[556](m),   CHSLOPE=[0.0900](%),
845                                     FPSLOPE=[0.0900](%),
846                     SECNUM=[1.0],       NSEG=[4]
847                     ( SEGROUGH, SEGDIST (m))=
848                         [0.04,-41.5
849                         0.1,-14.0
850                         -0.045,14.0
851                         0.1,41.1] NSEG times

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```

852          ( DISTANCE (m), ELEVATION (m))=
853              [-275.8, 93.00]
854              [-248.6, 92.50]
855              [-237.0, 92.00]
856              [-219.3, 91.50]
857              [-202.1, 91.50]
858              [-186.0, 92.00]
859              [-129.2, 92.00]
860              [-117.6, 91.50]
861              [-100.6, 91.00]
862              [-41.5, 91.00]
863              [-20.0, 91.00]
864              [-14.0, 90.54]
865              [14.0, 90.54]
866              [15.3, 91.00]
867              [17.3, 91.50]
868              [38.4, 92.00]
869              [39.8, 92.50]
870              [41.1, 93.00]
871  *%-----|-----
872  *#
873  *# Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
874  *#
875  ADD HYD          NHYDsum=["S_N5A"], NHYDs to add=["N5A"+"SW_5A2"+"SW_5A1"]
876  *%-----|-----
877  *#
878  *# Sum of hydrographs from Node 5A routed to Node 4
879  *# Section 8
880  *#
881  ROUTE CHANNEL    NHYDout=["N4"] ,NHYDin=["S_N5A"] ,
882                  RDT=[1](min),
883                  CHLGTH=[4630](m),  CHSLOPE=[0.0432](%),
884                                          FPSLOPE=[0.0432](%),
885                  SECNUM=[1.0],      NSEG=[3]
886                  ( SEGROUGH, SEGDIST (m))=
887                      [0.05,-28.2
888                      -0.035,28.2
889                      0.05,173.1] NSEG times
890                  ( DISTANCE (m), ELEVATION (m))=
891                      [-38.9, 92.00]
892                      [-35.8, 91.50]
893                      [-33.3, 91.00]
894                      [-28.2, 90.50]
895                      [-15.0, 87.48]
896                      [-5.0, 88.34]
897                      [5.0, 86.20]
898                      [15.0, 88.55]
899                      [28.2, 90.50]
900                      [29.7, 91.00]
901                      [46.5, 91.00]
902                      [127.8, 91.00]
903                      [148.7, 91.50]
904                      [173.1, 92.00]
905  *%-----|-----
906  *#
907  *# Addition of Subwatershed 4 and Leamy Creek to Node 4
908  *#
909  ADD HYD          NHYDsum=["S_N4"], NHYDs to add=["N4"+"SW_4"+"LM_CK"]
910  SAVE HYD        NHYD=["S_N4"], # OF PCYCLES=[-1], ICASEsh=[1]
911                  HYD_COMMENT=["flow at S_N4"]
912  *%-----|-----
913  *#
914  *# Sum of hydrographs from Node 4 routed to Node 2
915  *# Section 9
916  *#
917  ROUTE CHANNEL    NHYDout=["N2"] ,NHYDin=["S_N4"] ,

```

```

918 RDT=[1](min),
919 CHLGTH=[1667](m), CHSLOPE=[0.0600](%),
920 FPSLOPE=[0.0600](%),
921 SECNUM=[1.0], NSEG=[4]
922 ( SEGROUGH, SEGDIST (m))=
923 [0.1,-28.0
924 -0.04,28.4
925 0.06,31.7
926 0.04,80.2] NSEG times
927 ( DISTANCE (m), ELEVATION (m))=
928 [-36.3, 92.00]
929 [-32.6, 91.50]
930 [-30.2, 91.00]
931 [-28.0, 90.45]
932 [-15.0, 87.48]
933 [-5.0, 88.34]
934 [5.0, 86.20]
935 [15.0, 88.55]
936 [28.0, 90.45]
937 [28.4, 90.50]
938 [30.4, 91.00]
939 [31.7, 91.50]
940 [80.2, 92.00]
941 *%-----|-----
942 *#
943 *# Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2
944 *#
945 ADD HYD NHYDsum=["S_N2"], NHYDs to add=["N2"+"SW_2"+"SM_DR"+"MO_DR"]
946 *%-----|-----
947 SAVE HYD NHYD=["S_N2"], # OF PCYCLES=[-1], ICASEsh=[-1]
948 HYD_FILENAME=["H_SN2"]
949 HYD_COMMENT=["flow at S_N2 Jock River Gauge at Moodie Dr."]
950 *%-----|-----
951 *#
952 *# Sum of hydrographs from Node 2 routed to Node 1
953 *# Section 10
954 *#
955 *#*****
956 *%READ HYD NHYD=["S_N2"],
957 *% HYD_FILENAME=["H-S_N2"]
958 *%-----|-----
959 *#
960 *# Hydrograph from Node 2 routed to Node 416
961 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 9025
962 *#
963 ROUTE CHANNEL NHYDout=["N_416"] ,NHYDin=["S_N2"] ,
964 RDT=[1](min),
965 CHLGTH=[2327](m), CHSLOPE=[0.0498](%),
966 FPSLOPE=[0.0498](%),
967 SECNUM=[1.0], NSEG=[3]
968 ( SEGROUGH, SEGDIST (m))=
969 [0.075,-23.96
970 -0.055,23.96
971 0.075,157.38] NSEG times
972 ( DISTANCE (m), ELEVATION (m))=
973 [-336.97,93.5]
974 [-318.85,93]
975 [-259,92.5]
976 [-133.18,92]
977 [-33.17,92]
978 [-27.21,92]
979 [-26.14,91.5]
980 [-24.99,91]
981 [-23.96,90.5]
982 [-14.33,88.26]
983 [-0.68,88.12]

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984 [14.33,88.26]
985 [23.96,90.5]
986 [32.12,91]
987 [43.74,91.5]
988 [57.09,92]
989 [73.53,92.5]
990 [108.27,93]
991 [125.88,93.5]
992 [144.81,94]
993 [157.38,94.5]
994 *%-----|-----|
995 *#*****|
996 *# Catchment SW-1a
997 *# - Portion of RVCA catchment SW_1 outside of Reach 1 subwatershed
998 *# - Undeveloped agricultural land
999 *#*****|
1000 CONTINUOUS NASHYD NHYD=["SW_1a"], DT=[1]min, AREA=[536.42](ha),
1001 DWF=[0](cms), CN/C=[72], IA=[4.67](mm),
1002 N=[3], TP=[2.79]hrs,
1003 Continuous simulation parameters:
1004 IaREcper=[4](hrs),
1005 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1006 InterEventTime=[12](hrs)
1007 Baseflow simulation parameters:
1008 BaseFlowOption=[1],
1009 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1010 VHydCond=[0.055](mm/hr), END=-1
1011 *%-----|-----|
1012 * -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
before station 7245 on Jock River
1013 CONTINUOUS STANDHYD NHYD=["S-1-Okeefe"], DT=[1](min), AREA=[44.93](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
1014 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
IAPER=[4.67](mm), SLPP=[2.0](%),
1015 LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
1016 LGI=[547.296](m), MNI=[0.013], SCI=[0](min),
1017 Continuous simulation parameters:
1018 IaREcper=[4](hrs), IaREcimp=[4](hrs),
1019 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1020 InterEventTime=[12](hrs), END=-1
1021 *%-----|-----|
1022 COMPUTE DUALHYD NHYDin=["S-1-Okeefe"], CINLET=[4.591](cms), NINLET=[1],
1023 MajNHYD=["S-1-OkMJ"]
1024 MinNHYD=["S-1-OkMN"]
1025 TMJSTO=[9999999](cu-m)
1026 *%-----|-----|
1027 ADD HYD NHYDsum=["S-1-OkS"], NHYDs to add=["S-1-OkMJ"+"S-1-OkMN"]
1028 *%-----|-----|
1029 ROUTE RESERVOIR NHYDout=["S-1-OkSR"],NHYDin=["S-1-OkS"],
1030 RDT=[1](min),
1031 TABLE of ( OUTFLOW-STORAGE ) values
1032 (cms) - (ha-m)
1033 [ 0.0 , 0.0 ]
1034 [ 0.5370, 1.7917 ]
1035 [ -1 , -1 ] (max twenty pts)
1036 NHYDovf=["S-1-OkSovf"]
1037 *%-----|-----|
1038 ADD HYD NHYDsum=["SN_416"], NHYDs to
add=["N_416"+"SW_1a"+"S-1-OkSR"+"S-1-OkSovf"]
1039 *%-----|-----|
1040 SAVE HYD NHYD=["SN_416"], # OF PCYCLES=[-1], ICASEsh=[1]
1041 HYD_COMMENT=["Total Flows at Highway 416 before Station 7245"]
1042 *%-----|-----|
1043 *#
1044 *# Hydrograph from Node 416 routed to Node at Okeefe drain

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1045  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 7245
1046  *#
1047  ROUTE CHANNEL      NHYDout=["N_OK"] ,NHYDin=["SN_416"] ,
1048                    RDT=[1](min),
1049                    CHLGTH=[497](m),  CHSLOPE=[0.3018](%),
1050                    FPSLOPE=[0.3018](%),
1051                    SECNUM=[1.0],      NSEG=[3]
1052                    ( SEGROUGH, SEGDIST (m))=
1053                    [0.075,-19.40
1054                    -0.055,19.40
1055                    0.075,377.02] NSEG times
1056                    ( DISTANCE (m), ELEVATION (m))=
1057                    [-1061.41, 92.50]
1058                    [-945.91, 92.00]
1059                    [-783.64, 91.50]
1060                    [-136.74, 91.00]
1061                    [-86.04, 91.00]
1062                    [-20.86, 91.00]
1063                    [-20.18, 90.50]
1064                    [-19.40, 90.00]
1065                    [-11.68, 86.89]
1066                    [0.00, 86.10]
1067                    [12.09, 86.81]
1068                    [19.40, 90.00]
1069                    [34.68, 90.50]
1070                    [60.56, 91.00]
1071                    [170.14, 91.00]
1072                    [175.05, 90.50]
1073                    [180.29, 90.00]
1074                    [193.41, 90.00]
1075                    [195.98, 90.50]
1076                    [377.02, 92.50]
1077  *%-----|-----|
1078  *#*****|
1079  *# Catchment OKEEFE
1080  *# - To O'Keefe drain (north of the Jock)
1081  *# - Developed with assumed 43% imp.
1082  *# - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area
1083  *# - 2020-11-20 Okeefe detailed model was added as per the NOVATECH SWMHYMO model
1084  *# - Citi-Gate 2014).
1084  *%-----|-----|
1085  *POST DEVELOPMENT CONDITIONS
1086  *%-----|-----|
1087  *#*****|
1088  CONTINUOUS NASHYD  NHYD=["O-1"], DT=[1]min, AREA=[63.72](ha),
1089                    DWF=[0](cms), CN/C=[61], IA=[6.2](mm), N=[3], TP=[.9]hrs,
1090                    Continuous simulation parameters:
1091                    IaREcper=[4](hrs),
1092                    SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
1093                    InterEventTime=[12](hrs)
1094                    Baseflow simulation parameters:
1095                    BaseFlowOption=[1] ,
1096                    InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1097                    VHydCond=[0.055](mm/hr),  END=-1
1098  *%-----|-----|
1099  *ROUTE FLOW THROUGH AREA 0-2
1100  ROUTE CHANNEL      NHYDout=["O-1R"], NHYDin=["O-1"], RDT=[1](min),
1101                    CHLGTH=[960](m), CHSLOPE=[0.63](%), FPSLOPE=[0.63](%),
1102                    SECNUM=[1], NSEG=[3]
1103                    ( SEGROUGH, SEGDIST (m))=[0.06,4 -.043,6 0.06,10] NSEG times
1104                    ( DISTANCE (m), ELEVATION (m))=[0.00, 2.0]
1105                    [0.0, 2.0]
1106                    [4.0, 0.0]
1107                    [6.0, 0.0]

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1108         [10.0, 2.0]
1109 *%-----|-----|
1110 CONTINUOUS NASHYD NHYD=["O-2"], DT=[1]min, AREA=[28.61](ha),
1111 DWF=[0](cms), CN/C=[57], IA=[5.2](mm), N=[3], TP=[1.1]hrs,
1112 Continuous simulation parameters:
1113 IaREcper=[4](hrs),
1114 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1115 InterEventTime=[12](hrs)
1116 Baseflow simulation parameters:
1117 BaseFlowOption=[1] ,
1118 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1119 VHydCond=[0.055](mm/hr), END=-1
1120 *%-----|-----|
1121 CONTINUOUS NASHYD NHYD=["O-4"], DT=[1]min, AREA=[46.94](ha),
1122 DWF=[0](cms), CN/C=[49], IA=[9.2](mm), N=[3], TP=[0.9]hrs,
1123 Continuous simulation parameters:
1124 IaREcper=[4](hrs),
1125 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1126 InterEventTime=[12](hrs)
1127 Baseflow simulation parameters:
1128 BaseFlowOption=[1] ,
1129 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1130 VHydCond=[0.055](mm/hr), END=-1
1131 *%-----|-----|
1132 *TOTAL EXTERNAL FLOW NORTH OF O'KEEFE CT. CROSSING
1133 ADD HYD NHYDsum=["OKF-N"], NHYDs to add=["O-1R"+"O-2"+"O-4"]
1134 *%-----|-----|
1135 *ROUTE FLOW THROUGH AREA O-6
1136 ROUTE CHANNEL ROUTE CHANNEL NHYDout=["OKF-NR"], NHYDin=["OKF-N"], RDT=[1](min),
1137 CHLGTH=[210](m), CHSLOPE=[.81](%), FPSLOPE=[.81](%),
1138 SECNUM=[1], NSEG=[3]
1139 ( SEGRROUGH, SEGDIST (m))=[0.043,22.43 -0.043,25.07
1140 0.043,45.54] NSEG times
1141 ( DISTANCE (m), ELEVATION (m))=[0.00, 3.73]
1142 (14.62, 1.56)
1143 (18.41, 1.44)
1144 (22.43, 0.00)
1145 (25.07, 0.70)
1146 (29.10, 1.79)
1147 (33.73, 2.71)
1148 (45.54, 3.58)
1149 *%-----|-----|
1150 CONTINUOUS NASHYD NHYD=["O-6"], DT=[1]min, AREA=[16.46](ha),
1151 DWF=[0](cms), CN/C=[43], IA=[9.2](mm), N=[3], TP=[0.7]hrs,
1152 Continuous simulation parameters:
1153 IaREcper=[4](hrs),
1154 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1155 InterEventTime=[12](hrs)
1156 Baseflow simulation parameters:
1157 BaseFlowOption=[1] ,
1158 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1159 VHydCond=[0.055](mm/hr), END=-1
1160 *%-----|-----|
1161 CONTINUOUS STANDHYD NHYD=["O-3"], DT=[1](min), AREA=[39.67](ha), XIMP=[0.15],
1162 TIMP=[0.30], DWF=[0](cms),
1163 LOSS=[2], SCS curve number CN=[50], Pervious surfaces:
1164 IAper=[4.67](mm), SLPP=[0.32](%),
1165 LGP=[440](m), MNP=[0.035], SCP=[0](min), Impervious surfaces:
1166 IAimp=[1.57](mm), SLPI=[0.32](%),
1167 LGI=[1880](m), MNI=[0.013], SCI=[0](min),
1168 Continuous simulation parameters:
1169 IaREcper=[4](hrs), IaREcimp=[4](hrs),
1170 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1171 InterEventTime=[12](hrs), END=-1
1172 *%-----|-----|
1173 CONTINUOUS STANDHYD NHYD=["O-5"], DT=[1](min), AREA=[60.63](ha), XIMP=[0.13],

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TIMP=[0.26], DWF=[0](cms),
1171      LOSS=[2], SCS curve number CN=[61],
1172      Pervious surfaces: IAper=[4.67](mm), SLPP=[1.38](%),
1173      LGP=[550](m), MNP=[0.035], SCP=[0](min), Impervious surfaces:
      IAimp=[1.57](mm), SLPI=[1.38](%),
1174      LGI=[1450](m), MNI=[0.013], SCI=[0](min),
1175      Continuous simulation parameters:
1176      IaRECper=[4](hrs), IaRECimp=[4](hrs),
1177      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1178      InterEventTime=[12](hrs), END=-1
1179  *%-----|-----|
1180  *TOTAL EXTERNAL FLOWS WEST OF THE SITE AND NORTH OF O'KEEFE CRT
1181  *%-----|-----|
1182  ADD HYD      NHYDsum=["PT1"], NHYDs to add=["OKF-NR"+"O-3"+"O-5"+"O-6"]
1183  *%-----|-----|
1184  CONTINUOUS NASHYD  NHYD=["O-7"], DT=[1]min, AREA=[5.28](ha),
1185      DWF=[0](cms), CN/C=[54], IA=[7.5](mm), N=[3], TP=[0.6]hrs,
1186      Continuous simulation parameters:
1187      IaRECper=[4](hrs),
1188      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1189      InterEventTime=[12](hrs)
1190      Baseflow simulation parameters:
1191      BaseFlowOption=[1] ,
1192      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1193      VHydCond=[0.055](mm/hr), END=-1
1194  *%-----|-----|
1195  *ANALYSIS POINT 1 - TOTAL FLOW NORTH OF FALLOWFIELD DR. AND O'KEEFE CRT.
1196  ADD HYD      NHYDsum=["FF"], NHYDs to add=["PT1"+"O-7"]
1197  *%-----|-----|
1198  *ROUTE FLOW through O'Keefe Drain 1
1199  ROUTE CHANNEL  NHYDout=["DRAIN1"], NHYDin=["FF"], RDT=[1](min),
1200      CHLGTH=[302]{m}, CHSLOPE=[1.00](%), FPSLOPE=[1.00](%),
1201      SECNUM=[1], NSEG=[3]
1202      ( SEGROUGH, SEGDIST (m))=[0.07,13.45 -0.043,16.55 0.07,30.00] NSEG
      times
1203      ( DISTANCE (m), ELEVATION (m))=[0.00, 1.70]
1204      (3.45, 0.60)
1205      (13.45, 0.50)
1206      (14.45, 0.00)
1207      (15.55, 0.00)
1208      (16.55, 0.50)
1209      (26.55, 0.60)
1210      (30.00, 1.70)
1211  *%-----|-----|
1212  CONTINUOUS NASHYD  NHYD=["D1"], DT=[1]min, AREA=[1.17](ha),
1213      DWF=[0](cms), CN/C=[84], IA=[9.0](mm), N=[3], TP=[0.28]hrs,
1214      Continuous simulation parameters:
1215      IaRECper=[4](hrs),
1216      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1217      InterEventTime=[12](hrs)
1218      Baseflow simulation parameters:
1219      BaseFlowOption=[1] ,
1220      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1221      VHydCond=[0.055](mm/hr), END=-1
1222  *%-----|-----|
1223  CONTINUOUS STANDHYD  NHYD=["A1"], DT=[1]min, AREA=[2.50](ha), XIMP=[0.68], TIMP=[0.85],
      DWF=[0](cms), LOSS=[1]:
1224      Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
      F=[0.00](mm),
1225      Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
      MNP=[0.250], SCP=[0](min),
1226      Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
      LGI=[223.607](m), MNI=[0.013], SCI=[0](min),
1227      Continuous simulation parameters:
1228      IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
      END=-1

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1229 *%-----|-----|
1230 ROUTE RESERVOIR NHYDout=["A1-STR"], NHYDin=["A1"], RDT=[1](min),
1231 TABLE of ( OUTFLOW-STORAGE ) values
1232 (cms) - (ha-m)
1233 [ 0.000 , 0.000 ]
1234 [ 0.035 , 0.038 ]
1235 [ 0.072 , 0.051 ]
1236 [ 0.100 , 0.059 ]
1237 [ 0.125 , 0.070 ]
1238 [ 0.160 , 0.074 ]
1239 [ 0.185 , 0.081 ]
1240 [ -1 , -1 ] (max twenty pts)
1241 NHYDovf=["A1-OVF"]
1242 *%-----|-----|
1243 CONTINUOUS STANDHYD NHYD=["ST-2"], DT=[1]min, AREA=[0.59](ha), XIMP=[0.46],
TIMP=[0.57], DWF=[0](cms), LOSS=[1]:
1244 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1245 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1246 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[108.628](m), MNI=[0.013], SCI=[0](min),
1247 Continuous simulation parameters:
1248 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1249 *%-----|-----|
1250 ROUTE RESERVOIR NHYDout=["ST2STR"], NHYDin=["ST-2"], RDT=[1](min),
1251 TABLE of ( OUTFLOW-STORAGE ) values
1252 (cms) - (ha-m)
1253 [ 0.000 , 0.0000 ]
1254 [ 0.052 , 0.0010 ]
1255 [ 0.053 , 0.0080 ]
1256 [ -1 , -1 ] (max twenty pts)
1257 NHYDovf=["ST2OVF"]
1258 *%-----|-----|
1259 *%-----|-----|
1260 *TOTAL FLOW NORTH OF STRANDHERD DR. (EAST BRANCH) CROSSING
1261 *%-----|-----|
1262 CONTINUOUS NASHYD NHYD=["O-8"], DT=[1]min, AREA=[60.55](ha),
1263 DWF=[0](cms), CN/C=[69], IA=[4.0](mm), N=[3], TP=[1.0]hrs,
1264 Continuous simulation parameters:
1265 IaREcper=[4](hrs),
1266 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1267 InterEventTime=[12](hrs)
1268 Baseflow simulation parameters:
1269 BaseFlowOption=[1] ,
1270 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1271 VHydCond=[0.055](mm/hr), END=-1
1272 *%-----|-----|
1273 ROUTE PIPE PTYPE=[2]rect, NHYDout=["O8PIPE"], RNUMBER=[1], PWIDTH=[1800](mm),
PHEIGHT=[1200](mm), PLNGTH=[335.1](m),
1274 PROUGH=[0.013], PSLOPE=[0.001](m/m), NHYDin=["O-8"], RDT=[1](min)
1275 *%-----|-----|
1276 *%-----|-----|
1277 ADD HYD NHYDsum=["ST2-IN"], NHYDs to
add=["DRAIN1"+"D1"+"A1-STR"+"A1-OVF"+"ST2STR"+"ST2OVF"+"O8PIPE"]
1278 *%-----|-----|
1279 CONTINUOUS STANDHYD NHYD=["A7"], DT=[1]min, AREA=[3.51](ha), XIMP=[0.68], TIMP=[0.85],
DWF=[0](cms), LOSS=[1]:
1280 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1281 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1282 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[264.953](m), MNI=[0.013], SCI=[0](min),
1283 Continuous simulation parameters:

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1284 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
      END=-1
1285 *%-----|-----|
1286 ROUTE RESERVOIR NHYDout=["A7-STR"], NHYDin=["A7"], RDT=[1](min),
1287                 TABLE of ( OUTFLOW-STORAGE ) values
1288                 (cms) - (ha-m)
1289                 [ 0.000 , 0.000 ]
1290                 [ 0.049 , 0.054 ]
1291                 [ 0.102 , 0.072 ]
1292                 [ 0.140 , 0.082 ]
1293                 [ 0.175 , 0.099 ]
1294                 [ 0.225 , 0.105 ]
1295                 [ 0.260 , 0.114 ]
1296                 [ -1 , -1 ] (max twenty pts)
1297                 NHYDovf=["A7-OVF"]
1298 *%-----|-----|
1299 CONTINUOUS STANDHYD NHYD=["ST-3"], DT=[1]min, AREA=[0.71](ha), XIMP=[0.46],
1300 TIMP=[0.57], DWF=[0](cms), LOSS=[1]:
1301 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1302 F=[0.00](mm),
1303 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1304 MNP=[0.250], SCP=[0](min),
1305 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
1306 LGI=[119.164](m), MNI=[0.013], SCI=[0](min),
1307 Continuous simulation parameters:
1308 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
1309 END=-1
1310 *%-----|-----|
1311 ROUTE RESERVOIR NHYDout=["ST3STR"], NHYDin=["ST-3"], RDT=[1](min),
1312                 TABLE of ( OUTFLOW-STORAGE ) values
1313                 (cms) - (ha-m)
1314                 [ 0.000 , 0.0000 ]
1315                 [ 0.063 , 0.0010 ]
1316                 [ 0.064 , 0.0094 ]
1317                 [ -1 , -1 ] (max twenty pts)
1318                 NHYDovf=["ST3OVF"]
1319 *%-----|-----|
1320 *ANALYSIS POINT 2 - TOTAL FLOW AT OUTLET OF STREET 2/3 INTERSECTION
1321 *%-----|-----|
1322 ADD HYD NHYDsum=["PT2ST3"], NHYDs to
1323 add=["ST2-IN"+"A7-STR"+"A7-OVF"+"ST3STR"+"ST3OVF"]
1324 *%-----|-----|
1325 *ROUTE FLOW through O'Keefe Drain 2
1326 ROUTE CHANNEL NHYDout=["DRAIN2"], NHYDin=["PT2ST3"], RDT=[1](min),
1327 CHLGTH=[592]{m}, CHSLOPE=[.23](%), FPSLOPE=[.23](%),
1328 SECNUM=[1], NSEG=[3]
1329 ( SEGROUGH, SEGDIST (m))=[0.07,12.60 -0.043,17.40 0.07,30.00] NSEG
1330 times
1331 ( DISTANCE (m), ELEVATION (m))=[0.00, 1.70]
1332 (2.60, 0.95)
1333 (12.60, 0.75)
1334 (14.10, 0.00)
1335 (15.90, 0.00)
1336 (17.40, 0.75)
1337 (27.40, 0.95)
1338 (30.00, 1.70)
1339 *%-----|-----|
1340 CONTINUOUS NASHYD NHYD=["D2"], DT=[1]min, AREA=[2.28](ha), DWF=[0](cms), CN/C=[84],
1341 IA=[9.0](mm),
1342 N=[3], TP=[0.99]hrs,
1343 Continuous simulation parameters:
1344 IaREcper=[4](hrs),
1345 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1346 InterEventTime=[12](hrs)
1347 Baseflow simulation parameters:
1348 BaseFlowOption=[1] ,

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1341          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1342          VHydCond=[0.055](mm/hr),   END=-1
1343  *%-----|-----|
1344  CONTINUOUS STANDHYD NHYD=["A17"], DT=[1]min, AREA=[12.04](ha), XIMP=[0.68],
TIMP=[0.85], DWF=[0](cms), LOSS=[1]:
1345          Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1346          Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1347          Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[490.714](m), MNI=[0.013], SCI=[0](min),
1348          Continuous simulation parameters:
1349          IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1350  *%-----|-----|
1351  ROUTE RESERVOIR NHYDout=["A17STR"], NHYDin=["A17"], RDT=[1](min),
1352          TABLE of ( OUTFLOW-STORAGE ) values
1353          (cms) - (ha-m)
1354          [ 0.000 , 0.000 ]
1355          [ 0.169 , 0.185 ]
1356          [ 0.349 , 0.248 ]
1357          [ 0.482 , 0.283 ]
1358          [ 0.602 , 0.338 ]
1359          [ 0.771 , 0.359 ]
1360          [ 0.891 , 0.391 ]
1361          [ -1 , -1 ] (max twenty pts)
1362          NHYDovf=["A17OVF"]
1363  *%-----|-----|
1364  CONTINUOUS STANDHYD NHYD=["ST-4"], DT=[1]min, AREA=[0.35](ha), XIMP=[0.46],
TIMP=[0.57], DWF=[0](cms), LOSS=[1]:
1365          Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1366          Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1367          Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[83.666](m),
MNI=[0.013], SCI=[0](min),
1368          Continuous simulation parameters:
1369          IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1370  *%-----|-----|
1371  ROUTE RESERVOIR NHYDout=["ST4STR"], NHYDin=["ST-4"], RDT=[1](min),
1372          TABLE of ( OUTFLOW-STORAGE ) values
1373          (cms) - (ha-m)
1374          [ 0.000 , 0.0000 ]
1375          [ 0.031 , 0.0010 ]
1376          [ 0.032 , 0.0050 ]
1377          [ -1 , -1 ] (max twenty pts)
1378          NHYDovf=["ST4OVF"]
1379  *%-----|-----|
1380  CONTINUOUS STANDHYD NHYD=["A18"], DT=[1]min, AREA=[5.30](ha), XIMP=[0.68], TIMP=[0.85],
DWF=[0](cms), LOSS=[1]:
1381          Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1382          Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1383          Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[325.576](m), MNI=[0.013], SCI=[0](min),
1384          Continuous simulation parameters:
1385          IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1386  *%-----|-----|
1387  ROUTE RESERVOIR NHYDout=["A18STR"], NHYDin=["A18"], RDT=[1](min),
1388          TABLE of ( OUTFLOW-STORAGE ) values
1389          (cms) - (ha-m)
1390          [ 0.000 , 0.000 ]
1391          [ 0.074 , 0.082 ]

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1392         [ 0.154 , 0.109 ]
1393         [ 0.212 , 0.125 ]
1394         [ 0.265 , 0.149 ]
1395         [ 0.339 , 0.158 ]
1396         [ 0.392 , 0.172 ]
1397         [ -1 , -1 ] (max twenty pts)
1398         NHYDovf=["A18OVF"]
1399 *%-----|-----|
1400 *ANALYSIS POINT 3 - TOTAL FLOW AT OUTLET OF STREET 4
1401 *%-----|-----|
1402 ADD HYD          NHYDsum=["PT3ST4"], NHYDs to
add=["DRAIN2"+"D2"+"A17STR"+"A17OVF"+"ST4STR"+"ST4OVF"+"A18STR"+"A18OVF"]
1403 *%-----|-----|
1404 *ROUTE FLOW through O'Keefe Drain 3
1405 ROUTE CHANNEL   NHYDout=["DRAIN3"], NHYDin=["PT3ST4"], RDT=[1](min),
1406                CHLGTH=[525]{m}, CHSLOPE=[.23](%), FPSLOPE=[.23](%),
1407                SECNUM=[1], NSEG=[3]
1408                ( SEGROUGH, SEGDIST (m))=[0.07,12.50 -0.043,17.50 0.07,30.00] NSEG
1409                times
1410                ( DISTANCE (m), ELEVATION (m))=[0.00, 1.70]
1411                (2.50, 1.00)
1412                (12.50, 0.80)
1413                (14.10, 0.00)
1414                (15.90, 0.00)
1415                (17.50, 0.80)
1416                (27.50, 1.00)
1417                (30.00, 1.70)
1418 *%-----|-----|
1419 CONTINUOUS NASHYD NHYD=["D3"], DT=[1]min, AREA=[2.51](ha),
1420                DWF=[0](cms), CN/C=[86], IA=[8.7](mm), N=[3], TP=[0.73]hrs,
1421                Continuous simulation parameters:
1422                IaREcper=[4](hrs),
1423                SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1424                InterEventTime=[12](hrs)
1425                Baseflow simulation parameters:
1426                BaseFlowOption=[1] ,
1427                InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1428                VHydCond=[0.055](mm/hr), END=-1
1429 *%-----|-----|
1430 CONTINUOUS STANDHYD NHYD=["C1"], DT=[1]min, AREA=[3.41](ha), XIMP=[0.68], TIMP=[0.85],
1431                DWF=[0](cms), LOSS=[1]:
1432                Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1433                F=[0.00](mm),
1434                Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1435                MNP=[0.250], SCP=[0](min),
1436                Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
1437                LGI=[261.151](m), MNI=[0.013], SCI=[0](min),
1438                Continuous simulation parameters:
1439                IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
1440                END=-1
1441 *%-----|-----|
1442 ROUTE RESERVOIR  NHYDout=["C1-STR"], NHYDin=["C1"], RDT=[1](min),
1443                TABLE of ( OUTFLOW-STORAGE ) values
1444                (cms) - (ha-m)
1445                [ 0.000 , 0.000 ]
1446                [ 0.048 , 0.052 ]
1447                [ 0.099 , 0.070 ]
1448                [ 0.136 , 0.080 ]
1449                [ 0.170 , 0.096 ]
1450                [ 0.218 , 0.102 ]
1451                [ 0.252 , 0.111 ]
1452                [ -1 , -1 ] (max twenty pts)
1453                NHYDovf=["C1-OVF"]
1454 *%-----|-----|
1455 CONTINUOUS STANDHYD NHYD=["ST-5"], DT=[1]min, AREA=[0.45](ha), XIMP=[0.46],
1456                TIMP=[0.57], DWF=[0](cms), LOSS=[1]:

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1450 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
      F=[0.00](mm),
1451 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
      MNP=[0.250], SCP=[0](min),
1452 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[94.868](m),
      MNI=[0.013], SCI=[0](min),
1453 Continuous simulation parameters:
1454 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
      END=-1
1455 *%-----|-----|
1456 ROUTE RESERVOIR NHYDout=["ST5STR"], NHYDin=["ST-5"], RDT=[1](min),
1457 TABLE of ( OUTFLOW-STORAGE ) values
1458 (cms) - (ha-m)
1459 [ 0.000 , 0.0000 ]
1460 [ 0.040 , 0.0010 ]
1461 [ 0.041 , 0.0062 ]
1462 [ -1 , -1 ] (max twenty pts)
1463 NHYDovf=["ST5OVF"]
1464 *%-----|-----|
1465 ADD HYD NHYDsum=["ST5-E"], NHYDs to
add=["DRAIN3"+"D3"+"C1-STR"+"C1-OVF"+"ST5STR"+"ST5OVF"]
1466 *%-----|-----|
1467 CONTINUOUS STANDHYD NHYD=["STRAND"], DT=[1](min), AREA=[7.59](ha),
1468 XIMP=[0.64], TIMP=[0.85], DWF=[0](cms), LOSS=[1]:
1469 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
      F=[0.00](mm),
1470 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[40](m),
      MNP=[0.250], SCP=[0](min),
1471 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[1230](m),
      MNI=[0.013], SCI=[0](min),
1472 Continuous simulation parameters:
1473 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
      END=-1
1474 *%-----|-----|
1475 ROUTE RESERVOIR NHYDout=["S-POND"], NHYDin=["STRAND"], RDT=[1](min),
1476 TABLE of ( OUTFLOW-STORAGE ) values
1477 (cms) - (ha-m)
1478 [ 0.000 , 0.000 ]
1479 [ 0.033 , 0.188 ]
1480 [ 0.057 , 0.253 ]
1481 [ 0.104 , 0.287 ]
1482 [ 0.160 , 0.336 ]
1483 [ 0.340 , 0.346 ]
1484 [ 0.471 , 0.360 ]
1485 [ 0.824 , 0.390 ]
1486 [ -1 , -1 ] (max twenty pts)
1487 NHYDovf=["S-OVF"]
1488 *%-----|-----|
1489 ADD HYD NHYDsum=["SSAOUT"], NHYDs to add=["ST5-E"+"S-POND"+"S-OVF"]
1490 *%-----|-----|
1491 SAVE HYD NHYD=["SSAOUT"], # OF PCYCLES=[5], ICASEsh=[1]
1492 HYD_COMMENT=["SSAOUT"]
1493 *%-----|-----|
1494 CONTINUOUS STANDHYD NHYD=["Area-A"], DT=[1]min, AREA=[66.75](ha), XIMP=[0.64],
1495 TIMP=[0.80], DWF=[0](cms), LOSS=[1]:
1496 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
      F=[0.00](mm),
1497 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
      MNP=[0.250], SCP=[0](min),
1498 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
      LGI=[1155.422](m), MNI=[0.013], SCI=[0](min),
1499 Continuous simulation parameters:
IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1500 *%-----|-----|
1501 SAVE HYD NHYD=["Area-A"], # OF PCYCLES=[1], ICASEsh=[1]

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1502 HYD_COMMENT=["SMWF-A Inflow"]
1503 *%-----|-----|
1504 ROUTE RESERVOIR NHYDout=["SMWF-A"], NHYDin=["Area-A"], RDT=[1](min),
1505 TABLE of ( OUTFLOW-STORAGE ) values
1506 (cms) - (ha-m)
1507 [ 0.000 , 0.000 ]
1508 [ 0.103 , 1.077 ]
1509 [ 0.128 , 1.749 ]
1510 [ 0.382 , 2.282 ]
1511 [ 0.703 , 2.582 ]
1512 [ 1.256 , 2.978 ]
1513 [ 1.567 , 3.202 ]
1514 [ 1.955 , 3.493 ]
1515 [ 2.100 , 3.600 ]
1516 [ -1 , -1 ] (max twenty pts)
1517 NHYDovf=["SWMAOV"]
1518 *%-----|-----|
1519 SAVE HYD NHYD=["SMWF-A"], # OF PCYCLES=[1], ICASEsh=[1]
1520 HYD_COMMENT=["SMWF-A Outflow"]
1521 *%-----|-----|
1522 *ANALYSIS POINT 4 - TOTAL FLOW AT OUTLET OF STREET 5
1523 *%-----|-----|
1524 ADD HYD NHYDsum=["PT4ST5"], NHYDs to add=["SSAOUT"+"SMWF-A"+"SWMAOV"]
1525 *%-----|-----|
1526 CONTINUOUS STANDHYD NHYD=["C6"], DT=[1]min, AREA=[1.87](ha), XIMP=[0.68], TIMP=[0.85],
DWF=[0](cms), LOSS=[1]:
1527 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1528 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1529 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[193.391](m), MNI=[0.013], SCI=[0](min),
1530 Continuous simulation parameters:
1531 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1532 *%-----|-----|
1533 ROUTE RESERVOIR NHYDout=["C6-STR"], NHYDin=["C6"], RDT=[1](min),
1534 TABLE of ( OUTFLOW-STORAGE ) values
1535 (cms) - (ha-m)
1536 [ 0.000 , 0.000 ]
1537 [ 0.026 , 0.029 ]
1538 [ 0.054 , 0.038 ]
1539 [ 0.075 , 0.044 ]
1540 [ 0.093 , 0.052 ]
1541 [ 0.120 , 0.056 ]
1542 [ 0.138 , 0.061 ]
1543 [ -1 , -1 ] (max twenty pts)
1544 NHYDovf=["C6-OVF"]
1545 *%-----|-----|
1546 CONTINUOUS STANDHYD NHYD=["C7"], DT=[1]min, AREA=[1.62](ha), XIMP=[0.68], TIMP=[0.85],
DWF=[0](cms), LOSS=[1]:
1547 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1548 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1549 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[180.000](m), MNI=[0.013], SCI=[0](min),
1550 Continuous simulation parameters:
1551 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1552 *%-----|-----|
1553 ROUTE RESERVOIR NHYDout=["C7-STR"], NHYDin=["C7"], RDT=[1](min),
1554 TABLE of ( OUTFLOW-STORAGE ) values
1555 (cms) - (ha-m)
1556 [ 0.000 , 0.000 ]
1557 [ 0.023 , 0.025 ]

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1558         [ 0.047 , 0.033 ]
1559         [ 0.065 , 0.038 ]
1560         [ 0.081 , 0.045 ]
1561         [ 0.104 , 0.048 ]
1562         [ 0.120 , 0.053 ]
1563         [ -1 , -1 ] (max twenty pts)
1564         NHYDovf=["C7-OVF"]
1565 *%-----|-----|
1566 CONTINUOUS STANDHYD NHYD=["ST-6"], DT=[1]min, AREA=[0.41](ha),XIMP=[0.46], TIMP=[0.57],
DWF=[0](cms), LOSS=[1]:
1567 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1568 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1569 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[90.554](m),
MNI=[0.013], SCI=[0](min),
1570 Continuous simulation parameters:
1571 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1572 *%-----|-----|
1573 ROUTE RESERVOIR NHYDout=["ST6STR"], NHYDin=["ST-6"], RDT=[1](min),
1574 TABLE of ( OUTFLOW-STORAGE ) values
1575 (cms) - (ha-m)
1576 [ 0.000 , 0.0000 ]
1577 [ 0.036 , 0.0010 ]
1578 [ 0.037 , 0.0058 ]
1579 [ -1 , -1 ] (max twenty pts)
1580 NHYDovf=["ST6OVF"]
1581 *%-----|-----|
1582 *ANALYSIS POINT 5 - TOTAL FLOW AT OUTLET OF STREET 6
1583 *%-----|-----|
1584 ADD HYD NHYDsum=["PT5ST6"], NHYDs to
add=["PT4ST5"+"C6-STR"+"C6-OVF"+"C7-STR"+"C7-OVF"+"ST6STR"+"ST6OVF"]
1585 *%-----|-----|
1586 *ROUTE FLOW through O'Keefe Drain 4
1587 ROUTE CHANNEL NHYDout=["DRAIN4"], NHYDin=["PT5ST6"], RDT=[1](min),
1588 CHLGTH=[324]{m}, CHSLOPE=[.10](%), FPSLOPE=[.10](%),
1589 SECNUM=[1], NSEG=[3]
1590 ( SEGROUGH, SEGDIST (m))=[0.07,12.00 -0.043,18.00 0.07,30.00] NSEG
times
1591 ( DISTANCE (m), ELEVATION (m))=[0.00, 2.00]
1592 (2.00, 1.20)
1593 (12.00, 1.00)
1594 (14.00, 0.00)
1595 (16.00, 0.00)
1596 (18.00, 1.00)
1597 (28.00, 1.20)
1598 (30.00, 2.00)
1599 *%-----|-----|
1600 CONTINUOUS NASHYD NHYD=["D4"], DT=[1]min, AREA=[1.73](ha), DWF=[0](cms), CN/C=[88],
IA=[8.4](mm),
1601 N=[3], TP=[0.60]hrs,
1602 Continuous simulation parameters:
1603 IaRECper=[4](hrs),
1604 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1605 InterEventTime=[12](hrs)
1606 Baseflow simulation parameters:
1607 BaseFlowOption=[1] ,
1608 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1609 VHydCond=[0.055](mm/hr), END=-1
1610 *%-----|-----|
1611 CONTINUOUS STANDHYD NHYD=["Area-B"], DT=[1]min, AREA=[24.04](ha), XIMP=[0.62],
TIMP=[0.77], DWF=[0](cms), LOSS=[1]:
1612 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1613 Pervious areas: IAper=[4.67](mm), SLPP=[1.4](%), LGP=[50](m),

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MNP=[0.250], SCP=[0](min),
1614 Impervious areas: IAimp=[1.57](mm), SLPI=[1.4](%),
LGI=[693.397](m), MNI=[0.013], SCI=[0](min),
1615 Continuous simulation parameters:
1616 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1

1617 *%-----|-----|
1618 ROUTE RESERVOIR NHYDout=["SWMF-B"], NHYDin=["Area-B"], RDT=[1](min),
1619 TABLE of ( OUTFLOW-STORAGE ) values
1620 (cms) - (ha-m)
1621 [ 0.000 , 0.000 ]
1622 [ 0.025 , 0.090 ]
1623 [ 0.175 , 0.510 ]
1624 [ 0.350 , 0.710 ]
1625 [ 0.495 , 0.820 ]
1626 [ 0.648 , 0.980 ]
1627 [ 0.965 , 1.045 ]
1628 [ 1.072 , 1.140 ]
1629 [ -1 , -1 ] (max twenty pts)
1630 NHYDovf=["SWMBOVF"]

1631 *%-----|-----|
1632 ADD HYD NHYDsum=["D4-EX"], NHYDs to add=["DRAIN4"+"D4"+"SWMF-B"+"SWMBOVF"]
1633 *%-----|-----|
1634 *ROUTE FLOW THROUGH O'Keefe Drain 5
1635 * JFSA: Nov. 2020, added en points to close X-Section
1636 ROUTE CHANNEL NHYDout=["DRAIN5"], NHYDin=["D4-EX"], RDT=[1](min),
1637 CHLGTH=[413.0](m), CHSLOPE=[0.16](%), FPSLOPE=[0.16](%),
1638 SECNUM=[1], NSEG=[3]
1639 ( SEGROUGH, SEGDIST (m))=[0.043,12.29 -0.033,17.97
1640 0.043,32.84] NSEG times
1641 ( DISTANCE (m), ELEVATION (m))=(-0.01, 2.50)
1642 [0.00, 1.41]
1643 [6.13, 0.97]
1644 [12.29, 0.89]
1645 [15.71, 0.00]
1646 [17.97, 0.39]
1647 [23.04, 0.35]
1648 [32.83, 0.96]
1649 (32.84, 2.50)

1650 *%-----|-----|
1651 CONTINUOUS NASHYD NHYD=["D5"], DT=[1]min, AREA=[1.90](ha),
1652 DWF=[0](cms), CN/C=[86], IA=[8.7](mm), N=[3], TP=[0.69]hrs,
1653 Continuous simulation parameters:
1654 IaREcper=[4](hrs),
1655 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1656 InterEventTime=[12](hrs)
1657 Baseflow simulation parameters:
1658 BaseFlowOption=[1] ,
1659 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1660 VHydCond=[0.055](mm/hr), END=-1

1661 *%-----|-----|
1662 *EXTERNAL FLOWS SOUTHEAST OF THE SITE NORTH OF McKENNA CASEY DR.
1663 CONTINUOUS NASHYD NHYD=["O-13SDF"], DT=[1]min, AREA=[9.74](ha),
1664 DWF=[0](cms), CN/C=[81], IA=[4.0](mm), N=[3], TP=[.43]hrs,
1665 Continuous simulation parameters:
1666 IaREcper=[4](hrs),
1667 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1668 InterEventTime=[12](hrs)
1669 Baseflow simulation parameters:
1670 BaseFlowOption=[1] ,
1671 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1672 VHydCond=[0.055](mm/hr), END=-1

1673 *%-----|-----|
1674 *SNOW DISPOSAL FACILITY
1675 *PARAMETERS BASED ON ROBINSON 2006 MODEL
1676 ROUTE RESERVOIR NHYDout=["SDF"], NHYDin=["O-13SDF"], RDT=[1](min),

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1677             TABLE of ( OUTFLOW-STORAGE ) values
1678                 (cms) - (ha-m)
1679                 [0.000,0.000]
1680                 [0.150,0.600]
1681                 (0.200,1.500)
1682                 [ -1 , -1 ] (max twenty pts)
1683                 NHYDovf=["OVFSDF"]
1684 *%-----|-----|
1685 *ANALYSIS POINT 6 - McKenna Casey Dr.
1686 *%-----|-----|
1687 ADD HYD      NHYDsum=["PT6MC"], NHYDs to add=["DRAIN5"+"D5"+"SDF"]
1688 *%-----|-----|
1689 CONTINUOUS NASHYD  NHYD=["O-15"], DT=[1]min, AREA=[10.67](ha),
1690                   DWF=[0](cms), CN/C=[82], IA=[7.5](mm), N=[3], TP=[0.30]hrs,
1691                   Continuous simulation parameters:
1692                   IaREcper=[4](hrs),
1693                   SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
1694                   InterEventTime=[12](hrs)
1695                   Baseflow simulation parameters:
1696                   BaseFlowOption=[1] ,
1697                   InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1698                   VHydCond=[0.055](mm/hr),  END=-1
1699 *%-----|-----|
1700 *TOTAL FLOW NORTH OF McKENNA CASEY DR.
1701 ADD HYD      NHYDsum=["M-C"], NHYDs to add=["PT6MC"+"O-15"]
1702 *%-----|-----|
1703 *ROUTE FLOW THROUGH AREA O-14
1704 * JFSA: Nov. 2020, added end points to close X-section
1705 ROUTE CHANNEL  NHYDout=["O-14Ch"], NHYDin=["M-C"], RDT=[1](min),
1706                CHLGTH=[845.3](m), CHSLOPE=[0.10](%), FPSLOPE=[0.10](%),
1707                SECNUM=[1], NSEG=[3]
1708                ( SEGROUGH, SEGDIST (m))=[0.06,15.00 -0.033,18.04 0.06,31.85] NSEG
1709                times
1710                ( DISTANCE (m), ELEVATION (m))=[-0.01, 2.5
1711                (0.00, 1.53]
1712                (5.56, 1.47)
1713                (9.21, 1.45)
1714                (12.45, 1.53)
1715                (13.70, 1.50)
1716                (15.00, 0.69)
1717                (15.34, 0.00)
1718                (16.51, 0.05)
1719                (17.30, 0.17)
1720                (18.04, 0.74)
1721                (19.29, 1.32)
1722                (22.73, 1.47)
1723                (31.84, 1.41)
1724                (31.85, 2.50)
1725 *%-----|-----|
1726 *% -Change O-14 from NASHYD to STANDHYD, name it "S-1-Okeefe" and add it to S-1
1727 *% -JFSA 2021-02-16, add detailed subcatchment drainage area for each subcatchment
1728 *% in Corrigan sub-catchment. After adding part of O-14 to S_1 sub-catchment so O-14
1729 *% becomes 5 ha instead of 30.02 ha and TP becomes 0.133 (5*0.8/30.02) instead of 0.8
1730 CONTINUOUS NASHYD  NHYD=["O-14"], DT=[1]min, AREA=[5](ha),
1731                   DWF=[0](cms), CN/C=[82], IA=[7.5](mm), N=[3], TP=[0.133]hrs,
1732                   Continuous simulation parameters:
1733                   IaREcper=[4](hrs),
1734                   SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
1735                   InterEventTime=[12](hrs)
1736                   Baseflow simulation parameters:
1737                   BaseFlowOption=[1] ,
1738                   InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1739                   VHydCond=[0.055](mm/hr),  END=-1
1740 *
1741 *%-----|-----|

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```

1739 *ANALYSIS POINT 7 - JOCK RIVER
1740 * 2020-12-01 To Foster Drain
1741 * 2020-12-01 replace ("PT7JR") by ("OKEEFE")
1742 *%-----|-----
1743 ADD HYD          NHYDsum=["OKEEFE"], NHYDs to add=["O-14Ch"+"O-14"]
1744 *%-----|-----
1745 *CONTINUOUS STANDHYD NHYD=["OKEEFE"], DT=[1](min), AREA=[448](ha),
1746 *                XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
1747 *                SCS curve number CN=[77],
1748 *                Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
1749 *                LGP=[40](m), MNP=[0.25], SCP=[0](min),
1750 *                Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
1751 *                LGI=[1728](m), MNI=[0.013], SCI=[0](min),
1752 *                Continuous simulation parameters:
1753 *                IaRECper=[4](hrs), IaRECimp=[4](hrs),
1754 *                SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1755 *                InterEventTime=[18](hrs), END=-1
1756 *#*****
1757 *#      Okeefe Pond
1758 *#      - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1759 *#      and a ratio of the catchment area to the West Clarke pond rating curve
1760 *#      from the MSS for the next coordinates
1761 *#*****
1762 *ROUTE RESERVOIR   NHYDout=["P_OKE"], NHYDin=["OKEEFE"],
1763 *                RDT=[1](min),
1764 *                TABLE of ( OUTFLOW-STORAGE ) values
1765 *                (cms) - (ha-m)
1766 *                [ 0.0 , 0.0]
1767 *                [ 14.13 , 13.0]
1768 *                [ -1 , -1 ] (maximum one hundred pairs of points)
1769 *                NHYDovf=["ok-OVF"],
1770 *%-----|-----
1771 * -JFSA 2021-02-25 "S-1-D2" and "S-1-D3" are part of S-1 sub-catchment. They are
1772 * moved to drain before station 6215 on Jock River
1773 *CONTINUOUS STANDHYD NHYD=["S-1-D2"], DT=[1](min), AREA=[18.67](ha), XIMP=[0.65],
1774 *                TIMP=[0.65], DWF=[0](cms),
1775 *                LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
1776 *                IAper=[4.67](mm), SLPP=[2.0](%),
1777 *                LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
1778 *                IAimp=[1.57](mm), SLPI=[0.75](%),
1779 *                LGI=[352.798](m), MNI=[0.013], SCI=[0](min),
1780 *                Continuous simulation parameters:
1781 *                IaRECper=[4](hrs), IaRECimp=[4](hrs),
1782 *                SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1783 *                InterEventTime=[12](hrs), END=-1
1784 *%-----|-----
1785 *CONTINUOUS NASHYD  NHYD=["S-1-D2"], DT=[1]min, AREA=[18.67](ha),
1786 *                DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
1787 *                N=[3], TP=[1.120]hrs,
1788 *                Continuous simulation parameters:
1789 *                IaRECper=[4](hrs),
1790 *                SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1791 *                InterEventTime=[12](hrs)
1792 *                Baseflow simulation parameters:
1793 *                BaseFlowOption=[1] ,
1794 *                InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1795 *                VHydCond=[0.055](mm/hr), END=-1
1796 *%-----|-----
1797 *COMPUTE DUALHYD   NHYDin=["S-1-D2"], CINLET=[2.097](cms), NINLET=[1],
1798 *                MajNHYD=["S-1-D2J"]
1799 *                MinNHYD=["S-1-D2N"]
1800 *                TMJSTO=[9999999](cu-m)
1801 *%-----|-----
1802 *ADD HYD           NHYDsum=["S-1-D2S"], NHYDs to add=["S-1-D2J"+"S-1-D2N"]
1803 *%-----|-----

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1800 ROUTE RESERVOIR      NHYDout=["S-1-D2R"] ,NHYDin=["S-1-D2S"] ,
1801                      RDT=[1](min),
1802                      TABLE of ( OUTFLOW-STORAGE ) values
1803                          (cms) - (ha-m)
1804                          [ 0.0      , 0.0 ]
1805                          [ 0.2231, 0.7445 ]
1806                          [   -1   ,  -1   ] (max twenty pts)
1807                      NHYDovf=["S-1-D2Rovf"]
1808 *%-----|-----|
1809 CONTINUOUS STANDHYD NHYD=["S-1-D3"], DT=[1](min), AREA=[6.79](ha), XIMP=[0.65],
1810 TIMP=[0.65], DWF=[0](cms),
1811 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
1812 IAper=[4.67](mm), SLPP=[2.0](%),
1813 LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
1814 IAimp=[1.57](mm), SLPI=[0.75](%),
1815 LGI=[212.760](m), MNI=[0.013], SCI=[0](min),
1816 Continuous simulation parameters:
1817 IaREcper=[4](hrs), IaREcimp=[4](hrs),
1818 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1819 InterEventTime=[12](hrs), END=-1
1820 *%-----|-----|
1821 *CONTINUOUS NASHYD  NHYD=["S-1-D3"], DT=[1]min, AREA=[6.79](ha),
1822 *                    DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
1823 *                    N=[3], TP=[1.281]hrs,
1824 *                    Continuous simulation parameters:
1825 *                    IaREcper=[4](hrs),
1826 *                    SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1827 *                    InterEventTime=[12](hrs)
1828 *                    Baseflow simulation parameters:
1829 *                    BaseFlowOption=[1] ,
1830 *                    InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1831 *                    VHydCond=[0.055](mm/hr), END=-1
1832 *%-----|-----|
1833 COMPUTE DUALHYD     NHYDin=["S-1-D3"], CINLET=[0.831](cms), NINLET=[1],
1834 MaJNHYD=["S-1-D3J"]
1835 MinNHYD=["S-1-D3N"]
1836 TMJSTO=[9999999](cu-m)
1837 *%-----|-----|
1838 ADD HYD              NHYDsum=["S-1-D3S"], NHYDs to add=["S-1-D3J"+"S-1-D3N"]
1839 *%-----|-----|
1840 ROUTE RESERVOIR      NHYDout=["S-1-D3R"] ,NHYDin=["S-1-D3S"] ,
1841                      RDT=[1](min),
1842                      TABLE of ( OUTFLOW-STORAGE ) values
1843                          (cms) - (ha-m)
1844                          [ 0.0      , 0.0 ]
1845                          [ 0.0811, 0.2708 ]
1846                          [   -1   ,  -1   ] (max twenty pts)
1847                      NHYDovf=["S-1-D3Rovf"]
1848 *%-----|-----|
1849 ADD HYD              NHYDsum=["SN_OK"], NHYDs to
1850 add=["N_OK"+"OKEEFE"+"S-1-D2R"+"S-1-D3R"+"S-1-D2Rovf"+"S-1-D3Rovf"]
1851 *%-----|-----|
1852 SAVE HYD             NHYD=["SN_OK"], # OF PCYCLES=[-1], ICASEsh=[1]
1853 HYD_COMMENT=["Total Flows at Okeefe Drain"]
1854 *%-----|-----|
1855 ROUTE CHANNEL        NHYDout=["N_FO"] ,NHYDin=["SN_OK"] ,
1856                      RDT=[1](min),
1857                      CHLGTH=[1183](m), CHSLOPE=[0.0761](%),
1858                      FPSLOPE=[0.0761](%),
1859                      SECNUM=[1.0], NSEG=[3]
1860                      ( SEGROUGH, SEGDIST (m))=
1861                      [0.050,-33.89

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1862         -0.035,31.59
1863         0.050,34.41] NSEG times
1864         ( DISTANCE (m), ELEVATION (m))=
1865         [-794.18, 91.00]
1866         [-775.41, 91.50]
1867         [-702.63, 91.50]
1868         [-546.19, 91.50]
1869         [-529.54, 91.50]
1870         [-323.44, 91.00]
1871         [-320.71, 91.00]
1872         [-183.59, 91.00]
1873         [-182.54, 90.50]
1874         [-181.36, 90.00]
1875         [-177.37, 90.00]
1876         [-87.70, 90.00]
1877         [-33.89, 90.00]
1878         [-18.52, 86.88]
1879         [0.00,85.20]
1880         [16.20, 86.83]
1881         [31.59, 90.00]
1882         [33.03, 90.50]
1883         [34.41, 91.00]
1884 *%-----|-----|
1885 *#*****
1886 *#   Catchment FOSTER
1887 *#   - To Foster ditch (north of the Jock)
1888 *#   - Partially developed (medium density); remaining agricultural
1889 *#   - 2020-12-01 JFSA Foster area is 332 as per Foster SWMF Environmental Study
1890 *#   - 2020-12-01 decrease Foster drainage area from (373 HA) to (307.98 HA) after
1891 *#   - 2021-02-12 update Foster area to 325.44 ha as measured from QGIS
1892 *#*****
1893 CONTINUOUS STANDHYD NHYD=["FOSTER"], DT=[1]min, AREA=[325.44](ha),
1894 XIMP=[0.55], TIMP=[0.55], DWF=[0](cms), LOSS=[2],
1895 SCS curve number CN=[74],
1896 Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
1897 LGP=[40](m), MNP=[0.25], SCP=[0](min),
1898 Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
1899 LGI=[1472.956](m), MNI=[0.013], SCI=[0](min),
1900 Continuous simulation parameters:
1901 IaRECper=[4](hrs), IaRECimp=[4](hrs),
1902 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1903 InterEventTime=[18](hrs), END=-1
1904 *#*****
1905 *#   Foster Pond
1906 *#   - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1907 *#   and a ratio of the catchment area to the West Clarke pond rating curve
1908 *#   from the MSS for the next coordinates
1909 *#*****
1910 ROUTE RESERVOIR NHYDout=["P_FOS"], NHYDin=["FOSTER"],
1911 RDT=[1](min),
1912 TABLE of ( OUTFLOW-STORAGE ) values
1913 (cms) - (ha-m)
1914 [ 0.0 , 0.0 ]
1915 [ 10.34 , 10]
1916 [ -1 , -1 ] (max twenty pts)
1917 NHYDovf=["FO-OVF"]
1918 *%-----|-----|
1919 ADD HYD NHYDsum=["FOSTER-OUT"], NHYDs to add=["P_FOS"+"FO-OVF"]
1920 *%-----|-----|
1921 *#*****
1922 * -Brazeau area from P 1800-19 =[71.751], change to 63.59 ha based on GIS measurements
1923 * -JFSA, 2021-01-19 update "W_CLAR_BRAZ" to 73.29 ha based on GIS measurements
1924 * -JFSA, 2021-01-22 Brazeau ("MS_P10"+"P10-OVF")brazeau pond discharges directly

```



to the jock river through a road side ditch on the west side of Borrisokane road (station 6016)

1925 **CONTINUOUS STANDHYD** NHYD=["W\_CLAR\_BRAZ"], DT=[1]min, AREA=[73.29](ha),  
1926 XIMP=[0.6], TIMP=[0.65], DWF=[0](cms), LOSS=[2],  
1927 SCS curve number CN=[77],  
1928 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),  
1929 LGP=[40](m), MNP=[0.25], SCP=[0](min),  
1930 Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),  
1931 LGI=[699.00](m), MNI=[0.013], SCI=[0](min),  
1932 Continuous simulation parameters:  
1933 IaRECPper=[4](hrs), IaRECImp=[4](hrs),  
1934 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),  
1935 InterEventTime=[18](hrs), END=-1

\*%-----|-----  
\* 2020-12-01 correct pond curve values

1938 **ROUTE RESERVOIR** NHYDout=["MS\_P10"], NHYDin=["W\_CLAR\_BRAZ"],  
1939 RDT=[1](min),

1940 TABLE of ( OUTFLOW-STORAGE ) values  
1941 (cms) - (ha-m)  
1942 [ 0.0 , 0.0 ]  
1943 [ 0.068 , 0.001 ]  
1944 [ 0.271 , 0.022 ]  
1945 [ 0.379 , 0.051 ]  
1946 [ 0.48 , 0.091 ]  
1947 [ 0.853 , 0.341 ]  
1948 [ 1.005 , 0.61 ]  
1949 [ 1.128 , 1.231 ]  
1950 [ 1.155 , 1.592 ]  
1951 [ 1.194 , 1.876 ]  
1952 [ 1.2 , 1.921 ]  
1953 [ 1.259 , 2.369 ]  
1954 [ 1.3 , 2.665 ]  
1955 [ 1.349 , 2.813 ]  
1956 [ -1 , -1 ] (max twenty pts)  
1957 NHYDovf=["P10-OVF"]

\*%-----|-----  
\* -JFSA 2021-02-26 "S-1-FO-D2" is a part of S-1 sub-catchment. It is moved to drain before station 980 on Foster Drain

1960 **CONTINUOUS STANDHYD** NHYD=["S-1-FO-D2"], DT=[1]min, AREA=[4.94](ha),  
1961 XIMP=[0.55], TIMP=[0.55], DWF=[0](cms), LOSS=[2],  
1962 SCS curve number CN=[74],  
1963 Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),  
1964 LGP=[40](m), MNP=[0.25], SCP=[0](min),  
1965 Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),  
1966 LGI=[181.475](m), MNI=[0.013], SCI=[0](min),  
1967 Continuous simulation parameters:  
1968 IaRECPper=[4](hrs), IaRECImp=[4](hrs),  
1969 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),  
1970 InterEventTime=[18](hrs), END=-1

\*%-----|-----  
\*CONTINUOUS NASHYD NHYD=["S-1-FO-D2"], DT=[1]min, AREA=[4.94](ha),  
1972 \* DWF=[0](cms), CN/C=[77], IA=[4.67](mm),  
1973 \* N=[3], TP=[1.10]hrs,  
1974 \* Continuous simulation parameters:  
1975 \* IaRECPper=[4](hrs),  
1976 \* SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),  
1977 \* InterEventTime=[12](hrs)  
1978 \* Baseflow simulation parameters:  
1979 \* BaseFlowOption=[1] ,  
1980 \* InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)  
1981 \* VHydCond=[0.055](mm/hr), END=-1  
1982 \*%-----|-----

1984 **COMPUTE DUALHYD** NHYDin=["S-1-FO-D2"], CINLET=[0.508](cms), NINLET=[1],  
1985 MajNHYD=["S-1-FO-D2J"]  
1986 MinNHYD=["S-1-FO-D2N"]  
1987 TMJSTO=[9999999](cu-m)

```

1988  *%-----|-----|
1989  ADD HYD      NHYDsum=["S-1-FO-D2S"], NHYDs to add=["S-1-FO-D2J"+"S-1-FO-D2N"]
1990  *%-----|-----|
1991  ROUTE RESERVOIR  NHYDout=["S-1-FO-D2R"] ,NHYDin=["S-1-FO-D2S"] ,
1992  RDT=[1](min),
1993  TABLE of ( OUTFLOW-STORAGE ) values
1994  (cms) - (ha-m)
1995  [ 0.0      , 0.0 ]
1996  [ 0.0590, 0.1970 ]
1997  [      -1 , -1      ] (max twenty pts)
1998  NHYDovf=["S-1FOD2ovf"]
1999  *%-----|-----|
2000  ADD HYD      NHYDsum=["980"], NHYDs to
add=["FOSTER-OUT"+"S-1-FO-D2R"+"S-1FOD2ovf"]
2001  *%-----|-----|
2002  SAVE HYD     NHYD=["980"], # OF PCYCLES=[-1], ICASEsh=[1]
2003  HYD_COMMENT=["Total Flows at Station 980 on Foster Drain"]
2004  *%-----|-----|
2005  *#
2006  *# Hydrograph from Node Foster SWM (Station 980)to Node at station 520
2007  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 980
2008  *#
2009  ROUTE CHANNEL  NHYDout=["980-out"] ,NHYDin=["980"] ,
2010  RDT=[1](min),
2011  CHLGTH=[460](m),  CHSLOPE=[0.04348](%),
2012  FPSLOPE=[0.04348](%),
2013  SECNUM=[1.0],      NSEG=[3]
2014  ( SEGROUGH, SEGDIST (m))=
2015  [0.050,45.90
2016  -0.035,53.30
2017  0.050,100] NSEG times
2018  ( DISTANCE (m), ELEVATION (m))=
2019  [0, 91.75 ]
2020  [42.4, 92.18 ]
2021  [43.5, 92.16 ]
2022  [44.1, 92.1 ]
2023  [44.6, 92 ]
2024  [44.8, 91.86 ]
2025  [45.9, 91.04 ]
2026  [46.4, 90.65 ]
2027  [46.8, 90.36 ]
2028  [47.9, 90.32 ]
2029  [48.7, 90.35 ]
2030  [50.7, 90.33 ]
2031  [52.2, 90.38 ]
2032  [52.5, 90.59 ]
2033  [53.3, 91.28 ]
2034  [54, 91.83 ]
2035  [54.3, 92 ]
2036  [54.8, 92.08 ]
2037  [55.4, 92.12 ]
2038  [100, 91.84 ]
2039  *%-----|-----|
2040  * -JFSA 2021-02-26 "S-1-FO-D1" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2041  CONTINUOUS STANDHYD  NHYD=["S-1-FO-D1"], DT=[1]min, AREA=[5.11](ha),
2042  XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2043  SCS curve number CN=[74],
2044  Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2045  LGP=[40](m), MNP=[0.25], SCP=[0](min),
2046  Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2047  LGI=[184.572](m), MNI=[0.013], SCI=[0](min),
2048  Continuous simulation parameters:
2049  IaRECper=[4](hrs), IaRECimp=[4](hrs),
2050  SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2051  InterEventTime=[18](hrs), END=-1

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2052 *%-----|-----|
2053 COMPUTE DUALHYD NHYDin=["S-1-FO-D1"], CINLET=[0.605](cms), NINLET=[1],
2054 MajNHYD=["S-1-FO-D1J"]
2055 MinNHYD=["S-1-FO-D1N"]
2056 TMJSTO=[9999999](cu-m)
2057 *%-----|-----|
2058 ADD HYD NHYDsum=["S-1-FO-D1S"], NHYDs to add=["S-1-FO-D1N"+"S-1-FO-D1J"]
2059 *%-----|-----|
2060 ROUTE RESERVOIR NHYDout=["S-1-FO-D1R"], NHYDin=["S-1-FO-D1S"],
2061 RDT=[1](min),
2062 TABLE of ( OUTFLOW-STORAGE ) values
2063 (cms) - (ha-m)
2064 [ 0.0 , 0.0 ]
2065 [ 0.0611, 0.2038 ]
2066 [ -1 , -1 ] (max twenty pts)
2067 NHYDovf=["S-1FODlovf"]
2068 *%-----|-----|
2069 ADD HYD NHYDsum=["520"], NHYDs to add=["980-out"+"S-1-FO-D1R"+"S-1FODlovf"]
2070 *%-----|-----|
2071 SAVE HYD NHYD=["520"], # OF PCYCLES=[-1], ICASEsh=[1]
2072 HYD_COMMENT=["Total Flows at Sation 520 on Foster Drain"]
2073 *%-----|-----|
2074 *# Hydrograph from Node at Station 520 (Foster Drain) to Node at station 6016 (Jock
River)
2075 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 520
2076 *#
2077 ROUTE CHANNEL NHYDout=["520-out"], NHYDin=["520"],
2078 RDT=[1](min),
2079 CHLGTH=[860](m), CHSLOPE=[0.5872](%),
2080 FPSLOPE=[0.5872](%),
2081 SECNUM=[1.0], NSEG=[3]
2082 ( SEGROUGH, SEGDIST (m))=
2083 [0.050,45.90
2084 -0.035,54.3
2085 0.050,100.1097] NSEG times
2086 ( DISTANCE (m), ELEVATION (m))=
2087 [0, 91.26 ]
2088 [44.9, 91.46 ]
2089 [45.1, 91.37 ]
2090 [45.9, 90.84 ]
2091 [47, 90.32 ]
2092 [47.5, 90.22 ]
2093 [48, 90.17 ]
2094 [50.7, 90.19 ]
2095 [51.5, 90.17 ]
2096 [52.2, 90.13 ]
2097 [52.7, 90.12 ]
2098 [53.3, 90.14 ]
2099 [53.5, 90.31 ]
2100 [53.9, 90.59 ]
2101 [54.3, 90.87 ]
2102 [54.7, 91.04 ]
2103 [55.3, 91.24 ]
2104 [55.5, 91.26 ]
2105 [63.7, 91.37 ]
2106 [100.1097, 91.43 ]
2107 *%-----|-----|
2108 * -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2109 CONTINUOUS STANDHYD NHYD=["S-1-FO-F-D"], DT=[1]min, AREA=[14.96](ha),
2110 XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2111 SCS curve number CN=[74],
2112 Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2113 LGP=[40](m), MNP=[0.25], SCP=[0](min),
2114 Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2115 LGI=[315.806](m), MNI=[0.013], SCI=[0](min),

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2116 Continuous simulation parameters:
2117 IaREcper=[4](hrs), IaREcimp=[4](hrs),
2118 SMIN=[-1](mm), SMAx=[-1](mm), SK=[0.010]/(mm),
2119 InterEventTime=[18](hrs), END=-1
2120 *%-----|-----|
2121 *CONTINUOUS NASHYD NHYD=["S-1-FO-F-D"], DT=[1]min, AREA=[14.96](ha),
2122 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2123 * N=[3], TP=[1.007]hrs,
2124 * Continuous simulation parameters:
2125 * IaREcper=[4](hrs),
2126 * SMIN=[-1](mm), SMAx=[-1](mm), SK=[0.010]/(mm),
2127 * InterEventTime=[12](hrs)
2128 * Baseflow simulation parameters:
2129 * BaseFlowOption=[1] ,
2130 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2131 * VHydCond=[0.055](mm/hr), END=-1
2132 *%-----|-----|
2133 COMPUTE DUALHYD NHYDin=["S-1-FO-F-D"], CINLET=[1.615](cms), NINLET=[1],
2134 MajNHYD=["S-1FO-F-DJ"]
2135 MinNHYD=["S-1FO-F-DN"]
2136 TMJSTO=[9999999](cu-m)
2137 *%-----|-----|
2138 ADD HYD NHYDsum=["S-1FO-F-DS"], NHYDs to add=["S-1FO-F-DJ"+"S-1FO-F-DN"]
2139 *%-----|-----|
2140 ROUTE RESERVOIR NHYDout=["S-1FO-F-DR"],NHYDin=["S-1FO-F-DS"] ,
2141 RDT=[1](min),
2142 TABLE of ( OUTFLOW-STORAGE ) values
2143 (cms) - (ha-m)
2144 [ 0.0 , 0.0 ]
2145 [ 0.1788, 0.5966 ]
2146 [ -1 , -1 ] (max twenty pts)
2147 NHYDovf=["S-1FoFDovf"]
2148 *%-----|-----|
2149 * -JFSA 2021-02-26 "S-1-D8" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2150 CONTINUOUS STANDHYD NHYD=["S-1-D8"], DT=[1]min, AREA=[5.27](ha), XIMP=[0.325],
TIMP=[0.65], DWF=[0](cms), LOSS=[1]:
2151 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
2152 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
2153 Impervious areas: IAimp=[0.785](mm), SLPI=[0.75](%),
LGI=[187.439](m), MNI=[0.013], SCI=[0](min),
2154 Continuous simulation parameters:
2155 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
2156 *%-----|-----|
2157 *CONTINUOUS NASHYD NHYD=["S-1-D8"], DT=[1]min, AREA=[5.27](ha),
2158 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2159 * N=[3], TP=[1.10]hrs,
2160 * Continuous simulation parameters:
2161 * IaREcper=[4](hrs),
2162 * SMIN=[-1](mm), SMAx=[-1](mm), SK=[0.010]/(mm),
2163 * InterEventTime=[12](hrs)
2164 * Baseflow simulation parameters:
2165 * BaseFlowOption=[1] ,
2166 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2167 * VHydCond=[0.055](mm/hr), END=-1
2168 *%-----|-----|
2169 COMPUTE DUALHYD NHYDin=["S-1-D8"], CINLET=[0.672](cms), NINLET=[1],
2170 MajNHYD=["S-1-D8J"]
2171 MinNHYD=["S-1-D8N"]
2172 TMJSTO=[9999999](cu-m)
2173 *%-----|-----|
2174 ADD HYD NHYDsum=["S-1-D8S"], NHYDs to add=["S-1-D8J"+"S-1-D8N"]
2175 *%-----|-----|

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2176 *ADD HYD          NHYDsum=["S-1-D"], NHYDs to add=["S-1-Okeefe"+"S-1"+"S-1-Post"]
2177 *%-----|-----|
2178 *COMPUTE DUALHYD  NHYDin=["S-1-D"], CINLET=[11.616](cms), NINLET=[1],
2179 *                MajNHYD=["S-1-D-MJ"]
2180 *                MinNHYD=["S-1-D-MN"]
2181 *                TMJSTO=[5974](cu-m)
2182 *%-----|-----|
2183 *ADD HYD          NHYDsum=["S-1-DEV"], NHYDs to add=["S-1-D-MJ"+"S-1-D-MN"]
2184 *%-----|-----|
2185 ROUTE RESERVOIR NHYDout=["S-1-D8R"] ,NHYDin=["S-1-D8S"] ,
2186 RDT=[1](min),
2187             TABLE of ( OUTFLOW-STORAGE ) values
2188                   (cms) - (ha-m)
2189                   [ 0.0      , 0.0 ]
2190                   [ 0.0630, 0.2102 ]
2191                   [    -1    , -1    ] (max twenty pts)
2192             NHYDovf=["S-1-D8Rovf"]
2193 *%-----|-----|
2194 *   -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2195 CONTINUOUS NASHYD NHYD=["S-1-A"], DT=[1]min, AREA=[75.88](ha),
2196 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2197 N=[3], TP=[0.619]hrs,
2198 Continuous simulation parameters:
2199 IaREcper=[4](hrs),
2200 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2201 InterEventTime=[12](hrs)
2202 Baseflow simulation parameters:
2203 BaseFlowOption=[1] ,
2204 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2205 VHydCond=[0.055](mm/hr), END=-1
2206 *%-----|-----|
2207 *   -JFSA, 2021-01-22 "W_CLAR_UNDE" (west of Clarke sub-catchment) discharges
directly to the jock river through a road side ditch on the west side of Borrisokane
road (station 6016)
2208 CONTINUOUS NASHYD NHYD=["W_CLAR_UNDE"], DT=[1]min, AREA=[35.65](ha),
2209 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2210 N=[3], TP=[1.10]hrs,
2211 Continuous simulation parameters:
2212 IaREcper=[4](hrs),
2213 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2214 InterEventTime=[12](hrs)
2215 Baseflow simulation parameters:
2216 BaseFlowOption=[1] ,
2217 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2218 VHydCond=[0.055](mm/hr), END=-1
2219 *%-----|-----|
2220 ADD HYD          NHYDsum=["SN_FO"], NHYDs to
add=["N_FO"+"520-out"+"MS_P10"+"P10-OVF"+"W_CLAR_UNDE"+"S-1FoFDovf"+"S-1FO-F-DR"+"S-1-D8R
ovf"+"S-1-D8R"+"S-1-A"]
2221 *%-----|-----|
2222 SAVE HYD        NHYD=["SN_FO"], # OF PCYCLES=[-1], ICASEsh=[1]
2223 HYD_COMMENT=["Total Flows at Foster Drain"]
2224 *%-----|-----|
2225 *# Hydrograph from Node Foster routed to Node at Cedarview Road
2226 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6016
2227 *#
2228 ROUTE CHANNEL  NHYDout=["N_CE"] ,NHYDin=["SN_FO"] ,
2229 RDT=[1](min),
2230 CHLGTH=[159](m), CHSLOPE=[0.0818](%),
2231                   FPSLOPE=[0.0818](%),
2232 SECNUM=[1.0], NSEG=[3]
2233 ( SEGROUGH, SEGDIST (m))=
2234 [0.050,-15.46
2235 -0.035,26.55
2236 0.050,116.76] NSEG times

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2237      ( DISTANCE (m), ELEVATION (m))=
2238      [-645.23, 91.50]
2239      [-391.20, 91.50]
2240      [-91.00, 91.50]
2241      [-85.52, 91.50]
2242      [-15.46, 89.40]
2243      [-9.79, 89.31]
2244      [-3.22, 86.24]
2245      [3.22, 85.07]
2246      [10.96, 85.79]
2247      [16.44, 86.49]
2248      [26.55, 89.45]
2249      [29.03, 90.27]
2250      [35.76, 90.67]
2251      [36.67, 91.00]
2252      [108.08, 91.00]
2253      [109.82, 90.50]
2254      [112.04, 90.50]
2255      [114.62, 91.00]
2256      [116.76, 91.50]
2257      *%-----|-----|
2258      *#*****|
2259      *#      Catchment S-1
2260      *#      - To Jock River (north and south of Jock)
2261      *#      - Primarily agricultural fields; portion of sand quarry
2262      *%-----|-----|
2263      *%      -2020-12-17 "S-1-Undev" and "S-1-Fost" was a part of Foster drain, they are below
the foster pond. Now they are added to S-1 subcatchment based on Project 1474-BCDC,
JFSA, Nov. 2020
2264      *%      -2020-12-17 Change O-14 (it was part of Okeefe drain) to "S-1-Okeefe" and add it
to S-1 subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
2265      *%      -2020-12-17 Add "S-1-BCDC" as NASHYD
2266      *%      -2020-12-17 all other S-1 subcatchment as STANDHYD with DUALHYD and ROUTE RESERVOIR
2267      *%-----|-----|
2268      *#*****|
2269      *      -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2270      *CONTINUOUS NASHYD      NHYD=["S-1-A"], DT=[1]min, AREA=[75.88](ha),
2271      *      DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2272      *      N=[3], TP=[0.619]hrs,
2273      *      Continuous simulation parameters:
2274      *      IaRECper=[4](hrs),
2275      *      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2276      *      InterEventTime=[12](hrs)
2277      *      Baseflow simulation parameters:
2278      *      BaseFlowOption=[1] ,
2279      *      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2280      *      VHydCond=[0.055](mm/hr), END=-1
2281      *%-----|-----|
2282      CONTINUOUS NASHYD      NHYD=["S-1-B"], DT=[1]min, AREA=[55.36](ha),
2283      DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2284      N=[3], TP=[0.451]hrs,
2285      Continuous simulation parameters:
2286      IaRECper=[4](hrs),
2287      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2288      InterEventTime=[12](hrs)
2289      Baseflow simulation parameters:
2290      BaseFlowOption=[1] ,
2291      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2292      VHydCond=[0.055](mm/hr), END=-1
2293      *%-----|-----|
2294      *#      - JFSA 2021-02-24 change the name from S-1-BCDC to S-1-A and S-1-B. Change their
TP values based on the new areas compared to the old ones.
2295      *CONTINUOUS NASHYD      NHYD=["S-1-BCDC"], DT=[1]min, AREA=[134.9](ha),
2296      *      DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2297      *      N=[3], TP=[1.10]hrs,

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2298 * Continuous simulation parameters:
2299 * IaRECper=[4](hrs),
2300 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2301 * InterEventTime=[12](hrs)
2302 * Baseflow simulation parameters:
2303 * BaseFlowOption=[1] ,
2304 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2305 * VHydCond=[0.055](mm/hr), END=-1
2306 *%-----|-----|
2307 *# - JFSA 2021-02-24 "S-1-BCDC-1" and "S-1-BCDC-2" are not existing anymore.
    "S-1-BCDC-1" is part of "S-1-FO-D2" and "S-1-BCDC-2" is part of "S-1-D2" and "S-1-D3"
2308 *CONTINUOUS NASHYD NHYD=["S-1-BCDC-1"], DT=[1]min, AREA=[0.3](ha),
2309 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2310 * N=[3], TP=[1.10]hrs,
2311 * Continuous simulation parameters:
2312 * IaRECper=[4](hrs),
2313 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2314 * InterEventTime=[12](hrs)
2315 * Baseflow simulation parameters:
2316 * BaseFlowOption=[1] ,
2317 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2318 * VHydCond=[0.055](mm/hr), END=-1
2319 *%-----|-----|
2320 *CONTINUOUS NASHYD NHYD=["S-1-BCDC-2"], DT=[1]min, AREA=[1.3](ha),
2321 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2322 * N=[3], TP=[1.10]hrs,
2323 * Continuous simulation parameters:
2324 * IaRECper=[4](hrs),
2325 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2326 * InterEventTime=[12](hrs)
2327 * Baseflow simulation parameters:
2328 * BaseFlowOption=[1] ,
2329 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2330 * VHydCond=[0.055](mm/hr), END=-1
2331 *%-----|-----|
2332 *# - JFSA 2021-01-19, after adding Greenbank pond, "S-1-BCDC-3" is not existing
    anymore
2333 *CONTINUOUS NASHYD NHYD=["S-1-BCDC-3"], DT=[1]min, AREA=[3.9](ha),
2334 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2335 * N=[3], TP=[1.10]hrs,
2336 * Continuous simulation parameters:
2337 * IaRECper=[4](hrs),
2338 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2339 * InterEventTime=[12](hrs)
2340 * Baseflow simulation parameters:
2341 * BaseFlowOption=[1] ,
2342 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2343 * VHydCond=[0.055](mm/hr), END=-1
2344 *%-----|-----|
2345 * -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
    before station 7245 on Jock River
2346 *CONTINUOUS STANDHYD NHYD=["S-1-Okeefe"], DT=[1](min), AREA=[44.93](ha), XIMP=[0.65],
    TIMP=[0.65], DWF=[0](cms),
2347 * LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
    IAper=[4.67](mm), SLPP=[2.0](%),
2348 * LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
    IAimp=[1.57](mm), SLPI=[0.75](%),
2349 * LGI=[547.296](m), MNI=[0.013], SCI=[0](min),
2350 * Continuous simulation parameters:
2351 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
2352 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2353 * InterEventTime=[12](hrs), END=-1
2354 *%-----|-----|
2355 *COMPUTE DUALHYD NHYDin=["S-1-Okeefe"], CINLET=[4.796](cms), NINLET=[1],
2356 * MajNHYD=["S-1-OkMJ"]
2357 * MinNHYD=["S-1-OkMN"]

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2358 * TMJSTO=[9999999](cu-m)
2359 *%-----|-----|
2360 *ADD HYD NHYDsum=["S-1-OkS"], NHYDs to add=["S-1-OkMJ"+"S-1-OkMN"]
2361 *%-----|-----|
2362 *ROUTE RESERVOIR NHYDout=["S-1-OkSR"] ,NHYDin=["S-1-OkS"] ,
2363 * RDT=[1](min),
2364 * TABLE of ( OUTFLOW-STORAGE ) values
2365 * (cms) - (ha-m)
2366 * [ 0.0 , 0.0 ]
2367 * [ 0.5370, 1.7917 ]
2368 * [ -1 , -1 ] (max twenty pts)
2369 * NHYDovf=["S-1-OkSovf"]
2370 *%-----|-----|
2371 *CONTINUOUS NASHYD NHYD=["S-1-Okeefe"], DT=[1]min, AREA=[44.93](ha),
2372 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2373 * N=[3], TP=[1.049]hrs,
2374 * Continuous simulation parameters:
2375 * IaRECper=[4](hrs),
2376 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2377 * InterEventTime=[12](hrs)
2378 * Baseflow simulation parameters:
2379 * BaseFlowOption=[1] ,
2380 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2381 * VHydCond=[0.055](mm/hr), END=-1
2382 *%-----|-----|
2383 * -JFSA 2021-02-26 "S-1-FO-D1" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2384 *CONTINUOUS STANDHYD NHYD=["S-1-FO-D1"], DT=[1]min, AREA=[5.11](ha),
2385 * XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2386 * SCS curve number CN=[74],
2387 * Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2388 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
2389 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2390 * LGI=[184.572](m), MNI=[0.013], SCI=[0](min),
2391 * Continuous simulation parameters:
2392 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
2393 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2394 * InterEventTime=[18](hrs), END=-1
2395 *%-----|-----|
2396 *COMPUTE DUALHYD NHYDin=["S-1-FO-D1"], CINLET=[0.605](cms), NINLET=[1],
2397 * MajNHYD=["S-1-FO-D1J"]
2398 * MinNHYD=["S-1-FO-D1N"]
2399 * TMJSTO=[9999999](cu-m)
2400 *%-----|-----|
2401 *ADD HYD NHYDsum=["S-1-FO-D1S"], NHYDs to add=["S-1-FO-D1N"+"S-1-FO-D1J"]
2402 *%-----|-----|
2403 *ROUTE RESERVOIR NHYDout=["S-1-FO-D1R"] ,NHYDin=["S-1-FO-D1S"] ,
2404 * RDT=[1](min),
2405 * TABLE of ( OUTFLOW-STORAGE ) values
2406 * (cms) - (ha-m)
2407 * [ 0.0 , 0.0 ]
2408 * [ 0.0611, 0.2038 ]
2409 * [ -1 , -1 ] (max twenty pts)
2410 * NHYDovf=["S-1FOD1ovf"]
2411 *%-----|-----|
2412 *CONTINUOUS NASHYD NHYD=["S-1-FO-D1"], DT=[1]min, AREA=[5.11](ha),
2413 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2414 * N=[3], TP=[1.10]hrs,
2415 * Continuous simulation parameters:
2416 * IaRECper=[4](hrs),
2417 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2418 * InterEventTime=[12](hrs)
2419 * Baseflow simulation parameters:
2420 * BaseFlowOption=[1] ,
2421 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2422 * VHydCond=[0.055](mm/hr), END=-1

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2423 *%-----|-----|
2424 *   -JFSA 2021-02-26 "S-1-FO-D2" is a part of S-1 sub-catchment. It is moved to drain
before station 980 on Foster Drain
2425 *CONTINUOUS STANDHYD NHYD=["S-1-FO-D2"], DT=[1]min, AREA=[4.94](ha),
2426 *   XIMP=[0.55], TIMP=[0.55], DWF=[0](cms), LOSS=[2],
2427 *   SCS curve number CN=[74],
2428 *   Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2429 *   LGP=[40](m), MNP=[0.25], SCP=[0](min),
2430 *   Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2431 *   LGI=[181.475](m), MNI=[0.013], SCI=[0](min),
2432 *   Continuous simulation parameters:
2433 *   IaRECper=[4](hrs), IaRECimp=[4](hrs),
2434 *   SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2435 *   InterEventTime=[18](hrs), END=-1
2436 *%-----|-----|
2437 *CONTINUOUS NASHYD NHYD=["S-1-FO-D2"], DT=[1]min, AREA=[4.94](ha),
2438 *   DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2439 *   N=[3], TP=[1.10]hrs,
2440 *   Continuous simulation parameters:
2441 *   IaRECper=[4](hrs),
2442 *   SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2443 *   InterEventTime=[12](hrs)
2444 *   Baseflow simulation parameters:
2445 *   BaseFlowOption=[1] ,
2446 *   InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2447 *   VHydCond=[0.055](mm/hr), END=-1
2448 *%-----|-----|
2449 *COMPUTE DUALHYD NHYDin=["S-1-FO-D2"], CINLET=[0.508](cms), NINLET=[1],
2450 *   MajNHYD=["S-1-FO-D2J"]
2451 *   MinNHYD=["S-1-FO-D2N"]
2452 *   TMJSTO=[9999999](cu-m)
2453 *%-----|-----|
2454 *ADD HYD NHYDsum=["S-1-FO-D2S"], NHYDs to add=["S-1-FO-D2J"+"S-1-FO-D2N"]
2455 *%-----|-----|
2456 *ROUTE RESERVOIR NHYDout=["S-1-FO-D2R"], NHYDin=["S-1-FO-D2S"] ,
2457 *   RDT=[1](min),
2458 *   TABLE of ( OUTFLOW-STORAGE ) values
2459 *   (cms) - (ha-m)
2460 *   [ 0.0 , 0.0 ]
2461 *   [ 0.0590, 0.1970 ]
2462 *   [ -1 , -1 ] (max twenty pts)
2463 *   NHYDovf=["S-1FOD2ovf"]
2464 *%-----|-----|
2465 *   -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2466 *CONTINUOUS STANDHYD NHYD=["S-1-FO-F-D"], DT=[1]min, AREA=[14.96](ha),
2467 *   XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2468 *   SCS curve number CN=[74],
2469 *   Pervious surfaces: IAper=[4.67](mm), SLPP=[0.5](%),
2470 *   LGP=[40](m), MNP=[0.25], SCP=[0](min),
2471 *   Impervious surfaces: IAimp=[1.57](mm), SLPI=[0.5](%),
2472 *   LGI=[315.806](m), MNI=[0.013], SCI=[0](min),
2473 *   Continuous simulation parameters:
2474 *   IaRECper=[4](hrs), IaRECimp=[4](hrs),
2475 *   SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2476 *   InterEventTime=[18](hrs), END=-1
2477 *%-----|-----|
2478 *CONTINUOUS NASHYD NHYD=["S-1-FO-F-D"], DT=[1]min, AREA=[14.96](ha),
2479 *   DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2480 *   N=[3], TP=[1.007]hrs,
2481 *   Continuous simulation parameters:
2482 *   IaRECper=[4](hrs),
2483 *   SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2484 *   InterEventTime=[12](hrs)
2485 *   Baseflow simulation parameters:
2486 *   BaseFlowOption=[1] ,

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2487 *          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2488 *          VHydCond=[0.055](mm/hr),   END=-1
2489 *%-----|-----|
2490 *COMPUTE DUALHYD  NHYDin=["S-1-FO-F-D"], CINLET=[1.749](cms), NINLET=[1],
2491 *                MajNHYD=["S-1FO-F-DJ"]
2492 *                MinNHYD=["S-1FO-F-DN"]
2493 *                TMJSTO=[9999999](cu-m)
2494 *%-----|-----|
2495 *ADD HYD          NHYDsum=["S-1FO-F-DS"], NHYDs to add=["S-1FO-F-DJ"+"S-1FO-F-DN"]
2496 *%-----|-----|
2497 *ROUTE RESERVOIR NHYDout=["S-1FO-F-DR"],NHYDin=["S-1FO-F-DS"],
2498 *                RDT=[1](min),
2499 *                TABLE of ( OUTFLOW-STORAGE ) values
2500 *                    (cms) - (ha-m)
2501 *                    [ 0.0      , 0.0 ]
2502 *                    [ 0.1788, 0.5966 ]
2503 *                    [   -1   , -1   ] (max twenty pts)
2504 *                NHYDovf=["S-1FoFDovf"]
2505 *%-----|-----|
2506 CONTINUOUS STANDHYD NHYD=["S-1-D1"], DT=[1](min), AREA=[21.67](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
2507 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
2508 IAper=[4.67](mm), SLPP=[2.0](%),
LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
2509 IAimp=[1.57](mm), SLPI=[0.75](%),
2510 LGI=[380.088](m), MNI=[0.013], SCI=[0](min),
2511 Continuous simulation parameters:
2512 IaRECper=[4](hrs), IaRECimp=[4](hrs),
2513 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2514 InterEventTime=[12](hrs),   END=-1
2515 *%-----|-----|
2516 *CONTINUOUS NASHYD  NHYD=["S-1-D1"], DT=[1]min, AREA=[21.67](ha),
2517 *                DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2518 *                N=[3], TP=[1.066]hrs,
2519 *                Continuous simulation parameters:
2520 *                IaRECper=[4](hrs),
2521 *                SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2522 *                InterEventTime=[12](hrs)
2523 *                Baseflow simulation parameters:
2524 *                BaseFlowOption=[1],
2525 *                InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2526 *                VHydCond=[0.055](mm/hr),   END=-1
2527 *%-----|-----|
2528 COMPUTE DUALHYD  NHYDin=["S-1-D1"], CINLET=[2.409](cms), NINLET=[1],
2529 *                MajNHYD=["S-1-D1J"]
2530 *                MinNHYD=["S-1-D1N"]
2531 *                TMJSTO=[9999999](cu-m)
2532 *%-----|-----|
2533 ADD HYD          NHYDsum=["S-1-D1S"], NHYDs to add=["S-1-D1J"+"S-1-D1N"]
2534 *%-----|-----|
2535 ROUTE RESERVOIR NHYDout=["S-1-D1R"],NHYDin=["S-1-D1S"],
2536 *                RDT=[1](min),
2537 *                TABLE of ( OUTFLOW-STORAGE ) values
2538 *                    (cms) - (ha-m)
2539 *                    [ 0.0      , 0.0 ]
2540 *                    [ 0.2590, 0.8642 ]
2541 *                    [   -1   , -1   ] (max twenty pts)
2542 *                NHYDovf=["S-1-D1Rovf"]
2543 *%-----|-----|
2544 *          -JFSA 2021-02-25 "S-1-D2" and "S-1-D3" are part of S-1 sub-catchment. They are
moved to drain before station 6215 on Jock River
2545 *CONTINUOUS STANDHYD NHYD=["S-1-D2"], DT=[1](min), AREA=[18.67](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
2546 *                LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
IAper=[4.67](mm), SLPP=[2.0](%),
2547 *                LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:

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IAimp=[1.57](mm), SLPI=[0.75](%),
2547 *          LGI=[352.798](m), MNI=[0.013], SCI=[0](min),
2548 *          Continuous simulation parameters:
2549 *          IaRECper=[4](hrs), IaRECimp=[4](hrs),
2550 *          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2551 *          InterEventTime=[12](hrs), END=-1
2552 *%-----|-----
2553 *CONTINUOUS NASHYD  NHYD=["S-1-D2"], DT=[1]min, AREA=[18.67](ha),
2554 *          DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2555 *          N=[3], TP=[1.120]hrs,
2556 *          Continuous simulation parameters:
2557 *          IaRECper=[4](hrs),
2558 *          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2559 *          InterEventTime=[12](hrs)
2560 *          Baseflow simulation parameters:
2561 *          BaseFlowOption=[1] ,
2562 *          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2563 *          VHydCond=[0.055](mm/hr), END=-1
2564 *%-----|-----
2565 *COMPUTE DUALHYD  NHYDin=["S-1-D2"], CINLET=[2.062](cms), NINLET=[1],
2566 *          MajNHYD=["S-1-D2J"]
2567 *          MinNHYD=["S-1-D2N"]
2568 *          TMJSTO=[9999999](cu-m)
2569 *%-----|-----
2570 *ADD HYD          NHYDsum=["S-1-D2S"], NHYDs to add=["S-1-D2J"+"S-1-D2N"]
2571 *%-----|-----
2572 *ROUTE RESERVOIR  NHYDout=["S-1-D2R"], NHYDin=["S-1-D2S"],
2573 *          RDT=[1](min),
2574 *          TABLE of ( OUTFLOW-STORAGE ) values
2575 *                   (cms) - (ha-m)
2576 *                   [ 0.0      , 0.0 ]
2577 *                   [ 0.2231, 0.7445 ]
2578 *                   [   -1   ,  -1   ] (max twenty pts)
2579 *          NHYDovf=["S-1-D2Rovf"]
2580 *%-----|-----
2581 *CONTINUOUS STANDHYD NHYD=["S-1-D3"], DT=[1](min), AREA=[6.79](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
2582 *          LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
IAper=[4.67](mm), SLPP=[2.0](%),
2583 *          LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
2584 *          LGI=[212.760](m), MNI=[0.013], SCI=[0](min),
2585 *          Continuous simulation parameters:
2586 *          IaRECper=[4](hrs), IaRECimp=[4](hrs),
2587 *          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2588 *          InterEventTime=[12](hrs), END=-1
2589 *%-----|-----
2590 *CONTINUOUS NASHYD  NHYD=["S-1-D3"], DT=[1]min, AREA=[6.79](ha),
2591 *          DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2592 *          N=[3], TP=[1.281]hrs,
2593 *          Continuous simulation parameters:
2594 *          IaRECper=[4](hrs),
2595 *          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2596 *          InterEventTime=[12](hrs)
2597 *          Baseflow simulation parameters:
2598 *          BaseFlowOption=[1] ,
2599 *          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2600 *          VHydCond=[0.055](mm/hr), END=-1
2601 *%-----|-----
2602 *COMPUTE DUALHYD  NHYDin=["S-1-D3"], CINLET=[0.719](cms), NINLET=[1],
2603 *          MajNHYD=["S-1-D3J"]
2604 *          MinNHYD=["S-1-D3N"]
2605 *          TMJSTO=[9999999](cu-m)
2606 *%-----|-----
2607 *ADD HYD          NHYDsum=["S-1-D3S"], NHYDs to add=["S-1-D3J"+"S-1-D3N"]
2608 *%-----|-----

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2609 *ROUTE RESERVOIR      NHYDout=["S-1-D3R"] ,NHYDin=["S-1-D3S"] ,
2610 *                      RDT=[1](min),
2611 *                      TABLE of ( OUTFLOW-STORAGE ) values
2612 *                      (cms) - (ha-m)
2613 *                      [ 0.0      , 0.0 ]
2614 *                      [ 0.0811, 0.2708 ]
2615 *                      [   -1   ,  -1   ] (max twenty pts)
2616 *                      NHYDovf=["S-1-D3Rovf"]
2617 *%-----|-----
2618 CONTINUOUS STANDHYD NHYD=["S-1-D4"], DT=[1](min), AREA=[3.28](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
2619 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
IAper=[4.67](mm), SLPP=[2.0](%),
2620 LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
2621 LGI=[147.874](m), MNI=[0.013], SCI=[0](min),
2622 Continuous simulation parameters:
2623 IaRECper=[4](hrs), IaRECimp=[4](hrs),
2624 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2625 InterEventTime=[12](hrs), END=-1
2626 *%-----|-----
2627 *CONTINUOUS NASHYD    NHYD=["S-1-D4"], DT=[1]min, AREA=[3.28](ha),
2628 *                      DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2629 *                      N=[3], TP=[1.10]hrs,
2630 *                      Continuous simulation parameters:
2631 *                      IaRECper=[4](hrs),
2632 *                      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2633 *                      InterEventTime=[12](hrs)
2634 *                      Baseflow simulation parameters:
2635 *                      BaseFlowOption=[1] ,
2636 *                      InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2637 *                      VHydCond=[0.055](mm/hr), END=-1
2638 *%-----|-----
2639 COMPUTE DUALHYD    NHYDin=["S-1-D4"], CINLET=[0.421](cms), NINLET=[1],
2640 *                      MajNHYD=["S-1-D4J"]
2641 *                      MinNHYD=["S-1-D4N"]
2642 *                      TMJSTO=[9999999](cu-m)
2643 *%-----|-----
2644 ADD HYD           NHYDsum=["S-1-D4S"], NHYDs to add=["S-1-D4J"+"S-1-D4N"]
2645 *%-----|-----
2646 ROUTE RESERVOIR  NHYDout=["S-1-D4R"] ,NHYDin=["S-1-D4S"] ,
2647 *                      RDT=[1](min),
2648 *                      TABLE of ( OUTFLOW-STORAGE ) values
2649 *                      (cms) - (ha-m)
2650 *                      [ 0.0      , 0.0 ]
2651 *                      [ 0.0392, 0.1308 ]
2652 *                      [   -1   ,  -1   ] (max twenty pts)
2653 *                      NHYDovf=["S-1-D4Rovf"]
2654 *%-----|-----
2655 CONTINUOUS STANDHYD NHYD=["S-1-D5"], DT=[1](min), AREA=[12.84](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
2656 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
IAper=[4.67](mm), SLPP=[2.0](%),
2657 LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
2658 LGI=[292.57](m), MNI=[0.013], SCI=[0](min),
2659 Continuous simulation parameters:
2660 IaRECper=[4](hrs), IaRECimp=[4](hrs),
2661 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2662 InterEventTime=[12](hrs), END=-1
2663 *%-----|-----
2664 *CONTINUOUS NASHYD    NHYD=["S-1-D5"], DT=[1]min, AREA=[12.84](ha),
2665 *                      DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2666 *                      N=[3], TP=[1.10]hrs,
2667 *                      Continuous simulation parameters:
2668 *                      IaRECper=[4](hrs),

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2669 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2670 * InterEventTime=[12](hrs)
2671 * Baseflow simulation parameters:
2672 * BaseFlowOption=[1] ,
2673 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2674 * VHydCond=[0.055](mm/hr), END=-1
2675 *%-----|-----
2676 COMPUTE DUALHYD NHYDin=["S-1-D5"], CINLET=[1.5](cms), NINLET=[1],
2677 MajNHYD=["S-1-D5J"]
2678 MinNHYD=["S-1-D5N"]
2679 TMJSTO=[9999999](cu-m)
2680 *%-----|-----
2681 ADD HYD NHYDsum=["S-1-D5S"], NHYDs to add=["S-1-D5J"+"S-1-D5N"]
2682 *%-----|-----
2683 ROUTE RESERVOIR NHYDout=["S-1-D5R"],NHYDin=["S-1-D5S"] ,
2684 RDT=[1](min),
2685 TABLE of ( OUTFLOW-STORAGE ) values
2686 (cms) - (ha-m)
2687 [ 0.0 , 0.0 ]
2688 [ 0.1535, 0.5120 ]
2689 [ -1 , -1 ] (max twenty pts)
2690 NHYDovf=["S-1-D5Rovf"]
2691 *%-----|-----
2692 CONTINUOUS STANDHYD NHYD=["S-1-D6"], DT=[1](min), AREA=[1.75](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
2693 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
2694 IAper=[4.67](mm), SLPP=[2.0](%),
LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
2695 IAimp=[1.57](mm), SLPI=[0.75](%),
2696 LGI=[108.01](m), MNI=[0.013], SCI=[0](min),
2697 Continuous simulation parameters:
2698 IaREcper=[4](hrs), IaREcimp=[4](hrs),
2699 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
InterEventTime=[12](hrs), END=-1
2700 *%-----|-----
2701 *CONTINUOUS NASHYD NHYD=["S-1-D6"], DT=[1]min, AREA=[1.75](ha),
2702 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2703 N=[3], TP=[1.10]hrs,
2704 Continuous simulation parameters:
2705 IaREcper=[4](hrs),
2706 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2707 InterEventTime=[12](hrs)
2708 Baseflow simulation parameters:
2709 BaseFlowOption=[1] ,
2710 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2711 VHydCond=[0.055](mm/hr), END=-1
2712 *%-----|-----
2713 COMPUTE DUALHYD NHYDin=["S-1-D6"], CINLET=[0.232](cms), NINLET=[1],
2714 MajNHYD=["S-1-D6J"]
2715 MinNHYD=["S-1-D6N"]
2716 TMJSTO=[9999999](cu-m)
2717 *%-----|-----
2718 ADD HYD NHYDsum=["S-1-D6S"], NHYDs to add=["S-1-D6J"+"S-1-D6N"]
2719 *%-----|-----
2720 ROUTE RESERVOIR NHYDout=["S-1-D6R"],NHYDin=["S-1-D6S"] ,
2721 RDT=[1](min),
2722 TABLE of ( OUTFLOW-STORAGE ) values
2723 (cms) - (ha-m)
2724 [ 0.0 , 0.0 ]
2725 [ 0.0209, 0.0698 ]
2726 [ -1 , -1 ] (max twenty pts)
2727 NHYDovf=["S-1-D6Rovf"]
2728 *%-----|-----
2729 CONTINUOUS STANDHYD NHYD=["S-1-D7"], DT=[1](min), AREA=[2.03](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
2730 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:

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2731 IAper=[4.67](mm), SLPP=[2.0](%),
LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
2732 IAimp=[1.57](mm), SLPI=[0.75](%),
2733 LGI=[116.33](m), MNI=[0.013], SCI=[0](min),
2734 Continuous simulation parameters:
2735 IaREcper=[4](hrs), IaREcimp=[4](hrs),
2736 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2737 InterEventTime=[12](hrs), END=-1
2738 *%-----|-----
2738 *CONTINUOUS NASHYD NHYD=["S-1-D7"], DT=[1]min, AREA=[2.03](ha),
2739 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2740 * N=[3], TP=[1.10]hrs,
2741 * Continuous simulation parameters:
2742 * IaREcper=[4](hrs),
2743 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2744 * InterEventTime=[12](hrs)
2745 * Baseflow simulation parameters:
2746 * BaseFlowOption=[1] ,
2747 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2748 * VHydCond=[0.055](mm/hr), END=-1
2749 *%-----|-----
2750 COMPUTE DUALHYD NHYDin=["S-1-D7"], CINLET=[0.265](cms), NINLET=[1],
2751 MajNHYD=["S-1-D7J"]
2752 MinNHYD=["S-1-D7N"]
2753 TMJSTO=[9999999](cu-m)
2754 *%-----|-----
2755 ADD HYD NHYDsum=["S-1-D7S"], NHYDs to add=["S-1-D7J"+"S-1-D7N"]
2756 *%-----|-----
2757 ROUTE RESERVOIR NHYDout=["S-1-D7R"],NHYDin=["S-1-D7S"] ,
2758 RDT=[1](min),
2759 TABLE of ( OUTFLOW-STORAGE ) values
2760 (cms) - (ha-m)
2761 [ 0.0 , 0.0 ]
2762 [ 0.0243, 0.0810 ]
2763 [ -1 , -1 ] (max twenty pts)
2764 NHYDovf=["S-1-D7Rovf"]
2765 *%-----|-----
2766 * -JFSA 2021-02-26 "S-1-D8" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2767 *CONTINUOUS STANDHYD NHYD=["S-1-D8"], DT=[1](min), AREA=[5.27](ha), XIMP=[0.65],
TIMP=[0.65], DWF=[0](cms),
2768 * LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
2769 IAper=[4.67](mm), SLPP=[2.0](%),
2770 * LGI=[187.439](m), MNI=[0.013], SCI=[0](min),
2771 * Continuous simulation parameters:
2772 * IaREcper=[4](hrs), IaREcimp=[4](hrs),
2773 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2774 * InterEventTime=[12](hrs), END=-1
2775 *%-----|-----
2776 *CONTINUOUS NASHYD NHYD=["S-1-D8"], DT=[1]min, AREA=[5.27](ha),
2777 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2778 * N=[3], TP=[1.10]hrs,
2779 * Continuous simulation parameters:
2780 * IaREcper=[4](hrs),
2781 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2782 * InterEventTime=[12](hrs)
2783 * Baseflow simulation parameters:
2784 * BaseFlowOption=[1] ,
2785 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2786 * VHydCond=[0.055](mm/hr), END=-1
2787 *%-----|-----
2788 *COMPUTE DUALHYD NHYDin=["S-1-D8"], CINLET=[2.279](cms), NINLET=[1],
2789 * MajNHYD=["S-1-D8J"]
2790 * MinNHYD=["S-1-D8N"]

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2791 *          TMJSTO=[9999999](cu-m)
2792 *%-----|-----|
2793 *ADD HYD          NHYDsum=["S-1-D8S"], NHYDs to add=["S-1-D8J"+"S-1-D8N"]
2794 *%-----|-----|
2795 *ADD HYD          NHYDsum=["S-1-D"], NHYDs to add=["S-1-Okeefe"+"S-1"+"S-1-Fost"]
2796 *%-----|-----|
2797 *COMPUTE DUALHYD  NHYDin=["S-1-D"], CINLET=[11.616](cms), NINLET=[1],
2798 *                MajNHYD=["S-1-D-MJ"]
2799 *                MinNHYD=["S-1-D-MN"]
2800 *                TMJSTO=[5974](cu-m)
2801 *%-----|-----|
2802 *ADD HYD          NHYDsum=["S-1-DEV"], NHYDs to add=["S-1-D-MJ"+"S-1-D-MN"]
2803 *%-----|-----|
2804 *ROUTE RESERVOIR  NHYDout=["S-1-D8R"], NHYDin=["S-1-D8S"],
2805 *                RDT=[1](min),
2806 *                TABLE of ( OUTFLOW-STORAGE ) values
2807 *                    (cms) - (ha-m)
2808 *                    [ 0.0      , 0.0 ]
2809 *                    [ 0.0630, 0.2102 ]
2810 *                    [   -1   ,  -1   ] (max twenty pts)
2811 *                NHYDovf=["S-1-D8Rovf"]
2812 *%-----|-----|
2813 *%-----|-----|
2814 *          -JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
(W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
2815 *#    Catchment W_CLAR
2816 *#    - To West Clarke Drain (south of the Jock)
2817 *#    - Subdivision with 43% imp. as per Barrhaven South MSS
2818 *#    - 2020-11-30 update CLARKE Tributary Drainage Area to = 121 ha based on
P598(04)-11
2819 *#    - 2020-11-30 split CLARKE Drainage Area to MAJOR and ALL
2820 *#*****
2821 CONTINUOUS STANDHYD NHYD=["W_CLAR_MJ"], DT=[1]min, AREA=[1.772](ha),
2822 XIMP=[0.46], TIMP=[0.59], DWF=[0](cms), LOSS=[2],
2823 SCS curve number CN=[77],
2824 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
2825 LGP=[40](m), MNP=[0.25], SCP=[0](min),
2826 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
2827 LGI=[109](m), MNI=[0.013], SCI=[0](min),
2828 Continuous simulation parameters:
2829 IaRECper=[4](hrs), IaRECimp=[4](hrs),
2830 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2831 InterEventTime=[18](hrs), END=-1
2832 *%-----|-----|
2833 *COMPUTE DUALHYD  NHYDin=["W_CLAR_MJ"], CINLET=[0.213](cms), NINLET=[1],
2834 *                MajNHYD=["W_CLAR_MJj"]
2835 *                MinNHYD=["W_CLAR_MJn"]
2836 *                TMJSTO=[0.1](cu-m)
2837 *%-----|-----|
2838 *# 5-Year + 12% Capture
2839 ROUTE RESERVOIR NHYDout=["W_CLAR_MJn"], NHYDin=["W_CLAR_MJ"],
2840 RDT=[1](min),
2841 TABLE of ( OUTFLOW-STORAGE ) values
2842 (cms) - (ha-m)
2843 [ 0.0      , 0.0 ]
2844 [ 0.213   , 0.0001 ]
2845 [   -1   ,  -1   ] (max twenty pts)
2846 NHYDovf=["W_CLAR_MJj"],
2847 *%-----|-----|
2848 *          -Clarke_All area from P 598(04)-11 = 120.207 ha, change to 127.298 ha based on
GIS measurements,
2849 *          -JFSA, 2021-01-19 update W_CLAR_ALL to (121.17-1.772=119.398) ha based on GIS
measurements W_CLAR is 121.17 ha and W_CLAR_MJ is 1.772 ha
2850 CONTINUOUS STANDHYD NHYD=["W_CLAR_ALL"], DT=[1]min, AREA=[119.398](ha),
2851 XIMP=[0.60], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
2852 SCS curve number CN=[77],

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2853 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
2854 LGP=[40](m), MNP=[0.25], SCP=[0](min),
2855 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
2856 LGI=[892.18](m), MNI=[0.013], SCI=[0](min),
2857 Continuous simulation parameters:
2858 IaREcper=[4](hrs), IaREcimp=[4](hrs),
2859 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2860 InterEventTime=[18](hrs), END=-1
2861 *%-----|-----|
2862 ADD HYD NHYDsum=["W_CLAR"], NHYDs to add=["W_CLAR_ALL"+"W_CLAR_MJj"]
2863 *%-----|-----|
2864 SAVE HYD NHYD=["W_CLAR"], # OF PCYCLES=[-1], ICASEsh=[1]
2865 HYD_COMMENT=["Total Flows to West Clarke"]
2866 *#*****
2867 *# West Clarke Pond 2
2868 *# - Rating curve obtained from Barrhaven South MSS modeling
2869 *# - Tributary Drainage Area to MSS Pond 2 = 241 ha
2870 *#*****
2871 ROUTE RESERVOIR NHYDout=["MS_P2"], NHYDin=["W_CLAR"],
2872 RDT=[1](min),
2873 TABLE of ( OUTFLOW-STORAGE ) values
2874 (cms) - (ha-m)
2875 [ 0.0 , 0.0 ]
2876 [ 0.128 , 0.161 ]
2877 [ 0.138 , 0.409 ]
2878 [ 0.148 , 0.68 ]
2879 [ 0.227 , 0.931 ]
2880 [ 0.354 , 1.223 ]
2881 [ 0.505 , 1.52 ]
2882 [ 0.666 , 1.821 ]
2883 [ 0.831 , 2.123 ]
2884 [ 0.995 , 2.434 ]
2885 [ 1.069 , 2.583 ]
2886 [ 1.51 , 2.647 ]
2887 [ 4.904 , 2.861 ]
2888 [ 13.048 , 3.188 ]
2889 [ 23.745 , 3.523 ]
2890 [ 36.474 , 3.871 ]
2891 [ 45.938 , 4.127 ]
2892 [ 61.652 , 4.539 ]
2893 [ -1 , -1 ] (max twenty pts)
2894 NHYDovf=["P2-OVF"]
2895 *%-----|-----|
2896 *#*****
2897 * -JFSA, 2021-01-22 "W_CLAR_UNDE" (west of Clarke sub-catchment) discharges
directly to the jock river through a road side ditch on the west side of Borrisokane
road (station 6016)
2898 *CONTINUOUS NASHYD NHYD=["W_CLAR_UNDE"], DT=[1]min, AREA=[35.65](ha),
2899 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
2900 * N=[3], TP=[1.10]hrs,
2901 * Continuous simulation parameters:
2902 * IaREcper=[4](hrs),
2903 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2904 * InterEventTime=[12](hrs)
2905 * Baseflow simulation parameters:
2906 * BaseFlowOption=[1] ,
2907 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2908 * VHydCond=[0.055](mm/hr), END=-1
2909 *%-----|-----|
2910 ADD HYD NHYDsum=["SN_CE"], NHYDs to
add=["N_CE"+"S-1-D4R"+"S-1-D5R"+"S-1-D4Rovf"+"S-1-D5Rovf"+"MS_P2"+"P2-OVF"]
2911 *%-----|-----|
2912 SAVE HYD NHYD=["SN_CE"], # OF PCYCLES=[-1], ICASEsh=[1]
2913 HYD_COMMENT=["Total Flows before Station 5737 on Jock River"]
2914 *%-----|-----|
2915 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5737

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2916  *# 2021-02-25 add station 5737 before station 5002. Station 5737 was extracted from the
HEC-RAS model
T:\PROJ\1474-16\Design\20201026-QuantityControlAnalysis\HEC-RAS\JockLidar2005
2917  *# JFSA 2021-03-02 change the slope to 0.0175% instead of 0.02593 to stabilize the model
2918  ROUTE CHANNEL      NHYDout=["5737"] ,NHYDin=["SN_CE"] ,
2919                      RDT=[1](min),
2920                      CHLGTH=[270](m),   CHSLOPE=[0.0175](%),
2921                      FPSLOPE=[0.0175](%),
2922                      SECNUM=[1.0],      NSEG=[3]
2923                      ( SEGROUGH, SEGDIST (m))=
2924                      [0.050,-24.04
2925                      -0.035,23.92
2926                      0.050,1130.8] NSEG times
2927                      ( DISTANCE (m), ELEVATION (m))=
2928                      [-1060.52, 94 ]
2929                      [-268.6, 91.5 ]
2930                      [-259.43, 91.5 ]
2931                      [-179.48, 91.5 ]
2932                      [-67.9, 91.5 ]
2933                      [-59.21, 91.5 ]
2934                      [-33.19, 91 ]
2935                      [-26.08, 90.5 ]
2936                      [-24.04, 90 ]
2937                      [-13.14, 86.77 ]
2938                      [0, 85 ]
2939                      [14.68, 86.74 ]
2940                      [23.92, 90 ]
2941                      [25.78, 90.5 ]
2942                      [31.91, 91 ]
2943                      [91.95, 91.5 ]
2944                      [772.15, 92 ]
2945                      [961.49, 92.5 ]
2946                      [1044.69, 93 ]
2947                      [1130.8, 95 ]
2948  *%-----|-----|
2949  ADD HYD          NHYDsum=["5002"], NHYDs to
add=["5737"+"S-1-D1R"+"S-1-D6R"+"S-1-D7R"+"S-1-D1Rovf"+"S-1-D6Rovf"+"S-1-D7Rovf"]
2950  *%-----|-----|
2951  SAVE HYD        NHYD=["5002"],   # OF PCYCLES=[-1],   ICASEsh=[1]
2952                  HYD_COMMENT=["Total Flows before Station 5002 on Jock River"]
2953  *%-----|-----|
2954  *# Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain
2955  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5002
2956  *# JFSA 2021-02-19 Change the slope from 0.01 % (as per Stantec Report 2007) to 0.0255
% so the model will be more stable and give reasonable results. It is justifiable as
ROUTE CHANNELs aren't well suited to really flat slopes.
2957  *# JFSA 2021-02-19 Change to three ROUTE CHANNEL with length 275 m each instead of one
with 825 m length so the model will be more stable
2958  *# JFSA 2021-02-26 change the length of 5002 route channel from 825 m to 736 m. That is
because of adding station 5737 between station 6016 and station 5002. Then the length
from station 5737 to station 5002 is 736 m. Change the slope from 0.0255 % to 0.09511 %
2959  *
2960  ROUTE CHANNEL    NHYDout=["N_WCa"] ,NHYDin=["5002"] ,
2961                  RDT=[1](min),
2962                  CHLGTH=[245.33333](m),   CHSLOPE=[0.09511](%),
2963                  FPSLOPE=[0.09511](%),
2964                  SECNUM=[1.0],      NSEG=[3]
2965                  ( SEGROUGH, SEGDIST (m))=
2966                  [0.050,-37.5
2967                  -0.035,37.50
2968                  0.050,157.05] NSEG times
2969                  ( DISTANCE (m), ELEVATION (m))=
2970                  [-601.81, 91.5]
2971                  [-37.50, 90.00]
2972                  [-19.61, 87.04]
2973                  [0.00, 85.70]

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2974      [14.87, 86.93]
2975      [37.50, 90.00]
2976      [38.54, 90.50]
2977      [42.23, 91]
2978      [157.05,91.50]
2979      *      [161.44, 91.50]
2980      *      [236.48, 93.00]
2981      *      [385.47, 92.50]
2982      *      [390.78, 92.50]
2983      *%-----|-----
2984      ROUTE CHANNEL      NHYDout=["N_WCb"] ,NHYDin=["N_WCa"] ,
2985      RDT=[1](min),
2986      CHLGTH=[245.33333](m),   CHSLOPE=[0.09511](%),
2987      FPSLOPE=[0.09511](%),
2988      SECNUM=[1.0],          NSEG=[3]
2989      ( SEGROUGH, SEGDIST (m))=
2990      [0.050,-37.5
2991      -0.035,37.50
2992      0.050,157.05] NSEG times
2993      ( DISTANCE (m), ELEVATION (m))=
2994      [-601.81, 91.5]
2995      [-37.50, 90.00]
2996      [-19.61, 87.04]
2997      [0.00, 85.70]
2998      [14.87, 86.93]
2999      [37.50, 90.00]
3000      [38.54, 90.50]
3001      [42.23, 91]
3002      [157.05,91.50]
3003      *%-----|-----
3004      ROUTE CHANNEL      NHYDout=["N_WC"] ,NHYDin=["N_WCb"] ,
3005      RDT=[1](min),
3006      CHLGTH=[245.33333](m),   CHSLOPE=[0.09511](%),
3007      FPSLOPE=[0.09511](%),
3008      SECNUM=[1.0],          NSEG=[3]
3009      ( SEGROUGH, SEGDIST (m))=
3010      [0.050,-37.5
3011      -0.035,37.50
3012      0.050,157.05] NSEG times
3013      ( DISTANCE (m), ELEVATION (m))=
3014      [-601.81, 91.5]
3015      [-37.50, 90.00]
3016      [-19.61, 87.04]
3017      [0.00, 85.70]
3018      [14.87, 86.93]
3019      [37.50, 90.00]
3020      [38.54, 90.50]
3021      [42.23, 91]
3022      [157.05,91.50]
3023      *#*****
3024      *      -JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
(W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
3025      *ADD HYD      NHYDsum=["SN_WC"], NHYDs to
add=["MS_P2"+"P2-OVF"+"N_WC"+"W_CLAR_UNDE"]
3026      *%-----|-----
3027      *SAVE HYD      NHYD=["SN_WC"], # OF PCYCLES=[-1], ICASEsh=[1]
3028      *      HYD_COMMENT=["Total Flows at West Clarke Pond Outlet"]
3029      *%-----|-----
3030      *# Hydrograph from Node West Clarke routed to Node at Kennedy - Burnett Drain
3031      *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4534
3032      *#
3033      ROUTE CHANNEL      NHYDout=["N_KB"] ,NHYDin=["N_WC"] ,
3034      RDT=[1](min),
3035      CHLGTH=[1020](m),   CHSLOPE=[0.0498](%),
3036      FPSLOPE=[0.0498](%),
3037      SECNUM=[1.0],          NSEG=[3]

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3038      ( SEGROUGH, SEGDIST (m))=
3039      [0.050,-23.63
3040      -0.035,23.63
3041      0.050,728.3] NSEG times
3042      ( DISTANCE (m), ELEVATION (m))=
3043      [-1082.01,94]
3044      [-1028.17,92.5]
3045      [-992.3,93.5]
3046      [-279.34,90]
3047      [-23.63,90]
3048      [-13.45,87.13]
3049      [-0.07,86.24]
3050      [10.54,87.15]
3051      [23.63,90]
3052      [24.86,90.5]
3053      [26.72,91]
3054      [45.07,91.5]
3055      [128.17,91.5]
3056      [270.7,92.5]
3057      [728.3,95]
3058      *%-----|-----|
3059      *#*****|
3060      *#      Catchment KEN_BU
3061      *#      - To Kennedy-Burnett SWM Facility
3062      *#      - Outlets to Fraser-Clarke drain (north of the Jock)
3063      *#      - Medium density residential subdivision
3064      *      - Add Kennedy Burnett model (Convert PCSWMM from NOVATECH June, 2020 to SWMHYMO)
3065      *#*****|
3066      *CONTINUOUS STANDHYD NHYD=["KEN_BU"], DT=[1]min, AREA=[281](ha),
3067      *          XIMP=[0.55], TIMP=[0.55], DWF=[0](cms), LOSS=[2],
3068      *          SCS curve number CN=[71],
3069      *          Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3070      *          LGP=[40](m), MNP=[0.25], SCP=[0](min),
3071      *          Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3072      *          LGI=[1369](m), MNI=[0.013], SCI=[0](min),
3073      *          Continuous simulation parameters:
3074      *          IaRECper=[4](hrs), IaRECimp=[4](hrs),
3075      *          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3076      *          InterEventTime=[18](hrs), END=-1
3077      *%-----|-----|
3078      *#*****|
3079      *#      Existing Kennedy-Burnett SWM Facility
3080      *#      - Rating curve obtained from URTKBP
3081      *#      - Tributary Drainage Area to Pond = 160 ha
3082      *#*****|
3083      *ROUTE RESERVOIR      NHYDout=["KEN_P"], NHYDin=["KEN_BU"],
3084      *          RDT=[1](min),
3085      *          TABLE of ( OUTFLOW-STORAGE ) values
3086      *          (cms) - (ha-m)
3087      *          [ 0.0 , 0.0 ]
3088      *          [ 0.13 , 0.26]
3089      *          [ 0.43 , 0.56]
3090      *          [ 0.67 , 0.90]
3091      *          [ 0.86 , 1.32]
3092      *          [ 1.01 , 1.79]
3093      *          [ 1.15 , 2.33]
3094      *          [ -1 , -1 ] (max twenty pts)
3095      *          NHYDovf=["KEN-OV"]
3096      *%-----|-----|
3097      *      -JFSA, 2021-01-19 update all KEN_BU areas based on GIS measurements
3098      CONTINUOUS STANDHYD NHYD=["KB-01A"], DT=[1]min, AREA=[40.82](ha), XIMP=[0.097],
3099      TIMP=[0.4], DWF=[0](cms), LOSS=[1]:
3099      Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3100      F=[0.00](mm),
3100      Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[40](m),
3100      MNP=[0.250], SCP=[0](min),

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3101      Impervious areas: IAimp=[0.785](mm), SLPI=[0.5](%),
3102      LGI=[521.664](m), MNI=[0.013], SCI=[0](min),
3103      Continuous simulation parameters:
3103      IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
3103      END=-1
3104      *%-----|-----|
3105      COMPUTE DUALHYD      NHYDin=["KB-01A"], CINLET=[3.6](cms), NINLET=[1],
3106      MajNHYD=["KB-01A-MJ"]
3107      MinNHYD=["KB-01A-MN"]
3108      TMJSTO=[4995](cu-m)
3109      *%-----|-----|
3110      ADD HYD              NHYDsum=["KB-01A-S"], NHYDs to add=["KB-01A-MJ"+"KB-01A-MN"]
3111      *%-----|-----|
3112      CONTINUOUS STANDHYD NHYD=["KB-01B"], DT=[1]min, AREA=[31.1](ha), XIMP=[0.1875],
3112      TIMP=[0.375], DWF=[0](cms), LOSS=[1]:
3113      Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3113      F=[0.00](mm),
3114      Pervious areas: IAper=[4.67](mm), SLPP=[0.42](%), LGP=[40](m),
3114      MNP=[0.250], SCP=[0](min),
3115      Impervious areas: IAimp=[0.785](mm), SLPI=[0.42](%),
3115      LGI=[455.339](m), MNI=[0.013], SCI=[0](min),
3116      Continuous simulation parameters:
3117      IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
3117      END=-1
3118      *%-----|-----|
3119      COMPUTE DUALHYD      NHYDin=["KB-01B"], CINLET=[1.585](cms), NINLET=[1],
3120      MajNHYD=["KB-01B-MJ"]
3121      MinNHYD=["KB-01B-MN"]
3122      TMJSTO=[6075](cu-m)
3123      *%-----|-----|
3124      ADD HYD              NHYDsum=["KB-01B-S"], NHYDs to add=["KB-01B-MJ"+"KB-01B-MN"]
3125      *%-----|-----|
3126      CONTINUOUS STANDHYD NHYD=["KB-01C"], DT=[1]min, AREA=[13.78](ha), XIMP=[0.2045],
3126      TIMP=[0.409], DWF=[0](cms), LOSS=[1]:
3127      Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3127      F=[0.00](mm),
3128      Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3128      MNP=[0.250], SCP=[0](min),
3129      Impervious areas: IAimp=[0.785](mm), SLPI=[0.5](%),
3129      LGI=[303.095](m), MNI=[0.013], SCI=[0](min),
3130      Continuous simulation parameters:
3131      IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
3131      END=-1
3132      *%-----|-----|
3133      COMPUTE DUALHYD      NHYDin=["KB-01C"], CINLET=[1.35](cms), NINLET=[1],
3134      MajNHYD=["KB-01C-MJ"]
3135      MinNHYD=["KB-01C-MN"]
3136      TMJSTO=[1880](cu-m)
3137      *%-----|-----|
3138      ADD HYD              NHYDsum=["KB-01C-S"], NHYDs to add=["KB-01C-MJ"+"KB-01C-MN"]
3139      *%-----|-----|
3140      CONTINUOUS STANDHYD NHYD=["KB-03"], DT=[1]min, AREA=[84.78](ha), XIMP=[0.197],
3140      TIMP=[0.394], DWF=[0](cms), LOSS=[1]:
3141      Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3141      F=[0.00](mm),
3142      Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3142      MNP=[0.250], SCP=[0](min),
3143      Impervious areas: IAimp=[0.785](mm), SLPI=[0.63](%),
3143      LGI=[751.798](m), MNI=[0.013], SCI=[0](min),
3144      Continuous simulation parameters:
3145      IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
3145      END=-1
3146      *%-----|-----|
3147      COMPUTE DUALHYD      NHYDin=["KB-03"], CINLET=[5.27](cms), NINLET=[1],
3148      MajNHYD=["KB-03-MJ"]
3149      MinNHYD=["KB-03-MN"]

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3150          TMJSTO=[15500](cu-m)
3151  *%-----|-----|
3152  ADD HYD      NHYDsum=["KB-03-S"], NHYDs to add=["KB-03-MJ"+"KB-03-MN"]
3153  *%-----|-----|
3154  CONTINUOUS STANDHYD NHYD=["KB-04"], DT=[1]min, AREA=[6.95](ha), XIMP=[0.85],
TIMP=[0.85], DWF=[0](cms), LOSS=[1]:
3155          Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3156          Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3157          Impervious areas: IAimp=[0.942](mm), SLPI=[0.5](%),
LGI=[215.252](m), MNI=[0.013], SCI=[0](min),
3158          Continuous simulation parameters:
3159          IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3160  *%-----|-----|
3161  COMPUTE DUALHYD NHYDin=["KB-04"], CINLET=[0.503](cms), NINLET=[1],
3162          MajNHYD=["KB-04-MJ"]
3163          MinNHYD=["KB-04-MN"]
3164          TMJSTO=[1972](cu-m)
3165  *%-----|-----|
3166  ADD HYD      NHYDsum=["KB-04-S"], NHYDs to add=["KB-04-MJ"+"KB-04-MN"]
3167  *%-----|-----|
3168  CONTINUOUS STANDHYD NHYD=["KB-05"], DT=[1]min, AREA=[5.19](ha), XIMP=[0.93],
TIMP=[0.93], DWF=[0](cms), LOSS=[1]:
3169          Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3170          Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3171          Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[186.011](m), MNI=[0.013], SCI=[0](min),
3172          Continuous simulation parameters:
3173          IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3174  *%-----|-----|
3175  *%-----|-----|
3176  CONTINUOUS STANDHYD NHYD=["KB-06"], DT=[1]min, AREA=[12.93](ha), XIMP=[0.873],
TIMP=[0.873], DWF=[0](cms), LOSS=[1]:
3177          Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3178          Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3179          Impervious areas: IAimp=[0.942](mm), SLPI=[4.75](%),
LGI=[293.598](m), MNI=[0.013], SCI=[0](min),
3180          Continuous simulation parameters:
3181          IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3182  *%-----|-----|
3183  COMPUTE DUALHYD NHYDin=["KB-06"], CINLET=[2.262](cms), NINLET=[1],
3184          MajNHYD=["KB-06-MJ"]
3185          MinNHYD=["KB-06-MN"]
3186          TMJSTO=[1950](cu-m)
3187  *%-----|-----|
3188  ADD HYD      NHYDsum=["KB-06-S"], NHYDs to add=["KB-06-MJ"+"KB-06-MN"]
3189  *%-----|-----|
3190  CONTINUOUS STANDHYD NHYD=["KB-11"], DT=[1]min, AREA=[4.03](ha), XIMP=[0.675],
TIMP=[0.675], DWF=[0](cms), LOSS=[1]:
3191          Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3192          Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3193          Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%),
LGI=[163.911](m), MNI=[0.013], SCI=[0](min),
3194          Continuous simulation parameters:
3195          IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1

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3196 *%-----|-----|
3197 COMPUTE DUALHYD NHYDin=["KB-11"], CINLET=[0.5773](cms), NINLET=[1],
3198 MajNHYD=["KB-11-MJ"]
3199 MinNHYD=["KB-11-MN"]
3200 TMJSTO=[597](cu-m)
3201 *%-----|-----|
3202 ADD HYD NHYDsum=["KB-11-S"], NHYDs to add=["KB-11-MJ"+"KB-11-MN"]
3203 *%-----|-----|
3204 CONTINUOUS STANDHYD NHYD=["S1"], DT=[1]min, AREA=[4.99](ha), XIMP=[0.93], TIMP=[0.93],
DWF=[0](cms), LOSS=[1]:
3205 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3206 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3207 Impervious areas: IAimp=[1.57](mm), SLPI=[2.0](%),
LGI=[182.392](m), MNI=[0.013], SCI=[0](min),
3208 Continuous simulation parameters:
3209 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3210 *%-----|-----|
3211 CONTINUOUS STANDHYD NHYD=["KB-15"], DT=[1]min, AREA=[2.15](ha), XIMP=[0.79],
TIMP=[0.79], DWF=[0](cms), LOSS=[1]:
3212 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3213 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3214 Impervious areas: IAimp=[0.157](mm), SLPI=[0.3](%),
LGI=[119.722](m), MNI=[0.013], SCI=[0](min),
3215 Continuous simulation parameters:
3216 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3217 *%-----|-----|
3218 *%-----|-----|
3219 ADD HYD NHYDsum=["KB-P1"], NHYDs to
add=["KB-01A-S"+"KB-01B-S"+"KB-01C-S"+"KB-03-S"+"KB-04-S"+"KB-05"+"KB-06-S"+"KB-11-S"+"KB
-15"+"S1"]
3220 *%-----|-----|
3221 ROUTE RESERVOIR NHYDout=["KB-P1R"], NHYDin=["KB-P1"],
3222 RDT=[1](min),
3223 TABLE of ( OUTFLOW-STORAGE ) values
3224 (cms) - (ha-m)
3225 [ 0.0 , 0.0 ]
3226 [0.076,0.003]
3227 [0.088,0.006]
3228 [0.136,0.011]
3229 [0.301,0.017]
3230 [0.454,0.027]
3231 [0.631,0.041]
3232 [1.173,0.068]
3233 [1.91,0.111]
3234 [4.847,0.231]
3235 [9.813,0.436]
3236 [12.134,0.617]
3237 [12.438,0.732]
3238 [12.424,0.811]
3239 [12.425,0.894]
3240 [ -1 , -1 ] (max twenty pts)
3241 NHYDovf=["KB-P1ovf"]
3242 *%-----|-----|
3243 ADD HYD NHYDsum=["KB-Pond1"], NHYDs to add=["KB-P1R"+"KB-P1ovf"]
3244 *%-----|-----|
3245 SAVE HYD NHYD=["KB-Pond1"], # OF PCYCLES=[-1], ICASEsh=[1]
3246 HYD_COMMENT=["Total Flows at KB first pond"]
3247 *%-----|-----|
3248 CONTINUOUS STANDHYD NHYD=["KB-07"], DT=[1]min, AREA=[10.86](ha), XIMP=[0.86],
TIMP=[0.86], DWF=[0](cms), LOSS=[1]:

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3249 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3250 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3251 Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%),
LGI=[269.072](m), MNI=[0.013], SCI=[0](min),
3252 Continuous simulation parameters:
3253 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3254 *%-----|-----|
3255 COMPUTE DUALHYD NHYDin=["KB-07"], CINLET=[2.094](cms), NINLET=[1],
3256 MaJNHYD=["KB-07-MJ"]
3257 MinNHYD=["KB-07-MN"]
3258 TMJSTO=[1378](cu-m)
3259 *%-----|-----|
3260 ADD HYD NHYDsum=["KB-07-S"], NHYDs to add=["KB-07-MJ"+"KB-07-MN"]
3261 *%-----|-----|
3262 CONTINUOUS STANDHYD NHYD=["KB-08"], DT=[1]min, AREA=[6.61](ha), XIMP=[0.64],
TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3263 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3264 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3265 Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%),
LGI=[209.921](m), MNI=[0.013], SCI=[0](min),
3266 Continuous simulation parameters:
3267 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3268 *%-----|-----|
3269 COMPUTE DUALHYD NHYDin=["KB-08"], CINLET=[1.058](cms), NINLET=[1],
3270 MaJNHYD=["KB-08-MJ"]
3271 MinNHYD=["KB-08-MN"]
3272 TMJSTO=[787](cu-m)
3273 *%-----|-----|
3274 ADD HYD NHYDsum=["KB-08-S"], NHYDs to add=["KB-08-MJ"+"KB-08-MN"]
3275 *%-----|-----|
3276 CONTINUOUS STANDHYD NHYD=["KB-09"], DT=[1]min, AREA=[2.6](ha), XIMP=[0.86],
TIMP=[0.86], DWF=[0](cms), LOSS=[1]:
3277 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3278 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3279 Impervious areas: IAimp=[1.57](mm), SLPI=[2.0](%),
LGI=[131.656](m), MNI=[0.013], SCI=[0](min),
3280 Continuous simulation parameters:
3281 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3282 *%-----|-----|
3283 *%-----|-----|
3284 CONTINUOUS STANDHYD NHYD=["KB-10_1"], DT=[1]min, AREA=[2.37](ha), XIMP=[0.86],
TIMP=[0.86], DWF=[0](cms), LOSS=[1]:
3285 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3286 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3287 Impervious areas: IAimp=[1.57](mm), SLPI=[2.0](%),
LGI=[125.698](m), MNI=[0.013], SCI=[0](min),
3288 Continuous simulation parameters:
3289 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3290 *%-----|-----|
3291 CONTINUOUS STANDHYD NHYD=["KB-10_2"], DT=[1]min, AREA=[1.14](ha), XIMP=[0.86],
TIMP=[0.86], DWF=[0](cms), LOSS=[1]:
3292 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3293 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),

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3294 MNP=[0.250], SCP=[0](min),
Impervious areas: IAimp=[1.57](mm), SLPI=[2.0](%), LGI=[87.178](m),
3295 MNI=[0.013], SCI=[0](min),
3296 Continuous simulation parameters:
IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1

3297 *%-----|-----|
3298 *%-----|-----|
3299 CONTINUOUS STANDHYD NHYD=["KB-12"], DT=[1]min, AREA=[4.86](ha), XIMP=[0.79],
TIMP=[0.79], DWF=[0](cms), LOSS=[1]:
3300 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3301 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3302 Impervious areas: IAimp=[1.099](mm), SLPI=[2.0](%),
LGI=[180.000](m), MNI=[0.013], SCI=[0](min),
3303 Continuous simulation parameters:
3304 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1

3305 *%-----|-----|
3306 COMPUTE DUALHYD NHYDin=["KB-12"], CINLET=[0.8665](cms), NINLET=[1],
3307 MajNHYD=["KB-12-MJ"]
3308 MinNHYD=["KB-12-MN"]
3309 TMJSTO=[632](cu-m)
3310 *%-----|-----|
3311 ADD HYD NHYDsum=["KB-12-S"], NHYDs to add=["KB-12-MJ"+"KB-12-MN"]
3312 *%-----|-----|
3313 CONTINUOUS STANDHYD NHYD=["KB-13"], DT=[1]min, AREA=[10.19](ha), XIMP=[0.64],
TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3314 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3315 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3316 Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%),
LGI=[260.640](m), MNI=[0.013], SCI=[0](min),
3317 Continuous simulation parameters:
3318 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1

3319 *%-----|-----|
3320 COMPUTE DUALHYD NHYDin=["KB-13"], CINLET=[1.722](cms), NINLET=[1],
3321 MajNHYD=["KB-13-MJ"]
3322 MinNHYD=["KB-13-MN"]
3323 TMJSTO=[1077](cu-m)
3324 *%-----|-----|
3325 ADD HYD NHYDsum=["KB-13-S"], NHYDs to add=["KB-13-MJ"+"KB-13-MN"]
3326 *%-----|-----|
3327 CONTINUOUS STANDHYD NHYD=["KB-14"], DT=[1]min, AREA=[5.47](ha), XIMP=[0.64],
TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3328 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3329 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3330 Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%),
LGI=[190.962](m), MNI=[0.013], SCI=[0](min),
3331 Continuous simulation parameters:
3332 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1

3333 *%-----|-----|
3334 COMPUTE DUALHYD NHYDin=["KB-14"], CINLET=[0.8734](cms), NINLET=[1],
3335 MajNHYD=["KB-14-MJ"]
3336 MinNHYD=["KB-14-MN"]
3337 TMJSTO=[631](cu-m)
3338 *%-----|-----|
3339 ADD HYD NHYDsum=["KB-14-S"], NHYDs to add=["KB-14-MJ"+"KB-14-MN"]
3340 *%-----|-----|
3341 *%-----|-----|

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3342 CONTINUOUS STANDHYD NHYD=["KB-16_2"], DT=[1]min, AREA=[3.42](ha), XIMP=[0.71],
TIMP=[0.71], DWF=[0](cms), LOSS=[1]:
3343 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3344 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3345 Impervious areas: IAimp=[0.157](mm), SLPI=[0.3](%),
LGI=[150.997](m), MNI=[0.013], SCI=[0](min),
3346 Continuous simulation parameters:
3347 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3348 *%-----|-----|
3349 ADD HYD NHYDsum=["KB-P2"], NHYDs to
add=["KB-Pond1"+"KB-07-S"+"KB-08-S"+"KB-09"+"KB-10_1"+"KB-10_2"+"KB-12-S"+"KB-13-S"+"KB-14-S"+"KB-16_2"]
3350 *%-----|-----|
3351 ROUTE RESERVOIR NHYDout=["KB-P2R"], NHYDin=["KB-P2"],
3352 RDT=[1](min),
3353 TABLE of ( OUTFLOW-STORAGE ) values
3354 (cms) - (ha-m)
3355 [ 0.0 , 0.0 ]
3356 [0.053,0.005]
3357 [0.132,0.009]
3358 [0.269,0.014]
3359 [0.455,0.023]
3360 [0.699,0.037]
3361 [0.947,0.056]
3362 [1.853,0.09]
3363 [2.712,0.146]
3364 [6.626,0.287]
3365 [11.228,0.515]
3366 [14.885,0.738]
3367 [16.473,0.893]
3368 [17.311,0.998]
3369 [17.633,1.063]
3370 [17.634,1.112]
3371 [ -1 , -1 ] (max twenty pts)
3372 NHYDovf=["KB-P2ovf"]
3373 *%-----|-----|
3374 ADD HYD NHYDsum=["KB-Pond2"], NHYDs to add=["KB-P2R"+"KB-P2ovf"]
3375 *%-----|-----|
3376 SAVE HYD NHYD=["KB-Pond2"], # OF PCYCLES=[-1], ICASEsh=[1]
3377 HYD_COMMENT=["Total Flows at KB second pond"]
3378 *%-----|-----|
3379 CONTINUOUS STANDHYD NHYD=["KB-16_1"], DT=[1]min, AREA=[2.8](ha), XIMP=[0.75],
TIMP=[0.75], DWF=[0](cms), LOSS=[1]:
3380 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3381 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3382 Impervious areas: IAimp=[0.157](mm), SLPI=[0.3](%),
LGI=[136.626](m), MNI=[0.013], SCI=[0](min),
3383 Continuous simulation parameters:
3384 IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3385 *%-----|-----|
3386 ADD HYD NHYDsum=["KB-P3"], NHYDs to add=["KB-Pond2"+"KB-16_1"]
3387 *%-----|-----|
3388 *%-----|-----|
3389 * One inflow node from pond 3 is added to the model (ROUTE RESERVOIR)
3390 * Another inflow node from right side of pond 3 is not added to the model
3391 ROUTE RESERVOIR NHYDout=["KB-P3R"], NHYDin=["KB-P3"],
3392 RDT=[1](min),
3393 TABLE of ( OUTFLOW-STORAGE ) values
3394 (cms) - (ha-m)
3395 [ 0.0 , 0.0 ]

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3396 [0.051,0.002]
3397 [0.048,0.003]
3398 [0.057,0.029]
3399 [0.089,0.045]
3400 [0.133,0.069]
3401 [0.199,0.106]
3402 [0.321,0.172]
3403 [1.029,0.306]
3404 [4.036,0.527]
3405 [8.332,0.761]
3406 [11.727,0.941]
3407 [14.125,1.067]
3408 [15.675,1.149]
3409 [16.555,1.196]
3410 [16.911,1.214]
3411 [ -1 , -1 ] (max twenty pts)
3412 NHYDovf=["KB-P3ovf"]
3413 *%-----|-----|
3414 ADD HYD NHYDsum=["KB-Pond3"], NHYDs to add=["KB-P3R"+"KB-P3ovf"]
3415 *%-----|-----|
3416 SAVE HYD NHYD=["KB-Pond3"], # OF PCYCLES=[-1], ICASEsh=[1]
3417 HYD_COMMENT=["Total Flows at KB third pond"]
3418 *%-----|-----|
3419 *#*****|
3420 *# EXISTING / PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118080), SWM
3421 Modeling Approach, NOVATECH Report June, 2020)
3422 *# - TO FRASER-CLARKE DRAIN
3423 *#*****|
3424 CONTINUOUS STANDHYD NHYD=["FC-01"], DT=[1]min, AREA=[8.03](ha), XIMP=[0.47],
3425 TIMP=[0.47], DWF=[0](cms), LOSS=[1]:
3426 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3427 F=[0.00](mm),
3428 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3429 MNP=[0.250], SCP=[0](min),
3430 Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
3431 LGI=[231.373](m), MNI=[0.013], SCI=[0](min),
3432 Continuous simulation parameters:
3433 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
3434 END=-1
3435 *%-----|-----|
3436 COMPUTE DUALHYD NHYDin=["FC-01"], CINLET=[0.756](cms), NINLET=[1],
3437 MajNHYD=["FC-01-MJ"]
3438 MinNHYD=["FC-01-MN"]
3439 TMJSTO=[714](cu-m)
3440 *%-----|-----|
3441 ADD HYD NHYDsum=["FC-01-S"], NHYDs to add=["FC-01-MJ"+"FC-01-MN"]
3442 *%-----|-----|
3443 CONTINUOUS STANDHYD NHYD=["FC-02"], DT=[1]min, AREA=[16.05](ha), XIMP=[0.93],
3444 TIMP=[0.93], DWF=[0](cms), LOSS=[1]:
3445 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
3446 F=[0.00](mm),
3447 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3448 MNP=[0.250], SCP=[0](min),
3449 Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
3450 LGI=[327.109](m), MNI=[0.013], SCI=[0](min),
3451 Continuous simulation parameters:
3452 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
3453 END=-1
3454 *%-----|-----|
3455 COMPUTE DUALHYD NHYDin=["FC-02"], CINLET=[1.159](cms), NINLET=[1],
3456 MajNHYD=["FC-02-MJ"]
3457 MinNHYD=["FC-02-MN"]
3458 TMJSTO=[2385](cu-m)
3459 *%-----|-----|
3460 ADD HYD NHYDsum=["FC-02-S"], NHYDs to add=["FC-02-MJ"+"FC-02-MN"]
3461 *%-----|-----|

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3451 CONTINUOUS STANDHYD NHYD=["FC-03"], DT=[1]min, AREA=[7.37](ha), XIMP=[0.64],
TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3452 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3453 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3454 Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
LGI=[221.660](m), MNI=[0.013], SCI=[0](min),
3455 Continuous simulation parameters:
3456 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3457 *%-----|
3458 COMPUTE DUALHYD NHYDin=["FC-03"], CINLET=[0.358](cms), NINLET=[1],
3459 MajNHYD=["FC-03-MJ"]
3460 MinNHYD=["FC-03-MN"]
3461 TMJSTO=[1131](cu-m)
3462 *%-----|
3463 ADD HYD NHYDsum=["FC-03-S"], NHYDs to add=["FC-03-MJ"+"FC-03-MN"]
3464 *%-----|
3465 CONTINUOUS STANDHYD NHYD=["FC-04"], DT=[1]min, AREA=[12.87](ha), XIMP=[0.64],
TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3466 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3467 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3468 Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
LGI=[292.916](m), MNI=[0.013], SCI=[0](min),
3469 Continuous simulation parameters:
3470 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3471 *%-----|
3472 COMPUTE DUALHYD NHYDin=["FC-04"], CINLET=[0.741](cms), NINLET=[1],
3473 MajNHYD=["FC-04-MJ"]
3474 MinNHYD=["FC-04-MN"]
3475 TMJSTO=[1794](cu-m)
3476 *%-----|
3477 ADD HYD NHYDsum=["FC-04-S"], NHYDs to add=["FC-04-MJ"+"FC-04-MN"]
3478 *%-----|
3479 *#*****
3480 *# PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118080), SWM Modeling
Approach, NOVATECH Report June, 2020)
3481 *# - TO JOCK RIVER
3482 *#*****
3483 CONTINUOUS STANDHYD NHYD=["JR-01"], DT=[1]min, AREA=[8.24](ha), XIMP=[0.64],
TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3484 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3485 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3486 Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
LGI=[234.379](m), MNI=[0.013], SCI=[0](min),
3487 Continuous simulation parameters:
3488 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3489 *%-----|
3490 COMPUTE DUALHYD NHYDin=["JR-01"], CINLET=[0.563](cms), NINLET=[1],
3491 MajNHYD=["JR-01-MJ"]
3492 MinNHYD=["JR-01-MN"]
3493 TMJSTO=[1040](cu-m)
3494 *%-----|
3495 ADD HYD NHYDsum=["JR-01-S"], NHYDs to add=["JR-01-MJ"+"JR-01-MN"]
3496 *%-----|
3497 CONTINUOUS STANDHYD NHYD=["JR-02"], DT=[1]min, AREA=[1.59](ha), XIMP=[0.64],
TIMP=[0.64], DWF=[0](cms), LOSS=[1]:
3498 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),

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3499          Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
3500          MNP=[0.250], SCP=[0](min),
3501          Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
3502          LGI=[102.956](m), MNI=[0.013], SCI=[0](min),
3503          Continuous simulation parameters:
3504          IaREcper=[4](hrs), IaREcimp=[4](hrs), InterEventTime=[12](hrs),
3505          END=-1
3506
3507 *%-----|-----|
3508 COMPUTE DUALHYD NHYDin=["JR-02"], CINLET=[0.153](cms), NINLET=[1],
3509          MajNHYD=["JR-02-MJ"]
3510          MinNHYD=["JR-02-MN"]
3511          TMJSTO=[153](cu-m)
3512
3513 *%-----|-----|
3514 ADD HYD NHYDsum=["JR-02-S"], NHYDs to add=["JR-02-MJ"+"JR-02-MN"]
3515
3516 *%-----|-----|
3517 *#*****|*****|
3518 *# Catchment FRASER
3519 *# - To Fraser-Clarke drain (north of the Jock)
3520 *# - Developed land with assumed 43% imp.
3521 *# - 2020-12-17 Change Fraser area to be 35.1 as measured from QGIS
3522 *# - 2020-12-17 All Fraser is undeveloped (Nashyd)
3523 *#*****|*****|
3524 CONTINUOUS NASHYD NHYD=["FRASER-DRN"], DT=[1]min, AREA=[13.65](ha),
3525          DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
3526          N=[3], TP=[0.4258]hrs,
3527          Continuous simulation parameters:
3528          IaREcper=[4](hrs),
3529          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3530          InterEventTime=[12](hrs)
3531          Baseflow simulation parameters:
3532          BaseFlowOption=[1],
3533          InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
3534          VHydCond=[0.055](mm/hr), END=-1
3535
3536 *
3537 CONTINUOUS STANDHYD NHYD=["FRASER-D"], DT=[1]min, AREA=[21.61](ha),
3538          XIMP=[0.585], TIMP=[0.585], DWF=[0](cms), LOSS=[2],
3539          SCS curve number CN=[80],
3540          Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3541          LGP=[40](m), MNP=[0.25], SCP=[0](min),
3542          Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3543          LGI=[379.561](m), MNI=[0.013], SCI=[0](min),
3544          Continuous simulation parameters:
3545          IaREcper=[4](hrs), IaREcimp=[4](hrs),
3546          SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3547          InterEventTime=[18](hrs), END=-1
3548
3549 *%-----|-----|
3550 COMPUTE DUALHYD NHYDin=["FRASER-D"], CINLET=[2.281](cms), NINLET=[1],
3551          MajNHYD=["FRASER-J"]
3552          MinNHYD=["FRASER-N"]
3553          TMJSTO=[9999999](cu-m)
3554
3555 *%-----|-----|
3556 ADD HYD NHYDsum=["FRASER-S"], NHYDs to add=["FRASER-J"+"FRASER-N"]
3557
3558 *%-----|-----|
3559 *ROUTE RESERVOIR NHYDout=["MS_P20"], NHYDin=["FRASER"],
3560          *
3561          RDT=[1](min),
3562          *
3563          TABLE of ( OUTFLOW-STORAGE ) values
3564          *
3565          (cms) - (ha-m)
3566          *
3567          [ 0.0 , 0.0 ]
3568          *
3569          [ 0.04 , 0.36 ]
3570          *
3571          [ -1 , -1 ] (max twenty pts)
3572          *
3573          NHYDovf=["P20-OVF"]
3574
3575 *%-----|-----|
3576 ADD HYD NHYDsum=["4241"], NHYDs to
3577          add=["KB-Pond3"+"S-1-B"+"FRASER-DRN"+"FRASER-S"+"N_KB"+"FC-01-S"+"FC-02-S"+"FC-03-S"]
3578
3579 *%-----|-----|
3580 SAVE HYD NHYD=["4241"], # OF PCYCLES=[-1], ICASEsh=[1]

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3561 HYD_COMMENT=["Total Flows at Ken-Burnett Outlet"]
3562 *%-----|-----|
3563 *# Hydrograph from Node Ken-Burnett to station 3633
3564 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4241
3565 *#
3566 ROUTE CHANNEL NHYDout=["4241-out"], NHYDin=["4241"], RDT=[1](min),
3567 CHLGTH=[294](m), CHSLOPE=[0.1088](%), FPSLOPE=[0.1088](%),
3568 SECNUM=[1.0], NSEG=[3]
3569 ( SEGROUGH, SEGDIST (m))=[0.05, -20.12
3570 -0.035, 45.26
3571 0.05, 403.84] NSEG times
3572 ( DISTANCE (m), ELEVATION (m))=[]
3573 [-909.72, 95 ]
3574 [-907.09, 94.5 ]
3575 [-904.65, 94 ]
3576 [-902.26, 93.5 ]
3577 [-44.51, 91.5 ]
3578 [-25.1, 91.5 ]
3579 [-20.98, 91 ]
3580 [-20.61, 90.5 ]
3581 [-20.12, 90 ]
3582 [-6.13, 87.26 ]
3583 [17.51, 86.56 ]
3584 [31.37, 87.2 ]
3585 [45.26, 90 ]
3586 [50.41, 90.5 ]
3587 [63.06, 91 ]
3588 [134.5, 91.5 ]
3589 [190.63, 92 ]
3590 [251.98, 92.5 ]
3591 [321.32, 93.5 ]
3592 [403.84, 95 ]
3593 *%-----|-----|
3594 ADD HYD NHYDsum=["SN_KB"], NHYDs to
add=["4241-out"+"FC-04-S"+"JR-01-S"+"JR-02-S"]
3595 *%-----|-----|
3596 SAVE HYD NHYD=["SN_KB"], # OF PCYCLES=[-1], ICASEsh=[1]
3597 HYD_COMMENT=["Total Flows before Station 3633"]
3598 *%-----|-----|
3599 *# Hydrograph from Station 3633 to Node Todd
3600 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 3633
3601 *# JFSA 2021-02-26 change the channel length (at station 3633) from 650m to 608m and
change the slope from 0.0498% to 0.24671%. That is because of adding station 4241
between station 4534 and station 3633
3602 *#
3603 ROUTE CHANNEL NHYDout=["N_TO"], NHYDin=["SN_KB"], RDT=[1](min),
3604 CHLGTH=[608](m), CHSLOPE=[0.24671](%), FPSLOPE=[0.24671](%),
3605 SECNUM=[1.0], NSEG=[3]
3606 ( SEGROUGH, SEGDIST (m))=[0.05, -23.74
3607 -0.035, 23.74
3608 0.05, 26.50] NSEG times
3609 ( DISTANCE (m), ELEVATION (m))=[]
3610 -29.24, 91.0
3611 -27.41, 90.5
3612 -25.64, 90
3613 -23.74, 89.5
3614 -22, 89.26
3615 -20, 88.51
3616 -19, 88.32
3617 -15, 88.1
3618 -10, 88.11
3619 -5, 88.17
3620 0, 88.27
3621 5, 88.19
3622 10, 88.06
3623 15, 88.48

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3624      16, 88.7
3625      23.74, 89.5
3626      24.68, 90
3627      25.57, 90.5
3628      26.50, 91.0
3629      *                [-29.24, 91]
3630      *                [-27.41, 90.5]
3631      *                [-25.64, 90]
3632      *                [-23.74, 89.5]
3633      *                [-22, 89.26]
3634      *                [-20, 88.51]
3635      *                [-19, 88.32]
3636      *                [-15, 88.1]
3637      *                [-10, 88.11]
3638      *                [-5, 88.17]
3639      *                [0, 88.27]
3640      *                [5, 88.19]
3641      *                [10, 88.06]
3642      *                [15, 88.48]
3643      *                [16, 88.7]
3644      *                [23.74, 89.5]
3645      *                [24.68, 90]
3646      *                [25.57, 90.5]
3647      *%-----|-----|
3648      *#*****|
3649      *#   Catchment Greenbank
3650      *#   - To Greenbank Drain (south of the Jock)
3651      *#   - JFSA 2021-01-18 add Greenbank pond as per JFSA, P598(06)-15, June 2016
3652      *#   - JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GIS measurements
3653      *#*****|
3654      CONTINUOUS STANDHYD NHYD=["Greenbank"], DT=[1]min, AREA=[36.6](ha),
3655      XIMP=[0.639], TIMP=[0.682], DWF=[0](cms), LOSS=[2],
3656      SCS curve number CN=[77],
3657      Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3658      LGP=[40](m), MNP=[0.25], SCP=[0](min),
3659      Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3660      LGI=[493.96](m), MNI=[0.013], SCI=[0](min),
3661      Continuous simulation parameters:
3662      IaREcper=[4](hrs), IaREcimp=[4](hrs),
3663      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3664      InterEventTime=[18](hrs), END=-1
3665      *%-----|-----|
3666      ROUTE RESERVOIR NHYDout=["GreenB_MN"], NHYDin=["Greenbank"],
3667      RDT=[1](min),
3668      TABLE of ( OUTFLOW-STORAGE ) values
3669      (cms) - (ha-m)
3670      [ 0.0 , 0.0 ]
3671      [ 0.033 , 0.084 ]
3672      [ 0.039 , 0.201 ]
3673      [ 0.113 , 0.292 ]
3674      [ 0.237 , 0.386 ]
3675      [ 0.382 , 0.484 ]
3676      [ 0.539 , 0.585 ]
3677      [ 0.7 , 0.692 ]
3678      [ 0.86 , 0.804 ]
3679      [ 4.684 , 0.922 ]
3680      [ 11.539 , 1.052 ]
3681      [ 20.867 , 1.168 ]
3682      [ 103.616 , 1.974 ]
3683      [ -1 , -1 ] (max twenty pts)
3684      NHYDovf=["GreenB_MJ"],
3685      *%-----|-----|
3686      *%-----|-----|
3687      ADD HYD NHYDsum=["GreenB"], NHYDs to add=["N_TO"+"GreenB_MJ"+"GreenB_MN"]
3688      *%-----|-----|
3689      SAVE HYD NHYD=["GreenB"], # OF PCYCLES=[-1], ICASEsh=[1]

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3690 HYD_COMMENT=["Total Flows at Greenbank Drain"]
3691 *%-----|-----|
3692 *#*****|
3693 *# Catchment TODD
3694 *# - To Todd Drain (south of the Jock)
3695 *# - Subdivision with 43% imp. as per Barrhaven South MSS
3696 *# - 2020-11-30 increase imp. based on P598(04)-11
3697 *# - 2020-11-30 update TODD Tributary Drainage Area to = 146.015 ha based on
P598(04)-11
3698 *# - 2020-11-30 split TODD Drainage Area to MAJOR, MINOR, POND and ALL
3699 *#*****|
3700 *# - JFSA 2021-01-19 add "TODD_MN1" as part of Clarke("W_CLAR_MJ") and remove it
from Todd
3701 *CONTINUOUS STANDHYD NHYD=["TODD_MN1"], DT=[1]min, AREA=[1.772](ha),
3702 * XIMP=[0.53], TIMP=[0.57], DWF=[0](cms), LOSS=[2],
3703 * SCS curve number CN=[77],
3704 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3705 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3706 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3707 * LGI=[108.689](m), MNI=[0.013], SCI=[0](min),
3708 * Continuous simulation parameters:
3709 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
3710 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3711 * InterEventTime=[18](hrs), END=-1
3712 *%-----|-----|
3713 CONTINUOUS STANDHYD NHYD=["TODD_MN2"], DT=[1]min, AREA=[2.1](ha),
3714 XIMP=[0.53], TIMP=[0.57], DWF=[0](cms), LOSS=[2],
3715 SCS curve number CN=[77],
3716 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3717 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3718 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3719 LGI=[118.322](m), MNI=[0.013], SCI=[0](min),
3720 Continuous simulation parameters:
3721 IaRECper=[4](hrs), IaRECimp=[4](hrs),
3722 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3723 InterEventTime=[18](hrs), END=-1
3724 *%-----|-----|
3725 CONTINUOUS STANDHYD NHYD=["TODD_MN3"], DT=[1]min, AREA=[0.117](ha),
3726 XIMP=[0.53], TIMP=[0.57], DWF=[0](cms), LOSS=[2],
3727 SCS curve number CN=[77],
3728 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3729 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3730 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3731 LGI=[27.928](m), MNI=[0.013], SCI=[0](min),
3732 Continuous simulation parameters:
3733 IaRECper=[4](hrs), IaRECimp=[4](hrs),
3734 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3735 InterEventTime=[18](hrs), END=-1
3736 *%-----|-----|
3737 CONTINUOUS STANDHYD NHYD=["TODD_MJ"], DT=[1]min, AREA=[30.230](ha),
3738 XIMP=[0.52], TIMP=[0.64], DWF=[0](cms), LOSS=[2],
3739 SCS curve number CN=[77],
3740 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3741 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3742 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3743 LGI=[448.925](m), MNI=[0.013], SCI=[0](min),
3744 Continuous simulation parameters:
3745 IaRECper=[4](hrs), IaRECimp=[4](hrs),
3746 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3747 InterEventTime=[18](hrs), END=-1
3748 *%-----|-----|
3749 * -JFSA, 2021-01-19 update "TODD_ALL" area from 108.741 ha to 112.908 ha based on
GIS measurements (148.41-30.23-0.117-2.1-3.055=112.908 ha)
3750 CONTINUOUS STANDHYD NHYD=["TODD_ALL"], DT=[1]min, AREA=[112.908](ha),
3751 XIMP=[0.52], TIMP=[0.57], DWF=[0](cms), LOSS=[2],
3752 SCS curve number CN=[77],

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3753 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3754 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3755 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3756 LGI=[867.594](m), MNI=[0.013], SCI=[0](min),
3757 Continuous simulation parameters:
3758 IaRECPper=[4](hrs), IaRECImp=[4](hrs),
3759 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3760 InterEventTime=[18](hrs), END=-1
3761 *%-----|-----
3762 CONTINUOUS STANDHYD NHYD=["TODD_P"], DT=[1]min, AREA=[3.055](ha),
3763 XIMP=[0.63], TIMP=[0.63], DWF=[0](cms), LOSS=[2],
3764 SCS curve number CN=[77],
3765 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3766 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3767 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3768 LGI=[142.712](m), MNI=[0.013], SCI=[0](min),
3769 Continuous simulation parameters:
3770 IaRECPper=[4](hrs), IaRECImp=[4](hrs),
3771 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3772 InterEventTime=[18](hrs), END=-1
3773 *%-----|-----
3774 *%-----|-----
3775 * -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"
and its parameters remain the same.
3776 *CONTINUOUS STANDHYD NHYD=["TODD_DEVL"], DT=[1]min, AREA=[15.87](ha),
3777 * XIMP=[0.63], TIMP=[0.63], DWF=[0](cms), LOSS=[2],
3778 * SCS curve number CN=[77],
3779 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3780 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3781 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3782 * LGI=[325.27](m), MNI=[0.013], SCI=[0](min),
3783 * Continuous simulation parameters:
3784 * IaRECPper=[4](hrs), IaRECImp=[4](hrs),
3785 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3786 * InterEventTime=[18](hrs), END=-1
3787 *%-----|-----
3788 * -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
is called "corr2" and its parameters remain the same.
3789 *CONTINUOUS NASHYD NHYD=["TODD_UnD"], DT=[1]min, AREA=[12.47](ha),
3790 * DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
3791 * N=[3], TP=[1.10]hrs,
3792 * Continuous simulation parameters:
3793 * IaRECPper=[4](hrs),
3794 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3795 * InterEventTime=[12](hrs)
3796 * Baseflow simulation parameters:
3797 * BaseFlowOption=[1] ,
3798 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
3799 * VHydCond=[0.055](mm/hr), END=-1
3800 *%-----|-----
3801 *# 5-Year + 12% Capture
3802 *COMPUTE DUALHYD NHYDin=["TODD_MJ"], CINLET=[3.314](cms), NINLET=[1],
3803 * MajNHYD=["TODD_MJj"]
3804 * MinNHYD=["TODD_MJn"]
3805 * TMJSTO=[0.1](cu-m)
3806 ROUTE RESERVOIR NHYDout=["TODD_MJn"],NHYDin=["TODD_MJ"],
3807 RDT=[1](min),
3808 TABLE of ( OUTFLOW-STORAGE ) values
3809 (cms) - (ha-m)
3810 [ 0.0 , 0.0 ]
3811 [ 3.314 , 0.0001 ]
3812 [ -1 , -1 ] (max twenty pts)
3813 NHYDovf=["TODD_MJj"],
3814 *%-----|-----
3815 *# 5-Year + 12% Capture

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3816 *COMPUTE DUALHYD      NHYDin=["TODD_MN1"], CINLET=[0.227](cms), NINLET=[1],
3817 *                      MajNHYD=["TODD_MN1j"]
3818 *                      MinNHYD=["TODD_MN1n"]
3819 *                      TMJSTO=[0.1](cu-m)
3820 *ROUTE RESERVOIR      NHYDout=["TODD_MN1n"],NHYDin=["TODD_MN1"],
3821 *                      RDT=[1](min),
3822 *                      TABLE of ( OUTFLOW-STORAGE ) values
3823 *                      (cms) - (ha-m)
3824 *                      [ 0.0 , 0.0 ]
3825 *                      [ 0.227 , 0.0001 ]
3826 *                      [ -1 , -1 ] (max twenty pts)
3827 *                      NHYDovf=["TODD_MN1j"],
3828 *%-----|-----|
3829 *COMPUTE DUALHYD      NHYDin=["TODD_MN2"], CINLET=[0.268](cms), NINLET=[1],
3830 *                      MajNHYD=["TODD_MN2j"]
3831 *                      MinNHYD=["TODD_MN2n"]
3832 *                      TMJSTO=[0.1](cu-m)
3833 ROUTE RESERVOIR      NHYDout=["TODD_MN2n"],NHYDin=["TODD_MN2"],
3834 *                      RDT=[1](min),
3835 *                      TABLE of ( OUTFLOW-STORAGE ) values
3836 *                      (cms) - (ha-m)
3837 *                      [ 0.0 , 0.0 ]
3838 *                      [ 0.268 , 0.0001 ]
3839 *                      [ -1 , -1 ] (max twenty pts)
3840 *                      NHYDovf=["TODD_MN2j"],
3841 *%-----|-----|
3842 *COMPUTE DUALHYD      NHYDin=["TODD_MN3"], CINLET=[0.016](cms), NINLET=[1],
3843 *                      MajNHYD=["TODD_MN3j"]
3844 *                      MinNHYD=["TODD_MN3n"]
3845 *                      TMJSTO=[0.1](cu-m)
3846 ROUTE RESERVOIR      NHYDout=["TODD_MN3n"],NHYDin=["TODD_MN3"],
3847 *                      RDT=[1](min),
3848 *                      TABLE of ( OUTFLOW-STORAGE ) values
3849 *                      (cms) - (ha-m)
3850 *                      [ 0.0 , 0.0 ]
3851 *                      [ 0.016 , 0.0001 ]
3852 *                      [ -1 , -1 ] (max twenty pts)
3853 *                      NHYDovf=["TODD_MN3j"],
3854 *%-----|-----|
3855 * -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
3856 * major system from A2 can be added to Todd
3857 CONTINUOUS STANDHYD  NHYD=["A2"], DT=[1]min, AREA=[25.5](ha),
3858 *                      XIMP=[0.42], TIMP=[0.52], DWF=[0](cms), LOSS=[2],
3859 *                      SCS curve number CN=[75],
3860 *                      Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3861 *                      LGP=[40](m), MNP=[0.25], SCP=[0](min),
3862 *                      Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3863 *                      LGI=[566](m), MNI=[0.013], SCI=[0](min),
3864 *                      Continuous simulation parameters:
3865 *                      IaREcper=[4](hrs), IaREcimp=[4](hrs),
3866 *                      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3867 *                      InterEventTime=[18](hrs), END=-1
3868 *%-----|-----|
3869 COMPUTE DUALHYD      NHYDin=["A2"], CINLET=[1.818](cms), NINLET=[1],
3870 *                      MajNHYD=["A2-MJ"]
3871 *                      MinNHYD=["A2-MN"]
3872 *                      TMJSTO=[924](cu-m)
3873 *%-----|-----|
3874 ADD HYD              NHYDsum=["TODD"], NHYDs to
3875 *                      add=["TODD_MN2n"+"TODD_MN3n"+"TODD_MJj"+"TODD_P"+"TODD_ALL"+"W_CLAR_MJn"]
3876 *%-----|-----|
3877 SAVE HYD             NHYD=["TODD"], # OF PCYCLES=[-1], ICASEsh=[1]
3878 *                      HYD_COMMENT=["Total Flows at Todd Drain"]
3879 *%-----|-----|
3880 *#*****
3881 *# Todd Pond 3

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3880 *# - Rating curve obtained from Barrhaven South MSS modeling
3881 *# - stantec 2007, Tributary Drainage Area to MSS Pond 3 = 193 ha
3882 *#*****
3883 ROUTE RESERVOIR      NHYDout=["MS_P3"],  NHYDin=["TODD"],
3884                      RDT=[1](min),
3885                      TABLE of ( OUTFLOW-STORAGE ) values
3886                      (cms) - (ha-m)
3887                      [ 0.0 , 0.0 ]
3888                      [ 0.014 , 0.155 ]
3889                      [ 0.048 , 0.394 ]
3890                      [ 0.061 , 0.56 ]
3891                      [ 0.08 , 0.909 ]
3892                      [ 0.088 , 1.089 ]
3893                      [ 0.109 , 1.652 ]
3894                      [ 0.118 , 1.952 ]
3895                      [ 0.122 , 2.099 ]
3896                      [ 1.972 , 2.269 ]
3897                      [ 9.135 , 2.598 ]
3898                      [ 15.608 , 2.826 ]
3899                      [ 19.256 , 2.942 ]
3900                      [ 27.282 , 3.181 ]
3901                      [ 40.957 , 3.55 ]
3902                      [ 56.372 , 3.929 ]
3903                      [ 73.349 , 4.317 ]
3904                      [ 85.469 , 4.579 ]
3905                      [ 104.771 , 4.977 ]
3906                      [ -1 , -1 ] (max twenty pts)
3907                      NHYDovf=["P3-OVF"]
3908 *%-----|-----
3909 ADD HYD          NHYDsum=["SN_TO"], NHYDs to
add=["GreenB"+"MS_P3"+"P3-OVF"+"TODD_MN2j"+"A2-MJ"]
3910 *%-----|-----
3911 SAVE HYD        NHYD=["SN_TO"], # OF PCYCLES=[-1], ICASEsh=[1]
3912                HYD_COMMENT=["Total Flows at Todd Drain"]
3913 *%-----|-----
3914 *#
3915 *# Hydrograph from Todd Drain routed to Corrigan Drain
3916 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
3917 *# 2021-02-19 Change the slope from 0.033 % (as per Stantec Report 2007) to 0.05 % so
the model will be more stable and give reasonable results. It is justifiable as ROUTE
CHANNELs aren't well suited to really flat slopes.
3918 *
3919 ROUTE CHANNEL    NHYDout=["N_TO"] ,NHYDin=["SN_TO"] ,
3920                RDT=[1](min),
3921                CHLGTH=[280](m),  CHSLOPE=[0.05](%),
3922                FPSLOPE=[0.05](%),
3923                SECNUM=[1.0],      NSEG=[3]
3924                ( SEGROUGH, SEGDIST (m))=
3925                [0.075,-17.72
3926                -0.045,17.72
3927                0.075,80.62] NSEG times
3928                ( DISTANCE (m), ELEVATION (m))=
3929                [-83.32, 90.00]
3930                [-81.36, 89.50]
3931                [-79.12, 89.00]
3932                [-76.13, 88.50]
3933                [-20.46, 88.00]
3934                [-19.36, 87.50]
3935                [-18.51, 87.00]
3936                [-17.72, 86.50]
3937                [-11.95, 85.24]
3938                [-0.11, 85.12]
3939                [11.49, 85.20]
3940                [17.72, 86.50]
3941                [19.74, 87.00]
3942                [21.22, 87.50]

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3943 [22.68, 88.00]
3944 [24.28, 88.50]
3945 [26.79, 89.00]
3946 [71.98, 90.00]
3947 [80.62, 90.50]
3948 *%-----|-----|
3949 SAVE HYD NHYD=["N_TO"], # OF PCYCLES=[-1], ICASEsh=[1]
3950 HYD_COMMENT=["Total inflows at Station 2462"]
3951 *%-----|-----|
3952 *#*****|*****|
3953 *# Catchment CORRIG
3954 *# - To Corrigan Drain (south of the Jock)
3955 *# - Primarily Developed (medium density)
3956 *# - JFSA JAN 2021, add Corrigan subcatchments as per IBI, July 2008
3957 *#*****|*****|
3958 *ROUTE RESERVOIR NHYDout=["MS_P1"], NHYDin=["CORRIG"],
3959 * RDT=[1](min),
3960 * TABLE of ( OUTFLOW-STORAGE ) values
3961 * (cms) - (ha-m)
3962 * [ 0.0 , 0.0 ]
3963 * [ 0.06 , 0.58]
3964 * [ -1 , -1 ] (max twenty pts)
3965 * NHYDovf=["P1-OVF"]
3966 *%-----|-----|
3967 *ADD HYD NHYDsum=["SN_CO"], NHYDs to add=["N_TO"+"P1-OVF"+"MS_P1"]
3968 *%-----|-----|
3969 *SAVE HYD NHYD=["SN_CO"], # OF PCYCLES=[-1], ICASEsh=[1]
3970 * HYD_COMMENT=["Total Flows at Corrigan Drain"]
3971 *%-----|-----|
3972 * -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"
and its parameters remain the same.
3973 CONTINUOUS STANDHYD NHYD=["corr1"], DT=[1]min, AREA=[15.87](ha),
3974 XIMP=[0.63], TIMP=[0.63], DWF=[0](cms), LOSS=[2],
3975 SCS curve number CN=[77],
3976 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3977 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3978 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3979 LGI=[325.27](m), MNI=[0.013], SCI=[0](min),
3980 Continuous simulation parameters:
3981 IaRECper=[4](hrs), IaRECimp=[4](hrs),
3982 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3983 InterEventTime=[18](hrs), END=-1
3984 *%-----|-----|
3985 * -JFSA 2021-02-23 add DUALHYD for "corr1". "corr1" DUALHYD Parameters are the
same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to "corr1".
3986 * At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for
A1-Corrig
3987 COMPUTE DUALHYD NHYDin=["corr1"], CINLET=[1.818](cms), NINLET=[1],
3988 MajNHYD=["corr1-MJ"]
3989 MinNHYD=["corr1-MN"]
3990 TMJSTO=[924](cu-m)
3991 *%-----|-----|
3992 * -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
is called "corr2" and its parameters remain the same.
3993 CONTINUOUS NASHYD NHYD=["corr2"], DT=[1]min, AREA=[12.47](ha),
3994 DWF=[0](cms), CN/C=[77], IA=[4.67](mm),
3995 N=[3], TP=[1.10]hrs,
3996 Continuous simulation parameters:
3997 IaRECper=[4](hrs),
3998 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3999 InterEventTime=[12](hrs)
4000 Baseflow simulation parameters:
4001 BaseFlowOption=[1] ,
4002 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4003 VHydCond=[0.055](mm/hr), END=-1

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4004 *%-----|-----|
4005 * -JFSA 2021-01-19 change A1-Corrig to be developed as per geottawa website and
apply the parameters of A2, the nearest sub-catchment to A1-Corrig, LGI is calculated
based on A1-Corrig area
4006 * -JFSA 2021-01-19 update all Corrigan areas based on GIS measurements, and keep
LGI as it is from Corrigan Report, IBI Group, 2008 because LGI calculated is less than
LGI from the Corrigan Report
4007 CONTINUOUS STANDHYD NHYD=["A1-Corrig"], DT=[1]min, AREA=[15.75](ha),
4008 XIMP=[0.42], TIMP=[0.52], DWF=[0](cms), LOSS=[2],
4009 SCS curve number CN=[75],
4010 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4011 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4012 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4013 LGI=[324.037](m), MNI=[0.013], SCI=[0](min),
4014 Continuous simulation parameters:
4015 IaREcper=[4](hrs), IaREcimp=[4](hrs),
4016 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4017 InterEventTime=[18](hrs), END=-1
4018 *
4019 * -JFSA 2021-01-25 add DUALHYD for A1-Corrig. A1-Corrig DUALHYD Parameters are the
same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to A1-Corrig.
4020 * At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for
A1-Corrig
4021 COMPUTE DUALHYD NHYDin=["A1-Corrig"], CINLET=[1.818](cms), NINLET=[1],
4022 MajNHYD=["A1-MJ"]
4023 MinNHYD=["A1-MN"]
4024 TMJSTO=[924](cu-m)
4025 *%-----|-----|
4026 *CONTINUOUS NASHYD NHYD=["A1-Corrig"], DT=[1]min, AREA=[15.75](ha),
4027 DWF=[0](cms), CN/C=[66], IA=[2.5](mm),
4028 N=[3.0], TP=[0.36]hrs,
4029 * Continuous simulation parameters:
4030 IaREcper=[4](hrs),
4031 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4032 InterEventTime=[12](hrs)
4033 * Baseflow simulation parameters:
4034 BaseFlowOption=[1] ,
4035 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4036 VHydCond=[0.055](mm/hr), END=-1
4037 *%-----|-----|
4038 CONTINUOUS NASHYD NHYD=["B1"], DT=[1]min, AREA=[2.77](ha),
4039 DWF=[0](cms), CN/C=[56], IA=[2.5](mm),
4040 N=[3.0], TP=[0.23]hrs,
4041 Continuous simulation parameters:
4042 IaREcper=[4](hrs),
4043 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4044 InterEventTime=[12](hrs)
4045 Baseflow simulation parameters:
4046 BaseFlowOption=[1] ,
4047 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4048 VHydCond=[0.055](mm/hr), END=-1
4049 *%-----|-----|
4050 CONTINUOUS STANDHYD NHYD=["A4"], DT=[1]min, AREA=[1.27](ha),
4051 XIMP=[0.65], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
4052 SCS curve number CN=[75],
4053 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4054 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4055 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4056 LGI=[253](m), MNI=[0.013], SCI=[0](min),
4057 Continuous simulation parameters:
4058 IaREcper=[4](hrs), IaREcimp=[4](hrs),
4059 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4060 InterEventTime=[18](hrs), END=-1
4061 *%-----|-----|
4062 COMPUTE DUALHYD NHYDin=["A4"], CINLET=[0.405](cms), NINLET=[1],
4063 MajNHYD=["A4-MJ"]

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4064 MinNHYD=["A4-MN"]
4065 TMJSTO=[68](cu-m)
4066 *%-----|-----|
4067 ADD HYD NHYDsum=["MH101"], NHYDs to
add=["A1-MJ"+"A1-MN"+"corr1-MJ"+"corr1-MN"+"corr2"+"B1"+"A4-MN"]
4068 *%-----|-----|
4069 SAVE HYD NHYD=["MH101"], # OF PCYCLES=[-1], ICASEsh=[1]
4070 HYD_COMMENT=["Total Flows at MH101"]
4071 *%-----|-----|
4072 ROUTE PIPE PTYPE=[1]circ, NHYDout=["101-102"], RNUMBER=[1.0], PDIAM=[1050](mm),
4073 PLNGTH=[368](m), PROUGH=[0.013], PSLOPE=[0.0054](m/m),
NHYDin=["MH101"], RDT=[1]
4074 *%-----|-----|
4075 * -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
major system from A2 can be added to Todd
4076 *CONTINUOUS STANDHYD NHYD=["A2"], DT=[1]min, AREA=[25.5](ha),
4077 * XIMP=[0.42], TIMP=[0.52], DWF=[0](cms), LOSS=[2],
4078 * SCS curve number CN=[75],
4079 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4080 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
4081 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4082 * LGI=[566](m), MNI=[0.013], SCI=[0](min),
4083 * Continuous simulation parameters:
4084 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
4085 * SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4086 * InterEventTime=[18](hrs), END=-1
4087 *%-----|-----|
4088 *COMPUTE DUALHYD NHYDin=["A2"], CINLET=[1.818](cms), NINLET=[1],
4089 * MajNHYD=["A2-MJ"]
4090 * MinNHYD=["A2-MN"]
4091 * TMJSTO=[924](cu-m)
4092 *%-----|-----|
4093 ADD HYD NHYDsum=["MH102"], NHYDs to add=["A2-MN"+"101-102"]
4094 *%-----|-----|
4095 SAVE HYD NHYD=["MH102"], # OF PCYCLES=[-1], ICASEsh=[1]
4096 HYD_COMMENT=["Total Flows at MH102"]
4097 *%-----|-----|
4098 CONTINUOUS STANDHYD NHYD=["A5"], DT=[1]min, AREA=[1.6](ha),
4099 XIMP=[0.71], TIMP=[0.71], DWF=[0](cms), LOSS=[2],
4100 SCS curve number CN=[75],
4101 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4102 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4103 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4104 LGI=[300](m), MNI=[0.013], SCI=[0](min),
4105 Continuous simulation parameters:
4106 IaRECper=[4](hrs), IaRECimp=[4](hrs),
4107 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4108 InterEventTime=[18](hrs), END=-1
4109 *%-----|-----|
4110 ADD HYD NHYDsum=["A5T"], NHYDs to add=["A4-MJ"+"A5"]
4111 *%-----|-----|
4112 COMPUTE DUALHYD NHYDin=["A5T"], CINLET=[0.357](cms), NINLET=[1],
4113 MajNHYD=["A5-MJ"]
4114 MinNHYD=["A5-MN"]
4115 TMJSTO=[60](cu-m)
4116 *%-----|-----|
4117 * -JFSA Jan. 2021, A3 is a part of Todd so it is removed
4118 * -JFSA Jan. 2021, "A2-MJ" added to "Todd"
4119 *CONTINUOUS STANDHYD NHYD=["A3"], DT=[1]min, AREA=[18.4](ha),
4120 * XIMP=[0.58], TIMP=[0.65], DWF=[0](cms), LOSS=[2],
4121 * SCS curve number CN=[75],
4122 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4123 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
4124 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4125 * LGI=[450](m), MNI=[0.013], SCI=[0](min),
4126 * Continuous simulation parameters:

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4127 *           IaREcper=[4](hrs), IaREcimp=[4](hrs),
4128 *           SMIN=[-1](mm),  SMAx=[-1](mm), SK=[0.010]/(mm),
4129 *           InterEventTime=[18](hrs),  END=-1
4130 *%-----|-----|
4131 *ADD HYD           NHYDsum=["A3-A2MJ"], NHYDs to add=["A2-MJ"+"A3"]
4132 *%-----|-----|
4133 *COMPUTE DUALHYD  NHYDin=["A3-A2MJ"], CINLET=[2.208](cms), NINLET=[1],
4134 *           MajNHYD=["A3R-MJ"]
4135 *           MinNHYD=["A3R-MN"]
4136 *           TMJSTO=[908](cu-m)
4137 *%-----|-----|
4138 ROUTE PIPE        PTYPE=[1]circ, NHYDout=["102-103"], RNUMBER=[1.0], PDIAM=[1500](mm),
4139 *           PLNGTH=[504](m), PROUGH=[0.013], PSLOPE=[0.0028](m/m),
4140 *           NHYDin=["MH102"], RDT=[1]
4141 *%-----|-----|
4141 ADD HYD           NHYDsum=["MH103"], NHYDs to add=["102-103"+"A5-MN"]
4142 *%-----|-----|
4143 SAVE HYD          NHYD=["MH103"], # OF PCYCLES=[-1], ICASEsh=[1]
4144 *           HYD_COMMENT=["Total Flows at MH103"]
4145 *%-----|-----|
4146 ROUTE PIPE        PTYPE=[1]circ, NHYDout=["103-104"], RNUMBER=[1.0], PDIAM=[1650](mm),
4147 *           PLNGTH=[438](m), PROUGH=[0.013], PSLOPE=[0.0046](m/m),
4148 *           NHYDin=["MH103"], RDT=[1]
4149 *%-----|-----|
4149 CONTINUOUS STANDHYD NHYD=["A6"], DT=[1]min, AREA=[1.56](ha),
4150 *           XIMP=[0.71], TIMP=[0.71], DWF=[0](cms), LOSS=[2],
4151 *           SCS curve number CN=[75],
4152 *           Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4153 *           LGP=[40](m), MNP=[0.25], SCP=[0](min),
4154 *           Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4155 *           LGI=[280](m), MNI=[0.013], SCI=[0](min),
4156 *           Continuous simulation parameters:
4157 *           IaREcper=[4](hrs), IaREcimp=[4](hrs),
4158 *           SMIN=[-1](mm),  SMAx=[-1](mm), SK=[0.010]/(mm),
4159 *           InterEventTime=[18](hrs),  END=-1
4160 *%-----|-----|
4161 ADD HYD           NHYDsum=["A6T"], NHYDs to add=["A5-MJ"+"A6"]
4162 *%-----|-----|
4163 COMPUTE DUALHYD  NHYDin=["A6T"], CINLET=[0.357](cms), NINLET=[1],
4164 *           MajNHYD=["A6-MJ"]
4165 *           MinNHYD=["A6-MN"]
4166 *           TMJSTO=[60](cu-m)
4167 *%-----|-----|
4168 * -JFSA Jan. 2021, A7-corrig is a part of Todd so it is removed
4169 *CONTINUOUS STANDHYD NHYD=["A7-corrig"], DT=[1]min, AREA=[11.8](ha),
4170 *           XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4171 *           SCS curve number CN=[75],
4172 *           Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4173 *           LGP=[40](m), MNP=[0.25], SCP=[0](min),
4174 *           Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4175 *           LGI=[438](m), MNI=[0.013], SCI=[0](min),
4176 *           Continuous simulation parameters:
4177 *           IaREcper=[4](hrs), IaREcimp=[4](hrs),
4178 *           SMIN=[-1](mm),  SMAx=[-1](mm), SK=[0.010]/(mm),
4179 *           InterEventTime=[18](hrs),  END=-1
4180 *%-----|-----|
4181 *ADD HYD           NHYDsum=["A7-A3RMJ"], NHYDs to add=["A3R-MJ"+"A7-corrig"]
4182 *%-----|-----|
4183 *COMPUTE DUALHYD  NHYDin=["A7-A3RMJ"], CINLET=[1.003](cms), NINLET=[1],
4184 *           MajNHYD=["A7R-MJ"]
4185 *           MinNHYD=["A7R-MN"]
4186 *           TMJSTO=[496](cu-m)
4187 *%-----|-----|
4188 ADD HYD           NHYDsum=["MH104"], NHYDs to add=["A6-MN"+"103-104"+"TODD_MJn"]
4189 *%-----|-----|
4190 SAVE HYD          NHYD=["MH104"], # OF PCYCLES=[-1], ICASEsh=[1]

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4191 HYD_COMMENT=["Total Flows at MH104"]
4192 *%-----|-----|
4193 CONTINUOUS STANDHYD NHYD=["B2"], DT=[1]min, AREA=[12.31](ha),
4194 XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4195 SCS curve number CN=[75],
4196 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4197 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4198 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4199 LGI=[417](m), MNI=[0.013], SCI=[0](min),
4200 Continuous simulation parameters:
4201 IaREcper=[4](hrs), IaREcimp=[4](hrs),
4202 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4203 InterEventTime=[18](hrs), END=-1
4204 *%-----|-----|
4205 COMPUTE DUALHYD NHYDin=["B2"], CINLET=[1.029](cms), NINLET=[1],
4206 MajNHYD=["B2-MJ"]
4207 MinNHYD=["B2-MN"]
4208 TMJSTO=[508](cu-m)
4209 *%-----|-----|
4210 ROUTE PIPE PTYPE=[1]circ, NHYDout=["315-333"], RNUMBER=[1.0], PDIAM=[1200](mm),
4211 PLNGTH=[254](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["B2-MN"], RDT=[1]
4212 *%-----|-----|
4213 CONTINUOUS STANDHYD NHYD=["B3"], DT=[1]min, AREA=[5.59](ha),
4214 XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4215 SCS curve number CN=[75],
4216 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4217 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4218 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4219 LGI=[345](m), MNI=[0.013], SCI=[0](min),
4220 Continuous simulation parameters:
4221 IaREcper=[4](hrs), IaREcimp=[4](hrs),
4222 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4223 InterEventTime=[18](hrs), END=-1
4224 *%-----|-----|
4225 COMPUTE DUALHYD NHYDin=["B3"], CINLET=[0.459](cms), NINLET=[1],
4226 MajNHYD=["B3-MJ"]
4227 MinNHYD=["B3-MN"]
4228 TMJSTO=[227](cu-m)
4229 *%-----|-----|
4230 ADD HYD NHYDsum=["MH333"], NHYDs to add=["B3-MN"+"315-333"]
4231 *%-----|-----|
4232 SAVE HYD NHYD=["MH333"], # OF PCYCLES=[-1], ICASEsh=[1]
4233 HYD_COMMENT=["Total Flows at MH333"]
4234 *%-----|-----|
4235 ROUTE PIPE PTYPE=[1]circ, NHYDout=["333-335"], RNUMBER=[1.0], PDIAM=[1200](mm),
4236 PLNGTH=[251](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["MH333"], RDT=[1]
4237 *%-----|-----|
4238 ROUTE PIPE PTYPE=[1]circ, NHYDout=["335-338"], RNUMBER=[1.0], PDIAM=[1200](mm),
4239 PLNGTH=[185](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["333-335"], RDT=[1]
4240 *%-----|-----|
4241 ROUTE PIPE PTYPE=[1]circ, NHYDout=["338-340"], RNUMBER=[1.0], PDIAM=[1350](mm),
4242 PLNGTH=[233](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["335-338"], RDT=[1]
4243 *%-----|-----|
4244 CONTINUOUS STANDHYD NHYD=["B4"], DT=[1]min, AREA=[7.6](ha),
4245 XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4246 SCS curve number CN=[75],
4247 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4248 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4249 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4250 LGI=[388](m), MNI=[0.013], SCI=[0](min),
4251 Continuous simulation parameters:
4252 IaREcper=[4](hrs), IaREcimp=[4](hrs),

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4314 *%-----|-----|
4315 DIVERT HYD NHYDin=["A8-MJ"] NIDout=[2]max five,
4316 outflow hydrographs (NHYDs)=["A8-MJ-JR" "A8-MJ-B6"]
4317 flow distribution table: (modify as necessary)
4318 Note: all flows are in (cms)
4319 QIDi + QIDii = QTOTAL
4320 [ 0 + 0 = 0 ]
4321 [ 50 + 50 = 100 ] end
4322 *%-----|-----|
-----|-----|
4323 DIVERT HYD NHYDin=["MH105"] NIDout=[2]max five,
4324 outflow hydrographs (NHYDs)=["MH105-JR" "MH105-B6"]
4325 flow distribution table: (modify as necessary)
4326 Note: all flows are in (cms)
4327 QIDi + QIDii = QTOTAL
4328 [ 0 + 0 = 0 ]
4329 [ 0 + 3.0 = 3.0 ]
4330 [ 96.9+ 3.1 = 100 ] end
4331 *%-----|-----|
-----|-----|
4332 CONTINUOUS STANDHYD NHYD=["B7"], DT=[1]min, AREA=[7.19](ha),
4333 XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4334 SCS curve number CN=[75],
4335 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4336 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4337 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4338 LGI=[211](m), MNI=[0.013], SCI=[0](min),
4339 Continuous simulation parameters:
4340 IaREcper=[4](hrs), IaREcimp=[4](hrs),
4341 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4342 InterEventTime=[18](hrs), END=-1
4343 *%-----|-----|
4344 ADD HYD NHYDsum=["B7-B4MJ"], NHYDs to add=["B4-MJ"+"B7"]
4345 *%-----|-----|
4346 COMPUTE DUALHYD NHYDin=["B7-B4MJ"], CINLET=[0.629](cms), NINLET=[1],
4347 MajNHYD=["B7R-MJ"]
4348 MinNHYD=["B7R-MN"]
4349 TMJSTO=[311](cu-m)
4350 *%-----|-----|
4351 ROUTE PIPE PTYPE=[1]circ, NHYDout=["360-106A"], RNUMBER=[1.0], PDIAM=[1050](mm),
4352 PLNGTH=[167](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["B7R-MN"], RDT=[1]
4353 *%-----|-----|
4354 * -JFSA 2021-01-19 change B6 to be developed as per geottawa website and apply the
parameters of A7, the nearest sub-catchment to B6, LGI is calculated based on B6 area
4355 CONTINUOUS STANDHYD NHYD=["B6"], DT=[1]min, AREA=[3.29](ha),
4356 XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4357 SCS curve number CN=[75],
4358 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4359 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4360 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4361 LGI=[148.099](m), MNI=[0.013], SCI=[0](min),
4362 Continuous simulation parameters:
4363 IaREcper=[4](hrs), IaREcimp=[4](hrs),
4364 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4365 InterEventTime=[18](hrs), END=-1
4366 *%-----|-----|
4367 * -JFSA 2021-01-25 add B1 DUALHYD as per Corrigan Report, IBI Group, 2008
4368 COMPUTE DUALHYD NHYDin=["B6"], CINLET=[0.064](cms), NINLET=[1],
4369 MajNHYD=["B6-MJ"]
4370 MinNHYD=["B6-MN"]
4371 TMJSTO=[5484](cu-m)
4372 *%-----|-----|
4373 *CONTINUOUS NASHYD NHYD=["B6"], DT=[1]min, AREA=[3.29](ha),
4374 * DWF=[0](cms), CN/C=[75], IA=[2.5](mm),
4375 * N=[3.0], TP=[0.36]hrs,

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4376 *           Continuous simulation parameters:
4377 *           IaRECper=[4](hrs),
4378 *           SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
4379 *           InterEventTime=[12](hrs)
4380 *           Baseflow simulation parameters:
4381 *           BaseFlowOption=[1] ,
4382 *           InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4383 *           VHydCond=[0.055](mm/hr),  END=-1
4384 *%-----|-----|
4385 *%   -EX-LAND is external land. It is a part of JOCKVA sub-catchment as per Corrigan
Report, IBI Group, 2008
4386 CONTINUOUS STANDHYD NHYD=["EX-LAND"], DT=[1]min, AREA=[32.5](ha),
4387 XIMP=[0.50], TIMP=[0.50], DWF=[0](cms), LOSS=[2],
4388 SCS curve number CN=[74],
4389 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4390 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4391 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4392 LGI=[465.475](m), MNI=[0.013], SCI=[0](min),
4393 Continuous simulation parameters:
4394 IaRECper=[4](hrs),  IaRECimp=[4](hrs),
4395 SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
4396 InterEventTime=[18](hrs),  END=-1
4397 *%-----|-----|
4398 COMPUTE DUALHYD NHYDin=["EX-LAND"], CINLET=[2.275](cms), NINLET=[1],
4399 MajNHYD=["EX-LAND-MJ"]
4400 MinNHYD=["EX-LAND-MN"]
4401 TMJSTO=[1365](cu-m)
4402 *%-----|-----|
4403 ADD HYD NHYDsum=["B6-B7ExMJ"], NHYDs to
add=["B7R-MJ"+"EX-LAND-MJ"+"B5-MJ"+"B6-MJ"+"B6-MN"+"A8-MJ-B6"]
4404 *%-----|-----|
4405 COMPUTE DUALHYD NHYDin=["B6-B7ExMJ"], CINLET=[0.064](cms), NINLET=[1],
4406 MajNHYD=["B6R-MJ"]
4407 MinNHYD=["B6R-MN"]
4408 TMJSTO=[5484](cu-m)
4409 *%-----|-----|
4410 ROUTE PIPE PTYPE=[1]circ, NHYDout=["105-106A"], RNUMBER=[1.0], PDIAM=[1800](mm),
4411 PLNGTH=[208](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["MH105-B6"], RDT=[1]
4412 *%-----|-----|
4413 ADD HYD NHYDsum=["MH106A"], NHYDs to
add=["360-106A"+"105-106A"+"B6R-MN"+"B6R-MJ"]
4414 *%-----|-----|
4415 SAVE HYD NHYD=["MH106A"], # OF PCYCLES=[-1], ICASEsh=[1]
4416 HYD_COMMENT=["Total Flows at MH106A"]
4417 *%-----|-----|
4418 *%   -JFSA 2021-01-12 THE MANHOLE MH106 is called MH117/106 in Corrigan Report, IBI
Group, July 2008
4419 *%
4420 ROUTE PIPE PTYPE=[1]circ, NHYDout=["106A-106"], RNUMBER=[1.0], PDIAM=[1800](mm),
4421 PLNGTH=[190](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["MH106A"], RDT=[1]
4422 *%-----|-----|
4423 CONTINUOUS STANDHYD NHYD=["A9"], DT=[1]min, AREA=[2.44](ha),
4424 XIMP=[0.71], TIMP=[0.71], DWF=[0](cms), LOSS=[2],
4425 SCS curve number CN=[75],
4426 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4427 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4428 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4429 LGI=[262](m), MNI=[0.013], SCI=[0](min),
4430 Continuous simulation parameters:
4431 IaRECper=[4](hrs),  IaRECimp=[4](hrs),
4432 SMIN=[-1](mm),  SMAX=[-1](mm), SK=[0.010]/(mm),
4433 InterEventTime=[18](hrs),  END=-1
4434 *%-----|-----|
4435 COMPUTE DUALHYD NHYDin=["A9"], CINLET=[0.547](cms), NINLET=[1],

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4436      MajNHYD=["A9-MJ"]
4437      MinNHYD=["A9-MN"]
4438      TMJSTO=[0](cu-m)
4439  *%-----|-----|
4440  ADD HYD      NHYDsum=["MH106"], NHYDs to add=["106A-106"+"A9-MN"]
4441  *%-----|-----|
4442  SAVE HYD     NHYD=["MH106"], # OF PCYCLES=[-1], ICASEsh=[1]
4443      HYD_COMMENT=["Total Flows at MH106"]
4444  *%-----|-----|
4445  *%      -JFSA 2021-01-12 THE MANHOLE MH107 is called MH118/107 in Corrigan Report, IBI
Group, July 2008
4446  *%-----|-----|
4447  ROUTE PIPE   PTYPE=[1]circ, NHYDout=["106-107"], RNUMBER=[1.0], PDIAM=[1800](mm),
4448      PLNGTH=[122.5](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
NHYDin=["MH106"], RDT=[1]
4449  *%-----|-----|
4450  CONTINUOUS STANDHYD NHYD=["A10"], DT=[1]min, AREA=[4.14](ha),
4451      XIMP=[0.35], TIMP=[0.47], DWF=[0](cms), LOSS=[2],
4452      SCS curve number CN=[75],
4453      Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4454          LGP=[40](m), MNP=[0.25], SCP=[0](min),
4455      Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4456          LGI=[183](m), MNI=[0.013], SCI=[0](min),
4457      Continuous simulation parameters:
4458      IaREcper=[4](hrs), IaREcimp=[4](hrs),
4459      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4460      InterEventTime=[18](hrs), END=-1
4461  *%-----|-----|
4462  COMPUTE DUALHYD NHYDin=["A10"], CINLET=[0.310](cms), NINLET=[1],
4463      MajNHYD=["A10-MJ"]
4464      MinNHYD=["A10-MN"]
4465      TMJSTO=[228](cu-m)
4466  *%-----|-----|
4467  CONTINUOUS STANDHYD NHYD=["A11"], DT=[1]min, AREA=[10.61](ha),
4468      XIMP=[0.53], TIMP=[0.62], DWF=[0](cms), LOSS=[2],
4469      SCS curve number CN=[75],
4470      Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4471          LGP=[40](m), MNP=[0.25], SCP=[0](min),
4472      Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4473          LGI=[379](m), MNI=[0.013], SCI=[0](min),
4474      Continuous simulation parameters:
4475      IaREcper=[4](hrs), IaREcimp=[4](hrs),
4476      SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4477      InterEventTime=[18](hrs), END=-1
4478  *%-----|-----|
4479  COMPUTE DUALHYD NHYDin=["A11"], CINLET=[0.993](cms), NINLET=[1],
4480      MajNHYD=["A11-MJ"]
4481      MinNHYD=["A11-MN"]
4482      TMJSTO=[556](cu-m)
4483  *%-----|-----|
4484  ADD HYD      NHYDsum=["MH107"], NHYDs to add=["106-107"+"A10-MN"+"A11-MN"]
4485  *%-----|-----|
4486  SAVE HYD     NHYD=["MH107"], # OF PCYCLES=[-1], ICASEsh=[1]
4487      HYD_COMMENT=["Total Flows at MH107"]
4488  *%-----|-----|
4489  ROUTE PIPE   PTYPE=[1]circ, NHYDout=["107-119"], RNUMBER=[1.0], PDIAM=[1800](mm),
4490      PLNGTH=[114](m), PROUGH=[0.013], PSLOPE=[0.0012](m/m),
NHYDin=["MH107"], RDT=[1]
4491  *%-----|-----|
4492  *%      -JFSA 2021-01-12 THE MANHOLE MH108 is called MH120/108 in Corrigan Report, IBI
Group, July 2008
4493  *%-----|-----|
4494  ROUTE PIPE   PTYPE=[1]circ, NHYDout=["119-108"], RNUMBER=[1.0], PDIAM=[1800](mm),
4495      PLNGTH=[65.8](m), PROUGH=[0.013], PSLOPE=[0.0012](m/m),
NHYDin=["107-119"], RDT=[1]
4496  *%-----|-----|

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4497 CONTINUOUS STANDHYD NHYD=["A12"], DT=[1]min, AREA=[12.29](ha),
4498 XIMP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4499 SCS curve number CN=[75],
4500 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4501 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4502 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4503 LGI=[183](m), MNI=[0.013], SCI=[0](min),
4504 Continuous simulation parameters:
4505 IaRECPper=[4](hrs), IaRECImp=[4](hrs),
4506 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4507 InterEventTime=[18](hrs), END=-1
4508 *%-----|
4509 COMPUTE DUALHYD NHYDin=["A12"], CINLET=[1.029](cms), NINLET=[1],
4510 MajNHYD=["A12-MJ"]
4511 MinNHYD=["A12-MN"]
4512 TMJSTO=[672](cu-m)
4513 *%-----|
4514 CONTINUOUS STANDHYD NHYD=["A13"], DT=[1]min, AREA=[2.59](ha),
4515 XIMP=[0.71], TIMP=[0.71], DWF=[0](cms), LOSS=[2],
4516 SCS curve number CN=[75],
4517 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4518 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4519 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4520 LGI=[379](m), MNI=[0.013], SCI=[0](min),
4521 Continuous simulation parameters:
4522 IaRECPper=[4](hrs), IaRECImp=[4](hrs),
4523 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4524 InterEventTime=[18](hrs), END=-1
4525 *%-----|
4526 COMPUTE DUALHYD NHYDin=["A13"], CINLET=[0.571](cms), NINLET=[1],
4527 MajNHYD=["A13-MJ"]
4528 MinNHYD=["A13-MN"]
4529 TMJSTO=[0](cu-m)
4530 *%-----|
4531 * -JFSA 2021-01-22 add the Corrigan pond area ("Pond-Block")
4532 CONTINUOUS STANDHYD NHYD=["Pond-Block"], DT=[1]min, AREA=[2.94](ha),
4533 XIMP=[0.415], TIMP=[0.415], DWF=[0](cms), LOSS=[2],
4534 SCS curve number CN=[75],
4535 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4536 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4537 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4538 LGI=[183](m), MNI=[0.013], SCI=[0](min),
4539 Continuous simulation parameters:
4540 IaRECPper=[4](hrs), IaRECImp=[4](hrs),
4541 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4542 InterEventTime=[18](hrs), END=-1
4543 *%-----|
4544 ADD HYD NHYDsum=["MH108"], NHYDs to add=["119-108"+"A13-MN"+"A12-MN"]
4545 *%-----|
4546 SAVE HYD NHYD=["MH108"], # OF PCYCLES=[-1], ICASEsh=[1]
4547 HYD_COMMENT=["Total Flows at MH108"]
4548 *%-----|
4549 ROUTE PIPE PTYPE=[1]circ, NHYDout=["108-116"], RNUMBER=[1.0], PDIAM=[1800](mm),
4550 PLNGTH=[76.6](m), PROUGH=[0.013], PSLOPE=[0.0013](m/m),
NHYDin=["MH108"], RDT=[1]
4551 *%-----|
4552 ROUTE PIPE PTYPE=[1]circ, NHYDout=["116-corrig"], RNUMBER=[1.0],
4553 PDIAM=[1800](mm),
PLNGTH=[79.5](m), PROUGH=[0.013], PSLOPE=[0.0013](m/m),
NHYDin=["108-116"], RDT=[1]
4554 *%-----|
4555 ADD HYD NHYDsum=["Corrigan"], NHYDs to add=["116-corrig"+"Pond-Block"]
4556 *%-----|
4557 SAVE HYD NHYD=["Corrigan"], # OF PCYCLES=[-1], ICASEsh=[1]
4558 HYD_COMMENT=["Total Flows at Corrigan Pond"]
4559 *%-----|

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4560 ROUTE RESERVOIR      NHYDout=["Co-P"],  NHYDin=["Corrigan"],
4561 RDT=[1](min),
4562          TABLE of ( OUTFLOW-STORAGE ) values
4563                    (cms) - (ha-m)
4564                    [ 0.0 , 0.0 ]
4565                    [ 0.015 , 0.04118]
4566                    [ 0.030 , 0.08297]
4567                    [ 0.045 , 0.12537]
4568                    [ 0.060 , 0.16837]
4569                    [ 0.075 , 0.21199]
4570                    [ 0.090 , 0.27545]
4571                    [ 0.105 , 0.34650]
4572                    [ 0.120 , 0.42049]
4573                    [ 0.135 , 0.50188]
4574                    [ 0.186 , 0.60307]
4575                    [ 2.110 , 0.79083]
4576                    [ 5.874 , 1.00271]
4577                    [ 11.395 , 1.29643]
4578                    [ 18.770 , 1.62054]
4579                    [ 28.143 , 1.97516]
4580                    [ -1 , -1 ] (max twenty pts)
4581          NHYDovf=["Co-P-OVF"]
4582 *%-----|-----|
4583 ADD HYD      NHYDsum=["corrig"], NHYDs to
add=["Co-P-OVF"+"Co-P"+"N_TO"+"MH105-JR"+"A8-MJ-JR"+"A9-MJ"+"A10-MJ"+"A11-MJ"+"A12-MJ"+"A
13-MJ"]
4584 *%-----|-----|
4585 SAVE HYD     NHYD=["corrig"], # OF PCYCLES=[-1], ICASEsh=[1]
4586             HYD_COMMENT=["Total Flows at Corrigan Pond"]
4587 *%-----|-----|
4588 *#*****|*****|
4589 *#   Corrigan Pond 1
4590 *#   - Rating curve obtained from Barrhaven South MSS modeling
4591 *#   - Tributary Drainage Area to MSS Pond 1 = 145 ha
4592 *#*****|*****|
4593 *ROUTE RESERVOIR      NHYDout=["MS_P1"],  NHYDin=["CORRIG"],
4594 * RDT=[1](min),
4595 *          TABLE of ( OUTFLOW-STORAGE ) values
4596 *                    (cms) - (ha-m)
4597 *                    [ 0.0 , 0.0 ]
4598 *                    [ 0.06 , 0.58]
4599 *                    [ -1 , -1 ] (max twenty pts)
4600 *          NHYDovf=["P1-OVF"]
4601 *%-----|-----|
4602 *ADD HYD      NHYDsum=["SN_CO"], NHYDs to add=["N_TO"+"P1-OVF"+"MS_P1"]
4603 *%-----|-----|
4604 *SAVE HYD     NHYD=["SN_CO"], # OF PCYCLES=[-1], ICASEsh=[1]
4605 *             HYD_COMMENT=["Total Flows at Corrigan Drain"]
4606 *%-----|-----|
4607 *#
4608 *# Hydrograph from Corrigan Drain routed to Jockvale Road
4609 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
4610 *#
4611 ROUTE CHANNEL      NHYDout=["N_MI"] ,NHYDin=["corrig"] ,
4612 RDT=[1](min),
4613 CHLGTH=[580](m),  CHSLOPE=[0.4448](%),
4614                    FPSLOPE=[0.4448](%),
4615 SECNUM=[1.0],      NSEG=[3]
4616 ( SEGROUGH, SEGDIST (m))=
4617 [0.075,-17.72
4618 -0.045,17.72
4619 0.075,80.62] NSEG times
4620 ( DISTANCE (m), ELEVATION (m))=
4621 [-83.32, 90.00]
4622 [-81.36, 89.50]
4623 [-79.12, 89.00]

```

```

4624      [-76.13, 88.50]
4625      [-20.46, 88.00]
4626      [-19.36, 87.50]
4627      [-18.51, 87.00]
4628      [-17.72, 86.50]
4629      [-11.95, 85.24]
4630      [-0.11, 85.12]
4631      [11.49, 85.20]
4632      [17.72, 86.50]
4633      [19.74, 87.00]
4634      [21.22, 87.50]
4635      [22.68, 88.00]
4636      [24.28, 88.50]
4637      [26.79, 89.00]
4638      [71.98, 90.00]
4639      [80.62, 90.50]

```

```

4640 *%-----|-----|
4641 *#*****|-----|

```

```

4642 *#   Catchment MILLS
4643 *#   - To SWM Facility north of the Jock
4644 *#   - Primarily residential development
4645 *#*****|-----|

```

```

4646 CONTINUOUS STANDHYD NHYD=["MILLS"], DT=[1]min, AREA=[175.99](ha),
4647 XIMP=[0.38], TIMP=[0.38], DWF=[0](cms), LOSS=[2],
4648 SCS curve number CN=[74],
4649 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4650 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4651 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4652 LGI=[1118.123](m), MNI=[0.013], SCI=[0](min),
4653 Continuous simulation parameters:
4654 IaRECper=[4](hrs), IaRECimp=[4](hrs),
4655 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4656 InterEventTime=[18](hrs), END=-1

```

```

4657 *%-----|-----|
4658 *#*****|-----|

```

```

4659 *#   Chapman Mills SWM Pond
4660 *#   - Rating curve obtained from CCL hydraulic modeling
4661 *#*****|-----|

```

```

4662 ROUTE RESERVOIR      NHYDout=["MILL_P"], NHYDin=["MILLS"],
4663 RDT=[1](min),
4664           TABLE of ( OUTFLOW-STORAGE ) values
4665                   (cms) - (ha-m)
4666                   [ 0.0 , 0.0 ]
4667                   [ 0.01 , 0.01]
4668                   [ 0.05 , 0.06]
4669                   [ 0.09 , 0.11]
4670                   [ 0.13 , 0.15]
4671                   [ 0.18 , 0.19]
4672                   [ 0.28 , 0.28]
4673                   [ 0.37 , 0.34]
4674                   [ 0.45 , 0.40]
4675                   [ 0.51 , 0.44]
4676                   [ 0.56 , 0.47]
4677                   [ 0.64 , 0.52]
4678                   [ 0.76 , 0.59]
4679                   [ 0.86 , 0.65]
4680                   [ 1.09 , 0.78]
4681                   [ 1.44 , 0.96]
4682                   [ 3.18 , 1.84]
4683                   [ 4.05 , 2.31]
4684                   [ -1 , -1 ] (max twenty pts)
4685                   NHYDovf=["MIL-OV"]

```

```

4686 *%-----|-----|
4687 ADD HYD      NHYDsum=["SN_MI"], NHYDs to add=["N_MI"+"MIL-OV"+"MILL_P"]
4688 *%-----|-----|

```

```

4689 SAVE HYD      NHYD=["SN_MI"], # OF PCYCLES=[-1], ICASEsh=[1]

```

```

4690 HYD_COMMENT=["Total Flows at Jockvale Road"]
4691 *%-----|-----|
4692 *#
4693 *# Hydrograph from Jockvale Road routed to Heart's Desire
4694 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 689
4695 *#
4696 ROUTE CHANNEL NHYDout=["N_DE"] ,NHYDin=["SN_MI"] ,
4697 RDT=[1](min),
4698 CHLGTH=[1962](m), CHSLOPE=[0.2227](%),
4699 FPSLOPE=[0.2227](%),
4700 SECNUM=[1.0], NSEG=[3]
4701 ( SEGROUGH, SEGDIST (m))=
4702 [0.075,-17.56
4703 -0.045,18.27
4704 0.075,32.51] NSEG times
4705 ( DISTANCE (m), ELEVATION (m))=
4706 [-54.07, 85.00]
4707 [-39.43, 84.50]
4708 [-28.30, 84.00]
4709 [-24.12, 83.50]
4710 [-22.30, 83.00]
4711 [-20.55, 82.50]
4712 [-17.56, 82.00]
4713 [-12.63, 81.22]
4714 [-0.11, 80.75]
4715 [11.55, 81.22]
4716 [18.27, 82.00]
4717 [19.82, 82.50]
4718 [22.48, 83.00]
4719 [27.90, 83.50]
4720 [29.31, 84.00]
4721 [30.81, 84.50]
4722 [32.51, 85.00]
4723 *%-----|-----|
4724 *#*****
4725 *# Catchment DESIRE
4726 *# - To Jock River (north of the Jock)
4727 *# - Rural-estate subdivision (Heart's Desire Community)
4728 *#*****
4729 CONTINUOUS STANDHYD NHYD=["DESIRE"], DT=[1]min, AREA=[23.78](ha),
4730 XIMP=[0.25], TIMP=[0.25], DWF=[0](cms), LOSS=[2],
4731 SCS curve number CN=[77],
4732 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4733 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4734 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4735 LGI=[400](m), MNI=[0.013], SCI=[0](min),
4736 Continuous simulation parameters:
4737 IaREcper=[4](hrs), IaREcimp=[4](hrs),
4738 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4739 InterEventTime=[18](hrs), END=-1
4740 *%-----|-----|
4741 *#*****
4742 *# Catchment JOCKVA
4743 *# - To Jockvale SWM Facility
4744 *# - Residential development & golf course
4745 *# - JFSA 2021-01-11 update JOCKVA after updating CORRIG as per IBI GROUP, July 2008.
4746 *# JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two
4747 *# areas JOCKVA and EX-LAND 32.5 ha as per IBI GROUP, July 2008.
4748 *#*****
4749 CONTINUOUS STANDHYD NHYD=["JOCKVA"], DT=[1]min, AREA=[225.13](ha),
4750 XIMP=[0.50], TIMP=[0.50], DWF=[0](cms), LOSS=[2],
4751 SCS curve number CN=[74],
4752 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4753 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4754 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4755 LGI=[1310.55](m), MNI=[0.013], SCI=[0](min),

```

```

4755 Continuous simulation parameters:
4756 IaREcper=[4](hrs), IaREcimp=[4](hrs),
4757 SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4758 InterEventTime=[18](hrs), END=-1
4759 *%-----|-----|
4760 ADD HYD NHYDsum=["JOCKVA-TO"], NHYDs to
add=["EX-LAND-MN"+"JOCKVA"+"B2-MJ"+"B3-MJ"]
4761 *%-----|-----|
4762 SAVE HYD NHYD=["JOCKVA-TO"], # OF PCYCLES=[-1], ICASEsh=[1]
4763 HYD_COMMENT=["Total Flows at KB first pond"]
4764 *%-----|-----|
4765 *#*****|*****|
4766 *# Jockvale SWM Facility
4767 *# - Rating curve obtained from Jockvale Servicing Study (CCL 1999)
4768 *#*****|*****|
4769 ROUTE RESERVOIR NHYDout=["JOCK_P"], NHYDin=["JOCKVA-TO"],
4770 RDT=[1](min),
4771 TABLE of ( OUTFLOW-STORAGE ) values
4772 (cms) - (ha-m)
4773 [ 0.0 , 0.0 ]
4774 [ 0.27 , 0.03]
4775 [ 0.28 , 0.55]
4776 [ 0.29 , 1.14]
4777 [ 0.30 , 1.80]
4778 [ 0.31 , 2.32]
4779 [ 1.12 , 2.87]
4780 [ 2.92 , 3.45]
4781 [ 4.64 , 4.07]
4782 [ 6.69 , 4.72]
4783 [ 9.02 , 5.39]
4784 [ 11.62 , 6.10]
4785 [ 14.42 , 6.85]
4786 [ 17.45 , 7.62]
4787 [ 20.69 , 8.44]
4788 [ 24.08 , 9.28]
4789 [ 27.68 , 10.17]
4790 [ -1 , -1 ] (max twenty pts)
4791 NHYDovf=["JO-OVF"]
4792 *%-----|-----|
4793 ADD HYD NHYDsum=["SN_DE"], NHYDs to add=["N_DE"+"DESIRE"+"JO-OVF"+"JOCK_P"]
4794 *%-----|-----|
4795 SAVE HYD NHYD=["SN_DE"], # OF PCYCLES=[-1], ICASEsh=[1]
4796 HYD_COMMENT=["Total Flows at Heart's Desire"]
4797 *%-----|-----|
4798 *#
4799 *# Hydrograph from Heart's Desire routed to Rideau River
4800 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 0
4801 *#
4802 ROUTE CHANNEL NHYDout=["N1"] ,NHYDin=["SN_DE"] ,
4803 RDT=[1](min),
4804 CHLGTH=[563](m), CHSLOPE=[0.9668](%),
4805 FPSLOPE=[0.9668](%),
4806 SECNUM=[1.0], NSEG=[3]
4807 ( SEGROUGH, SEGDIST (m))=
4808 [0.075,-30.20
4809 -0.045,30.20
4810 0.075,48.48] NSEG times
4811 ( DISTANCE (m), ELEVATION (m))=
4812 [-98.46, 81.50]
4813 [-92.24, 81.00]
4814 [-86.88, 80.50]
4815 [-81.54, 80.00]
4816 [-74.36, 79.50]
4817 [-63.54, 79.00]
4818 [-39.23, 78.50]
4819 [-34.51, 78.00]

```



```

4820          [-33.01, 77.50]
4821          [-30.20, 77.00]
4822          [-13.42, 76.18]
4823          [-1.14, 76.09]
4824          [17.06, 76.18]
4825          [30.20, 77.00]
4826          [32.95, 77.50]
4827          [34.06, 78.00]
4828          [35.11, 78.50]
4829          [36.32, 79.00]
4830          [37.74, 79.50]
4831          [48.48, 81.50]
4832  *%-----|-----|
4833  *#*****|*****|
4834  *#      Catchment S-2
4835  *#      - To Jock River (north and south)
4836  *#      - Undeveloped floodplain and river
4837  *#*****|*****|
4838  CONTINUOUS NASHYD  NHYD=["S-2"], DT=[1]min, AREA=[102.94](ha),
4839                    DWF=[0](cms), CN/C=[72], IA=[4.67](mm),
4840                    N=[3], TP=[0.40]hrs,
4841                    Continuous simulation parameters:
4842                    IaREcper=[4](hrs),
4843                    SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4844                    InterEventTime=[12](hrs)
4845                    Baseflow simulation parameters:
4846                    BaseFlowOption=[1] ,
4847                    InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4848                    VHydCond=[0.055](mm/hr), END=-1
4849  *%-----|-----|
4850  ADD HYD            NHYDsum=["SN_N1"], NHYDs to add=["N1"+"S-2"]
4851  *%-----|-----|
4852  SAVE HYD          NHYD=["SN_N1"], # OF PCYCLES=[-1], ICASEsh=[1]
4853                    HYD_COMMENT=["Total Flows at Rideau River"]
4854  *%-----|-----|
4855  *#####|#####|
4856  *% 5 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4857  START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[5]
4858  *%              ["C24SC005.stm"] <--storm filename, one per line for NSTORM time
4859  *%-----|-----|
4860  *% 10 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4861  START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[10]
4862  *%              ["C24SC010.stm"] <--storm filename, one per line for NSTORM time
4863  *%-----|-----|
4864  *% 25 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4865  START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[25]
4866  *%              ["C24SC025.stm"] <--storm filename, one per line for NSTORM time
4867  *%-----|-----|
4868  *% 50 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4869  START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[50]
4870  *%              ["C24SC050.stm"] <--storm filename, one per line for NSTORM time
4871  *%-----|-----|
4872  *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4873  *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4874  *%              ["100YC3H.STM"] <--storm filename, one per line for NSTORM time
4875  *%-----|-----|
4876  *% 100 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4877  START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4878  *%              ["C24SC100.stm"] <--storm filename, one per line for NSTORM time
4879  *%-----|-----|
4880  *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4881  *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4882  *%              ["C24SC100.stm"] <--storm filename, one per line for NSTORM time
4883  *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[101]
4884  *%              ["A24SC100.stm"] <--storm filename, one per line for NSTORM time
4885  *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[102]

```

```
4886  *% ["A24SC100_60.stm"] <--storm filename, one per line for NSTORM time
4887  FINISH
4888
```

```

00001 .....
00002 .....
00003 SSSS W W M M H H Y Y V V M M OOO 222 000 11 5555 .....
00004 S W W M M H H T T M M M O O 2 0 0 11 5 .....
00005 SSSS W W M M M H H H H Y Y M M M O O 2 0 0 11 5 Ver 5.800 .....
00006 S W W M M H H Y Y M M O O 222 0 0 11 555 PRE 2015 .....
00007 SSSS W W M M H H Y Y M M O O 2 0 0 11 5 .....
00008 .....
00009 Stormwater Management Hydrologic Model 222 0 0 11 5 .....
00010 .....
00011 .....
00012 ***** SWHYMO Ver 5.800 ***** .....
00013 ***** A single event and continuous hydrologic simulation model ***** .....
00014 ***** based on the principles of HMO and its successors ***** .....
00015 ***** OTHYMO=83 and OTHYMO=89 ***** .....
00016 ***** .....
00017 ***** Distributed by: J.F. Sabourin and Associates Inc. ***** .....
00018 ***** Ottawa, Ontario: (613) 886-8884 ***** .....
00019 ***** Gatineau, Quebec: (819) 243-6858 ***** .....
00020 ***** E-Mail: swmhy@jfsa.com ***** .....
00021 ***** .....
00022 ***** .....
00023 ***** .....
00024 ***** Licensed user: JFSaInc ***** .....
00025 ***** Ottawa SERIAL#:2549237 ***** .....
00026 ***** .....
00027 ***** .....
00028 ***** .....
00029 ***** PROGRAM ARRAY DIMENSIONS ***** .....
00030 ***** Maximum value for ID numbers : 11 ***** .....
00031 ***** Max. number of rainfall points: 105408 ***** .....
00032 ***** Max. number of flow points : 105408 ***** .....
00033 ***** .....
00034 ***** .....
00035 ***** SUMMARY OUTPUT ***** .....
00036 ***** .....
00037 ***** RUN DATE: 2021-03-04 TIME: 11:57:49 RUN COUNTER: 020284 ***** .....
00038 ***** .....
00039 ***** Input file: T:\PROJ\1474-16\Design\20210206-QuantityControlAnalysis\SWHYMO\SMH-Model\Updated\ *****
00040 ***** 3\SMR_S-1_SMR-PP_S.DAT ***** .....
00041 ***** .....
00042 ***** Output file: T:\PROJ\1474-16\Design\20210206-QuantityControlAnalysis\SWHYMO\SMH-Model\Updated\ *****
00043 ***** 3\SMR_S-1_SMR-PP_S.DAT ***** .....
00044 ***** Summary file: T:\PROJ\1474-16\Design\20210206-QuantityControlAnalysis\SWHYMO\SMH-Model\Updated\ *****
00045 ***** 3\SMR_S-1_SMR-PP_S.DAT ***** .....
00046 ***** User comment: ***** .....
00047 ***** 1: ***** .....
00048 ***** 2: ***** .....
00049 ***** 3: ***** .....
00050 ***** ***** .....
00051 ***** .....
00052 ***** .....
00053 ***** .....
00054 ***** SWHYMO Ver 5.800 ***** INPUT DATA FILE ***** .....
00055 ***** .....
00056 ***** Project Name: [Jock River] Project Number: [1474-16] ***** .....
00057 ***** Date [04-03-2021] ***** .....
00058 ***** Modeller [J.F.M.] ***** .....
00059 ***** Company [JFSaInc.] ***** .....
00060 ***** License # [2549237] ***** .....
00061 ***** ***** .....
00062 ***** CALIBRATION OF SUMMER MODEL PARAMETERS ***** .....
00063 ***** USING CONTINUOUS SIMULATIONS ***** .....
00064 ***** Rainfall data from JFSa raingage installed at site + other gauges by the City ***** .....
00065 ***** Use data collected from May 1st to July 14, 2003 ***** .....
00066 ***** 2020-11-30 Change W_CLEAR_SLOPE to 0.55, SLPD=[0.5] (impervious slope), and LGT up to 700m ***** .....
00067 ***** 2020-12-01 correct pond curve values ***** .....
00068 ***** 2020-12-01 change W_CLEAR_SLOPE to 0.55, SLPD=[0.5] (impervious slope), and LGT up to 700m ***** .....
00069 ***** 2021-02-19 Change the slope for ROUTE CHANNEL STATION 2462 (INVDout="R_NC") ,INVDin("SM_NC") from 0.03 K (as per st *****
00070 ***** 2021-02-19 Change the slope for ROUTE CHANNEL STATION 5002 (INVDout="R_NC") ,INVDin("SM_NC") from 0.01 K (as per st *****
00071 ***** ***** .....
00072 ***** ** END OF RUN : 1 ***** .....
00073 ***** .....
00074 ***** .....
00075 ***** .....
00076 ***** .....
00077 ***** .....
00078 ***** .....
00079 ***** .....
00080 ***** .....
00081 ***** R002:C0001 ***** .....
00082 ***** START ***** .....
00083 ***** [INTERD = 0 hrs on 0] ***** .....
00084 ***** [MFOU7 = 2 (1=imperial, 2=metric output)] ***** .....
00085 ***** [INTERR = 1] ***** .....
00086 ***** [NSUN = 0.02] ***** .....
00087 ***** ***** .....
00088 ***** SWHYMO Ver 5.02\Jan 0001 <BETA> - INPUT DATA FILE ***** .....
00089 ***** .....
00090 ***** Project Name: [Jock River] Project Number: [1474-16] ***** .....
00091 ***** Date [04-03-2021] ***** .....
00092 ***** Modeller [J.F.M.] ***** .....
00093 ***** Company [JFSaInc.] ***** .....
00094 ***** License # [2549237] ***** .....
00095 ***** ***** .....
00096 ***** CALIBRATION OF SUMMER MODEL PARAMETERS ***** .....
00097 ***** USING CONTINUOUS SIMULATIONS ***** .....
00098 ***** Rainfall data from JFSa raingage installed at site + other gauges by the City ***** .....
00099 ***** Use data collected from May 1st to July 14, 2003 ***** .....
00100 ***** 2020-11-30 Change W_CLEAR_SLOPE to 0.55, SLPD=[0.5] (impervious slope), and LGT up to 700m ***** .....
00101 ***** 2020-12-01 correct pond curve values ***** .....
00102 ***** 2020-12-01 change W_CLEAR_SLOPE to 0.55, SLPD=[0.5] (impervious slope), and LGT up to 700m ***** .....
00103 ***** 2021-02-19 Change the slope for ROUTE CHANNEL STATION 2462 (INVDout="R_NC") ,INVDin("SM_NC") from 0.03 K (as per st *****
00104 ***** 2021-02-19 Change the slope for ROUTE CHANNEL STATION 5002 (INVDout="R_NC") ,INVDin("SM_NC") from 0.01 K (as per st *****
00105 ***** ***** .....
00106 ***** R002:C0002 ***** .....
00107 ***** READ STORM ***** .....
00108 ***** Filename = storm.001 ***** .....
00109 ***** Comment = pluie dec de 34 hrs 112 ans pour Ottawa CDA ***** .....
00110 ***** [SD=10.00;SDUR= 24.00;P70= 45.51] ***** .....
00111 ***** R002:C0003 ***** .....
00112 ***** MODIFY STORM ***** .....
00113 ***** [RFACT = 1.00;TRHPT= 960.00 min] ***** .....
00114 ***** [SERFLO 00;SDUR= 47.00;P70= 45.51] ***** .....
00115 ***** R002:C0004 ***** .....
00116 ***** RESHAPE VALUES ***** .....
00117 ***** Filename = T:\PROJ\1474-16\Design\20210206-QuantityControlAnalysis\SWHYMO\SMH-Model\Updated\Citigate.DEP *****
00118 ***** ICRSDV = 1 (read and print data) ***** .....
00119 ***** File titles File comment: Based on various calibration exercises in Onta ***** .....
00120 ***** THE FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDARD COM ***** .....
00121 ***** Horton's infiltration equation parameter ***** .....
00122 ***** [Wp 76.20 mm/hr] [Cp=13.20 mm/h] [DCA= 4.14 ] [P = .00 mm] ***** .....
00123 ***** Parameters used in STANHYD ***** .....
00124 ***** [Iaper = 4.67 mm] [LWp=50.00 mm] [MHP= .250] ***** .....
00125 ***** Parameters used in HANHYD ***** .....
00126 ***** [Ia = 1.87 mm] [Cp= 0.33] ***** .....
00127 ***** Parameters used in HANHYD ***** .....
00128 ***** [Ia = 1.87 mm] [Cp= 0.33] ***** .....
00129 ***** Average monthly pan Evaporation data in (mm) ***** .....
00130 ***** JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC ***** .....
00131 ***** .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 ***** .....
00132 ***** Average monthly Potential Evapotranspiration in (mm) ***** .....
00133 ***** JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC ***** .....
00134 ***** .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 ***** .....
00135 ***** R002:C0005 ***** .....
00136 ***** COMPUTE API ***** .....
00137 ***** [API= 50.00; APIKdy = 8500; APIKdt= .988] ***** .....
00138 ***** [API= 50.12; APIKdy = 8574; APIKdt= 8.87] ***** .....
00139 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) ***** .....
00140 ***** of 1.32 ***** .....
00141 ***** R002:C0006 ***** .....
00142 ***** CONTINUOUS NASHVD 1.0 01:SR_NW 3680.00 6.204 No.Date 37:06 11:47 252 .000 *****
00143 ***** [Cm 64.01 N= 3.00; Tp = 1.13] ***** .....
00144 ***** [IaREC= 4.00; SMIN= 43.07; SMAX=380.32; SK= .010] ***** .....
00145 ***** [InterEventTime= 12.00] ***** .....
00146 ***** ***** .....
00147 ***** .....
00148 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) ***** .....
00149 ***** of 1.32 ***** .....
00150 ***** R002:C0007 ***** .....
00151 ***** CONTINUOUS NASHVD 1.0 01:SR_S3 971.00 2.187 No.Date 32:37 10:75 236 .000 *****
00152 ***** [Cm 61.01 N= 3.00; Tp = 1.71] ***** .....
00153 ***** [IaREC= 4.00; SMIN= 64.50; SMAX=430.01; SK= .010] ***** .....
00154 ***** [InterEventTime= 12.00] ***** .....
00155 ***** .....
00156 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) ***** .....
00157 ***** of 1.80 ***** .....
00158 ***** R002:C0008 ***** .....
00159 ***** CONTINUOUS NASHVD 1.0 01:SR_S1 374.00 3.218 No.Date 39:59 9:43 207 .000 *****
00160 ***** [Cm 55.01 N= 3.00; Tp = 1.33] ***** .....
00161 ***** [IaREC= 4.00; SMIN= 51.24; SMAX=554.96; SK= .010] ***** .....
00162 ***** [InterEventTime= 12.00] ***** .....
00163 ***** R002:C0009 ***** .....
00164 ***** CONTINUOUS NASHVD 1.0 01:SR_ASH 1781.00 5.504 No.Date 32:48 13:94 306 .000 *****
00165 ***** [Cm 72.01 N= 3.00; Tp = 1.91] ***** .....
00166 ***** [IaREC= 4.00; SMIN= 39.75; SMAX=264.99; SK= .010] ***** .....
00167 ***** [InterEventTime= 12.00] ***** .....
00168 ***** R002:C0010 ***** .....
00169 ***** CONTINUOUS NASHVD 1.0 01:SR_S1 1917.00 4.042 No.Date 34:34 11:98 263 .000 *****
00170 ***** [Cm 66.01 N= 3.00; Tp = 1.24] ***** .....
00171 ***** [IaREC= 4.00; SMIN= 52.62; SMAX=350.79; SK= .010] ***** .....
00172 ***** [InterEventTime= 12.00] ***** .....
00173 ***** .....
00174 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) ***** .....
00175 ***** of 1.80 ***** .....
00176 ***** R002:C0011 ***** .....
00177 ***** CONTINUOUS NASHVD 1.0 01:SR_CK 1917.00 4.042 No.Date 34:34 11:98 263 .000 *****
00178 ***** [Cm 66.01 N= 3.00; Tp = 1.24] ***** .....
00179 ***** [IaREC= 4.00; SMIN= 52.62; SMAX=350.79; SK= .010] ***** .....
00180 ***** [InterEventTime= 12.00] ***** .....
00181 ***** .....
00182 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) ***** .....
00183 ***** of 1.32 ***** .....
00184 ***** R002:C0012 ***** .....
00185 ***** CONTINUOUS NASHVD 1.0 01:SR_HD 5666.00 11:228 No.Date 38:07 13:94 306 .000 *****
00186 ***** [Cm 72.01 N= 3.00; Tp = 8.00] ***** .....
00187 ***** [IaREC= 4.00; SMIN= 39.75; SMAX=264.99; SK= .010] ***** .....

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00188 ***** [InterEventTime= 12.00] ***** .....
00189 ***** .....
00190 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) ***** .....
00191 ***** of 1.75 ***** .....
00192 ***** R002:C0013 ***** .....
00193 ***** CONTINUOUS NASHVD 1.0 01:SR_CK 8376.00 11:072 No.Date 39:59 11:98 263 .000 *****
00194 ***** [Cm 69.01 N= 3.00; Tp = 1.51] ***** .....
00195 ***** [IaREC= 4.00; SMIN= 52.62; SMAX=350.79; SK= .010] ***** .....
00196 ***** [InterEventTime= 12.00] ***** .....
00197 ***** .....
00198 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) ***** .....
00199 ***** of 1.68 ***** .....
00200 ***** R002:C0014 ***** .....
00201 ***** CONTINUOUS NASHVD 1.0 01:SR_S 1132.00 4.434 No.Date 30:58 13:98 293 .000 *****
00202 ***** [Cm 70.01 N= 3.00; Tp = 2.51] ***** .....
00203 ***** [IaREC= 4.00; SMIN= 43.07; SMAX=287.10; SK= .010] ***** .....
00204 ***** [InterEventTime= 12.00] ***** .....
00205 ***** .....
00206 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) ***** .....
00207 ***** of 1.82 ***** .....
00208 ***** R002:C0015 ***** .....
00209 ***** CONTINUOUS NASHVD 1.0 01:SR_CK 4664.00 5.504 No.Date 39:59 10:98 241 .000 *****
00210 ***** [Cm 62.01 N= 3.00; Tp = 1.21] ***** .....
00211 ***** [IaREC= 4.00; SMIN= 61.90; SMAX=412.66; SK= .010] ***** .....
00212 ***** [InterEventTime= 12.00] ***** .....
00213 ***** .....
00214 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) ***** .....
00215 ***** of 1.80 ***** .....
00216 ***** R002:C0016 ***** .....
00217 ***** CONTINUOUS NASHVD 1.0 01:SR_H 131.00 .805 No.Date 28:57 11:22 247 .000 *****
00218 ***** [Cm 63.01 N= 3.00; Tp = .93] ***** .....
00219 ***** [IaREC= 4.00; SMIN= 59.42; SMAX=396.11; SK= .010] ***** .....
00220 ***** [InterEventTime= 12.00] ***** .....
00221 ***** .....
00222 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) ***** .....
00223 ***** of 1.65 ***** .....
00224 ***** R002:C0017 ***** .....
00225 ***** CONTINUOUS NASHVD 1.0 01:SR_H 368.00 4.442 No.Date 38:46 11:98 263 .000 *****
00226 ***** [Cm 66.01 N= 3.00; Tp = 8.42] ***** .....
00227 ***** [IaREC= 4.00; SMIN= 51.24; SMAX=350.79; SK= .010] ***** .....
00228 ***** [InterEventTime= 12.00] ***** .....
00229 ***** .....
00230 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) ***** .....
00231 ***** of 1.82 ***** .....
00232 ***** R002:C0018 ***** .....
00233 ***** CONTINUOUS NASHVD 1.0 01:SR_W 1397.00 4.651 No.Date 36:31 9:85 217 .000 *****
00234 ***** [Cm 63.01 N= 3.00; Tp = .93] ***** .....
00235 ***** [IaREC= 4.00; SMIN= 76.32; SMAX=508.81; SK= .010] ***** .....
00236 ***** [InterEventTime= 12.00] ***** .....
00237 ***** .....
00238 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) ***** .....
00239 ***** of 1.75 ***** .....
00240 ***** R002:C0019 ***** .....
00241 ***** CONTINUOUS NASHVD 1.0 01:SR_B 165.00 .413 No.Date 33:07 12:24 269 .000 *****
00242 ***** [Cm 67.01 N= 3.00; Tp = 4.18] ***** .....
00243 ***** [IaREC= 4.00; SMIN= 60.55; SMAX=336.97; SK= .010] ***** .....
00244 ***** [InterEventTime= 12.00] ***** .....
00245 ***** .....
00246 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) ***** .....
00247 ***** of 1.67 ***** .....
00248 ***** R002:C0020 ***** .....
00249 ***** CONTINUOUS NASHVD 1.0 01:VDR 1332.00 3.148 No.Date 35:23 13:94 306 .000 *****
00250 ***** [Cm 72.01 N= 3.00; Tp = 5.93] ***** .....
00251 ***** [IaREC= 4.00; SMIN= 39.75; SMAX=264.99; SK= .010] ***** .....
00252 ***** [InterEventTime= 12.00] ***** .....
00253 ***** R002:C0021 ***** .....
00254 ***** CONTINUOUS NASHVD 1.0 01:SR_W 224.00 2.597 No.Date 28:45 15:91 350 .000 *****
00255 ***** [Cm 77.01 N= 3.00; Tp = .78] ***** .....
00256 ***** [IaREC= 4.00; SMIN= 31.31; SMAX=207.66; SK= .010] ***** .....
00257 ***** [InterEventTime= 12.00] ***** .....
00258 ***** .....
00259 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) ***** .....
00260 ***** of 1.23 ***** .....
00261 ***** R002:C0022 ***** .....
00262 ***** CONTINUOUS NASHVD 1.0 01:FL_CK 4945.00 14.839 No.Date 33:25 14:57 320 .000 *****
00263 ***** [Cm 74.01 N= 3.00; Tp = 4.63] ***** .....
00264 ***** [IaREC= 4.00; SMIN= 36.67; SMAX=244.49; SK= .010] ***** .....
00265 ***** [InterEventTime= 12.00] ***** .....
00266 ***** R002:C0023 ***** .....
00267 ***** CONTINUOUS NASHVD 1.0 01:SR_S2 20.00 .309 No.Date 28:36 17:79 391 .000 *****
00268 ***** [Cm 81.01 N= 3.00; Tp = 2.1] ***** .....
00269 ***** [IaREC= 4.00; SMIN= 25.21; SMAX=168.09; SK= .010] ***** .....
00270 ***** [InterEventTime= 12.00] ***** .....
00271 ***** .....
00272 ***** The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4) ***** .....
00273 ***** of 1.61 ***** .....
00274 ***** R002:C0024 ***** .....
00275 ***** CONTINUOUS NASHVD 1.0 01:SR_B 141.00 3.090 No.Date 30:04 15:22 334 .000 *****
00276 ***** [Cm 75.01 N= 3.00; Tp = 8.00] ***** .....
00277 ***** [IaREC= 4.00; SMIN= 13.81; SMAX=225.43; SK= .010] ***** .....
00278 ***** [InterEventTime= 12.00] ***** .....
00279 ***** R002:C0025 ***** .....
00280 ***** CONTINUOUS NASHVD 1.0 01:SR_H 585.00 4.325 No.Date 29:58 17:79 391 .000 *****
00281 ***** [Cm 81.01 N= 3.00; Tp = 1.75] ***** .....
00282 ***** [IaREC= 4.00; SMIN= 45.21; SMAX=168.09; SK= .010] ***** .....
00283 ***** [InterEventTime= 12.00] ***** .....
00284 ***** R002:C0026 ***** .....
00285 ***** CONTINUOUS NASHVD 1.0 01:LM_CK 1021.00 5.747 No.Date 30:50 17:39 382 .000 *****
00286 ***** [Cm 80.01 N= 3.00; Tp = .81] ***** .....
00287 ***** [IaREC= 4.00; SMIN= 39.75; SMAX=175.50; SK= .010] ***** .....
00288 ***** [InterEventTime= 12.00] ***** .....
00289 ***** R002:C0027 ***** .....
00290 ***** CONTINUOUS NASHVD 1.0 01:SR_W 177.00 2.052 No.Date 28:45 15:91 350 .000 *****
00291 ***** [Cm 77.01 N= 3.00; Tp = .78] ***** .....
00292 ***** [IaREC= 4.00; SMIN= 31.31; SMAX=207.66; SK= .010] ***** .....
00293 ***** [InterEventTime= 12.00] ***** .....
00294 ***** R002:C0028 ***** .....
00295 ***** CONTINUOUS NASHVD 1.0 01:SR_H 1122.00 5.337 No.Date 31:50 17:79 391 .000 *****
00296 ***** [Cm 81.01 N= 3.00; Tp = 2.83] ***** .....
00297 ***** [IaREC= 4.00; SMIN= 25.21; SMAX=168.09; SK= .010] ***** .....
00298 ***** [InterEventTime= 12.00] ***** .....
00299 ***** R002:C0029 ***** .....
00300 ***** CONTINUOUS NASHVD 1.0 01:SR_W 2737.00 11.528 No.Date 31:35 15:56 342 .000 *****
00301 ***** [Cm 76.01 N= 3.00; Tp = 1.21] ***** .....
00302 ***** [IaREC= 4.00; SMIN= 32.46; SMAX=216.39; SK= .010] ***** .....
00303 ***** [InterEventTime= 12.00] ***** .....
00304 ***** .....
00305 ***** Routing hydrographs ***** .....
00306 ***** .....
00307 ***** Starting with the addition of Jock River Headwater and Subwatershed 13 ***** .....
00308 ***** .....
00309 ***** R002:C0030 ***** .....
00310 ***** ADD HYD ***** .....
00311 ***** [IaREC= 1.02;SR_W 971.00 2.187 No.Date 32:37 10:75 n/a .000 *****
00312 ***** [IaREC= 1.01;SR_H 4651.00 7.871 No.Date 39:37 11:32 n/a .000 *****
00313 ***** [IaREC= 1.01;SR_S 1397.00 4.651 No.Date 36:31 9:85 n/a .000 *****
00314 ***** Sum of hydrographs from Node 13 routed to Node 13A ***** .....
00315 ***** [Approximated cross-section - see cross-section 258] ***** .....
00316 ***** Use n=0.04 for summer conditions and n=0.025 for spring conditions ***** .....
00317 ***** .....
00318 ***** R002:C0031 ***** .....
00319 ***** ROUTE CHANNEL -> 1.0 02:SR_S3 4651.00 7.871 No.Date 39:37 11:32 n/a .000 *****
00320 ***** [IaREC= 1.00] [IaREC= 1.0] [IaREC= 1.0] ***** .....
00321 ***** [IaREC= 1.00] [IaREC= 1.00] [IaREC= 1.00] ***** .....
00322 ***** [IaREC= 1.00] [IaREC= 1.00] [IaREC= 1.00] ***** .....
00323 ***** [IaREC= 1.00] [IaREC= 1.00] [IaREC= 1.00] ***** .....
00324 ***** Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A ***** .....
00325 ***** .....
00326 ***** R002:C0032 ***** .....
00327 ***** ADD HYD ***** .....
00328 ***** [IaREC= 1.02;SR_W 1074.00 3.218 No.Date 39:59 9:43 n/a .000 *****
00329 ***** [IaREC= 1.01;SR_H 7725.00 9.475 No.Date 39:59 10:57 n/a .000 *****
00330 ***** [IaREC= 1.01;SR_S 1397.00 4.651 No.Date 36:31 9:85 n/a .000 *****
00331 ***** Insertion of a reservoir to simulate the effects of the Goodwood Marsh ***** .....
00332 ***** .....
00333 ***** R002:C0033 ***** .....
00334 ***** ROUTE CHANNEL -> 1.0 02:SR_S3A 7725.00 9.475 No.Date 39:59 10:57 n/a .000 *****
00335 ***** [IaREC= 1.00] [IaREC= 1.00] [IaREC= 1.00] ***** .....
00336 ***** [IaREC= 1.00] [IaREC= 1.00] [IaREC= 1.00] ***** .....
00337 ***** [IaREC= 1.00] [IaREC= 1.00] [IaREC= 1.00] ***** .....
00338 ***** R002:C0034 ***** .....
00339 ***** ADD HYD ***** .....
00340 ***** [IaREC= 1.01;SR_H 7725.00 9.475 No.Date 39:59 10:57 n/a .000 *****
00341 ***** [IaREC= 1.01;SR_S 1397.00 4.651 No.Date 36:31 9:85 n/a .000 *****
00342 ***** Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12 ***** .....
00343 ***** [Approximated cross-section - see cross-section 258] ***** .....
00344 ***** Use n=0.04 for summer conditions and n=0.025 for spring conditions ***** .....
00345 ***** R002:C0035 ***** .....
00346 ***** ROUTE CHANNEL -> 1.0 02:SR_W 7725.00 9.475 No.Date 39:59 10:57 n/a .000 *****
00347 ***** [IaREC= 1.00] [IaREC= 1.00] [IaREC= 1.00] ***** .....
00348 ***** [IaREC= 1.00] [IaREC= 1.00] [IaREC= 1.00] ***** .....
00349 ***** [IaREC= 1.00] [IaREC= 1.00] [IaREC= 1.00] ***** .....
00350 ***** .....
00351 ***** Addition of Subwatershed Jock River at Ashton to Node 12 ***** .....
00352 ***** .....
00353 ***** R002:C0036 ***** .....
00354 ***** ADD HYD ***** .....
00355 ***** [IaREC= 1.02;SR_H 7725.00 9.475 No.Date 39:59 10:57 n/a .000 *****
00356 ***** [IaREC= 1.01;SR_W 7725.00 9.475 No.Date 39:59 10:57 n/a .000 *****
00357 ***** [IaREC= 1.01;SR_S 1397.00 4.651 No.Date 36:31 9:85 n/a .000 *****
00358 ***** R002:C0037 ***** .....
00359 ***** ADD HYD ***** .....
00360 ***** [IaREC= 1.01;SR_H 7725.00 9.475 No.Date 39:59 10:57 n/a .000 *****
00361 ***** [IaREC= 1.01;SR_W 7725.00 9.475 No.Date 39:59 10:57 n/a .000 *****
00362 ***** [IaREC= 1.01;SR_S 1397.00 4.651 No.Date 36:31 9:85 n/a .000 *****
00363 ***** [IaREC= 1.01;SR_H 7725.00 9.475 No.Date 39:59 10:57 n/a .000 *****
00364 ***** Use n=0.04 for summer conditions and n=0.025 for spring conditions ***** .....
00365 ***** .....
00366 ***** Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248 ***** .....
00367 ***** .....
00368 ***** R002:C0038 ***** .....
00369 ***** ROUTE CHANNEL -> 1.0 02:SR_H 9506.00 7.458 No.Date 32:50 11:20 n/a .000 *****
00370 ***** [IaREC= 1.00] [IaREC= 1.00] [IaREC= 1.00] ***** .....
00371 ***** [IaREC= 1.00] [IaREC= 1.00] [IaREC= 1.00] ***** .....
00372 ***** [IaREC= 1.00] [IaREC= 1.00] [IaREC= 1.00] ***** .....
00373 ***** [IaREC= 1.00] [IaREC= 1.00] [IaREC= 1.00] ***** .....
00374 ***** Addition of Subwatershed 11 and No Name Creek to Node 11 ***** .....

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00375# #
00376# R002/C00039-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00377# ADD HYD + 1.0 02:01M1 9506.00 7.379_MDate 33:12 11.20 n/a .000
00378# ROUTE CHANNEL -> 1.0 02:01M1 500.00 2.720_MDate 29:22 11.98 n/a .000
00379# + 1.0 02:01M2 1917.00 4.042_MDate 34:34 11.98 n/a .000
00380# SUM= 1.0 01:01M1 11923.00 12.077_MDate 33:14 11.36 n/a .000
00381#
00382# Sum of hydrographs from Node 11 routed to Node 10
00383# Section 1
00384#
00385# R002/C00040-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00386# ROUTE CHANNEL -> 1.0 02:01M1 11923.00 12.077_MDate 33:14 11.36 n/a .000
00387# [RPT= 1.00] out<- 1.0 01:01M0 11923.00 8.276_MDate 39:46 11.36 n/a .000
00388# [L/S/N= 392.9 / .057/.040]
00389# [Vmax=.462;Dmax=.886]
00390#
00391# Addition of Subwatershed 10 to Node 10
00392#
00393# R002/C00041-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00394# ADD HYD + 1.0 02:01M0 17859.00 19.451_MDate 38:31 12.19 n/a .000
00395# + 1.0 02:01M10 5646.00 11.228_MDate 38:07 13.94 n/a .000
00396# SUM= 1.0 01:01M0 17859.00 19.451_MDate 38:31 12.19 n/a .000
00397# R002/C00042-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00398# SAVE HYD + 1.0 01:01M0 17859.00 19.451_MDate 38:31 12.19 n/a .000
00399# fname :H_SMI0
00400# remark:flow at N10: M10 + SK_10
00401# Addition of Kings Creek to S_M10
00402#
00403# R002/C00043-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00404# ADD HYD + 1.0 02:01M0 17859.00 19.451_MDate 38:31 12.19 n/a .000
00405# + 1.0 02:01M2 8376.00 11.072_MDate 39:59 11.98 n/a .000
00406# SUM= 1.0 01:01M0A 25965.00 30.328_MDate 39:58 12.12 n/a .000
00407#
00408# Sum of hydrographs from Node 10 routed to Node 9
00409# Section 2
00410#
00411# R002/C00044-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00412# ROUTE CHANNEL -> 1.0 02:01M0A 25965.00 29.579_MDate 39:59 12.12 n/a .000
00413# [RPT= 1.00] out<- 1.0 01:01M 25965.00 29.579_MDate 39:59 12.12 n/a .000
00414# [L/S/N= 392.9 / .075/.040]
00415# [Vmax=.595;Dmax=1.208]
00416#
00417# Addition of Subwatershed 9 and Nichols Creek to Node 9
00418#
00419# R002/C00045-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00420# ADD HYD + 1.0 02:01M 25965.00 29.579_MDate 39:59 12.12 n/a .000
00421# + 1.0 02:01M2 4484.00 4.484_MDate 39:59 12.12 n/a .000
00422# + 1.0 02:01M2C 4464.00 5.504_MDate 39:59 10.98 n/a .000
00423# SUM= 1.0 01:01M 31561.00 36.313_MDate 39:59 12.00 n/a .000
00424#
00425# Sum of hydrographs from Node 9 routed to Node 8
00426# Section 3
00427#
00428# R002/C00046-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00429# ROUTE CHANNEL -> 1.0 02:01M 31561.00 36.313_MDate 39:59 12.00 n/a .000
00430# [RPT= 1.00] out<- 1.0 01:01M 31561.00 34.173_MDate 39:59 12.00 n/a .000
00431# [L/S/N= 392.9 / .087/.040]
00432# [Vmax=.418;Dmax=1.281]
00433#
00434# Addition of Subwatershed 8 and Bobb's Drain to Node 8
00435#
00436# R002/C00047-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00437# ADD HYD + 1.0 02:01M 31561.00 34.173_MDate 39:59 12.00 n/a .000
00438# + 1.0 02:01M2 405.00 4.050_MDate 39:59 11.22 n/a .000
00439# + 1.0 02:01M2C 3854.00 6.242_MDate 38:46 11.98 n/a .000
00440# SUM= 1.0 01:01M 35460.00 40.474_MDate 39:59 12.00 n/a .000
00441#
00442# Sum of hydrographs from Node 8 routed to Node 7
00443# Section 4
00444#
00445# R002/C00048-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00446# ROUTE CHANNEL -> 1.0 02:01M 35460.00 40.474_MDate 39:59 12.00 n/a .000
00447# [RPT= 1.00] out<- 1.0 01:01M 35460.00 32.892_MDate 44:30 12.00 n/a .000
00448# [L/S/N= 375.0 / .053/.070]
00449# [Vmax=.208;Dmax=1.651]
00450#
00451# Addition of Subwatershed 7 to Node 7
00452#
00453# R002/C00049-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00454# ADD HYD + 1.0 02:01M 35460.00 32.892_MDate 44:30 12.00 n/a .000
00455# + 1.0 02:01M2 3197.00 3.197_MDate 46:31 9.45 n/a .000
00456# SUM= 1.0 01:01M 37343.00 35.071_MDate 43:33 11.82 n/a .000
00457# R002/C00050-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00458# SAVE HYD + 1.0 01:01M 37343.00 35.071_MDate 43:33 11.82 n/a .000
00459# fname :H_SHT
00460# remark:flow at R_N7: M7 + SK_7
00461# Insertion of a Reservoir to simulate the effects of the Richmond Fen.
00462# Storage area and volumes were estimated from available topo maps.
00463# Release rate from Fen was assumed to be controlled by the downstream
00464# river cross-section for subwatershed. It is assumed that for up to
00465# 0.75 m of water, the main channel of the river provided the storage. Above
00466# this depth, the wetland starts to significantly store water.
00467#
00468# R002/C00051-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00469# ROUTE CHANNEL -> 1.0 02:01M 37343.00 35.071_MDate 43:33 11.82 n/a .000
00470# out<- 1.0 01:RES_RF 37343.00 23.265_MDate 55:09 11.82 n/a .000
00471# [Med:0.000;T:0.000]
00472# R002/C00052-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00473# SAVE HYD + 1.0 01:RES_RF 37343.00 23.265_MDate 55:09 11.82 n/a .000
00474# fname :H_RESRF
00475# remark:outflow of Richmond Fen
00476#
00477# Sum of hydrographs from Node 7 routed to Node 6
00478# Section 5
00479#
00480# R002/C00053-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00481# ROUTE CHANNEL -> 1.0 02:01M 37343.00 23.265_MDate 55:09 11.82 n/a .000
00482# [RPT= 1.00] out<- 1.0 01:01M 37343.00 23.228_MDate 56:38 11.82 n/a .000
00483# [L/S/N= 306.6 / .083/.040]
00484# [Vmax=.432;Dmax=.808]
00485#
00486# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
00487#
00488# R002/C00054-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00489# ADD HYD + 1.0 02:01M 37343.00 23.228_MDate 56:38 11.82 n/a .000
00490# + 1.0 02:01M2 1455.00 1.455_MDate 28:36 12.24 n/a .000
00491# + 1.0 02:01M2C 1332.00 3.148_MDate 35:23 13.94 n/a .000
00492# SUM= 1.0 01:01M 40240.00 23.318_MDate 39:59 11.89 n/a .000
00493#
00494# Sum of hydrographs from Node 6 routed to Node 5
00495# Section 6
00496#
00497# R002/C00055-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00498# ROUTE CHANNEL -> 1.0 02:01M 40240.00 23.318_MDate 39:59 11.89 n/a .000
00499# [RPT= 1.00] out<- 1.0 01:01M 40240.00 23.288_MDate 56:09 11.89 n/a .000
00500# [L/S/N= 306.6 / .050/.040]
00501# [Vmax=.378;Dmax=.917]
00502#
00503# Addition of Subwatershed 5 and Flowing Creek to Node 5
00504#
00505# R002/C00056-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00506# ADD HYD + 1.0 02:01M 40240.00 23.288_MDate 56:09 11.89 n/a .000
00507# + 1.0 02:01M2 224.94 2.249_MDate 28:36 12.24 n/a .000
00508# + 1.0 02:01M2C 4945.00 14.839_MDate 33:25 14.57 n/a .000
00509# SUM= 1.0 01:01M 45409.00 31.366_MDate 37:08 12.20 n/a .000
00510#
00511# Sum of hydrographs from Node 5 routed to Node 5A
00512# Section 7
00513#
00514# R002/C00057-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00515# ROUTE CHANNEL -> 1.0 02:01M 45409.00 31.366_MDate 37:08 12.20 n/a .000
00516# [RPT= 1.00] out<- 1.0 01:01M 45409.00 33.135_MDate 37:20 12.20 n/a .000
00517# [L/S/N= 556.7 / .090/.040]
00518# [Vmax=.443;Dmax=.937]
00519#
00520# Addition of Subwatershed 5A and Subwatershed 5A2 to Node 5A
00521#
00522# R002/C00058-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00523# ADD HYD + 1.0 02:01M 45409.00 31.366_MDate 37:20 12.20 n/a .000
00524# + 1.0 02:01M2 45409.00 31.315_MDate 37:33 12.24 n/a .000
00525# + 1.0 02:01M2C 1622.00 3.090_MDate 38:04 15.22 n/a .000
00526# SUM= 1.0 01:01M 90818.00 36.288_MDate 37:28 12.30 n/a .000
00527#
00528# Sum of hydrographs from Node 5A routed to Node 4
00529# Section 8
00530#
00531# R002/C00059-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00532# ROUTE CHANNEL -> 1.0 02:01M 90818.00 36.288_MDate 37:28 12.30 n/a .000
00533# [RPT= 1.00] out<- 1.0 01:01M 90818.00 35.288_MDate 39:22 12.30 n/a .000
00534# [L/S/N= 463.0 / .041/.035]
00535# [Vmax=.695;Dmax=2.444]
00536#
00537# Addition of Subwatershed 4 and Leamy Creek to Node 4
00538#
00539# R002/C00060-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00540# ADD HYD + 1.0 02:01M 90818.00 35.288_MDate 39:22 12.30 n/a .000
00541# + 1.0 02:01M2 585.00 4.325_MDate 29:58 17.79 n/a .000
00542# + 1.0 02:01M2C 1022.00 5.747_MDate 30:50 17.39 n/a .000
00543# SUM= 1.0 01:01M 96643.00 37.581_MDate 38:13 12.47 n/a .000
00544# R002/C00061-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00545# SAVE HYD + 1.0 01:01M 96643.00 37.581_MDate 38:13 12.47 n/a .000
00546# fname :H_4M.0002
00547# remark:flow at R_N4
00548#
00549# Sum of hydrographs from Node 4 routed to Node 2
00550# Section 9
00551#
00552# R002/C00062-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00553# ROUTE CHANNEL -> 1.0 02:01M 96643.00 37.581_MDate 38:13 12.47 n/a .000
00554# [RPT= 1.00] out<- 1.0 01:01M 96643.00 37.455_MDate 38:19 12.47 n/a .000
00555# [L/S/N= 1467.7 / .060/.040]
00556# [Vmax=.715;Dmax=2.485]
00557#
00558# Addition of Subwatershed 2 with Monahan Drain and Smith Drain to Node 2
00559#
00560# R002/C00063-----DtnIn-ID:HYD-----AREHA-QPEARcm-TPeakDate,hh:mm-----RvM-R,C-----DWPFms
00561# ADD HYD + 1.0 02:01M 96643.00 37.455_MDate 38:19 12.47 n/a .000

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014977 overflow <= 1.0 03:22-WVF 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
014978 [M$SysSto=0.000E+00, TotVolVol=0.000E+00, N=0, V=0, TotDurVof= 0 hrs]
014979 *****
015000 R0002-C00211-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015001 ADD HYD 1.0 02:18-CE 54118.36 49.269 26.04 34.41 12.96 n/a 0.00
015002 + 1.0 02:18-D4R 3.28 0.019 0.042 29.16 32.20 n/a 0.00
015003 + 1.0 02:18-D4Rovf 12.84 0.076 0.040 29.23 32.20 n/a 0.00
015004 + 1.0 02:18-D4Rovf 0.00 0.000 0.000 0.00 0.00 n/a 0.00
015005 + 1.0 02:18-D4Rovf 0.00 0.000 0.000 0.00 0.00 n/a 0.00
015006 + 1.0 02:18-D2 139.40 48.616 26.04 29.25 31.34 n/a 0.00
015007 + 1.0 02:18-D2 0.00 0.000 0.000 0.00 0.00 n/a 0.00
015008 + 1.0 02:18-D2 54253.88 49.833 26.04 34.41 13.00 n/a 0.00
015009 R0002-C00211-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015010 SAVE HYD 1.0 02:18-CE 54253.88 49.833 26.04 34.41 13.00 n/a 0.00
015011 *****
015012 # frame 1502.0002
015013 # remark:Total Flow before Station 5737 on Jack River
015014 # Channel X-Section obtained from RWCA Hydraulic Model - Station 5737
015015 # 2021-02-25 add station 5737 before station 5002. Station 5737 was extracted from the HEC-RAS model 7 (V9M1)474-16/6es
015016 # FFS# 2021-02-19 Change the slope at 5737 to 0.1218 instead of 0.2524 to stabilize the model
015017 # FFS# 2021-02-19 Change the slope at 5737 to 0.1 (as per Station Report 2007)
015018 # FFS# 2021-02-19 Change the length of ROUTE CHANNEL from 825 m to 786 m. That is because of adding station 5737 be
015019 # FFS# 2021-02-19 Change the length of ROUTE CHANNEL with length 275 m each instead of one with 825 m length so the model wi
015020 # FFS# 2021-02-26 Change the length of ROUTE CHANNEL from 825 m to 786 m. That is because of adding station 5737 be
015021 ROUTE CHANNEL -> 1.0 02:00-WC 54279.33 48.426 26.04 37.44 13.01 n/a 0.00
015022 [L/S= 275 / 0.07 / 0.05]
015023 # Vmax= 611.0max= 3.459]
015024 R0002-C00224-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015025 ADD HYD 1.0 02:18-D1R 21.67 0.126 0.042 29.27 32.20 n/a 0.00
015026 + 1.0 02:18-D1R 1.75 0.010 0.042 29.24 32.20 n/a 0.00
015027 + 1.0 02:18-D1R 2.03 0.012 0.042 29.15 32.20 n/a 0.00
015028 + 1.0 02:18-D1Rovf 0.00 0.000 0.000 0.00 0.00 n/a 0.00
015029 [R02= 1.00] out<= 1.0 02:18-D1Rovf 0.00 0.000 0.000 0.00 0.00 n/a 0.00
015030 R0002-C00224-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015031 # frame 1502.0002
015032 # remark:Total Flow before Station 5002 on Jack River
015033 # Hydrograph from Node output to Node at West Clarke Drain
015034 # Channel X-Section obtained from RWCA Hydraulic Model - Station 5002
015035 # FFS# 2021-02-19 Change the slope at 5002 to 0.1218 instead of 0.2524 to stabilize the model
015036 # FFS# 2021-02-19 Change the length of ROUTE CHANNEL from 825 m to 786 m. That is because of adding station 5737 be
015037 # FFS# 2021-02-19 Change the length of ROUTE CHANNEL with length 275 m each instead of one with 825 m length so the model wi
015038 ROUTE CHANNEL -> 1.0 02:00-WC 54279.33 48.426 26.04 37.44 13.01 n/a 0.00
015039 [L/S= 275 / 0.07 / 0.05]
015040 # Vmax= 611.0max= 3.459]
015041 R0002-C00223-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015042 ADD HYD 1.0 02:18-WCA 54279.33 48.484 26.04 37.20 13.01 n/a 0.00
015043 [L/S= 245 / 0.09 / 0.05]
015044 # Vmax= 961.0max= 3.103]
015045 R0002-C00223-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015046 ROUTE CHANNEL -> 1.0 02:18-WCA 54279.33 48.484 26.04 37.20 13.01 n/a 0.00
015047 [L/S= 245 / 0.09 / 0.05]
015048 # Vmax= 961.0max= 3.103]
015049 R0002-C00224-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015050 ROUTE CHANNEL -> 1.0 02:18-WCA 54279.33 48.484 26.04 37.20 13.01 n/a 0.00
015051 [L/S= 245 / 0.09 / 0.05]
015052 # Vmax= 961.0max= 3.103]
015053 # Hydrograph from Node output to Node at West Clarke Drain
015054 # Channel X-Section obtained from RWCA Hydraulic Model - Station 4534
015055 # FFS# 2021-02-19 Change the slope at 4534 to 0.1218 instead of 0.2524 to stabilize the model
015056 # FFS# 2021-02-19 Change the length of ROUTE CHANNEL from 825 m to 786 m. That is because of adding station 5737 be
015057 # FFS# 2021-02-19 Change the length of ROUTE CHANNEL with length 275 m each instead of one with 825 m length so the model wi
015058 ROUTE CHANNEL -> 1.0 02:18-WC 54279.33 48.460 26.04 36.26 13.01 n/a 0.00
015059 [L/S= 1020 / 0.05 / 0.05]
015060 # Vmax= 1020.0max= 3.103]
015061 # Vmax= 1020.0max= 3.103]
015062 # Vmax= 1020.0max= 3.103]
015063 *****
015064 # Catchment HEC-HMS
015065 # To Kennedy-Burnett SSM Facility
015066 # - Outlet to Fraser-Clarke drain (north of the dock)
015067 # Manning's roughness coefficient = 0.148
015068 *****
015069 # Existing Kennedy-Burnett SSM Facility
015070 # Existing Kennedy-Burnett SSM Facility
015071 # Rating curve obtained from DTRSP
015072 # Tributary drainage area = 160 ha
015073 *****
015074 R0002-C00228-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015075 CONTINUOUS STANDBY 1.0 01:18-D1A 40.82 1.627 0.042 28.18 14.35 315 0.00
015076 [XIMP= 10-TIMP= 84]
015077 [Horton parameters: Pow= 76.20Fpc= 13.20DCAV= 4.14 F= 0.0]
015078 [Previous area: IArea= 4.67SLP= 2.00LSD= 40.0MP= 250ISCP= 0]
015079 [Impervious area: IArea= 79.5SLP= 4.00LSD= 180.0MI= 013ISCI= 0]
015080 [IAreaScp= 4.00 IAreaCp= 4.00]
015081 R0002-C00228-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015082 COMPUTE DUALYD 1.0 01:18-D1A 40.82 1.627 0.042 28.18 14.35 n/a 0.00
015083 Major System / 1.0 02:18-D1A-MJ 0.00 0.000 0.000 0.00 0.00 n/a 0.00
015084 Minor System / 1.0 02:18-D1A-MN 40.77 1.627 0.042 28.18 14.35 n/a 0.00
015085 [M$SysSto=0.000E+00, TotVolVol=0.000E+00, N=0, V=0, TotDurVof= 0 hrs]
015086 R0002-C00228-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015087 ADD HYD 1.0 02:18-D1A-MJ 0.00 0.000 0.000 0.00 0.00 n/a 0.00
015088 + 1.0 02:18-D1A-MN 40.77 1.627 0.042 28.18 14.35 n/a 0.00
015089 + 1.0 02:18-D1A-MN 40.82 1.627 0.042 28.18 14.35 n/a 0.00
015090 R0002-C00229-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015091 CONTINUOUS STANDBY 1.0 01:18-D1B 40.82 1.627 0.042 28.08 16.28 388 0.00
015092 [XIMP= 19-TIMP= 38]
015093 [Horton parameters: Pow= 76.20Fpc= 13.20DCAV= 4.14 F= 0.0]
015094 [Previous area: IArea= 4.67SLP= 4.21LSD= 455.0MI= 013ISCI= 0]
015095 [Impervious area: IArea= 79.5SLP= 4.00LSD= 180.0MI= 013ISCI= 0]
015096 [IAreaScp= 4.00 IAreaCp= 4.00]
015097 R0002-C00230-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015098 COMPUTE DUALYD 1.0 01:18-D1B 40.82 1.627 0.042 28.08 16.28 n/a 0.00
015099 Major System / 1.0 02:18-D1B-MJ 0.00 0.000 0.000 0.00 0.00 n/a 0.00
015100 Minor System / 1.0 02:18-D1B-MN 40.77 1.627 0.042 28.08 16.28 n/a 0.00
015101 [M$SysSto=0.000E+00, TotVolVol=0.000E+00, N=0, V=0, TotDurVof= 0 hrs]
015102 R0002-C00231-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015103 ADD HYD 1.0 02:18-D1B-MJ 31.10 1.062 0.042 28.08 16.28 n/a 0.00
015104 + 1.0 02:18-D1B-MN 31.10 1.062 0.042 28.08 16.28 n/a 0.00
015105 R0002-C00232-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015106 CONTINUOUS STANDBY 1.0 01:18-D1C 13.78 0.776 0.042 28.06 17.09 375 0.00
015107 [XIMP= 20-TIMP= 41]
015108 [Horton parameters: Pow= 76.20Fpc= 13.20DCAV= 4.14 F= 0.0]
015109 [Previous area: IArea= 4.67SLP= 2.00LSD= 40.0MP= 250ISCP= 0]
015110 [Impervious area: IArea= 79.5SLP= 4.00LSD= 180.0MI= 013ISCI= 0]
015111 [IAreaScp= 4.00 IAreaCp= 4.00]
015112 R0002-C00233-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015113 COMPUTE DUALYD 1.0 01:18-D1C 13.78 0.776 0.042 28.06 17.09 n/a 0.00
015114 Major System / 1.0 02:18-D1C-MJ 0.00 0.000 0.000 0.00 0.00 n/a 0.00
015115 Minor System / 1.0 02:18-D1C-MN 13.78 0.776 0.042 28.06 17.09 n/a 0.00
015116 [M$SysSto=0.000E+00, TotVolVol=0.000E+00, N=0, V=0, TotDurVof= 0 hrs]
015117 R0002-C00234-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015118 ADD HYD 1.0 02:18-D1C-MJ 13.78 0.776 0.042 28.06 17.09 n/a 0.00
015119 + 1.0 02:18-D1C-MN 13.78 0.776 0.042 28.06 17.09 n/a 0.00
015120 R0002-C00235-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015121 CONTINUOUS STANDBY 1.0 01:18-D1D 84.78 3.788 0.042 28.12 16.73 368 0.00
015122 [XIMP= 19-TIMP= 39]
015123 [Horton parameters: Pow= 76.20Fpc= 13.20DCAV= 4.14 F= 0.0]
015124 [Previous area: IArea= 4.67SLP= 2.00LSD= 40.0MP= 250ISCP= 0]
015125 [Impervious area: IArea= 79.5SLP= 4.00LSD= 180.0MI= 013ISCI= 0]
015126 [IAreaScp= 4.00 IAreaCp= 4.00]
015127 R0002-C00235-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015128 COMPUTE DUALYD 1.0 01:18-D1D 84.78 3.788 0.042 28.12 16.73 n/a 0.00
015129 Major System / 1.0 02:18-D1D-MJ 84.78 3.788 0.042 28.12 16.73 n/a 0.00
015130 Minor System / 1.0 02:18-D1D-MN 84.78 3.788 0.042 28.12 16.73 n/a 0.00
015131 [M$SysSto=0.000E+00, TotVolVol=0.000E+00, N=0, V=0, TotDurVof= 0 hrs]
015132 R0002-C00237-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015133 ADD HYD 1.0 02:18-D1D-MJ 84.78 3.788 0.042 28.12 16.73 n/a 0.00
015134 + 1.0 02:18-D1D-MN 84.78 3.788 0.042 28.12 16.73 n/a 0.00
015135 R0002-C00238-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015136 CONTINUOUS STANDBY 1.0 01:18-D1E 6.95 0.92 0.042 28.01 38.80 853 0.00
015137 [XIMP= 85-TIMP= 85]
015138 [Horton parameters: Pow= 76.20Fpc= 13.20DCAV= 4.14 F= 0.0]
015139 [Previous area: IArea= 4.67SLP= 2.00LSD= 40.0MP= 250ISCP= 0]
015140 [Impervious area: IArea= 79.5SLP= 4.00LSD= 180.0MI= 013ISCI= 0]
015141 [IAreaScp= 4.00 IAreaCp= 4.00]
015142 R0002-C00239-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015143 COMPUTE DUALYD 1.0 01:18-D1E 6.95 0.92 0.042 28.01 38.80 n/a 0.00
015144 Major System / 1.0 02:18-D1E-MJ 0.00 0.000 0.000 0.00 0.00 n/a 0.00
015145 Minor System / 1.0 02:18-D1E-MN 6.95 0.92 0.042 28.01 38.80 n/a 0.00
015146 [M$SysSto=1.641E+03, TotVolVol=0.000E+00, N=0, V=0, TotDurVof= 0 hrs]
015147 R0002-C00240-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015148 ADD HYD 1.0 02:18-D1E-MJ 6.95 0.92 0.042 28.01 38.80 n/a 0.00
015149 + 1.0 02:18-D1E-MN 6.95 0.92 0.042 28.01 38.80 n/a 0.00
015150 R0002-C00241-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015151 CONTINUOUS STANDBY 1.0 01:18-D1F 6.95 0.92 0.042 28.01 38.80 n/a 0.00
015152 [XIMP= 93-TIMP= 93]
015153 [Horton parameters: Pow= 76.20Fpc= 13.20DCAV= 4.14 F= 0.0]
015154 [Previous area: IArea= 4.67SLP= 2.00LSD= 40.0MP= 250ISCP= 0]
015155 [Impervious area: IArea= 79.5SLP= 4.00LSD= 180.0MI= 013ISCI= 0]
015156 [IAreaScp= 4.00 IAreaCp= 4.00]
015157 R0002-C00242-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015158 COMPUTE DUALYD 1.0 01:18-D1F 12.93 1.683 0.042 28.00 39.68 n/a 0.00
015159 Major System / 1.0 02:18-D1F-MJ 12.93 1.683 0.042 28.00 39.68 n/a 0.00
015160 Minor System / 1.0 02:18-D1F-MN 12.93 1.683 0.042 28.00 39.68 n/a 0.00
015161 [M$SysSto=0.000E+00, TotVolVol=0.000E+00, N=0, V=0, TotDurVof= 0 hrs]
015162 R0002-C00244-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015163 ADD HYD 1.0 02:18-D1F-MJ 12.93 1.683 0.042 28.00 39.68 n/a 0.00
015164 + 1.0 02:18-D1F-MN 12.93 1.683 0.042 28.00 39.68 n/a 0.00
015165 R0002-C00245-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015166 CONTINUOUS STANDBY 1.0 01:18-D1G 4.03 0.425 0.042 28.00 32.17 707 0.00
015167 [XIMP= 70-TIMP= 48]
015168 [Horton parameters: Pow= 76.20Fpc= 13.20DCAV= 4.14 F= 0.0]
015169 [Previous area: IArea= 4.67SLP= 2.00LSD= 40.0MP= 250ISCP= 0]
015170 [Impervious area: IArea= 79.5SLP= 4.00LSD= 180.0MI= 013ISCI= 0]
015171 [IAreaScp= 4.00 IAreaCp= 4.00]
015172 R0002-C00244-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015173 ADD HYD 1.0 02:18-D1G-MJ 12.93 1.683 0.042 28.00 39.68 n/a 0.00
015174 + 1.0 02:18-D1G-MN 12.93 1.683 0.042 28.00 39.68 n/a 0.00
015175 R0002-C00245-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015176 CONTINUOUS STANDBY 1.0 01:18-D1H 4.03 0.425 0.042 28.00 32.17 707 0.00
015177 [XIMP= 70-TIMP= 48]
015178 [Horton parameters: Pow= 76.20Fpc= 13.20DCAV= 4.14 F= 0.0]
015179 [Previous area: IArea= 4.67SLP= 2.00LSD= 40.0MP= 250ISCP= 0]
015180 [Impervious area: IArea= 79.5SLP= 4.00LSD= 180.0MI= 013ISCI= 0]
015181 [IAreaScp= 4.00 IAreaCp= 4.00]
015182 R0002-C00245-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015183 ADD HYD 1.0 02:18-D1H-MJ 4.03 0.425 0.042 28.00 32.17 707 0.00
015184 + 1.0 02:18-D1H-MN 4.03 0.425 0.042 28.00 32.17 707 0.00
015185 R0002-C00246-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015186 CONTINUOUS STANDBY 1.0 01:18-D1I 2.15 0.241 0.042 28.00 37.11 815 0.00
015187 [XIMP= 78-TIMP= 78]
015188 [Horton parameters: Pow= 76.20Fpc= 13.20DCAV= 4.14 F= 0.0]
015189 [Previous area: IArea= 4.67SLP= 2.00LSD= 40.0MP= 250ISCP= 0]
015190 [Impervious area: IArea= 16.5SLP= 2.00LSD= 120.0MI= 013ISCI= 0]
015191 [IAreaScp= 4.00 IAreaCp= 4.00]
015192 R0002-C00250-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015193 ADD HYD 1.0 02:18-D1I-MJ 40.82 1.627 0.042 28.18 14.35 n/a 0.00
015194 + 1.0 02:18-D1I-MN 13.78 0.776 0.042 28.06 17.09 n/a 0.00
015195 + 1.0 02:18-D1I-MN 40.77 1.627 0.042 28.08 16.28 n/a 0.00
015196 + 1.0 02:18-D1I-MN 40.82 1.627 0.042 28.08 16.28 n/a 0.00
015197 R0002-C00251-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015198 CONTINUOUS STANDBY 1.0 01:18-D1J 4.99 0.689 0.042 28.00 42.29 907 0.00
015199 [XIMP= 83-TIMP= 93]
015200 [Horton parameters: Pow= 76.20Fpc= 13.20DCAV= 4.14 F= 0.0]
015201 [Previous area: IArea= 4.67SLP= 2.00LSD= 40.0MP= 250ISCP= 0]
015202 [Impervious area: IArea= 1.57SLP= 2.00LSD= 182.0MI= 013ISCI= 0]
015203 [IAreaScp= 4.00 IAreaCp= 4.00]
015204 R0002-C00249-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015205 CONTINUOUS STANDBY 1.0 01:18-D1K 2.15 0.241 0.042 28.00 37.11 815 0.00
015206 [XIMP= 78-TIMP= 78]
015207 [Horton parameters: Pow= 76.20Fpc= 13.20DCAV= 4.14 F= 0.0]
015208 [Previous area: IArea= 16.5SLP= 2.00LSD= 120.0MI= 013ISCI= 0]
015209 [Impervious area: IArea= 16.5SLP= 2.00LSD= 120.0MI= 013ISCI= 0]
015210 [IAreaScp= 4.00 IAreaCp= 4.00]
015211 R0002-C00250-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015212 ADD HYD 1.0 02:18-D1K-MJ 40.82 1.627 0.042 28.18 14.35 n/a 0.00
015213 + 1.0 02:18-D1K-MN 13.78 0.776 0.042 28.06 17.09 n/a 0.00
015214 + 1.0 02:18-D1K-MN 40.77 1.627 0.042 28.08 16.28 n/a 0.00
015215 + 1.0 02:18-D1K-MN 40.82 1.627 0.042 28.08 16.28 n/a 0.00
015216 R0002-C00251-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015217 CONTINUOUS STANDBY 1.0 01:18-D1L 5.19 0.693 0.042 28.01 42.29 n/a 0.00
015218 + 1.0 02:18-D1L 12.93 1.683 0.042 28.00 39.68 n/a 0.00
015219 + 1.0 02:18-D1L 4.03 0.425 0.042 28.00 32.17 n/a 0.00
015220 R0002-C00251-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015221 CONTINUOUS STANDBY 1.0 01:18-D1M 206.72 9.491 0.042 28.02 20.13 n/a 0.00
015222 [Horton parameters: Pow= 76.20Fpc= 13.20DCAV= 4.14 F= 0.0]
015223 [Previous area: IArea= 4.67SLP= 2.00LSD= 40.0MP= 250ISCP= 0]
015224 [Impervious area: IArea= 1.57SLP= 2.00LSD= 182.0MI= 013ISCI= 0]
015225 [IAreaScp= 4.00 IAreaCp= 4.00]
015226 R0002-C00252-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015227 ADD HYD 1.0 02:18-D1M-MJ 206.72 9.491 0.042 28.02 20.13 n/a 0.00
015228 + 1.0 02:18-D1M-MN 206.72 9.491 0.042 28.02 20.13 n/a 0.00
015229 R0002-C00253-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015230 SAVE HYD 1.0 01:18-D1M-MJ 206.72 9.491 0.042 28.02 20.13 n/a 0.00
015231 [XIMP= 86-TIMP= 86]
015232 # remark:Total Flows at KB first pond
015233 R0002-C00253-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015234 CONTINUOUS STANDBY 1.0 01:18-D1N 10.86 1.337 0.042 28.00 39.32 864 0.00
015235 [XIMP= 86-TIMP= 86]
015236 [Horton parameters: Pow= 76.20Fpc= 13.20DCAV= 4.14 F= 0.0]
015237 [Previous area: IArea= 4.67SLP= 2.00LSD= 40.0MP= 250ISCP= 0]
015238 [Impervious area: IArea= 7.0SLP= 2.00LSD= 269.0MI= 013ISCI= 0]
015239 [IAreaScp= 4.00 IAreaCp= 4.00]
015240 R0002-C00253-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015241 COMPUTE DUALYD 1.0 01:18-D1N 10.86 1.337 0.042 28.00 39.32 n/a 0.00
015242 Major System / 1.0 02:18-D1N-MJ 0.00 0.000 0.000 0.00 0.00 n/a 0.00
015243 Minor System / 1.0 02:18-D1N-MN 10.86 1.337 0.042 28.00 39.32 n/a 0.00
015244 [M$SysSto=0.000E+00, TotVolVol=0.000E+00, N=0, V=0, TotDurVof= 0 hrs]
015245 R0002-C00253-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015246 ADD HYD 1.0 02:18-D1N-MJ 10.86 1.337 0.042 28.00 39.32 n/a 0.00
015247 + 1.0 02:18-D1N-MN 10.86 1.337 0.042 28.00 39.32 n/a 0.00
015248 R0002-C00257-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015249 CONTINUOUS STANDBY 1.0 01:18-D1O 206.72 9.491 0.042 28.00 39.32 677 0.00
015250 [XIMP= 64-TIMP= 64]
015251 [Horton parameters: Pow= 76.20Fpc= 13.20DCAV= 4.14 F= 0.0]
015252 [Previous area: IArea= 4.67SLP= 2.00LSD= 40.0MP= 250ISCP= 0]
015253 [Impervious area: IArea= 7.9SLP= 2.00LSD= 120.0MI= 013ISCI= 0]
015254 [IAreaScp= 4.00 IAreaCp= 4.00]
015255 R0002-C00258-----Dtn:ID-HNYD-----AREHA-GPEARCS-TpeakDate_hh:mm-----Rvm-R-C-----DWPCS
015256 COMPUTE DUALYD 1.0 01:18-D1O 206.72 9.491 0.042 28.00 39.32 n/a 0.00
015257 Major System / 1.0 02:18-D1O-MJ 0.00 0.000 0.000 0.00 0.00 n/a 0.00
015258 Minor System / 1.0 02:18-D1O-MN 206.72 9.491 0.042 28.00 39.32 n/a 0.00
015259 [M$SysSto=0.000E+00, TotVolVol=0.000E+00, N=0
```





026139 [Impervious area IAlmp=1.57;SLP=1.00;LGI= 183.1;MI= .013;SCL= .0]
02620 [IAREXP= 4.00; IAREPC= 4.00]
02621 [SMIN= 33.81; SMAX=225.43; SK= .010]
02622 R0021 CO0402 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02623 COMPUTE DUALHYD 1.0 0.01A10 4.14 .246 NoDate 28:01 23.49 n/a .000
02624 Major System / 1.0 0.02A10-MJ 0.00 .000 NoDate 0:00 .00 n/a .000
02625 Minor System \ 1.0 0.03A11-MJ 4.14 .246 NoDate 28:01 23.49 n/a .000
02626 [MjSysSto=.0000E+00; TotOfVol=.0000E+00; N-ovf= 0; TotDurVof= 0 hrs]
02627 R0021 CO0403 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02628 CONTINUOUS STANBYD 1.0 0.01A11 10.61 .781 NoDate 28:02 29.20 1442 .000
02629 [XIMP= 53;TIMP= 42]
02630 [LQSS= 2 CM= 75.0]
02631 [Impervious area IAlmp=4.67;SLP=1.00;LGI= 40.1;MI= .250;SCL= .0]
02632 [IAREXP= 4.00; IAREPC= 4.00]
02633 [SMIN= 31.81; SMAX=225.43; SK= .010]
02634 R0021 CO0404 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02635 COMPUTE DUALHYD 1.0 0.01A10 10.61 .781 NoDate 28:02 29.20 n/a .000
02636 Major System / 1.0 0.02A11-MJ 0.00 .000 NoDate 0:00 .00 n/a .000
02637 Minor System \ 1.0 0.03A11-MJ 10.61 .781 NoDate 28:02 29.20 n/a .000
02638 [MjSysSto=.0000E+00; TotOfVol=.0000E+00; N-ovf= 0; TotDurVof= 0 hrs]
02639 R0021 CO0405 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02640 ADD HYD + 1.0 0.0210E-107 132.01 3.022 NoDate 28:06 26.40 n/a .000
02641 + 1.0 0.02A10-MJ 4.14 .246 NoDate 28:01 23.49 n/a .000
02642 + 1.0 0.02A11-MJ 10.61 .781 NoDate 28:02 29.20 n/a .000
02643 SIMM + 1.0 0.01SM187 146.76 4.889 NoDate 28:02 26.52 n/a .000
02644 R0021 CO0406 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02645 SAVE HYD fname :SMI\_0002 146.76 4.889 NoDate 28:02 26.52 n/a .000
02646 remark:Total Flows at Heart's Desire
02647 R0021 CO0407 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02648 ROUTE PIPE -> 1.0 0.0218107 146.76 4.889 NoDate 28:02 26.52 n/a .000
02649 [L/S= 114. / 1207.013]
02650 [Din= 1.80;Dused= 1.93]
02651 R0021 CO0408 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02652 ROUTE PIPE -> 1.0 0.02119-108 146.76 4.889 NoDate 28:07 26.52 n/a .000
02653 [L/S= 80. / 1397.013]
02654 [Vmax= 1.83;Dmax= 1.94]
02655 R0021 CO0409 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02656 CONTINUOUS STANBYD 1.0 0.01A12 12.29 .834 NoDate 28:01 25.66 1564 .000
02657 [XIMP= 53;TIMP= 42]
02658 [Impervious area IAlmp=1.57;SLP=1.00;LGI= 183.1;MI= .013;SCL= .0]
02659 [IAREXP= 4.00; IAREPC= 4.00]
02660 [SMIN= 33.81; SMAX=225.43; SK= .010]
02661 R0021 CO0410 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02662 COMPUTE DUALHYD 1.0 0.01A10 12.29 .834 NoDate 28:01 25.66 n/a .000
02663 Major System / 1.0 0.02A11-MJ 0.00 .000 NoDate 0:00 .00 n/a .000
02664 Minor System \ 1.0 0.03A11-MJ 12.29 .834 NoDate 28:01 25.66 n/a .000
02665 [MjSysSto=.0000E+00; TotOfVol=.0000E+00; N-ovf= 0; TotDurVof= 0 hrs]
02666 R0021 CO0411 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02667 CONTINUOUS STANBYD 1.0 0.01A10 2.94 .190 NoDate 28:02 34.21 752 .000
02668 [XIMP= 41;TIMP= 71]
02669 [Impervious area IAlmp=4.67;SLP=1.00;LGI= 40.1;MI= .250;SCL= .0]
02670 [IAREXP= 4.00; IAREPC= 4.00]
02671 [SMIN= 33.81; SMAX=225.43; SK= .010]
02672 R0021 CO0412 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02673 COMPUTE DUALHYD 1.0 0.01A10 12.29 .834 NoDate 28:01 25.66 n/a .000
02674 Major System / 1.0 0.02A11-MJ 0.00 .000 NoDate 0:00 .00 n/a .000
02675 Minor System \ 1.0 0.03A11-MJ 12.29 .834 NoDate 28:01 25.66 n/a .000
02676 [MjSysSto=.0000E+00; TotOfVol=.0000E+00; N-ovf= 0; TotDurVof= 0 hrs]
02677 R0021 CO0413 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02678 CONTINUOUS STANBYD 1.0 0.01A12 12.29 .834 NoDate 28:01 25.66 1564 .000
02679 [XIMP= 53;TIMP= 42]
02680 [Impervious area IAlmp=1.57;SLP=1.00;LGI= 183.1;MI= .013;SCL= .0]
02681 [IAREXP= 4.00; IAREPC= 4.00]
02682 [SMIN= 33.81; SMAX=225.43; SK= .010]
02683 R0021 CO0414 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02684 COMPUTE DUALHYD 1.0 0.01A10 12.29 .834 NoDate 28:01 25.66 n/a .000
02685 Major System / 1.0 0.02A11-MJ 0.00 .000 NoDate 0:00 .00 n/a .000
02686 Minor System \ 1.0 0.03A11-MJ 12.29 .834 NoDate 28:01 25.66 n/a .000
02687 [MjSysSto=.0000E+00; TotOfVol=.0000E+00; N-ovf= 0; TotDurVof= 0 hrs]
02688 R0021 CO0415 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02689 SAVE HYD fname :SMI\_0002 161.64 5.396 NoDate 28:03 26.58 n/a .000
02690 remark:Total Flows at Heart's Desire
02691 R0021 CO0416 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02692 ROUTE PIPE -> 1.0 0.0218108 161.64 5.396 NoDate 28:03 26.58 n/a .000
02693 [L/S= 71. / 1313.013]
02694 [Vmax= 1.87;Dmax= 1.93]
02695 R0021 CO0417 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02696 ROUTE PIPE -> 1.0 0.02108-116 161.64 5.396 NoDate 28:04 26.58 n/a .000
02697 [L/S= 80. / 1397.013]
02698 [Vmax= 1.83;Dmax= 1.94]
02699 R0021 CO0418 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02700 CONTINUOUS STANBYD 1.0 0.01A12 161.64 5.396 NoDate 28:04 26.58 n/a .000
02701 [XIMP= 53;TIMP= 42]
02702 [Impervious area IAlmp=1.57;SLP=1.00;LGI= 183.1;MI= .013;SCL= .0]
02703 [IAREXP= 4.00; IAREPC= 4.00]
02704 [SMIN= 33.81; SMAX=225.43; SK= .010]
02705 R0021 CO0419 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02706 ADD HYD + 1.0 0.02119-108 146.76 4.889 NoDate 28:07 26.52 n/a .000
02707 + 1.0 0.02A10-MJ 4.14 .246 NoDate 28:01 23.49 n/a .000
02708 + 1.0 0.02A11-MJ 10.61 .781 NoDate 28:02 29.20 n/a .000
02709 SIMM + 1.0 0.01SM187 146.76 4.889 NoDate 28:02 26.52 n/a .000
02710 R0021 CO0420 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02711 SAVE HYD fname :SMI\_0002 161.64 5.396 NoDate 28:04 26.54 n/a .000
02712 remark:Total Flows at Corriegan Pond
02713 R0021 CO0420 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02714 ROUTE RESERVOIR -> 1.0 0.02CORRIEGAN 164.58 5.322 NoDate 28:04 26.54 n/a .000
02715 R0021 CO0421 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02716 OVERFLOW -> 1.0 0.03COV-OFF 0.00 .000 NoDate 0:00 .00 n/a .000
02717 [MjSysSto=.0000E+00; TotOfVol=.0000E+00; N-ovf= 0; TotDurVof= 0 hrs]
02718 R0021 CO0421 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02719 ADD HYD + 1.0 0.0210E-107 164.58 4.889 NoDate 28:06 26.40 n/a .000
02720 + 1.0 0.02A10-MJ 4.14 .246 NoDate 28:01 23.49 n/a .000
02721 + 1.0 0.02A11-MJ 10.61 .781 NoDate 28:02 29.20 n/a .000
02722 SIMM + 1.0 0.01SM187 164.58 4.889 NoDate 28:02 26.52 n/a .000
02723 R0021 CO0422 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02724 SAVE HYD fname :CORRIEGAN\_0002 164.58 4.889 NoDate 28:06 26.30 n/a .000
02725 remark:Total Flows at Corriegan Pond
02726 R0021 CO0423 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02727 ROUTE RESERVOIR -> 1.0 0.03CORRIEGAN 164.58 5.322 NoDate 28:04 26.54 n/a .000
02728 R0021 CO0424 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02729 OVERFLOW -> 1.0 0.03COV-OFF 0.00 .000 NoDate 0:00 .00 n/a .000
02730 [MjSysSto=.0000E+00; TotOfVol=.0000E+00; N-ovf= 0; TotDurVof= 0 hrs]
02731 R0021 CO0424 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02732 ADD HYD + 1.0 0.0210E-107 164.58 4.889 NoDate 28:06 26.40 n/a .000
02733 + 1.0 0.02A10-MJ 4.14 .246 NoDate 28:01 23.49 n/a .000
02734 + 1.0 0.02A11-MJ 10.61 .781 NoDate 28:02 29.20 n/a .000
02735 SIMM + 1.0 0.01SM187 164.58 4.889 NoDate 28:02 26.52 n/a .000
02736 R0021 CO0425 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02737 SAVE HYD fname :CORRIEGAN\_0002 164.58 4.889 NoDate 28:06 26.30 n/a .000
02738 remark:Total Flows at Corriegan Pond
02739 R0021 CO0426 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02740 ROUTE RESERVOIR -> 1.0 0.03CORRIEGAN 164.58 5.322 NoDate 28:04 26.54 n/a .000
02741 R0021 CO0427 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02742 OVERFLOW -> 1.0 0.03COV-OFF 0.00 .000 NoDate 0:00 .00 n/a .000
02743 [MjSysSto=.0000E+00; TotOfVol=.0000E+00; N-ovf= 0; TotDurVof= 0 hrs]
02744 R0021 CO0427 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02745 ADD HYD + 1.0 0.0210E-107 164.58 4.889 NoDate 28:06 26.40 n/a .000
02746 + 1.0 0.02A10-MJ 4.14 .246 NoDate 28:01 23.49 n/a .000
02747 + 1.0 0.02A11-MJ 10.61 .781 NoDate 28:02 29.20 n/a .000
02748 SIMM + 1.0 0.01SM187 164.58 4.889 NoDate 28:02 26.52 n/a .000
02749 R0021 CO0428 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02750 SAVE HYD fname :SMI\_0002 159.94 4.925 NoDate 39:17 13.21 n/a .000
02751 remark:Total Flows at Jockvale Road
02752 R0021 CO0429 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02753 HYDROGRAPH FROM HEART'S DESIRE
02754 Channel X-Section obtained from RUCVA Hydraulic Model - Station 699
02755 R0021 CO0430 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02756 ROUTE CHANNEL -> 1.0 0.02CORR 55018.86 49.095 NoDate 38:55 13.18 n/a .000
02757 [L/S= 880. / 4481.845]
02758 [Vmax= 1.454;Dmax= 1.224]
02759 # Catchment MILLS
02760 # - To SW facility north of the Jock
02761 # - Primarily residential development
02762 R0021 CO0431 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02763 CONTINUOUS STANBYD 1.0 0.01MILLS 175.99 7.048 NoDate 28:08 22.75 1500 .000
02764 [XIMP= 38;TIMP= 38]
02765 [LQSS= 2 CM= 74.0]
02766 [Impervious area IAlmp=4.67;SLP=1.00;LGI= 40.1;MI= .250;SCL= .0]
02767 [IAREXP= 4.00; IAREPC= 4.00]
02768 [SMIN= 36.67; SMAX=207.66; SK= .010]
02769 R0021 CO0432 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02770 COMPUTE DUALHYD 1.0 0.01A10 175.99 7.048 NoDate 28:08 22.75 n/a .000
02771 Major System / 1.0 0.02MILLS 0.00 .000 NoDate 0:00 .00 n/a .000
02772 Minor System \ 1.0 0.03MILLS 175.99 7.048 NoDate 28:08 22.75 n/a .000
02773 [MjSysSto=.0000E+00; TotOfVol=.0000E+00; N-ovf= 0; TotDurVof= 0 hrs]
02774 R0021 CO0433 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02775 ADD HYD + 1.0 0.02181-MJ 175.99 7.048 NoDate 28:08 22.75 n/a .000
02776 + 1.0 0.02A10-MJ 4.14 .246 NoDate 28:01 23.49 n/a .000
02777 + 1.0 0.02A11-MJ 175.99 7.048 NoDate 28:08 22.75 n/a .000
02778 SIMM + 1.0 0.01SM187 175.99 7.048 NoDate 28:08 22.75 n/a .000
02779 R0021 CO0434 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02780 SAVE HYD fname :SMI\_0002 159.94 4.925 NoDate 39:17 13.21 n/a .000
02781 remark:Total Flows at Jockvale Road
02782 R0021 CO0435 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02783 HYDROGRAPH FROM HEART'S DESIRE
02784 Channel X-Section obtained from RUCVA Hydraulic Model - Station 699
02785 R0021 CO0436 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02786 ROUTE CHANNEL -> 1.0 0.02CORR 55194.85 49.250 NoDate 39:17 13.21 n/a .000
02787 [L/S= 1142. / 2211.845]
02788 [Vmax= 1.444;Dmax= 1.611]
02789 # Catchment DESIRE
02790 # - To Jock River (north of the Jock)
02791 # - Rural/semi residential development
02792 R0021 CO0437 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02793 CONTINUOUS STANBYD 1.0 0.01DESIRE 23.78 .936 NoDate 28:03 19.26 1423 .000
02794 [XIMP= 25;TIMP= 25]
02800 [LOSS= 2 CM= 77.0]
02801 [Impervious area IAlmp=4.67;SLP=1.00;LGI= 40.1;MI= .250;SCL= .0]
02802 [IAREXP= 4.00; IAREPC= 4.00]
02803 [SMIN= 31.81; SMAX=225.43; SK= .010]
02804 R0021 CO0438 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02805 COMPUTE DUALHYD 1.0 0.01A10 23.78 .936 NoDate 28:03 19.26 n/a .000
02806 Major System / 1.0 0.02JOCKVA 0.00 .000 NoDate 0:00 .00 n/a .000
02807 Minor System \ 1.0 0.03JOCKVA 23.78 .936 NoDate 28:03 19.26 n/a .000
02808 [MjSysSto=.0000E+00; TotOfVol=.0000E+00; N-ovf= 0; TotDurVof= 0 hrs]
02809 R0021 CO0439 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02810 CONTINUOUS STANBYD 1.0 0.01JOCKVA 257.63 12.234 NoDate 28:07 26.85 990 .000
02811 [XIMP= 50;TIMP= 50]
02812 [LQSS= 2 CM= 74.0]
02813 [Impervious area IAlmp=4.67;SLP=1.00;LGI= 40.1;MI= .250;SCL= .0]
02814 [IAREXP= 4.00; IAREPC= 4.00]
02815 [SMIN= 36.67; SMAX=244.49; SK= .010]
02816 R0021 CO0440 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02817 ADD HYD + 1.0 0.0210E-107 32.50 2.093 NoDate 28:02 26.85 n/a .000
02818 + 1.0 0.02JOCKVA-MN 257.63 12.234 NoDate 28:07 26.85 n/a .000
02819 + 1.0 0.02B2-MJ 0.00 .000 NoDate 0:00 .00 n/a .000
02820 + 1.0 0.02B3-MJ 0.00 .000 NoDate 0:00 .00 n/a .000
02821 SIMM + 1.0 0.01SM187 257.63 12.234 NoDate 28:07 26.85 n/a .000
02822 R0021 CO0441 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02823 SAVE HYD fname :JOCKVA-TD\_0002 257.63 12.234 NoDate 28:07 26.85 n/a .000
02824 remark:Total Flows at RR first pond
02825 R0021 CO0442 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02826 HYDROGRAPH FROM HEART'S DESIRE
02827 Channel X-Section obtained from RUCVA Hydraulic Model - Station 0
02828 R0021 CO0443 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02829 ROUTE CHANNEL -> 1.0 0.02RIDEAU 55476.26 49.606 NoDate 39:13 13.27 n/a .000
02830 [L/S= 563. / 957.445]
02831 [Vmax= 1.490;Dmax= .801]
02832 R0021 CO0444 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02833 CONTINUOUS STANBYD 1.0 0.01R-2 102.94 1.373 NoDate 28:20 13.01 286 .000
02834 [XIMP= 50;TIMP= 50]
02835 [Impervious area IAlmp=1.57;SLP=1.00;LGI= 183.1;MI= .013;SCL= .0]
02836 [IAREXP= 4.00; IAREPC= 4.00]
02837 [SMIN= 33.81; SMAX=225.43; SK= .010]
02838 R0021 CO0445 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02839 COMPUTE DUALHYD 1.0 0.01A10 102.94 1.373 NoDate 28:20 13.01 286 .000
02840 Major System / 1.0 0.02RIDEAU 0.00 .000 NoDate 0:00 .00 n/a .000
02841 Minor System \ 1.0 0.03RIDEAU 102.94 1.373 NoDate 28:20 13.01 286 .000
02842 [MjSysSto=.0000E+00; TotOfVol=.0000E+00; N-ovf= 0; TotDurVof= 0 hrs]
02843 R0021 CO0446 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02844 ADD HYD + 1.0 0.02181-DE 55194.85 49.250 NoDate 39:17 13.21 n/a .000
02845 + 1.0 0.02JOCKVA-MN 257.63 12.234 NoDate 28:07 26.85 n/a .000
02846 SIMM + 1.0 0.01SM187 55194.85 49.250 NoDate 39:17 13.21 n/a .000
02847 R0021 CO0447 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02848 SAVE HYD fname :SMI\_0002 55476.26 49.606 NoDate 39:13 13.27 n/a .000
02849 remark:Total Flows at Rideau River
02850 R0021 CO0448 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02851 HYDROGRAPH FROM HEART'S DESIRE
02852 Channel X-Section obtained from RUCVA Hydraulic Model - Station 0
02853 R0021 CO0449 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02854 ROUTE CHANNEL -> 1.0 0.02RIDEAU 55476.26 49.606 NoDate 39:13 13.27 n/a .000
02855 [L/S= 563. / 957.445]
02856 [Vmax= 1.490;Dmax= .801]
02857 R0021 CO0450 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02858 CONTINUOUS STANBYD 1.0 0.01R-2 102.94 1.373 NoDate 28:20 13.01 286 .000
02859 [XIMP= 50;TIMP= 50]
02860 [Impervious area IAlmp=1.57;SLP=1.00;LGI= 183.1;MI= .013;SCL= .0]
02861 [IAREXP= 4.00; IAREPC= 4.00]
02862 [SMIN= 33.81; SMAX=225.43; SK= .010]
02863 R0021 CO0451 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02864 COMPUTE DUALHYD 1.0 0.01A10 102.94 1.373 NoDate 28:20 13.01 286 .000
02865 Major System / 1.0 0.02RIDEAU 0.00 .000 NoDate 0:00 .00 n/a .000
02866 Minor System \ 1.0 0.03RIDEAU 102.94 1.373 NoDate 28:20 13.01 286 .000
02867 [MjSysSto=.0000E+00; TotOfVol=.0000E+00; N-ovf= 0; TotDurVof= 0 hrs]
02868 R0021 CO0452 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02869 ADD HYD + 1.0 0.02181-DE 55194.85 49.250 NoDate 39:17 13.21 n/a .000
02870 + 1.0 0.02JOCKVA-MN 257.63 12.234 NoDate 28:07 26.85 n/a .000
02871 SIMM + 1.0 0.01SM187 55194.85 49.250 NoDate 39:17 13.21 n/a .000
02872 R0021 CO0453 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02873 SAVE HYD fname :SMI\_0002 55476.26 49.606 NoDate 39:13 13.27 n/a .000
02874 remark:Total Flows at Rideau River
02875 R0021 CO0454 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02876 HYDROGRAPH FROM HEART'S DESIRE
02877 Channel X-Section obtained from RUCVA Hydraulic Model - Station 0
02878 R0021 CO0455 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02879 ROUTE CHANNEL -> 1.0 0.02RIDEAU 55476.26 49.606 NoDate 39:13 13.27 n/a .000
02880 [L/S= 563. / 957.445]
02881 [Vmax= 1.490;Dmax= .801]
02882 R0021 CO0456 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02883 CONTINUOUS STANBYD 1.0 0.01R-2 102.94 1.373 NoDate 28:20 13.01 286 .000
02884 [XIMP= 50;TIMP= 50]
02885 [Impervious area IAlmp=1.57;SLP=1.00;LGI= 183.1;MI= .013;SCL= .0]
02886 [IAREXP= 4.00; IAREPC= 4.00]
02887 [SMIN= 33.81; SMAX=225.43; SK= .010]
02888 R0021 CO0457 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02889 COMPUTE DUALHYD 1.0 0.01A10 102.94 1.373 NoDate 28:20 13.01 286 .000
02890 Major System / 1.0 0.02RIDEAU 0.00 .000 NoDate 0:00 .00 n/a .000
02891 Minor System \ 1.0 0.03RIDEAU 102.94 1.373 NoDate 28:20 13.01 286 .000
02892 [MjSysSto=.0000E+00; TotOfVol=.0000E+00; N-ovf= 0; TotDurVof= 0 hrs]
02893 R0021 CO0458 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02894 ADD HYD + 1.0 0.02181-DE 55194.85 49.250 NoDate 39:17 13.21 n/a .000
02895 + 1.0 0.02JOCKVA-MN 257.63 12.234 NoDate 28:07 26.85 n/a .000
02896 SIMM + 1.0 0.01SM187 55194.85 49.250 NoDate 39:17 13.21 n/a .000
02897 R0021 CO0459 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02898 SAVE HYD fname :SMI\_0002 55476.26 49.606 NoDate 39:13 13.27 n/a .000
02899 remark:Total Flows at Rideau River
02900 R0021 CO0460 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02901 HYDROGRAPH FROM HEART'S DESIRE
02902 Channel X-Section obtained from RUCVA Hydraulic Model - Station 0
02903 R0021 CO0461 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02904 ROUTE CHANNEL -> 1.0 0.02RIDEAU 55476.26 49.606 NoDate 39:13 13.27 n/a .000
02905 [L/S= 563. / 957.445]
02906 [Vmax= 1.490;Dmax= .801]
02907 R0021 CO0462 -----DRAIN-ID=HYD-----AREHA-OPEAFCMS-TPeakDate\_hh:mm-----RvM-R-C-----DWPFMS
02908 CONTINUOUS STANBYD 1.0 0.01R-2 102.94 1.373 NoDate 28:20 13.01 286 .000
02909 [XIMP= 50;TIMP= 50]
02910 [Impervious area IAlmp=1.57;SLP=1.00;LGI= 183.1;MI= .013;SCL= .0]
02911

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02993 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
02994 # of 1.52
02995 R005C0012-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
02996 CONTINUOUS NASHVD 1.0 01:R05_CK 5666.00 16.924 No_date 38:02 20.12 352 0.000
02997 [Cm 72.01 Nn 3.00 Tp 8.00]
02998 [AREC 4.00 SMIN: 39.75; SMAK:264.99; EK -010]
02999 [InterVTime= 12.00]
03000 #
03001 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
03002 # of 3.75
03003 R005C0011-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03004 CONTINUOUS NASHVD 1.0 01:R05_CK 8376.00 16.342 No_date 39:59 17.18 301 0.000
03005 [Cm 66.01 Nn 3.00 Tp 11.64]
03006 [AREC 4.00 SMIN: 55.62; SMAK:350.79; EK -010]
03007 [InterVTime= 12.00]
03008 #
03009 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
03010 # of 1.68
03011 R005C0014-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03012 CONTINUOUS NASHVD 1.0 01:R05_S 1132.00 6.963 No_date 30:55 19.24 137 0.000
03013 [Cm 70.01 Nn 3.00 Tp 2.51]
03014 [AREC 4.00 SMIN: 43.07; SMAK:287.10; EK -010]
03015 [InterVTime= 12.00]
03016 #
03017 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
03018 # of 1.82
03019 R005C0015-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03020 CONTINUOUS NASHVD 1.0 01:R05_CK 4464.00 8.109 No_date 39:59 15.66 274 0.000
03021 [Cm 62.01 Nn 3.00 Tp 11.32]
03022 [AREC 4.00 SMIN: 61.90; SMAK:412.66; EK -010]
03023 [InterVTime= 12.00]
03024 #
03025 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
03026 # of 1.80
03027 R005C0016-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03028 CONTINUOUS NASHVD 1.0 01:R05_S 131.00 1.298 No_date 28:57 16.03 281 0.000
03029 [Cm 61.01 Nn 3.00 Tp .90]
03030 [AREC 4.00 SMIN: 59.42; SMAK:396.11; EK -010]
03031 [InterVTime= 12.00]
03032 #
03033 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
03034 # of 1.81
03035 R005C0017-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03036 CONTINUOUS NASHVD 1.0 01:R05_DR 3854.00 9.385 No_date 38:41 17.18 301 0.000
03037 [Cm 62.01 Nn 3.00 Tp 8.91]
03038 [AREC 4.00 SMIN: 52.62; SMAK:350.79; EK -010]
03039 [InterVTime= 12.00]
03040 #
03041 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
03042 # of 1.82
03043 R005C0018-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03044 CONTINUOUS NASHVD 1.0 01:R05_CK 1397.21 7.027 No_date 36:28 13.49 243 0.000
03045 [Cm 57.01 Nn 3.00 Tp 6.61]
03046 [AREC 4.00 SMIN: 59.42; SMAK:508.81; EK -010]
03047 [InterVTime= 12.00]
03048 #
03049 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
03050 # of 3.75
03051 R005C0019-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03052 CONTINUOUS NASHVD 1.0 01:R05_E 165.00 .641 No_date 33:06 17.58 308 0.000
03053 [Cm 47.01 Nn 3.00 Tp 1.81]
03054 [AREC 4.00 SMIN: 50.55; SMAK:336.97; EK -010]
03055 [InterVTime= 12.00]
03056 #
03057 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
03058 # of 1.47
03059 R005C0020-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03060 CONTINUOUS NASHVD 1.0 01:R05_DR 1332.00 4.803 No_date 35:19 20.12 352 0.000
03061 [Cm 72.01 Nn 3.00 Tp 9.91]
03062 [AREC 4.00 SMIN: 39.75; SMAK:264.99; EK -010]
03063 [InterVTime= 12.00]
03064 R005C0021-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03065 CONTINUOUS NASHVD 1.0 01:R05_S 224.00 4.100 No_date 28:45 22.97 402 0.000
03066 [Cm 77.01 Nn 3.00 Tp .75]
03067 [AREC 4.00 SMIN: 31.15; SMAK:207.66; EK -010]
03068 [InterVTime= 12.00]
03069 #
03070 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
03071 # of 1.50
03072 R005C0022-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03073 CONTINUOUS NASHVD 1.0 01:R05_CK 4945.00 22.837 No_date 33:22 21.04 368 0.000
03074 [Cm 74.01 Nn 3.00 Tp 4.45]
03075 [AREC 4.00 SMIN: 31.67; SMAK:244.49; EK -010]
03076 [InterVTime= 12.00]
03077 R005C0023-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03078 CONTINUOUS NASHVD 1.0 01:R05_S2 20.00 .483 No_date 28:36 25.62 448 0.000
03079 [Cm 81.01 Nn 3.00 Tp .62]
03080 [AREC 4.00 SMIN: 25.21; SMAK:168.09; EK -010]
03081 [InterVTime= 12.00]
03082 #
03083 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
03084 # of 1.61
03085 R005C0024-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03086 CONTINUOUS NASHVD 1.0 01:R05_S1 1412.00 4.646 No_date 37:58 21.98 385 0.000
03087 [Cm 70.01 Nn 3.00 Tp 9.91]
03088 [AREC 4.00 SMIN: 31.81; SMAK:225.43; EK -010]
03089 [InterVTime= 12.00]
03090 R005C0025-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03091 CONTINUOUS NASHVD 1.0 01:R05_A 585.00 6.888 No_date 29:57 25.62 448 0.000
03092 [Cm 81.01 Nn 3.00 Tp 2.46]
03093 [AREC 4.00 SMIN: 25.21; SMAK:168.09; EK -010]
03094 [InterVTime= 12.00]
03095 R005C0026-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03096 CONTINUOUS NASHVD 1.0 01:R05_CK 1021.00 8.861 No_date 30:48 25.07 439 0.000
03097 [Cm 80.01 Nn 3.00 Tp 2.46]
03098 [AREC 4.00 SMIN: 26.32; SMAK:175.50; EK -010]
03099 [InterVTime= 12.00]
03100 R005C0027-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03101 CONTINUOUS NASHVD 1.0 01:R05_CK 177.00 3.240 No_date 28:45 22.97 402 0.000
03102 [Cm 77.01 Nn 3.00 Tp .75]
03103 [AREC 4.00 SMIN: 31.15; SMAK:207.66; EK -010]
03104 [InterVTime= 12.00]
03105 R005C0028-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03106 CONTINUOUS NASHVD 1.0 01:R05_S 1122.00 8.265 No_date 31:48 25.62 448 0.000
03107 [Cm 81.01 Nn 3.00 Tp 1.25]
03108 [AREC 4.00 SMIN: 31.15; SMAK:168.09; EK -010]
03109 [InterVTime= 12.00]
03110 R005C0029-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03111 CONTINUOUS NASHVD 1.0 01:R05_CK 2737.00 17.459 No_date 31:33 22.47 393 0.000
03112 [Cm 76.01 Nn 3.00 Tp 3.03]
03113 [AREC 4.00 SMIN: 31.15; SMAK:216.39; EK -010]
03114 [InterVTime= 12.00]
03115 #
03116 Routing hydrographs
03117 #
03118 Starting with the addition of Jock River Headwater and Subwatershed 13
03119 #
03120 R005C0030-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03121 ADD HYD + 1.0 02:R05_RV 3680.00 9.398 No_date 37:02 16.41 n/a 0.000
03122 + 1.0 02:R05_CK 1122.00 11.405 No_date 32:16 15.29 n/a 0.000
03123 SUM 1.0 01:R05_S1 4651.00 11.949 No_date 35:13 16.37 n/a 0.000
03124 #
03125 Sum of hydrographs from Node 13 routed to Node 13A
03126 [Approximated cross-section - see cross-section 258]
03127 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
03128 #
03129 R005C0031-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03130 ROUTE CHANNEL -> 1.0 01:R05_M3 4651.00 11.949 No_date 35:13 16.17 n/a 0.000
03131 [RPT= 1.00] out<- 1.0 01:R05_M3 4651.00 9.514 No_date 39:57 16.17 n/a 0.000
03132 [L/S=n 5974. / .027/.040]
03133 [Vmax= .478;Dmax= 3.020]
03134 #
03135 Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
03136 #
03137 R005C0032-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03138 ADD HYD + 1.0 02:R05_M3 4651.00 9.514 No_date 39:57 16.17 n/a 0.000
03139 + 1.0 02:R05_CK 3874.00 4.682 No_date 39:59 13.23 n/a 0.000
03140 SUM 1.0 01:R05_M3 7725.00 14.196 No_date 39:59 15.00 n/a 0.000
03141 #
03142 Insertion of a reservoir to simulate the effects of the Goodwood Marsh
03143 #
03144 R005C0033-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03145 ROUTE RESERVOIR -> 1.0 02:R05_M3 7725.00 14.196 No_date 39:59 15.00 n/a 0.000
03146 [Mdt=0.05d-.631E+02 m3]
03147 [InterVTime= 12.00]
03148 #
03149 R005C0034-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03150 SAVE HYD 1.0 01:R05_CK 7725.00 3.149 No_date 57:25 15.00 n/a 0.000
03151 frame_H_R05M3
03152 remark:flow at Res Out
03153 #
03154 Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
03155 # [Approximated cross-section - see cross-section 258]
03156 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
03157 R005C0035-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03158 ROUTE CHANNEL -> 1.0 02:R05_M2 7725.00 3.149 No_date 57:25 15.00 n/a 0.000
03159 [RPT= 1.00] out<- 1.0 02:R05_M2 7725.00 1.377 No_date 60:12 15.00 n/a 0.000
03160 [L/S=n 5926. / .076/.040]
03161 [Vmax= .527;Dmax= 1.429]
03162 #
03163 Addition of Subwatershed Jock River at Ashton to Node 12
03164 #
03165 R005C0036-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03166 ADD HYD + 1.0 02:R05_ASH 1781.00 8.521 No_date 32:43 20.12 n/a 0.000
03167 + 1.0 02:R05_M2 9506.00 10.498 No_date 32:46 15.96 n/a 0.000
03168 SUM 1.0 01:R05_M2 11287.00 18.989 No_date 32:46 15.96 n/a 0.000
03169 R005C0037-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS
03170 SAVE HYD 1.0 01:R05_M2 9506.00 10.498 No_date 32:46 15.96 n/a 0.000
03171 frame_H_R05M2
03172 remark:flow at R_M2 near Ashton
03173 #
03174 Sum of hydrographs from Node 12 routed to Node 11
03175 [Approximated cross-section - see cross-section 258]
03176 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
03177 #
03178 Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
03179 #
03180 R005C0038-----DtnIn-ID:HYD-----AREAh-QPEARCS-TpeakDate_hh:mm-----RvM-R.C-----DWFCMS

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052377	[SMIN:33.81;SMAX:225.43;SK:010]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
052378	REMARK:Total Flows at MH140	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
052379	COMPUTE DUALHYD	1.0 01:184	7.60	638	28:02	34.82	n/a
052380	Major System	1.0 01:285-MJ	0.00	0.00	0:00	0.00	n/a
052381	Minor System	1.0 01:285-MN	7.60	638	28:02	34.82	n/a
052420	[MjSysTot=0.0000E+00;TotOvVol=0.0000E+00;N-OvFl=0;TotDurOvFl=0.hrs]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
052443	ADD HYD	1.0 01:338-10A	17.90	1,183	28:06	34.84	n/a
052445	+	1.0 01:285-MJ	7.60	638	28:02	34.82	n/a
052446	SUM=	1.0 01:363A0	25.50	1,761	28:06	34.83	n/a
052480	SAVE HYD	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
052481	fname:MH140.0005	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
052500	REMARK:Total Flows at MH140	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
052511	COMPUTE DUALHYD	1.0 01:184	25.50	1,761	28:05	34.83	n/a
052520	Major System	1.0 01:285-MJ	0.00	0.00	0:00	0.00	n/a
052521	Minor System	1.0 01:285-MN	25.50	1,761	28:05	34.83	n/a
052560	SUM=	1.0 01:363A0	25.50	1,761	28:05	34.83	n/a
052599	SAVE HYD	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
052599	+	1.0 01:363A0	25.50	1,761	28:05	34.83	n/a
052620	ROUTER PIPE	1.0 01:363A0	132.52	8,463	28:04	35.27	n/a
052621	ROUTER PIPE	1.0 01:363A0	132.52	8,463	28:04	35.27	n/a
052623	[RPT:1.00] out<-	1.0 01:104-105	132.52	8,468	28:06	35.27	n/a
052640	[L/S= 380. / 100.013]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
052655	[Vmax:1.65;Dused=1.65]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
052670	CONTINUOUS STANDBY	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
052670	[LOGS:2 C/M= 75.0]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
052700	[Previous area: IArea: 4.67;SLP=1.0;LID= 40;HNP= 250;SCP= 0]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
052720	[Interp area: IArea: 1.57;SLP=1.0;LID= 183;HNP= 013;SCP= 0]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
052730	[IAreaClamp: 4.00; IAreaCrv: 4.00]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
052774	[SMIN:33.81;SMAX:225.43;SK:010]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
052775	COMPUTE DUALHYD	1.0 01:184	2.40	150	28:00	44.32	n/a
052776	Major System	1.0 01:285-MJ	0.00	0.00	0:00	0.00	n/a
052777	Minor System	1.0 01:285-MN	2.40	150	28:00	44.32	n/a
052780	[MjSysTot=0.0000E+00;TotOvVol=0.0000E+00;N-OvFl=0;TotDurOvFl=0.hrs]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
052810	ADD HYD	1.0 01:285-MJ	2.40	150	28:00	44.32	n/a
052811	ROUTER PIPE	1.0 01:285-MJ	132.52	8,463	28:04	35.27	n/a
053003	ROUTER PIPE	1.0 01:285-MJ	132.52	8,463	28:04	35.27	n/a
053010	[RPT:1.00] out<-	1.0 01:104-105	132.52	8,468	28:06	35.27	n/a
053020	[L/S= 380. / 100.013]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053030	[Vmax:2.01;Dmax=1.66]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053060	CONTINUOUS STANDBY	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053060	[LOGS:2 C/M= 75.0]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053070	[Previous area: IArea: 4.67;SLP=1.0;LID= 40;HNP= 250;SCP= 0]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053090	[Interp area: IArea: 1.57;SLP=1.0;LID= 186;HNP= 013;SCP= 0]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053100	[IAreaClamp: 4.00; IAreaCrv: 4.00]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053140	[SMIN:33.81;SMAX:225.43;SK:010]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053141	COMPUTE DUALHYD	1.0 01:184	0.96	130	28:00	44.32	n/a
053142	Major System	1.0 01:285-MJ	0.00	0.00	0:00	0.00	n/a
053143	Minor System	1.0 01:285-MN	0.96	130	28:00	44.32	n/a
053180	SUM=	1.0 01:363A0	0.96	130	28:00	44.32	n/a
053199	SAVE HYD	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053199	+	1.0 01:363A0	0.96	130	28:00	44.32	n/a
053230	ROUTER PIPE	1.0 01:363A0	132.52	8,463	28:06	35.27	n/a
053231	ROUTER PIPE	1.0 01:363A0	132.52	8,463	28:06	35.27	n/a
053233	[RPT:1.00] out<-	1.0 01:285-MJ	2.40	150	28:00	44.32	n/a
053240	[L/S= 240. / 100.013]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053255	[Vmax:1.66;Dmax=1.66]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053280	CONTINUOUS STANDBY	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053280	[LOGS:2 C/M= 75.0]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053290	[Previous area: IArea: 4.67;SLP=1.0;LID= 40;HNP= 250;SCP= 0]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053310	[Interp area: IArea: 1.57;SLP=1.0;LID= 186;HNP= 013;SCP= 0]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053320	[IAreaClamp: 4.00; IAreaCrv: 4.00]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053360	[SMIN:33.81;SMAX:225.43;SK:010]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053361	COMPUTE DUALHYD	1.0 01:184	0.96	130	28:00	44.32	n/a
053362	Major System	1.0 01:285-MJ	0.00	0.00	0:00	0.00	n/a
053363	Minor System	1.0 01:285-MN	0.96	130	28:00	44.32	n/a
053400	SUM=	1.0 01:363A0	0.96	130	28:00	44.32	n/a
053419	SAVE HYD	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053419	+	1.0 01:363A0	0.96	130	28:00	44.32	n/a
053450	ROUTER PIPE	1.0 01:363A0	132.52	8,463	28:06	35.27	n/a
053451	ROUTER PIPE	1.0 01:363A0	132.52	8,463	28:06	35.27	n/a
053453	[RPT:1.00] out<-	1.0 01:285-MJ	2.40	150	28:00	44.32	n/a
053460	[L/S= 240. / 100.013]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053475	[Vmax:1.66;Dmax=1.66]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053500	CONTINUOUS STANDBY	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053500	[LOGS:2 C/M= 75.0]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053510	[Previous area: IArea: 4.67;SLP=1.0;LID= 40;HNP= 250;SCP= 0]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053530	[Interp area: IArea: 1.57;SLP=1.0;LID= 186;HNP= 013;SCP= 0]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053540	[IAreaClamp: 4.00; IAreaCrv: 4.00]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053580	[SMIN:33.81;SMAX:225.43;SK:010]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053581	COMPUTE DUALHYD	1.0 01:184	3.29	2,064	28:02	35.73	n/a
053582	Major System	1.0 01:285-MJ	0.00	0.00	0:00	0.00	n/a
053583	Minor System	1.0 01:285-MN	3.29	2,064	28:02	35.73	n/a
053620	SUM=	1.0 01:363A0	3.29	2,064	28:02	35.73	n/a
053639	SAVE HYD	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053639	+	1.0 01:363A0	3.29	2,064	28:02	35.73	n/a
053670	ROUTER PIPE	1.0 01:363A0	132.52	8,463	28:06	35.27	n/a
053671	ROUTER PIPE	1.0 01:363A0	132.52	8,463	28:06	35.27	n/a
053673	[RPT:1.00] out<-	1.0 01:105-106A	110.61	3,005	28:08	35.39	n/a
053680	[L/S= 208. / 100.013]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053695	[Vmax:1.97;Dmax=1.84]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053820	[Din:1.80;Dused=1.80]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053830	CONTINUOUS STANDBY	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053830	[LOGS:2 C/M= 75.0]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053840	[Previous area: IArea: 4.67;SLP=1.0;LID= 40;HNP= 250;SCP= 0]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053860	[Interp area: IArea: 1.57;SLP=1.0;LID= 186;HNP= 013;SCP= 0]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053870	[IAreaClamp: 4.00; IAreaCrv: 4.00]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053910	[SMIN:36.67;SMAX:244.49;SK:010]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053911	COMPUTE DUALHYD	1.0 01:184	32.50	2,843	28:02	35.73	n/a
053912	Major System	1.0 01:285-MJ	0.00	0.00	0:00	0.00	n/a
053913	Minor System	1.0 01:285-MN	32.50	2,843	28:02	35.73	n/a
053950	SUM=	1.0 01:363A0	32.50	2,843	28:02	35.73	n/a
053969	SAVE HYD	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
053969	+	1.0 01:363A0	32.50	2,843	28:02	35.73	n/a
053990	ROUTER PIPE	1.0 01:363A0	132.52	8,463	28:06	35.27	n/a
053991	ROUTER PIPE	1.0 01:363A0	132.52	8,463	28:06	35.27	n/a
053993	[RPT:1.00] out<-	1.0 01:105-106A	110.61	3,005	28:08	35.39	n/a
054000	[L/S= 208. / 100.013]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
054015	[Vmax:1.63;Dmax=1.84]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
054020	[Din:1.80;Dused=1.84]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
054030	CONTINUOUS STANDBY	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
054030	[LOGS:2 C/M= 75.0]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
054040	[Previous area: IArea: 4.67;SLP=1.0;LID= 40;HNP= 250;SCP= 0]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
054060	[Interp area: IArea: 1.57;SLP=1.0;LID= 186;HNP= 013;SCP= 0]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
054070	[IAreaClamp: 4.00; IAreaCrv: 4.00]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
054110	[SMIN:33.81;SMAX:225.43;SK:010]	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
054111	COMPUTE DUALHYD	1.0 01:184	2.44	150	28:00	44.32	n/a
054112	Major System	1.0 01:285-MJ	0.00	0.00	0:00	0.00	n/a
054113	Minor System	1.0 01:285-MN	2.44	150	28:00	44.32	n/a
054150	SUM=	1.0 01:363A0	2.44	150	28:00	44.32	n/a
054169	SAVE HYD	-----	AREBAh-GPEARCS-TpeakDate_hh:mm	-----	RvMm-R.C.	-----	DWPFMS
054169	+	1.0 01:363A0	2.44	150	28:00	44.32	n/a
054190	ROUTER PIPE	1.0 01:363A0	132.52	8,463	28:06		

05611 # - To Jock River (north of the Jock)
05612 # Rural/Urban subwatershed (Heart's Desire Community)
05613 # \*\*\*\*\*
05614 # \*\*\*\*\*
05615 CONTINUOUS STANBYD 1.0 01:DESIRE 23.78 1.359 No.Date 28:03 27.22 477 .000
05616 [XMP= 25;TVP= 25]
05617 [LQSS= 2;CN= 77.0]
05618 [Previous area Iaper= 4.67;SLP1=0.0;LID= 40.0;MND= 250;DPC= 0]
05619 [Impervious area Iaper= 1.57;SLP1=0.0;LID= 400.0;MNI= 013;RCL= 0]
05620 [IareClmp= 4.00;IareKper= 4.00]
05621 [SIN= 15.0;SMX= 34.0;01]
05622 [InterEventTime= 12.00]
05623 # Catchment JockVA
05624 # To Jockvale SWM Facility
05625 # - Residential development & golf course
05626 # - JFSA 2021-11-11 updated JockVA area updating CONRID as per IRI GROUP, July 2008.
05627 # JockVA area became 235.13 ha instead of 257.63 ha. JockVA separated into two areas JockVA and EX-LAND 32.5 ha as
05628 # \*\*\*\*\*
05629 # \*\*\*\*\*
05630 CONTINUOUS STANBYD 1.0 01:JOCKVA 225.13 14.675 No.Date 28:09 35.73 626 .000
05631 [XMP= 50;TVP= 50]
05632 [LQSS= 2;CN= 74.0]
05633 [Previous area Iaper= 4.67;SLP1=0.0;LID= 40.0;MND= 250;DPC= 0]
05634 [Impervious area Iaper= 1.57;SLP1=0.0;LID= 400.0;MNI= 013;RCL= 0]
05635 [IareClmp= 4.00;IareKper= 4.00]
05636 [SIN= 15.0;SMX= 34.0;01]
05637 # \*\*\*\*\*
05638 # \*\*\*\*\*
05639 # \*\*\*\*\*
05640 # \*\*\*\*\*
05641 # \*\*\*\*\*
05642 # \*\*\*\*\*
05643 # \*\*\*\*\*
05644 # \*\*\*\*\*
05645 # \*\*\*\*\*
05646 # \*\*\*\*\*
05647 # \*\*\*\*\*
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06359# R0101C00091-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06360# ROUTE RESERVOIR -> 1.0 01:01:STRT 3.51 .518 No.Date 28:25 38.69 n/a .000
06361# out <= 1.0 01:01:STRT 59 .052 No.Date 28:05 38.69 n/a .000
06362# overFlow <= 1.0 01:01:STRT 59 .052 No.Date 28:05 38.69 n/a .000
06363# [MstOfsed:1835E-02 n3, TotOfVol:0.000E+00 n3, N-Ovrf: 0, TotDurOfV: 0 hrs]
06364# R0101C00092-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06365# CONTINUOUS STANDBY 1.0 01:01:STRT 59 .052 No.Date 28:04 22.40 346 .000
06366# [Cm: 60.0 N: 3.00 T: 1.0]
06367# [IARc: 4.00 SMI: 23.09 SMAX:140.62 SK: 010]
06368# [InterEventTime: 12.00]
06369# R0101C00093-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06370# ROUTE PIPE -> 1.0 02:01:STRT 60.55 .857 No.Date 29:04 22.40 n/a .000
06371# [RPT: 1.00] out <= 1.0 01:01:STRT 60.55 .852 No.Date 29:08 22.40 n/a .000
06372# [L/S: 528. / 230. / 043]
06373# [Vmax: 1.00]
06374# [XIMP: 68 TIMP: 85]
06375# R0101C00094-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06376# ADD HYD + 1.0 02:01:STRT 261.31 2.972 No.Date 28:31 17.14 n/a .000
06377# out <= 1.0 02:01:STRT 3.51 .518 No.Date 28:25 38.69 n/a .000
06378# + 1.0 02:01:STRT 2.50 .098 No.Date 28:24 50.29 n/a .000
06379# + 1.0 02:01:STRT 3.51 .518 No.Date 28:25 38.69 n/a .000
06380# + 1.0 02:01:STRT 59 .052 No.Date 28:05 38.69 n/a .000
06381# + 1.0 02:01:STRT 59 .052 No.Date 28:05 38.69 n/a .000
06382# + 1.0 02:01:STRT 60.55 .852 No.Date 29:08 22.40 n/a .000
06383# + 1.0 02:01:STRT 326.12 3.771 No.Date 28:40 18.45 n/a .000
06384# SUM 1.0 01:01:STRT 326.12 3.771 No.Date 28:40 18.45 n/a .000
06385# R0101C00095-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06386# CONTINUOUS STANDBY 1.0 01:01:STRT 3.51 .518 No.Date 28:01 50.29 777 .000
06387# [XIMP: 68 TIMP: 85]
06388# [Horton parameters: Fw: 76.20 Fc: 13.20 DCAV:4.14 Pa: 0.0]
06389# [Previous area: IApex: 4.67 SLPD: .50 LIDP: .50 HNDP: 250 IBCP: .0]
06390# [Impervious area: IAImp: 1.57 SLPD: .50 LIDP: 1.57 HNDP: 193.0 MI: .013 IBCI: .0]
06391# [IARcImp: 4.00 IARcP: 4.00]
06392# R0101C00096-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06393# ROUTE RESERVOIR -> 1.0 02:01:STRT 3.51 .518 No.Date 28:01 50.29 n/a .000
06394# out <= 1.0 02:01:STRT 3.51 .518 No.Date 28:01 50.29 n/a .000
06395# overFlow <= 1.0 02:01:STRT 0.00 .000 No.Date 0:00 .00 n/a .000
06396# [MstOfsed:1817E-01 n3, TotOfVol:0.000E+00 n3, N-Ovrf: 0, TotDurOfV: 0 hrs]
06397# R0101C00097-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06398# CONTINUOUS STANDBY 1.0 01:01:STRT 71 .089 No.Date 28:00 38.69 598 .000
06399# [XIMP: 68 TIMP: 87]
06400# [Horton parameters: Fw: 76.20 Fc: 13.20 DCAV:4.14 Pa: 0.0]
06401# [Previous area: IApex: 4.67 SLPD: .50 LIDP: .50 HNDP: 250 IBCP: .0]
06402# [Impervious area: IAImp: 1.57 SLPD: .50 LIDP: 1.57 HNDP: 193.0 MI: .013 IBCI: .0]
06403# [IARcImp: 4.00 IARcP: 4.00]
06404# R0101C00098-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06405# ROUTE RESERVOIR -> 1.0 02:01:STRT 71 .089 No.Date 28:00 38.69 n/a .000
06406# out <= 1.0 02:01:STRT 71 .089 No.Date 28:00 38.69 n/a .000
06407# overFlow <= 1.0 02:01:STRT 0.00 .000 No.Date 0:00 .00 n/a .000
06408# [MstOfsed:1988E-02 n3, TotOfVol:0.000E+00 n3, N-Ovrf: 0, TotDurOfV: 0 hrs]
06409# R0101C00099-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06410# ADD HYD + 1.0 02:01:STRT 326.12 3.771 No.Date 28:40 18.45 n/a .000
06411# out <= 1.0 02:01:STRT 3.51 .518 No.Date 28:25 38.69 n/a .000
06412# + 1.0 02:01:STRT 2.50 .098 No.Date 28:24 50.29 n/a .000
06413# + 1.0 02:01:STRT 3.51 .518 No.Date 28:25 38.69 n/a .000
06414# + 1.0 02:01:STRT 59 .052 No.Date 28:05 38.69 n/a .000
06415# + 1.0 02:01:STRT 60.55 .852 No.Date 29:08 22.40 n/a .000
06416# SUM 330.34 3.914 No.Date 28:39 18.83 n/a .000
06417# R0101C00100-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06418# ROUTE CHANNEL -> 1.0 02:01:STRT 330.34 3.914 No.Date 28:39 18.83 n/a .000
06419# [RPT: 1.00] [L/S: 528. / 230. / 043]
06420# [Vmax: 1.00]
06421# [XIMP: 68 TIMP: 85]
06422# R0101C00101-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06423# CONTINUOUS STANDBY 1.0 01:01:STRT 2.28 .046 No.Date 29:04 29.30 453 .000
06424# [Cm: 60.0 N: 3.00 T: 1.0]
06425# [IARc: 4.00 SMI: 23.09 SMAX:140.62 SK: 010]
06426# [InterEventTime: 12.00]
06427# R0101C00102-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06428# CONTINUOUS STANDBY 1.0 01:01:STRT 12.04 1.618 No.Date 28:04 50.29 777 .000
06429# [XIMP: 68 TIMP: 85]
06430# [Horton parameters: Fw: 76.20 Fc: 13.20 DCAV:4.14 Pa: 0.0]
06431# [Previous area: IApex: 4.67 SLPD: .50 LIDP: .50 HNDP: 250 IBCP: .0]
06432# [Impervious area: IAImp: 1.57 SLPD: .50 LIDP: 1.57 HNDP: 193.0 MI: .013 IBCI: .0]
06433# [IARcImp: 4.00 IARcP: 4.00]
06434# R0101C00103-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06435# ROUTE RESERVOIR -> 1.0 02:01:STRT 12.04 1.618 No.Date 28:04 50.29 n/a .000
06436# out <= 1.0 02:01:STRT 12.04 1.618 No.Date 28:04 50.29 n/a .000
06437# overFlow <= 1.0 02:01:STRT 0.00 .000 No.Date 0:00 .00 n/a .000
06438# [MstOfsed:1771E-01 n3, TotOfVol:0.000E+00 n3, N-Ovrf: 0, TotDurOfV: 0 hrs]
06439# R0101C00104-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06440# CONTINUOUS STANDBY 1.0 01:01:STRT 3.5 .046 No.Date 28:00 38.69 598 .000
06441# [XIMP: 68 TIMP: 87]
06442# [Horton parameters: Fw: 76.20 Fc: 13.20 DCAV:4.14 Pa: 0.0]
06443# [Previous area: IApex: 4.67 SLPD: .50 LIDP: .50 HNDP: 250 IBCP: .0]
06444# [Impervious area: IAImp: 1.57 SLPD: .50 LIDP: 1.57 HNDP: 193.0 MI: .013 IBCI: .0]
06445# [IARcImp: 4.00 IARcP: 4.00]
06446# R0101C00105-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06447# ROUTE RESERVOIR -> 1.0 02:01:STRT 3.5 .046 No.Date 28:00 38.69 n/a .000
06448# out <= 1.0 02:01:STRT 3.5 .046 No.Date 28:00 38.69 n/a .000
06449# overFlow <= 1.0 02:01:STRT 0.00 .000 No.Date 0:00 .00 n/a .000
06450# [MstOfsed:1424E-01 n3, TotOfVol:0.000E+00 n3, N-Ovrf: 0, TotDurOfV: 0 hrs]
06451# R0101C00106-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06452# CONTINUOUS STANDBY 1.0 01:01:STRT 5.30 .780 No.Date 28:02 50.29 777 .000
06453# [XIMP: 68 TIMP: 85]
06454# [Horton parameters: Fw: 76.20 Fc: 13.20 DCAV:4.14 Pa: 0.0]
06455# [Previous area: IApex: 4.67 SLPD: .50 LIDP: .50 HNDP: 250 IBCP: .0]
06456# [Impervious area: IAImp: 1.57 SLPD: .50 LIDP: 1.57 HNDP: 193.0 MI: .013 IBCI: .0]
06457# [IARcImp: 4.00 IARcP: 4.00]
06458# R0101C00107-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06459# ROUTE RESERVOIR -> 1.0 02:01:STRT 5.30 .780 No.Date 28:02 50.29 n/a .000
06460# out <= 1.0 02:01:STRT 5.30 .780 No.Date 28:02 50.29 n/a .000
06461# overFlow <= 1.0 02:01:STRT 0.00 .000 No.Date 0:00 .00 n/a .000
06462# [MstOfsed:1322E-01 n3, TotOfVol:0.000E+00 n3, N-Ovrf: 0, TotDurOfV: 0 hrs]
06463# R0101C00108-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06464# ADD HYD + 1.0 02:01:STRT 330.34 3.914 No.Date 28:39 18.83 n/a .000
06465# out <= 1.0 02:01:STRT 12.04 1.618 No.Date 28:31 50.29 n/a .000
06466# + 1.0 02:01:STRT 3.51 .518 No.Date 28:25 38.69 n/a .000
06467# + 1.0 02:01:STRT 2.50 .098 No.Date 28:24 50.29 n/a .000
06468# + 1.0 02:01:STRT 3.51 .518 No.Date 28:25 38.69 n/a .000
06469# + 1.0 02:01:STRT 59 .052 No.Date 28:05 38.69 n/a .000
06470# + 1.0 02:01:STRT 60.55 .852 No.Date 29:08 22.40 n/a .000
06471# SUM 330.34 3.914 No.Date 28:39 18.83 n/a .000
06472# R0101C00109-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06473# ROUTE CHANNEL -> 1.0 02:01:STRT 330.34 3.914 No.Date 28:39 18.83 n/a .000
06474# [RPT: 1.00] [L/S: 528. / 230. / 043]
06475# [Vmax: 1.00]
06476# [XIMP: 68 TIMP: 85]
06477# R0101C00110-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06478# CONTINUOUS STANDBY 1.0 01:01:STRT 2.28 .046 No.Date 29:04 29.30 453 .000
06479# [Cm: 60.0 N: 3.00 T: 1.0]
06480# [IARc: 4.00 SMI: 23.09 SMAX:140.62 SK: 010]
06481# [InterEventTime: 12.00]
06482# R0101C00111-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06483# CONTINUOUS STANDBY 1.0 01:01:STRT 4.41 .523 No.Date 28:01 50.29 777 .000
06484# [XIMP: 68 TIMP: 85]
06485# [Horton parameters: Fw: 76.20 Fc: 13.20 DCAV:4.14 Pa: 0.0]
06486# [Previous area: IApex: 4.67 SLPD: .50 LIDP: .50 HNDP: 250 IBCP: .0]
06487# [Impervious area: IAImp: 1.57 SLPD: .50 LIDP: 1.57 HNDP: 193.0 MI: .013 IBCI: .0]
06488# [IARcImp: 4.00 IARcP: 4.00]
06489# R0101C00112-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06490# ROUTE RESERVOIR -> 1.0 02:01:STRT 4.41 .523 No.Date 28:01 50.29 n/a .000
06491# out <= 1.0 02:01:STRT 4.41 .523 No.Date 28:01 50.29 n/a .000
06492# overFlow <= 1.0 02:01:STRT 0.00 .000 No.Date 0:00 .00 n/a .000
06493# [MstOfsed:7930E-01 n3, TotOfVol:0.000E+00 n3, N-Ovrf: 0, TotDurOfV: 0 hrs]
06494# R0101C00113-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06495# CONTINUOUS STANDBY 1.0 01:01:STRT 45 .058 No.Date 28:00 38.69 598 .000
06496# [XIMP: 68 TIMP: 87]
06497# [Horton parameters: Fw: 76.20 Fc: 13.20 DCAV:4.14 Pa: 0.0]
06498# [Previous area: IApex: 4.67 SLPD: .50 LIDP: .50 HNDP: 250 IBCP: .0]
06499# [Impervious area: IAImp: 1.57 SLPD: .50 LIDP: 1.57 HNDP: 193.0 MI: .013 IBCI: .0]
06500# [IARcImp: 4.00 IARcP: 4.00]
06501# R0101C00114-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06502# ROUTE RESERVOIR -> 1.0 02:01:STRT 45 .058 No.Date 28:00 38.69 n/a .000
06503# out <= 1.0 02:01:STRT 45 .058 No.Date 28:00 38.69 n/a .000
06504# overFlow <= 1.0 02:01:STRT 0.00 .000 No.Date 0:00 .00 n/a .000
06505# [MstOfsed:1552E-02 n3, TotOfVol:0.000E+00 n3, N-Ovrf: 0, TotDurOfV: 0 hrs]
06506# R0101C00115-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06507# ADD HYD + 1.0 02:01:STRT 350.31 4.037 No.Date 29:17 20.48 n/a .000
06508# out <= 1.0 02:01:STRT 3.51 .518 No.Date 28:25 38.69 n/a .000
06509# + 1.0 02:01:STRT 2.50 .098 No.Date 28:24 50.29 n/a .000
06510# + 1.0 02:01:STRT 3.51 .518 No.Date 28:25 38.69 n/a .000
06511# + 1.0 02:01:STRT 59 .052 No.Date 28:05 38.69 n/a .000
06512# + 1.0 02:01:STRT 60.55 .852 No.Date 29:08 22.40 n/a .000
06513# SUM 350.31 4.037 No.Date 29:17 20.48 n/a .000
06514# R0101C00116-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06515# CONTINUOUS STANDBY 1.0 01:01:STRT 7.59 .759 No.Date 28:11 49.05 758 .000
06516# [XIMP: 64 TIMP: 85]
06517# [Horton parameters: Fw: 76.20 Fc: 13.20 DCAV:4.14 Pa: 0.0]
06518# [Previous area: IApex: 4.67 SLPD: .50 LIDP: .50 HNDP: 250 IBCP: .0]
06519# [Impervious area: IAImp: 1.57 SLPD: .50 LIDP: 1.57 HNDP: 193.0 MI: .013 IBCI: .0]
06520# [IARcImp: 4.00 IARcP: 4.00]
06521# R0101C00117-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06522# ROUTE RESERVOIR -> 1.0 02:01:STRT 7.59 .759 No.Date 28:11 49.05 n/a .000
06523# out <= 1.0 02:01:STRT 7.59 .759 No.Date 28:11 49.05 n/a .000
06524# overFlow <= 1.0 02:01:STRT 0.00 .000 No.Date 0:00 .00 n/a .000
06525# [MstOfsed:1594E-02 n3, TotOfVol:0.000E+00 n3, N-Ovrf: 0, TotDurOfV: 0 hrs]
06526# R0101C00118-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06527# ADD HYD + 1.0 02:01:STRT 356.68 4.181 No.Date 29:15 20.87 n/a .000
06528# out <= 1.0 02:01:STRT 3.51 .518 No.Date 28:25 38.69 n/a .000
06529# + 1.0 02:01:STRT 2.50 .098 No.Date 28:24 50.29 n/a .000
06530# + 1.0 02:01:STRT 3.51 .518 No.Date 28:25 38.69 n/a .000
06531# + 1.0 02:01:STRT 59 .052 No.Date 28:05 38.69 n/a .000
06532# + 1.0 02:01:STRT 60.55 .852 No.Date 29:08 22.40 n/a .000
06533# SUM 356.68 4.181 No.Date 29:15 20.87 n/a .000
06534# R0101C00119-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06535# SAVE HYD frame :SHAOUT:0010 364.27 4.242 No.Date 29:15 21.45 n/a .000
06536# remark:SHAOUT
06537# R0101C00120-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06538# CONTINUOUS STANDBY 1.0 01:01:STRT 66.75 6.470 No.Date 28:10 48.24 746 .000
06539# [XIMP: 68 TIMP: 80]
06540# [Horton parameters: Fw: 76.20 Fc: 13.20 DCAV:4.14 Pa: 0.0]
06541# [Previous area: IApex: 4.67 SLPD: .50 LIDP: .50 HNDP: 250 IBCP: .0]
06542# [Impervious area: IAImp: 1.57 SLPD: .50 LIDP: 1.57 HNDP: 193.0 MI: .013 IBCI: .0]
06543# [IARcImp: 4.00 IARcP: 4.00]
06544# R0101C00121-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS
06545# CONTINUOUS STANDBY 1.0 01:01:STRT 66.75 6.470 No.Date 28:10 48.24 n/a .000
06546# remark:SHAOUT
06547# R0101C00122-----DtmIn:ID:BNVY-----AREBA-QPEARCS-TpeakDate,hh:mm-----RvM-R-C-----DWFCMS







07855	Minor System	1.0	0.031-Corrig	15.87	1.818	28.09	48.38	n/a	.000
07856	[MjSysSto=0.000E+00, TotVolFv=0.000E+00, N-Dv=0.0, TotDurV=0.0 hrs]								
07857	[Impervious area: IAlp=1.571SDP+1.00LID= 40.1MD=250:SCP=0]								
07858	[IARClp= 4.00: IARClp= 4.00]								
07859	[SMin= 33.81: SMax=225.43: Sk= 0.010]								
07860	CONTINUOUS STANDBY	1.0	0.01A1-Corrig	15.75	1.640	28.02	40.97	63.3	.000
07861	[XMP= 42:TMP= 52]								
07862	[LDS= 2 Cn= 75.0]								
07863	[Previous area: IAlp= 4.671SDP+1.00LID= 40.1MD=250:SCP=0]								
07864	[Impervious area: IAlp= 1.571SDP+1.00LID= 324.1MI=0.13:SCI=0]								
07865	[IARClp= 4.00: IARClp= 4.00]								
07866	[SMin= 33.81: SMax=225.43: Sk= 0.010]								
07867	CONTINUOUS STANDBY	1.0	0.01A1-Corrig	15.75	1.640	28.02	40.97	63.3	.000
07868	[XMP= 42:TMP= 52]								
07869	[LDS= 2 Cn= 75.0]								
07870	[Previous area: IAlp= 4.671SDP+1.00LID= 40.1MD=250:SCP=0]								
07871	[Impervious area: IAlp= 1.571SDP+1.00LID= 324.1MI=0.13:SCI=0]								
07872	[IARClp= 4.00: IARClp= 4.00]								
07873	[SMin= 33.81: SMax=225.43: Sk= 0.010]								
07874	CONTINUOUS STANDBY	1.0	0.01A1-Corrig	15.75	1.640	28.02	40.97	n/a	.000
07875	[XMP= 42:TMP= 52]								
07876	[LDS= 2 Cn= 75.0]								
07877	[Previous area: IAlp= 4.671SDP+1.00LID= 40.1MD=250:SCP=0]								
07878	[Impervious area: IAlp= 1.571SDP+1.00LID= 324.1MI=0.13:SCI=0]								
07879	[IARClp= 4.00: IARClp= 4.00]								
07880	[SMin= 33.81: SMax=225.43: Sk= 0.010]								
07881	CONTINUOUS STANDBY	1.0	0.01A1-Corrig	15.75	1.640	28.02	40.97	n/a	.000
07882	[XMP= 42:TMP= 52]								
07883	[LDS= 2 Cn= 75.0]								
07884	[Previous area: IAlp= 4.671SDP+1.00LID= 40.1MD=250:SCP=0]								
07885	[Impervious area: IAlp= 1.571SDP+1.00LID= 253.1MI=0.13:SCI=0]								
07886	[IARClp= 4.00: IARClp= 4.00]								
07887	[SMin= 33.81: SMax=225.43: Sk= 0.010]								
07888	CONTINUOUS STANDBY	1.0	0.01A1-Corrig	15.75	1.640	28.02	40.97	n/a	.000
07889	[XMP= 42:TMP= 52]								
07890	[LDS= 2 Cn= 75.0]								
07891	[Previous area: IAlp= 4.671SDP+1.00LID= 40.1MD=250:SCP=0]								
07892	[Impervious area: IAlp= 1.571SDP+1.00LID= 324.1MI=0.13:SCI=0]								
07893	[IARClp= 4.00: IARClp= 4.00]								
07894	[SMin= 33.81: SMax=225.43: Sk= 0.010]								
07895	CONTINUOUS STANDBY	1.0	0.01A1-Corrig	15.75	1.640	28.02	40.97	n/a	.000
07896	[XMP= 42:TMP= 52]								
07897	[LDS= 2 Cn= 75.0]								
07898	[Previous area: IAlp= 4.671SDP+1.00LID= 40.1MD=250:SCP=0]								
07899	[Impervious area: IAlp= 1.571SDP+1.00LID= 324.1MI=0.13:SCI=0]								
07900	[IARClp= 4.00: IARClp= 4.00]								
07901	[SMin= 33.81: SMax=225.43: Sk= 0.010]								
07902	CONTINUOUS STANDBY	1.0	0.01A1-Corrig	15.75	1.640	28.02	40.97	n/a	.000
07903	[XMP= 42:TMP= 52]								
07904	[LDS= 2 Cn= 75.0]								
07905	[Previous area: IAlp= 4.671SDP+1.00LID= 40.1MD=250:SCP=0]								
07906	[Impervious area: IAlp= 1.571SDP+1.00LID= 324.1MI=0.13:SCI=0]								
07907	[IARClp= 4.00: IARClp= 4.00]								
07908	[SMin= 33.81: SMax=225.43: Sk= 0.010]								
07909	CONTINUOUS STANDBY	1.0	0.01A1-Corrig	15.75	1.640	28.02	40.97	n/a	.000
07910	[XMP= 42:TMP= 52]								
07911	[LDS= 2 Cn= 75.0]								
07912	[Previous area: IAlp= 4.671SDP+1.00LID= 40.1MD=250:SCP=0]								
07913	[Impervious area: IAlp= 1.571SDP+1.00LID= 324.1MI=0.13:SCI=0]								
07914	[IARClp= 4.00: IARClp= 4.00]								
07915	[SMin= 33.81: SMax=225.43: Sk= 0.010]								
07916	CONTINUOUS STANDBY	1.0	0.01A1-Corrig	15.75	1.640	28.02	40.97	n/a	.000
07917	[XMP= 42:TMP= 52]								
07918	[LDS= 2 Cn= 75.0]								
07919	[Previous area: IAlp= 4.671SDP+1.00LID= 40.1MD=250:SCP=0]								
07920	[Impervious area: IAlp= 1.571SDP+1.00LID= 324.1MI=0.13:SCI=0]								
07921	[IARClp= 4.00: IARClp= 4.00]								
07922	[SMin= 33.81: SMax=225.43: Sk= 0.010]								
07923	CONTINUOUS STANDBY	1.0	0.01A1-Corrig	15.75	1.640	28.02	40.97	n/a	.000
07924	[XMP= 42:TMP= 52]								
07925	[LDS= 2 Cn= 75.0]								
07926	[Previous area: IAlp= 4.671SDP+1.00LID= 40.1MD=250:SCP=0]								
07927	[Impervious area: IAlp= 1.571SDP+1.00LID= 324.1MI=0.13:SCI=0]								
07928	[IARClp= 4.00: IARClp= 4.00]								
07929	[SMin= 33.81: SMax=225.43: Sk= 0.010]								
07930	CONTINUOUS STANDBY	1.0	0.01A1-Corrig	15.75	1.640	28.02	40.97	n/a	.000
07931	[XMP= 42:TMP= 52]								
07932	[LDS= 2 Cn= 75.0]								
07933	[Previous area: IAlp= 4.671SDP+1.00LID= 40.1MD=250:SCP=0]								
07934	[Impervious area: IAlp= 1.571SDP+1.00LID= 324.1MI=0.13:SCI=0]								
07935	[IARClp= 4.00: IARClp= 4.00]								
07936	[SMin= 33.81: SMax=225.43: Sk= 0.010]								
07937	CONTINUOUS STANDBY	1.0	0.01A1-Corrig	15.75	1.640	28.02	40.97	n/a	.000
07938	[XMP= 42:TMP= 52]								
07939	[LDS= 2 Cn= 75.0]								
07940	[Previous area: IAlp= 4.671SDP+1.00LID= 40.1MD=250:SCP=0]								
07941	[Impervious area: IAlp= 1.571SDP+1.00LID= 324.1MI=0.13:SCI=0]								
07942	[IARClp= 4.00: IARClp= 4.00]								
07943	[SMin= 33.81: SMax=225.43: Sk= 0.010]								
07944	CONTINUOUS STANDBY	1.0	0.01A1-Corrig	15.75	1.640	28.02	40.97	n/a	.000
07945	[XMP= 42:TMP= 52]								
07946	[LDS= 2 Cn= 75.0]								
07947	[Previous area: IAlp= 4.671SDP+1.00LID= 40.1MD=250:SCP=0]								
07948	[Impervious area: IAlp= 1.571SDP+1.00LID= 324.1MI=0.13:SCI=0]								
07949	[IARClp= 4.00: IARClp= 4.00]								
07950	[SMin= 33.81: SMax=225.43: Sk= 0.010]								
07951	CONTINUOUS STANDBY	1.0	0.01A1-Corrig	15.75	1.640	28.02	40.97	n/a	.000
07952	[XMP= 42:TMP= 52]								
07953	[LDS= 2 Cn= 75.0]								
07954	[Previous area: IAlp= 4.671SDP+1.00LID= 40.1MD=250:SCP=0]								
07955	[Impervious area: IAlp= 1.571SDP+1.00LID= 324.1MI=0.13:SCI=0]								
07956	[IARClp= 4.00: IARClp= 4.00]								
07957	[SMin= 33.81: SMax=225.43: Sk= 0.010]								
07958	CONTINUOUS STANDBY	1.0	0.01A1-Corrig	15.75	1.640	28.02	40.97	n/a	.000
07959	[XMP= 42:TMP= 52]								
07960	[LDS= 2 Cn= 75.0]								
07961	[Previous area: IAlp= 4.671SDP+1.00LID= 40.1MD=250:SCP=0]								
07962	[Impervious area: IAlp= 1.571SDP+1.00LID= 324.1MI=0.13:SCI=0]								
07963	[IARClp= 4.00: IARClp= 4.00]								
07964	[SMin= 33.81: SMax=225.43: Sk= 0.010]								
07965	CONTINUOUS STANDBY	1.0	0.01A1-Corrig	15.75	1.640	28.02	40.97	n/a	.000
07966	[XMP= 42:TMP= 52]								
07967	[LDS= 2 Cn= 75.0]								
07968	[Previous area: IAlp= 4.671SDP+1.00LID= 40.1MD=250:SCP=0]								
07969	[Impervious area: IAlp= 1.571SDP+1.00LID= 324.1MI=0.13:SCI=0]								
07970	[IARClp= 4.00: IARClp= 4.00]								
07971	[SMin= 33.81: SMax=225.43: Sk= 0.010]								
07972	CONTINUOUS STANDBY	1.0	0.01A1-Corrig	15.75	1.640	28.02	40.97	n/a	.000
07973	[XMP= 42:TMP= 52]								
07974	[LDS= 2 Cn= 75.0]								
07975	[Previous area: IAlp= 4.671SDP+1.00LID= 40.1MD=250:SCP=0]								
07976	[Impervious area: IAlp= 1.571SDP+1.00LID= 324.1MI=0.13:SCI=0]								
07977	[IARClp= 4.00: IARClp= 4.00]								
07978	[SMin= 33.81: SMax=225.43: Sk= 0.010]								
07979	CONTINUOUS STANDBY	1.0	0.01A1-Corrig	15.75	1.640	28.02	40.97	n/a	.000
07980	[XMP= 42:TMP= 52]								
07981	[LDS= 2 Cn= 75.0]								
07982	[Previous area: IAlp= 4.671SDP+1.00LID= 40.1MD=250:SCP=0]								
07983	[Impervious area: IAlp= 1.571SDP+1.00LID= 324.1MI=0.13:SCI=0]								
07984	[IARClp= 4.00: IARClp= 4.00]								
07985	[SMin= 33.81: SMax=225.43: Sk= 0.010]								
07986	CONTINUOUS STANDBY	1.0	0.01A1-Corrig	15.75	1.640	28.02	40.		



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08603# [Cm 66.0: N# 3.00: Tp=1.24]
08604# [IAREK 4.00: SMIN: 52.62: SMAK=350.79: EK= .010]
08605# [InterVntTime= 12.00]
08606#
08607# The Tp was modified according to a Peak Reduction Factor (MTO-Chart B2-4)
08608#
08609# ROUTES/CO011-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08610# CONTINUOUS NASHVD 1.0 01:SR_CK 1917.00 10.351 No.Date 34:27 27.01 363 .000
08611# [Cm 66.0: N# 3.00: Tp=1.29]
08612# [IAREK 4.00: SMIN: 52.62: SMAK=350.79: EK= .010]
08613# [InterVntTime= 12.00]
08614#
08615# The Tp was modified according to a Peak Reduction Factor (MTO-Chart B2-4)
08616# # of 1.52
08617# ROUTES/CO012-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08618# CONTINUOUS NASHVD 1.0 01:SR_CK 5666.00 27.457 No.Date 37:54 31.50 423 .000
08619# [Cm 72.0: N# 3.00: Tp= 8.00]
08620# [IAREK 4.00: SMIN: 39.75: SMAK=264.99: EK= .010]
08621# [InterVntTime= 12.00]
08622#
08623# The Tp was modified according to a Peak Reduction Factor (MTO-Chart B2-4)
08624# # of 1.75
08625# ROUTES/CO013-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08626# CONTINUOUS NASHVD 1.0 01:SR_CK 8976.00 26.276 No.Date 39:59 27.01 363 .000
08627# [Cm 66.0: N# 3.00: Tp=11.66]
08628# [IAREK 4.00: SMIN: 52.62: SMAK=350.79: EK= .010]
08629# [InterVntTime= 12.00]
08630#
08631# The Tp was modified according to a Peak Reduction Factor (MTO-Chart B2-4)
08632# # of 1.68
08633# ROUTES/CO014-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08634# CONTINUOUS NASHVD 1.0 01:SR_S 1132.00 11.752 No.Date 30:54 30.18 406 .000
08635# [Cm 72.0: N# 3.00: Tp= 2.51]
08636# [IAREK 4.00: SMIN: 41.07: SMAK=287.10: EK= .010]
08637# [InterVntTime= 12.00]
08638#
08639# The Tp was modified according to a Peak Reduction Factor (MTO-Chart B2-4)
08640# # of 1.82
08641# ROUTES/CO015-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08642# CONTINUOUS NASHVD 1.0 01:SR_S 3197.00 11.663 No.Date 36:24 21.75 292 .000
08643# [Cm 62.0: N# 3.00: Tp=11.32]
08644# [IAREK 4.00: SMIN: 52.62: SMAK=350.79: EK= .010]
08645# [InterVntTime= 12.00]
08646#
08647# The Tp was modified according to a Peak Reduction Factor (MTO-Chart B2-4)
08648# # of 1.80
08649# ROUTES/CO016-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08650# CONTINUOUS NASHVD 1.0 01:SR_S 131.00 2.266 No.Date 28:57 25.20 139 .000
08651# [Cm 61.0: N# 3.00: Tp= .90]
08652# [IAREK 4.00: SMIN: 52.62: SMAK=350.79: EK= .010]
08653# [InterVntTime= 12.00]
08654#
08655# The Tp was modified according to a Peak Reduction Factor (MTO-Chart B2-4)
08656# # of 1.83
08657# ROUTES/CO017-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08658# CONTINUOUS NASHVD 1.0 01:SR_DR 3854.00 15.333 No.Date 38:34 27.01 363 .000
08659# [Cm 66.0: N# 3.00: Tp= 1.81]
08660# [IAREK 4.00: SMIN: 52.62: SMAK=350.79: EK= .010]
08661# [InterVntTime= 12.00]
08662#
08663# The Tp was modified according to a Peak Reduction Factor (MTO-Chart B2-4)
08664# # of 1.81
08665# ROUTES/CO018-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08666# CONTINUOUS NASHVD 1.0 01:VY_DR 1322.00 7.892 No.Date 35:14 31.50 423 .000
08667# [Cm 72.0: N# 3.00: Tp= 8.98]
08668# [IAREK 4.00: SMIN: 39.75: SMAK=264.99: EK= .010]
08669# [InterVntTime= 12.00]
08670#
08671# The Tp was modified according to a Peak Reduction Factor (MTO-Chart B2-4)
08672# # of 1.79
08673# ROUTES/CO019-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08674# CONTINUOUS NASHVD 1.0 01:SR_S 165.00 1.076 No.Date 33:03 27.63 371 .000
08675# [Cm 66.0: N# 3.00: Tp= 1.81]
08676# [IAREK 4.00: SMIN: 50.55: SMAK=336.97: EK= .010]
08677# [InterVntTime= 12.00]
08678#
08679# The Tp was modified according to a Peak Reduction Factor (MTO-Chart B2-4)
08680# # of 1.51
08681# ROUTES/CO020-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08682# CONTINUOUS NASHVD 1.0 01:VY_DR 1322.00 7.892 No.Date 35:14 31.50 423 .000
08683# [Cm 72.0: N# 3.00: Tp= 8.98]
08684# [IAREK 4.00: SMIN: 39.75: SMAK=264.99: EK= .010]
08685# [InterVntTime= 12.00]
08686#
08687# ROUTES/CO021-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08688# CONTINUOUS NASHVD 1.0 01:SR_S 224.00 6.892 No.Date 28:45 35.66 479 .000
08689# [Cm 77.0: N# 3.00: Tp= .75]
08690# [IAREK 4.00: SMIN: 31.58: SMAK=207.66: EK= .010]
08691# [InterVntTime= 12.00]
08692#
08693# The Tp was modified according to a Peak Reduction Factor (MTO-Chart B2-4)
08694# # of 1.50
08695# ROUTES/CO022-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08696# CONTINUOUS NASHVD 1.0 01:SR_CK 4945.00 37.664 No.Date 33:18 32.85 442 .000
08697# [Cm 74.0: N# 3.00: Tp= 4.45]
08698# [IAREK 4.00: SMIN: 56.67: SMAK=344.49: EK= .010]
08699# [InterVntTime= 12.00]
08700#
08701# ROUTES/CO023-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08702# CONTINUOUS NASHVD 1.0 01:SR_S 20.00 .798 No.Date 28:35 39.36 529 .000
08703# [Cm 57.0: N# 3.00: Tp= .62]
08704# [IAREK 4.00: SMIN: 25.21: SMAK=168.09: EK= .010]
08705# [InterVntTime= 12.00]
08706#
08707# The Tp was modified according to a Peak Reduction Factor (MTO-Chart B2-4)
08708# # of 1.61
08709# ROUTES/CO024-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08710# CONTINUOUS NASHVD 1.0 01:SR_SAI 1412.00 7.480 No.Date 37:50 34.24 460 .000
08711# [Cm 72.0: N# 3.00: Tp= 8.98]
08712# [IAREK 4.00: SMIN: 31.81: SMAK=225.43: EK= .010]
08713# [InterVntTime= 12.00]
08714#
08715# ROUTES/CO025-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08716# CONTINUOUS NASHVD 1.0 01:SR_S 585.00 10.942 No.Date 29:56 39.36 529 .000
08717# [Cm 81.0: N# 3.00: Tp= 1.00]
08718# [IAREK 4.00: SMIN: 25.21: SMAK=168.09: EK= .010]
08719# [InterVntTime= 12.00]
08720#
08721# ROUTES/CO026-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08722# CONTINUOUS NASHVD 1.0 01:SR_CK 1022.00 14.476 No.Date 30:46 38.00 519 .000
08723# [Cm 80.0: N# 3.00: Tp= 2.46]
08724# [IAREK 4.00: SMIN: 26.32: SMAK=175.50: EK= .010]
08725# [InterVntTime= 12.00]
08726#
08727# ROUTES/CO027-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08728# CONTINUOUS NASHVD 1.0 01:SR_CK 1122.00 13.229 No.Date 31:48 39.36 529 .000
08729# [Cm 81.0: N# 3.00: Tp= 1.25]
08730# [IAREK 4.00: SMIN: 35.83: SMAK=216.39: EK= .010]
08731# [InterVntTime= 12.00]
08732#
08733# ROUTES/CO028-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08734# CONTINUOUS NASHVD 1.0 01:SR_DR 2737.00 49.508 No.Date 31:30 34.94 470 .000
08735# [Cm 76.0: N# 3.00: Tp= 3.03]
08736# [IAREK 4.00: SMIN: 52.62: SMAK=350.79: EK= .010]
08737# [InterVntTime= 12.00]
08738#
08739# Routing hydrographs
08740# # Starting with the addition of Jock River Headwater and Subwatershed 13
08741#
08742# ROUTES/CO030-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08743# ADD HYD + 1.0 02:SR_SW 3680.00 16.500 No.Date 36:56 25.40 n/a .000
08744# + 1.0 02:SR_NH 971.00 5.778 No.Date 32:34 24.02 n/a .000
08745# SUM= 1.0 01:SR_N13 4651.00 19.777 No.Date 35:26 25.40 n/a .000
08746#
08747# Sum of hydrographs from Node 13 routed to Node 13A
08748# [Approximated cross-section - see cross-section 288]
08749# Use n=0.04 for summer conditions and n=0.025 for spring conditions
08750#
08751# ROUTES/CO031-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08752# ROUTE CHANNEL -> 1.0 02:SR_N13 4651.00 19.777 No.Date 35:26 25.42 n/a .000
08753# [R/S= 2074. / .025 / 0.0131A] 4651.00 15.935 No.Date 39:17 25.42 n/a .000
08754# [Vmax= .548/Dmax= 3.659]
08755#
08756# Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
08757#
08758# ROUTES/CO032-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08759# ADD HYD + 1.0 02:SR_N13 4651.00 15.935 No.Date 39:17 25.42 n/a .000
08760# + 1.0 01:SR_DR 7725.00 7.522 No.Date 39:59 20.65 n/a .000
08761# SUM= 1.0 01:SR_N13A 7725.00 23.402 No.Date 39:59 23.52 n/a .000
08762#
08763# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
08764#
08765# ROUTES/CO033-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08766# ROUTE RESERVOIR -> 1.0 02:SR_N13 7725.00 23.402 No.Date 39:59 23.52 n/a .000
08767# [Mstot=1192E+03 n] 7725.00 3.678 No.Date 60:27 23.52 n/a .000
08768#
08769# ROUTES/CO034-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08770# SAVE HYD + 1.0 01:RES_GM 7725.00 3.678 No.Date 60:27 23.52 n/a .000
08771# [Frame_H:RESUM]
08772# remark:Outflow from Res GM
08773# # Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
08774# [Approximated cross-section - see cross-section 259]
08775# Use n=0.04 for summer conditions and n=0.025 for spring conditions
08776#
08777# ROUTES/CO035-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08778# ROUTE CHANNEL -> 1.0 02:RES_GM 7725.00 3.678 No.Date 60:27 23.52 n/a .000
08779# [R/S= 1.1] out-> 1.0 01:SR_N12 7725.00 3.678 No.Date 63:05 23.52 n/a .000
08780# [L/S= 5926. / .076 / .040]
08781# [Vmax= .552/Dmax= 1.524]
08782#
08783# Addition of Subwatershed Jock River at Ashton to Node 12
08784#
08785# ROUTES/CO036-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08786# ADD HYD + 1.0 02:SR_SW 1781.00 14.166 No.Date 32:40 31.50 n/a .000
08787# + 1.0 01:SR_N12 9506.00 16.182 No.Date 32:43 25.02 n/a .000
08788# SUM= 1.0 01:SR_N12 9506.00 16.182 No.Date 32:43 25.02 n/a .000
08789#
08790# ROUTES/CO037-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08791# SAVE HYD + 1.0 01:SR_N12 9506.00 16.182 No.Date 32:43 25.02 n/a .000
08792# [Frame_H:RESUM]
08793# remark:flow at S_M12 near Ashton
08794#
08795# Sum of hydrographs from Node 12 routed to Node 12
08796# [Approximated cross-section - see cross-section 188]
08797# Use n=0.04 for summer conditions and n=0.025 for spring conditions
08798#
08799# ROUTES/CO038-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08800# ROUTE CHANNEL -> 1.0 02:SR_N12 9506.00 16.182 No.Date 32:43 25.02 n/a .000
08801# [R/S= 972. / .054 / .040]
08802# [Vmax= .721/Dmax= 2.847]
08803#
08804# Addition of Subwatershed 11 and Mo Name Creek to Node 11
08805#
08806# ROUTES/CO039-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08807# ADD HYD + 1.0 02:SR_N11 806.00 16.007 No.Date 33:02 27.02 n/a .000
08808# + 1.0 02:SR_N11 500.00 7.521 No.Date 29:22 27.01 n/a .000
08809# SUM= 1.0 01:SR_N11 1192.00 27.908 No.Date 33:04 25.42 n/a .000
08810#
08811# Sum of hydrographs from Node 11 routed to Node 10
08812#
08813# ROUTES/CO040-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08814# ROUTE CHANNEL -> 1.0 02:SR_N10 1192.00 27.908 No.Date 33:04 25.42 n/a .000
08815# [R/S= 1.00] out-> 1.0 01:SR_N10 1192.00 18.039 No.Date 40:01 25.42 n/a .000
08816# [L/S= 14028. / .197 / .040]
08817# [Vmax= .454/Dmax= 1.329]
08818#
08819# Addition of Subwatershed 10 to Node 10
08820#
08821# ROUTES/CO041-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08822# ADD HYD + 1.0 02:SR_N10 1192.00 27.908 No.Date 33:04 25.42 n/a .000
08823# + 1.0 02:SR_N10 8666.00 27.457 No.Date 37:54 31.50 n/a .000
08824# SUM= 1.0 01:SR_N10 9858.00 45.026 No.Date 38:35 27.98 n/a .000
08825#
08826# Sum of hydrographs from Node 10 routed to Node 9
08827#
08828# ROUTES/CO042-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08829# ADD HYD + 1.0 02:SR_N10 9858.00 45.026 No.Date 38:35 27.98 n/a .000
08830# + 1.0 02:SR_N10 1789.00 17.899 No.Date 38:35 27.98 n/a .000
08831# SUM= 1.0 01:SR_N10A 2966.00 26.276 No.Date 39:59 27.01 n/a .000
08832#
08833# Sum of hydrographs from Node 10 routed to Node 9
08834# Section 2
08835#
08836# ROUTES/CO043-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08837# ADD HYD + 1.0 02:SR_N10 1789.00 17.899 No.Date 38:35 27.98 n/a .000
08838# + 1.0 02:SR_N10 8375.00 26.276 No.Date 39:59 27.01 n/a .000
08839# SUM= 1.0 01:SR_N10A 2966.00 70.812 No.Date 39:59 27.01 n/a .000
08840#
08841# Sum of hydrographs from Node 10 routed to Node 9
08842# Section 2
08843#
08844# ROUTES/CO044-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08845# ROUTE CHANNEL -> 1.0 02:SR_N10A 2966.00 70.812 No.Date 39:59 27.01 n/a .000
08846# [R/S= 1.00] out-> 1.0 01:SR_N10 2966.00 69.032 No.Date 39:59 27.01 n/a .000
08847# [L/S= 3982. / .075 / .040]
08848# [Vmax= .454/Dmax= 1.329]
08849#
08850# Addition of Subwatershed 9 and Nicholn Creek to Node 9
08851#
08852# ROUTES/CO045-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08853# ADD HYD + 1.0 02:SR_N9 1332.00 11.752 No.Date 30:54 30.18 n/a .000
08854# + 1.0 02:SR_N9 4464.00 13.075 No.Date 39:59 24.62 n/a .000
08855# SUM= 1.0 01:SR_N9 5796.00 34.684 No.Date 39:59 26.99 n/a .000
08856#
08857# Sum of hydrographs from Node 9 routed to Node 8
08858#
08859# ROUTES/CO046-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08860# ADD HYD + 1.0 02:SR_N9 5796.00 34.684 No.Date 39:59 26.99 n/a .000
08861# + 1.0 01:SR_N9 31561.00 79.245 No.Date 39:59 26.99 n/a .000
08862# SUM= 1.0 01:SR_N9 37357.00 114.369 No.Date 39:59 26.99 n/a .000
08863#
08864# Addition of Subwatershed 8 and Hobb's Drain to Node 8
08865#
08866# ROUTES/CO047-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08867# ADD HYD + 1.0 02:SR_N8 31561.00 79.245 No.Date 39:59 26.99 n/a .000
08868# + 1.0 02:SR_N8 133.00 2.266 No.Date 28:57 25.20 n/a .000
08869# SUM= 1.0 01:SR_N8 31694.00 81.511 No.Date 39:59 26.99 n/a .000
08870#
08871# Sum of hydrographs from Node 8 routed to Node 7
08872#
08873# ROUTES/CO048-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08874# ROUTE CHANNEL -> 1.0 02:SR_N8 31694.00 81.511 No.Date 39:59 26.99 n/a .000
08875# [R/S= 1.00] out-> 1.0 01:SR_N8 31694.00 81.511 No.Date 39:59 26.99 n/a .000
08876# [L/S= 1752. / .053 / .070]
08877# [Vmax= .226/Dmax= 2.161]
08878#
08879# Addition of Subwatershed 7 to Node 7
08880#
08881# ROUTES/CO049-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08882# ADD HYD + 1.0 02:SR_N7 35846.00 84.997 No.Date 39:59 26.99 n/a .000
08883# + 1.0 02:SR_N7 3584.00 80.337 No.Date 45:08 26.98 n/a .000
08884# SUM= 1.0 01:SR_N7 39430.00 165.334 No.Date 39:59 26.99 n/a .000
08885#
08886# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
08887#
08888# ROUTES/CO050-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08889# ADD HYD + 1.0 02:SR_N6 39430.00 165.334 No.Date 39:59 26.99 n/a .000
08890# + 1.0 02:SR_N6 38743.00 11.865 No.Date 36:24 21.95 n/a .000
08891# SUM= 1.0 01:SR_N6 78173.00 177.199 No.Date 39:59 26.99 n/a .000
08892#
08893# Sum of hydrographs from Node 7 routed to Node 6
08894# Section 5
08895#
08896# ROUTES/CO051-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08897# ROUTE CHANNEL -> 1.0 02:SR_N6 78173.00 177.199 No.Date 39:59 26.99 n/a .000
08898# [R/S= 1.00] out-> 1.0 01:SR_N6 78173.00 177.199 No.Date 39:59 26.99 n/a .000
08899# [L/S= 1056. / .082 / .028]
08900# [Vmax= .916/Dmax= 1.120]
08901#
08902# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
08903#
08904# ROUTES/CO052-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08905# ADD HYD + 1.0 02:SR_N6 78173.00 177.199 No.Date 39:59 26.99 n/a .000
08906# + 1.0 02:SR_N6 38743.00 42.032 No.Date 60:05 26.55 n/a .000
08907# SUM= 1.0 01:SR_N6 81916.00 219.231 No.Date 39:59 26.55 n/a .000
08908#
08909# Insertion of a reservoir to simulate the effects of the Richmond Fen.
08910#
08911# ROUTES/CO053-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08912# ROUTE RESERVOIR -> 1.0 02:SR_N6 38743.00 42.032 No.Date 60:05 26.55 n/a .000
08913# [Mstot=367E+03 n]
08914#
08915# Release of rain from fen was assumed to be controlled by the downstream
08916# river cross-section for summer conditions. It is assumed that for up to
08917# 0.75 m of water above the rim provided the storage. Above
08918# this depth, the wetland starts to significantly store water.
08919#
08920# ROUTES/CO054-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08921# ROUTE CHANNEL -> 1.0 02:SR_N6 38743.00 42.032 No.Date 60:05 26.55 n/a .000
08922# [R/S= 1.00] out-> 1.0 01:SR_N6 38743.00 42.032 No.Date 60:05 26.55 n/a .000
08923# [L/S= 1056. / .082 / .028]
08924# [Vmax= .916/Dmax= 1.120]
08925#
08926# Sum of hydrographs from Node 6 routed to Node 5
08927# Section 6
08928#
08929# ROUTES/CO055-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08930# ADD HYD + 1.0 02:SR_N5 42042.01 41.832 No.Date 61:20 26.72 n/a .000
08931# + 1.0 02:SR_N5 165.00 1.076 No.Date 33:03 27.63 n/a .000
08932# SUM= 1.0 01:SR_N5 42207.01 42.908 No.Date 61:20 26.72 n/a .000
08933#
08934# Sum of hydrographs from Node 6 routed to Node 5
08935# Section 6
08936#
08937# ROUTES/CO056-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08938# ADD HYD + 1.0 02:SR_N5 42207.01 42.908 No.Date 61:20 26.72 n/a .000
08939# + 1.0 02:SR_N5 224.00 6.892 No.Date 28:45 35.66 n/a .000
08940# SUM= 1.0 01:SR_N5 42431.01 49.800 No.Date 61:20 27.43 n/a .000
08941#
08942# Sum of hydrographs from Node 5 routed to Node 5A
08943# Section 7
08944#
08945# ROUTES/CO057-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08946# ADD HYD + 1.0 02:SR_N5A 42431.01 49.800 No.Date 61:20 27.43 n/a .000
08947# + 1.0 01:SR_N5A 45409.01 62.684 No.Date 34:43 27.43 n/a .000
08948# SUM= 1.0 01:SR_N5A 87840.01 112.484 No.Date 34:43 27.43 n/a .000
08949#
08950# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
08951#
08952# ROUTES/CO058-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08953# ROUTE RESERVOIR -> 1.0 02:SR_N5A 87840.01 112.484 No.Date 34:43 27.43 n/a .000
08954# [Mstot=1192E+03 n] 87840.01 3.678 No.Date 60:27 23.52 n/a .000
08955#
08956# Addition of Subwatershed 5A and Subwatershed 5A2 to Node 5A
08957#
08958# ROUTES/CO059-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08959# ADD HYD + 1.0 02:SR_N5A 87840.01 112.484 No.Date 34:43 27.43 n/a .000
08960# + 1.0 02:SR_N5A 45409.01 62.684 No.Date 34:43 27.43 n/a .000
08961# SUM= 1.0 01:SR_N5A 133249.01 175.168 No.Date 34:43 27.43 n/a .000
08962#
08963# Sum of hydrographs from Node 5A routed to Node 4
08964# Section 8
08965#
08966# ROUTES/CO060-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08967# ROUTE CHANNEL -> 1.0 02:SR_N5A 133249.01 175.168 No.Date 34:43 27.43 n/a .000
08968# [R/S= 1.00] out-> 1.0 01:SR_N5A 133249.01 175.168 No.Date 34:43 27.43 n/a .000
08969# [L/S= 565. / .080 / .030]
08970# [Vmax= .840/Dmax= 3.530]
08971#
08972# Addition of Subwatershed 4 and Leamy Creek to Node 4
08973#
08974# ROUTES/CO061-----DTrain-ID:HYD-----AREHA-OPEAKs-TPeakDate_hh:mm-----RVM-R.C-----DWFCms
08975# ADD HYD + 1.0 02:SR_N4 46841.01 66.496 No.Date 36:27 27.64 n/a .000
08976# + 1.0 02:SR_N4 5812.00 10.942 No.Date 31:04 27.64 n/a .000
08977# SUM= 1.0 01:SR_N4 52653.01 77.438 No.Date 36:27 27.64 n/a .000

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08977# R025<C00061-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
08978# SAVE HYD                               48447.00 79.819_MoDate 35:41 28:02 n/a .000
08979# fname 'S_44.0025
08980# remark:flow at S_N
08981#
08982# Sum of hydrographs from Node 4 routed to Node 2
08983# Section 3
08984#
08985# R025<C00062-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
08986# ROUTE CHANNEL -> 1.0 02:18:34 48447.00 79.819_MoDate 35:41 28:02 n/a .000
08987# [RPT: 1.00] out<= 1.0 02:18:34 48447.00 79.819_MoDate 35:41 28:02 n/a .000
08988# [L/S= 167.1 / 067.040]
08989# [Vmax = .874IDmax= 3.970]
08990#
08991# Addition of Subwatershed 3 with Monohm Drain and Smith Drain to Node 2
08992#
08993# R025<C00063-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
08994# ADD HYD + 1.0 02:18:34 48447.00 79.819_MoDate 35:41 28:02 n/a .000
08995# [RPT: 1.00] out<= 1.0 02:18:34 48447.00 79.819_MoDate 35:41 28:02 n/a .000
08996# [L/S= 1.00] out<= 1.0 02:18:34 48447.00 79.819_MoDate 35:41 28:02 n/a .000
08997# [Vmax = 1.00] out<= 1.0 02:18:34 48447.00 79.819_MoDate 35:41 28:02 n/a .000
08998# SUM= 1.0 02:18:34 52483.00 106.109_MoDate 33:07 28:44 n/a .000
08999#
09000# SAVE HYD                               52483.00 106.109_MoDate 33:07 28:44 n/a .000
09001# fname 'H_S2M
09002# remark:flow at S_NJ Jack River Gauge at Moodle Dr.
09003#
09004# Sum of hydrographs from Node 2 routed to Node 1
09005# Section 10
09006#
09007#
09008#
09009# Hydrograph from Node 2 routed to Node 416
09010# Channel X-Section obtained from RWCA Hydraulic Model - Station 9025
09011#
09012# R025<C00065-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09013# ROUTE CHANNEL -> 1.0 02:18:34 52483.00 106.109_MoDate 33:07 28:44 n/a .000
09014# [RPT: 1.00] out<= 1.0 02:18:34 52483.00 106.109_MoDate 33:07 28:44 n/a .000
09015# [L/S= 2327. / 050. / 055]
09016# [Vmax = 1.00] out<= 1.0 02:18:34 52483.00 106.109_MoDate 33:07 28:44 n/a .000
09017#
09018# Catchment SM-1
09019# Portion of RWCA catchment SM_1 outside of Reach 3 subwatershed
09020# Undeveloped agricultural land
09021#
09022# R025<C00066-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09023# CONTINUOUS STANDBY 1.0 01:18:41 53642.42 5.154_MoDate 31:16 30:33 .405 .000
09024# [CM= 72.01 N= 3.00] Tp = 2.79
09025# [IAREC= 4.00] SMIN= 39.75; SMAX=264.99; SK = .010]
09026# [InterEventTime= 12.00]
09027# [XIMP= 65.7TMP= 85]
09028# [LOGS= 2 CM= 61.0]
09029# [Previous area: IAREC= 4.67;SLP= 2.00;IDP= 4.00; IAREP= 50.0; IAREC= 0]
09030# [Impervious area: IAREP= 1.57;SLP= 1.75;IDP= 1.547; IAREP= 250; IAREC= 0]
09031# [IAREC= 4.00] IAREP= 4.00]
09032# [SMIN= 33.81; SMAX=225.43; SK = .010]
09033#
09034# R025<C00067-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09035# COMPETE DUALHYD 1.0 01:18:41 44.93 6.507_MoDate 28:03 57.38 n/a .000
09036# Major System + 1.0 01:18:41 44.93 6.507_MoDate 28:03 57.38 n/a .000
09037# Minor System + 1.0 01:18:41 44.93 6.507_MoDate 28:03 57.38 n/a .000
09038# [MjSysStor= .1037E+04, TotVol= 0.000E+00, N-Orv= 0, TotDurV= 0 hrs]
09039#
09040# ADD HYD + 1.0 02:18:1-OKM 44.93 6.507_MoDate 28:03 57.38 n/a .000
09041# [L/S= 1.00] out<= 1.0 02:18:1-OKM 44.93 6.507_MoDate 28:03 57.38 n/a .000
09042# SUM= 1.0 01:18:1-OKM 44.93 6.507_MoDate 28:03 57.38 n/a .000
09043#
09044# R025<C00070-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09045# ROUTE RESERVOIR -> 1.0 02:18:1-OKM 44.93 6.507_MoDate 28:03 57.38 n/a .000
09046# out<= 1.0 01:18:1-OKM 44.93 6.507_MoDate 28:03 57.38 n/a .000
09047# overVol= 0.00 0.00 MoDate 28:03 57.38 n/a .000
09048# [MjStor= .1559E+01 m3, TotVol= 0.000E+00 m3, N-Orv= 0, TotDurV= 0 hrs]
09049#
09050# ADD HYD + 1.0 02:18:41 52483.00 106.109_MoDate 33:07 28:44 n/a .000
09051# [L/S= 1.00] out<= 1.0 02:18:41 52483.00 106.109_MoDate 33:07 28:44 n/a .000
09052# SUM= 1.0 01:18:1-OKM 44.93 6.507_MoDate 28:03 57.38 n/a .000
09053#
09054# R025<C00071-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09055# CONTINUOUS STANDBY 1.0 01:18:41 53642.42 5.154_MoDate 31:16 30:33 .405 .000
09056# [IAREC= 4.00] SMIN= 39.75; SMAX=264.99; SK = .010]
09057# [InterEventTime= 12.00]
09058# fname 'SN_416.0025
09059# remark:Total Flows at Highway 416 before Station 7245
09060#
09061# Hydrograph from Node 416 routed to Node at Okeefe drain
09062# Channel X-Section obtained from RWCA Hydraulic Model - Station 7245
09063#
09064# R025<C00073-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09065# ROUTE CHANNEL -> 1.0 02:18:41 53642.42 5.154_MoDate 31:16 30:33 .405 .000
09066# [RPT: 1.00] out<= 1.0 02:18:41 53642.42 5.154_MoDate 31:16 30:33 .405 .000
09067# [L/S= 1.00] out<= 1.0 02:18:41 53642.42 5.154_MoDate 31:16 30:33 .405 .000
09068# [Vmax = 1.569IDmax= 2.814]
09069#
09070# Catchment OKEEFE
09071# - To O'Keefe drain (north of the Jack)
09072#
09073# Develop with area 519.02 HA
09074# - 2020-12-01 add Okeefe model (Area 519.02 HA) instead of current Okeefe (Area 513.02 HA)
09075# - 2020-12-01 add Okeefe model (Area 519.02 HA) instead of current Okeefe (Area 513.02 HA)
09076# - 2020-12-01 add Okeefe model (Area 519.02 HA) instead of current Okeefe (Area 513.02 HA)
09077#
09078# R025<C00074-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09079# CONTINUOUS STANDBY 1.0 01:18:41 53642.42 5.154_MoDate 31:16 30:33 .405 .000
09080# [CM= 61.0 N= 3.00] Tp = .90]
09081# [IAREC= 4.00] SMIN= 43.00; SMAX=430.01; SK = .010]
09082# [InterEventTime= 12.00]
09083#
09084# R025<C00075-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09085# ROUTE CHANNEL -> 1.0 02:18:41 63.72 8.777_MoDate 28:58 22.21 n/a .000
09086# [RPT: 1.00] out<= 1.0 02:18:41 63.72 8.777_MoDate 28:58 22.21 n/a .000
09087# [L/S= 1.00] out<= 1.0 02:18:41 63.72 8.777_MoDate 28:58 22.21 n/a .000
09088# [Vmax = .829IDmax= .198]
09089#
09090# CONTINUOUS STANDBY 1.0 01:18:41 28.61 3.330_MoDate 29:13 20.55 .276 .000
09091# [CM= 37.0 N= 1.00] Tp = 1.00]
09092# [IAREC= 4.00] SMIN= 75.32; SMAX=508.81; SK = .010]
09093# [InterEventTime= 12.00]
09094#
09095# R025<C00076-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09096# CONTINUOUS STANDBY 1.0 01:18:41 46.94 4.426_MoDate 29:00 15.62 .210 .000
09097# [CM= 40.0 N= 3.00] Tp = .90]
09098# [IAREC= 4.00] SMIN= 104.59; SMAX=697.25; SK = .010]
09099# [InterEventTime= 12.00]
09100#
09101# R025<C00078-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09102# ADD HYD + 1.0 02:18:41 63.72 8.777_MoDate 29:11 19.65 n/a .000
09103# [RPT: 1.00] out<= 1.0 02:18:41 63.72 8.777_MoDate 29:11 19.65 n/a .000
09104# [L/S= 1.00] out<= 1.0 02:18:41 63.72 8.777_MoDate 29:11 19.65 n/a .000
09105# SUM= 1.0 01:18:41 46.94 4.426_MoDate 29:00 15.62 .210 .000
09106#
09107# R025<C00079-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09108# CONTINUOUS STANDBY 1.0 01:18:41 16.46 1.143_MoDate 28:45 13.49 .181 .000
09109# [CM= 43.0 N= 3.00] Tp = .70]
09110# [IAREC= 4.00] SMIN= 134.47; SMAX=896.47; SK = .010]
09111# [InterEventTime= 12.00]
09112#
09113# R025<C00081-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09114# CONTINUOUS STANDBY 1.0 01:18:41 39.67 1.013_MoDate 28:23 24.45 .329 .000
09115# [XIMP= 15.7TMP= 30]
09116# [LOGS= 2 CM= 61.0]
09117# [Previous area: IAREC= 4.67;SLP= 3.31;IDP= 440; IAREP= 0; IAREC= 0]
09118# [Impervious area: IAREP= 1.57;SLP= 3.31;IDP= 1880; IAREP= 250; IAREC= 0]
09119# [IAREC= 4.00] IAREP= 4.00]
09120# [SMIN= 95.77; SMAX=465.12; SK = .010]
09121#
09122# R025<C00082-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09123# CONTINUOUS STANDBY 1.0 01:18:41 60.63 2.500_MoDate 28:10 28.05 .377 .000
09124# [XIMP= 13.7TMP= 26]
09125# [LOGS= 2 CM= 61.0]
09126# [Previous area: IAREC= 4.67;SLP= 3.81;IDP= 550; IAREP= 0; IAREC= 0]
09127# [Impervious area: IAREP= 1.57;SLP= 3.81;IDP= 1450; IAREP= 250; IAREC= 0]
09128# [IAREC= 4.00] IAREP= 4.00]
09129# [SMIN= 64.50; SMAX=430.01; SK = .010]
09130#
09131# R025<C00083-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09132# ADD HYD + 1.0 02:18:41 139.27 1.620_MoDate 29:14 19.65 n/a .000
09133# [RPT: 1.00] out<= 1.0 02:18:41 139.27 1.620_MoDate 29:14 19.65 n/a .000
09134# [L/S= 1.00] out<= 1.0 02:18:41 139.27 1.620_MoDate 29:14 19.65 n/a .000
09135# SUM= 1.0 01:18:41 60.63 2.500_MoDate 28:10 28.05 .377 .000
09136#
09137# R025<C00084-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09138# CONTINUOUS STANDBY 1.0 01:18:41 5.28 0.076_MoDate 28:37 38.08 .243 .000
09139# [CM= 54.0 N= 3.00] Tp = .60]
09140# [IAREC= 4.00] SMIN= 194.27; SMAX=500.07; SK = .010]
09141# [InterEventTime= 12.00]
09142#
09143# R025<C00085-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09144# ADD HYD + 1.0 02:18:41 256.03 4.071_MoDate 28:22 21.98 n/a .000
09145# [RPT: 1.00] out<= 1.0 02:18:41 256.03 4.071_MoDate 28:22 21.98 n/a .000
09146# [L/S= 1.00] out<= 1.0 02:18:41 256.03 4.071_MoDate 28:22 21.98 n/a .000
09147# [Vmax = 793IDmax = 719]
09148#
09149# R025<C00087-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09150# CONTINUOUS STANDBY 1.0 01:18:41 2.50 0.464_MoDate 28:12 37.38 .562 .000
09151# [CM= 84.0 N= 3.00] Tp = .28]
09152# [IAREC= 4.00] SMIN= 140.62; SK = .010]
09153# [InterEventTime= 12.00]
09154#
09155# R025<C00088-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09156# CONTINUOUS STANDBY 1.0 01:18:41 66.75 7.878_MoDate 28:01 58.43 .785 .000
09157# [XIMP= 68.7TMP= 85]
09158# [LOGS= 2 CM= 61.0]
09159# [Previous area: IAREC= 4.67;SLP= 3.30;IDP= 4.14; P = .00]
09160# [Impervious area: IAREP= 1.57;SLP= 3.30;IDP= 50; IAREP= 250; IAREC= 0]
09161# [IAREC= 4.00] IAREP= 4.00]
09162# [SMIN= 95.77; SMAX=465.12; SK = .010]
09163#
09164# R025<C00089-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09165# CONTINUOUS STANDBY 1.0 01:18:41 66.75 7.878_MoDate 28:01 58.43 .785 .000
09166# [XIMP= 68.7TMP= 85]
09167# [LOGS= 2 CM= 61.0]
09168# [Previous area: IAREC= 4.67;SLP= 3.30;IDP= 4.14; P = .00]
09169# [Impervious area: IAREP= 1.57;SLP= 3.30;IDP= 50; IAREP= 250; IAREC= 0]
09170# [IAREC= 4.00] IAREP= 4.00]
09171# [SMIN= 95.77; SMAX=465.12; SK = .010]
09172#
09173# R025<C00090-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09174# CONTINUOUS STANDBY 1.0 01:18:41 66.75 7.878_MoDate 28:01 58.43 .785 .000
09175# [XIMP= 68.7TMP= 85]
09176# [LOGS= 2 CM= 61.0]
09177# [Previous area: IAREC= 4.67;SLP= 3.30;IDP= 4.14; P = .00]
09178# [Impervious area: IAREP= 1.57;SLP= 3.30;IDP= 50; IAREP= 250; IAREC= 0]
09179# [IAREC= 4.00] IAREP= 4.00]
09180# [SMIN= 95.77; SMAX=465.12; SK = .010]
09181#
09182# R025<C00091-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09183# CONTINUOUS STANDBY 1.0 01:18:41 66.75 7.878_MoDate 28:01 58.43 .785 .000
09184# [XIMP= 68.7TMP= 85]
09185# [LOGS= 2 CM= 61.0]
09186# [Previous area: IAREC= 4.67;SLP= 3.30;IDP= 4.14; P = .00]
09187# [Impervious area: IAREP= 1.57;SLP= 3.30;IDP= 50; IAREP= 250; IAREC= 0]
09188# [IAREC= 4.00] IAREP= 4.00]
09189# [SMIN= 95.77; SMAX=465.12; SK = .010]
09190#
09191# R025<C00092-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09192# CONTINUOUS STANDBY 1.0 01:18:41 66.75 7.878_MoDate 28:01 58.43 .785 .000
09193# [XIMP= 68.7TMP= 85]
09194# [LOGS= 2 CM= 61.0]
09195# [Previous area: IAREC= 4.67;SLP= 3.30;IDP= 4.14; P = .00]
09196# [Impervious area: IAREP= 1.57;SLP= 3.30;IDP= 50; IAREP= 250; IAREC= 0]
09197# [IAREC= 4.00] IAREP= 4.00]
09198# [SMIN= 95.77; SMAX=465.12; SK = .010]
09199#
09200# R025<C00093-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09201# CONTINUOUS STANDBY 1.0 01:18:41 66.75 7.878_MoDate 28:01 58.43 .785 .000
09202# [XIMP= 68.7TMP= 85]
09203# [LOGS= 2 CM= 61.0]
09204# [Previous area: IAREC= 4.67;SLP= 3.30;IDP= 4.14; P = .00]
09205# [Impervious area: IAREP= 1.57;SLP= 3.30;IDP= 50; IAREP= 250; IAREC= 0]
09206# [IAREC= 4.00] IAREP= 4.00]
09207# [SMIN= 95.77; SMAX=465.12; SK = .010]
09208#
09209# R025<C00094-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09210# CONTINUOUS STANDBY 1.0 01:18:41 66.75 7.878_MoDate 28:01 58.43 .785 .000
09211# [XIMP= 68.7TMP= 85]
09212# [LOGS= 2 CM= 61.0]
09213# [Previous area: IAREC= 4.67;SLP= 3.30;IDP= 4.14; P = .00]
09214# [Impervious area: IAREP= 1.57;SLP= 3.30;IDP= 50; IAREP= 250; IAREC= 0]
09215# [IAREC= 4.00] IAREP= 4.00]
09216# [SMIN= 95.77; SMAX=465.12; SK = .010]
09217#
09218# R025<C00095-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09219# CONTINUOUS STANDBY 1.0 01:18:41 66.75 7.878_MoDate 28:01 58.43 .785 .000
09220# [XIMP= 68.7TMP= 85]
09221# [LOGS= 2 CM= 61.0]
09222# [Previous area: IAREC= 4.67;SLP= 3.30;IDP= 4.14; P = .00]
09223# [Impervious area: IAREP= 1.57;SLP= 3.30;IDP= 50; IAREP= 250; IAREC= 0]
09224# [IAREC= 4.00] IAREP= 4.00]
09225# [SMIN= 95.77; SMAX=465.12; SK = .010]
09226#
09227# R025<C00096-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09228# CONTINUOUS STANDBY 1.0 01:18:41 66.75 7.878_MoDate 28:01 58.43 .785 .000
09229# [XIMP= 68.7TMP= 85]
09230# [LOGS= 2 CM= 61.0]
09231# [Previous area: IAREC= 4.67;SLP= 3.30;IDP= 4.14; P = .00]
09232# [Impervious area: IAREP= 1.57;SLP= 3.30;IDP= 50; IAREP= 250; IAREC= 0]
09233# [IAREC= 4.00] IAREP= 4.00]
09234# [SMIN= 95.77; SMAX=465.12; SK = .010]
09235#
09236# R025<C00097-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09237# CONTINUOUS STANDBY 1.0 01:18:41 66.75 7.878_MoDate 28:01 58.43 .785 .000
09238# [XIMP= 68.7TMP= 85]
09239# [LOGS= 2 CM= 61.0]
09240# [Previous area: IAREC= 4.67;SLP= 3.30;IDP= 4.14; P = .00]
09241# [Impervious area: IAREP= 1.57;SLP= 3.30;IDP= 50; IAREP= 250; IAREC= 0]
09242# [IAREC= 4.00] IAREP= 4.00]
09243# [SMIN= 95.77; SMAX=465.12; SK = .010]
09244#
09245# R025<C00098-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09246# CONTINUOUS STANDBY 1.0 01:18:41 66.75 7.878_MoDate 28:01 58.43 .785 .000
09247# [XIMP= 68.7TMP= 85]
09248# [LOGS= 2 CM= 61.0]
09249# [Previous area: IAREC= 4.67;SLP= 3.30;IDP= 4.14; P = .00]
09250# [Impervious area: IAREP= 1.57;SLP= 3.30;IDP= 50; IAREP= 250; IAREC= 0]
09251# [IAREC= 4.00] IAREP= 4.00]
09252# [SMIN= 95.77; SMAX=465.12; SK = .010]
09253#
09254# R025<C00099-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09255# CONTINUOUS STANDBY 1.0 01:18:41 66.75 7.878_MoDate 28:01 58.43 .785 .000
09256# [XIMP= 68.7TMP= 85]
09257# [LOGS= 2 CM= 61.0]
09258# [Previous area: IAREC= 4.67;SLP= 3.30;IDP= 4.14; P = .00]
09259# [Impervious area: IAREP= 1.57;SLP= 3.30;IDP= 50; IAREP= 250; IAREC= 0]
09260# [IAREC= 4.00] IAREP= 4.00]
09261# [SMIN= 95.77; SMAX=465.12; SK = .010]
09262#
09263# R025<C00100-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09264# CONTINUOUS STANDBY 1.0 01:18:41 66.75 7.878_MoDate 28:01 58.43 .785 .000
09265# [XIMP= 68.7TMP= 85]
09266# [LOGS= 2 CM= 61.0]
09267# [Previous area: IAREC= 4.67;SLP= 3.30;IDP= 4.14; P = .00]
09268# [Impervious area: IAREP= 1.57;SLP= 3.30;IDP= 50; IAREP= 250; IAREC= 0]
09269# [IAREC= 4.00] IAREP= 4.00]
09270# [SMIN= 95.77; SMAX=465.12; SK = .010]
09271#
09272# R025<C00101-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09273# CONTINUOUS STANDBY 1.0 01:18:41 66.75 7.878_MoDate 28:01 58.43 .785 .000
09274# [XIMP= 68.7TMP= 85]
09275# [LOGS= 2 CM= 61.0]
09276# [Previous area: IAREC= 4.67;SLP= 3.30;IDP= 4.14; P = .00]
09277# [Impervious area: IAREP= 1.57;SLP= 3.30;IDP= 50; IAREP= 250; IAREC= 0]
09278# [IAREC= 4.00] IAREP= 4.00]
09279# [SMIN= 95.77; SMAX=465.12; SK = .010]
09280#
09281# R025<C00102-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09282# CONTINUOUS STANDBY 1.0 01:18:41 66.75 7.878_MoDate 28:01 58.43 .785 .000
09283# [XIMP= 68.7TMP= 85]
09284# [LOGS= 2 CM= 61.0]
09285# [Previous area: IAREC= 4.67;SLP= 3.30;IDP= 4.14; P = .00]
09286# [Impervious area: IAREP= 1.57;SLP= 3.30;IDP= 50; IAREP= 250; IAREC= 0]
09287# [IAREC= 4.00] IAREP= 4.00]
09288# [SMIN= 95.77; SMAX=465.12; SK = .010]
09289#
09290# R025<C00103-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09291# CONTINUOUS STANDBY 1.0 01:18:41 66.75 7.878_MoDate 28:01 58.43 .785 .000
09292# [XIMP= 68.7TMP= 85]
09293# [LOGS= 2 CM= 61.0]
09294# [Previous area: IAREC= 4.67;SLP= 3.30;IDP= 4.14; P = .00]
09295# [Impervious area: IAREP= 1.57;SLP= 3.30;IDP= 50; IAREP= 250; IAREC= 0]
09296# [IAREC= 4.00] IAREP= 4.00]
09297# [SMIN= 95.77; SMAX=465.12; SK = .010]
09298#
09299# R025<C00104-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09300# CONTINUOUS STANDBY 1.0 01:18:41 66.75 7.878_MoDate 28:01 58.43 .785 .000
09301# [XIMP= 68.7TMP= 85]
09302# [LOGS= 2 CM= 61.0]
09303# [Previous area: IAREC= 4.67;SLP= 3.30;IDP= 4.14; P = .00]
09304# [Impervious area: IAREP= 1.57;SLP= 3.30;IDP= 50; IAREP= 250; IAREC= 0]
09305# [IAREC= 4.00] IAREP= 4.00]
09306# [SMIN= 95.77; SMAX=465.12; SK = .010]
09307#
09308# R025<C00105-----DtmIn-ID:HYD-----AREHA-GPEAFcMs-TPeakDate,hh:mm-----RvM-R-C-----DWfCms
09309# CONTINUOUS STANDBY 1.0 01:18:41 66.75 7.878_MoDate 2
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10847	ROUTE PIPE	>>	1.0	02:19:35-338	17.90	1.490	N_Date	28:26	49.83	n/a	.000	
10848	[From 1.00] out<		1.0	02:19:34-340	17.90	1.456	N_Date	28:26	49.83	n/a	.000	
10849	[L/S=	233.7	/100.0]									
10850	[Vmax	1.35]	Dmax	1.35]								
10851	[Din	1.80]	Dused	1.80]								
10852	ROUT25-C00336	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	
10853	CONTINUOUS STANDBY											
10854	[L/S=	233.7	/100.0]									
10855	[Vmax	1.35]	Dmax	1.35]								
10856	[Din	1.80]	Dused	1.80]								
10857	[Previous area	IAPer	4.67]	SLP=1.00]	40.0	MP=	250.0]	SC=	0.0]			
10858	[Impervious area	IAlmp	1.57]	SLP=1.00]	181.0	MI=	0.13]	SC=	0.0]			
10859	[IARECimp	4.00]	IARECimp	4.00]								
10860	[SMIN	33.81]	SMAX	225.43]	SK	0.01]						
10861	COMPUTE DUALHDY											
10862	Major System	/	1.0	02:18-MJ	0.00	0.00	N_Date	0:00	0.0	n/a	.000	
10863	Minor System	/	1.0	02:18-MJ	0.00	0.00	N_Date	0:00	0.0	n/a	.000	
10864	[MjSysStor	.0000E+00,	ToCovVol	.0000E+00,	N-OvF	0,	ToTurDovF	.0 hrs]				
10865	ADD HYD											
10866	[L/S=	240.7	/100.0]									
10867	[Vmax	1.09]	Dmax	1.09]								
10868	[Din	1.80]	Dused	1.80]								
10869	ROUT25-C00339	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	
10870	SAVE HYD											
10871	fname	MH104.0025										
10872	remark	Total Flows at MH104										
10873	ROUT25-C00370	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	
10874	ROUTE PIPE	>>	1.0	02:19:34-340	25.50	2.104	N_Date	28:18	49.88	n/a	.000	
10875	[RPT	1.00]	out<		1.0	02:19:34-340	25.50	2.086	N_Date	28:18	49.88	n/a
10876	[L/S=	240.7	/100.0]									
10877	[Vmax	1.22]	Dmax	1.22]								
10878	[Din	1.65]	Dused	1.65]								
10879	ROUT25-C00371	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	
10880	ADD HYD											
10881	[L/S=	240.7	/100.0]									
10882	[Vmax	1.01]	Dmax	1.01]								
10883	[Din	1.01]	Dused	1.01]								
10884	COMPUTE DUALHDY											
10885	Major System	/	1.0	02:18-MJ	0.00	0.00	N_Date	0:00	0.0	n/a	.000	
10886	Minor System	/	1.0	02:18-MJ	0.00	0.00	N_Date	0:00	0.0	n/a	.000	
10887	[MjSysStor	.0000E+00,	ToCovVol	.0000E+00,	N-OvF	0,	ToTurDovF	.0 hrs]				
10888	ADD HYD											
10889	[L/S=	240.7	/100.0]									
10890	[Vmax	1.01]	Dmax	1.01]								
10891	[Din	1.01]	Dused	1.01]								
10892	ROUT25-C00372	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	
10893	CONTINUOUS STANDBY											
10894	[L/S=	240.7	/100.0]									
10895	[Vmax	1.01]	Dmax	1.01]								
10896	[Din	1.01]	Dused	1.01]								
10897	[Previous area	IAPer	4.67]	SLP=1.00]	40.0	MP=	250.0]	SC=	0.0]			
10898	[Impervious area	IAlmp	1.57]	SLP=1.00]	181.0	MI=	0.13]	SC=	0.0]			
10899	[IARECimp	4.00]	IARECimp	4.00]								
10900	[SMIN	33.81]	SMAX	225.43]	SK	0.01]						
10901	COMPUTE DUALHDY											
10902	Major System	/	1.0	02:18-MJ	0.00	0.00	N_Date	0:00	0.0	n/a	.000	
10903	Minor System	/	1.0	02:18-MJ	0.00	0.00	N_Date	0:00	0.0	n/a	.000	
10904	[MjSysStor	.0000E+00,	ToCovVol	.0000E+00,	N-OvF	0,	ToTurDovF	.0 hrs]				
10905	ADD HYD											
10906	[L/S=	240.7	/100.0]									
10907	[Vmax	1.01]	Dmax	1.01]								
10908	[Din	1.01]	Dused	1.01]								
10909	ROUT25-C00373	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	
10910	ROUTE PIPE	>>	1.0	02:19:34-340	25.50	2.104	N_Date	28:18	49.88	n/a	.000	
10911	[RPT	1.00]	out<		1.0	02:19:34-340	25.50	2.086	N_Date	28:18	49.88	n/a
10912	[L/S=	240.7	/100.0]									
10913	[Vmax	1.22]	Dmax	1.22]								
10914	[Din	1.65]	Dused	1.65]								
10915	ROUT25-C00374	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	
10916	ADD HYD											
10917	[L/S=	240.7	/100.0]									
10918	[Vmax	1.01]	Dmax	1.01]								
10919	[Din	1.01]	Dused	1.01]								
10920	COMPUTE DUALHDY											
10921	Major System	/	1.0	02:18-MJ	0.00	0.00	N_Date	0:00	0.0	n/a	.000	
10922	Minor System	/	1.0	02:18-MJ	0.00	0.00	N_Date	0:00	0.0	n/a	.000	
10923	[MjSysStor	.0000E+00,	ToCovVol	.0000E+00,	N-OvF	0,	ToTurDovF	.0 hrs]				
10924	ADD HYD											
10925	[L/S=	240.7	/100.0]									
10926	[Vmax	1.01]	Dmax	1.01]								
10927	[Din	1.01]	Dused	1.01]								
10928	ROUT25-C00375	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	
10929	SAVE HYD											
10930	fname	MH105.0025										
10931	remark	Total Flows at MH105										
10932	ROUT25-C00380	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	
10933	DIVERTED	<=>	1.0	02:18-MJ	0.00	0.00	N_Date	0:00	0.0	n/a	.000	
10934	diverted	<=>	1.0	02:18-MJ-2R	0.00	0.00	N_Date	0:00	0.0	n/a	.000	
10935	diverted	<=>	1.0	02:18-MJ-86	0.00	0.00	N_Date	0:00	0.0	n/a	.000	
10936	diverted	<=>	1.0	02:18-MJ-2R	0.00	0.00	N_Date	0:00	0.0	n/a	.000	
10937	diverted	<=>	1.0	02:18-MJ-86	0.00	0.00	N_Date	0:00	0.0	n/a	.000	
10938	diverted	<=>	1.0	02:18-MJ-2R	0.00	0.00	N_Date	0:00	0.0	n/a	.000	
10939	diverted	<=>	1.0	02:18-MJ-86	0.00	0.00	N_Date	0:00	0.0	n/a	.000	
10940	ROUT25-C00382	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	
10941	CONTINUOUS STANDBY											
10942	[L/S=	233.7	/100.0]									
10943	[Vmax	1.08]	Dmax	1.08]								
10944	[Din	1.08]	Dused	1.08]								
10945	ROUT25-C00383	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	
10946	ADD HYD											
10947	[L/S=	233.7	/100.0]									
10948	[Vmax	1.08]	Dmax	1.08]								
10949	[Din	1.08]	Dused	1.08]								
10950	COMPUTE DUALHDY											
10951	Major System	/	1.0	02:18-MJ	0.00	0.00	N_Date	0:00	0.0	n/a	.000	
10952	Minor System	/	1.0	02:18-MJ	0.00	0.00	N_Date	0:00	0.0	n/a	.000	
10953	[MjSysStor	.0000E+00,	ToCovVol	.0000E+00,	N-OvF	0,	ToTurDovF	.0 hrs]				
10954	ADD HYD											
10955	[L/S=	233.7	/100.0]									
10956	[Vmax	1.08]	Dmax	1.08]								
10957	[Din	1.08]	Dused	1.08]								
10958	ROUT25-C00384	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	
10959	CONTINUOUS STANDBY											
10960	[L/S=	233.7	/100.0]									
10961	[Vmax	1.08]	Dmax	1.08]								
10962	[Din	1.08]	Dused	1.08]								
10963	[Previous area	IAPer	4.67]	SLP=1.00]	40.0	MP=	250.0]	SC=	0.0]			
10964	[Impervious area	IAlmp	1.57]	SLP=1.00]	181.0	MI=	0.13]	SC=	0.0]			
10965	[IARECimp	4.00]	IARECimp	4.00]								
10966	[SMIN	33.81]	SMAX	225.43]	SK	0.01]						
10967	COMPUTE DUALHDY											
10968	Major System	/	1.0	02:18-MJ	0.00	0.00	N_Date	0:00	0.0	n/a	.000	
10969	Minor System	/	1.0	02:18-MJ	0.00	0.00	N_Date	0:00	0.0	n/a	.000	
10970	[MjSysStor	.0000E+00,	ToCovVol	.0000E+00,	N-OvF	0,	ToTurDovF	.0 hrs]				
10971	ADD HYD											
10972	[L/S=	233.7	/100.0]									
10973	[Vmax	1.08]	D									

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11221 # remark/Total Flows at Jockvale Road
11222 #
11223 # Hydrograph from Jockvale Road routed to Heart's Desire
11224 # Channel X-Section obtained from RWCA Hydraulic Model - Station 699
11225 #
11226 #
11227 ROUTE CHANNEl 1.0 01:RSH_DE 55194.86 104.140 No.Date 39:49 29.33 n/a .000
11228 [RFD= 1.00] out< 1.0 01:RSH_DE 55194.86 104.140 No.Date 39:45 29.33 n/a .000
11229 [L/S= 221.5]
11230 [Vmax= 1.483;Dmax= 2.264]
11231 #
11232 # Catchment DESIRE
11233 # - To Jock River (north of the Jock)
11234 # Rural-estate subdivision of Heart's Desire Community)
11235 #
11236 ROUTE CHANNEl 1.0 01:RSH_DE 55194.86 104.140 No.Date 39:49 29.33 n/a .000
11237 CONTINUOUS STANdRD 1.0 01:DESIRE 23.78 2.161 No.Date 28:03 40.77 1548 .000
11238 [XMP= 25.0;TMD= 25]
11239 [S= 1.0]
11240 [Perivous area IArea= 4.67;SLDPI= 0.0;LDD= 4.0;MMD= 250;SOCI= 0]
11241 [Impervious area IArea= 1.57;SLDPI= 0.0;LDD= 4.0;MMD= 250;SOCI= 0]
11242 [S= 1.0]
11243 [S= 1.0]
11244 #
11245 # Catchment JOCKVA
11246 # - To Jockvale SWM Facility
11247 # - Residential development & golf course
11248 # JFSA 2021-01-11 update JOCKVA after updating CORSS as per INV 01/08/2021, July 2008.
11249 # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX-LAND 12.5 ha as
11250 #
11251 ROUTE CHANNEl 1.0 01:JOCKVA 225.13 21.797 No.Date 28:07 50.08 673 .000
11252 CONTINUOUS STANdRD 1.0 01:JOCKVA 225.13 21.797 No.Date 28:07 50.08 673 .000
11253 [XMP= 25.0;TMD= 25]
11254 [S= 1.0]
11255 [Perivous area IArea= 4.67;SLDPI= 0.0;LDD= 4.0;MMD= 250;SOCI= 0]
11256 [Impervious area IArea= 1.57;SLDPI= 0.0;LDD= 4.0;MMD= 250;SOCI= 0]
11257 [S= 1.0]
11258 #
11259 ROUTE CHANNEl 1.0 01:RSH_DE 55194.86 104.140 No.Date 39:49 29.33 n/a .000
11260 [RFD= 1.00] out< 1.0 01:JOCKVA 225.13 21.797 No.Date 28:07 50.08 n/a .000
11261 [L/S= 221.5]
11262 [Vmax= 1.483;Dmax= 2.264]
11263 #
11264 #
11265 ROUTE CHANNEl 1.0 01:JOCKVA 225.13 21.797 No.Date 28:07 50.10 n/a .000
11266 [RFD= 1.00] out< 1.0 01:JOCKVA 225.13 21.797 No.Date 28:07 50.10 n/a .000
11267 [L/S= 221.5]
11268 #
11269 #
11270 #
11271 # Rating curve obtained from Jockvale Servicing Study (CC 1999)
11272 #
11273 ROUTE CHANNEl 1.0 01:RSH_DE 55194.86 104.140 No.Date 39:49 29.33 n/a .000
11274 ROUTE RESERVEd 1.0 01:RSH_DE 55194.86 104.140 No.Date 39:49 29.33 n/a .000
11275 out< 1.0 01:JOCK_P 257.63 9.145 No.Date 28:37 50.10 n/a .000
11276 [XMP= 25.0;TMD= 25]
11277 [S= 1.0]
11278 #
11279 #
11280 ROUTE CHANNEl 1.0 01:RSH_DE 55194.86 104.140 No.Date 39:49 29.33 n/a .000
11281 [RFD= 1.00] out< 1.0 01:DESIRE 23.78 2.161 No.Date 28:03 40.77 n/a .000
11282 [L/S= 221.5]
11283 [Vmax= 1.483;Dmax= 2.264]
11284 #
11285 #
11286 ROUTE CHANNEl 1.0 01:RSH_DE 55194.86 104.140 No.Date 39:49 29.33 n/a .000
11287 [RFD= 1.00] out< 1.0 01:DESIRE 23.78 2.161 No.Date 28:03 40.77 n/a .000
11288 [L/S= 221.5]
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13091	+	1.0 01:18-12:0	4.86	567	28:09	68.93	n/a	.000
13092	+	1.0 01:18-14:0	5.47	873	28:09	60.02	n/a	.000
13093	+	1.0 01:18-16:0	7.42	1244	28:09	46.87	n/a	.000
13094	+	1.0 01:18-18:0	10.00	1800	28:09	34.06	n/a	.000
13095	+	1.0 01:18-20:0	13.24	2639	28:09	24.67	n/a	.000
13096	+	1.0 01:18-22:0	17.14	3734	28:09	17.84	n/a	.000
13097	+	1.0 01:18-24:0	21.74	5084	28:09	12.87	n/a	.000
13098	+	1.0 01:18-26:0	27.00	6720	28:09	9.00	n/a	.000
13099	+	1.0 01:18-28:0	32.86	8661	28:09	6.60	n/a	.000
13100	+	1.0 01:18-30:0	39.30	10926	28:09	4.87	n/a	.000
13101	+	1.0 01:18-32:0	46.30	13527	28:09	3.60	n/a	.000
13102	+	1.0 01:18-34:0	53.80	16474	28:09	2.67	n/a	.000
13103	+	1.0 01:18-36:0	61.80	19777	28:09	1.97	n/a	.000
13104	+	1.0 01:18-38:0	70.30	23446	28:09	1.45	n/a	.000
13105	+	1.0 01:18-40:0	79.30	27491	28:09	1.07	n/a	.000
13106	+	1.0 01:18-42:0	88.80	31922	28:09	0.78	n/a	.000
13107	+	1.0 01:18-44:0	98.80	36749	28:09	0.57	n/a	.000
13108	+	1.0 01:18-46:0	109.30	41984	28:09	0.42	n/a	.000
13109	+	1.0 01:18-48:0	120.30	47637	28:09	0.31	n/a	.000
13110	+	1.0 01:18-50:0	131.80	53710	28:09	0.22	n/a	.000
13111	+	1.0 01:18-52:0	143.80	60213	28:09	0.16	n/a	.000
13112	+	1.0 01:18-54:0	156.30	67146	28:09	0.12	n/a	.000
13113	+	1.0 01:18-56:0	169.30	74509	28:09	0.09	n/a	.000
13114	+	1.0 01:18-58:0	182.80	82302	28:09	0.07	n/a	.000
13115	+	1.0 01:18-60:0	196.80	90525	28:09	0.05	n/a	.000
13116	+	1.0 01:18-62:0	211.30	99188	28:09	0.04	n/a	.000
13117	+	1.0 01:18-64:0	226.30	108291	28:09	0.03	n/a	.000
13118	+	1.0 01:18-66:0	241.80	117944	28:09	0.02	n/a	.000
13119	+	1.0 01:18-68:0	257.80	128057	28:09	0.02	n/a	.000
13120	+	1.0 01:18-70:0	274.30	138630	28:09	0.01	n/a	.000
13121	+	1.0 01:18-72:0	291.30	149663	28:09	0.01	n/a	.000
13122	+	1.0 01:18-74:0	308.80	161166	28:09	0.01	n/a	.000
13123	+	1.0 01:18-76:0	326.80	173139	28:09	0.01	n/a	.000
13124	+	1.0 01:18-78:0	345.30	185582	28:09	0.01	n/a	.000
13125	+	1.0 01:18-80:0	364.30	198505	28:09	0.01	n/a	.000
13126	+	1.0 01:18-82:0	383.80	211918	28:09	0.01	n/a	.000
13127	+	1.0 01:18-84:0	403.80	225831	28:09	0.01	n/a	.000
13128	+	1.0 01:18-86:0	424.30	240244	28:09	0.01	n/a	.000
13129	+	1.0 01:18-88:0	445.30	255157	28:09	0.01	n/a	.000
13130	+	1.0 01:18-90:0	466.80	270570	28:09	0.01	n/a	.000
13131	+	1.0 01:18-92:0	488.80	286483	28:09	0.01	n/a	.000
13132	+	1.0 01:18-94:0	511.30	302896	28:09	0.01	n/a	.000
13133	+	1.0 01:18-96:0	534.30	319809	28:09	0.01	n/a	.000
13134	+	1.0 01:18-98:0	557.80	337222	28:09	0.01	n/a	.000
13135	+	1.0 01:18-100:0	581.80	355135	28:09	0.01	n/a	.000
13136	+	1.0 01:18-102:0	606.30	373548	28:09	0.01	n/a	.000
13137	+	1.0 01:18-104:0	631.30	392461	28:09	0.01	n/a	.000
13138	+	1.0 01:18-106:0	656.80	411874	28:09	0.01	n/a	.000
13139	+	1.0 01:18-108:0	682.80	431787	28:09	0.01	n/a	.000
13140	+	1.0 01:18-110:0	709.30	452200	28:09	0.01	n/a	.000
13141	+	1.0 01:18-112:0	736.30	473113	28:09	0.01	n/a	.000
13142	+	1.0 01:18-114:0	763.80	494526	28:09	0.01	n/a	.000
13143	+	1.0 01:18-116:0	791.80	516439	28:09	0.01	n/a	.000
13144	+	1.0 01:18-118:0	820.30	538852	28:09	0.01	n/a	.000
13145	+	1.0 01:18-120:0	849.30	561765	28:09	0.01	n/a	.000
13146	+	1.0 01:18-122:0	878.80	585178	28:09	0.01	n/a	.000
13147	+	1.0 01:18-124:0	908.80	609091	28:09	0.01	n/a	.000
13148	+	1.0 01:18-126:0	939.30	633504	28:09	0.01	n/a	.000
13149	+	1.0 01:18-128:0	970.30	658417	28:09	0.01	n/a	.000
13150	+	1.0 01:18-130:0	1001.80	683830	28:09	0.01	n/a	.000
13151	+	1.0 01:18-132:0	1033.80	709743	28:09	0.01	n/a	.000
13152	+	1.0 01:18-134:0	1066.30	736156	28:09	0.01	n/a	.000
13153	+	1.0 01:18-136:0	1099.30	763069	28:09	0.01	n/a	.000
13154	+	1.0 01:18-138:0	1132.80	790482	28:09	0.01	n/a	.000
13155	+	1.0 01:18-140:0	1166.80	818395	28:09	0.01	n/a	.000
13156	+	1.0 01:18-142:0	1201.30	846808	28:09	0.01	n/a	.000
13157	+	1.0 01:18-144:0	1236.30	875721	28:09	0.01	n/a	.000
13158	+	1.0 01:18-146:0	1271.80	905134	28:09	0.01	n/a	.000
13159	+	1.0 01:18-148:0	1307.80	935047	28:09	0.01	n/a	.000
13160	+	1.0 01:18-150:0	1344.30	965460	28:09	0.01	n/a	.000
13161	+	1.0 01:18-152:0	1381.30	996373	28:09	0.01	n/a	.000
13162	+	1.0 01:18-154:0	1418.80	1027786	28:09	0.01	n/a	.000
13163	+	1.0 01:18-156:0	1456.80	1088799	28:09	0.01	n/a	.000
13164	+	1.0 01:18-158:0	1495.30	1150312	28:09	0.01	n/a	.000
13165	+	1.0 01:18-160:0	1534.30	1212325	28:09	0.01	n/a	.000
13166	+	1.0 01:18-162:0	1573.80	1274838	28:09	0.01	n/a	.000
13167	+	1.0 01:18-164:0	1613.80	1337851	28:09	0.01	n/a	.000
13168	+	1.0 01:18-166:0	1654.30	1401364	28:09	0.01	n/a	.000
13169	+	1.0 01:18-168:0	1695.30	1465377	28:09	0.01	n/a	.000
13170	+	1.0 01:18-170:0	1736.80	1530890	28:09	0.01	n/a	.000
13171	+	1.0 01:18-172:0	1778.80	1597903	28:09	0.01	n/a	.000
13172	+	1.0 01:18-174:0	1821.30	1666416	28:09	0.01	n/a	.000
13173	+	1.0 01:18-176:0	1864.30	1736429	28:09	0.01	n/a	.000
13174	+	1.0 01:18-178:0	1907.80	1807942	28:09	0.01	n/a	.000
13175	+	1.0 01:18-180:0	1951.80	1880955	28:09	0.01	n/a	.000
13176	+	1.0 01:18-182:0	1996.30	1955468	28:09	0.01	n/a	.000
13177	+	1.0 01:18-184:0	2041.30	2031481	28:09	0.01	n/a	.000
13178	+	1.0 01:18-186:0	2086.80	2108994	28:09	0.01	n/a	.000
13179	+	1.0 01:18-188:0	2132.80	2188007	28:09	0.01	n/a	.000
13180	+	1.0 01:18-190:0	2179.30	2268520	28:09	0.01	n/a	.000
13181	+	1.0 01:18-192:0	2226.30	2350533	28:09	0.01	n/a	.000
13182	+	1.0 01:18-194:0	2273.80	2434046	28:09	0.01	n/a	.000
13183	+	1.0 01:18-196:0	2321.80	2519059	28:09	0.01	n/a	.000
13184	+	1.0 01:18-198:0	2370.30	2605572	28:09	0.01	n/a	.000
13185	+	1.0 01:18-200:0	2419.30	2693585	28:09	0.01	n/a	.000
13186	+	1.0 01:18-202:0	2468.80	2783098	28:09	0.01	n/a	.000
13187	+	1.0 01:18-204:0	2518.80	2874111	28:09	0.01	n/a	.000
13188	+	1.0 01:18-206:0	2569.30	2966624	28:09	0.01	n/a	.000
13189	+	1.0 01:18-208:0	2620.30	3060637	28:09	0.01	n/a	.000
13190	+	1.0 01:18-210:0	2671.80	3156150	28:09	0.01	n/a	.000
13191	+	1.0 01:18-212:0	2723.80	3253163	28:09	0.01	n/a	.000
13192	+	1.0 01:18-214:0	2776.30	3351676	28:09	0.01	n/a	.000
13193	+	1.0 01:18-216:0	2829.30	3451689	28:09	0.01	n/a	.000
13194	+	1.0 01:18-218:0	2882.80	3553202	28:09	0.01	n/a	.000
13195	+	1.0 01:18-220:0	2936.80	3656215	28:09	0.01	n/a	.000
13196	+	1.0 01:18-222:0	2991.30	3760728	28:09	0.01	n/a	.000
13197	+	1.0 01:18-224:0	3046.30	3866741	28:09	0.01	n/a	.000
13198	+	1.0 01:18-226:0	3101.80	3974254	28:09	0.01	n/a	.000
13199	+	1.0 01:18-228:0	3157.80	4083267	28:09	0.01	n/a	.000
13200	+	1.0 01:18-230:0	3214.30	4193780	28:09	0.01	n/a	.000
13201	+	1.0 01:18-232:0	3271.30	4305793	28:09	0.01	n/a	.000
13202	+	1.0 01:18-234:0	3328.80	4419306	28:09	0.01	n/a	.000
13203	+	1.0 01:18-236:0	3386.80	4534319	28:09	0.01	n/a	.000
13204	+	1.0 01:18-238:0	3445.30	4650832	28:09	0.01	n/a	.000
13205	+	1.0 01:18-240:0	3504.30	4768845	28:09	0.01	n/a	.000
13206	+	1.0 01:18-242:0	3563.80	4888358	28:09	0.01	n/a	.000
132								







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14213 R0100C0009-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14214 CONTINUOUS NASHVD 1.0 01:01R_ASH 3074.00 10.428 NoDate 39:59 28.29 319 .000
14215 [Cm 50.0i No 3.00i Tp=11.33]
14216 [AREC 4.00i SMIN: 51.62i SMAK=554.96i SK= .010]
14217 [InterVntTime= 12.00]
14218 R0100C0009-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14219 CONTINUOUS NASHVD 1.0 01:01R_ASH 1781.00 19.695 NoDate 32:38 42.49 480 .000
14220 [Cm 72.0i No 3.00i Tp= 9.91]
14221 [AREC 4.00i SMIN: 52.62i SMAK=264.99i SK= .010]
14222 [InterVntTime= 12.00]
14223 R0100C0011-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14224 CONTINUOUS NASHVD 1.0 01:01R_M11 800.00 10.735 NoDate 29:21 36.76 415 .000
14225 [Cm 66.0i No 3.00i Tp= 1.24]
14226 [AREC 4.00i SMIN: 52.62i SMAK=350.79i SK= .010]
14227 [InterVntTime= 12.00]
14228 #
14229 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
14230 # of 1.80
14231 R0100C0011-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14232 CONTINUOUS NASHVD 1.0 01:01R_M11 1937.00 14.496 NoDate 34:24 36.76 415 .000
14233 [Cm 66.0i No 3.00i Tp= 1.24]
14234 [AREC 4.00i SMIN: 52.62i SMAK=350.79i SK= .010]
14235 [InterVntTime= 12.00]
14236 #
14237 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
14238 # of 1.82
14239 R0100C0011-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14240 CONTINUOUS NASHVD 1.0 01:01R_M11 5666.00 18.060 NoDate 37:48 42.49 480 .000
14241 [Cm 72.0i No 3.00i Tp= 8.00]
14242 [AREC 4.00i SMIN: 51.75i SMAK=264.99i SK= .010]
14243 [InterVntTime= 12.00]
14244 #
14245 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
14246 # of 1.78
14247 R0100C0011-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14248 CONTINUOUS NASHVD 1.0 01:01R_M11 8376.00 36.118 NoDate 39:59 36.76 415 .000
14249 [Cm 60.0i No 3.00i Tp=11.66]
14250 [AREC 4.00i SMIN: 52.62i SMAK=350.79i SK= .010]
14251 [InterVntTime= 12.00]
14252 #
14253 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
14254 # of 1.80
14255 R0100C0014-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14256 CONTINUOUS NASHVD 1.0 01:01R_S 1132.00 16.501 NoDate 30:52 40.82 461 .000
14257 [Cm 43.0i No 3.00i Tp= .90]
14258 [AREC 4.00i SMIN: 43.07i SMAK=287.10i SK= .010]
14259 [InterVntTime= 12.00]
14260 #
14261 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
14262 # of 1.82
14263 R0100C0011-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14264 CONTINUOUS NASHVD 1.0 01:01R_M11 4844.00 18.060 NoDate 39:59 31.61 380 .000
14265 [Cm 62.0i No 3.00i Tp=11.32]
14266 [AREC 4.00i SMIN: 52.62i SMAK=412.66i SK= .010]
14267 [InterVntTime= 12.00]
14268 #
14269 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
14270 # of 1.80
14271 R0100C0011-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14272 CONTINUOUS NASHVD 1.0 01:01R_S 131.00 3.259 NoDate 28:57 34.39 388 .000
14273 [Cm 43.0i No 3.00i Tp= .90]
14274 [AREC 4.00i SMIN: 52.62i SMAK=396.11i SK= .010]
14275 [InterVntTime= 12.00]
14276 #
14277 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
14278 # of 1.88
14279 R0100C0011-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14280 CONTINUOUS NASHVD 1.0 01:01R_M11 3854.00 21.238 NoDate 38:28 36.76 415 .000
14281 [Cm 66.0i No 3.00i Tp= 1.24]
14282 [AREC 4.00i SMIN: 52.62i SMAK=350.79i SK= .010]
14283 [InterVntTime= 12.00]
14284 #
14285 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
14286 # of 1.82
14287 R0100C0011-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14288 CONTINUOUS NASHVD 1.0 01:01R_M11 3197.00 16.421 NoDate 36:21 39.79 336 .000
14289 [Cm 57.0i No 3.00i Tp= 6.65]
14290 [AREC 4.00i SMIN: 52.62i SMAK=508.81i SK= .010]
14291 [InterVntTime= 12.00]
14292 #
14293 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
14294 # of 1.79
14295 R0100C0011-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14296 CONTINUOUS NASHVD 1.0 01:01R_S 165.00 1.511 NoDate 33:01 37.57 424 .000
14297 [Cm 47.0i No 3.00i Tp= 1.81]
14298 [AREC 4.00i SMIN: 52.62i SMAK=336.97i SK= .010]
14299 [InterVntTime= 12.00]
14300 #
14301 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
14302 # of 1.87
14303 R0100C0020-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14304 CONTINUOUS NASHVD 1.0 01:01R_M20 1332.00 10.892 NoDate 35:10 42.49 480 .000
14305 [Cm 72.0i No 3.00i Tp= 7.95]
14306 [AREC 4.00i SMIN: 39.75i SMAK=264.99i SK= .010]
14307 [InterVntTime= 12.00]
14308 R0100C0021-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14309 CONTINUOUS NASHVD 1.0 01:01R_M21 224.00 3.976 NoDate 28:44 47.62 538 .000
14310 [Cm 77.0i No 3.00i Tp= .75]
14311 [AREC 4.00i SMIN: 31.35i SMAK=207.66i SK= .010]
14312 [InterVntTime= 12.00]
14313 #
14314 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
14315 # of 1.20
14316 R0100C0022-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14317 CONTINUOUS NASHVD 1.0 01:01R_C 4945.00 52.056 NoDate 33:16 44.17 499 .000
14318 [Cm 74.0i No 3.00i Tp= 4.45]
14319 [AREC 4.00i SMIN: 36.47i SMAK=244.49i SK= .010]
14320 [InterVntTime= 12.00]
14321 R0100C0023-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14322 CONTINUOUS NASHVD 1.0 01:01R_S 20.00 1.097 NoDate 28:35 52.06 588 .000
14323 [Cm 81.0i No 3.00i Tp= 1.62]
14324 [AREC 4.00i SMIN: 25.21i SMAK=168.09i SK= .010]
14325 [InterVntTime= 12.00]
14326 #
14327 # The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
14328 # of 1.51
14329 R0100C0024-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14330 CONTINUOUS NASHVD 1.0 01:01R_S 1412.00 10.184 NoDate 37:44 45.88 518 .000
14331 [Cm 75.0i No 3.00i Tp= 1.00]
14332 [AREC 4.00i SMIN: 31.81i SMAK=225.43i SK= .010]
14333 [InterVntTime= 12.00]
14334 R0100C0025-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14335 CONTINUOUS NASHVD 1.0 01:01R_C 585.00 14.953 NoDate 29:55 52.06 588 .000
14336 [Cm 81.0i No 3.00i Tp= 1.75]
14337 [AREC 4.00i SMIN: 25.21i SMAK=168.09i SK= .010]
14338 [InterVntTime= 12.00]
14339 R0100C0026-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14340 CONTINUOUS NASHVD 1.0 01:01R_C 1021.00 19.792 NoDate 30:45 51.26 578 .000
14341 [Cm 80.0i No 3.00i Tp= 2.46]
14342 [AREC 4.00i SMIN: 25.21i SMAK=175.50i SK= .010]
14343 [InterVntTime= 12.00]
14344 R0100C0027-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14345 CONTINUOUS NASHVD 1.0 01:01R_C 177.00 7.767 NoDate 28:44 47.62 538 .000
14346 [Cm 77.0i No 3.00i Tp= .75]
14347 [AREC 4.00i SMIN: 31.35i SMAK=207.66i SK= .010]
14348 [InterVntTime= 12.00]
14349 R0100C0028-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14350 CONTINUOUS NASHVD 1.0 01:01R_M 1122.00 17.981 NoDate 31:42 52.06 588 .000
14351 [Cm 81.0i No 3.00i Tp= 1.25]
14352 [AREC 4.00i SMIN: 25.21i SMAK=168.09i SK= .010]
14353 [InterVntTime= 12.00]
14354 R0100C0029-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14355 CONTINUOUS NASHVD 1.0 01:01R_LR 2737.00 40.730 NoDate 31:28 46.75 528 .000
14356 [Cm 76.0i No 3.00i Tp= 1.01]
14357 [AREC 4.00i SMIN: 32.46i SMAK=216.39i SK= .010]
14358 [InterVntTime= 12.00]
14359 #
14360 # Routing hydrographs
14361 #
14362 # Starting with the addition of Jock River Headwater and Subwatershed 13
14363 #
14364 R0100C0030-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14365 ADD HYD + 1.0 02:01R_SW 3680.00 21.616 NoDate 36:52 35.18 n/a .000
14366 [AREC 4.00i SMIN: 31.81i SMAK=225.43i SK= .010]
14367 [InterVntTime= 12.00]
14368 #
14369 # Sum of hydrographs from Node 13 routed to Node 13A
14370 # (Approximated cross-section - see cross-section 258)
14371 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
14372 #
14373 R0100C0031-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14374 ROUTE CHANNEL -> 1.0 02:01R_M13 4651.00 27.660 NoDate 35:21 34.69 n/a .000
14375 [AREC 4.00i SMIN: 31.81i SMAK=225.43i SK= .010]
14376 [InterVntTime= 12.00]
14377 [Vmax= .598iDmax= 4.178]
14378 #
14379 # Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
14380 #
14381 R0100C0032-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14382 ADD HYD + 1.0 02:01R_M13 4651.00 22.998 NoDate 38:56 34.69 n/a .000
14383 [AREC 4.00i SMIN: 31.81i SMAK=225.43i SK= .010]
14384 [InterVntTime= 12.00]
14385 #
14386 # Insertion of a reservoir to simulate the effects of the Goodwood Marsh
14387 #
14388 R0100C0033-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14389 ROUTE RESERVOIR -> 1.0 02:01R_M13 7725.00 32.845 NoDate 39:44 32.14 n/a .000
14390 [Mactotiesd=.1796E+03]
14391 [InterVntTime= 12.00]
14392 #
14393 R0100C0034-----Dtn-ID-NHYD-----AREHA-OPEACms-TpeakDate_hh:mm-----Rvm-R.C-----DWFCms
14394 SAVE HYD FROM 1.0 01:01R_RES 7725.00 3.950 NoDate 62:26 32.14 n/a .000
14395 [AREC 4.00i SMIN: 31.81i SMAK=225.43i SK= .010]
14396 [InterVntTime= 12.00]
14397 # Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
14398 # (Approximated cross-section - see cross-section 258)
14399 # Use n=0.04 for summer conditions and n=0.025 for spring conditions

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164457	ROUTE PIPE	>>	1.0 02:01:00	17.35	1.488	28:00	28:35	62.96	n/a	.000
164458	[RPT= 1.00] out<	>>	1.0 02:01:00	17.35	1.489	28:00	28:37	62.96	n/a	.000
164459	[L/S= 251 / 100 / 0.13]									
164460	[Vmax= 1.302Dmax= 1.29]									
164461	[Din= 1.80] Dused= 2.19									
164462	CONTINUOUS STANDBY									
164463	[XMP= 41:TMP= 54]									
164464	[L/S= 251 / 100 / 0.13]									
164465	[Vmax= 1.302Dmax= 1.29]									
164466	[Din= 1.80] Dused= 2.19									
164467	CONTINUOUS STANDBY									
164468	[XMP= 41:TMP= 54]									
164469	[L/S= 251 / 100 / 0.13]									
164470	[Vmax= 1.302Dmax= 1.29]									
164471	[Din= 1.80] Dused= 2.19									
164472	CONTINUOUS STANDBY									
164473	[XMP= 41:TMP= 54]									
164474	[L/S= 251 / 100 / 0.13]									
164475	[Vmax= 1.302Dmax= 1.29]									
164476	[Din= 1.80] Dused= 2.19									
164477	CONTINUOUS STANDBY									
164478	[XMP= 41:TMP= 54]									
164479	[L/S= 251 / 100 / 0.13]									
164480	[Vmax= 1.302Dmax= 1.29]									
164481	[Din= 1.80] Dused= 2.19									
164482	CONTINUOUS STANDBY									
164483	[XMP= 41:TMP= 54]									
164484	[L/S= 251 / 100 / 0.13]									
164485	[Vmax= 1.302Dmax= 1.29]									
164486	[Din= 1.80] Dused= 2.19									
164487	CONTINUOUS STANDBY									
164488	[XMP= 41:TMP= 54]									
164489	[L/S= 251 / 100 / 0.13]									
164490	[Vmax= 1.302Dmax= 1.29]									
164491	[Din= 1.80] Dused= 2.19									
164492	CONTINUOUS STANDBY									
164493	[XMP= 41:TMP= 54]									
164494	[L/S= 251 / 100 / 0.13]									
164495	[Vmax= 1.302Dmax= 1.29]									
164496	[Din= 1.80] Dused= 2.19									
164497	CONTINUOUS STANDBY									
164498	[XMP= 41:TMP= 54]									
164499	[L/S= 251 / 100 / 0.13]									
164500	[Vmax= 1.302Dmax= 1.29]									
164501	[Din= 1.80] Dused= 2.19									
164502	CONTINUOUS STANDBY									
164503	[XMP= 41:TMP= 54]									
164504	[L/S= 251 / 100 / 0.13]									
164505	[Vmax= 1.302Dmax= 1.29]									
164506	[Din= 1.80] Dused= 2.19									
164507	CONTINUOUS STANDBY									
164508	[XMP= 41:TMP= 54]									
164509	[L/S= 251 / 100 / 0.13]									
164510	[Vmax= 1.302Dmax= 1.29]									
164511	[Din= 1.80] Dused= 2.19									
164512	CONTINUOUS STANDBY									
164513	[XMP= 41:TMP= 54]									
164514	[L/S= 251 / 100 / 0.13]									
164515	[Vmax= 1.302Dmax= 1.29]									
164516	[Din= 1.80] Dused= 2.19									
164517	CONTINUOUS STANDBY									
164518	[XMP= 41:TMP= 54]									
164519	[L/S= 251 / 100 / 0.13]									
164520	[Vmax= 1.302Dmax= 1.29]									
164521	[Din= 1.80] Dused= 2.19									
164522	CONTINUOUS STANDBY									
164523	[XMP= 41:TMP= 54]									
164524	[L/S= 251 / 100 / 0.13]									
164525	[Vmax= 1.302Dmax= 1.29]									
164526	[Din= 1.80] Dused= 2.19									
164527	CONTINUOUS STANDBY									
164528	[XMP= 41:TMP= 54]									
164529	[L/S= 251 / 100 / 0.13]									
164530	[Vmax= 1.302Dmax= 1.29]									
164531	[Din= 1.80] Dused= 2.19									
164532	CONTINUOUS STANDBY									
164533	[XMP= 41:TMP= 54]									
164534	[L/S= 251 / 100 / 0.13]									
164535	[Vmax= 1.302Dmax= 1.29]									
164536	[Din= 1.80] Dused= 2.19									
164537	CONTINUOUS STANDBY									
164538	[XMP= 41:TMP= 54]									
164539	[L/S= 251 / 100 / 0.13]									
164540	[Vmax= 1.302Dmax= 1.29]									
164541	[Din= 1.80] Dused= 2.19									
164542	CONTINUOUS STANDBY									
164543	[XMP= 41:TMP= 54]									
164544	[L/S= 251 / 100 / 0.13]									
164545	[Vmax= 1.302Dmax= 1.29]									
164546	[Din= 1.80] Dused= 2.19									
164547	CONTINUOUS STANDBY									
164548	[XMP= 41:TMP= 54]									
164549	[L/S= 251 / 100 / 0.13]									
164550	[Vmax= 1.302Dmax= 1.29]									
164551	[Din= 1.80] Dused= 2.19									
164552	CONTINUOUS STANDBY									
164553	[XMP= 41:TMP= 54]									
164554	[L/S= 251 / 100 / 0.13]									
164555	[Vmax= 1.302Dmax= 1.29]									
164556	[Din= 1.80] Dused= 2.19									
164557	CONTINUOUS STANDBY									
164558	[XMP= 41:TMP= 54]									
164559	[L/S= 251 / 100 / 0.13]									
164560	[Vmax= 1.302Dmax= 1.29]									
164561	[Din= 1.80] Dused= 2.19									
164562	CONTINUOUS STANDBY									
164563	[XMP= 41:TMP= 54]									
164564	[L/S= 251 / 100 / 0.13]									
164565	[Vmax= 1.302Dmax= 1.29]									
164566	[Din= 1.80] Dused= 2.19									
164567	CONTINUOUS STANDBY									
164568	[XMP= 41:TMP= 54]									
164569	[L/S= 251 / 100 / 0.13]									
164570	[Vmax= 1.302Dmax= 1.29]									
164571	[Din= 1.80] Dused= 2.19									
164572	CONTINUOUS STANDBY									
164573	[XMP= 41:TMP= 54]									
164574	[L/S= 251 / 100 / 0.13]									
164575	[Vmax= 1.302Dmax= 1.29]									
164576	[Din= 1.80] Dused= 2.19									
164577	CONTINUOUS STANDBY									
164578	[XMP= 41:TMP= 54]									
164579	[L/S= 251 / 100 / 0.13]									
164580	[Vmax= 1.302Dmax= 1.29]									
164581	[Din= 1.80] Dused= 2.19									
164582	CONTINUOUS STANDBY									
164583	[XMP= 41:TMP= 54]									
164584	[L/S= 251 / 100 / 0.13]									
164585	[Vmax= 1.302Dmax= 1.29]									
164586	[Din= 1.80] Dused= 2.19									
164587	CONTINUOUS STANDBY									
164588	[XMP= 41:TMP= 54]									
164589	[L/S= 251 / 100 / 0.13]									
164590	[Vmax= 1.302Dmax= 1.29]									
164591	[Din= 1.80] Dused= 2.19									
164592	CONTINUOUS STANDBY									
164593	[XMP= 41:TMP= 54]									
164594	[L/S= 251 / 100 / 0.13]									
164595	[Vmax= 1.302Dmax= 1.29]									
164596	[Din= 1.80] Dused= 2.19									
164597	CONTINUOUS STANDBY									
164598	[XMP= 41:TMP= 54]									
164599	[L/S= 251 / 100 / 0.13]									
164600	[Vmax= 1.302Dmax= 1.29]									
164601	[Din= 1.80] Dused= 2.19									



```

16831 ROUTE RESERVOIR -> 1.0 01:MI_L_P 175.99 20.390 No_date 28:06 56.87 n/a .000
16832 out <= 1.0 01:MI_L_P 146.22 4.050 No_date 28:08 56.87 n/a .000
16833 overflow <= 1.0 01:MI_L_P 29.77 16.228 No_date 28:08 56.87 n/a .000
16834 (MxOv=2.110) out <= 1.0 01:MI_L_P 29.77 16.228 No_date 28:08 56.87 n/a .000
16835 R0100:CO0426-----DRAIN-ID:HYD-----AREBA-QPEARCs-TpeakDate,h:mm-----RvM-R-C-----DWFCMs
16836 ADD HYD + 1.0 02:MI_M 5520.07 145.768 No_date 36:59 39.46 n/a .000
16837 + 1.0 02:MI_M 29.77 16.228 No_date 28:08 56.87 n/a .000
16838 + 1.0 02:MI_L_P 146.22 4.050 No_date 28:08 56.87 n/a .000
16839 SUM+ 55196.05 146.199 No_date 36:59 39.51 n/a .000
16840 R0100:CO0427-----DRAIN-ID:HYD-----AREBA-QPEARCs-TpeakDate,h:mm-----RvM-R-C-----DWFCMs
16841 SAVE HYD 1.0 01:SI_M 55196.05 146.199 No_date 36:58 39.51 n/a .000
16842 frame :SN_MI_0100
16843 remark:Total Flows at Jockvale Road
16844 #
16845 # Hydrograph from Jockvale Road routed to Heart's Desire
16846 # Channel X-Section obtained from RVCA Hydraulic Model - Station 689
16847 #
16848 R0100:CO0428-----DRAIN-ID:HYD-----AREBA-QPEARCs-TpeakDate,h:mm-----RvM-R-C-----DWFCMs
16849 ROUTE CHANNEL + 1.0 01:SI_M 55196.05 146.199 No_date 36:58 39.51 n/a .000
16850 [RDr= 1.00] out <= 1.0 01:SI_DE 55196.05 146.071 No_date 37:13 39.51 n/a .000
16851 [L/S= 192 / 227.045]
16852 [Vmax= 1.642:Dmax= 2.661]
16853 *****
16854 # Catchment DESIRE
16855 # - To Jock River (north of the Jock)
16856 # Rural-subur subdivision (Heart's Desire Community)
16857 #*****
16858 R0100:CO0429-----DRAIN-ID:HYD-----AREBA-QPEARCs-TpeakDate,h:mm-----RvM-R-C-----DWFCMs
16859 CONTINUOUS STANDHYD 1.0 01:DESIRE 23.78 3.004 No_date 28:03 53.11 .600 .000
16860 [XIMP= 25:TIMP= 25]
16861 [LOSS= 2 :CM= 77.0]
16862 [Previous area IArea= 4.67:SLIP=1.00:LD= 40.0:MD= 250:SCD= 0]
16863 [Impervious area IArea= 1.57:SLIP=1.00:LD= 400.0:MI= 013:SI= 0]
16864 [IAREClimp= 4.00: IAREKPer= 4.00]
16865 [SIN= 31.35: SMAX=41.49: SK= 010]
16866 *****
16867 # Catchment JOCKVA
16868 # - To Jockvale SSM Facility
16869 # - Residential development & golf course
16870 # JESA 2021-01-11 update JOCKVA after updating COBRG as per IRI GROUP, July 2008.
16871 # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX-LAND 32.5 ha as
16872 # per IRI GROUP, July 2008.
16873 R0100:CO0430-----DRAIN-ID:HYD-----AREBA-QPEARCs-TpeakDate,h:mm-----RvM-R-C-----DWFCMs
16874 CONTINUOUS STANDHYD 1.0 01:JOCKVA 225.13 28.623 No_date 28:07 62.70 .708 .000
16875 [XIMP= 25:TIMP= 50]
16876 [LOSS= 2 :CM= 74.0]
16877 [Previous area IArea= 4.67:SLIP=1.00:LD= 40.0:MD= 250:SCD= 0]
16878 [Impervious area IArea= 1.57:SLIP=1.00:LD= 1311.0:MI= 013:SI= 0]
16879 [IAREClimp= 4.00: IAREKPer= 4.00]
16880 [SIN= 36.47: SMAX=41.49: SK= 010]
16881 R0100:CO0431-----DRAIN-ID:HYD-----AREBA-QPEARCs-TpeakDate,h:mm-----RvM-R-C-----DWFCMs
16882 ADD HYD + 1.0 01:SI_M 30.00 16.228 No_date 27:02 62.82 n/a .000
16883 + 1.0 02:JOCKVA 225.13 28.623 No_date 28:07 62.70 n/a .000
16884 + 1.0 02:MI_M 29.77 16.228 No_date 28:08 56.87 n/a .000
16885 + 1.0 02:SI_M 19.402 No_date 28:04 62.88 n/a .000
16886 SUM+ 1.0 01:JOCKVA 256.41 31.850 No_date 28:06 62.71 n/a .000
16887 R0100:CO0432-----DRAIN-ID:HYD-----AREBA-QPEARCs-TpeakDate,h:mm-----RvM-R-C-----DWFCMs
16888 SAVE HYD 1.0 01:JOCKVA 256.41 31.850 No_date 28:06 62.71 n/a .000
16889 frame :JOCKVA_TO_0100
16890 remark:Total Flows at KB first pond
16891 #*****
16892 # Jockvale SSM Facility
16893 # Rating curve obtained from Jockvale Servicing Study (CC 1999)
16894 #*****
16895 R0100:CO0433-----DRAIN-ID:HYD-----AREBA-QPEARCs-TpeakDate,h:mm-----RvM-R-C-----DWFCMs
16896 ROUTE RESERVOIR + 1.0 01:SI_M 256.41 31.850 No_date 28:06 62.71 n/a .000
16897 out <= 1.0 01:JOCK_P 256.41 12.850 No_date 28:35 62.71 n/a .000
16898 overflow <= 1.0 01:COV-P 0.00 0.00 No_date 0:00 .00 n/a .000
16899 (MxOv=2.43) out <= 1.0 01:SI_M 256.41 12.850 No_date 28:06 62.71 n/a .000
16900 R0100:CO0434-----DRAIN-ID:HYD-----AREBA-QPEARCs-TpeakDate,h:mm-----RvM-R-C-----DWFCMs
16901 ADD HYD + 1.0 02:SI_DE 55196.05 146.071 No_date 37:13 39.51 n/a .000
16902 + 1.0 01:DESIRE 23.78 3.004 No_date 28:03 53.11 n/a .000
16903 + 1.0 02:COV-P 0.00 0.00 No_date 0:00 .00 n/a .000
16904 + 1.0 02:JOCK_P 256.41 12.850 No_date 28:35 62.71 n/a .000
16905 SUM+ 1.0 01:SI_DE 55476.25 147.027 No_date 37:12 39.63 n/a .000
16906 R0100:CO0435-----DRAIN-ID:HYD-----AREBA-QPEARCs-TpeakDate,h:mm-----RvM-R-C-----DWFCMs
16907 SAVE HYD 1.0 01:SI_DE 55476.25 147.027 No_date 37:12 39.63 n/a .000
16908 frame :SN_DE_0100
16909 remark:Total Flows at Heart's Desire
16910 #
16911 # Hydrograph from Heart's Desire routed to Rideau River
16912 # Channel X-Section obtained from RVCA Hydraulic Model - Station 0
16913 #
16914 R0100:CO0436-----DRAIN-ID:HYD-----AREBA-QPEARCs-TpeakDate,h:mm-----RvM-R-C-----DWFCMs
16915 ROUTE CHANNEL + 1.0 02:SI_DE 55476.25 147.027 No_date 37:12 39.63 n/a .000
16916 [RDr= 1.00] out <= 1.0 01:SI 55476.25 147.014 No_date 37:15 39.63 n/a .000
16917 [L/S= 563 / 367.045]
16918 [Vmax= 2.19:Dmax= 1.78]
16919 *****
16920 # Catchment 0-0
16921 # - To Jock River (north and south)
16922 # Undeveloped floodplain and river
16923 #*****
16924 R0100:CO0437-----DRAIN-ID:HYD-----AREBA-QPEARCs-TpeakDate,h:mm-----RvM-R-C-----DWFCMs
16925 CONTINUOUS STANDHYD 1.0 01:0-2 102.94 5.685 No_date 28:20 40.95 .462 .000
16926 [Cm= 72.0: N= 3.00: Tpe= 40]
16927 [IAREC= 4.00: SMAX= 264.99: SK= 010]
16928 [InterEventTime= 12.00]
16929 R0100:CO0438-----DRAIN-ID:HYD-----AREBA-QPEARCs-TpeakDate,h:mm-----RvM-R-C-----DWFCMs
16930 ADD HYD + 1.0 02:MI 55476.25 147.014 No_date 37:15 39.63 n/a .000
16931 + 1.0 02:0-2 102.94 5.685 No_date 28:20 40.95 n/a .000
16932 SUM+ 1.0 01:SI_M 55579.19 147.276 No_date 37:15 39.63 n/a .000
16933 R0100:CO0439-----DRAIN-ID:HYD-----AREBA-QPEARCs-TpeakDate,h:mm-----RvM-R-C-----DWFCMs
16934 SAVE HYD 1.0 01:SI_M 55579.19 147.276 No_date 37:15 39.63 n/a .000
16935 frame :SN_MI_0100
16936 remark:Total Flows at Rideau River
16937 #*****
16938 R0100:CO0502-----DRAIN-ID:HYD-----AREBA-QPEARCs-TpeakDate,h:mm-----RvM-R-C-----DWFCMs
16939 FINISH
16940 *****
16941 *****
16942 *****
16943 *****
16944 R0202:CO0319 ROUTE RESERVOIR ->
16945 *** WARNING: Inflow peak was not reduced! Check OUTFLOW/STORAGE table or reduce DT.
16946 R0202:CO0341 ROUTE PIPE ->
16947 *** WARNING: New pipe size used for routing.
16948 R0202:CO0347 ROUTE PIPE ->
16949 *** WARNING: New pipe size used for routing.
16950 R0202:CO0386 DIVERT HYD ->
16951 *** NOTE: Inflow hyd. is dry and cannot be diverted.
16952 R0202:CO0400 ROUTE PIPE ->
16953 *** WARNING: New pipe size used for routing.
16954 R0202:CO0407 ROUTE PIPE ->
16955 *** WARNING: New pipe size used for routing.
16956 R0202:CO0408 ROUTE PIPE ->
16957 *** WARNING: New pipe size used for routing.
16958 R0202:CO0416 ROUTE PIPE ->
16959 *** WARNING: New pipe size used for routing.
16960 R0202:CO0417 ROUTE PIPE ->
16961 *** WARNING: New pipe size used for routing.
16962 R0205:CO0319 ROUTE RESERVOIR ->
16963 *** WARNING: Inflow peak was not reduced! Check OUTFLOW/STORAGE table or reduce DT.
16964 R0205:CO0341 ROUTE PIPE ->
16965 *** WARNING: New pipe size used for routing.
16966 R0205:CO0347 ROUTE PIPE ->
16967 *** WARNING: New pipe size used for routing.
16968 R0205:CO0363 ROUTE PIPE ->
16969 *** WARNING: New pipe size used for routing.
16970 R0205:CO0364 ROUTE PIPE ->
16971 *** WARNING: New pipe size used for routing.
16972 R0205:CO0372 ROUTE PIPE ->
16973 *** WARNING: New pipe size used for routing.
16974 R0205:CO0386 DIVERT HYD ->
16975 *** NOTE: Inflow hyd. is dry and cannot be diverted.
16976 R0205:CO0395 ROUTE PIPE ->
16977 *** WARNING: New pipe size used for routing.
16978 R0205:CO0400 ROUTE PIPE ->
16979 *** WARNING: New pipe size used for routing.
16980 R0205:CO0407 ROUTE PIPE ->
16981 *** WARNING: New pipe size used for routing.
16982 R0205:CO0408 ROUTE PIPE ->
16983 *** WARNING: New pipe size used for routing.
16984 R0205:CO0416 ROUTE PIPE ->
16985 *** WARNING: New pipe size used for routing.
16986 R0205:CO0417 ROUTE PIPE ->
16987 *** WARNING: New pipe size used for routing.
16988 R0101:CO0341 ROUTE PIPE ->
16989 *** WARNING: New pipe size used for routing.
16990 R0101:CO0347 ROUTE PIPE ->
16991 *** WARNING: New pipe size used for routing.
16992 R0101:CO0363 ROUTE PIPE ->
16993 *** WARNING: New pipe size used for routing.
16994 R0101:CO0364 ROUTE PIPE ->
16995 *** WARNING: New pipe size used for routing.
16996 R0101:CO0372 ROUTE PIPE ->
16997 *** WARNING: New pipe size used for routing.
16998 R0101:CO0386 DIVERT HYD ->
16999 *** NOTE: Inflow hyd. is dry and cannot be diverted.
17000 R0101:CO0395 ROUTE PIPE ->
17001 *** WARNING: New pipe size used for routing.
17002 R0101:CO0400 ROUTE PIPE ->
17003 *** WARNING: New pipe size used for routing.
17004 R0101:CO0407 ROUTE PIPE ->
17005 *** WARNING: New pipe size used for routing.
17006 R0101:CO0408 ROUTE PIPE ->
17007 *** WARNING: New pipe size used for routing.
17008 R0101:CO0416 ROUTE PIPE ->
17009 *** WARNING: New pipe size used for routing.
17009 R0101:CO0417 ROUTE PIPE ->
17010 R0101:CO0417 ROUTE PIPE ->
17011 *** WARNING: New pipe size used for routing.
17012 R0205:CO0341 ROUTE PIPE ->
17013 *** WARNING: New pipe size used for routing.
17014 R0205:CO0347 ROUTE PIPE ->
17015 *** WARNING: New pipe size used for routing.
17016 R0205:CO0363 ROUTE PIPE ->
17017 *** WARNING: New pipe size used for routing.
17018 R0205:CO0364 ROUTE PIPE ->
17019 *** WARNING: New pipe size used for routing.
17020 R0205:CO0372 ROUTE PIPE ->
17021 *** WARNING: New pipe size used for routing.
17022 R0205:CO0380 DIVERT HYD ->
17023 *** NOTE: Inflow hyd. is dry and cannot be diverted.
17024 R0205:CO0385 ROUTE PIPE ->
17025 *** WARNING: New pipe size used for routing.
17026 R0205:CO0400 ROUTE PIPE ->
17027 *** WARNING: New pipe size used for routing.
17028 R0205:CO0407 ROUTE PIPE ->
17029 *** WARNING: New pipe size used for routing.
17030 R0205:CO0408 ROUTE PIPE ->
17031 *** WARNING: New pipe size used for routing.
17032 R0205:CO0416 ROUTE PIPE ->
17033 *** WARNING: New pipe size used for routing.
17034 R0205:CO0417 ROUTE PIPE ->
17035 *** WARNING: New pipe size used for routing.
17036 R0205:CO0341 ROUTE PIPE ->
17037 *** WARNING: New pipe size used for routing.
17038 R0205:CO0347 ROUTE PIPE ->
17039 *** WARNING: New pipe size used for routing.
17040 R0205:CO0380 DIVERT HYD ->
17041 *** NOTE: Inflow hyd. is dry and cannot be diverted.
17042 R0205:CO0386 ROUTE PIPE ->
17043 *** WARNING: New pipe size used for routing.
17044 R0205:CO0372 ROUTE PIPE ->
17045 *** WARNING: New pipe size used for routing.
17046 R0205:CO0380 DIVERT HYD ->
17047 R0205:CO0383 ROUTE PIPE ->
17048 R0205:CO0395 ROUTE PIPE ->
17049 *** WARNING: New pipe size used for routing.
17050 R0205:CO0400 ROUTE PIPE ->
17051 *** WARNING: New pipe size used for routing.
17052 R0205:CO0407 ROUTE PIPE ->
17053 *** WARNING: New pipe size used for routing.
17054 R0205:CO0408 ROUTE PIPE ->
17055 *** WARNING: New pipe size used for routing.
17056 R0205:CO0416 ROUTE PIPE ->
17057 *** WARNING: New pipe size used for routing.
17058 R0205:CO0417 ROUTE PIPE ->
17059 R0205:CO0417 ROUTE PIPE ->
17060 R0100:CO0341 ROUTE PIPE ->
17061 *** WARNING: New pipe size used for routing.
17062 R0100:CO0347 ROUTE PIPE ->
17063 *** WARNING: New pipe size used for routing.
17064 R0100:CO0400 ROUTE PIPE ->
17065 *** WARNING: New pipe size used for routing.
17066 R0100:CO0384 ROUTE PIPE ->
17067 *** WARNING: New pipe size used for routing.
17068 R0100:CO0372 ROUTE PIPE ->
17069 *** WARNING: New pipe size used for routing.
17070 R0100:CO0380 DIVERT HYD ->
17071 *** NOTE: Inflow hyd. is dry and cannot be diverted.
17072 R0100:CO0395 ROUTE PIPE ->
17073 *** WARNING: New pipe size used for routing.
17074 R0100:CO0400 ROUTE PIPE ->
17075 *** WARNING: New pipe size used for routing.
17076 R0100:CO0407 ROUTE PIPE ->
17077 *** WARNING: New pipe size used for routing.
17078 R0100:CO0416 ROUTE PIPE ->
17079 *** WARNING: New pipe size used for routing.
17080 R0100:CO0417 ROUTE PIPE ->
17081 *** WARNING: New pipe size used for routing.
17082 R0100:CO0417 ROUTE PIPE ->
17083 *** WARNING: New pipe size used for routing.
17084 Simulation ended on 2021-03-04 at 12:01:23
17085 *****
17086 *****
17087 *****

```

# Attachment F

Updated Subcatchment Schematics & Tables











- Legend**
- Channel Cross Sections
  - S-1 Sub-catchments and Fraser Sub-catchments
  - S-1 Sub-catchments
  - FRASER-DRN
  - FRASER-D
  - Google Hybrid

File name:  
Figure 4A - S-1 & Fraser Clarke Sub-catchments.pdf

XS 3633 Cross Section at station 3633

S-1-A  
90.84 ha  
Ref. 1

▼ Area ID  
► Area (ha)  
► Reference Number

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**DSEL**  
david schaeffer engineering ltd

PROJECT :  
BCDC - Quantity Control Study

TITLE :  
Figure 4A - S-1 & Fraser Clarke Sub-catchments  
Table 4A - S-1 & Fraser Clarke Sub-catchments

PROJECT NO. 1474-16

DRAWN: MM

DATE: Mar. 2021

Station	Channel Name	Channel Type	Channel Material	Channel Slope	Channel Width	Channel Depth	Channel Velocity	Channel Discharge	Channel Capacity	Channel Status	Channel Notes
3633	S-1-A	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-B	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-C	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-D	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-E	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-F	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-G	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-H	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-I	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-J	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-K	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-L	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-M	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-N	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-O	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-P	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-Q	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-R	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-S	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-T	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-U	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-V	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-W	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-X	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-Y	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	
3633	S-1-Z	Channel	Grass	0.000	1.00	0.50	0.00	0.00	0.00	Open	











- Legend**
- Channel Cross Sections
  - S-1 Sub-catchments and Fraser Sub-catchments
  - S-1 Sub-catchments
  - FRASER-DRN
  - FRASER-D
  - Google Hybrid

File name: Figure 4B - S-1 & Fraser Clarke Sub-catchments.pdf

XS 3633 Cross Section at station 3633

S-1-A Area ID  
 90.84 ha Area (ha)  
 Ref. 1 Reference Number

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**DSEL**  
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PROJECT :  
 BCDC - Quantity Control Study

TITLE :  
 Figure 4B - S-1 & Fraser Clarke Sub-catchments  
 Table 4B - S-1 & Fraser Clarke Sub-catchments

PROJECT NO.	1474-16
DRAWN:	MM
DATE:	Mar. 2021

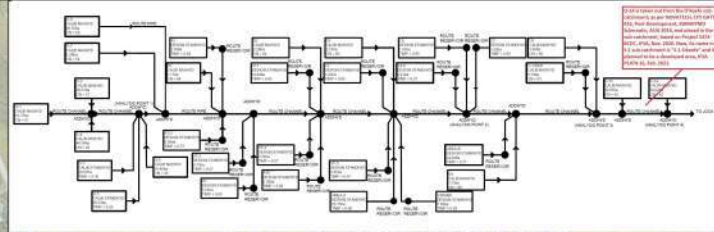
Station	Area (ha)	Reference	Notes
3633	90.84	1	S-1-A
3634	...	...	...
3635	...	...	...
3636	...	...	...
3637	...	...	...
3638	...	...	...
3639	...	...	...
3640	...	...	...
3641	...	...	...
3642	...	...	...
3643	...	...	...
3644	...	...	...
3645	...	...	...
3646	...	...	...
3647	...	...	...
3648	...	...	...
3649	...	...	...
3650	...	...	...
3651	...	...	...
3652	...	...	...
3653	...	...	...
3654	...	...	...
3655	...	...	...
3656	...	...	...
3657	...	...	...
3658	...	...	...
3659	...	...	...
3660	...	...	...
3661	...	...	...
3662	...	...	...
3663	...	...	...
3664	...	...	...
3665	...	...	...
3666	...	...	...
3667	...	...	...
3668	...	...	...
3669	...	...	...
3670	...	...	...
3671	...	...	...
3672	...	...	...
3673	...	...	...
3674	...	...	...
3675	...	...	...
3676	...	...	...
3677	...	...	...
3678	...	...	...
3679	...	...	...
3680	...	...	...
3681	...	...	...
3682	...	...	...
3683	...	...	...
3684	...	...	...
3685	...	...	...
3686	...	...	...
3687	...	...	...
3688	...	...	...
3689	...	...	...
3690	...	...	...
3691	...	...	...
3692	...	...	...
3693	...	...	...
3694	...	...	...
3695	...	...	...
3696	...	...	...
3697	...	...	...
3698	...	...	...
3699	...	...	...
3700	...	...	...











Area ID	Area (ha)	Reference Number	Area ID	Area (ha)	Reference Number
O-1	47.34	1	O-14	5	31
O-2	26.61	2	O-15	11.76	30
O-3	43.68	5	O-16	0.44	16
O-4	43	3	O-17	11.99	15
O-5	64.2	6	O-18	0.72	10
O-6	16.14	4	O-19	3.42	19
O-7	3.67	7	O-20	0.59	20
O-8	48.69	11	O-21	5.69	21
O-9	2.6	9	O-22	68.04	22
O-10	0.99	13	O-23	1.98	23
O-11	3.51	12	O-24	1.78	24
O-12	0.72	10	O-25	0.42	25
O-13	0.99	13	O-26	1.56	26
O-14	5	31	O-27	23.18	27
O-15	11.99	15	O-28	1.94	28
O-16	0.44	16	O-29	8.68	29
O-17	11.99	15	O-30	11.76	30
O-18	0.72	10	O-31	5	31
O-19	3.42	19			
O-20	0.59	20			
O-21	5.69	21			
O-22	68.04	22			
O-23	1.98	23			
O-24	1.78	24			
O-25	0.42	25			
O-26	1.56	26			
O-27	23.18	27			
O-28	1.94	28			
O-29	8.68	29			
O-30	11.76	30			
O-31	5	31			

File name: Figure F1 - O'Keefe Sub-catchments.pdf

20210129-O'Keefe Sub-catchment Boundaries  
 O'Keefe Sub-catchment Boundaries  
 Google Hybrid

Legend  
 XS 7245 Cross Section at station 7245

HYDROLOGIC MODELING (SWHYMO) ANALYSIS POINT  
 ENVIRONMENTAL MANAGEMENT (EMP) ANALYSIS POINT  
 S1 - E1  
 Area ID  
 Area (ha)  
 Reference Number  
 STA. 1840.6 CROSS SECTION AND STATION

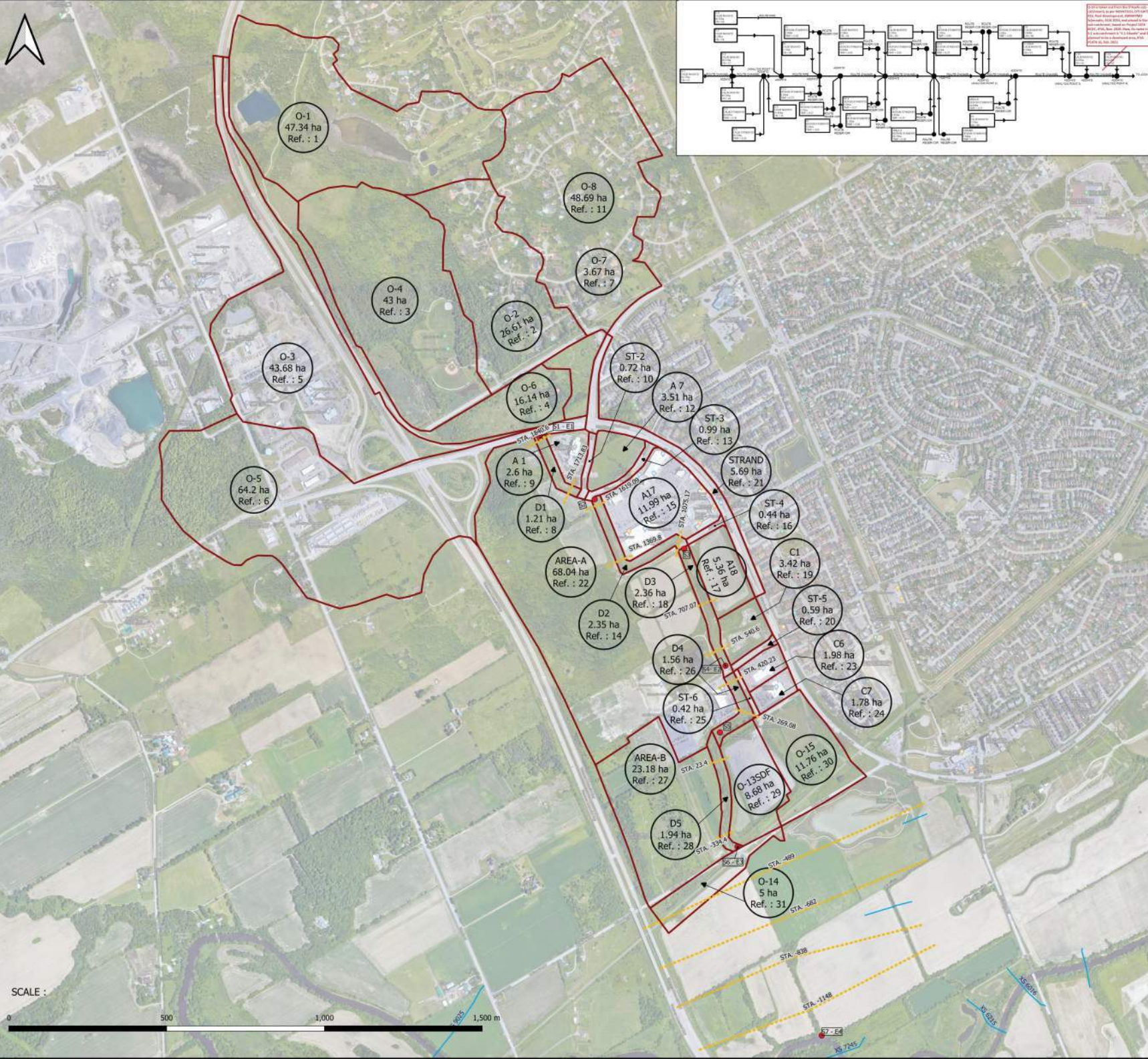
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PROJECT :  
 BCDC - Quantity Control Study

TITLE :  
 Figure F1 - O'Keefe Sub-catchments  
 Table F1 - O'Keefe Sub-catchments  
 Schematic F1 - O'Keefe Sub-catchments

PROJECT NO.	1474
DRAWN:	MM
DATE:	Mar. 2021









Ref.	Name ID	Area (ha)	Major System To	Minor System To	T. Imperv.	XIMP	CN	LGI: Length (m) =SQRT (Area*10000/1.5)	Slope (%)		ROUTE RESERVOIR					ROUTE CHANNEL (Station 6016)					
									SLPP (Pervious)	SLPI (Impervious)	NHYDin	NHYDout	NHYDovf (OVERFLOW)	Outflow (cms)	Storage (ha-m)	NHYDin	NHYDout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)
1	FOSTER	325.44	FOSTER-OUT = ["P_FOS"+"FO-OVF"]		0.55	0.55	74	1472.956211	0.5	0.5	FOSTER	P_FOS	FO-OVF	10.34	10	SN_FO (Total Flows at Foster Drain)	N_CE	159	0.0818	-645.23	91.5
																				-391.2	91.5
																				-91	91.5
																				-85.52	91.5
																				-15.46	89.4
																				-9.79	89.31
																				-3.22	86.24
																				3.22	85.07
																				10.96	85.79
																				16.44	86.49
																				26.55	89.45
																				29.03	90.27
																				35.76	90.67
																				36.67	91
																				108.08	91
																				109.82	90.5
																				112.04	90.5
																				114.62	91
																				116.76	91.5





Ref.	Route ID (Link Sub-catchment)	Area (ha)	Major System To	Minor System To	T. Imperv. FIP (%)	XIMP	CR	Slope (%)	ROUTE RESERVOIR			ROUTE CHANNEL (Station #348)											
									WYDIn	WYDOut	WYDDef (OVERFLOW)	WYDIn	WYDOut	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)						
1	W_CLAR_MJ	1,772	Clarke	Todd	0.50	0.80	77	109		W_CLAR_MJ	W_CLAR_Min	W_CLAR_MJ	0.213	0.0001*									
2	W_CLAR_ALL	119,338	Clarke		0.05	0.4	77	892.18	1	W_CLAR = W_CLAR_ALL + W_CLAR_MJ	MS_P2	P2-OVF	0.128	0.351									
													0.138	0.409									
													0.149	0.468									
													0.177	0.561									
													0.234	1.223									
													0.305	1.32									
													0.486	1.821									
													0.881	2.125									
													0.995	2.434									
													1.089	2.383									
1.51	2.647																						
4.884	2.861																						
13.048	3.188																						
23.745	3.523																						
36.476	3.871																						
42.989	4.227																						
51.652	4.589																						
3	W_CLAR_UNDE	35.65	Jock River (Station 4534)				77																
	Total	156.83																					

\* Small storage was assumed to allow overflow and direct the flow towards minor and major systems  
 \*\* N\_WC is AFFDOut from ROUTE CHANNEL at Channel X-Section obtained from RIVICA Hydraulic Model - Station 5062 (Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain)

**Legend**

- Channel Cross Sections
- SWMF Drains
  - Brazeau & Clarke Undeveloped
  - Clarke
- SWMF ponds
  - West Clarke
  - Brazeau
- Clarke Sub-catchment & Brazeau Sub-catchment
  - W\_CLAR\_MJ
  - W\_CLAR\_MJ (Major Only to Clarke SWM Pond)
  - W\_CLAR\_ALL
  - W\_CLAR\_BRAZ
  - W\_CLAR\_UNDE
  - Clarke-Brazeau-CAD
- Google Hybrid

File name: Figure F3 - Clarke & Brazeau Sub-catchments.pdf

XS 4534 Cross Section at station 4534 Minor System

W\_CLAR\_MJ (Major Only to Clarke SWM Pond) 1,772 ha & Ref. 1

- Area ID
- Reference Number
- Area (ha)

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PROJECT : BCDC - Quantity Control Study

TITLE : Figure F3 - Clarke & Brazeau Sub-catchments  
 Table F3-1 - Clarke Sub-catchments  
 Figure F3-2 - Brazeau Sub-catchment

PROJECT NO.	1474-16
DRAWN:	MM
DATE:	Mar. 2021

Area	Route ID (Link Sub-catchment)	Area (ha)	Major System To	Minor System To	T. Imperv. FIP (%)	XIMP	CR	Slope (%)	ROUTE RESERVOIR		ROUTE CHANNEL (Station #348)											
									WYDIn	WYDOut	WYDDef (OVERFLOW)	WYDIn	WYDOut	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)					
4	W_CLAR_BRAZ	73.29	Clarke	Todd	0.05	0.4	77	89	1	W_CLAR_BRAZ	MS_P2	P2-OVF	0.088	0.301								
													0.271	0.583								
													0.576	0.911								
													0.88	0.983								
													0.851	0.943								
													1.288	0.93								
													1.838	1.043								
													2.253	1.282								
													1.194	1.476								
													1.1	1.851								
1.233	1.389																					
1.1	1.885																					
1.388	2.023																					

\* Small storage was assumed to allow overflow and direct the flow towards minor and major systems



Ref.	Name ID (Clarke Sub-catchment)	Area (ha)	Major System To	Minor System To	T. Imperv. [TP (hr)]	XIMP	CN	LGI: Length (m) =SQRT (Area*10000/1.5)	Slope (%)	ROUTE RESERVOIR					ROUTE CHANNEL (Station 4534)						
										NHYDin	NHYDout	NHYDovf (OVERFLOW)	Outflow (cms)	Storage (ha-m)	NHYDin	NHYDout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)	
1	W_CLAR_MJ	1.772	Clarke	Todd	0.59	0.46	77	109	1	W_CLAR_MJ	W_CLAR_MJn	W_CLAR_MJj	0.213	0.0001*							
2	W_CLAR_ALL	119.398	Clarke		0.65	0.6	77	892.18	1	W_CLAR = W_CLAR_ALL + W_CLAR_MJj	MS_P2	P2-OVF	0.128	0.161	N_WC**	N_KB	1020	0.0498			
													0.138	0.409					-1082.01	94	
													0.148	0.68					-1028.17	92.5	
													0.227	0.931					-992.3	93.5	
													0.354	1.223					-279.34	90	
													0.505	1.52					-23.63	90	
													0.666	1.821					-13.45	87.13	
													0.831	2.123					-0.07	86.24	
													0.995	2.434					10.54	87.15	
													1.069	2.583					23.63	90	
													1.51	2.647					24.86	90.5	
													4.904	2.861					26.72	91	
													13.048	3.188					45.07	91.5	
													23.745	3.523					128.17	91.5	
36.474	3.871	270.7	92.5																		
45.938	4.127	728.3	95																		
61.652	4.539																				
3	W_CLAR_UNDE	35.65	Jock River (Station		[1.10]		77														
Total		156.82																			

\* Small storage was assumed to allow overflow and direct the flow towards minor and major systems

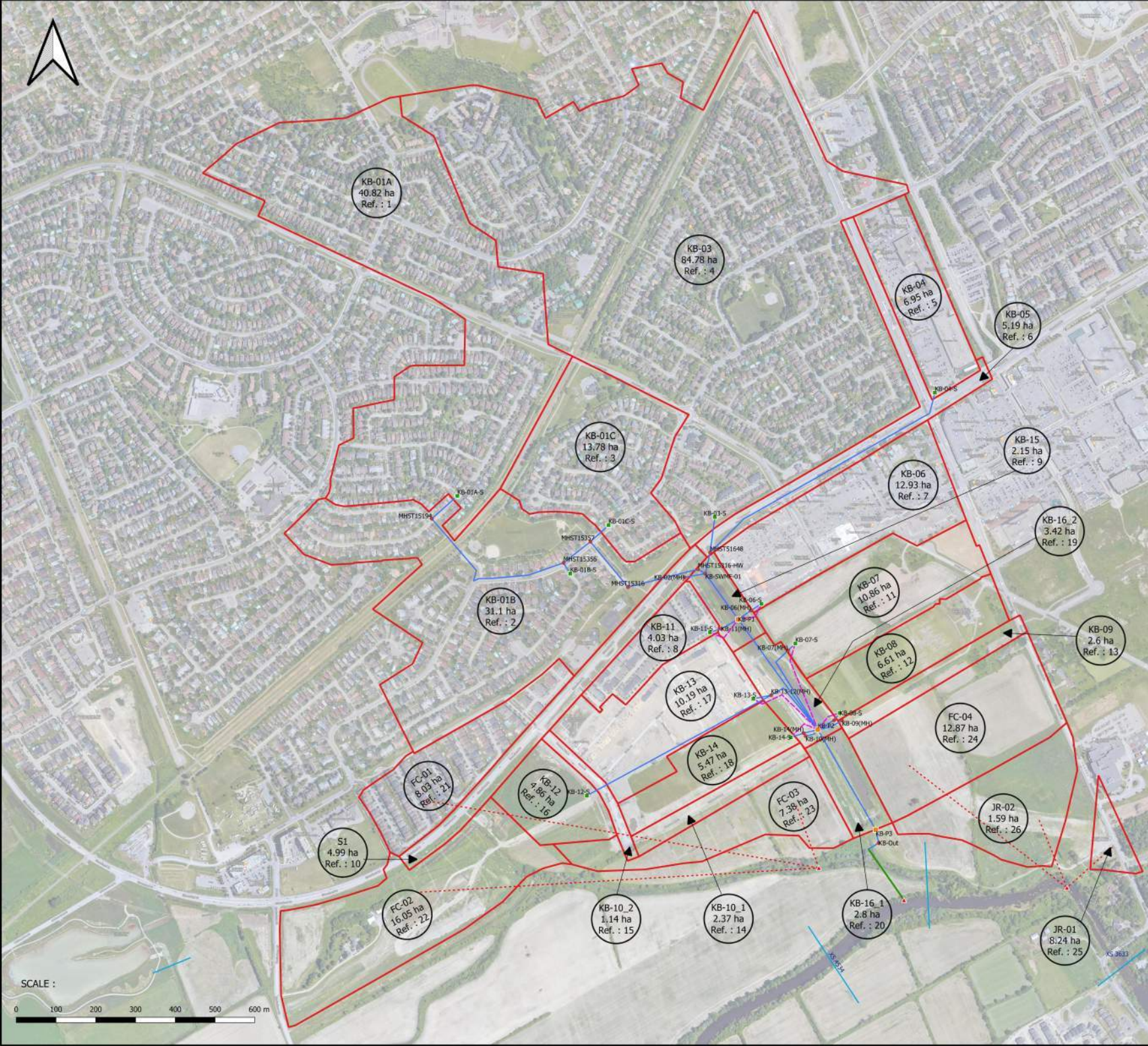
\*\* N\_WC is NHYDout from ROUTE CHANNEL at Channel X-Section obtained from RVCA Hydraulic Model - Station 5002 (Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain)

Ref.	ID (Brazeau Sub-catchment)	Area (ha)	Major System To	Minor System To	T. Imperv. [TP (hr)]	XIMP	CN	LGI: Length (m) =SQRT (Area*10000/1.5)	Slope (%)		ROUTE RESERVOIR					ROUTE CHANNEL (Station 6016)					
									SLPP (Pervious)	SLPI (Impervious)	NHYDin	NHYDout	NHYDovf (OVERFLOW)	Outflow (cms)	Storage (ha-m)	NHYDin	NHYDout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)
4	W_CLAR_BRAZ	73.29	Pond in Brazeau which drains to Jock River (station 6016)*		0.65	0.6	77	699	1	0.5	W_CLAR_BRAZ	MS_P10	P10-OVF	0.068	0.001	SN_FO (Total Flows at Foster Drain)	N_CE**	159	0.0818	-645.23	91.5
														0.271	0.022					-391.2	91.5
														0.379	0.051					-91	91.5
														0.48	0.091					-85.52	91.5
														0.853	0.341					-15.46	89.4
														1.005	0.61					-9.79	89.31
														1.128	1.231					-3.22	86.24
														1.155	1.592					3.22	85.07
														1.194	1.876					10.96	85.79
														1.2	1.921					16.44	86.49
														1.259	2.369					26.55	89.45
														1.3	2.665					29.03	90.27
														1.349	2.813					35.76	90.67
																				36.67	91
																				108.08	91
		109.82	90.5																		
		112.04	90.5																		
		114.62	91																		
		116.76	91.5																		
Total		73.29																			

\* Brazeau pond discharges directly to the jock river through a road side ditch on the west side of Borrisokane road (station 6016)

\*\* N\_CE is NHYDout from ROUTE CHANNEL at Channel X-Section obtained from RVCA Hydraulic Model - Station 6016 (Hydrograph from Node Foster routed to Node at Cedarview Road)





Area ID	Area (ha)	Reference Number
KB-01A	40.82	1
KB-01B	31.1	2
KB-01C	13.78	3
KB-03	84.78	4
KB-04	6.95	5
KB-05	5.19	6
KB-06	12.93	7
KB-07	10.86	11
KB-08	6.61	12
KB-09	2.6	13
KB-10_1	2.37	14
KB-10_2	1.14	15
KB-11	4.03	8
KB-12	4.86	16
KB-13	10.19	17
KB-14	5.47	18
KB-15	2.15	9
KB-16_1	2.8	20
KB-16_2	3.42	19
FC-01	8.03	21
FC-02	16.05	22
FC-03	7.36	23
FC-04	12.87	24
JR-01	8.24	25
JR-02	1.59	26
S1	4.99	10

- Legend**
- Ken-BU storage
  - Ken-BU MH
  - ▲ Ken-BU Pond
  - ▲ Ken-BU Outfalls
  - Ken-BU Pipe
  - Ken-BU Major System
  - Ken-BU Channel
  - Ken-BU to FC (Fraser Clarke) and JR(Jock River)
  - Kennedy Burnett Sub-catchment
  - Kennedy Burnett (Ken-BU)
  - Google Hybrid

File name: Figure F4 - Kennedy Burnett Sub-catchments.pdf



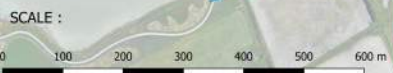
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PROJECT :  
 BCDC - Quantity Control Study

TITLE :  
 Figure F4 - Kennedy Burnett Sub-catchments  
 Table F4 - Kennedy Burnett Sub-catchments

PROJECT NO.	1474
DRAWN:	MM
DATE:	Mar. 2021











Ref.	Name ID (Todd)	Area (ha)	Major System To	Minor System To	T. Imperv.	XIMP	CN	LGI: Length (m) =SQRT (Area*10000/1.5)	Slope (%)	ROUTE RESERVOIR					ROUTE CHANNEL (Station 2462)					
										NHYDin	NHYDout	NHYDovf (OVERFLOW)	Outflow (cms)	Storage (ha-m)	NHYDin	NHYDout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)
1	TODD_MN2	2.1	Jock River (Station 2462)	Todd	0.57	0.53	77	118.322	1	TODD_MN2	TODD_MN2n	TODD_MN2j	0.268	0.0001*						
2	TODD_MN3	0.117	Corrigan	Todd	0.57	0.53	77	27.928	1	TODD_MN3	TODD_MN3n	TODD_MN3j	0.016	0.0001*						
3	TODD_MJ	30.23	Todd	Corrigan	0.64	0.52	77	448.925	1	TODD_MJ	TODD_MJn	TODD_MJj	3.314	0.0001*						
4	TODD_ALL	112.908	Todd	Todd	0.57	0.52	77	867.594	1											
5	TODD_P	3.055	Todd	Todd	0.63	0.63	77	142.712	1	"TODD" = ["TODD_MN2n"+ "TODD_MN3n"+ "TODD_MJj"+ "TODD_P"+ "TODD_ALL"+ "W_CLAR_MJn"***]	MS_P3	P3-OVF	0.014 0.048 0.061 0.08 0.088 0.109 0.118 0.122 1.972 9.135 15.608 19.256 27.282 40.957 56.372 73.349 85.469 104.771	0.155 0.394 0.56 0.909 1.089 1.652 1.952 2.099 2.269 2.598 2.826 2.942 3.181 3.55 3.929 4.317 4.579 4.977	SN_TO = ["GreenB" (Greenbank Pond)+ "MS_P3"+"P3-OVF"+ "TODD_MN2j"+ "A2-MJ"***]	N_TO	280	0.033	-83.32 -81.36 -79.12 -76.13 -20.46 -19.36 -18.51 -17.72 -11.95 -0.11 11.49 17.72 19.74 21.22 22.68 24.28 26.79 71.98 80.62	90 89.5 89 88.5 88 87.5 87 86.5 85.24 85.12 85.2 86.5 87 87.5 88 88.5 89 90 90.5
Total		148.41																		

\* Small storage was assumed to allow overflow and direct the flow towards minor and major systems

\*\* "W\_CLAR\_MJn" is the minor system from the major system area(Area = 1.772 ha & TIMP = 0.59 & XIMP = 0.46 & CN = 75 & Slope = 1% & Outflow = 0.213 cms)in Clarke sub-catchment (Schematic 3) to Jock River (Station 2462)

\*\*\* "A2-MJ" is the major system from A2 area (Area = 25.5 ha & TIMP = 0.52 & XIMP = 0.42 & CN = 75 & Slope = 1% & Storage = 924 cu-m & Flow rate = 1.818 cms ) in Corrigan sub-catchment (Schematic 1) to Todd sub-catchment











1. O'KEEFE MUNICIPAL DRAIN – APPOINTMENT OF ENGINEER  
DRAIN MUNICIPAL O'KEEFE– NOMINATION D'UN INGÉNIEUR

**COMMITTEE RECOMMENDATION**

That Council appoint Mr. Andy Robinson, P. Eng of Robinson Consultants Inc. as the Engineer of record to prepare a report under Section 78 (1) of the *Drainage Act* to inform Council on the current status of the O'Keefe Municipal Drain and whether one or more of the projects listed under Section 78 (1.1) is required for the better use, maintenance or repair of the drainage works or lands or roads.

**RECOMMANDATION DU COMITÉ**

Que le Conseil nomme M. Andy Robinson, ing., de la firme Robinson Consultants Inc., comme ingénieur chargé de rédiger un rapport aux termes du paragraphe 78(1) de la *Loi sur le drainage* afin de renseigner le Conseil sur l'état actuel du drain municipal O'Keefe et de lui indiquer si un ou plusieurs des projets énumérés au paragraphe 78(1.1) sont nécessaires pour faciliter l'utilisation, l'entretien ou la remise en état des installations de drainage, des terrains ou des routes.

**Documentation/Documentation**

1. Director's report, Parks, Forestry & Stormwater Services, dated April 30, 2021 (ACS2021-PWE-PFS-0005)  
Rapport de la Directrice, Services des parcs, de la foresterie et des eaux pluviales, daté le 30 juin 2021 (ACS2021-PWE-PFS-0005)

**AGRICULTURE AND RURAL  
AFFAIRS COMMITTEE  
REPORT 22  
JUNE 9, 2021**

**16**

**COMITÉ DE L'AGRICULTURE ET  
DES AFFAIRES RURALES  
RAPPORT 22  
LE 9 JUIN 2021**

**Report to  
Rapport au:**

**Agriculture and Rural Affairs Committee  
Comité de l'agriculture et des affaires rurales  
3 June 2021 / 3 juin 2021**

**and Council  
et au Conseil  
9 June 2021 / 9 juin 2021**

**Submitted on April 30, 2021  
Soumis le 30 avril 2021**

**Submitted by  
Soumis par:**

**Allyson Downs, Director, Parks, Forestry & Stormwater Services / Directrice,  
Services des parcs, de la foresterie et des eaux pluviales**

**Contact Person**

**Personne ressource:**

**Dave Ryan, Drainage Superintendent  
613-580-2424, x25106 David.Ryan@ottawa.ca**

**Ward: BARRHAVEN (3)**

**File Number: ACS2021-PWE-PFS-0005**

**SUBJECT: O'Keefe Municipal Drain – Appointment of Engineer**

**OBJET: Drain municipal O'Keefe– Nomination d'un ingénieur**

## **REPORT RECOMMENDATIONS**

**That the Agriculture and Rural Affairs Committee recommend that Council appoint Mr. Andy Robinson, P. Eng of Robinson Consultants Inc. as the Engineer of record to prepare a report under Section 78 (1) of the Drainage Act to inform**

**Council on the current status of the O'Keefe Municipal Drain and whether one or more of the projects listed under Section 78 (1.1) is required for the better use, maintenance or repair of the drainage works or lands or roads.**

**RECOMMANDATIONS DU RAPPORT**

**Que le Comité de l'agriculture et des affaires rurales recommande au Conseil de nommer M. Andy Robinson, ing., de la firme Robinson Consultants Inc., comme ingénieur chargé de rédiger un rapport aux termes du paragraphe 78(1) de la *Loi sur le drainage* afin de renseigner le Conseil sur l'état actuel du drain municipal O'Keefe et de lui indiquer si un ou plusieurs des projets énumérés au paragraphe 78(1.1) sont nécessaires pour faciliter l'utilisation, l'entretien ou la remise en état des installations de drainage, des terrains ou des routes.**

**BACKGROUND**

Development is proposed on multiple parcels of land within the existing watershed of the O'Keefe Municipal Drain which may result in changes in the land use, surface, subsurface and storm water flows from the existing parcels of land. The proposed developments are located in Part of Lots 14 and 15, Concession 4 former Township of Nepean, Barrhaven Ward.

A Drainage Engineer will be required to examine the proposed development within Part of Lots 14 and 15, Concession 4 former Township of Nepean, Barrhaven Ward, to determine the proposed changes to the extent and nature of use within the watershed of the O'Keefe Municipal Drain. An engineer's report will be required in order to address any work required due to the potential improvements required to address the developer's proposed changes.

The original O'Keefe Municipal Drain is located in Part Lots 14 to 20, Concession 4, former Township of Nepean, Barrhaven Ward and was first constructed in 1967 by the former Township of Nepean under the engineer's report prepared by Graham, Berman and Associates Ltd. dated October 10, 1967 By-law 17-68. Modifications to the existing O'Keefe Municipal Drain by Robinson Consultants Inc. were adopted under engineer's reports, the first modification dated March 2006 and By-law No. 2006-389, the second modification dated March 2015 and By-law No. 2016-149 and the third modification dated November 2018 and By-law No. 2019-281.



## **DISCUSSION**

The O'Keefe Municipal Drain is a private communal drainage system which has legal status under the provincial *Drainage Act*, RSO 1990 c.17. As such, any changes to the drainage works requires the approval of Council based on the report of a qualified Drainage Engineer, pursuant to Section 78 of the *Act*. The City's Drainage Superintendent is recommending the appointment of Andy Robinson, P.Eng., a qualified Drainage Engineer from Robinson Consultants Inc., as the engineer of record as he has experience with similar *Drainage Act* projects, a specialized field of engineering in Ontario. He was also involved in the 2006, 2015 and 2018 Engineer's Reports on this drainage works.

This report has no tax or budget implications. All costs associated with the engineer's report will be initially paid by the Parks, Forestry and Stormwater Services Branch of the Public Works and Environmental Services Department but eventually recovered from the owners of land as determined by the Engineers' Report. The Engineers' Report will include an updated assessment for each parcel of land within the existing watershed of the O'Keefe Municipal Drain for a proportion of the costs of any drainage works projects that the drainage engineer determines is required under subsection 78 (1.1).

Under the *Drainage Act*, all lands that will benefit from the drainage works are assigned an assessment by the engineer. "Benefit" is defined under the *Drainage Act* as the advantages to any lands from the construction, improvement, repair or maintenance of a drainage works such as will result in a higher market value or increased crop production or improved appearance or better control of surface or subsurface water, or any other advantages relating to the betterment of the lands.

As such, the lands that benefit the most from improved drainage as a result of a Subsection 78 (1.1) project will be assessed a greater proportion of the costs of the project.

The estimated initial engineering cost of the report is \$100,000. Until the costs are recovered from the owners of the assessed lands, all costs associated with the preparation of the engineer's report, engineering, administration, implementation and regulatory documentation required to complete any improvements recommended by the

engineer and approved by Council, will be paid from the 2021 approved capital budget for the Municipal Drains Program for the cost of the engineer's report.

The *Drainage Act* prescribes the process and timelines to be followed for any variations in assessments within the Engineer's Report of an existing Petition Drain.

This report places the request for an Engineer's Report on the current status of the O'Keefe Municipal Drain and whether one or more of the projects listed under Section 78 (1.1) is required for the better use, maintenance or repair of the drainage works or lands or roads before the Agriculture and Rural Affairs Committee and Council as required under Section 78(1) of the *Drainage Act*.

### **RURAL IMPLICATIONS**

The proposed development will benefit from this undertaking through the provision of legal and sufficient outlet, improved drainage and reduced risk of flooding.

### **CONSULTATION**

Consultation with the Ward Councillor and City staff is ongoing.

### **COMMENTS BY THE WARD COUNCILLOR(S)**

The Councillor is aware of this report.

### **LEGAL IMPLICATIONS**

There are no legal impediments to Committee and Council's approval of the recommendation of this report.

### **RISK MANAGEMENT IMPLICATIONS**

There are no risk implications associated with this report.

### **FINANCIAL IMPLICATIONS**

This report has no tax or budget implications. The estimated initial cost of \$100,000 for the Engineer's Report will be initially paid by the City of Ottawa, Parks, Forestry and Stormwater Services of the Public Works and Environmental Services Department and

recovered, as per the assessment schedule included in the final Engineer's Report. Funds are available in the 2021 approved Capital Budget - Municipal Drainage Program.

### **ACCESSIBILITY IMPACTS**

There are no accessibility impacts associated with this report.

### **ENVIRONMENTAL IMPLICATIONS**

The modifications to the O'Keefe Municipal Drain are associated with proposed development. Any proposed works will require compliance with City, provincial and federal policies, standards, regulations and legislation.

### **TERM OF COUNCIL PRIORITIES**

The recommendations of this report align with the current Strategic Priority as part of the sustainable environmental services strategic priority by supporting an environmentally sustainable Ottawa.

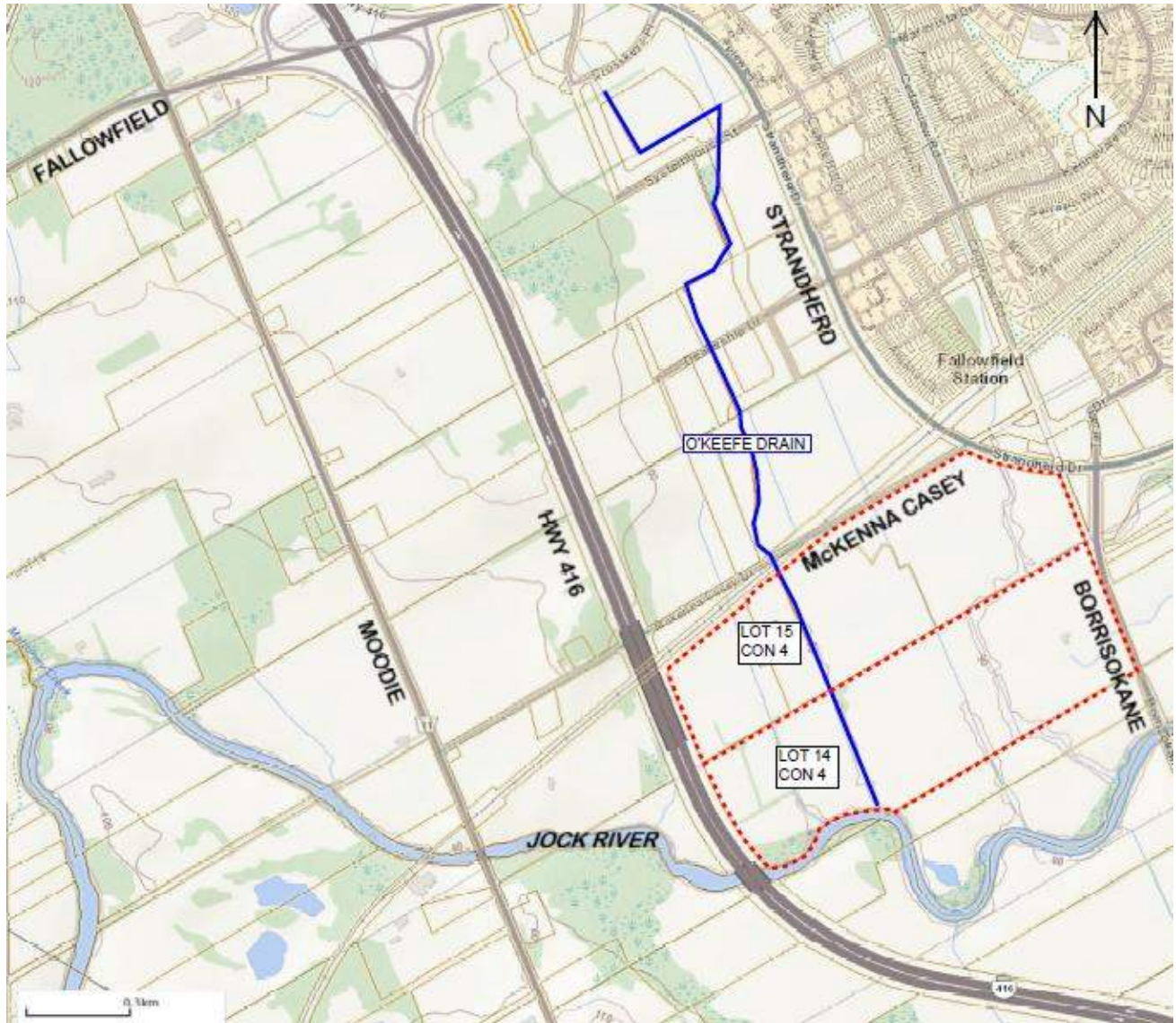
### **SUPPORTING DOCUMENTATION**

DOCUMENT 1 – Location Plan

### **DISPOSITION**

Once approved by Council, a separate new internal order will be created for this specific drain and all necessary funding will be transferred accordingly.

Document 1





October 21, 2021

Project Number: 1474

David Schaeffer Engineering Ltd  
120 Iber Road, Unit 103  
Ottawa, Ontario  
K2S 1E9

**Attention: Steve Pichette, P.Eng**

**Subject: BCD Phase 3 (Conservancy West) – Preliminary Water Balance**

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## Introduction

Phase 3 (Conservancy West) of the Barrhaven Conservancy Development is located in Barrhaven, Ontario, north of the Jock River, east of Highway 416 and west of the Foster Creek. The proposed development is approximately 35.6 ha that will primarily comprise of single and townhouse residential lots along with a 3.54 ha of parks. The following memo outlines how the proposed development will match/exceed the existing water budget through the use of LIDs.

## Water Balance Overview

A pre-and post-development water balance has been completed for the site based on continuous hydrologic model simulations. As such a SWMHYMO model was developed that reflects the hydrologic conditions of these lands under pre-development, post-development without LIDs and post-development with LIDs conditions. These models were run using 36 years of hourly rainfall data from the Ottawa International Airport from 1967 to 2003 (excluding 2001 - missing rainfall data), the average annual runoff volumes from the subject site were computed and compared. Table A1 in Attachment A outlines the continuous modelling parameters for both pre and post-development conditions. The following section outlines the modelling approach for each scenario and the results of this analysis.

## Pre-Development

Based on the Soil Survey Complex mapping from the Ontario Ministry of Agriculture, Food, and Rural Affairs (OMAFRA) the site primarily consists of Carsonby - Silt (Type C) and Brandon -Silty Clay- (Type D) Soils. This was confirmed by Paterson Groups through onsite field investigations and boreholes which also reported Silt and Silty Clays through the majority of the site.

Based on the Southern Ontario Land Resource Information System (SOLRIS) the site consists primarily of tilled lands and hedgerows. Based on the underlying Land Use Type and Soil Classification at each location within a subcatchment, a Curve Number (CN) was calculated, based on applicable values outlined in Tables A2 and A3 in the SWMHYMO Manual. Each Curve Number was then weighted based on the total area within the subcatchment to determine the weighted CN for that subcatchment. The CN value calculated was then converted to CN\*, as CN\* values have been shown to correlate well with measured flows and perform well in continuous SWMHYMO modelling (as discussed in the July 1989 INTERHYMO / OTTHYMO 89 Manual), when compared to conventional CN. Full details of the derivation of CN under existing conditions have been outlined in Table A2 and Figures A1 & A2 in Attachment A.



For this area, the time to peak has been calculated based on existing topography. Flow paths have been discretized based on the topographic data using GIS tools and the longest major flow path within the subcatchment identified; refer to Figure A3 in Attachment A for the flow paths discretized for these lands. The upstream and downstream topographic elevations and flow lengths were identified for this subcatchment and used in the calculations. For these lands, the Federal Aviation Administration (FAA) method was determined to be the most appropriate method to calculate the Time to Peak. Full details of these calculations have been provided in Table A3 in Attachment A, along with other time to peak values using alternative calculation methods. This site under pre-development conditions has been represented in SWMHYMO using a CONTINUOUS NASHYD command, with all continuous parameters outlined in Table A1 of Attachment A.

### Post-Development – Without LIDs

Under post-development conditions, the site will have 4 individual storm sewer outlets, as such the development lands have been broken into these 4 discrete areas (with a total drainage area of 35.6 ha, matching existing conditions). Based on the development conceptual plan, the 35.6 ha site will have a total imperviousness of 64%, see figure A4 in Attachment A for an overview of the proposed development plan. These developed lands have been represented using CONTINUOUS STANDHYD commands in SWMHYMO, with City default Horton infiltration parameters for urban developments of  $F_o=76.2$  mm/hr,  $F_c=13.2$  mm/hr,  $DCAY=4.14$  /hr,  $F=0$  mm applied. This scenario has been provided to quantify the average annual reduction in infiltration volume throughout the site due to the increase in impervious area.

### Post-Development – With LIDs

As mentioned above the proposed development will have LIDs implemented throughout the site to offset any deficit in annual infiltration volume produced by the increase in the impervious area due to the development. For this analysis, it is assumed that the development will have infiltration LIDs implemented at the road catch basins. Runoff captured by the road catch basins will be directed to an infiltration trench, where it can infiltrate before discharging to the storm sewer system (see Figure 5 in DSEL Figures & Drawings package for more details about the proposed LID configuration). A conceptual design of these LIDs systems has been completed but will be refined at detailed design when detailed grading is available, to yield optimal benefit from this LID approach. Table 1 below outlines the parameters of these conceptual LIDs based on the current development plan. Each of the LID clusters have been represented in the model as single lumped ROUTE RESERVOIR commands, with the outflow of each command reflective of the soil infiltration rate and the volume reflective of the storage volume within each LID.

### Soil Infiltration & Draw Down Time

Based on the Paterson Groups geotechnical Investigation, the site consists of soil that typically has infiltration rates in the range of 9 mm/hr - 25 mm/hr. As such it has been assumed that this site will have an infiltration rate of 9mm/hr with a safety factor of 2.5 (3.6 mm/hr). based on a trench height of 0.4m (with a void ratio of 0.4) these trenches will have a draw downtime of approximately 45 hours. Note that in this analysis it is assumed that only the bottom of the trench can infiltrate, which is a conservative assumption.

Table 1: Proposed LID Summary

Parameter	OGS W1	OGS W2	OGS W3	OGS W4
Area (ha)	8.92	8.22	9.9	8.6
Runoff Coefficient	0.65	0.65	0.65	0.65
Pipe Length (m)	1991	1896	1693	1693
Pipe Dia (mm)	250	250	250	250
Perf. Pipe Length (m)	1500	1440	1320	1320
Pipe Vol. (m <sup>3</sup> )	73.6	70.7	64.8	64.8
Trench Width (m)	1.25	1.25	1.25	1.25
Trench Height (m)	0.4	0.4	0.4	0.4
Trench Length (m)	30	30	30	30
Void Ratio	0.4	0.4	0.4	0.4
Trench Vol. (m <sup>3</sup> )	270.55	259.73	238.08	238.08
Total Vol. (m <sup>3</sup> )	344	330	303	303
Area of Trench (m <sup>2</sup> )	1875	1800	1650	1650
# of CB's	50	48	44	44
Soil Infiltration Rate (mm/hr)	9	9	9	9
Safety Factor	2.5	2.5	2.5	2.5
Reduced Rate (mm/hr)	3.6	3.6	3.6	3.6
Infiltration rate (m <sup>3</sup> /hr)	0.001875	0.0018	0.00165	0.00165

## Water Budget Scenario Summary

The models were run for 36 years using hourly rainfall data from the Ottawa Airport, and the annual evaporation, infiltration and runoff volumes calculated for each scenario. Tables 2-4 summarize the annual average water balance under existing conditions and post-development conditions for the proposed development lands with and without LID measures in place, as m<sup>3</sup>/year, mm/year and % of total annual rainfall.

**Table 2:Pre-Development Water Balance**

Drainage Area (ha)		35.64	Imperviousness:	7%
Annual Average Volume	Precipitation	Evapotranspiration	Runoff	Infiltration
m <sup>3</sup>	212,328	121,651	14,501	76,176
mm	596	341	41	214
%	100%	57.3%	6.8%	35.9%

**Table 3:Post Development Water Balance – Without LIDs**

Drainage Area (ha)		35.64	Imperviousness:	64%
Annual Average Volume	Precipitation	Evapotranspiration	Runoff	Infiltration
m <sup>3</sup>	212,328	77,264	88,035	47,029
mm	596	217	247	132
%	100.0%	36.4%	41.5%	22.1%

**Table 4:Post Development Water Balance – With LIDs**

Drainage Area (ha)		35.64	Imperviousness:	64%
Annual Average Volume	Precipitation	Evapotranspiration	Runoff	Infiltration
m <sup>3</sup>	212,328	77,264	43,497	91,567
mm	596	217	122	257
%	100%	36.4%	20.5%	43.1%

Based on this analysis of pre-development conditions this site will evaporate 57.3%, runoff 6.8% and infiltrate 35.9% of all annual rainfall. Under Post-development conditions without LIDs, this site will evaporate 36.4%, runoff 41.5% and infiltrate 22.1% of all annual rainfall, resulting in a deficit of 82 mm/year infiltrated from pre-development conditions. Under post-development conditions with LIDs, this site will evaporate 36.4%, runoff 20.5% and infiltrate 43.1% and of all annual rainfall, resulting in an excess of 43 mm/year, exceeding existing pre-development infiltration rates. Full annual breakdowns of the three conditions have been provided in Attachment B, tables B1-B3. An average annual summary of the infiltration volume for each of the proposed LID measures is outlined in Table B4, which shows that the LIDs alone provide a total average annual infiltration volume of 125 mm/year.

## Conclusion

A preliminary water balance analysis of the existing site was completed to determine pre-development infiltration rates, based on continuous hydrologic model simulations. A post-development analysis for the site, where no LIDs were implemented, showed that the volume of annual rainfall infiltrated would decrease by 82 mm/yr. (-38% from existing). Implementing LIDs in the way of infiltration trenches connected to the catchbasins would offset this deficit and exceed pre-development conditions by 43mm/year (+20% from existing). Based on the above it has been shown that Phase 3 of the Barrhaven Conservancy Development will be able to meet pre-development infiltration rates under post-development conditions through the use of LIDs.

Yours truly,

**J.F Sabourin and Associates Inc.**



Jonathon Burnett, P.Eng  
Water Resources Engineer

cc: J.F Sabourin, M.Eng, P.Eng  
Director of Water Resources Projects



## Tables

- Table 1: Proposed LID Summary
- Table 2: Pre-Development Water Balance
- Table 3: Post Development Water Balance – Without LIDs
- Table 4: Post Development Water Balance – With LIDs

## Attachments

- Attachment A: SWMHYMO Models & Parameters
- Attachment B: Water Budget Results



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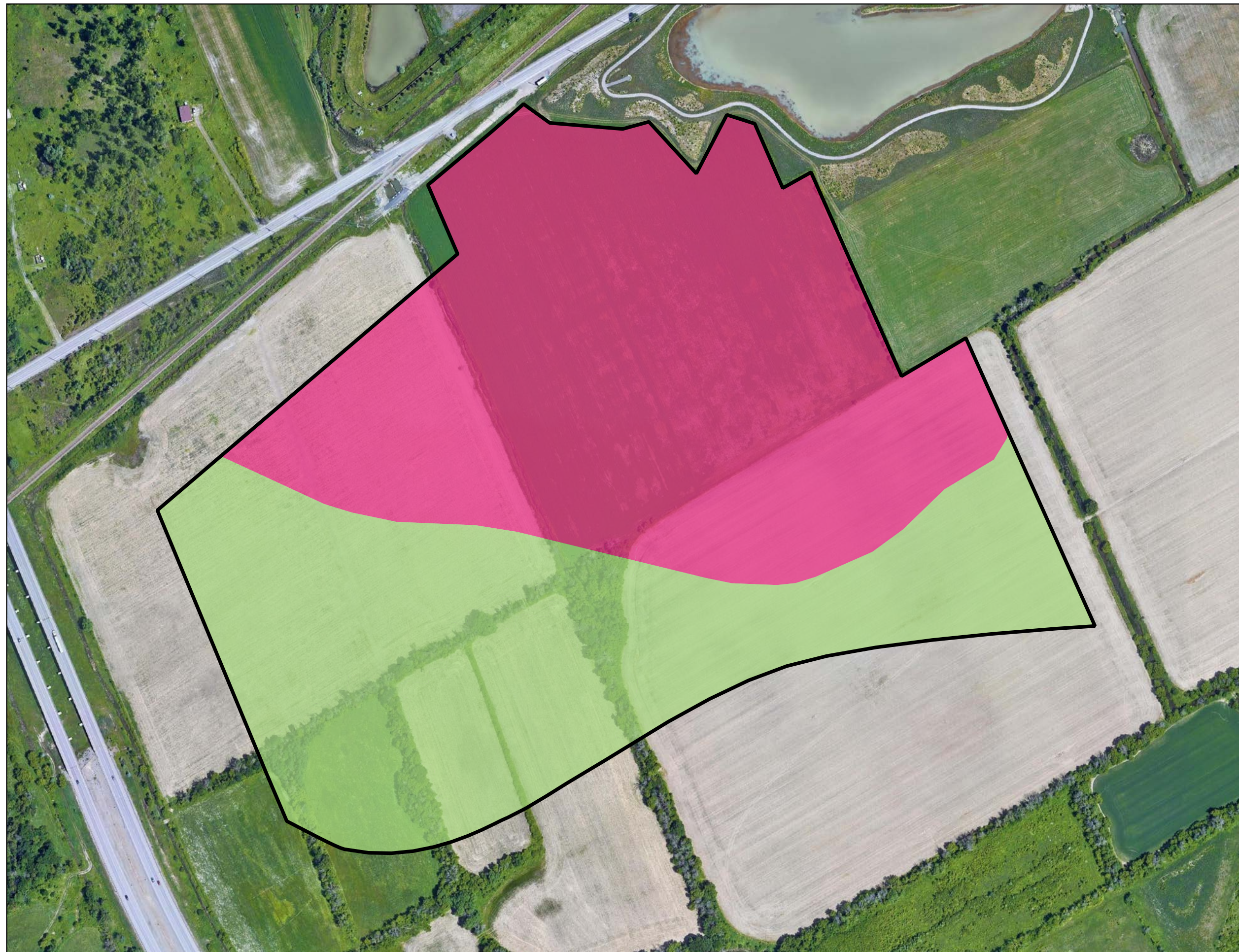
[jfsa.com](http://jfsa.com)

Ottawa, ON  
Paris, ON  
Gatineau, QC  
Montréal, QC  
Québec, QC

# Attachment A

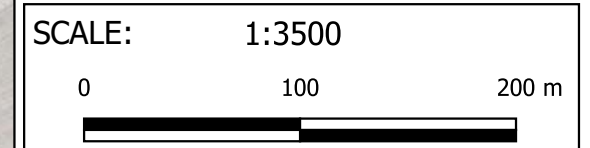
SWMHYMO Models & Parameters





**Legend**

- Soil Name (SCS Value)
- BRANDON (D)
- CARSONBY (C)
- Development Area



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BCD Phase 3

Figure A1: Soil Types

PROJECT	1474(03)
DRAWN	JB
DATE	OCT 2021





**Legend**

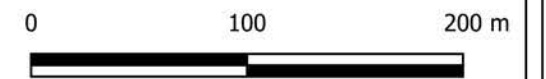
Land Use

Hedge Rows

Tilled

Development Area

SCALE: 1:3500



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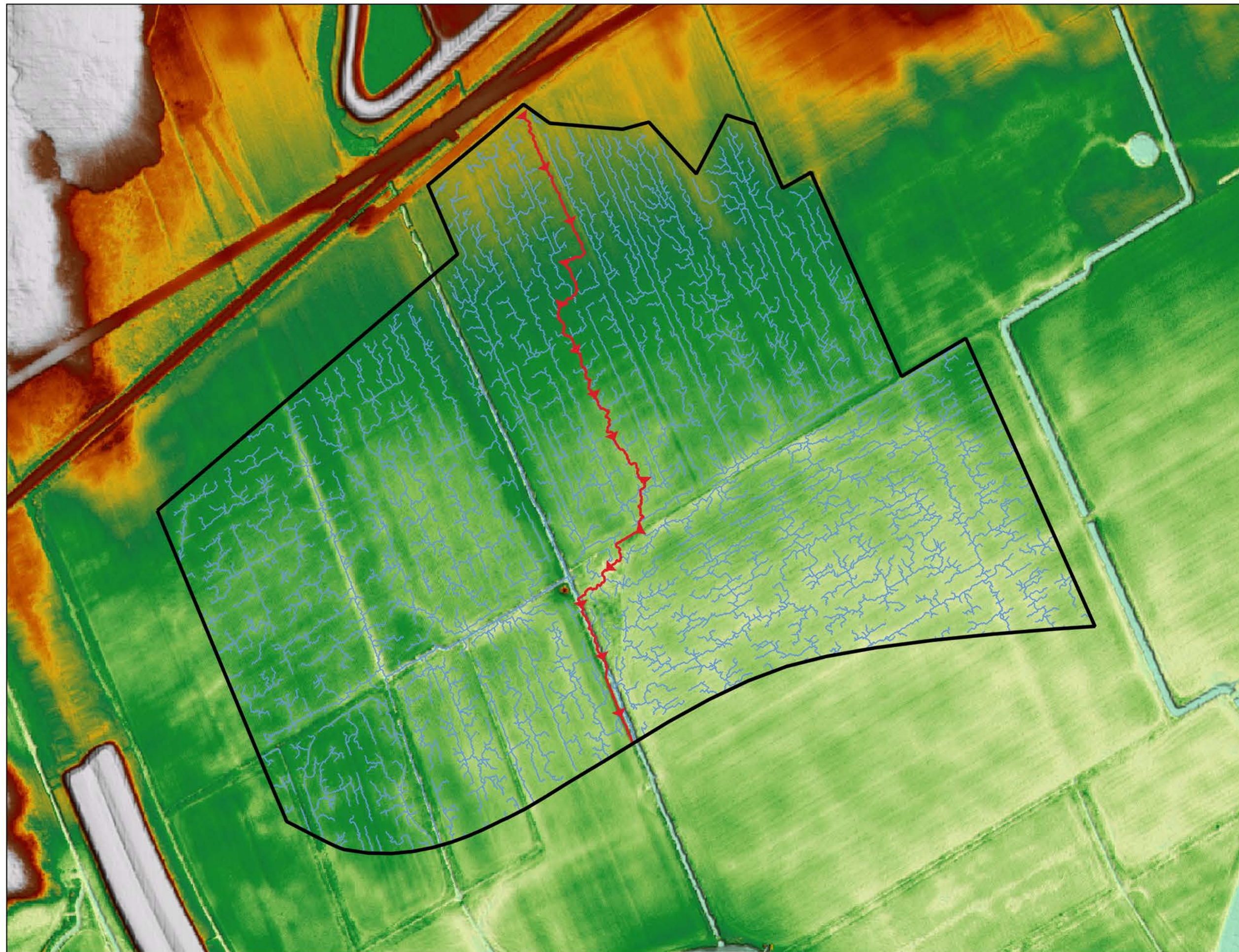
Figure A2: Land Use

PROJECT	1474(03)
---------	----------

DRAWN	JB
-------	----

DATE	OCT 2021
------	----------





**Legend**

- Major Flow Path
- Streams
- Terrain (m)
- 90.5
- 91
- 91.5
- 92
- 92.5
- 93
- 93.5
- 94
- 94.5
- Development Area

SCALE: 1:3500

0 100 200 m

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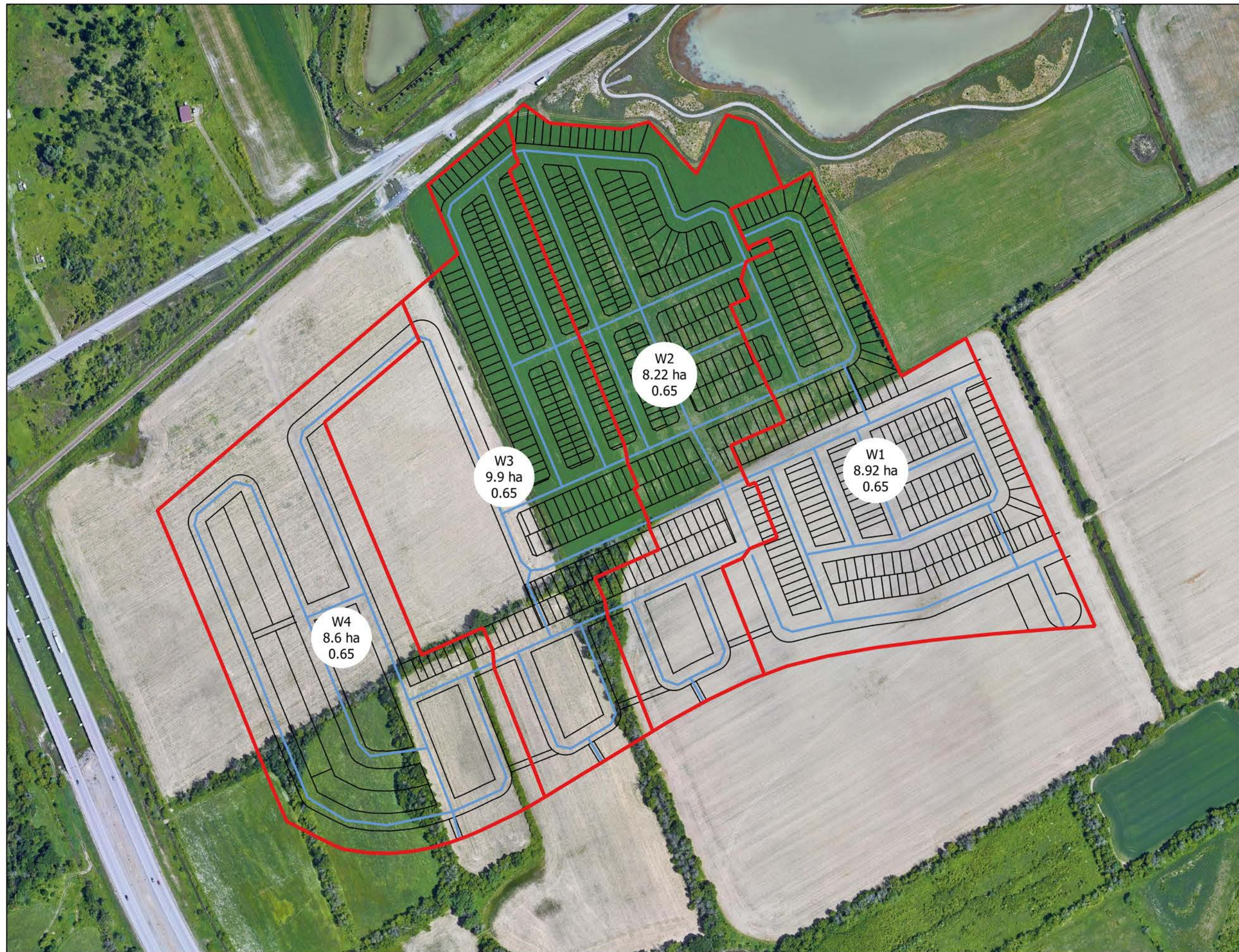
**DSEL**  
 david schaeffer engineering ltd

BCD Phase 3

Figure A3: Flow Paths

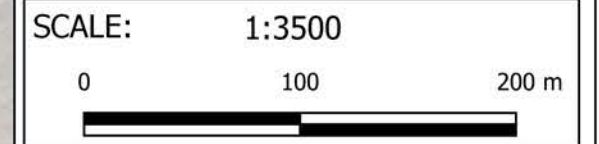
PROJECT	1474(03)
DRAWN	JB
DATE	OCT 2021





**Legend**

- Site Plan
- Minor System
- Lumped Areas:  
<Name>  
<Area>  
<Runoff Coefficient>



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BCD Phase 3

Figure A4: Proposed Development

PROJECT	1474(03)
DRAWN	JB
DATE	OCT 2021



**Table A1: Continuous Simulation Parameters**

Parameter(s) & Value(s)	Description
APII=[50], APIK=[0.90]/day	Used to compute the Antecedent Precipitation Index during the continuous simulation. Without model calibration, these are the default values.
IAimp = [1.57](mm), IAper=[4.67](mm)	Default Initial Abstraction (IA) values per the City of Ottawa Design Guidelines
IaREC=[6](hrs);	The time that it takes for the Initial Abstraction over pervious areas to recover during a dry period in undeveloped areas.
SMIN=[-1], SMAX=[-1](mm)	The negative values indicate that the storage volume in the SCS procedure will vary between the "S" determined for AMC I and AMC III conditions of the entered CN value in undeveloped and urban areas.
SK=[0.03]/(mm);	A calibration coefficient that can typically vary from 0.01 to 0.3 for undeveloped and urban areas. The higher the value, the more runoff generated. To set the baseline for existing conditions, it was decided to take a value in the low range.
InitGWResVol=[10](mm), GWResK=[0.9](mm/day/mm), VhydCond=[1](mm/hr);	Parameters that are used to simulate both the groundwater storage and discharge to surface watercourses from undeveloped areas. Without adequate field measurements, these parameters were selected based on previous continuous modelling experience.
IaRECper=[6](hrs);	The time that it takes for the Initial Abstraction over pervious areas to recover during a dry period in urban areas.
IaRECimp=[1.5](hrs);	The time that it takes for the Initial Abstraction over impervious areas to recover during a dry period in urban areas.
InterEventTime=[12](hrs)	The continuous dry time is required to reset the parameters in the SCS procedure to their initial values.

**Table A2: Calculation of SCS Curve Number (CN) and Modified Curve Number (CN\*)**

		EX ( 35.654 ha)							
Name	Total Area (ha)	Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
EX	35.654	0.034	Hedge Rows	BRANDON	D	Fair	77	0.1%	0.1
EX	35.654	19.68	Tilled	BRANDON	D	Fair	84	55.2%	46.4
EX	35.654	1.767	Hedge Rows	CARSONBY	C	Fair	70	5.0%	3.5
EX	35.654	14.173	Tilled	CARSONBY	C	Fair	79	39.8%	31.4
								<b>CN</b>	<b>81.3</b>
								<b>CN*</b>	<b>74</b>

**Table A3: Time to Peak Calculations**

Parameter	Units	EX
Area	ha	35.65
CN*	-	74
Ptotal to calc C from CN, use 2 yr 12 hr SCS stom	P(mm)	43.2
	Ia(mm)	4.67
	RV(mm)	11.7
C	-	0.27
Length of Channel	m	832
	ft	2728
Elevation of Head Water	m	92.07
	ft	302
Elevation of Outlet	m	89.90
	ft	295
Average Slope	m/m	0.26%
	ft/ft	0.26%
<b>Kirpich</b>		
Time of Concentration	mins	34
Time to Peak	min	23
Time to Peak	Hours	0.38
<b>FAA</b>		
Time of Concentration	mins	122
Time to Peak	mins	81
Time to Peak	Hours	1.35
<b>Barnsby Williams</b>		
Time of Concentration	mins	44
Time to Peak	mins	29
Time to Peak	Hours	0.49
<b>SCS</b>		
Time of Concentration	mins	165
Time to Peak	mins	110
Time to Peak	Hours	1.83
<b>Selected Method</b>		
FAA		
Time to Peak	min	81
Time to Peak	Hours	1.35

Note:

All methods calculated as per Appendix A of the SWMHYMO manual

Time to Peak calculated as 2/3 Time of concentration



```

1  20      Metric units / ID Numbers OFF
2  *#*****
3  *# SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
4  *#*****
5  *# Project Name: Barrhaven Conservancy Development
6  *# Project Number: 1474
7  *# Date       : 2021/Oct/18
8  *# Modeller   : J.Burnett, P.Eng.
9  *# Company    : J.F. Sabourin and Associates
10 *# License #   : 2582634
11 *#*****
12 START          TZERO=[1967.0101], METOUT=[2], NSTORM=[0], NRUN=[67]
13 *%            [""] <--storm filename, one per line for NSTORM time
14 *%-----|-----
15 *# Ottawa International Airport (1967 - 2003)
16 READ AES DATA AES_FILENAME=["YOW_1967_2007.123"],
17                IELEM=[123], START_DATE=[0], END_DATE=[-364]
18 *%-----|-----
19 COMPUTE API    APII=[50], APIK=[0.90]/day
20 *%-----|-----
21 *#*****
22 *#           Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE
23 DEVELOPMENT CONDITIONS
24 *#*****
25 *%-----|-----
26 CONTINUOUS NASHYD NHYD=["EX"], DT=[5] (min), AREA=[35.64] (ha)
27 DWF=[0] (cms), CN/C=[52], IA=[4.67] (mm), N=[3], TP=[1.35] (hrs),
28 Continuous simulation parameters:
29 IaRECper=[6] (hrs), SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.03]/(mm),
30 InterEventTime=[12] (hrs)
31 Baseflow simulation parameters:
32 BaseFlowOption=[1] , InitGWResVol=[10] (mm), GWResK=[0.9] (mm/day/mm)
33 VHydCond=[1.0] (mm/hr), END=-1
34 *%-----|-----
35 *#*****
36 *#           Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) -
37 PRE DEVELOPMENT CONDITIONS
38 *#*****
39 *#           Set infiltration to 0 (CN = 99.99) for water balance analysis
40 *#*****
41 *%-----|-----
42 *%           Drainage Area 1A
43 *%-----|-----
44 CONTINUOUS NASHYD NHYD=["INF-EX"], DT=[5] (min), AREA=[35.64] (ha)
45 DWF=[0] (cms), CN/C=[99.999], IA=[4.67] (mm), N=[3], TP=[1.35] (hrs),
46 Continuous simulation parameters:
47 IaRECper=[6] (hrs), SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.03]/(mm),
48 InterEventTime=[12] (hrs)
49 Baseflow simulation parameters:
50 BaseFlowOption=[1] , InitGWResVol=[10] (mm), GWResK=[0.9] (mm/day/mm)
51 VHydCond=[1.0] (mm/hr), END=-1

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48 *%-----|-----  
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49 *%-----|-----  
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50 *#####  
51 *# CONTINUOUS RAINFALL DATA  
52 *#####  
53 *%-----|-----  
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54 *%-----|-----  
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55 START          TZERO=[1968.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[68]  
56 *%-----|-----  
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57 START          TZERO=[1969.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[69]  
58 *%-----|-----  
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59 START          TZERO=[1970.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[70]  
60 *%-----|-----  
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61 START          TZERO=[1971.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[71]  
62 *%-----|-----  
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63 START          TZERO=[1972.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[72]  
64 *%-----|-----  
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65 START          TZERO=[1973.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[73]  
66 *%-----|-----  
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67 START          TZERO=[1974.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[74]  
68 *%-----|-----  
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69 START          TZERO=[1975.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[75]  
70 *%-----|-----  
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71 START          TZERO=[1976.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[76]  
72 *%-----|-----  
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73 START          TZERO=[1977.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[77]  
74 *%-----|-----  
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75 START          TZERO=[1978.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[78]  
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77 START          TZERO=[1979.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[79]  
78 *%-----|-----  
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79 START          TZERO=[1980.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[80]  
80 *%-----|-----  
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81 START          TZERO=[1981.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[81]  
82 *%-----|-----  
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83 START          TZERO=[1982.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[82]  
84 *%-----|-----  
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85 START          TZERO=[1983.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[83]  
86 *%-----|-----  
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87 START          TZERO=[1984.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[84]  
88 *%-----|-----  
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89 START          TZERO=[1985.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[85]  
90 *%-----|-----  
-----|  
91 START          TZERO=[1986.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[86]
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92  *%-----|-----  
-----|-----  
93  START          TZERO=[1987.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[87]  
94  *%-----|-----  
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95  START          TZERO=[1988.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[88]  
96  *%-----|-----  
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97  START          TZERO=[1989.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[89]  
98  *%-----|-----  
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99  START          TZERO=[1990.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[90]  
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101 START          TZERO=[1991.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[91]  
102 *%-----|-----  
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103 START          TZERO=[1992.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[92]  
104 *%-----|-----  
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105 START          TZERO=[1993.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[93]  
106 *%-----|-----  
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107 START          TZERO=[1994.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[94]  
108 *%-----|-----  
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109 START          TZERO=[1995.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[95]  
110 *%-----|-----  
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111 START          TZERO=[1996.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[96]  
112 *%-----|-----  
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113 START          TZERO=[1997.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[97]  
114 *%-----|-----  
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115 START          TZERO=[1998.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[98]  
116 *%-----|-----  
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117 START          TZERO=[1999.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[99]  
118 *%-----|-----  
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119 START          TZERO=[2000.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[100]  
120 *%-----|-----  
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121 *% MISSING FROM AES RAINFALL DATA  
122 *%START          TZERO=[2001.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[101]  
123 *%-----|-----  
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124 START          TZERO=[2002.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[102]  
125 *%-----|-----  
-----|-----  
126 START          TZERO=[2003.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[103]  
127 *%-----|-----  
-----|-----  
128 FINISH
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00002 .....
00003 SSSS W W M M H H Y Y M M O O O 222 000 11 555 .....
00004 S W W M M M M H H Y Y M M O O O 2 0 0 11 5 .....
00005 SSSS W W M M M H H H Y Y M M O O O 2 0 0 11 5 Ver 5.500 .....
00006 S W W M M H H H Y Y M M O O O 222 0 0 11 555 FEB 2013 .....
00007 SSSS W W M M H H Y Y M M O O O 2 0 0 11 5 .....
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00009 StormWater Management Hydrologic Model 222 000 11 555 .....
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00361# 24.60 16.40 11.67 6.13 3.09 1.56 1.06 .79 .54 mm/hr
00362# 24.60 16.40 11.67 6.13 3.09 1.56 1.06 .79 .54 mm/hr
00363# 19710810 19710810 19710810 19710810 19710810 19710810 19710810 19710810 19710810 date
00364# Number of rainfall events per following interval time
00365# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00366# 1.56 1.23 1.13 .93 7.2 61 52 42 33
00367# Number of events with at least the following durations
00368# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00369# 1.55 81 59 21 2 0 0 0 0 0
00370# R0073C0000-----
00371# COMPUTE API
00372# [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
00373# [AFImax= 62.22; AFIPavg= 14.84; AFIPmin= .36]
00374# \*\*\*\*\*
00375# # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00376# #
00377# R0073C0004-----
00378# CONTINUOUS NASHYD 5.0 01:EX 35.64 .161 1971.0810;16;40 22.27 .043 .000
00379# [CM= 52.0; N= 3.00; Tpe= 1.35]
00380# [IAREC= 6.00; SMIN= 95.25; SMAX= 635.00; SK= .030]
00381# [InterEventTime= 12.00]
00382# \*\*\*\*\*
00383# # Barhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00384# #
00385# # Set infiltration to 0 (CN = 99.99) for water balance analysis
00386# #
00387# R0073C0005-----
00388# CONTINUOUS NASHYD 5.0 01:INF-EX 35.64 1.010 1971.0810;16;20 181.82 .348 .000
00389# [CM= 100.0; N= 3.00; Tpe= 1.35]
00390# [IAREC= 6.00; SMIN= 1.39; SMAX= 9.24; SK= .030]
00391# [InterEventTime= 12.00]
00392# \*\*\*\*\*
00393# # CONTINUOUS RAINFALL DATA
00394# \*\*\*\*\*
00395# \*\* END OF RUN : 74
00396# \*\*\*\*\*
00397# \*\*\*\*\*
00398# \*\*\*\*\*
00399# \*\*\*\*\*
00400# \*\*\*\*\*
00401# \*\*\*\*\*
00402# \*\*\*\*\*
00403# RUN#COMMAND#
00404# R0073C0001#
00405# START
00406# [TZERO = .00 hrs on 1970101]
00407# [METOUT= 2 (1=imperial, 2=metric output)]
00408# [INSTORM= 0]
00409# [NRUN = 0074]
00410# \*\*\*\*\*
00411# # SWMRYD Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00412# \*\*\*\*\*
00413# # Project Name: Barhaven Conservancy Development
00414# # Project Number: 1474
00415# # Date : 2021/Oct/18
00416# # Modeller : J.Burnett, P.Eng.
00417# # Company : J.F. Sabourin and Associates
00418# # License # : 2582634
00419# # \*\*\*\*\*
00420# # Ottawa International Airport (1967 - 2003)
00421# R0073C0002-----
00422# READ RES DATA
00423# [Filename = YOM\_1967\_2007.123 ]
00424# [Start\_date= 1972.0101; End\_date= 1972.1231]
00425# [DT= 60;min; Length= 8760;hrs; WetHrs= 320; DryHrs= 8440; PTOT= 386.20]
00426# Maximum average rainfall intensities over
00427# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00428# 37.30 19.15 12.97 8.15 4.50 2.53 2.00 1.71 1.17 mm/hr
00429# 37.30 38.30 38.90 48.90 54.00 60.70 62.10 82.20 84.20 mm
00430# 197012 197012 197012 197012 197012 197012 197012 197012 197012 date
00431# Number of rainfall events per following interval time
00432# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00433# 170 133 122 86 76 60 45 41 32
00434# Number of events with at least the following durations
00435# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00436# 169 96 58 21 5 0 0 0 0 0
00437# R0073C0003-----
00438# COMPUTE API
00439# [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
00440# [AFImax= 62.22; AFIPavg= 14.84; AFIPmin= .36]
00441# \*\*\*\*\*
00442# # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00443# #
00444# R0073C0004-----
00445# CONTINUOUS NASHYD 5.0 01:EX 35.64 .163 1972.0808;0;00 71.40 .094 .000
00446# [CM= 52.0; N= 3.00; Tpe= 1.35]
00447# [IAREC= 6.00; SMIN= 95.25; SMAX= 635.00; SK= .030]
00448# [InterEventTime= 12.00]
00449# \*\*\*\*\*
00450# # Barhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00451# #
00452# # Set infiltration to 0 (CN = 99.99) for water balance analysis
00453# #
00454# R0073C0005-----
00455# CONTINUOUS NASHYD 5.0 01:INF-EX 35.64 1.077 1972.0808;0;00 375.41 479 .000
00456# [CM= 100.0; N= 3.00; Tpe= 1.35]
00457# [IAREC= 6.00; SMIN= 1.39; SMAX= 9.24; SK= .030]
00458# [InterEventTime= 12.00]
00459# \*\*\*\*\*
00460# # CONTINUOUS RAINFALL DATA
00461# \*\*\*\*\*
00462# \*\* END OF RUN : 72
00463# \*\*\*\*\*
00464# \*\*\*\*\*
00465# \*\*\*\*\*
00466# \*\*\*\*\*
00467# \*\*\*\*\*
00468# \*\*\*\*\*
00469# \*\*\*\*\*
00470# RUN#COMMAND#
00471# R0073C0001#
00472# START
00473# [TZERO = .00 hrs on 1970101]
00474# [METOUT= 2 (1=imperial, 2=metric output)]
00475# [INSTORM= 0]
00476# [NRUN = 0073]
00477# \*\*\*\*\*
00478# # SWMRYD Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00479# \*\*\*\*\*
00480# # Project Name: Barhaven Conservancy Development
00481# # Project Number: 1474
00482# # Date : 2021/Oct/18
00483# # Modeller : J.Burnett, P.Eng.
00484# # Company : J.F. Sabourin and Associates
00485# # License # : 2582634
00486# # \*\*\*\*\*
00487# # Ottawa International Airport (1967 - 2003)
00488# R0073C0002-----
00489# READ RES DATA
00490# [Filename = YOM\_1967\_2007.123 ]
00491# [Start\_date= 1973.0101; End\_date= 1973.1231]
00492# [DT= 60;min; Length= 8760;hrs; WetHrs= 349; DryHrs= 8211; PTOT= 744.30]
00493# Maximum average rainfall intensities over
00494# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00495# 30.00 17.25 12.33 7.10 3.63 1.89 1.28 .96 .86 mm/hr
00496# 30.00 34.50 37.00 42.60 43.60 45.40 46.00 46.00 69.20 date
00497# 197301 197301 197301 197301 197301 197301 197301 197301 197301 date
00498# Number of rainfall events per following interval time
00499# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00500# 200 164 143 108 79 61 54 43 37
00501# Number of events with at least the following durations
00502# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00503# 200 162 142 106 78 60 49 37 30
00504# R0073C0003-----
00505# COMPUTE API
00506# [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
00507# [AFImax= 78.26; AFIPavg= 20.56; AFIPmin= .06]
00508# \*\*\*\*\*
00509# # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00510# #
00511# R0073C0004-----
00512# CONTINUOUS NASHYD 5.0 01:EX 35.64 .168 1973.0808;0;00 51.01 .068 .000
00513# [CM= 52.0; N= 3.00; Tpe= 1.35]
00514# [IAREC= 6.00; SMIN= 95.25; SMAX= 635.00; SK= .030]
00515# [InterEventTime= 12.00]
00516# \*\*\*\*\*
00517# # Barhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00518# #
00519# # Set infiltration to 0 (CN = 99.99) for water balance analysis
00520# #
00521# R0073C0005-----
00522# CONTINUOUS NASHYD 5.0 01:INF-EX 35.64 1.245 1973.0808;0;00 337.66 453 .000
00523# [CM= 100.0; N= 3.00; Tpe= 1.35]
00524# [IAREC= 6.00; SMIN= 1.39; SMAX= 9.24; SK= .030]
00525# [InterEventTime= 12.00]
00526# \*\*\*\*\*
00527# # CONTINUOUS RAINFALL DATA
00528# \*\*\*\*\*
00529# \*\* END OF RUN : 73
00530# \*\*\*\*\*
00531# \*\*\*\*\*
00532# \*\*\*\*\*
00533# \*\*\*\*\*
00534# \*\*\*\*\*
00535# \*\*\*\*\*
00536# \*\*\*\*\*
00537# RUN#COMMAND#
00538# R0074C0001#
00539# START
00540# [TZERO = .00 hrs on 1970101]
00541# [METOUT= 2 (1=imperial, 2=metric output)]
00542# [INSTORM= 0]
00543# [NRUN = 0074]
00544# \*\*\*\*\*
00545# # SWMRYD Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00546# \*\*\*\*\*
00547# # Project Name: Barhaven Conservancy Development
00548# # Project Number: 1474
00549# # Date : 2021/Oct/18
00550# # Modeller : J.Burnett, P.Eng.
00551# # Company : J.F. Sabourin and Associates
00552# # License # : 2582634
00553# # \*\*\*\*\*
00554# # Ottawa International Airport (1967 - 2003)
00555# R0074C0002-----
00556# READ RES DATA
00557# [Filename = YOM\_1967\_2007.123 ]
00558# [Start\_date= 1974.0101; End\_date= 1974.1231]
00559# [DT= 60;min; Length= 8760;hrs; WetHrs= 320; DryHrs= 8440; PTOT= 386.20]
00560# Maximum average rainfall intensities over
00561# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00562# 20.60 15.40 10.37 5.18 2.98 1.63 1.08 .81 .54 mm/hr
00563# 20.60 30.80 31.10 31.10 35.70 39.00 39.00 39.00 39.00 date
00564# 19740718 19740719 19740719 19740719 19740719 19740719 19740719 19740719 19740719 date
00565# Number of rainfall events per following interval time
00566# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00567# 129 105 93 77 63 50 38 33 23
00568# Number of events with at least the following durations
00569# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00570# 128 104 92 76 62 49 37 32 22
00571# R0074C0003-----
00572# COMPUTE API
00573# [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
00574# [AFImax= 52.91; AFIPavg= 11.16; AFIPmin= .00]
00575# \*\*\*\*\*
00576# # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00577# #
00578# R0074C0004-----
00579# CONTINUOUS NASHYD 5.0 01:EX 35.64 .093 1974.0718;1;50 13.35 .035 .000
00580# [CM= 52.0; N= 3.00; Tpe= 1.35]
00581# [IAREC= 6.00; SMIN= 95.25; SMAX= 635.00; SK= .030]
00582# [InterEventTime= 12.00]
00583# \*\*\*\*\*
00584# # Barhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00585# #
00586# # Set infiltration to 0 (CN = 99.99) for water balance analysis
00587# #
00588# R0074C0005-----
00589# CONTINUOUS NASHYD 5.0 01:INF-EX 35.64 .804 1974.0718;1;35 119.81 .310 .000
00590# [CM= 100.0; N= 3.00; Tpe= 1.35]
00591# [IAREC= 6.00; SMIN= 1.39; SMAX= 9.24; SK= .030]
00592# [InterEventTime= 12.00]
00593# \*\*\*\*\*
00594# # CONTINUOUS RAINFALL DATA
00595# \*\*\*\*\*
00596# \*\* END OF RUN : 74
00597# \*\*\*\*\*
00598# \*\*\*\*\*
00599# \*\*\*\*\*
00600# \*\*\*\*\*
00601# \*\*\*\*\*
00602# \*\*\*\*\*
00603# \*\*\*\*\*
00604# RUN#COMMAND#
00605# R0073C0001#
00606# START
00607# [TZERO = .00 hrs on 1970101]
00608# [METOUT= 2 (1=imperial, 2=metric output)]
00609# [INSTORM= 0]
00610# [NRUN = 0075]
00611# \*\*\*\*\*
00612# # SWMRYD Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00613# \*\*\*\*\*
00614# # Project Name: Barhaven Conservancy Development
00615# # Project Number: 1474
00616# # Date : 2021/Oct/18
00617# # Modeller : J.Burnett, P.Eng.
00618# # Company : J.F. Sabourin and Associates
00619# # License # : 2582634
00620# # \*\*\*\*\*
00621# # Ottawa International Airport (1967 - 2003)
00622# R0073C0002-----
00623# READ RES DATA
00624# [Filename = YOM\_1967\_2007.123 ]
00625# [Start\_date= 1975.0101; End\_date= 1975.1231]
00626# [DT= 60;min; Length= 8760;hrs; WetHrs= 344; DryHrs= 8416; PTOT= 535.50]
00627# Maximum average rainfall intensities over
00628# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00629# 34.80 18.40 12.50 6.32 3.33 1.73 1.15 .89 .62 mm/hr
00630# 34.80 35.80 37.60 41.60 41.90 40.00 41.50 41.80 44.40 date
00631# 19750708 19750720 19750720 19750720 19750721 19750721 19750721 19750721 19750728 date
00632# Number of rainfall events per following interval time
00633# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00634# 136 118 99 78 61 49 40 33 25
00635# Number of events with at least the following durations
00636# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00637# 135 116 98 77 60 48 39 32 24
00638# R0073C0003-----
00639# COMPUTE API
00640# [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
00641# [AFImax= 73.23; AFIPavg= 15.16; AFIPmin= .00]
00642# \*\*\*\*\*
00643# # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00644# #
00645# R0073C0004-----
00646# CONTINUOUS NASHYD 5.0 01:EX 35.64 .169 1975.0720;1;55 30.69 .057 .000
00647# [CM= 52.0; N= 3.00; Tpe= 1.35]
00648# [IAREC= 6.00; SMIN= 95.25; SMAX= 635.00; SK= .030]
00649# [InterEventTime= 12.00]
00650# \*\*\*\*\*
00651# # Barhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00652# #
00653# # Set infiltration to 0 (CN = 99.99) for water balance analysis
00654# #
00655# R0073C0005-----
00656# CONTINUOUS NASHYD 5.0 01:INF-EX 35.64 1.042 1975.0708;1;00 219.51 410 .000
00657# [CM= 100.0; N= 3.00; Tpe= 1.35]
00658# [IAREC= 6.00; SMIN= 1.39; SMAX= 9.24; SK= .030]
00659# [InterEventTime= 12.00]
00660# \*\*\*\*\*
00661# # CONTINUOUS RAINFALL DATA
00662# \*\*\*\*\*
00663# \*\* END OF RUN : 75
00664# \*\*\*\*\*
00665# \*\*\*\*\*
00666# \*\*\*\*\*
00667# \*\*\*\*\*
00668# \*\*\*\*\*
00669# \*\*\*\*\*
00670# \*\*\*\*\*
00671# RUN#COMMAND#
00672# R0076C0001#
00673# START
00674# [TZERO = .00 hrs on 1970101]
00675# [METOUT= 2 (1=imperial, 2=metric output)]
00676# [INSTORM= 0]
00677# [NRUN = 0076]
00678# \*\*\*\*\*
00679# # SWMRYD Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00680# \*\*\*\*\*
00681# # Project Name: Barhaven Conservancy Development
00682# # Project Number: 1474
00683# # Date : 2021/Oct/18
00684# # Modeller : J.Burnett, P.Eng.
00685# # Company : J.F. Sabourin and Associates
00686# # License # : 2582634
00687# # \*\*\*\*\*
00688# # Ottawa International Airport (1967 - 2003)
00689# R0076C0002-----
00690# READ RES DATA
00691# [Filename = YOM\_1967\_2007.123 ]
00692# [Start\_date= 1976.0101; End\_date= 1976.1231]
00693# [DT= 60;min; Length= 8664;hrs; WetHrs= 390; DryHrs= 7674; PTOT= 493.20]
00694# Maximum average rainfall intensities over
00695# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00696# 14.00 8.90 6.43 4.65 2.35 1.39 .97 .99 .80 mm/hr
00697# 14.00 19.00 21.00 21.00 28.00 33.00 33.00 33.00 47.60 date
00698# 19760828 19760828 19760828 19760828 19760828 19760828 19760828 19760828 19760828 date
00699# Number of rainfall events per following interval time
00700# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00701# 164 133 117 89 72 62 46 40 28
00702# Number of events with at least the following durations
00703# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00704# 163 132 116 87 71 54 40 34 27
00705# R0076C0003-----
00706# COMPUTE API
00707# [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
00708# [AFImax= 59.66; AFIPavg= 15.35; AFIPmin= .02]
00709# \*\*\*\*\*
00710# # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00711# #
00712# R0076C0004-----
00713# CONTINUOUS NASHYD 5.0 01:EX 35.64 .085 1976.0518;2;30 19.66 .040 .000
00714# [CM= 52.0; N= 3.00; Tpe= 1.35]
00715# [IAREC= 6.00; SMIN= 95.25; SMAX= 635.00; SK= .030]
00716# [InterEventTime= 12.00]
00717# \*\*\*\*\*
00718# # Barhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
00719# #
00720# # Set infiltration to 0 (CN = 99.99) for water balance analysis





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01081 # SWMRYM Ver:5.02/jan 2001 <BETA> / INPUT DATA FILE
01082 *****
01083 # Project Name: Barhaven Conservancy Development
01084 # Project Number: 1474
01085 # Date : 2021/Oct/18
01086 # Modeller : J.Burnett, P.Eng.
01087 # Company : J.F. Sabourin and Associates
01088 # License # : 2582634
01089 *****
01090 # Ottawa International Airport (1967 - 2003)
01091 R0882.C0002-----
01092 # READ AES DATA
01093 [Filename = YOM_1967_2007.123 ]
01094 [Start_date= 1982.0101; End_date= 1982.1231 ]
01095 [DT= 60.min; Length= 8760.hrs; WetHrs= 436; DryHrs= 8324; PTOT= 596.10 ]
01096 Maximum average rainfall intensities over
01097 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01098 19.80 10.75 7.60 5.83 3.36 1.68 1.12 .96 .80 mm/hr
01099 19.80 21.90 22.80 35.00 40.30 40.30 46.30 57.30 mm
01100 1982001 1982001 1982002 1982002 1982002 1982002 1982002 1982002 date
01101 Number of rainfall events per following interevent time
01102 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01103 134 110 98 78 66 57 48 41 33
01104 Number of events with at least the following durations
01105 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01106 133 81 58 18 4 1 1 0 0
01107 R0882.C0003-----
01108 # COMPUTE API
01109 [APIIn= 50.00; APIQty= 9000; APIkdt= .9956 ]
01110 [APIImax= 56.66; APIAv= .03 ]
01111 *****
01112 # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01113 #
01114 R0882.C0004-----DTIn=ID:INVD-----AREAh-Q:PARCms-TpaakDate_hh:mm-----RvM-R:C-----DWfCms
01115 CONTINUOUS NASHVD 35.64 .149 1982.0825.1340 25.39 .044 .000
01116 [CM= 52.0; N= 3.00; Tm= 1.35 ]
01117 [IAREC= 6.00; SMIN= 95.25; SMAX= 635.00; SK= .030 ]
01118 [InterEventTime= 12.00 ]
01119 *****
01120 # Barhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01121 #
01122 R0882.C0005-----DTIn=ID:INVD-----AREAh-Q:PARCms-TpaakDate_hh:mm-----RvM-R:C-----DWfCms
01123 CONTINUOUS NASHVD 35.64 .149 1982.0825.1340 25.39 .044 .000
01124 [CM= 100.0; N= 3.00; Tm= 1.35 ]
01125 [IAREC= 6.00; SMIN= 95.25; SMAX= 635.00; SK= .030 ]
01126 [InterEventTime= 12.00 ]
01127 *****
01128 # CONTINUOUS RAINFALL DATA
01129 *****
01130 *****
01131 *****
01132 *****
01133 *****
01134 *****
01135 *****
01136 *****
01137 *****
01138 *****
01139 *****
01140 RUN:COMMAND#
01141 R0883.C0001-----
01142 # START
01143 [TZERO = .00 hrs on 19830101 ]
01144 [METOUT= 2 (1=Imperial, 2=metric output)]
01145 [NETOUT= 0 ]
01146 [NRUN = 0083 ]
01147 *****
01148 # SWMRYM Ver:5.02/jan 2001 <BETA> / INPUT DATA FILE
01149 *****
01150 # Project Name: Barhaven Conservancy Development
01151 # Project Number: 1474
01152 # Date : 2021/Oct/18
01153 # Modeller : J.Burnett, P.Eng.
01154 # Company : J.F. Sabourin and Associates
01155 # License # : 2582634
01156 *****
01157 # Ottawa International Airport (1967 - 2003)
01158 R0883.C0002-----
01159 # READ AES DATA
01160 [Filename = YOM_1967_2007.123 ]
01161 [Start_date= 1983.0101; End_date= 1983.1231 ]
01162 [DT= 60.min; Length= 8760.hrs; WetHrs= 462; DryHrs= 8298; PTOT= 587.50 ]
01163 Maximum average rainfall intensities over
01164 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01165 10.40 9.70 7.53 5.43 3.18 2.16 1.48 1.32 .92 mm/hr
01166 10.40 19.40 22.60 32.60 38.20 36.70 60.40 63.20 66.00 mm
01167 1983004 1983001 1983001 1983001 1983001 1983001 1983001 1983001 date
01168 Number of rainfall events per following interevent time
01169 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01170 148 135 103 85 70 45 50 45 35
01171 Number of events with at least the following durations
01172 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01173 142 87 56 28 5 0 0 0 0
01174 R0883.C0003-----
01175 # COMPUTE API
01176 [APIIn= 50.00; APIQty= 9000; APIkdt= .9956 ]
01177 [APIImax= 79.86; APIAv= 16.33; APImin= .03 ]
01178 *****
01179 # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01180 #
01181 R0883.C0004-----DTIn=ID:INVD-----AREAh-Q:PARCms-TpaakDate_hh:mm-----RvM-R:C-----DWfCms
01182 CONTINUOUS NASHVD 35.64 .149 1983.1205.16150 28.87 .049 .000
01183 [CM= 52.0; N= 3.00; Tm= 1.35 ]
01184 [IAREC= 6.00; SMIN= 95.25; SMAX= 635.00; SK= .030 ]
01185 [InterEventTime= 12.00 ]
01186 *****
01187 # Barhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01188 #
01189 R0883.C0005-----DTIn=ID:INVD-----AREAh-Q:PARCms-TpaakDate_hh:mm-----RvM-R:C-----DWfCms
01190 CONTINUOUS NASHVD 35.64 .149 1983.1205.16151 21.20 .370 .000
01191 [CM= 100.0; N= 3.00; Tm= 1.35 ]
01192 [IAREC= 6.00; SMIN= 95.25; SMAX= 635.00; SK= .030 ]
01193 *****
01194 *****
01195 *****
01196 *****
01197 *****
01198 *****
01199 *****
01200 *****
01201 *****
01202 *****
01203 *****
01204 *****
01205 *****
01206 *****
01207 RUN:COMMAND#
01208 R0884.C0001-----
01209 # START
01210 [TZERO = .00 hrs on 19840101 ]
01211 [METOUT= 2 (1=Imperial, 2=metric output)]
01212 [NETOUT= 0 ]
01213 [NRUN = 0084 ]
01214 *****
01215 # SWMRYM Ver:5.02/jan 2001 <BETA> / INPUT DATA FILE
01216 *****
01217 # Project Name: Barhaven Conservancy Development
01218 # Project Number: 1474
01219 # Date : 2021/Oct/18
01220 # Modeller : J.Burnett, P.Eng.
01221 # Company : J.F. Sabourin and Associates
01222 # License # : 2582634
01223 *****
01224 # Ottawa International Airport (1967 - 2003)
01225 R0884.C0002-----
01226 # READ AES DATA
01227 [Filename = YOM_1967_2007.123 ]
01228 [Start_date= 1984.0101; End_date= 1984.1230 ]
01229 [DT= 60.min; Length= 8760.hrs; WetHrs= 308; DryHrs= 8452; PTOT= 459.40 ]
01230 Maximum average rainfall intensities over
01231 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01232 11.80 9.70 7.57 4.93 3.03 1.85 1.58 1.19 1.00 mm/hr
01233 11.80 19.40 22.70 26.00 36.10 44.30 57.00 57.00 62.00 mm
01234 1984001 1984001 1984002 1984002 1984002 1984001 1984001 1984001 date
01235 Number of rainfall events per following interevent time
01236 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01237 98 75 63 55 40 34 26
01238 Number of events with at least the following durations
01239 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01240 98 75 63 55 40 34 26
01241 R0884.C0003-----
01242 # COMPUTE API
01243 [APIIn= 50.00; APIQty= 9000; APIkdt= .9956 ]
01244 [APIImax= 86.83; APIAv= 13.22; APImin= .03 ]
01245 *****
01246 # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01247 #
01248 R0884.C0004-----DTIn=ID:INVD-----AREAh-Q:PARCms-TpaakDate_hh:mm-----RvM-R:C-----DWfCms
01249 CONTINUOUS NASHVD 35.64 .149 1984.0811.7130 27.58 .060 .000
01250 [CM= 52.0; N= 3.00; Tm= 1.35 ]
01251 [IAREC= 6.00; SMIN= 95.25; SMAX= 635.00; SK= .030 ]
01252 [InterEventTime= 12.00 ]
01253 *****
01254 # Barhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01255 #
01256 R0884.C0005-----DTIn=ID:INVD-----AREAh-Q:PARCms-TpaakDate_hh:mm-----RvM-R:C-----DWfCms
01257 CONTINUOUS NASHVD 35.64 .149 1984.0811.7155 20.71 .451 .000
01258 [CM= 100.0; N= 3.00; Tm= 1.35 ]

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01261 [IAREC= 6.00; SMIN= 1.39; SMAX= 9.24; SK= .030 ]
01262 [InterEventTime= 12.00 ]
01263 *****
01264 # CONTINUOUS RAINFALL DATA
01265 *****
01266 *****
01267 *****
01268 *****
01269 *****
01270 *****
01271 *****
01272 *****
01273 *****
01274 RUN:COMMAND#
01275 R0885.C0001-----
01276 # START
01277 [TZERO = .00 hrs on 19850101 ]
01278 [METOUT= 2 (1=Imperial, 2=metric output)]
01279 [NETOUT= 0 ]
01280 [NRUN = 0085 ]
01281 *****
01282 # SWMRYM Ver:5.02/jan 2001 <BETA> / INPUT DATA FILE
01283 *****
01284 # Project Name: Barhaven Conservancy Development
01285 # Project Number: 1474
01286 # Date : 2021/Oct/18
01287 # Modeller : J.Burnett, P.Eng.
01288 # Company : J.F. Sabourin and Associates
01289 # License # : 2582634
01290 *****
01291 # Ottawa International Airport (1967 - 2003)
01292 R0885.C0002-----
01293 # READ AES DATA
01294 [Filename = YOM_1967_2007.123 ]
01295 [Start_date= 1985.0101; End_date= 1985.1231 ]
01296 [DT= 60.min; Length= 8760.hrs; WetHrs= 354; DryHrs= 8406; PTOT= 559.90 ]
01297 Maximum average rainfall intensities over
01298 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01299 19.00 13.60 11.70 6.60 3.30 1.65 1.11 .89 .60 mm/hr
01300 19.00 21.90 25.20 35.20 40.60 39.60 40.30 42.80 43.40 mm
01301 1985016 1985017 1985017 1985018 1985018 1985018 1985018 1985018 1985018 date
01302 Number of rainfall events per following interevent time
01303 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01304 108 84 74 69 56 49 43 32
01305 Number of events with at least the following durations
01306 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01307 107 70 43 33 4 2 1 0 0
01308 R0885.C0003-----
01309 # COMPUTE API
01310 [APIIn= 50.00; APIQty= 9000; APIkdt= .9956 ]
01311 [APIImax= 57.29; APIAv= 15.86; APImin= .20 ]
01312 *****
01313 # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01314 #
01315 R0885.C0004-----DTIn=ID:INVD-----AREAh-Q:PARCms-TpaakDate_hh:mm-----RvM-R:C-----DWfCms
01316 CONTINUOUS NASHVD 35.64 .149 1985.0618.0150 29.00 .052 .000
01317 [CM= 52.0; N= 3.00; Tm= 1.35 ]
01318 [IAREC= 6.00; SMIN= 95.25; SMAX= 635.00; SK= .030 ]
01319 [InterEventTime= 12.00 ]
01320 *****
01321 # Barhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01322 #
01323 R0885.C0005-----DTIn=ID:INVD-----AREAh-Q:PARCms-TpaakDate_hh:mm-----RvM-R:C-----DWfCms
01324 CONTINUOUS NASHVD 35.64 .149 1985.0618.0150 26.29 .468 .000
01325 [CM= 100.0; N= 3.00; Tm= 1.35 ]
01326 [IAREC= 6.00; SMIN= 95.25; SMAX= 635.00; SK= .030 ]
01327 *****
01328 # CONTINUOUS RAINFALL DATA
01329 *****
01330 *****
01331 *****
01332 *****
01333 *****
01334 *****
01335 *****
01336 *****
01337 *****
01338 *****
01339 *****
01340 RUN:COMMAND#
01341 R0886.C0001-----
01342 # START
01343 [TZERO = .00 hrs on 19860101 ]
01344 [METOUT= 2 (1=Imperial, 2=metric output)]
01345 [NETOUT= 0 ]
01346 [NRUN = 0086 ]
01347 *****
01348 # SWMRYM Ver:5.02/jan 2001 <BETA> / INPUT DATA FILE
01349 *****
01350 # Project Name: Barhaven Conservancy Development
01351 # Project Number: 1474
01352 # Date : 2021/Oct/18
01353 # Modeller : J.Burnett, P.Eng.
01354 # Company : J.F. Sabourin and Associates
01355 # License # : 2582634
01356 *****
01357 # Ottawa International Airport (1967 - 2003)
01358 R0886.C0002-----
01359 # READ AES DATA
01360 [Filename = YOM_1967_2007.123 ]
01361 [Start_date= 1986.0101; End_date= 1986.1231 ]
01362 [DT= 60.min; Length= 8400.hrs; WetHrs= 520; DryHrs= 7520; PTOT= 849.40 ]
01363 Maximum average rainfall intensities over
01364 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01365 18.30 17.80 13.57 7.07 4.84 2.89 2.42 1.85 1.31 mm/hr
01366 18.30 21.90 22.60 32.60 38.20 36.70 60.40 63.20 66.00 mm
01367 1986072 1986072 1986072 1986072 1986072 1986072 1986072 1986072 1986072 date
01368 Number of rainfall events per following interevent time
01369 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01370 178 144 131 104 80 63 53 48 33
01371 Number of events with at least the following durations
01372 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01373 177 104 76 24 2 0 0 0 0
01374 R0886.C0003-----
01375 # COMPUTE API
01376 [APIIn= 50.00; APIQty= 9000; APIkdt= .9956 ]
01377 [APIImax= 102.23; APIAv= 25.30; APImin= .17 ]
01378 *****
01379 # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01380 #
01381 R0886.C0004-----DTIn=ID:INVD-----AREAh-Q:PARCms-TpaakDate_hh:mm-----RvM-R:C-----DWfCms
01382 CONTINUOUS NASHVD 35.64 .149 1986.0911.23155 88.54 .104 .000
01383 [CM= 52.0; N= 3.00; Tm= 1.35 ]
01384 [IAREC= 6.00; SMIN= 95.25; SMAX= 635.00; SK= .030 ]
01385 [InterEventTime= 12.00 ]
01386 *****
01387 # Barhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01388 #
01389 R0886.C0005-----DTIn=ID:INVD-----AREAh-Q:PARCms-TpaakDate_hh:mm-----RvM-R:C-----DWfCms
01390 CONTINUOUS NASHVD 35.64 .149 1986.0911.23155 418.06 .492 .000
01391 [CM= 100.0; N= 3.00; Tm= 1.35 ]
01392 [IAREC= 6.00; SMIN= 95.25; SMAX= 635.00; SK= .030 ]
01393 *****
01394 *****
01395 *****
01396 *****
01397 *****
01398 *****
01399 *****
01400 *****
01401 *****
01402 *****
01403 *****
01404 *****
01405 *****
01406 *****
01407 *****
01408 RUN:COMMAND#
01409 R0887.C0001-----
01410 # START
01411 [TZERO = .00 hrs on 19870101 ]
01412 [METOUT= 2 (1=Imperial, 2=metric output)]
01413 [NETOUT= 0 ]
01414 [NRUN = 0087 ]
01415 *****
01416 # SWMRYM Ver:5.02/jan 2001 <BETA> / INPUT DATA FILE
01417 *****
01418 # Project Name: Barhaven Conservancy Development
01419 # Project Number: 1474
01420 # Date : 2021/Oct/18
01421 # Modeller : J.Burnett, P.Eng.
01422 # Company : J.F. Sabourin and Associates
01423 # License # : 2582634
01424 *****
01425 # Ottawa International Airport (1967 - 2003)
01426 R0887.C0002-----
01427 # READ AES DATA
01428 [Filename = YOM_1967_2007.123 ]
01429 [Start_date= 1987.0101; End_date= 1987.1231 ]
01430 [DT= 60.min; Length= 7844.hrs; WetHrs= 482; DryHrs= 6552; PTOT= 640.10 ]
01431 Maximum average rainfall intensities over
01432 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01433 20.00 13.90 14.03 7.05 4.87 2.46 1.84 1.40 .93 mm/hr
01434 20.00 21.80 42.10 42.30 58.40 59.00 66.40 67.00 67.00 mm
01435 1987024 1987024 1987024 1987024 1987024 1987025 1987025 1987025 1987025 date
01436 Number of rainfall events per following interevent time
01437 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01438 180 147 128 93 74 55 49 41 28
01439 Number of events with at least the following durations
01440 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs

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01441: 179 94 60 20 3 0 0 0 0 0
01442: R0087C0002
01443: COMPUTE API
01444: [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
01445: [ZTZO= 0.00 hrs on 1990101]
01446: [METOUT= 2 (1=Imperial, 2=metric output)]
01447: [INSTORM= 0]
01448: [NRUN = 0089 ]
01449: # SWHYMD Ver:5.02/Jan 2001 «BETA» / INPUT DATA FILE
01450: # Project Name: Barhaven Conservancy Development
01451: # Project Number: 1474
01452: # Date : 2021/Oct/18
01453: # Modeler : J.Burnett, P.Eng.
01454: # Company : J.F. Sabourin and Associates
01455: # License # : 2582634
01456: # Location : 2582634
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01801 *****
01802 ** END OF RUN : 92
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01810 RUN:COMMAND#
01811 R0993:C0001-----
01812 *****
01813 [TZERO = .00 hrs on 19930101]
01814 [METOUT= 2 (1=Imperial, 2=metric output)]
01815 [INTFORM= 0]
01816 [NRUN = 0093]
01817 *****
01818 # SMMHYO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
01819 #
01820 # Project Name: Barhaven Conservancy Development
01821 # Project Number: 1474
01822 # Date : 2021/Oct/18
01823 # Modeler : J.Burnett, P.Eng.
01824 # Company : J.F. Sabourin and Associates
01825 # License # : 2582634
01826 *****
01827 # Ottawa International Airport (1967 - 2003)
01828 R0993:C0002-----
01829 *****
01830 * HEAD AER DATA
01831 [Filename = YOM_1967_2007_123 ]
01832 [Start_date= 1993.0101; End_date= 1993.1231]
01833 [DT= 60.min; Length= 3760.hrs; WetHrs= 385; DryHrs= 8175; PTO= 721.30]
01834 *****
01835 Maximum average rainfall intensities over
01836 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01837 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 mm/hr
01838 199303 199303 199303 1993128 1993128 1993128 1993128 1993128 1993128 date
01839 *****
01840 Number of rainfall events per following interval time
01841 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01842 1 1 1 1 1 1 1 1 1
01843 1 2 3 6 12 24 36 48 72
01844 190 110 66 27 7 2 0 0 0
01845 R0993:C0003-----
01846 *****
01847 COMPUTE API
01848 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
01849 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
01850 *****
01851 # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01852 #
01853 # Project Name: Barhaven Conservancy Development
01854 # Project Number: 1474
01855 # Date : 2021/Oct/18
01856 # Modeler : J.Burnett, P.Eng.
01857 # Company : J.F. Sabourin and Associates
01858 # License # : 2582634
01859 *****
01860 # Ottawa International Airport (1967 - 2003)
01861 R0993:C0004-----
01862 *****
01863 * HEAD AER DATA
01864 [Filename = YOM_1967_2007_123 ]
01865 [Start_date= 1993.0101; End_date= 1993.1231]
01866 [DT= 60.min; Length= 3760.hrs; WetHrs= 387; DryHrs= 8175; PTO= 721.30]
01867 *****
01868 Maximum average rainfall intensities over
01869 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01870 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 mm/hr
01871 199303 199303 199303 1993128 1993128 1993128 1993128 1993128 1993128 date
01872 *****
01873 Number of rainfall events per following interval time
01874 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01875 1 1 1 1 1 1 1 1 1
01876 1 2 3 6 12 24 36 48 72
01877 190 110 66 27 7 2 0 0 0
01878 R0993:C0005-----
01879 *****
01880 COMPUTE API
01881 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
01882 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
01883 *****
01884 # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01885 #
01886 # Project Name: Barhaven Conservancy Development
01887 # Project Number: 1474
01888 # Date : 2021/Oct/18
01889 # Modeler : J.Burnett, P.Eng.
01890 # Company : J.F. Sabourin and Associates
01891 # License # : 2582634
01892 *****
01893 # Ottawa International Airport (1967 - 2003)
01894 R0993:C0006-----
01895 *****
01896 * HEAD AER DATA
01897 [Filename = YOM_1967_2007_123 ]
01898 [Start_date= 1994.0101; End_date= 1994.1231]
01899 [DT= 60.min; Length= 3760.hrs; WetHrs= 387; DryHrs= 8175; PTO= 721.30]
01900 *****
01901 Maximum average rainfall intensities over
01902 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01903 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 mm/hr
01904 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 date
01905 *****
01906 Number of rainfall events per following interval time
01907 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01908 1 1 1 1 1 1 1 1 1
01909 1 2 3 6 12 24 36 48 72
01910 190 110 66 27 7 2 0 0 0
01911 R0994:C0001-----
01912 *****
01913 COMPUTE API
01914 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
01915 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
01916 *****
01917 # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01918 #
01919 # Project Name: Barhaven Conservancy Development
01920 # Project Number: 1474
01921 # Date : 2021/Oct/18
01922 # Modeler : J.Burnett, P.Eng.
01923 # Company : J.F. Sabourin and Associates
01924 # License # : 2582634
01925 *****
01926 # Ottawa International Airport (1967 - 2003)
01927 R0994:C0002-----
01928 *****
01929 * HEAD AER DATA
01930 [Filename = YOM_1967_2007_123 ]
01931 [Start_date= 1994.0101; End_date= 1994.1231]
01932 [DT= 60.min; Length= 3760.hrs; WetHrs= 387; DryHrs= 8175; PTO= 721.30]
01933 *****
01934 Maximum average rainfall intensities over
01935 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01936 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 mm/hr
01937 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 date
01938 *****
01939 Number of rainfall events per following interval time
01940 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01941 1 1 1 1 1 1 1 1 1
01942 1 2 3 6 12 24 36 48 72
01943 190 110 66 27 7 2 0 0 0
01944 R0994:C0003-----
01945 *****
01946 COMPUTE API
01947 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
01948 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
01949 *****
01950 # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01951 #
01952 # Project Name: Barhaven Conservancy Development
01953 # Project Number: 1474
01954 # Date : 2021/Oct/18
01955 # Modeler : J.Burnett, P.Eng.
01956 # Company : J.F. Sabourin and Associates
01957 # License # : 2582634
01958 *****
01959 # Ottawa International Airport (1967 - 2003)
01960 R0994:C0004-----
01961 *****
01962 * HEAD AER DATA
01963 [Filename = YOM_1967_2007_123 ]
01964 [Start_date= 1993.0101; End_date= 1993.1231]
01965 [DT= 60.min; Length= 3760.hrs; WetHrs= 387; DryHrs= 8175; PTO= 721.30]
01966 *****
01967 Maximum average rainfall intensities over
01968 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01969 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 mm/hr
01970 199303 199303 199303 1993128 1993128 1993128 1993128 1993128 1993128 date
01971 *****
01972 Number of rainfall events per following interval time
01973 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01974 1 1 1 1 1 1 1 1 1
01975 1 2 3 6 12 24 36 48 72
01976 190 110 66 27 7 2 0 0 0
01977 R0995:C0001-----
01978 *****
01979 COMPUTE API
01980 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]

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01981 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
01982 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
01983 *****
01984 # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
01985 #
01986 # Project Name: Barhaven Conservancy Development
01987 # Project Number: 1474
01988 # Date : 2021/Oct/18
01989 # Modeler : J.Burnett, P.Eng.
01990 # Company : J.F. Sabourin and Associates
01991 # License # : 2582634
01992 *****
01993 # Ottawa International Airport (1967 - 2003)
01994 R0995:C0005-----
01995 *****
01996 * HEAD AER DATA
01997 [Filename = YOM_1967_2007_123 ]
01998 [Start_date= 1993.0101; End_date= 1993.1231]
01999 [DT= 60.min; Length= 3760.hrs; WetHrs= 387; DryHrs= 8175; PTO= 721.30]
02000 *****
02001 Maximum average rainfall intensities over
02002 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02003 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 mm/hr
02004 199303 199303 199303 1993128 1993128 1993128 1993128 1993128 1993128 date
02005 *****
02006 Number of rainfall events per following interval time
02007 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02008 1 1 1 1 1 1 1 1 1
02009 1 2 3 6 12 24 36 48 72
02010 190 110 66 27 7 2 0 0 0
02011 R0995:C0006-----
02012 *****
02013 COMPUTE API
02014 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
02015 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
02016 *****
02017 # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02018 #
02019 # Project Name: Barhaven Conservancy Development
02020 # Project Number: 1474
02021 # Date : 2021/Oct/18
02022 # Modeler : J.Burnett, P.Eng.
02023 # Company : J.F. Sabourin and Associates
02024 # License # : 2582634
02025 *****
02026 # Ottawa International Airport (1967 - 2003)
02027 R0995:C0007-----
02028 *****
02029 * HEAD AER DATA
02030 [Filename = YOM_1967_2007_123 ]
02031 [Start_date= 1993.0101; End_date= 1993.1231]
02032 [DT= 60.min; Length= 3760.hrs; WetHrs= 387; DryHrs= 8175; PTO= 721.30]
02033 *****
02034 Maximum average rainfall intensities over
02035 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02036 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 mm/hr
02037 199303 199303 199303 1993128 1993128 1993128 1993128 1993128 1993128 date
02038 *****
02039 Number of rainfall events per following interval time
02040 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02041 1 1 1 1 1 1 1 1 1
02042 1 2 3 6 12 24 36 48 72
02043 190 110 66 27 7 2 0 0 0
02044 R0996:C0001-----
02045 *****
02046 COMPUTE API
02047 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
02048 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
02049 *****
02050 # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02051 #
02052 # Project Name: Barhaven Conservancy Development
02053 # Project Number: 1474
02054 # Date : 2021/Oct/18
02055 # Modeler : J.Burnett, P.Eng.
02056 # Company : J.F. Sabourin and Associates
02057 # License # : 2582634
02058 *****
02059 # Ottawa International Airport (1967 - 2003)
02060 R0996:C0002-----
02061 *****
02062 * HEAD AER DATA
02063 [Filename = YOM_1967_2007_123 ]
02064 [Start_date= 1994.0101; End_date= 1994.1231]
02065 [DT= 60.min; Length= 3760.hrs; WetHrs= 387; DryHrs= 8175; PTO= 721.30]
02066 *****
02067 Maximum average rainfall intensities over
02068 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02069 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 mm/hr
02070 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 date
02071 *****
02072 Number of rainfall events per following interval time
02073 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02074 1 1 1 1 1 1 1 1 1
02075 1 2 3 6 12 24 36 48 72
02076 190 110 66 27 7 2 0 0 0
02077 R0997:C0001-----
02078 *****
02079 COMPUTE API
02080 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
02081 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
02082 *****
02083 # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02084 #
02085 # Project Name: Barhaven Conservancy Development
02086 # Project Number: 1474
02087 # Date : 2021/Oct/18
02088 # Modeler : J.Burnett, P.Eng.
02089 # Company : J.F. Sabourin and Associates
02090 # License # : 2582634
02091 *****
02092 # Ottawa International Airport (1967 - 2003)
02093 R0997:C0002-----
02094 *****
02095 * HEAD AER DATA
02096 [Filename = YOM_1967_2007_123 ]
02097 [Start_date= 1994.0101; End_date= 1994.1231]
02098 [DT= 60.min; Length= 3760.hrs; WetHrs= 387; DryHrs= 8175; PTO= 721.30]
02099 *****
02100 Maximum average rainfall intensities over
02101 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02102 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 mm/hr
02103 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 1994029 date
02104 *****
02105 Number of rainfall events per following interval time
02106 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02107 1 1 1 1 1 1 1 1 1
02108 1 2 3 6 12 24 36 48 72
02109 190 110 66 27 7 2 0 0 0
02110 R0998:C0001-----
02111 *****
02112 COMPUTE API
02113 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
02114 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
02115 *****
02116 # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02117 #
02118 # Project Name: Barhaven Conservancy Development
02119 # Project Number: 1474
02120 # Date : 2021/Oct/18
02121 # Modeler : J.Burnett, P.Eng.
02122 # Company : J.F. Sabourin and Associates
02123 # License # : 2582634
02124 *****
02125 # Ottawa International Airport (1967 - 2003)
02126 R0998:C0002-----
02127 *****
02128 * HEAD AER DATA
02129 [Filename = YOM_1967_2007_123 ]
02130 [Start_date= 1993.0101; End_date= 1993.1231]
02131 [DT= 60.min; Length= 3760.hrs; WetHrs= 387; DryHrs= 8175; PTO= 721.30]
02132 *****
02133 Maximum average rainfall intensities over
02134 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02135 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 mm/hr
02136 199303 199303 199303 1993128 1993128 1993128 1993128 1993128 1993128 date
02137 *****
02138 Number of rainfall events per following interval time
02139 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02140 1 1 1 1 1 1 1 1 1
02141 1 2 3 6 12 24 36 48 72
02142 190 110 66 27 7 2 0 0 0
02143 R0999:C0001-----
02144 *****
02145 COMPUTE API
02146 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
02147 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]
02148 *****
02149 # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02150 #
02151 # Project Name: Barhaven Conservancy Development
02152 # Project Number: 1474
02153 # Date : 2021/Oct/18
02154 # Modeler : J.Burnett, P.Eng.
02155 # Company : J.F. Sabourin and Associates
02156 # License # : 2582634
02157 *****
02158 # Ottawa International Airport (1967 - 2003)
02159 R0999:C0002-----
02160 *****
02161 * HEAD AER DATA
02162 [Filename = YOM_1967_2007_123 ]
02163 [Start_date= 1993.0101; End_date= 1993.1231]
02164 [DT= 60.min; Length= 3760.hrs; WetHrs= 387; DryHrs= 8175; PTO= 721.30]
02165 *****
02166 Maximum average rainfall intensities over
02167 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02168 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 12.50 mm/hr
02169 199303 199303 199303 1993128 1993128 1993128 1993128 1993128 1993128 date
02170 *****
02171 Number of rainfall events per following interval time
02172 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02173 1 1 1 1 1 1 1 1 1
02174 1 2 3 6 12 24 36 48 72
02175 190 110 66 27 7 2 0 0 0
02176 R1000:C0001-----
02177 *****
02178 COMPUTE API
02179 [APIIn= 50.00; APIkdy= 9000; APIkdt= .9956]

```

```

02161: *****
02162: # Ottawa International Airport (1967 - 2003)
02163: R0098:CO0002-----
02164: * READ AES DATA
02165: [Filename = YOM_1967_2007.123 ]
02166: [Start_date = 1998.0101; End_date = 1999.1231]
02167: [DT= 60.min; Length= 4440.hrs; WetHrs= 291; DryHrs= 479; PTO= 440.30]
02168: Maximum average rainfall intensities over
02169: 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02170: 15.00 10.10 9.00 6.97 5.27 4.45 3.82 3.21 2.71 mm/hr
02171: 15.80 17.80 22.80 24.00 30.50 43.60 45.80 40.80 54.60
02172: 1999016 1999027 1999037 1999047 1999057 1999067 1999077 1999087 1999098 date
02173: Number of rainfall events per following increment time
02174: 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02175: 126 104 76 62 42 37 32 21
02176: Number of events with at least the following durations
02177: 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02178: 125 64 43 8 1 0 0 0 0
02179: R0098:CO0003-----
02180: COMPUTE API
02181: [API=In= 50.00; APIKdy= .9000; APIKdt= .9956]
02182: [API=Out= 57.22; APIAvge= 11.99; APImin= 1.69]
02183: *****
02184: # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02185: *****
02186: R0098:CO0004-----OtmIn-ID:INHYD-----AREAhA-QFAPARms-TpaeDate_hJm-----RvM-R-C-----DWfms
02187: [CM= 52.0; N= 3.00; Tp= 1.35] 35.64 .091 1999.0927.1510 17.72 .040 .000
02188: [IARC= 6.00; SMIN= 95.25; SMAK= 635.00; EK= .030]
02189: [InterEventTime= 12.00]
02190: *****
02191: # Barhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02192: *****
02193: # Set infiltration to 0 (CN = 99.99) for water balance analysis
02194: *****
02195: R0098:CO0005-----OtmIn-ID:INHYD-----AREAhA-QFAPARms-TpaeDate_hJm-----RvM-R-C-----DWfms
02196: [CM= 100.0; N= 3.00; Tp= 1.35] 35.64 .496 1999.0627.2105 163.10 .370 .000
02197: [IARC= 6.00; SMIN= 1.39; SMAK= 9.24; EK= .030]
02198: [InterEventTime= 12.00]
02199: *****
02200: *****
02201: *****
02202: # CONTINUOUS RAINFALL DATA
02203: *****
02204: ** END OF RUN : 98
02205: *****
02206: *****
02207: *****
02208: *****
02209: *****
02210: *****
02211: *****
02212: R0099:CO0001-----
02213: R0099:CO0001-----
02214: START
02215: [ITER= .00 hrs on 19990101]
02216: [MOUT= 2 (1=Imperial, 2=metric output)]
02217: [NFORM= 0]
02218: [NUN = 0099 ]
02219: *****
02220: # SMWVMD Ver5.02/Jan 2001 <BETA> / INPUT DATA FILE
02221: *****
02222: # Project Name: Barhaven Conservancy Development
02223: # Project Number: 1474
02224: # Date : 2021/Oct/18
02225: # Modeler : J.F. Sabourin, P.Eng.
02226: # Company : J.F. Sabourin and Associates
02227: # License # : 2582634
02228: *****
02229: # Ottawa International Airport (1967 - 2003)
02230: R0099:CO0002-----
02231: * READ AES DATA
02232: [Filename = YOM_1967_2007.123 ]
02233: [Start_date = 1999.0101; End_date = 1999.1231]
02234: [DT= 60.min; Length= 4440.hrs; WetHrs= 247; DryHrs= 4193; PTO= 424.40]
02235: Maximum average rainfall intensities over
02236: 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02237: 15.00 10.10 9.00 6.97 5.27 4.45 3.82 3.21 2.71 mm/hr
02238: 17.50 20.20 27.10 39.40 39.70 52.20 58.60 69.50
02239: 1999017 1999071 1999086 1999096 1999096 1999096 1999097 1999098 1999098 date
02240: Number of rainfall events per following increment time
02241: 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02242: 102 80 70 63 56 49 31 28 18
02243: Number of events with at least the following durations
02244: 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02245: 101 77 61 1 0 0 0 0 0
02246: R0099:CO0003-----
02247: COMPUTE API
02248: [API=In= 50.00; APIKdy= .9000; APIKdt= .9956]
02249: [API=Out= 69.11; APIAvge= 23.97; APImin= 1.93]
02250: *****
02251: # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02252: *****
02253: R0099:CO0004-----OtmIn-ID:INHYD-----AREAhA-QFAPARms-TpaeDate_hJm-----RvM-R-C-----DWfms
02254: [CM= 52.0; N= 3.00; Tp= 1.35] 35.64 .115 1999.0906.1030 18.48 .044 .000
02255: [IARC= 6.00; SMIN= 95.25; SMAK= 635.00; EK= .030]
02256: [InterEventTime= 12.00]
02257: *****
02258: *****
02259: # Barhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02260: *****
02261: # Set infiltration to 0 (CN = 99.99) for water balance analysis
02262: *****
02263: R0099:CO0005-----OtmIn-ID:INHYD-----AREAhA-QFAPARms-TpaeDate_hJm-----RvM-R-C-----DWfms
02264: [CM= 100.0; N= 3.00; Tp= 1.35] 35.64 .745 1999.0906.9120 171.71 .405 .000
02265: [IARC= 6.00; SMIN= 1.39; SMAK= 9.24; EK= .030]
02266: [InterEventTime= 12.00]
02267: *****
02268: *****
02269: # CONTINUOUS RAINFALL DATA
02270: *****
02271: ** END OF RUN : 99
02272: *****
02273: *****
02274: *****
02275: *****
02276: *****
02277: *****
02278: *****
02279: R0099:CO0001-----
02280: R0100:CO0001-----
02281: START
02282: [ITER= .00 hrs on 20000101]
02283: [MOUT= 2 (1=Imperial, 2=metric output)]
02284: [NFORM= 0]
02285: [NUN = 0100 ]
02286: *****
02287: # SMWVMD Ver5.02/Jan 2001 <BETA> / INPUT DATA FILE
02288: *****
02289: # Project Name: Barhaven Conservancy Development
02290: # Project Number: 1474
02291: # Date : 2021/Oct/18
02292: # Modeler : J.F. Sabourin, P.Eng.
02293: # Company : J.F. Sabourin and Associates
02294: # License # : 2582634
02295: *****
02296: # Ottawa International Airport (1967 - 2003)
02297: R0100:CO0002-----
02298: * READ AES DATA
02299: [Filename = YOM_1967_2007.123 ]
02300: [Start_date = 2000.0101; End_date = 2000.1230]
02301: [DT= 60.min; Length= 5160.hrs; WetHrs= 401; DryHrs= 4759; PTO= 535.90]
02302: Maximum average rainfall intensities over
02303: 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02304: 14.70 9.60 8.00 6.43 3.89 1.95 1.30 1.03 .84 mm/hr
02305: 14.70 19.20 24.10 38.50 46.70 46.70 49.30 60.40
02306: 2000025 2000025 2000025 2000025 2000025 2000025 2000026 2000026 2000051 2000051 date
02307: Number of rainfall events per following increment time
02308: 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02309: 156 125 110 86 67 46 34 30 23
02310: Number of events with at least the following durations
02311: 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02312: 155 82 49 16 2 0 0 0 0
02313: R0100:CO0003-----
02314: COMPUTE API
02315: [API=In= 50.00; APIKdy= .9000; APIKdt= .9956]
02316: [API=Out= 76.65; APIAvge= 25.66; APImin= 5.70]
02317: *****
02318: # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02319: *****
02320: R0100:CO0004-----OtmIn-ID:INHYD-----AREAhA-QFAPARms-TpaeDate_hJm-----RvM-R-C-----DWfms
02321: [CM= 52.0; N= 3.00; Tp= 1.35] 35.64 .270 2000.0625.1055 31.76 .059 .000
02322: [IARC= 6.00; SMIN= 95.25; SMAK= 635.00; EK= .030]
02323: [InterEventTime= 12.00]
02324: *****
02325: *****
02326: # Barhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02327: *****
02328: # Set infiltration to 0 (CN = 99.99) for water balance analysis
02329: *****
02330: R0100:CO0005-----OtmIn-ID:INHYD-----AREAhA-QFAPARms-TpaeDate_hJm-----RvM-R-C-----DWfms
02331: [CM= 100.0; N= 3.00; Tp= 1.35] 35.64 .816 2000.0625.1040 214.65 .401 .000
02332: [IARC= 6.00; SMIN= 1.39; SMAK= 9.24; EK= .030]
02333: [InterEventTime= 12.00]
02334: *****
02335: *****
02336: # CONTINUOUS RAINFALL DATA
02337: *****
02338: ** END OF RUN : 101
02339: *****
02340: *****

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```

02341: *****
02342: *****
02343: *****
02344: *****
02345: *****
02346: R0100:CO0001-----
02347: R0100:CO0001-----
02348: START
02349: [ITER= .00 hrs on 20020101]
02350: [MOUT= 2 (1=Imperial, 2=metric output)]
02351: [NFORM= 0]
02352: [NUN = 0102 ]
02353: *****
02354: # SMWVMD Ver5.02/Jan 2001 <BETA> / INPUT DATA FILE
02355: *****
02356: # Project Name: Barhaven Conservancy Development
02357: # Project Number: 1474
02358: # Date : 2021/Oct/18
02359: # Modeler : J.Burnett, P.Eng.
02360: # Company : J.F. Sabourin and Associates
02361: # License # : 2582634
02362: *****
02363: # Ottawa International Airport (1967 - 2003)
02364: R0100:CO0002-----
02365: * READ AES DATA
02366: [Filename = YOM_1967_2007.123 ]
02367: [Start_date = 2002.0101; End_date = 2002.1231]
02368: [DT= 60.min; Length= 5088.hrs; WetHrs= 304; DryHrs= 4784; PTO= 551.50]
02369: Maximum average rainfall intensities over
02370: 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02371: 45.00 26.75 18.40 9.48 4.74 2.48 2.08 1.56 1.04 mm/hr
02372: 45.00 53.50 55.20 56.90 56.90 59.50 74.90 74.90 74.90
02373: 2002027 2002027 2002027 2002027 2002027 2002027 2002028 2002028 2002029 date
02374: Number of rainfall events per following increment time
02375: 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02376: 100 83 78 56 47 41 36 34 25
02377: Number of events with at least the following durations
02378: 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02379: 100 59 33 13 5 0 0 0 0
02380: R0100:CO0003-----
02381: COMPUTE API
02382: [API=In= 50.00; APIKdy= .9000; APIKdt= .9956]
02383: [API=Out= 114.05; APIAvge= 26.37; APImin= 4.40]
02384: *****
02385: # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02386: *****
02387: R0100:CO0004-----OtmIn-ID:INHYD-----AREAhA-QFAPARms-TpaeDate_hJm-----RvM-R-C-----DWfms
02388: [CM= 52.0; N= 3.00; Tp= 1.35] 35.64 .595 2002.0627.1510 62.73 .114 .000
02389: [IARC= 6.00; SMIN= 95.25; SMAK= 635.00; EK= .030]
02390: [InterEventTime= 12.00]
02391: *****
02392: *****
02393: # Barhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02394: *****
02395: # Set infiltration to 0 (CN = 99.99) for water balance analysis
02396: *****
02397: R0100:CO0005-----OtmIn-ID:INHYD-----AREAhA-QFAPARms-TpaeDate_hJm-----RvM-R-C-----DWfms
02398: [CM= 100.0; N= 3.00; Tp= 1.35] 35.64 1.806 2002.0627.1455 294.04 .533 .000
02399: [IARC= 6.00; SMIN= 1.39; SMAK= 9.24; EK= .030]
02400: [InterEventTime= 12.00]
02401: *****
02402: *****
02403: # CONTINUOUS RAINFALL DATA
02404: *****
02405: *****
02406: *****
02407: ** END OF RUN : 102
02408: *****
02409: *****
02410: *****
02411: *****
02412: *****
02413: R0100:CO0001-----
02414: R0100:CO0001-----
02415: START
02416: [ITER= .00 hrs on 20030101]
02417: [MOUT= 2 (1=Imperial, 2=metric output)]
02418: [NFORM= 0]
02419: [NUN = 0103 ]
02420: *****
02421: # SMWVMD Ver5.02/Jan 2001 <BETA> / INPUT DATA FILE
02422: *****
02423: # Project Name: Barhaven Conservancy Development
02424: # Project Number: 1474
02425: # Date : 2021/Oct/18
02426: # Modeler : J.Burnett, P.Eng.
02427: # Company : J.F. Sabourin and Associates
02428: # License # : 2582634
02429: *****
02430: # Ottawa International Airport (1967 - 2003)
02431: R0100:CO0002-----
02432: * READ AES DATA
02433: [Filename = YOM_1967_2007.123 ]
02434: [Start_date = 2003.0101; End_date = 2003.1231]
02435: [DT= 60.min; Length= 4440.hrs; WetHrs= 404; DryHrs= 4034; PTO= 554.60]
02436: Maximum average rainfall intensities over
02437: 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02438: 15.10 10.00 7.13 4.28 3.18 1.86 1.25 .94 .81 mm/hr
02439: 15.10 20.00 21.40 25.70 38.20 44.60 44.90 45.10 58.30
02440: 2003011 2003011 2003011 2003011 2003011 2003015 2003025 2003026 2003027 date
02441: Number of rainfall events per following increment time
02442: 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02443: 145 127 109 86 64 45 38 25 15
02444: Number of events with at least the following durations
02445: 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02446: 144 80 43 13 5 1 0 0 0
02447: R0100:CO0003-----
02448: COMPUTE API
02449: [API=In= 50.00; APIKdy= .9000; APIKdt= .9956]
02450: [API=Out= 72.10; APIAvge= 22.97; APImin= 4.50]
02451: *****
02452: # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02453: *****
02454: R0100:CO0004-----OtmIn-ID:INHYD-----AREAhA-QFAPARms-TpaeDate_hJm-----RvM-R-C-----DWfms
02455: [CM= 52.0; N= 3.00; Tp= 1.35] 35.64 .173 2003.0711.1755 42.15 .078 .000
02456: [IARC= 6.00; SMIN= 95.25; SMAK= 635.00; EK= .030]
02457: [InterEventTime= 12.00]
02458: *****
02459: *****
02460: # Barhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - PRE DEVELOPMENT CONDITIONS
02461: *****
02462: # Set infiltration to 0 (CN = 99.99) for water balance analysis
02463: *****
02464: R0100:CO0005-----OtmIn-ID:INHYD-----AREAhA-QFAPARms-TpaeDate_hJm-----RvM-R-C-----DWfms
02465: [CM= 100.0; N= 3.00; Tp= 1.35] 35.64 .753 2003.0711.1755 251.88 .454 .000
02466: [IARC= 6.00; SMIN= 1.39; SMAK= 9.24; EK= .030]
02467: [InterEventTime= 12.00]
02468: *****
02469: *****
02470: # CONTINUOUS RAINFALL DATA
02471: *****
02472: *****
02473: FINISH
02474: *****
02475: *****
02476: *****
02477: *****
02478: R0067:CO0002 READ AES DATA
02479: *****
02480: *****
02481: *****
02482: *****
02483: *****
02484: *****
02485: *****
02486: *****
02487: *****
02488: *****
02489: *****
02490: *****
02491: *****
02492: *****
02493: *****
02494: *****
02495: *****
02496: *****
02497: *****
02498: *****
02499: *****
02500: *****
02501: *****
02502: *****
02503: *****
02504: *****
02505: *****
02506: *****
02507: *****
02508: *****
02509: *****
02510: *****
02511: *****
02512: *****
02513: *****
02514: *****
02515: *****
02516: *****
02517: *****
02518: *****
02519: *****
02520: *****

```

02521> \*\*\* WARNING: Requested start date is less than start date in file.  
02522> \*\*\* WARNING: Missing rainfall increments were set to 0.  
02523> \*\*\* WARNING: Requested start date is less than start date in file.  
02524> \*\*\* WARNING: Missing rainfall increments were set to 0.  
02525> Simulation ended on 2021-10-19 at 08:49:50  
02526> -----  
02527>

```

1  20      Metric units / ID Numbers OFF
2  *#*****
3  *# SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
4  *#*****
5  *# Project Name: Barrhaven Conservancy Development
6  *# Project Number: 1474
7  *# Date       : 2021/Oct/18
8  *# Modeller   : J.Burnett, P.Eng.
9  *# Company    : J.F. Sabourin and Associates
10 *# License #   : 2582634
11 *#*****
12 START          TZERO=[1967.0101], METOUT=[2], NSTORM=[0], NRUN=[67]
13 *%            [""] <--storm filename, one per line for NSTORM time
14 *%-----|-----
15 *# Ottawa International Airport (1967 - 2003)
16 READ AES DATA AES_FILENAME=["YOW_1967_2007.123"],
17                IELEM=[123], START_DATE=[0], END_DATE=[-364]
18 *%-----|-----
19 COMPUTE API    APII=[50], APIK=[0.90]/day
20 *%-----|-----
21 *#*****
22 *#                Barrhaven Conservancy Development Phase 3 (WITH INFILTRATION) -
23 POST DEVELOPMENT CONDITIONS
24 *#*****
25 *%-----|-----
26 CONTINUOUS STANDHYD NHYD=["W1"], DT=[5] (min), AREA=[8.92] (ha)
27                    XIMP=[0.54], TIMP=[0.64], DWF=[0] (cms),
28                    LOSS=[1]: Horton: Fo=[76.2] (mm/hr), Fc=[13.2] (mm/hr),
29                    DCAY=[4.14] (/hr), F=[0] (mm),
30                    Pervious areas: IAper=[4.67] (mm), SLPP=[2.0] (%), LGP=[40] (m),
31                    MNP=[0.250], SCP=[0] (min),
32                    Impervious areas: IAimp=[1.57] (mm), SLPI=[0.5] (%), LGI=[244] (m),
33                    MNI=[0.013], SCI=[0] (min),
34                    Continuous simulation parameters:
35                    IaRECper=[6] (hrs), IaRECimp=[1.5] (hrs),
36                    SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.03]/(mm),
37                    InterEventTime=[12] (hrs), END=-1
38 *%-----|-----
39 *# LID for Outlet W1
40 *# Assumed trench 1.25m wide 0.4 deep, 1991m long, porosity of 0.4 with 250mm
41 perforated pipe
42 *# Total Volume provided by LID - 344 m3
43 *# Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
44 ROUTE RESERVOIR NHYDout=["W1-LID"], NHYDin=["W1"], RDT=[5] (min),
45                    TABLE of ( OUTFLOW-STORAGE ) values
46                    (cms) - (ha-m)
47                    [ 0.0000 , 0.00000 ]
48                    [ 0.0019 , 0.00010 ]
49                    [ 0.0020 , 0.0344 ]
50                    [ -1 , -1 ]
51                    NHYDovf=["W1-LID-Out"],
52 *%-----|-----
53 *#*****
54 CONTINUOUS STANDHYD NHYD=["W2"], DT=[5] (min), AREA=[8.22] (ha)
55                    XIMP=[0.54], TIMP=[0.64], DWF=[0] (cms),
56                    LOSS=[1]: Horton: Fo=[76.2] (mm/hr), Fc=[13.2] (mm/hr),

```



```

50          DCAY=[4.14] (/hr), F=[0] (mm),
          Pervious areas: IAper=[4.67] (mm), SLPP=[2.0] (%), LGP=[40] (m),
          MNP=[0.250], SCP=[0] (min),
51          Impervious areas: IAimp=[1.57] (mm), SLPI=[0.5] (%), LGI=[234] (m),
          MNI=[0.013], SCI=[0] (min),
52          Continuous simulation parameters:
53          IaRECper=[6] (hrs), IaRECimp=[1.5] (hrs),
54          SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.03] / (mm),
          InterEventTime=[12] (hrs), END=-1

```

```

55  *%-----|-----
          |-----|

```

```

56  *# LID for Outlet W2
57  *# Assumed trench 1.25m wide 0.4 deep, 1896m long, porosity of 0.4 with 250mm
perforated pipe

```

```

58  *# Total Volume provided by LID - 330 m³
59  *# Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5

```

```

60  ROUTE RESERVOIR      NHYDout=["W2-LID"], NHYDin=["W2"], RDT=[5] (min),

```

```

61          TABLE of ( OUTFLOW-STORAGE ) values

```

```

62          (cms) - (ha-m)
63          [ 0.00000 , 0.00000 ]
64          [ 0.0018 , 0.00010 ]
65          [ 0.0019 , 0.0330 ]
66          [ -1 , -1 ]

```

```

67          NHYDovf=["W2-LID-Out"],

```

```

68  *%-----|-----
          |-----|

```

```

69  CONTINUOUS STANDHYD NHYD=["W3"], DT=[5] (min), AREA=[9.9] (ha)

```

```

70          XIMP=[0.54], TIMP=[0.64], DWF=[0] (cms),

```

```

71          LOSS=[1]: Horton: Fo=[76.2] (mm/hr), Fc=[13.2] (mm/hr),

```

```

72          DCAY=[4.14] (/hr), F=[0] (mm),

```

```

73          Pervious areas: IAper=[4.67] (mm), SLPP=[2.0] (%), LGP=[40] (m),

```

```

74          MNP=[0.250], SCP=[0] (min),

```

```

75          Impervious areas: IAimp=[1.57] (mm), SLPI=[0.5] (%), LGI=[257] (m),

```

```

76          MNI=[0.013], SCI=[0] (min),

```

```

77          Continuous simulation parameters:

```

```

78          IaRECper=[6] (hrs), IaRECimp=[1.5] (hrs),

```

```

79          SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.03] / (mm),

```

```

80          InterEventTime=[12] (hrs), END=-1

```

```

81  *%-----|-----
          |-----|

```

```

82  *# LID for Outlet W3

```

```

83  *# Assumed trench 1.25m wide 0.4 deep, 1693m long, porosity of 0.4 with 250mm
perforated pipe

```

```

84  *# Total Volume provided by LID - 303 m³

```

```

85  *# Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5

```

```

86  ROUTE RESERVOIR      NHYDout=["W3-LID"], NHYDin=["W3"], RDT=[5] (min),

```

```

87          TABLE of ( OUTFLOW-STORAGE ) values

```

```

88          (cms) - (ha-m)
89          [ 0.00000 , 0.00000 ]
90          [ 0.0017 , 0.0001 ]
91          [ 0.0017 , 0.0303 ]
92          [ -1 , -1 ]

```

```

93          NHYDovf=["W3-LID-Out"],

```

```

94  *%-----|-----
          |-----|

```

```

95  CONTINUOUS STANDHYD NHYD=["W4"], DT=[5] (min), AREA=[8.6] (ha)

```

```

96          XIMP=[0.54], TIMP=[0.64], DWF=[0] (cms),

```

```

97          LOSS=[1]: Horton: Fo=[76.2] (mm/hr), Fc=[13.2] (mm/hr),

```

```

98          DCAY=[4.14] (/hr), F=[0] (mm),

```

```

99          Pervious areas: IAper=[4.67] (mm), SLPP=[2.0] (%), LGP=[40] (m),

```

```

100         MNP=[0.250], SCP=[0] (min),

```

```

101         Impervious areas: IAimp=[1.57] (mm), SLPI=[0.5] (%), LGI=[239] (m),

```

```

102         MNI=[0.013], SCI=[0] (min),

```

```

103         Continuous simulation parameters:

```

```

104         IaRECper=[6] (hrs), IaRECimp=[1.5] (hrs),

```

```

105         SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.03] / (mm),

```

```

106         InterEventTime=[12] (hrs), END=-1

```

```

InterEventTime=[12] (hrs), END=-1
99  *%-----|-----
-----|
100 *# LID for Outlet W4
101 *# Assumed trench 1.25m wide 0.4 deep, 1693m long, porosity of 0.4 with 250mm
perforated pipe
102 *# Total Volume provided by LID - 303 m3
103 *# Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
104 ROUTE RESERVOIR NHYDout=["W4-LID"], NHYDin=["W4"], RDT=[5] (min),
105 TABLE of ( OUTFLOW-STORAGE ) values
106 (cms) - (ha-m)
107 [ 0.00000 , 0.00000 ]
108 [ 0.0017, 0.00010 ]
109 [ 0.0017, 0.0303 ]
110 [ -1 , -1 ]
111 NHYDovf=["W4-LID-Out"],
112 *%-----|-----
-----|
113 *Development Without LIDs
114 ADD HYD NHYDsum=["BCD-PH3"], NHYDs to add=["W1", "W2", "W3", "W4"]
115 *%-----|-----
-----|
116 *Development With LIDs
117 ADD HYD NHYDsum=["BCD-PH3-LID"], NHYDs to
add=["W1-LID-Out", "W2-LID-Out", "W3-LID-Out", "W4-LID-Out"]
118 *%-----|-----
-----|
119 *#*****
*****
120 *# Barrhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) -
POST DEVELOPMENT CONDITIONS
121 *#*****
*****
122 *# Set infiltration to 0 (CN = 99.99) for water balance analysis
123 *#*****
*****
124 CONTINUOUS STANDHYD NHYD=["INF-W1"], DT=[5] (min), AREA=[8.92] (ha)
125 XIMP=[0.54], TIMP=[0.64], DWF=[0] (cms),
126 LOSS=[2]: SCS curve number CN=[99.99],
127 Pervious areas: IAper=[4.67] (mm), SLPP=[2.0] (%), LGP=[40] (m),
MNP=[0.250], SCP=[0] (min),
128 Impervious areas: IAimp=[1.57] (mm), SLPI=[0.5] (%), LGI=[244] (m),
MNI=[0.013], SCI=[0] (min),
129 Continuous simulation parameters:
130 IaREcper=[6] (hrs), IaREcimp=[1.5] (hrs),
131 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.03]/(mm),
InterEventTime=[12] (hrs), END=-1
132 *%-----|-----
-----|
133 CONTINUOUS STANDHYD NHYD=["INF-W2"], DT=[5] (min), AREA=[8.22] (ha)
134 XIMP=[0.54], TIMP=[0.64], DWF=[0] (cms),
135 LOSS=[2]: SCS curve number CN=[99.99],
136 Pervious areas: IAper=[4.67] (mm), SLPP=[2.0] (%), LGP=[40] (m),
MNP=[0.250], SCP=[0] (min),
137 Impervious areas: IAimp=[1.57] (mm), SLPI=[0.5] (%), LGI=[234] (m),
MNI=[0.013], SCI=[0] (min),
138 Continuous simulation parameters:
139 IaREcper=[6] (hrs), IaREcimp=[1.5] (hrs),
140 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.03]/(mm),
InterEventTime=[12] (hrs), END=-1
141 *%-----|-----
-----|
142 CONTINUOUS STANDHYD NHYD=["INF-W3"], DT=[5] (min), AREA=[9.9] (ha)
143 XIMP=[0.54], TIMP=[0.64], DWF=[0] (cms),
144 LOSS=[2]: SCS curve number CN=[99.99],
145 Pervious areas: IAper=[4.67] (mm), SLPP=[2.0] (%), LGP=[40] (m),

```

146 MNP=[0.250], SCP=[0] (min),  
 Impervious areas: IAimp=[1.57] (mm), SLPI=[0.5] (%), LGI=[257] (m),  
 MNI=[0.013], SCI=[0] (min),  
 147 Continuous simulation parameters:  
 148 IaRECper=[6] (hrs), IaRECimp=[1.5] (hrs),  
 149 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.03]/(mm),  
 InterEventTime=[12] (hrs), END=-1

150 \*%-----	-----

151 **CONTINUOUS STANDHYD** NHYD=["INF-W4"], DT=[5] (min), AREA=[8.6] (ha)  
 152 XIMP=[0.54], TIMP=[0.64], DWF=[0] (cms),  
 153 LOSS=[2]: SCS curve number CN=[99.99],  
 154 Pervious areas: IAper=[4.67] (mm), SLPP=[2.0] (%), LGP=[40] (m),  
 MNP=[0.250], SCP=[0] (min),  
 155 Impervious areas: IAimp=[1.57] (mm), SLPI=[0.5] (%), LGI=[239] (m),  
 MNI=[0.013], SCI=[0] (min),  
 156 Continuous simulation parameters:  
 157 IaRECper=[6] (hrs), IaRECimp=[1.5] (hrs),  
 158 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.03]/(mm),  
 InterEventTime=[12] (hrs), END=-1

159 \*%-----	-----

160 \*Development Without Infiltration for water budget

161 **ADD HYD** NHYDsum=["INF-BCD-PH3"], NHYDs to add=["INF-W1", "INF-W2",  
 "INF-W3", "INF-W4"]

162 \*%-----	-----

163 \*#####

164 \*# CONTINUOUS RAINFALL DATA

165 \*#####

166 \*%-----	-----

167 \*%-----	-----

168 **START** TZERO=[1968.0101], METOUT=[2], NSTORM=[0], NRUN=[68]

169 \*%-----	-----

170 **START** TZERO=[1969.0101], METOUT=[2], NSTORM=[0], NRUN=[69]

171 \*%-----	-----

172 **START** TZERO=[1970.0101], METOUT=[2], NSTORM=[0], NRUN=[70]

173 \*%-----	-----

174 **START** TZERO=[1971.0101], METOUT=[2], NSTORM=[0], NRUN=[71]

175 \*%-----	-----

176 **START** TZERO=[1972.0101], METOUT=[2], NSTORM=[0], NRUN=[72]

177 \*%-----	-----

178 **START** TZERO=[1973.0101], METOUT=[2], NSTORM=[0], NRUN=[73]

179 \*%-----	-----

180 **START** TZERO=[1974.0101], METOUT=[2], NSTORM=[0], NRUN=[74]

181 \*%-----	-----

182 **START** TZERO=[1975.0101], METOUT=[2], NSTORM=[0], NRUN=[75]

183 \*%-----	-----

184 **START** TZERO=[1976.0101], METOUT=[2], NSTORM=[0], NRUN=[76]

185 \*%-----	-----

186 **START** TZERO=[1977.0101], METOUT=[2], NSTORM=[0], NRUN=[77]

187 \*%-----	-----

188 **START** TZERO=[1978.0101], METOUT=[2], NSTORM=[0], NRUN=[78]

189 \*%-----	-----

```
-----|
190 START          TZERO=[1979.0101], METOUT=[2], NSTORM=[0], NRUN=[79]
191 *%-----|
-----|
192 START          TZERO=[1980.0101], METOUT=[2], NSTORM=[0], NRUN=[80]
193 *%-----|
-----|
194 START          TZERO=[1981.0101], METOUT=[2], NSTORM=[0], NRUN=[81]
195 *%-----|
-----|
196 START          TZERO=[1982.0101], METOUT=[2], NSTORM=[0], NRUN=[82]
197 *%-----|
-----|
198 START          TZERO=[1983.0101], METOUT=[2], NSTORM=[0], NRUN=[83]
199 *%-----|
-----|
200 START          TZERO=[1984.0101], METOUT=[2], NSTORM=[0], NRUN=[84]
201 *%-----|
-----|
202 START          TZERO=[1985.0101], METOUT=[2], NSTORM=[0], NRUN=[85]
203 *%-----|
-----|
204 START          TZERO=[1986.0101], METOUT=[2], NSTORM=[0], NRUN=[86]
205 *%-----|
-----|
206 START          TZERO=[1987.0101], METOUT=[2], NSTORM=[0], NRUN=[87]
207 *%-----|
-----|
208 START          TZERO=[1988.0101], METOUT=[2], NSTORM=[0], NRUN=[88]
209 *%-----|
-----|
210 START          TZERO=[1989.0101], METOUT=[2], NSTORM=[0], NRUN=[89]
211 *%-----|
-----|
212 START          TZERO=[1990.0101], METOUT=[2], NSTORM=[0], NRUN=[90]
213 *%-----|
-----|
214 START          TZERO=[1991.0101], METOUT=[2], NSTORM=[0], NRUN=[91]
215 *%-----|
-----|
216 START          TZERO=[1992.0101], METOUT=[2], NSTORM=[0], NRUN=[92]
217 *%-----|
-----|
218 START          TZERO=[1993.0101], METOUT=[2], NSTORM=[0], NRUN=[93]
219 *%-----|
-----|
220 START          TZERO=[1994.0101], METOUT=[2], NSTORM=[0], NRUN=[94]
221 *%-----|
-----|
222 START          TZERO=[1995.0101], METOUT=[2], NSTORM=[0], NRUN=[95]
223 *%-----|
-----|
224 START          TZERO=[1996.0101], METOUT=[2], NSTORM=[0], NRUN=[96]
225 *%-----|
-----|
226 START          TZERO=[1997.0101], METOUT=[2], NSTORM=[0], NRUN=[97]
227 *%-----|
-----|
228 START          TZERO=[1998.0101], METOUT=[2], NSTORM=[0], NRUN=[98]
229 *%-----|
-----|
230 START          TZERO=[1999.0101], METOUT=[2], NSTORM=[0], NRUN=[99]
231 *%-----|
-----|
232 START          TZERO=[2000.0101], METOUT=[2], NSTORM=[0], NRUN=[100]
233 *%-----|
```

```
-----|
234  *% MISSING FROM AES RAINFALL DATA
235  *%START          TZERO=[2001.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[101]
236  *%-----|-----
-----|
237  START          TZERO=[2002.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[102]
238  *%-----|-----
-----|
239  START          TZERO=[2003.0101],  METOUT=[2],  NSTORM=[0],  NRUN=[103]
240  *%-----|-----
-----|
241  FINISH
```





00361# R0686C0001-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00362# CONTINUOUS STANDBY 5.0 01:1NF-W2 8.92 .193 1969.0817\_5:00 378.65\_6.39 .000
00363# [XMP=54:TIMP=.64]
00364# [LOSS=2:ICN=10.0]
00365# [Previous area: IArea= 4.67:SLFP=2.00:LGP= 40.0MP=250:SCP= .0]
00366# [Impervious area: IAlmp=1.57:SLIP=.50:LI=244.0MI=.013:ICI=.0]
00367# [IARECimp= 1.50: IARECPer= 6.00]
00368# [SMN= 1.39: SMAX= 9.24: SK= .030]
00369# R0686C0017-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00370# CONTINUOUS STANDBY 5.0 01:1NF-W2 8.92 .193 1969.0817\_5:00 378.65\_6.39 .000
00371# [XMP=54:TIMP=.64]
00372# [LOSS=2:ICN=10.0]
00373# [Previous area: IArea= 4.67:SLFP=2.00:LGP= 40.0MP=250:SCP= .0]
00374# [Impervious area: IAlmp=1.57:SLIP=.50:LI=244.0MI=.013:ICI=.0]
00375# [IARECimp= 1.50: IARECPer= 6.00]
00376# [SMN= 1.39: SMAX= 9.24: SK= .030]
00377# R0686C0018-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00378# CONTINUOUS STANDBY 5.0 01:1NF-W2 8.92 .193 1969.0817\_5:00 378.65\_6.39 .000
00379# [XMP=54:TIMP=.64]
00380# [LOSS=2:ICN=10.0]
00381# [Previous area: IArea= 4.67:SLFP=2.00:LGP= 40.0MP=250:SCP= .0]
00382# [Impervious area: IAlmp=1.57:SLIP=.50:LI=244.0MI=.013:ICI=.0]
00383# [IARECimp= 1.50: IARECPer= 6.00]
00384# [SMN= 1.39: SMAX= 9.24: SK= .030]
00385# R0686C0019-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00386# CONTINUOUS STANDBY 5.0 01:1NF-W2 8.60 .195 1969.0817\_5:00 378.65\_6.39 .000
00387# [XMP=54:TIMP=.64]
00388# [LOSS=2:ICN=10.0]
00389# [Previous area: IArea= 4.67:SLFP=2.00:LGP= 40.0MP=250:SCP= .0]
00390# [Impervious area: IAlmp=1.57:SLIP=.50:LI=239.0MI=.013:ICI=.0]
00391# [IARECimp= 1.50: IARECPer= 6.00]
00392# [SMN= 1.39: SMAX= 9.24: SK= .030]
00393# R0686C0018-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00394# ADD HYD + 5.0 02:1NF-W2 8.92 .193 1969.0817\_5:00 378.65 n/a .000
00395# + 5.0 02:1NF-W2 8.92 .193 1969.0817\_5:00 378.65 n/a .000
00396# + 5.0 02:1NF-W2 8.92 .193 1969.0817\_5:00 378.65 n/a .000
00397# + 5.0 02:1NF-W2 8.92 .193 1969.0817\_5:00 378.65 n/a .000
00398# + 5.0 01:1NF-W2 8.92 .193 1969.0817\_5:00 378.65 n/a .000
00399# SUM 35.64 3.127 1969.0817\_5:00 378.65 n/a .000
00400# \*\*\*\*\*
00401# \*\*\*\*\*
00402# \*\*\*\*\*
00403# \*\*\*\*\*
00404# \*\*\*\*\*
00405# \*\*\*\*\*
00406# \*\*\*\*\*
00407# \*\*\*\*\*
00408# \*\*\*\*\*
00409# \*\*\*\*\*
00410# RvM:COMMANDS
00411# R0686C0001-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00412# START \*\*\*\*\*
00413# [TZERO = .00 hrs on 1969/01/01]
00414# [MTOPT= 2 (1-Imperial, 2-metric output)]
00415# [MFORM= 0]
00416# [MUN = 0069]
00417# \*\*\*\*\*
00418# # SWHYD Ver:5.02/Jan 2001 «BETA» / INPUT DATA FILE
00419# \*\*\*\*\*
00420# # Project Name: Barhaves Conservancy Development
00421# # Project Number: 1474
00422# # Date : 2021/Oct/18
00423# # Modeler : J.Burnett, P.Eng.
00424# # Company : J.F. Sabourin and Associates
00425# # License #: 258234
00426# # Octava International Airport (1967 - 2003)
00427# \*\*\*\*\*
00428# R0686C0002-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00429# # HEAD AREA DATA
00430# [Filename = YOM\_1967\_2007\_123 ]
00431# [Start\_date= 1969\_0101; End\_date= 1969\_1231]
00432# [DT= 60:Min; Length= 960; WetPer= 470; DryPer= 8390; PTO= 570.30]
00433# Maximum average rainfall intensities over
00434# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00435# 21.10 36.25 46.70 67.20 80.30 90.50 102.10 114.00 126.60 mm/hr
00436# 21.10 32.50 32.50 46.70 67.20 80.30 90.50 102.10 114.00 mm/hr
00437# 1969018 1969018 1969018 1969018 1969018 1969018 1969018 1969018 1969018 date
00438# Number of rainfall events per following interval time
00439# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00440# 157 119 72 58 49 43 32
00441# Number of events with at least the following durations
00442# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00443# 156 84 58 21 5 0 0 0 0
00444# R0686C0003-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00445# COMPUTE API
00446# [APIIn= 50.00; APIkty= 9900; APIkdt= .9956]
00447# [APIOut= 171.00; APIkty= 9900; APIkdt= .9956]
00448# \*\*\*\*\*
00449# # Barhaves Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITIONS
00450# \*\*\*\*\*
00451# R0686C0004-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00452# CONTINUOUS STANDBY 5.0 01:1NF-W2 8.92 .142 1969.0818\_2:00 226.65\_3.97 .000
00453# [XMP=54:TIMP=.64]
00454# [Horton parameters: Fw= 76.20:Fc= 13.20:DCAV=4.14: F= .00]
00455# [Previous area: IArea= 4.67:SLFP=2.00:LGP= 40.0MP=250:SCP= .0]
00456# [Impervious area: IAlmp=1.57:SLIP=.50:LI=244.0MI=.013:ICI=.0]
00457# [IARECimp= 1.50: IARECPer= 6.00]
00458# # LID for Outlet W
00459# # Assumed trench 1.25m wide 0.4 deep, 193m long, porosity of 0.4 with 250mm perforated pipe
00460# # Total Volume provided by LID = 303 m³
00461# # Soil infiltration rates assumed at 9m/hr with a safety factor of 2.5
00462# R0686C0005-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00463# ROUTE RESERVOIR -> 5.0 02:1NF-W2 8.92 .342 1969.0818\_2:00 226.65 n/a .000
00464# out <= 5.0 01:1NF-LID 4.92 .002 1969.0124\_12:55 226.65 n/a .000
00465# overflow <= 5.0 03:1NF-LID 4.00 .135 1969.0818\_2:00 226.65 n/a .000
00466# [MstOfsed=.3420E-01 m3, TotOfVol=.9066E+00 m3, N-Ofv= .55, TotDurOfv= 104 hrs]
00467# R0686C0006-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00468# CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .315 1969.0818\_2:00 226.65\_3.97 .000
00469# [XMP=54:TIMP=.64]
00470# [Horton parameters: Fw= 76.20:Fc= 13.20:DCAV=4.14: F= .00]
00471# [Previous area: IArea= 4.67:SLFP=2.00:LGP= 40.0MP=250:SCP= .0]
00472# [Impervious area: IAlmp=1.57:SLIP=.50:LI=244.0MI=.013:ICI=.0]
00473# [IARECimp= 1.50: IARECPer= 6.00]
00474# # LID for Outlet W
00475# # Assumed trench 1.25m wide 0.4 deep, 169m long, porosity of 0.4 with 250mm perforated pipe
00476# # Total Volume provided by LID = 303 m³
00477# # Soil infiltration rates assumed at 9m/hr with a safety factor of 2.5
00478# R0686C0007-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00479# ROUTE RESERVOIR -> 5.0 02:1NF-W2 8.22 .315 1969.0818\_2:00 226.65 n/a .000
00480# out <= 5.0 01:1NF-LID 4.44 .002 1969.0124\_8:55 226.65 n/a .000
00481# overflow <= 5.0 03:1NF-LID 5.20 .272 1969.0818\_2:00 226.65 n/a .000
00482# [MstOfsed=.3029E-01 m3, TotOfVol=.1120E+01 m3, N-Ofv= .59, TotDurOfv= 104 hrs]
00483# R0686C0008-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00484# CONTINUOUS STANDBY 5.0 01:1NF-W2 9.90 .379 1969.0818\_2:00 226.65\_3.97 .000
00485# [XMP=54:TIMP=.64]
00486# [Horton parameters: Fw= 76.20:Fc= 13.20:DCAV=4.14: F= .00]
00487# [Previous area: IArea= 4.67:SLFP=2.00:LGP= 40.0MP=250:SCP= .0]
00488# [Impervious area: IAlmp=1.57:SLIP=.50:LI=251.0MI=.013:ICI=.0]
00489# [IARECimp= 1.50: IARECPer= 6.00]
00490# # LID for Outlet W
00491# # Assumed trench 1.25m wide 0.4 deep, 163m long, porosity of 0.4 with 250mm perforated pipe
00492# # Total Volume provided by LID = 303 m³
00493# # Soil infiltration rates assumed at 9m/hr with a safety factor of 2.5
00494# R0686C0009-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00495# ROUTE RESERVOIR -> 5.0 02:1NF-W2 8.60 .330 1969.0818\_2:00 226.65 n/a .000
00496# out <= 5.0 01:1NF-LID 4.44 .002 1969.0124\_8:55 226.65 n/a .000
00497# overflow <= 5.0 03:1NF-LID 5.20 .272 1969.0818\_2:00 226.65 n/a .000
00498# [MstOfsed=.3029E-01 m3, TotOfVol=.1200E+01 m3, N-Ofv= .67, TotDurOfv= 127 hrs]
00499# R0686C0010-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00500# CONTINUOUS STANDBY 5.0 01:1NF-W2 8.60 .330 1969.0818\_2:00 226.65\_3.97 .000
00501# [XMP=54:TIMP=.64]
00502# [Horton parameters: Fw= 76.20:Fc= 13.20:DCAV=4.14: F= .00]
00503# [Previous area: IArea= 4.67:SLFP=2.00:LGP= 40.0MP=250:SCP= .0]
00504# [Impervious area: IAlmp=1.57:SLIP=.50:LI=239.0MI=.013:ICI=.0]
00505# [IARECimp= 1.50: IARECPer= 6.00]
00506# # LID for Outlet W
00507# # Assumed trench 1.25m wide 0.4 deep, 163m long, porosity of 0.4 with 250mm perforated pipe
00508# # Total Volume provided by LID = 303 m³
00509# # Soil infiltration rates assumed at 9m/hr with a safety factor of 2.5
00510# R0686C0011-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00511# ROUTE RESERVOIR -> 5.0 02:1NF-W2 8.60 .330 1969.0818\_2:00 226.65 n/a .000
00512# out <= 5.0 01:1NF-LID 4.44 .002 1969.0124\_8:55 226.65 n/a .000
00513# overflow <= 5.0 03:1NF-LID 4.16 .232 1969.0818\_2:00 226.65 n/a .000
00514# [MstOfsed=.3029E-01 m3, TotOfVol=.3424E+00 m3, N-Ofv= .59, TotDurOfv= 114 hrs]
00515# R0686C0012-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00516# ADD HYD + 5.0 02:1NF-W2 8.92 .342 1969.0818\_2:00 226.65 n/a .000
00517# + 5.0 02:1NF-W2 8.92 .342 1969.0818\_2:00 226.65 n/a .000
00518# + 5.0 02:1NF-W2 8.92 .342 1969.0818\_2:00 226.65 n/a .000
00519# + 5.0 02:1NF-W2 8.92 .342 1969.0818\_2:00 226.65 n/a .000
00520# + 5.0 01:1NF-W2 8.92 .342 1969.0818\_2:00 226.65 n/a .000
00521# R0686C0013-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00522# ADD HYD + 5.0 01:1NF-W2 8.60 .330 1969.0818\_2:00 226.65 n/a .000
00523# + 5.0 02:1NF-LID 4.92 .002 1969.0124\_12:55 226.65 n/a .000
00524# + 5.0 02:1NF-LID 4.92 .002 1969.0124\_12:55 226.65 n/a .000
00525# + 5.0 02:1NF-LID 4.92 .002 1969.0124\_12:55 226.65 n/a .000
00526# + 5.0 01:1NF-W2 8.60 .330 1969.0818\_2:00 226.65 n/a .000
00527# SUM 5.0 01:1NF-W2 17.03 1.328 1969.0818\_2:00 226.65 n/a .000
00528# \*\*\*\*\*
00529# # Barhaves Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDITIONS
00530# \*\*\*\*\*
00531# # Set Infiltration to 0 (CN = 99.99) for water balance analysis
00532# R0686C0014-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00533# CONTINUOUS STANDBY 5.0 01:1NF-W2 8.92 .507 1969.0818\_2:00 349.05\_6.12 .000
00534# [XMP=54:TIMP=.64]
00535# [LOSS=2:ICN=10.0]
00536# [Previous area: IArea= 4.67:SLFP=2.00:LGP= 40.0MP=250:SCP= .0]
00537# [Impervious area: IAlmp=1.57:SLIP=.50:LI=244.0MI=.013:ICI=.0]
00538# [IARECimp= 1.50: IARECPer= 6.00]
00539# [SMN= 1.39: SMAX= 9.24: SK= .030]
00540# R0686C0015-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00541# CONTINUOUS STANDBY 5.0 01:1NF-W2 8.92 .468 1969.0818\_2:00 349.05\_6.12 .000
00542# [XMP=54:TIMP=.64]
00543# [LOSS=2:ICN=10.0]
00544# [Previous area: IArea= 4.67:SLFP=2.00:LGP= 40.0MP=250:SCP= .0]
00545# [Impervious area: IAlmp=1.57:SLIP=.50:LI=234.0MI=.013:ICI=.0]
00546# [IARECimp= 1.50: IARECPer= 6.00]
00547# [SMN= 1.39: SMAX= 9.24: SK= .030]
00548# R0686C0016-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00549# CONTINUOUS STANDBY 5.0 01:1NF-W2 9.90 .562 1969.0818\_2:00 349.05\_6.12 .000
00550# [XMP=54:TIMP=.64]
00551# [LOSS=2:ICN=10.0]
00552# [Previous area: IArea= 4.67:SLFP=2.00:LGP= 40.0MP=250:SCP= .0]
00553# [Impervious area: IAlmp=1.57:SLIP=.50:LI=257.0MI=.013:ICI=.0]
00554# [IARECimp= 1.50: IARECPer= 6.00]
00555# [SMN= 1.39: SMAX= 9.24: SK= .030]
00556# R0686C0017-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00557# CONTINUOUS STANDBY 5.0 01:1NF-W2 8.60 .489 1969.0818\_2:00 349.05\_6.12 .000
00558# [XMP=54:TIMP=.64]
00559# [LOSS=2:ICN=10.0]
00560# [Previous area: IArea= 4.67:SLFP=2.00:LGP= 40.0MP=250:SCP= .0]
00561# [Impervious area: IAlmp=1.57:SLIP=.50:LI=239.0MI=.013:ICI=.0]
00562# [IARECimp= 1.50: IARECPer= 6.00]
00563# [SMN= 1.39: SMAX= 9.24: SK= .030]
00564# R0686C0018-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00565# ADD HYD + 5.0 02:1NF-W2 8.22 .468 1969.0818\_2:00 349.05 n/a .000
00566# + 5.0 02:1NF-W2 8.22 .468 1969.0818\_2:00 349.05 n/a .000
00567# + 5.0 02:1NF-W2 8.22 .468 1969.0818\_2:00 349.05 n/a .000
00568# + 5.0 02:1NF-W2 8.22 .468 1969.0818\_2:00 349.05 n/a .000
00569# + 5.0 01:1NF-W2 8.22 .468 1969.0818\_2:00 349.05 n/a .000
00570# \*\*\*\*\*
00571# # CONTINUOUS RAINFALL DATA
00572# \*\*\*\*\*
00573# # END OF RUN : 69
00574# \*\*\*\*\*
00575# \*\*\*\*\*
00576# \*\*\*\*\*
00577# \*\*\*\*\*
00578# \*\*\*\*\*
00579# \*\*\*\*\*
00580# \*\*\*\*\*
00581# RvM:COMMANDS
00582# [TZERO = .00 hrs on 1970/01/01]
00583# [MFORM= 0 (1-Imperial, 2-metric output)]
00584# [MTOPT= 0]
00585# [MUN = 0069]
00586# \*\*\*\*\*
00587# \*\*\*\*\*
00588# \*\*\*\*\*
00589# # SWHYD Ver:5.02/Jan 2001 «BETA» / INPUT DATA FILE
00590# \*\*\*\*\*
00591# # Project Name: Barhaves Conservancy Development
00592# # Project Number: 1474
00593# # Date : 2021/Oct/18
00594# # Modeler : J.Burnett, P.Eng.
00595# # Company : J.F. Sabourin and Associates
00596# # License #: 258234
00597# # Octava International Airport (1967 - 2003)
00598# \*\*\*\*\*
00599# R0700C0002-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00600# # HEAD AREA DATA
00601# [Filename = YOM\_1967\_2007\_123 ]
00602# [Start\_date= 1969\_0101; End\_date= 1970\_1231]
00603# [DT= 60:Min; Length= 8760; WetPer= 373; DryPer= 8387; PTO= 558.90]
00604# Maximum average rainfall intensities over
00605# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00606# 35.30 35.30 46.70 67.20 80.30 90.50 102.10 114.00 126.60 mm/hr
00607# 35.30 35.30 46.70 67.20 80.30 90.50 102.10 114.00 126.60 mm/hr
00608# 1970026 1970026 1970026 1970026 1970027 1970028 1970029 1970030 1970031 date
00609# Number of rainfall events per following interval time
00610# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00611# 148 127 109 84 72 60 54 41 30
00612# Number of events with at least the following durations
00613# 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00614# 147 79 40 15 3 0 0 0 0
00615# R0700C0003-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00616# COMPUTE API
00617# [APIIn= 50.00; APIkty= 9900; APIkdt= .9956]
00618# [APIOut= 171.00; APIkty= 9900; APIkdt= .9956]
00619# \*\*\*\*\*
00620# # Barhaves Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITIONS
00621# \*\*\*\*\*
00622# R0700C0004-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00623# CONTINUOUS STANDBY 5.0 01:1NF-W2 8.92 .630 1970.0926\_2:10 230.67\_4.13 .000
00624# [XMP=54:TIMP=.64]
00625# [Horton parameters: Fw= 76.20:Fc= 13.20:DCAV=4.14: F= .00]
00626# [Previous area: IArea= 4.67:SLFP=2.00:LGP= 40.0MP=250:SCP= .0]
00627# [Impervious area: IAlmp=1.57:SLIP=.50:LI=244.0MI=.013:ICI=.0]
00628# [IARECimp= 1.50: IARECPer= 6.00]
00629# # LID for Outlet W
00630# # Assumed trench 1.25m wide 0.4 deep, 193m long, porosity of 0.4 with 250mm perforated pipe
00631# # Total Volume provided by LID = 344 m³
00632# # Soil infiltration rates assumed at 9m/hr with a safety factor of 2.5
00633# R0700C0005-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00634# ROUTE RESERVOIR -> 5.0 02:1NF-W2 8.92 .630 1970.0926\_2:10 230.67 n/a .000
00635# out <= 5.0 01:1NF-LID 4.84 .002 1970.0202\_14:00 230.67 n/a .000
00636# overflow <= 5.0 03:1NF-LID 4.07 .615 1970.0926\_2:10 230.67 n/a .000
00637# [MstOfsed=.2438E-01 m3, TotOfVol=.3298E+00 m3, N-Ofv= 60, TotDurOfv= 6 hrs]
00638# R0700C0006-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00639# CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .581 1970.0926\_2:10 230.67\_4.13 .000
00640# [XMP=54:TIMP=.64]
00641# [Horton parameters: Fw= 76.20:Fc= 13.20:DCAV=4.14: F= .00]
00642# [Previous area: IArea= 4.67:SLFP=2.00:LGP= 40.0MP=250:SCP= .0]
00643# [Impervious area: IAlmp=1.57:SLIP=.50:LI=234.0MI=.013:ICI=.0]
00644# [IARECimp= 1.50: IARECPer= 6.00]
00645# # LID for Outlet W
00646# # Assumed trench 1.25m wide 0.4 deep, 189m long, porosity of 0.4 with 250mm perforated pipe
00647# # Total Volume provided by LID = 330 m³
00648# # Soil infiltration rates assumed at 9m/hr with a safety factor of 2.5
00649# R0700C0007-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00650# ROUTE RESERVOIR -> 5.0 02:1NF-W2 8.60 .608 1970.0926\_2:10 230.67 n/a .000
00651# out <= 5.0 01:1NF-LID 4.58 .002 1970.0202\_14:00 230.67 n/a .000
00652# overflow <= 5.0 03:1NF-LID 4.64 .627 1970.0926\_2:10 230.67 n/a .000
00653# [MstOfsed=.2399E-01 m3, TotOfVol=.8404E+00 m3, N-Ofv= 64, TotDurOfv= 74 hrs]
00654# R0700C0008-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00655# CONTINUOUS STANDBY 5.0 01:1NF-W2 8.60 .698 1970.0926\_2:10 230.67\_4.13 .000
00656# [XMP=54:TIMP=.64]
00657# [Horton parameters: Fw= 76.20:Fc= 13.20:DCAV=4.14: F= .00]
00658# [Previous area: IArea= 4.67:SLFP=2.00:LGP= 40.0MP=250:SCP= .0]
00659# [Impervious area: IAlmp=1.57:SLIP=.50:LI=257.0MI=.013:ICI=.0]
00660# [IARECimp= 1.50: IARECPer= 6.00]
00661# # LID for Outlet W
00662# # Assumed trench 1.25m wide 0.4 deep, 163m long, porosity of 0.4 with 250mm perforated pipe
00663# # Total Volume provided by LID = 303 m³
00664# # Soil infiltration rates assumed at 9m/hr with a safety factor of 2.5
00665# R0700C0009-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00666# ROUTE RESERVOIR -> 5.0 02:1NF-W2 9.90 .698 1970.0926\_2:10 230.67 n/a .000
00667# out <= 5.0 02:1NF-LID 4.58 .002 1970.0202\_14:00 230.67 n/a .000
00668# overflow <= 5.0 03:1NF-LID 5.20 .374 1970.0926\_2:10 230.67 n/a .000
00669# [MstOfsed=.2030E-01 m3, TotOfVol=.1233E+01 m3, N-Ofv= 68, TotDurOfv= 94 hrs]
00670# R0700C0010-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00671# CONTINUOUS STANDBY 5.0 01:1NF-W2 8.60 .608 1970.0926\_2:10 230.67\_4.13 .000
00672# [XMP=54:TIMP=.64]
00673# [Horton parameters: Fw= 76.20:Fc= 13.20:DCAV=4.14: F= .00]
00674# [Previous area: IArea= 4.67:SLFP=2.00:LGP= 40.0MP=250:SCP= .0]
00675# [Impervious area: IAlmp=1.57:SLIP=.50:LI=239.0MI=.013:ICI=.0]
00676# [IARECimp= 1.50: IARECPer= 6.00]
00677# # LID for Outlet W
00678# # Assumed trench 1.25m wide 0.4 deep, 163m long, porosity of 0.4 with 250mm perforated pipe
00679# # Total Volume provided by LID = 303 m³
00680# # Soil infiltration rates assumed at 9m/hr with a safety factor of 2.5
00681# R0700C0011-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00682# ROUTE RESERVOIR -> 5.0 02:1NF-W2 8.60 .608 1970.0926\_2:10 230.67 n/a .000
00683# out <= 5.0 01:1NF-LID 4.38 .002 1970.0202\_14:00 230.67 n/a .000
00684# overflow <= 5.0 03:1NF-LID 4.22 .593 1970.0926\_2:10 230.67 n/a .000
00685# [MstOfsed=.2029E-01 m3, TotOfVol=.9728E+00 m3, N-Ofv= 81, TotDurOfv= 83 hrs]
00686# R0700C0012-----Dtain-ID:INHYD-----AREAA-QFEARCS-TpeakDate\_hh:mm-----RvM-R-C-----DWFCMS
00687# ADD HYD + 5.0 02:1NF-W2 8.22 .581 1970.0926\_2:10 230.67 n/a .000
00688# + 5.0 02:1NF-W2 8.22 .581 1970.0926\_2:10 230.67 n/a .000
00689# + 5.0 02:1NF-W2 8.22 .581 1970.0926\_2:10 230.67 n/a .000
00690# + 5.0 02

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00721 [XIMP=54;TIMP=64]
00722 [LQSS=2;CN=100.0]
00723 [Impervious area: IArea= 4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
00724 [Impervious area: IArea= 1.57;SIFP= .50;LGI= 239.1;MNI= .013;SCI= .0]
00725 [SIMP= 1.39;SMAX= 9.24;SK= .030]
00726 [IAreaCimp= 1.50;IAECPe= 6.00]
00727 [SIMP= 1.39;SMAX= 9.24;SK= .030]
00728 CONTINUOUS STANDYD 5.0 01:1NF-W4 8.60 .814 1970.0925,21.000 341.01 610 .000
00729 [XIMP=54;TIMP=64]
00730 [LQSS=2;CN=100.0]
00731 [Impervious area: IArea= 4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
00732 [Impervious area: IArea= 1.57;SIFP= .50;LGI= 239.1;MNI= .013;SCI= .0]
00733 [IAreaCimp= 1.50;IAECPe= 6.00]
00734 [SIMP= 1.39;SMAX= 9.24;SK= .030]
00735 R071C0011-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00736 ADD HYD + 5.0 02:1NF-W1 8.92 .833 1970.0925,21.000 341.01 n/a .000
00737 + 5.0 02:1NF-W2 8.22 .719 1971.0810,15.000 300.01 n/a .000
00738 + 5.0 02:1NF-W3 9.90 .922 1970.0925,21.000 341.01 n/a .000
00739 + 5.0 02:1NF-W4 8.60 .814 1970.0925,21.000 341.01 n/a .000
00740 [Filename SUM= 3.148 1970.0925,21.000 341.01 n/a .000]
00741 *****
00742 # CONTINUOUS STANDYD 5.0 01:1NF-W4 8.60 .814 1970.0925,21.000 341.01 n/a .000
00743 *****
00744 ** END OF RUN : 70
00745 *****
00746 *****
00747 *****
00748 *****
00749 *****
00750 *****
00751 *****
00752 RUN:COMMAND#
00753 R071C0001-----
00754 START
00755 [TZERO= .00 hrs on 19710101]
00756 [MOUT= 2 (1=Imperial, 2=metric output)]
00757 [INSTORM= 0]
00758 [NUN= .0071]
00759 *****
00760 # SMHYND Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00761 *****
00762 # Project Name: Barhaven Conservancy Development
00763 # Project Number: 1474
00764 # Date : 2/21/02/Oct/18
00765 # Modeler : J.P. Sabourin & P.Eng.
00766 # Company : J.P. Sabourin and Associates
00767 # License # : 2582634
00768 *****
00769 # Ottawa International Airport (1967 - 2003)
00770 R071C0002-----
00771 # READ AED DATA
00772 [Filename = YOM_1967_2007_123 ]
00773 [Start_date= 1971.0101; End_date= 1971.1231]
00774 [ID= 60;min: Length= 9760;hrs: Wetness= 412; Dryhrs= 8348; PTOF= 522.10]
00775 Maximum average rainfall intensities over
00776 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00777 24.60 16.40 11.67 6.13 3.09 1.36 2.06 .79 .54 mm/hr
00778 24.60 33.20 35.00 36.80 37.10 37.40 38.00 38.00 38.90
00779 19710810 19710810 19710810 19710810 19710810 19710810 19710810 19710810 19710830 date
00780 Number of rainfall events per following interval time
00781 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00782 155 123 113 93 12 52 42 33
00783 Number of events with at least the following durations
00784 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00785 81 59 21 2 0 0 0
00786 R071C0003-----
00787 COMPUTE API
00788 [API= 50.00; APIKdy= .9000; APIKdt= .9956]
00789 [APIave= 62.22; APIavg= 14.84; APImin= .36]
00790 *****
00791 # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITIONS
00792 *****
00793 # CONTINUOUS STANDYD-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00794 CONTINUOUS STANDYD 5.0 01:1NF 8.92 .374 1971.0810,15.000 201.40 386 .000
00795 [XIMP=54;TIMP=64]
00796 [Horton parameters: Fw= 76.20;Fc= 13.20;DCAV= 4.14; F= .00]
00797 [Impervious area: IArea= 4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
00798 [Impervious area: IArea= 1.57;SIFP= .50;LGI= 244.1;MNI= .013;SCI= .0]
00799 [IAreaCimp= 1.50;IAECPe= 6.00]
00800 # LID for Outlet W4
00801 # Assumed trench 1.25m wide 0.4 deep, 193m long, porosity of 0.4 with 250mm perforated pipe
00802 # Total Volume provided by LID = 344 m³
00803 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00804 R071C0004-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00805 ROUTE RESERVOIR -> 5.0 02:1NF 8.22 .345 1971.0810,15.000 201.40 n/a .000
00806 out <= 5.0 01:1NF-LID 5.31 .002 1971.0504,10.435 201.40 n/a .000
00807 overlow <= 5.0 03:1NF-LID 4.41 .404 1971.0810,15.000 201.40 n/a .000
00808 [MxTotDsed=.3434E-01 m3, TotDVol= .6668E+00 m3, N-Over= .51, TotDOver= .51 hrs]
00809 R071C0005-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00810 CONTINUOUS STANDYD-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00811 [XIMP=54;TIMP=64]
00812 [Horton parameters: Fw= 76.20;Fc= 13.20;DCAV= 4.14; F= .00]
00813 [Impervious area: IArea= 4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
00814 [Impervious area: IArea= 1.57;SIFP= .50;LGI= 234.1;MNI= .013;SCI= .0]
00815 [IAreaCimp= 1.50;IAECPe= 6.00]
00816 # LID for Outlet W4
00817 # Assumed trench 1.25m wide 0.4 deep, 193m long, porosity of 0.4 with 250mm perforated pipe
00818 # Total Volume provided by LID = 330 m³
00819 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00820 R071C0006-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00821 ROUTE RESERVOIR -> 5.0 02:1NF 8.22 .345 1971.0810,15.000 201.40 n/a .000
00822 out <= 5.0 01:1NF-LID 5.31 .002 1971.0504,10.435 201.40 n/a .000
00823 overlow <= 5.0 03:1NF-LID 4.41 .404 1971.0810,15.000 201.40 n/a .000
00824 [MxTotDsed=.3101E-01 m3, TotDVol=.6075E+00 m3, N-Over= .46, TotDOver= .47 hrs]
00825 R071C0007-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00826 CONTINUOUS STANDYD 5.0 01:1NF 9.90 .414 1971.0810,15.000 201.40 386 .000
00827 [XIMP=54;TIMP=64]
00828 [Horton parameters: Fw= 76.20;Fc= 13.20;DCAV= 4.14; F= .00]
00829 [Impervious area: IArea= 4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
00830 [Impervious area: IArea= 1.57;SIFP= .50;LGI= 257.1;MNI= .013;SCI= .0]
00831 [IAreaCimp= 1.50;IAECPe= 6.00]
00832 # LID for Outlet W4
00833 # Assumed trench 1.25m wide 0.4 deep, 163m long, porosity of 0.4 with 250mm perforated pipe
00834 # Total Volume provided by LID = 303 m³
00835 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00836 R071C0008-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00837 ROUTE RESERVOIR -> 5.0 02:1NF 8.22 .345 1971.0810,15.000 201.40 n/a .000
00838 out <= 5.0 01:1NF-LID 5.19 .002 1971.0212,18.45 201.45 n/a .000
00839 overlow <= 5.0 03:1NF-LID 4.71 .404 1971.0810,15.000 201.40 n/a .000
00840 [MxTotDsed=.3029E-01 m3, TotDVol=.9481E+00 m3, N-Over= .64, TotDOver= .72 hrs]
00841 R071C0009-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00842 CONTINUOUS STANDYD 5.0 01:1NF 8.60 .360 1971.0810,15.000 201.40 386 .000
00843 [XIMP=54;TIMP=64]
00844 [Horton parameters: Fw= 76.20;Fc= 13.20;DCAV= 4.14; F= .00]
00845 [Impervious area: IArea= 4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
00846 [Impervious area: IArea= 1.57;SIFP= .50;LGI= 239.1;MNI= .013;SCI= .0]
00847 [IAreaCimp= 1.50;IAECPe= 6.00]
00848 # LID for Outlet W4
00849 # Assumed trench 1.25m wide 0.4 deep, 163m long, porosity of 0.4 with 250mm perforated pipe
00850 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00851 R071C0010-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00852 ROUTE RESERVOIR -> 5.0 02:1NF 8.60 .360 1971.0810,15.000 201.40 n/a .000
00853 out <= 5.0 01:1NF-LID 4.97 .002 1971.0212,18.50 201.45 n/a .000
00854 overlow <= 5.0 03:1NF-LID 3.63 .352 1971.0810,15.000 201.40 n/a .000
00855 [MxTotDsed=.3029E-01 m3, TotDVol=.7110E+00 m3, N-Over= .53, TotDOver= .60 hrs]
00856 R071C0011-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00857 ADD HYD + 5.0 02:1NF 8.92 .374 1971.0810,15.000 201.40 n/a .000
00858 + 5.0 02:1NF 8.22 .345 1971.0810,15.000 201.40 n/a .000
00859 + 5.0 02:1NF 9.90 .414 1971.0810,15.000 201.40 n/a .000
00860 + 5.0 02:1NF 8.60 .360 1971.0810,15.000 201.40 n/a .000
00861 [Filename SUM= 3.148 1970.0925,21.000 341.01 n/a .000]
00862 R071C0012-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00863 ADD HYD + 5.0 02:1NF-LID 3.41 .364 1971.0810,15.000 201.40 n/a .000
00864 + 5.0 02:1NF-LID 3.02 .336 1971.0810,15.000 201.40 n/a .000
00865 + 5.0 02:1NF-LID 4.71 .404 1971.0810,15.000 201.40 n/a .000
00866 + 5.0 02:1NF-LID 3.63 .352 1971.0810,15.000 201.40 n/a .000
00867 [Filename SUM= 14.76 1.456 1971.0810,15.000 201.40 n/a .000]
00868 *****
00869 # Barhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDITIONS
00870 *****
00871 # Set infiltration to 0 (CN = 99.99) for water balance analysis
00872 *****
00873 # CONTINUOUS STANDYD-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00874 R071C0013-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00875 CONTINUOUS STANDYD 5.0 01:1NF-W2 8.22 .527 1971.0810,15.000 300.01 575 .000
00876 [XIMP=54;TIMP=64]
00877 [LQSS=2;CN=100.0]
00878 [Impervious area: IArea= 4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
00879 [Impervious area: IArea= 1.57;SIFP= .50;LGI= 244.1;MNI= .013;SCI= .0]
00880 [SIMP= 1.39;SMAX= 9.24;SK= .030]
00881 [IAreaCimp= 1.50;IAECPe= 6.00]
00882 R071C0014-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00883 CONTINUOUS STANDYD 5.0 01:1NF-W2 8.22 .527 1971.0810,15.000 300.01 575 .000
00884 [XIMP=54;TIMP=64]
00885 [LQSS=2;CN=100.0]
00886 [Impervious area: IArea= 4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
00887 [Impervious area: IArea= 1.57;SIFP= .50;LGI= 234.1;MNI= .013;SCI= .0]
00888 [SIMP= 1.39;SMAX= 9.24;SK= .030]
00889 [IAreaCimp= 1.50;IAECPe= 6.00]
00890 R071C0015-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00891 CONTINUOUS STANDYD 5.0 01:1NF-W4 9.90 .632 1971.0810,15.000 300.01 575 .000
00892 [XIMP=54;TIMP=64]
00893 [LQSS=2;CN=100.0]
00894 [Impervious area: IArea= 4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
00895 [Impervious area: IArea= 1.57;SIFP= .50;LGI= 257.1;MNI= .013;SCI= .0]
00896 [SIMP= 1.39;SMAX= 9.24;SK= .030]
00897 [IAreaCimp= 1.50;IAECPe= 6.00]
00898 R071C0016-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00899 CONTINUOUS STANDYD 5.0 01:1NF-W4 8.60 .551 1971.0810,15.000 300.01 575 .000
00900 [XIMP=54;TIMP=64]

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00901 [LQSS=2;CN=100.0]
00902 [Previous area: IArea= 4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
00903 [Impervious area: IArea= 1.57;SIFP= .50;LGI= 239.1;MNI= .013;SCI= .0]
00904 [IAreaCimp= 1.50;IAECPe= 6.00]
00905 [SIMP= 1.39;SMAX= 9.24;SK= .030]
00906 R071C0018-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00907 ADD HYD + 5.0 02:1NF-W2 8.22 .517 1971.0810,15.000 300.01 n/a .000
00908 + 5.0 02:1NF-W3 9.90 .632 1971.0810,15.000 300.01 n/a .000
00909 + 5.0 02:1NF-W4 8.60 .551 1971.0810,15.000 300.01 n/a .000
00910 [Filename SUM= 3.148 1970.0925,21.000 341.01 n/a .000]
00911 *****
00912 # CONTINUOUS STANDYD 5.0 01:1NF-W4 8.60 .551 1971.0810,15.000 300.01 n/a .000
00913 *****
00914 *****
00915 *****
00916 *****
00917 *****
00918 *****
00919 *****
00920 *****
00921 *****
00922 *****
00923 RUN:COMMAND#
00924 R072C0001-----
00925 START
00926 [TZERO= .00 hrs on 19720101]
00927 [MOUT= 2 (1=Imperial, 2=metric output)]
00928 [INSTORM= 0]
00929 [NUN= .0072]
00930 *****
00931 # SMHYND Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
00932 *****
00933 # Project Name: Barhaven Conservancy Development
00934 # Project Number: 1474
00935 # Date : 2/21/02/Oct/18
00936 # Modeler : J.P. Sabourin & P.Eng.
00937 # Company : J.P. Sabourin and Associates
00938 # License # : 2582634
00939 *****
00940 # Ottawa International Airport (1967 - 2003)
00941 R072C0002-----
00942 # READ AED DATA
00943 [Filename = YOM_1967_2007_123 ]
00944 [Start_date= 1972.0101; End_date= 1972.1231]
00945 [ID= 50;min: Length= 8740;hrs: Wetness= 489; Dryhrs= 8271; PTOF= 784.30]
00946 Maximum average rainfall intensities over
00947 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00948 37.30 19.15 12.97 6.15 4.50 2.53 2.00 1.71 1.17 mm/hr
00949 37.30 38.30 38.90 48.90 54.00 60.70 72.10 82.20 84.20
00950 19720123 19720123 19720123 19720123 19720123 19720123 19720123 19720123 19720123 date
00951 Number of rainfall events per following interval time
00952 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00953 170 133 122 86 76 60 45 41 31
00954 Number of events with at least the following durations
00955 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
00956 169 96 58 21 5 0 0 0 0
00957 *****
00958 # COMPUTE API
00959 [API= 50.00; APIKdy= .9000; APIKdt= .9956]
00960 [APIave= 62.22; APIavg= 14.84; APImin= .36]
00961 *****
00962 # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITIONS
00963 *****
00964 R072C0004-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00965 CONTINUOUS STANDYD 5.0 01:1NF 8.22 .682 1972.0712,4.000 345.65 441 .000
00966 [XIMP=54;TIMP=64]
00967 [Horton parameters: Fw= 76.20;Fc= 13.20;DCAV= 4.14; F= .00]
00968 [Impervious area: IArea= 4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
00969 [Impervious area: IArea= 1.57;SIFP= .50;LGI= 244.1;MNI= .013;SCI= .0]
00970 [IAreaCimp= 1.50;IAECPe= 6.00]
00971 # LID for Outlet W4
00972 # Assumed trench 1.25m wide 0.4 deep, 193m long, porosity of 0.4 with 250mm perforated pipe
00973 # Total Volume provided by LID = 344 m³
00974 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00975 R072C0005-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00976 ROUTE RESERVOIR -> 5.0 02:1NF 8.92 .682 1972.0712,4.000 345.65 n/a .000
00977 out <= 5.0 01:1NF-LID 4.03 .002 1972.0411,11.15 345.65 n/a .000
00978 overlow <= 5.0 03:1NF-LID 4.89 .667 1972.0712,4.000 345.65 n/a .000
00979 [MxTotDsed=.3442E-01 m3, TotDVol=.1691E+01 m3, N-Over= .79, TotDOver= .113 hrs]
00980 R072C0006-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00981 CONTINUOUS STANDYD 5.0 01:1NF 8.22 .630 1972.0712,4.000 345.65 441 .000
00982 [XIMP=54;TIMP=64]
00983 [Horton parameters: Fw= 76.20;Fc= 13.20;DCAV= 4.14; F= .00]
00984 [Impervious area: IArea= 4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
00985 [Impervious area: IArea= 1.57;SIFP= .50;LGI= 234.1;MNI= .013;SCI= .0]
00986 [IAreaCimp= 1.50;IAECPe= 6.00]
00987 # LID for Outlet W4
00988 # Assumed trench 1.25m wide 0.4 deep, 186m long, porosity of 0.4 with 250mm perforated pipe
00989 # Total Volume provided by LID = 310 m³
00990 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
00991 R072C0007-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00992 ROUTE RESERVOIR -> 5.0 02:1NF 8.22 .630 1972.0712,4.000 345.65 n/a .000
00993 out <= 5.0 01:1NF-LID 3.81 .002 1972.0411,11.20 345.66 n/a .000
00994 overlow <= 5.0 03:1NF-LID 4.44 .616 1972.0712,4.000 345.65 n/a .000
00995 [MxTotDsed=.3292E-01 m3, TotDVol=.1525E+01 m3, N-Over= .82, TotDOver= .113 hrs]
00996 R072C0008-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
00997 CONTINUOUS STANDYD 5.0 01:1NF 9.90 .756 1972.0712,4.000 345.65 441 .000
00998 [XIMP=54;TIMP=64]
00999 [Horton parameters: Fw= 76.20;Fc= 13.20;DCAV= 4.14; F= .00]
01000 [Impervious area: IArea= 4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
01001 [Impervious area: IArea= 1.57;SIFP= .50;LGI= 257.1;MNI= .013;SCI= .0]
01002 [IAreaCimp= 1.50;IAECPe= 6.00]
01003 # LID for Outlet W4
01004 # Assumed trench 1.25m wide 0.4 deep, 163m long, porosity of 0.4 with 250mm perforated pipe
01005 # Total Volume provided by LID = 303 m³
01006 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01007 R072C0011-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
01008 ROUTE RESERVOIR -> 5.0 02:1NF 8.22 .630 1972.0712,4.000 345.65 n/a .000
01009 out <= 5.0 01:1NF-LID 3.81 .002 1972.0411,11.20 345.75 n/a .000
01010 overlow <= 5.0 03:1NF-LID 4.09 .740 1972.0712,4.000 345.75 n/a .000
01011 [MxTotDsed=.3029E-01 m3, TotDVol=.2106E+01 m3, N-Over= .83, TotDOver= 140.75 hrs]
01012 R072C0012-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
01013 CONTINUOUS STANDYD 5.0 01:1NF 8.60 .658 1972.0712,4.000 345.65 441 .000
01014 [XIMP=54;TIMP=64]
01015 [Horton parameters: Fw= 76.20;Fc= 13.20;DCAV= 4.14; F= .00]
01016 [Impervious area: IArea= 4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
01017 [Impervious area: IArea= 1.57;SIFP= .50;LGI= 239.1;MNI= .013;SCI= .0]
01018 [IAreaCimp= 1.50;IAECPe= 6.00]
01019 # LID for Outlet W4
01020 # Assumed trench 1.25m wide 0.4 deep, 163m long, porosity of 0.4 with 250mm perforated pipe
01021 # Total Volume provided by LID = 303 m³
01022 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
01023 R072C0013-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
01024 ROUTE RESERVOIR -> 5.0 02:1NF 8.60 .658 1972.0712,4.000 345.65 n/a .000
01025 out <= 5.0 01:1NF-LID 3.63 .002 1972.0411,11.20 345.75 n/a .000
01026 overlow <= 5.0 03:1NF-LID 4.97 .644 1972.0712,4.000 345.65 n/a .000
01027 [MxTotDsed=.3029E-01 m3, TotDVol=.1715E+01 m3, N-Over= .78, TotDOver= .113 hrs]
01028 R072C0014-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
01029 ADD HYD + 5.0 02:1NF 8.92 .682 1972.0712,4.000 345.65 n/a .000
01030 + 5.0 02:1NF 8.22 .630 1972.0712,4.000 345.65 n/a .000
01031 + 5.0 02:1NF 9.90 .756 1972.0712,4.000 345.65 n/a .000
01032 + 5.0 02:1NF 8.60 .658 1972.0712,4.000 345.65 n/a .000
01033 [Filename SUM= 3.148 1970.0925,21.000 341.01 n/a .000]
01034 R072C0015-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
01035 CONTINUOUS STANDYD 5.0 01:1NF-W3 35.64 2.272 1972.0712,4.000 345.65 n/a .000
01036 [XIMP=54;TIMP=64]
01037 + 5.0 02:1NF-LID 4.41 .616 1972.0712,4.000 345.65 n/a .000
01038 + 5.0 02:1NF-LID 4.09 .740 1972.0712,4.000 345.65 n/a .000
01039 [Filename SUM= 3.148 1970.0925,21.000 341.01 n/a .000]
01040 # Barhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDITIONS
01041 # Set infiltration to 0 (CN = 99.99) for water balance analysis
01042 *****
01043 # CONTINUOUS STANDYD-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
01044 R072C0016-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
01045 CONTINUOUS STANDYD 5.0 01:1NF-W1 8.92 .895 1972.0712,4.000 527.33 672 .000
01046 [XIMP=54;TIMP=64]
01047 [LQSS=2;CN=100.0]
01048 [Previous area: IArea= 4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
01049 [Impervious area: IArea= 1.57;SIFP= .50;LGI= 244.1;MNI= .013;SCI= .0]
01050 [SIMP= 1.39;SMAX= 9.24;SK= .030]
01051 [IAreaCimp= 1.50;IAECPe= 6.00]
01052 R072C0017-----Dtain-ID:INHYD-----AREAA-QFARCS=TspeakDate_hhm-----RvM-R.C-----DWFCMS
01053 CONTINUOUS STANDYD 5.0 01:1NF-W1 8.92 .895 1972.0712,4.000 527.33 672 .000
01054 [XIMP=54;TIMP=64]
01055 [LQSS=2;CN=100.0]
01056 [Previous area: IArea= 4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
01057 [Impervious area: IArea= 1.57;SIFP= .50;LGI= 2
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01441: [INTORW = 0 ]
01442: [INTORW = 1 ]
01443: \*\*\*\*\*
01444: # SWMRYD Ver:02/Jan 2001 cBETA / INPUT DATA FILE
01445: # \*\*\*\*\*
01446: # Project Name: Barhaven Conservancy Development
01447: # Project Number: 1474
01448: # Date : 2/021/Oct/18
01449: # Modeler : J.Burnett, P.Eng.
01450: # Company : J.P. Sabourin and Associates
01451: # License # : 2582634
01452: \*\*\*\*\*
01453: # Ottawa International Airport (1967 - 2003)
01454: # \*\*\*\*\*
01455: # READ RES DATA
01456: [FileName = YOM\_1967\_2007\_123 ]
01457: [Start\_date = 1975.0101; End\_date = 1975.1231 ]
01458: [DT= 60.min; Length= 876.hrs; Methrs= 344; Dryhrs= 8416; PTOF= 535.50 ]
01459: Maximum average rainfall intensities over
01460: 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01461: 34.80 18.40 12.53 6.32 3.33 1.73 1.15 .87 .62 mm/hr
01462: 34.80 36.80 37.60 37.90 40.00 41.80 41.30 41.80 44.40 mm
01463: 19750708 19750720 19750720 19750721 19750721 19750721 19750721 19750721 19750928 date
01464: Number of rainfall events per following interval time
01465: 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01466: 1.36 1.18 .99 .78 .61 .49 .40 .33 .25
01467: Number of events with at least the following durations
01468: 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
01469: 1.36 1.18 .99 .78 .61 .49 .40 .33 .25
01470: # \*\*\*\*\*
01471: # COMPUTE API
01472: [APIIn= 50.00; APIkdy= 9000; APIkdt= 9956 ]
01473: [APIIn= 73.23; APIkdy= 15.16; APIIn= .00 ]
01474: # \*\*\*\*\*
01475: # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITIONS
01476: # \*\*\*\*\*
01477: # CONTINUOUS STANDBY 5.0 0.1IN1 8.92 .616 1975.0708.1700 224.27 419 .000
01478: [XIMP= 54.7IMP= 64 ]
01479: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01480: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01481: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01482: [IARCLIP= 1.50; IARCEP= 6.00 ]
01483: # \*\*\*\*\*
01484: # LID for Outlet W
01485: # Assumed trench 1.25m wide 0.4 deep, 1939m long, porosity of 0.4 with 250mm perforated pipe
01486: # Total Volume provided by LID = 343 m³
01487: # Soil infiltration rates assumed at 9m/hr with a safety factor of 2.5
01488: # \*\*\*\*\*
01489: # ROUTE RESERVOIR -> 5.0 02M1 8.92 .616 1975.0708.1700 224.27 n/a .000
01490: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01491: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01492: [IARCLIP= 1.50; IARCEP= 6.00 ]
01493: # \*\*\*\*\*
01494: # overflow out <= 5.0 01M1-LID-out 4.85 .002 1975.0708.2115 224.26 n/a .000
01495: [MStoUsed= .3296E-01 m3, TotOVVol= .8142E+00 m3, N-OvF= .50, TotDurOvF= 49.8 hrs]
01496: # \*\*\*\*\*
01497: # CONTINUOUS STANDBY 5.0 0.1IN2 8.22 .569 1975.0708.1700 224.27 419 .000
01498: [XIMP= 54.7IMP= 64 ]
01499: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01500: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01501: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01502: [IARCLIP= 1.50; IARCEP= 6.00 ]
01503: # \*\*\*\*\*
01504: # LID for Outlet W
01505: # Assumed trench 1.25m wide 0.4 deep, 1896m long, porosity of 0.4 with 250mm perforated pipe
01506: # Total Volume provided by LID = 326 m³
01507: # Soil infiltration rates assumed at 9m/hr with a safety factor of 2.5
01508: # \*\*\*\*\*
01509: # ROUTE RESERVOIR -> 5.0 02M1 9.90 .683 1975.0708.1700 224.27 n/a .000
01510: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01511: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01512: [IARCLIP= 1.50; IARCEP= 6.00 ]
01513: # \*\*\*\*\*
01514: # overflow out <= 5.0 01M1-LID-out 4.39 .002 1975.0605.2115 224.27 n/a .000
01515: [MStoUsed= .3296E-01 m3, TotOVVol= .8142E+00 m3, N-OvF= .49, TotDurOvF= 49.8 hrs]
01516: # \*\*\*\*\*
01517: # CONTINUOUS STANDBY 5.0 0.1IN4 8.60 .595 1975.0708.1700 224.27 419 .000
01518: [XIMP= 54.7IMP= 64 ]
01519: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01520: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01521: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01522: [IARCLIP= 1.50; IARCEP= 6.00 ]
01523: # \*\*\*\*\*
01524: # overflow out <= 5.0 01M1-LID-out 5.36 .002 1975.0708.1700 224.27 n/a .000
01525: [MStoUsed= .3027E-01 m3, TotOVVol= .1202E+01 m3, N-OvF= .60, TotDurOvF= 72 hrs]
01526: # \*\*\*\*\*
01527: # CONTINUOUS STANDBY 5.0 0.1IN4 8.60 .595 1975.0708.1700 224.27 419 .000
01528: [XIMP= 54.7IMP= 64 ]
01529: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01530: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01531: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01532: [IARCLIP= 1.50; IARCEP= 6.00 ]
01533: # \*\*\*\*\*
01534: # LID for Outlet W
01535: # Assumed trench 1.25m wide 0.4 deep, 1639m long, porosity of 0.4 with 250mm perforated pipe
01536: # Total Volume provided by LID = 303 m³
01537: # Soil infiltration rates assumed at 9m/hr with a safety factor of 2.5
01538: # \*\*\*\*\*
01539: # ROUTE RESERVOIR -> 5.0 02M1 9.90 .683 1975.0708.1700 224.27 n/a .000
01540: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01541: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01542: [IARCLIP= 1.50; IARCEP= 6.00 ]
01543: # \*\*\*\*\*
01544: # overflow out <= 5.0 01M1-LID-out 4.38 .002 1975.0109.6125 224.27 n/a .000
01545: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
01546: # \*\*\*\*\*
01547: # CONTINUOUS STANDBY 5.0 0.1IN4 8.60 .595 1975.0708.1700 224.27 n/a .000
01548: [XIMP= 54.7IMP= 64 ]
01549: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01550: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01551: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01552: [IARCLIP= 1.50; IARCEP= 6.00 ]
01553: # \*\*\*\*\*
01554: # overflow out <= 5.0 01M1-LID-out 4.22 .002 1975.0708.1700 224.27 n/a .000
01555: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
01556: # \*\*\*\*\*
01557: # CONTINUOUS STANDBY 5.0 0.1IN1F-W2 8.22 .564 1975.0708.1700 336.48 628 .000
01558: [XIMP= 54.7IMP= 64 ]
01559: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01560: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01561: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01562: [IARCLIP= 1.50; IARCEP= 6.00 ]
01563: # \*\*\*\*\*
01564: # overflow out <= 5.0 01M1-LID-out 4.22 .002 1975.0708.1700 336.48 n/a .000
01565: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
01566: # \*\*\*\*\*
01567: # CONTINUOUS STANDBY 5.0 0.1IN1F-W2 8.22 .564 1975.0708.1700 336.48 628 .000
01568: [XIMP= 54.7IMP= 64 ]
01569: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01570: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01571: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01572: [IARCLIP= 1.50; IARCEP= 6.00 ]
01573: # \*\*\*\*\*
01574: # overflow out <= 5.0 01M1-LID-out 4.22 .002 1975.0708.1700 336.48 n/a .000
01575: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
01576: # \*\*\*\*\*
01577: # CONTINUOUS STANDBY 5.0 0.1IN1F-W4 8.60 .599 1975.0708.1700 336.48 628 .000
01578: [XIMP= 54.7IMP= 64 ]
01579: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01580: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01581: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01582: [IARCLIP= 1.50; IARCEP= 6.00 ]
01583: # \*\*\*\*\*
01584: # overflow out <= 5.0 01M1-LID-out 4.22 .002 1975.0708.1700 336.48 n/a .000
01585: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
01586: # \*\*\*\*\*
01587: # CONTINUOUS STANDBY 5.0 0.1IN1F-W4 8.60 .599 1975.0708.1700 336.48 628 .000
01588: [XIMP= 54.7IMP= 64 ]
01589: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01590: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01591: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01592: [IARCLIP= 1.50; IARCEP= 6.00 ]
01593: # \*\*\*\*\*
01594: # overflow out <= 5.0 02IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01595: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
01596: # \*\*\*\*\*
01597: # CONTINUOUS STANDBY 5.0 0.1IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01598: [XIMP= 54.7IMP= 64 ]
01599: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01600: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01601: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01602: [IARCLIP= 1.50; IARCEP= 6.00 ]
01603: # \*\*\*\*\*
01604: # overflow out <= 5.0 02IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01605: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
01606: # \*\*\*\*\*
01607: # CONTINUOUS STANDBY 5.0 0.1IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01608: [XIMP= 54.7IMP= 64 ]
01609: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01610: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01611: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01612: [IARCLIP= 1.50; IARCEP= 6.00 ]
01613: # \*\*\*\*\*
01614: # overflow out <= 5.0 02IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01615: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
01616: # \*\*\*\*\*
01617: # CONTINUOUS STANDBY 5.0 0.1IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01618: [XIMP= 54.7IMP= 64 ]
01619: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01620: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01621: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01622: [IARCLIP= 1.50; IARCEP= 6.00 ]
01623: # \*\*\*\*\*
01624: # overflow out <= 5.0 02IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01625: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
01626: # \*\*\*\*\*
01627: # CONTINUOUS STANDBY 5.0 0.1IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01628: [XIMP= 54.7IMP= 64 ]
01629: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01630: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01631: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01632: [IARCLIP= 1.50; IARCEP= 6.00 ]
01633: # \*\*\*\*\*
01634: # overflow out <= 5.0 02IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01635: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
01636: # \*\*\*\*\*
01637: # CONTINUOUS STANDBY 5.0 0.1IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01638: [XIMP= 54.7IMP= 64 ]
01639: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01640: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01641: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01642: [IARCLIP= 1.50; IARCEP= 6.00 ]
01643: # \*\*\*\*\*
01644: # overflow out <= 5.0 02IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01645: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
01646: # \*\*\*\*\*
01647: # CONTINUOUS STANDBY 5.0 0.1IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01648: [XIMP= 54.7IMP= 64 ]
01649: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01650: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01651: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01652: [IARCLIP= 1.50; IARCEP= 6.00 ]
01653: # \*\*\*\*\*
01654: # overflow out <= 5.0 02IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01655: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
01656: # \*\*\*\*\*
01657: # CONTINUOUS STANDBY 5.0 0.1IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01658: [XIMP= 54.7IMP= 64 ]
01659: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01660: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01661: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01662: [IARCLIP= 1.50; IARCEP= 6.00 ]
01663: # \*\*\*\*\*
01664: # overflow out <= 5.0 02IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01665: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
01666: # \*\*\*\*\*
01667: # CONTINUOUS STANDBY 5.0 0.1IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01668: [XIMP= 54.7IMP= 64 ]
01669: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01670: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01671: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01672: [IARCLIP= 1.50; IARCEP= 6.00 ]
01673: # \*\*\*\*\*
01674: # overflow out <= 5.0 02IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01675: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
01676: # \*\*\*\*\*
01677: # CONTINUOUS STANDBY 5.0 0.1IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01678: [XIMP= 54.7IMP= 64 ]
01679: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01680: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01681: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01682: [IARCLIP= 1.50; IARCEP= 6.00 ]
01683: # \*\*\*\*\*
01684: # overflow out <= 5.0 02IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01685: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
01686: # \*\*\*\*\*
01687: # CONTINUOUS STANDBY 5.0 0.1IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01688: [XIMP= 54.7IMP= 64 ]
01689: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01690: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01691: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01692: [IARCLIP= 1.50; IARCEP= 6.00 ]
01693: # \*\*\*\*\*
01694: # overflow out <= 5.0 02IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01695: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
01696: # \*\*\*\*\*
01697: # CONTINUOUS STANDBY 5.0 0.1IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01698: [XIMP= 54.7IMP= 64 ]
01699: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01700: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01701: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01702: [IARCLIP= 1.50; IARCEP= 6.00 ]
01703: # \*\*\*\*\*
01704: # overflow out <= 5.0 02IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01705: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
01706: # \*\*\*\*\*
01707: # CONTINUOUS STANDBY 5.0 0.1IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01708: [XIMP= 54.7IMP= 64 ]
01709: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01710: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01711: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01712: [IARCLIP= 1.50; IARCEP= 6.00 ]
01713: # \*\*\*\*\*
01714: # overflow out <= 5.0 02IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01715: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
01716: # \*\*\*\*\*
01717: # CONTINUOUS STANDBY 5.0 0.1IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01718: [XIMP= 54.7IMP= 64 ]
01719: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01720: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01721: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01722: [IARCLIP= 1.50; IARCEP= 6.00 ]
01723: # \*\*\*\*\*
01724: # overflow out <= 5.0 02IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01725: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
01726: # \*\*\*\*\*
01727: # CONTINUOUS STANDBY 5.0 0.1IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01728: [XIMP= 54.7IMP= 64 ]
01729: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01730: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01731: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01732: [IARCLIP= 1.50; IARCEP= 6.00 ]
01733: # \*\*\*\*\*
01734: # overflow out <= 5.0 02IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01735: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
01736: # \*\*\*\*\*
01737: # CONTINUOUS STANDBY 5.0 0.1IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01738: [XIMP= 54.7IMP= 64 ]
01739: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01740: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01741: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01742: [IARCLIP= 1.50; IARCEP= 6.00 ]
01743: # \*\*\*\*\*
01744: # overflow out <= 5.0 02IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01745: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
01746: # \*\*\*\*\*
01747: # CONTINUOUS STANDBY 5.0 0.1IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01748: [XIMP= 54.7IMP= 64 ]
01749: [Horton parameters: Fw= 76.20;Fp= 13.20;DCAV= 4.14; F= .00 ]
01750: [Previous area: IAPer= 4.67;SIFP= 2.00;LIP= 40.1MNF= 250;SCP= .0 ]
01751: [Impervious area: IAIM= 1.57;SIFP= .50;LIG= 244.1MNF= .013;SIC= .0 ]
01752: [IARCLIP= 1.50; IARCEP= 6.00 ]
01753: # \*\*\*\*\*
01754: # overflow out <= 5.0 02IN1F-W2 8.22 .564 1975.0708.1700 336.48 n/a .000
01755: [MStoUsed= .3027E-01 m3, TotOVVol= .9465E+00 m3, N-OvF= .48, TotDurOvF= 59.8 hrs]
0



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02161 R0079C0004 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02162 CONTINUOUS STANDBY 5.0 0.01NF-W1 8.92 .490 1979.0616.1400 383.97 443 .000
02163 [XIMP=54;TIMP=.64]
02164 (Horton parameters: Fw=76.20;Fp=13.20;DCAV=4.14; F= .00)
02165 [Previous area: IApw=4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
02166 [Impervious area: IAImp=1.57;SIFP=.50;IIM=244.0;MNI=.013;SICI=.0]
02167 [IARECimp= 1.50; IARECp= 6.00]
02168 # LID for Outlet W2
02169 # Assumed trench 1.25m wide 0.4 deep, 199m long, porosity of 0.4 with 250mm perforated pipe
02170 # Total Volume provided by LID = 303 m³
02171 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02172 R0079C0007 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02173 ROUTE RESERVOIR -> 5.0 021NF-W1 8.92 .680 1979.0616.1400 383.97 n/a .000
02174 out <= 5.0 01NF-LID 3.82 .002 1979.0616.1400 383.98 n/a .000
02175 overflow <= 5.0 03NF-LID-Out 5.17 .647 1979.0616.1400 383.97 n/a .000
02176 (MstOsd=3440E-01 m3, TotDvVol=1.957E+01 m3, N-Ofv= 79, TotDvOrv= 134.hrs)
02177 R0079C0008 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02178 CONTINUOUS STANDBY 5.0 01NF-W2 8.22 .627 1979.0616.1400 383.97 443 .000
02179 [XIMP=54;TIMP=.64]
02180 (Horton parameters: Fw=76.20;Fp=13.20;DCAV=4.14; F= .00)
02181 [Previous area: IApw=4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
02182 [Impervious area: IAImp=1.57;SIFP=.50;IIM=244.0;MNI=.013;SICI=.0]
02183 [IARECimp= 1.50; IARECp= 6.00]
02184 # LID for Outlet W2
02185 # Assumed trench 1.25m wide 0.4 deep, 189m long, porosity of 0.4 with 250mm perforated pipe
02186 # Total Volume provided by LID = 330 m³
02187 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02188 R0079C0007 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02189 ROUTE RESERVOIR -> 5.0 021NF-W1 8.92 .680 1979.0616.1400 383.97 n/a .000
02190 out <= 5.0 01NF-LID 3.82 .002 1979.0616.1400 383.98 n/a .000
02191 overflow <= 5.0 03NF-LID-Out 5.17 .647 1979.0616.1400 383.97 n/a .000
02192 (MstOsd=330E-01 m3, TotDvVol=1.165E+01 m3, N-Ofv= 79, TotDvOrv= 131.hrs)
02193 R0079C0008 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02194 CONTINUOUS STANDBY 5.0 01NF-W1 9.90 .754 1979.0616.1400 383.97 443 .000
02195 [XIMP=54;TIMP=.64]
02196 (Horton parameters: Fw=76.20;Fp=13.20;DCAV=4.14; F= .00)
02197 [Previous area: IApw=4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
02198 [Impervious area: IAImp=1.57;SIFP=.50;IIM=251.0;MNI=.013;SICI=.0]
02199 [IARECimp= 1.50; IARECp= 6.00]
02200 # LID for Outlet W2
02201 # Assumed trench 1.25m wide 0.4 deep, 163m long, porosity of 0.4 with 250mm perforated pipe
02202 # Total Volume provided by LID = 303 m³
02203 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02204 R0079C0009 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02205 ROUTE RESERVOIR -> 5.0 021NF-W1 8.60 .656 1979.0616.1400 383.97 n/a .000
02206 out <= 5.0 01NF-LID 3.56 .002 1979.0616.1400 383.97 n/a .000
02207 overflow <= 5.0 03NF-LID-Out 5.17 .647 1979.0616.1400 383.97 n/a .000
02208 (MstOsd=303E-01 m3, TotDvVol=.2435E+01 m3, N-Ofv= 83, TotDvOrv= 152.hrs)
02209 R0079C0010 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02210 CONTINUOUS STANDBY 5.0 01NF-W1 8.60 .656 1979.0616.1400 383.97 443 .000
02211 [XIMP=54;TIMP=.64]
02212 (Horton parameters: Fw=76.20;Fp=13.20;DCAV=4.14; F= .00)
02213 [Previous area: IApw=4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
02214 [Impervious area: IAImp=1.57;SIFP=.50;IIM=239.0;MNI=.013;SICI=.0]
02215 [IARECimp= 1.50; IARECp= 6.00]
02216 # LID for Outlet W2
02217 # Assumed trench 1.25m wide 0.4 deep, 163m long, porosity of 0.4 with 250mm perforated pipe
02218 # Total Volume provided by LID = 303 m³
02219 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02220 R0079C0011 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02221 ROUTE RESERVOIR -> 5.0 021NF-W1 8.60 .656 1979.0616.1400 383.97 n/a .000
02222 out <= 5.0 01NF-LID 3.56 .002 1979.0616.1400 383.97 n/a .000
02223 overflow <= 5.0 03NF-LID-Out 5.17 .647 1979.0616.1400 383.97 n/a .000
02224 (MstOsd=303E-01 m3, TotDvVol=1.985E+01 m3, N-Ofv= 78, TotDvOrv= 142.hrs)
02225 R0079C0012 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02226 ADD HYD + 5.0 021NF-W1 8.92 .680 1979.0616.1400 383.97 n/a .000
02227 + 5.0 021NF-W2 8.92 .680 1979.0616.1400 383.97 n/a .000
02228 + 5.0 021NF-W3 8.92 .680 1979.0616.1400 383.97 n/a .000
02229 + 5.0 021NF-W4 8.92 .680 1979.0616.1400 383.97 n/a .000
02230 SUM= 5.0 01NF-W1 35.64 2.117 1979.0616.1400 383.97 n/a .000
02231 R0079C0013 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02232 ADD HYD + 5.0 021NF-W1 4.60 .618 1979.0616.1400 383.97 n/a .000
02233 + 5.0 021NF-LID-Out 4.60 .618 1979.0616.1400 383.97 n/a .000
02234 + 5.0 021NF-LID 6.34 .743 1979.0616.1400 383.97 n/a .000
02235 + 5.0 021NF-W2 5.17 .647 1979.0616.1400 383.97 n/a .000
02236 SUM= 5.0 01NF-W1 21.21 2.678 1979.0616.1400 383.97 n/a .000
02237 *****
02238 # Barhavan Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITIONS
02239 *****
02240 # Set Infiltration to 0 (CN = 99.99) for water balance analysis
02241 *****
02242 R0079C0014 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02243 CONTINUOUS STANDBY 5.0 01NF-W1 8.92 .856 1979.0616.1400 604.35 497 .000
02244 [XIMP=54;TIMP=.64]
02245 [LOGS= 2;CN=100.0]
02246 [Previous area: IApw=4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
02247 [Impervious area: IAImp=1.57;SIFP=.50;IIM=244.0;MNI=.013;SICI=.0]
02248 [IARECimp= 1.50; IARECp= 6.00]
02249 [SMN= 1.39; SMAX= 9.24; SK= .030]
02250 R0079C0015 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02251 CONTINUOUS STANDBY 5.0 01NF-W2 8.22 .790 1979.0616.1400 604.35 497 .000
02252 [XIMP=54;TIMP=.64]
02253 [LOGS= 2;CN=100.0]
02254 [Previous area: IApw=4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
02255 [Impervious area: IAImp=1.57;SIFP=.50;IIM=234.0;MNI=.013;SICI=.0]
02256 [IARECimp= 1.50; IARECp= 6.00]
02257 [SMN= 1.39; SMAX= 9.24; SK= .030]
02258 R0079C0016 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02259 CONTINUOUS STANDBY 5.0 01NF-W3 9.90 .940 1979.0616.1400 604.35 497 .000
02260 [XIMP=54;TIMP=.64]
02261 [LOGS= 2;CN=100.0]
02262 [Previous area: IApw=4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
02263 [Impervious area: IAImp=1.57;SIFP=.50;IIM=251.0;MNI=.013;SICI=.0]
02264 [IARECimp= 1.50; IARECp= 6.00]
02265 [SMN= 1.39; SMAX= 9.24; SK= .030]
02266 R0079C0017 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02267 CONTINUOUS STANDBY 5.0 01NF-W4 8.60 .826 1979.0616.1400 604.35 497 .000
02268 [XIMP=54;TIMP=.64]
02269 [LOGS= 2;CN=100.0]
02270 [Previous area: IApw=4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
02271 [Impervious area: IAImp=1.57;SIFP=.50;IIM=239.0;MNI=.013;SICI=.0]
02272 [IARECimp= 1.50; IARECp= 6.00]
02273 [SMN= 1.39; SMAX= 9.24; SK= .030]
02274 R0079C0018 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02275 ADD HYD + 5.0 021NF-W1 8.22 .896 1979.0616.1400 604.35 n/a .000
02276 + 5.0 021NF-W2 8.22 .896 1979.0616.1400 604.35 n/a .000
02277 + 5.0 021NF-W3 8.22 .896 1979.0616.1400 604.35 n/a .000
02278 + 5.0 021NF-W4 8.22 .896 1979.0616.1400 604.35 n/a .000
02279 SUM= 5.0 01NF-W1 35.64 3.411 1979.0616.1400 604.35 n/a .000
02280 *****
02281 # CONTINUOUS RAINFALL DATA
02282 *****
02283 ** END OF RUN : 79
02284 *****
02285 # *****
02286 # *****
02287 # *****
02288 # *****
02289 # *****
02290 # *****
02291 RUN/COMMAND *****
02292 R0080C0001 *****
02293 START *****
02294 [ZERO = .00 hrs on 19801011]
02295 [METOUT= 2 (Impervious, 2-metric output)]
02296 [INTERM= 0]
02297 [NRUN = 0081]
02298 *****
02299 # SWHWRD Ver:02/Jan 2001 -BETA / INPUT DATA FILE
02300 *****
02301 # Project Name: Barhavan Conservancy Development
02302 # Project Number: 1474
02303 # Date : 2021/Oct/18
02304 # Modeler : J.F. Sabourin, P.Eng.
02305 # License # : 2582634
02306 *****
02307 # *****
02308 # Ottawa International Airport (1967 - 2003)
02309 R0080C0002 *****
02310 # READ AES DATA
02311 [Filename = YOW_1967_2007_123 ]
02312 [Start_date= 1967.0101; End_date= 1980.1230]
02313 [DT= 60;min;Length= 8760;hrs;WetHrs= 4271;DryHrs= 8333; PTOF= 622.00]
02314 [Maximum average rainfall intensities over
02315 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02316 15.00 9.20 6.50 4.72 3.57 1.97 1.35 1.01 .86 mm/hr
02317 15.00 18.40 42.80 42.80 47.20 48.60 48.60 48.60 48.60]
02318 19800830 19800830 19801025 19801025 19801026 19801026 19801027 19801027 19801028
02319 Number of rainfall events per following interevent time
02320 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02321 151 125 112 93 79 62 49 44 28
02322 Number of events with at least the following durations
02323 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02324 150 85 54 16 4 0 0 0 0
02325 R0080C0003 *****
02326 COMPUTE API *****
02327 [API= 50.00; APIkdy= .9000; APIkdx= .9956]
02328 [AFmax= 68.72; AFpave= 17.50; AFpinm= .06]
02329 *****
02330 # Barhavan Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITIONS
02331 *****
02332 R0080C0004 *****
02333 CONTINUOUS STANDBY 5.0 01NF-W1 8.92 .198 1980.0830.1400 255.07 410 .000
02334 [XIMP=54;TIMP=.64]
02335 (Horton parameters: Fw=76.20;Fp=13.20;DCAV=4.14; F= .00)
02336 [Previous area: IApw=4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
02337 [Impervious area: IAImp=1.57;SIFP=.50;IIM=244.0;MNI=.013;SICI=.0]
02338 [IARECimp= 1.50; IARECp= 6.00]
02339 # LID for Outlet W2
02340 # Assumed trench 1.25m wide 0.4 deep, 199m long, porosity of 0.4 with 250mm perforated pipe

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02341 # Total Volume provided by LID = 344 m³
02342 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02343 R0080C0005 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02344 ROUTE RESERVOIR -> 5.0 021NF-W1 8.92 .198 1980.0830.1400 255.07 n/a .000
02345 out <= 5.0 01NF-LID 4.05 .002 1980.0830.1400 255.07 n/a .000
02346 overflow <= 5.0 03NF-LID-Out 5.19 .196 1980.0830.1400 255.07 n/a .000
02347 (MstOsd=344E-01 m3, TotDvVol=1.017E+01 m3, N-Ofv= 79, TotDvOrv= 99.hrs)
02348 R0080C0006 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02349 CONTINUOUS STANDBY 5.0 01NF-W2 8.22 .183 1980.0830.1400 255.07 410 .000
02350 [XIMP=54;TIMP=.64]
02351 (Horton parameters: Fw=76.20;Fp=13.20;DCAV=4.14; F= .00)
02352 [Previous area: IApw=4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
02353 [Impervious area: IAImp=1.57;SIFP=.50;IIM=234.0;MNI=.013;SICI=.0]
02354 [IARECimp= 1.50; IARECp= 6.00]
02355 # LID for Outlet W2
02356 # Assumed trench 1.25m wide 0.4 deep, 189m long, porosity of 0.4 with 250mm perforated pipe
02357 # Total Volume provided by LID = 324 m³
02358 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02359 R0080C0007 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02360 ROUTE RESERVOIR -> 5.0 021NF-W1 8.22 .183 1980.0830.1400 255.07 n/a .000
02361 out <= 5.0 01NF-LID 4.67 .002 1980.0830.1400 255.07 n/a .000
02362 overflow <= 5.0 03NF-LID-Out 5.55 .180 1980.0830.1400 255.07 n/a .000
02363 (MstOsd=330E-01 m3, TotDvVol=.9061E+01 m3, N-Ofv= 71, TotDvOrv= 95.hrs)
02364 R0080C0008 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02365 CONTINUOUS STANDBY 5.0 01NF-W2 8.90 .220 1980.0830.1400 255.07 410 .000
02366 [XIMP=54;TIMP=.64]
02367 (Horton parameters: Fw=76.20;Fp=13.20;DCAV=4.14; F= .00)
02368 [Previous area: IApw=4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
02369 [Impervious area: IAImp=1.57;SIFP=.50;IIM=257.0;MNI=.013;SICI=.0]
02370 [IARECimp= 1.50; IARECp= 6.00]
02371 # LID for Outlet W2
02372 # Assumed trench 1.25m wide 0.4 deep, 163m long, porosity of 0.4 with 250mm perforated pipe
02373 # Total Volume provided by LID = 303 m³
02374 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02375 R0080C0009 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02376 ROUTE RESERVOIR -> 5.0 021NF-W1 9.90 .220 1980.0830.1400 255.07 n/a .000
02377 out <= 5.0 01NF-LID 4.63 .002 1980.0830.1400 255.07 n/a .000
02378 overflow <= 5.0 03NF-LID-Out 5.30 .217 1980.0830.1400 255.07 n/a .000
02379 (MstOsd=303E-01 m3, TotDvVol=.1352E+01 m3, N-Ofv= 81, TotDvOrv= 136.hrs)
02380 R0080C0010 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02381 CONTINUOUS STANDBY 5.0 01NF-W1 8.60 .199 1980.0830.1400 255.07 410 .000
02382 [XIMP=54;TIMP=.64]
02383 (Horton parameters: Fw=76.20;Fp=13.20;DCAV=4.14; F= .00)
02384 [Previous area: IApw=4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
02385 [Impervious area: IAImp=1.57;SIFP=.50;IIM=239.0;MNI=.013;SICI=.0]
02386 [IARECimp= 1.50; IARECp= 6.00]
02387 # LID for Outlet W2
02388 # Assumed trench 1.25m wide 0.4 deep, 163m long, porosity of 0.4 with 250mm perforated pipe
02389 # Total Volume provided by LID = 303 m³
02390 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
02391 R0080C0011 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02392 ROUTE RESERVOIR -> 5.0 021NF-W1 8.60 .199 1980.0830.1400 255.07 n/a .000
02393 out <= 5.0 01NF-LID 4.43 .002 1980.0830.1400 255.07 n/a .000
02394 overflow <= 5.0 03NF-LID-Out 5.17 .189 1980.0830.1400 255.07 n/a .000
02395 (MstOsd=303E-01 m3, TotDvVol=.1064E+01 m3, N-Ofv= 79, TotDvOrv= 106.hrs)
02396 R0080C0012 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02397 ADD HYD + 5.0 021NF-W1 8.92 .198 1980.0830.1400 255.07 n/a .000
02398 + 5.0 021NF-W2 8.22 .183 1980.0830.1400 255.07 n/a .000
02399 + 5.0 021NF-W3 9.90 .220 1980.0830.1400 255.07 n/a .000
02400 + 5.0 021NF-W4 8.60 .199 1980.0830.1400 255.07 n/a .000
02401 SUM= 5.0 01NF-W1 35.64 3.564 1980.0830.1400 255.07 n/a .000
02402 R0080C0013 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02403 ADD HYD + 5.0 021NF-LID-Out 4.17 .189 1980.0830.1400 255.07 n/a .000
02404 + 5.0 021NF-LID-Out 3.55 .186 1980.0830.1400 255.07 n/a .000
02405 + 5.0 021NF-LID 4.17 .189 1980.0830.1400 255.07 n/a .000
02406 + 5.0 021NF-W2 5.19 .217 1980.0830.1400 255.07 n/a .000
02407 SUM= 5.0 01NF-W1 21.21 2.678 1979.0616.1400 383.97 n/a .000
02408 *****
02409 # Barhavan Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITIONS
02410 *****
02411 # Set Infiltration to 0 (CN = 99.99) for water balance analysis
02412 *****
02413 R0080C0014 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02414 CONTINUOUS STANDBY 5.0 01NF-W1 8.92 .288 1980.0830.1400 393.13 632 .000
02415 [XIMP=54;TIMP=.64]
02416 [LOGS= 2;CN=100.0]
02417 [Previous area: IApw=4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
02418 [Impervious area: IAImp=1.57;SIFP=.50;IIM=244.0;MNI=.013;SICI=.0]
02419 [IARECimp= 1.50; IARECp= 6.00]
02420 [SMN= 1.39; SMAX= 9.24; SK= .030]
02421 R0080C0015 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02422 CONTINUOUS STANDBY 5.0 01NF-W2 8.22 .266 1980.0830.1400 393.13 632 .000
02423 [XIMP=54;TIMP=.64]
02424 [LOGS= 2;CN=100.0]
02425 [Previous area: IApw=4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
02426 [Impervious area: IAImp=1.57;SIFP=.50;IIM=234.0;MNI=.013;SICI=.0]
02427 [IARECimp= 1.50; IARECp= 6.00]
02428 [SMN= 1.39; SMAX= 9.24; SK= .030]
02429 R0080C0016 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02430 CONTINUOUS STANDBY 5.0 01NF-W3 8.90 .298 1980.0830.1400 393.13 632 .000
02431 [XIMP=54;TIMP=.64]
02432 [LOGS= 2;CN=100.0]
02433 [Previous area: IApw=4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
02434 [Impervious area: IAImp=1.57;SIFP=.50;IIM=257.0;MNI=.013;SICI=.0]
02435 [IARECimp= 1.50; IARECp= 6.00]
02436 [SMN= 1.39; SMAX= 9.24; SK= .030]
02437 R0080C0017 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02438 CONTINUOUS STANDBY 5.0 01NF-W4 8.60 .278 1980.0830.1400 393.13 632 .000
02439 [XIMP=54;TIMP=.64]
02440 [LOGS= 2;CN=100.0]
02441 [Previous area: IApw=4.67;SIFP=2.00;LGP= 40.0;MNP=250;SCP= .0]
02442 [Impervious area: IAImp=1.57;SIFP=.50;IIM=239.0;MNI=.013;SICI=.0]
02443 [IARECimp= 1.50; IARECp= 6.00]
02444 [SMN= 1.39; SMAX= 9.24; SK= .030]
02445 R0080C0018 -----Dtain-IDNHYD-----AREAA-OPeARs-TpaeDate_hh:mm-----RvM-R.C-----DWfms
02446 ADD HYD + 5.0 021NF-W1 8.92 .288 1980.0830.1400 393.13 n/a .000
02447 + 5.0 021NF-W2 8.22 .266 1980.0830.1400 393.13 n/a .000
02448 + 5.0 021NF-W3 8.90 .298 1980.0830.1400 393.13 n/a .000
02449 + 5.0 021NF-W4 8.60 .278 1980.0830.1400 393.13 n/a .000
02450 SUM= 5.0 01NF-W1 35.64 3.564 1980.0830.1400 393.13 n/a .000
02451 *****
02452 # *****
02453 *****
02454 *****
02455 *****
02456 *****
02457 *****
02458 *****
02459 *****
02460 *****
02461 *****
02462 *****
02463 R0081C0001 *****
02464 START *****
02465 [ZERO = .00 hrs on 19810101]
02466 [METOUT= 2 (Impervious, 2-metric output)]
02467 [INTERM= 0]
02468 [NRUN = 0081]
02469 *****
02470 # SWHWRD Ver:02/Jan 2001 -BETA / INPUT DATA FILE
02471 *****
02472 # Project Name: Barhavan Conservancy Development
02473 # Project Number: 1474
02474 # Date : 2021/Oct/18
02475 # Modeler : J.F. Sabourin, P.Eng.
02476 # License # : 2582634
02477 *****
02478 # *****
02479 # Ottawa International Airport (1967 - 2003)
02480 R0081C0002 *****
02481 # READ AES DATA
02482 [Filename = YOW_1967_2007_123 ]
02483 [Start_date= 1967.0101; End_date= 1981.1231]
02484 [DT= 60;min;Length= 8760;hrs;WetHrs= 641;DryHrs= 8119; PTOF= 936.40]
02485 [Maximum average rainfall intensities over
02486 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02487 15.00 9.20 6.50 4.72 3.57 1.97 1.35 1.01 .86 mm/hr
02488 35.30 63.70 78.60 108.90 111.30 115.90 115.90 116.70 mm
02489 19810805 19810805 19810805 19810805 19810805 19810805 19810805 19810805 19810805
02490 Number of rainfall events per following interevent time
02491 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02492 225 171 136 129 78 24 24 24 24]
02493 Number of events with at least the following durations
02494 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
02495 225 171 136 129 78 24 24 24 24]
02496 R0081C0003 *****
02497 COMPUTE API *****
02498 [API= 50.00; APIkdy= .9000; APIkdx= .9956]
02499 [AFmax= 123.49; AFpave= 25.
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03601 + 5.0 021NF-LID-out 3.43 .243 1987.0724.13100 254.01 n/a .000
03602 + 5.0 021NF-LID-out 3.43 .243 1987.0724.13100 254.01 n/a .000
03603 + 5.0 021NF-LID-out 3.98 .255 1987.0724.13100 254.01 n/a .000
03604 SUM 5.0 018CD-PH3-LI 16.32 1.055 1987.0724.13100 254.01 n/a .000
03605 # Barhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDITIONS
03606 # [TERR= 0.00 hrs on 19880101]
03607 # [METOUT= 2 (1=imperial, 2=metric output)]
03608 # [INFORM= 0]
03609 # Set infiltration to 0 (CN = 99.99) for water balance analysis
03610 R0881C00014 -----Dtain-ID-INVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----Rvm-R.C-----DMFcms
03611 CONTINUOUS STANDRD 5.0 011NF-W1 8.92 .430 1987.0724.13100 383.53 1599 .000
03612 [XIMP= 54:TIMP= 64]
03613 [LOSS= 2 :CN=100.0]
03614 [Previous area: IApex= 4.67:SLFP= 2.00:LGP= 40.1MNF= 250:SCP= .0]
03615 [Impervious area: IAlmp= 1.57:SLFP= .50:LIGL= 234.1MNI=.013:SCI= .0]
03616 [IARECLMP= 1.50: IARECPE= 6.00]
03617 [SMN= 1.39: SMAX= 9.24: SK= .030]
03618 R0881C00015 -----Dtain-ID-INVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----Rvm-R.C-----DMFcms
03619 CONTINUOUS STANDRD 5.0 011NF-W2 8.22 .397 1987.0724.13100 383.53 1599 .000
03620 [XIMP= 54:TIMP= 64]
03621 [LOSS= 2 :CN=100.0]
03622 [Previous area: IApex= 4.67:SLFP= 2.00:LGP= 40.1MNF= 250:SCP= .0]
03623 [Impervious area: IAlmp= 1.57:SLFP= .50:LIGL= 234.1MNI=.013:SCI= .0]
03624 [IARECLMP= 1.50: IARECPE= 6.00]
03625 [SMN= 1.39: SMAX= 9.24: SK= .030]
03626 R0881C00016 -----Dtain-ID-INVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----Rvm-R.C-----DMFcms
03627 CONTINUOUS STANDRD 5.0 011NF-W3 9.90 .476 1987.0724.13100 383.53 1599 .000
03628 [XIMP= 54:TIMP= 64]
03629 [LOSS= 2 :CN=100.0]
03630 [Previous area: IApex= 4.67:SLFP= 2.00:LGP= 40.1MNF= 250:SCP= .0]
03631 [Impervious area: IAlmp= 1.57:SLFP= .50:LIGL= 251.1MNI=.013:SCI= .0]
03632 [IARECLMP= 1.50: IARECPE= 6.00]
03633 [SMN= 1.39: SMAX= 9.24: SK= .030]
03634 R0881C00017 -----Dtain-ID-INVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----Rvm-R.C-----DMFcms
03635 CONTINUOUS STANDRD 5.0 011NF-W4 8.60 .415 1987.0724.13100 383.53 1599 .000
03636 [XIMP= 54:TIMP= 64]
03637 [LOSS= 2 :CN=100.0]
03638 [Previous area: IApex= 4.67:SLFP= 2.00:LGP= 40.1MNF= 250:SCP= .0]
03639 [Impervious area: IAlmp= 1.57:SLFP= .50:LIGL= 239.1MNI=.013:SCI= .0]
03640 [IARECLMP= 1.50: IARECPE= 6.00]
03641 [SMN= 1.39: SMAX= 9.24: SK= .030]
03642 R0881C00018 -----Dtain-ID-INVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----Rvm-R.C-----DMFcms
03643 ADD HYD 5.0 021NF-W1 8.92 .430 1987.0724.13100 383.53 n/a .000
03644 + 5.0 021NF-W2 8.22 .397 1987.0724.13100 383.53 n/a .000
03645 + 5.0 021NF-W3 8.60 .415 1987.0724.13100 383.53 n/a .000
03646 + 5.0 021NF-W4 8.60 .415 1987.0724.13100 383.53 n/a .000
03647 SUM 5.0 018CD-PH3-LI 16.32 1.055 1987.0724.13100 383.53 n/a .000
03648 #####
03649 # CONTINUOUS RAINFALL DATA
03650 #####
03651 \*\* END OF RUN : 87
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03659 RUN#COMMAND#
03660 R0881C00019 -----Dtain-ID-INVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----Rvm-R.C-----DMFcms
03661 START
03662 [TERR= 0.00 hrs on 19880101]
03663 [METOUT= 2 (1=imperial, 2=metric output)]
03664 [INFORM= 0]
03665 [MNI= 008]
03666 # Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - INPUT DATA FILE
03667 # SWMNO Ver:5.02/Jan 2001 «BETA» / INPUT DATA FILE
03668 # Project Name: Barhaven Conservancy Development
03669 # Project Number: 1474
03670 # Date: 1/20/02/18
03671 # Modeler: J.F. Sabourin, P.Eng.
03672 # Company: J.F. Sabourin and Associates
03673 # License #: 2582634
03674 # Ontas International Airport (1967 - 2003)
03675 # READ RES DATA
03676 # FILENAME = YOM\_1967\_2003\_123
03677 [Start\_date: 1989.0101: EndDate: 1989.1231]
03678 [Start\_date: 1989.0101: EndDate: 1989.1231]
03679 [Start\_date: 1989.0101: EndDate: 1989.1231]
03680 [Start\_date: 1989.0101: EndDate: 1989.1231]
03681 [Start\_date: 1989.0101: EndDate: 1989.1231]
03682 [Start\_date: 1989.0101: EndDate: 1989.1231]
03683 [Start\_date: 1989.0101: EndDate: 1989.1231]
03684 [Start\_date: 1989.0101: EndDate: 1989.1231]
03685 [Start\_date: 1989.0101: EndDate: 1989.1231]
03686 [Start\_date: 1989.0101: EndDate: 1989.1231]
03687 [Start\_date: 1989.0101: EndDate: 1989.1231]
03688 [Start\_date: 1989.0101: EndDate: 1989.1231]
03689 [Start\_date: 1989.0101: EndDate: 1989.1231]
03690 [Start\_date: 1989.0101: EndDate: 1989.1231]
03691 [Start\_date: 1989.0101: EndDate: 1989.1231]
03692 [Start\_date: 1989.0101: EndDate: 1989.1231]
03693 [Start\_date: 1989.0101: EndDate: 1989.1231]
03694 [Start\_date: 1989.0101: EndDate: 1989.1231]
03695 [Start\_date: 1989.0101: EndDate: 1989.1231]
03696 [Start\_date: 1989.0101: EndDate: 1989.1231]
03697 [Start\_date: 1989.0101: EndDate: 1989.1231]
03698 [Start\_date: 1989.0101: EndDate: 1989.1231]
03699 [Start\_date: 1989.0101: EndDate: 1989.1231]
03700 [Start\_date: 1989.0101: EndDate: 1989.1231]
03701 [Start\_date: 1989.0101: EndDate: 1989.1231]
03702 [Start\_date: 1989.0101: EndDate: 1989.1231]
03703 [Start\_date: 1989.0101: EndDate: 1989.1231]
03704 [Start\_date: 1989.0101: EndDate: 1989.1231]
03705 [Start\_date: 1989.0101: EndDate: 1989.1231]
03706 [Start\_date: 1989.0101: EndDate: 1989.1231]
03707 # LID for Outlet W1
03708 # Assumed trench 1.25m wide 0.4 deep, 1639m long, porosity of 0.4 with 250mm perforated pipe
03709 # Total Volume provided by LID = 344 m³
03710 # Soil infiltration rates assumed at 9m/hr with a safety factor of 2.5
03711 R0881C00020 -----Dtain-ID-INVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----Rvm-R.C-----DMFcms
03712 ROUTE RESERVOIR --> 5.0 021NF 8.22 .340 1988.0917.19100 261.22 n/a .000
03713 out <= 5.0 018M-LID 4.80 .002 1988.0325.21350 261.22 n/a .000
03714 overflow <= 5.0 031NF-LID-out 4.12 .002 1988.0917.19100 261.22 n/a .000
03715 [MxStoUsed=.2028E+01 m3, TotVol=1076E+01 m3, N-Ovr= 54, TotDur=75 hrs]
03716 R0881C00021 -----Dtain-ID-INVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----Rvm-R.C-----DMFcms
03717 CONTINUOUS STANDRD 5.0 011NF 8.22 .340 1988.0917.19100 261.22 406 .000
03718 [XIMP= 54:TIMP= 64]
03719 [Horton parameters: Pw= 76.20:F= 13.20:DCAY=4.14: F= .00]
03720 [Previous area: IApex= 4.67:SLFP= 2.00:LGP= 40.1MNF= 250:SCP= .0]
03721 [Impervious area: IAlmp= 1.57:SLFP= .50:LIGL= 234.1MNI=.013:SCI= .0]
03722 [IARECLMP= 1.50: IARECPE= 6.00]
03723 # LID for Outlet W2
03724 # Assumed trench 1.25m wide 0.4 deep, 1639m long, porosity of 0.4 with 250mm perforated pipe
03725 # Total Volume provided by LID = 303 m³
03726 # Soil infiltration rates assumed at 9m/hr with a safety factor of 2.5
03727 R0881C00022 -----Dtain-ID-INVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----Rvm-R.C-----DMFcms
03728 ROUTE RESERVOIR --> 5.0 021NF 8.22 .340 1988.0917.19100 261.22 n/a .000
03729 out <= 5.0 018M-LID 4.51 .002 1988.0326.2100 261.22 n/a .000
03730 overflow <= 5.0 031NF-LID-out 4.71 .002 1988.0917.19100 261.22 n/a .000
03731 [MxStoUsed=.2028E+01 m3, TotVol=9700E+00 m3, N-Ovr= 46, TotDur=73 hrs]
03732 R0881C00023 -----Dtain-ID-INVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----Rvm-R.C-----DMFcms
03733 CONTINUOUS STANDRD 5.0 011NF 8.22 .340 1988.0917.19100 261.22 406 .000
03734 [XIMP= 54:TIMP= 64]
03735 [Horton parameters: Pw= 76.20:F= 13.20:DCAY=4.14: F= .00]
03736 [Previous area: IApex= 4.67:SLFP= 2.00:LGP= 40.1MNF= 250:SCP= .0]
03737 [Impervious area: IAlmp= 1.57:SLFP= .50:LIGL= 234.1MNI=.013:SCI= .0]
03738 [IARECLMP= 1.50: IARECPE= 6.00]
03739 # LID for Outlet W3
03740 # Assumed trench 1.25m wide 0.4 deep, 1639m long, porosity of 0.4 with 250mm perforated pipe
03741 # Total Volume provided by LID = 303 m³
03742 # Soil infiltration rates assumed at 9m/hr with a safety factor of 2.5
03743 R0881C00024 -----Dtain-ID-INVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----Rvm-R.C-----DMFcms
03744 ROUTE RESERVOIR --> 5.0 021NF 8.22 .340 1988.0917.19100 261.22 n/a .000
03745 out <= 5.0 018M-LID 4.66 .002 1988.0317.18100 261.22 n/a .000
03746 overflow <= 5.0 031NF-LID-out 5.24 .002 1988.0317.18100 261.22 n/a .000
03747 [MxStoUsed=.2028E+01 m3, TotVol=11668E+01 m3, N-Ovr= 56, TotDur=75 hrs]
03748 R0881C00025 -----Dtain-ID-INVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----Rvm-R.C-----DMFcms
03749 CONTINUOUS STANDRD 5.0 011NF 8.60 .355 1988.0917.19100 261.22 406 .000
03750 [XIMP= 54:TIMP= 64]
03751 [Horton parameters: Pw= 76.20:F= 13.20:DCAY=4.14: F= .00]
03752 [Previous area: IApex= 4.67:SLFP= 2.00:LGP= 40.1MNF= 250:SCP= .0]
03753 [Impervious area: IAlmp= 1.57:SLFP= .50:LIGL= 239.1MNI=.013:SCI= .0]
03754 [IARECLMP= 1.50: IARECPE= 6.00]
03755 # LID for Outlet W4
03756 # Assumed trench 1.25m wide 0.4 deep, 1639m long, porosity of 0.4 with 250mm perforated pipe
03757 # Total Volume provided by LID = 303 m³
03758 # Soil infiltration rates assumed at 9m/hr with a safety factor of 2.5
03759 R0881C00026 -----Dtain-ID-INVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----Rvm-R.C-----DMFcms
03760 ROUTE RESERVOIR --> 5.0 021NF 8.22 .340 1988.0917.19100 261.22 n/a .000
03761 out <= 5.0 018M-LID 4.39 .002 1988.0317.18100 261.22 n/a .000
03762 overflow <= 5.0 031NF-LID-out 4.71 .002 1988.0917.19100 261.22 n/a .000
03763 [MxStoUsed=.2028E+01 m3, TotVol=1100E+01 m3, N-Ovr= 49, TotDur=75 hrs]
03764 R0881C00027 -----Dtain-ID-INVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----Rvm-R.C-----DMFcms
03765 ADD HYD 5.0 021NF 8.22 .340 1988.0917.19100 261.22 n/a .000
03766 + 5.0 021NF 8.22 .340 1988.0917.19100 261.22 n/a .000
03767 + 5.0 021NF 8.22 .340 1988.0917.19100 261.22 n/a .000
03768 + 5.0 021NF 8.22 .340 1988.0917.19100 261.22 n/a .000
03769 SUM 5.0 018CD-PH3-LI 16.32 1.055 1988.0917.19100 261.22 n/a .000
03770 R0881C00028 -----Dtain-ID-INVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----Rvm-R.C-----DMFcms
03771 CONTINUOUS STANDRD 5.0 011NF 8.22 .340 1988.0917.19100 261.22 406 .000
03772 [XIMP= 54:TIMP= 64]
03773 [LOSS= 2 :CN=100.0]
03774 [Previous area: IApex= 4.67:SLFP= 2.00:LGP= 40.1MNF= 250:SCP= .0]
03775 [Impervious area: IAlmp= 1.57:SLFP= .50:LIGL= 239.1MNI=.013:SCI= .0]
03776 [IARECLMP= 1.50: IARECPE= 6.00]
03777 # Set infiltration to 0 (CN = 99.99) for water balance analysis
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03961 CONTINUOUS STANDBY 5.0 01:1NF-W4 8.22 .489 1989.0727,15:00 314.66 .601 .000
03962 [XIMP=54:TIMP=64]
03963 [LOGS=2 ICM=100.0]
03964 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
03965 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
03966 [IARCL= 1.50: IARCE= 6.00]
03967 [SM= 1.39: SMA= 9.24: SK= .030]
03968 R0899C0016-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
03969 CONTINUOUS STANDBY 5.0 01:1NF-W4 9.90 .587 1989.0727,15:00 314.66 .601 .000
03970 [XIMP=54:TIMP=64]
03971 [LOGS=2 ICM=100.0]
03972 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
03973 [Impervious area: IAlp= 1.57:SLP= .50:IM= 257.0:MI=.013:ICI= .0]
03974 [IARCL= 1.50: IARCE= 6.00]
03975 [SM= 1.39: SMA= 9.24: SK= .030]
03976 R0899C0017-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
03977 CONTINUOUS STANDBY 5.0 01:1NF-W4 8.60 .511 1989.0727,15:00 314.66 .601 .000
03978 [XIMP=54:TIMP=64]
03979 [LOGS=2 ICM=100.0]
03980 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
03981 [Impervious area: IAlp= 1.57:SLP= .50:IM= 239.0:MI=.013:ICI= .0]
03982 [IARCL= 1.50: IARCE= 6.00]
03983 [SM= 1.39: SMA= 9.24: SK= .030]
03984 R0899C0018-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
03985 ADD HYD + 5.0 02:1NF-W2 8.22 .489 1989.0727,15:00 314.66 n/a .000
03986 + 5.0 02:1NF-W2 9.90 .587 1989.0727,15:00 314.66 n/a .000
03987 + 5.0 02:1NF-W4 8.60 .511 1989.0727,15:00 314.66 n/a .000
03988 + 5.0 02:1NF-W4 8.60 .511 1989.0727,15:00 314.66 n/a .000
03989 SUM= 5.0 01:1NF-WCD-PH 35.64 2.118 1989.0727,15:00 314.66 n/a .000
03990 \*\*\*\*\* CONTINUOUS RAINFALL DATA \*\*\*\*\*
03991 \*\*\*\*\* END OF RUN : 89 \*\*\*\*\*
03992 \*\*\*\*\* RAINFALL DATA \*\*\*\*\*
03993 \*\*\*\*\* END OF RUN : 89 \*\*\*\*\*
04000 R0899C0002-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04001 RUN:COMMANDS
04002 [FILENAME= Y06\_1967\_1007\_123 ]
04003 [START DATE= 1990.0101:END DATE= 1990.1231 ]
04004 [DT= 60,min:Length= 7944,hrs:WetHrs= 6181:DryHrs= 6766:PTOT= 727.80]
04005 Maximum average rainfall intensities over:
04006 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
04007 20.60 12.25 9.60 5.58 4.43 2.25 1.50 1.06 mm/hr
04008 20.60 24.50 24.50 54.00 54.00 59.00 74.00 74.00
04009 1990720 1990720 1990828 1990828 1990720 1990720 1990722 1990723 date
04010 Number of rainfall events per following interval time:
04011 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
04012 204 156 141 107 84 66 56 47 33
04013 Number of events with at least the following durations:
04014 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
04015 203 116 75 31 16 1 0 0 0
04016 R0899C0003-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04017 COMPUTE API
04018 [API= 50.00: APIkdy= 9000: APIkdx= 9956]
04019 [APImax= 75.10: APIave= 23.47: APImin= 3.10]
04020 \*\*\*\*\* Barhaven Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITIONS \*\*\*\*\*
04021 \*\*\*\*\* END OF RUN : 89 \*\*\*\*\*
04022 CONTINUOUS STANDBY 5.0 01:1NF-W4 8.92 .291 1990.0720, 5:00 293.09 403 .000
04023 [XIMP=54:TIMP=64]
04024 [Horton parameters: Fw= 76.20:Fc= 13.20:DCAV=4.14: F= .00]
04025 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04026 [Impervious area: IAlp= 1.57:SLP= .50:IM= 244.0:MI=.013:ICI= .0]
04027 [IARCL= 1.50: IARCE= 6.00]
04028 # Lid for Outlet W4
04029 # Assumed trench 1.25m wide 0.4 deep, 199m long, porosity of 0.4 with 250mm perforated pipe
04030 # Total Volume provided by Lid = 348 m3
04031 # Soil infiltration rates assumed at 9m/hr with a safety factor of 2.5
04032 R0899C0005-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04033 ROUTE RESERVOIR -> 5.0 02:1NF 8.92 .291 1990.0720, 5:00 293.09 n/a .000
04034 out <= 5.0 01:1NF-LID 4.88 .002 1990.0302,11:00 293.09 n/a .000
04035 overflow <= 5.0 03:1NF-LID-out 4.04 .285 1990.0720, 5:00 293.09 n/a .000
04036 [MxSto= 3300E-01 m3, TotDvVol= 1183E+01 m3, N-Ov= 74, TotDvOv= 122,hrs]
04037 R0899C0006-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04038 CONTINUOUS STANDBY 5.0 01:1NF-W4 8.22 .268 1990.0720, 5:00 293.09 403 .000
04039 [XIMP=54:TIMP=64]
04040 [Horton parameters: Fw= 76.20:Fc= 13.20:DCAV=4.14: F= .00]
04041 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04042 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04043 [IARCL= 1.50: IARCE= 6.00]
04044 # Lid for Outlet W2
04045 # Assumed trench 1.25m wide 0.4 deep, 199m long, porosity of 0.4 with 250mm perforated pipe
04046 # Total Volume provided by Lid = 326 m3
04047 # Soil infiltration rates assumed at 9m/hr with a safety factor of 2.5
04048 R0899C0007-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04049 ROUTE RESERVOIR -> 5.0 02:1NF 8.92 .291 1990.0720, 5:00 293.09 n/a .000
04050 out <= 5.0 01:1NF-LID 4.60 .002 1990.0302,11:00 293.09 n/a .000
04051 overflow <= 5.0 03:1NF-LID-out 4.64 .285 1990.0720, 5:00 293.09 n/a .000
04052 [MxSto= 3300E-01 m3, TotDvVol= 1183E+01 m3, N-Ov= 80, TotDvOv= 122,hrs]
04053 R0899C0008-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04054 CONTINUOUS STANDBY 5.0 01:1NF-W4 8.60 .280 1990.0720, 5:00 293.09 403 .000
04055 [XIMP=54:TIMP=64]
04056 [Horton parameters: Fw= 76.20:Fc= 13.20:DCAV=4.14: F= .00]
04057 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04058 [Impervious area: IAlp= 1.57:SLP= .50:IM= 257.0:MI=.013:ICI= .0]
04059 [IARCL= 1.50: IARCE= 6.00]
04060 # Lid for Outlet W2
04061 # Assumed trench 1.25m wide 0.4 deep, 169m long, porosity of 0.4 with 250mm perforated pipe
04062 # Total Volume provided by Lid = 303 m3
04063 # Soil infiltration rates assumed at 9m/hr with a safety factor of 2.5
04064 R0899C0009-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04065 ROUTE RESERVOIR -> 5.0 02:1NF 8.60 .280 1990.0720, 5:00 293.09 n/a .000
04066 out <= 5.0 01:1NF-LID 4.64 .002 1990.0302,11:00 293.09 n/a .000
04067 overflow <= 5.0 03:1NF-LID-out 5.26 .317 1990.0720, 5:00 293.09 n/a .000
04068 [MxSto= 3300E-01 m3, TotDvVol= 1183E+01 m3, N-Ov= 83, TotDvOv= 153,hrs]
04069 R0899C0010-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04070 CONTINUOUS STANDBY 5.0 01:1NF-W4 8.60 .280 1990.0720, 5:00 293.09 403 .000
04071 [XIMP=54:TIMP=64]
04072 [Horton parameters: Fw= 76.20:Fc= 13.20:DCAV=4.14: F= .00]
04073 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04074 [Impervious area: IAlp= 1.57:SLP= .50:IM= 257.0:MI=.013:ICI= .0]
04075 [IARCL= 1.50: IARCE= 6.00]
04076 # Lid for Outlet W2
04077 # Assumed trench 1.25m wide 0.4 deep, 169m long, porosity of 0.4 with 250mm perforated pipe
04078 # Total Volume provided by Lid = 303 m3
04079 # Soil infiltration rates assumed at 9m/hr with a safety factor of 2.5
04080 R0899C0011-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04081 ROUTE RESERVOIR -> 5.0 02:1NF 8.60 .280 1990.0720, 5:00 293.09 n/a .000
04082 out <= 5.0 01:1NF-LID 4.39 .002 1990.0302,11:00 293.09 n/a .000
04083 overflow <= 5.0 03:1NF-LID-out 4.19 .275 1990.0720, 5:00 293.09 n/a .000
04084 [MxSto= 3300E-01 m3, TotDvVol= 1227E+01 m3, N-Ov= 80, TotDvOv= 140,hrs]
04085 R0899C0012-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04086 ADD HYD + 5.0 02:1NF 8.22 .268 1990.0720, 5:00 293.09 n/a .000
04087 + 5.0 02:1NF 9.90 .322 1990.0720, 5:00 293.09 n/a .000
04088 + 5.0 02:1NF 8.60 .280 1990.0720, 5:00 293.09 n/a .000
04089 SUM= 5.0 01:1NF-WCD-PH 35.64 2.118 1990.0720, 5:00 293.09 n/a .000
04090 \*\*\*\*\* Barhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDITIONS \*\*\*\*\*
04091 \*\*\*\*\* END OF RUN : 89 \*\*\*\*\*
04092 \*\*\*\*\* RAINFALL DATA \*\*\*\*\*
04093 \*\*\*\*\* END OF RUN : 89 \*\*\*\*\*
04094 CONTINUOUS STANDBY 5.0 01:1NF-W4 8.22 .477 1990.0720, 5:00 456.65 627 .000
04095 [XIMP=54:TIMP=64]
04096 [LOGS=2 ICM=100.0]
04097 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04098 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04099 [IARCL= 1.50: IARCE= 6.00]
04100 [SM= 1.39: SMA= 9.24: SK= .030]
04101 R0899C00016-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04102 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04103 [XIMP=54:TIMP=64]
04104 [LOGS=2 ICM=100.0]
04105 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04106 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04107 [IARCL= 1.50: IARCE= 6.00]
04108 [SM= 1.39: SMA= 9.24: SK= .030]
04109 R0899C00017-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04110 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04111 [XIMP=54:TIMP=64]
04112 [LOGS=2 ICM=100.0]
04113 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04114 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04115 [IARCL= 1.50: IARCE= 6.00]
04116 [SM= 1.39: SMA= 9.24: SK= .030]
04117 R0899C00018-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04118 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04119 [XIMP=54:TIMP=64]
04120 [LOGS=2 ICM=100.0]
04121 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04122 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04123 [IARCL= 1.50: IARCE= 6.00]
04124 [SM= 1.39: SMA= 9.24: SK= .030]
04125 R0899C00019-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04126 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04127 [XIMP=54:TIMP=64]
04128 [LOGS=2 ICM=100.0]
04129 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04130 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04131 [IARCL= 1.50: IARCE= 6.00]
04132 [SM= 1.39: SMA= 9.24: SK= .030]
04133 R0899C00020-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04134 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04135 [XIMP=54:TIMP=64]
04136 [LOGS=2 ICM=100.0]
04137 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04138 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04139 [IARCL= 1.50: IARCE= 6.00]
04140 [SM= 1.39: SMA= 9.24: SK= .030]
04141 R0899C00021-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04142 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04143 [XIMP=54:TIMP=64]
04144 [LOGS=2 ICM=100.0]
04145 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04146 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04147 [IARCL= 1.50: IARCE= 6.00]
04148 [SM= 1.39: SMA= 9.24: SK= .030]
04149 R0899C00022-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04150 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04151 [XIMP=54:TIMP=64]
04152 [LOGS=2 ICM=100.0]
04153 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04154 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04155 [IARCL= 1.50: IARCE= 6.00]
04156 [SM= 1.39: SMA= 9.24: SK= .030]
04157 R0899C00023-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04158 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04159 [XIMP=54:TIMP=64]
04160 [LOGS=2 ICM=100.0]
04161 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04162 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04163 [IARCL= 1.50: IARCE= 6.00]
04164 [SM= 1.39: SMA= 9.24: SK= .030]
04165 R0899C00024-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04166 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04167 [XIMP=54:TIMP=64]
04168 [LOGS=2 ICM=100.0]
04169 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04170 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04171 [IARCL= 1.50: IARCE= 6.00]
04172 [SM= 1.39: SMA= 9.24: SK= .030]
04173 R0899C00025-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04174 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04175 [XIMP=54:TIMP=64]
04176 [LOGS=2 ICM=100.0]
04177 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04178 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04179 [IARCL= 1.50: IARCE= 6.00]
04180 [SM= 1.39: SMA= 9.24: SK= .030]
04181 R0899C00026-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04182 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04183 [XIMP=54:TIMP=64]
04184 [LOGS=2 ICM=100.0]
04185 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04186 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04187 [IARCL= 1.50: IARCE= 6.00]
04188 [SM= 1.39: SMA= 9.24: SK= .030]
04189 R0899C00027-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04190 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04191 [XIMP=54:TIMP=64]
04192 [LOGS=2 ICM=100.0]
04193 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04194 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04195 [IARCL= 1.50: IARCE= 6.00]
04196 [SM= 1.39: SMA= 9.24: SK= .030]
04197 R0899C00028-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04198 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04199 [XIMP=54:TIMP=64]
04200 [LOGS=2 ICM=100.0]
04201 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04202 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04203 [IARCL= 1.50: IARCE= 6.00]
04204 [SM= 1.39: SMA= 9.24: SK= .030]
04205 R0899C00029-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04206 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04207 [XIMP=54:TIMP=64]
04208 [LOGS=2 ICM=100.0]
04209 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04210 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04211 [IARCL= 1.50: IARCE= 6.00]
04212 [SM= 1.39: SMA= 9.24: SK= .030]
04213 R0899C00030-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04214 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04215 [XIMP=54:TIMP=64]
04216 [LOGS=2 ICM=100.0]
04217 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04218 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04219 [IARCL= 1.50: IARCE= 6.00]
04220 [SM= 1.39: SMA= 9.24: SK= .030]
04221 R0899C00031-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04222 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04223 [XIMP=54:TIMP=64]
04224 [LOGS=2 ICM=100.0]
04225 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04226 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04227 [IARCL= 1.50: IARCE= 6.00]
04228 [SM= 1.39: SMA= 9.24: SK= .030]
04229 R0899C00032-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04230 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04231 [XIMP=54:TIMP=64]
04232 [LOGS=2 ICM=100.0]
04233 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04234 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04235 [IARCL= 1.50: IARCE= 6.00]
04236 [SM= 1.39: SMA= 9.24: SK= .030]
04237 R0899C00033-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04238 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04239 [XIMP=54:TIMP=64]
04240 [LOGS=2 ICM=100.0]
04241 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04242 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04243 [IARCL= 1.50: IARCE= 6.00]
04244 [SM= 1.39: SMA= 9.24: SK= .030]
04245 R0899C00034-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04246 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04247 [XIMP=54:TIMP=64]
04248 [LOGS=2 ICM=100.0]
04249 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04250 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04251 [IARCL= 1.50: IARCE= 6.00]
04252 [SM= 1.39: SMA= 9.24: SK= .030]
04253 R0899C00035-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04254 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04255 [XIMP=54:TIMP=64]
04256 [LOGS=2 ICM=100.0]
04257 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04258 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04259 [IARCL= 1.50: IARCE= 6.00]
04260 [SM= 1.39: SMA= 9.24: SK= .030]
04261 R0899C00036-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04262 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04263 [XIMP=54:TIMP=64]
04264 [LOGS=2 ICM=100.0]
04265 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04266 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04267 [IARCL= 1.50: IARCE= 6.00]
04268 [SM= 1.39: SMA= 9.24: SK= .030]
04269 R0899C00037-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04270 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04271 [XIMP=54:TIMP=64]
04272 [LOGS=2 ICM=100.0]
04273 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04274 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04275 [IARCL= 1.50: IARCE= 6.00]
04276 [SM= 1.39: SMA= 9.24: SK= .030]
04277 R0899C00038-----Dtain-IDINVD-----AREAh-QFEARs-TpeakDate\_hh:mm-----RvM-R-C-----DWfms
04278 CONTINUOUS STANDBY 5.0 01:1NF-W2 8.22 .440 1990.0720, 5:00 456.65 627 .000
04279 [XIMP=54:TIMP=64]
04280 [LOGS=2 ICM=100.0]
04281 [Previous area: IArea= 4.67:SLFP=2.00:LG= 40.0:IMP=250:SCP= .0]
04282 [Impervious area: IAlp= 1.57:SLP= .50:IM= 234.0:MI=.013:ICI= .0]
04283 [I

042321 [LOGS 2 ICM=100.0]
042322 [Previous area IApex= 4.675LFPF=2.001LGP= 40.0MNF=250.0SFC= .0]
042323 [Impervious area IAlmp=1.571SLP= .501IM= 239.0MM= .013IC=1]
042324 [IARECLIP= 1.50 IARECPE= 6.00]
042325 [SMIN= 1.39 IEMAX= 9.24 SK= .030]
042326 [CONTINUOUS STANDBY]
042327 [ADD HYD]
042328 [SUM= 5.0 02:INF-W2 8.22 .240 1991.0409.1100 331.20 n/a .000]
042329 [SUM= 5.0 02:INF-W3 9.90 .286 1991.0409.1100 331.19 n/a .000]
042330 [SUM= 5.0 02:INF-W4 8.60 .249 1991.0409.1100 331.19 n/a .000]
042331 [SUM= 5.0 01:INF-BCD-PH 35.64 1.034 1991.0409.1100 331.20 n/a .000]
042332 [CONTINUOUS RAINFALL DATA]
042333 [TERR= .00 hrs on 19930101]
042334 [METOUT= 2 (1=Impervious, 2=metric output)]
042335 [NSTRM= 0]
042336 [NUN= .0092]
042337 [SWRNO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE]
042338 [Project Name: Barhaven Conservancy Development]
042339 [Project Number: 1474]
042340 [Date : 2021/Oct/18]
042341 [Modeler : J.Burnett, P.Eng.]
042342 [Company : J.F. Sabourin and Associates]
042343 [License : 2382634]
042344 [Ottawa International Airport (1967 - 2003)]
042345 [READ AES DATA]
042346 [FILENAME = YOM\_1967\_2003\_12 ]
042347 [Start\_date= 1992.0101; End\_date= 1992.1230 ]
042348 [DT= 60 min; Length= 8760 hrs; WetHrs= 585; DryHrs= 8175; PTO= 721.30 ]
042349 [Maximum average rainfall intensities over]
042350 [1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs]
042351 [31.50 18.00 13.00 7.22 4.14 2.26 1.51 1.51 1.02 mm/hr]
042352 [19920804 19920804 19920804 19920718 19920718 19920719 19920720]
042353 [Number of rainfall events per following interevent time]
042354 [1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs]
042355 [190 151 132 100 84 69 55 47 38]
042356 [Number of events with at least the following durations]
042357 [1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs]
042358 [189 109 70 22 5 1 0 0 0]
042359 [R0931C0002]
042360 [COMPUTE API]
042361 [APIIN= 30.00; APIKEY= 9000; APIKDF= .9956]
042362 [Previous area IApex= 4.675LFPF=2.001LGP= 40.0MNF=250.0SFC= .0]
042363 [Impervious area IAlmp=1.571SLP= .501IM= 234.0MM= .013IC=1]
042364 [IARECLIP= 1.50 IARECPE= 6.00]
042365 [LID for Outlet W2]
042366 [Assumed trench 1.25m wide 0.4 deep, 199m long, porosity of 0.4 with 250mm perforated pipe]
042367 [Total Volume provided by LID = 34 m³]
042368 [Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5]
042369 [ROUTE RESERVOIR -> 5.0 02:INF 8.92 .574 1992.0804.1400 308.60 n/a .000]
042370 [overflow <- 5.0 03:INF-LID 4.39 .563 1992.0804.1400 308.60 n/a .000]
042371 [MStoUsed= .3439E+01 m³, TotDrVVol= .1355E+01 m³, N-Over= 83, TotDrVVol= 100 hrs]
042372 [CONTINUOUS STANDBY 5.0 01:INF 8.22 .574 1992.0804.1400 308.60 421 .000]
042373 [XIMP= 54:TIMP= 64]
042374 [Horton parameters: Pw= 76.20; Fc= 13.20; DCAV= 4.14; F= .00]
042375 [Previous area IApex= 4.675LFPF=2.001LGP= 40.0MNF=250.0SFC= .0]
042376 [Impervious area IAlmp=1.571SLP= .501IM= 244.0MM= .013IC=1]
042377 [IARECLIP= 1.50 IARECPE= 6.00]
042378 [LID for Outlet W1]
042379 [Assumed trench 1.25m wide 0.4 deep, 199m long, porosity of 0.4 with 250mm perforated pipe]
042380 [Total Volume provided by LID = 34 m³]
042381 [Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5]
042382 [ROUTE RESERVOIR -> 5.0 02:INF 8.92 .574 1992.0804.1400 308.60 n/a .000]
042383 [overflow <- 5.0 03:INF-LID 4.39 .563 1992.0804.1400 308.60 n/a .000]
042384 [MStoUsed= .3297E+01 m³, TotDrVVol= .901E+01 m³, N-Over= 61, TotDrVVol= 122 hrs]
042385 [CONTINUOUS STANDBY 5.0 01:INF 8.22 .552 1992.0703.900 288.39 400 .000]
042386 [XIMP= 54:TIMP= 64]
042387 [Horton parameters: Pw= 76.20; Fc= 13.20; DCAV= 4.14; F= .00]
042388 [Previous area IApex= 4.675LFPF=2.001LGP= 40.0MNF=250.0SFC= .0]
042389 [Impervious area IAlmp=1.571SLP= .501IM= 234.0MM= .013IC=1]
042390 [IARECLIP= 1.50 IARECPE= 6.00]
042391 [LID for Outlet W2]
042392 [Assumed trench 1.25m wide 0.4 deep, 169m long, porosity of 0.4 with 250mm perforated pipe]
042393 [Total Volume provided by LID = 30 m³]
042394 [Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5]
042395 [ROUTE RESERVOIR -> 5.0 02:INF 8.92 .574 1992.0804.1400 308.60 n/a .000]
042396 [overflow <- 5.0 03:INF-LID 4.39 .563 1992.0804.1400 308.60 n/a .000]
042397 [MStoUsed= .3029E+01 m³, TotDrVVol= .1218E+01 m³, N-Over= 60, TotDrVVol= 85 hrs]
042398 [CONTINUOUS STANDBY 5.0 01:INF 8.60 .554 1992.0804.1400 308.60 421 .000]
042399 [XIMP= 54:TIMP= 64]
042400 [Horton parameters: Pw= 76.20; Fc= 13.20; DCAV= 4.14; F= .00]
042401 [Previous area IApex= 4.675LFPF=2.001LGP= 40.0MNF=250.0SFC= .0]
042402 [Impervious area IAlmp=1.571SLP= .501IM= 251.0MM= .013IC=1]
042403 [IARECLIP= 1.50 IARECPE= 6.00]
042404 [LID for Outlet W3]
042405 [Assumed trench 1.25m wide 0.4 deep, 169m long, porosity of 0.4 with 250mm perforated pipe]
042406 [Total Volume provided by LID = 30 m³]
042407 [Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5]
042408 [ROUTE RESERVOIR -> 5.0 02:INF 8.92 .574 1992.0804.1400 308.60 n/a .000]
042409 [overflow <- 5.0 03:INF-LID 4.39 .563 1992.0804.1400 308.60 n/a .000]
042410 [MStoUsed= .3029E+01 m³, TotDrVVol= .1218E+01 m³, N-Over= 60, TotDrVVol= 85 hrs]
042411 [CONTINUOUS STANDBY 5.0 01:INF 8.60 .554 1992.0804.1400 308.60 421 .000]
042412 [XIMP= 54:TIMP= 64]
042413 [Horton parameters: Pw= 76.20; Fc= 13.20; DCAV= 4.14; F= .00]
042414 [Previous area IApex= 4.675LFPF=2.001LGP= 40.0MNF=250.0SFC= .0]
042415 [Impervious area IAlmp=1.571SLP= .501IM= 239.0MM= .013IC=1]
042416 [IARECLIP= 1.50 IARECPE= 6.00]
042417 [LID for Outlet W4]
042418 [Assumed trench 1.25m wide 0.4 deep, 169m long, porosity of 0.4 with 250mm perforated pipe]
042419 [Total Volume provided by LID = 30 m³]
042420 [Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5]
042421 [ROUTE RESERVOIR -> 5.0 02:INF 8.92 .574 1992.0804.1400 308.60 n/a .000]
042422 [overflow <- 5.0 03:INF-LID 4.39 .563 1992.0804.1400 308.60 n/a .000]
042423 [MStoUsed= .3029E+01 m³, TotDrVVol= .1218E+01 m³, N-Over= 60, TotDrVVol= 85 hrs]
042424 [CONTINUOUS STANDBY 5.0 01:INF 8.60 .554 1992.0804.1400 308.60 421 .000]
042425 [XIMP= 54:TIMP= 64]
042426 [Horton parameters: Pw= 76.20; Fc= 13.20; DCAV= 4.14; F= .00]
042427 [Previous area IApex= 4.675LFPF=2.001LGP= 40.0MNF=250.0SFC= .0]
042428 [Impervious area IAlmp=1.571SLP= .501IM= 239.0MM= .013IC=1]
042429 [IARECLIP= 1.50 IARECPE= 6.00]
042430 [LID for Outlet W5]
042431 [Assumed trench 1.25m wide 0.4 deep, 169m long, porosity of 0.4 with 250mm perforated pipe]
042432 [Total Volume provided by LID = 30 m³]
042433 [Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5]
042434 [ROUTE RESERVOIR -> 5.0 02:INF 8.92 .574 1992.0804.1400 308.60 n/a .000]
042435 [overflow <- 5.0 03:INF-LID 4.39 .563 1992.0804.1400 308.60 n/a .000]
042436 [MStoUsed= .3029E+01 m³, TotDrVVol= .1218E+01 m³, N-Over= 60, TotDrVVol= 85 hrs]
042437 [CONTINUOUS STANDBY 5.0 01:INF 8.60 .554 1992.0804.1400 308.60 421 .000]
042438 [XIMP= 54:TIMP= 64]
042439 [Horton parameters: Pw= 76.20; Fc= 13.20; DCAV= 4.14; F= .00]
042440 [Previous area IApex= 4.675LFPF=2.001LGP= 40.0MNF=250.0SFC= .0]
042441 [Impervious area IAlmp=1.571SLP= .501IM= 239.0MM= .013IC=1]
042442 [IARECLIP= 1.50 IARECPE= 6.00]
042443 [LID for Outlet W6]
042444 [Assumed trench 1.25m wide 0.4 deep, 169m long, porosity of 0.4 with 250mm perforated pipe]
042445 [Total Volume provided by LID = 30 m³]
042446 [Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5]
042447 [ROUTE RESERVOIR -> 5.0 02:INF 8.92 .574 1992.0804.1400 308.60 n/a .000]
042448 [overflow <- 5.0 03:INF-LID 4.39 .563 1992.0804.1400 308.60 n/a .000]
042449 [MStoUsed= .3029E+01 m³, TotDrVVol= .1218E+01 m³, N-Over= 60, TotDrVVol= 85 hrs]
042450 [CONTINUOUS STANDBY 5.0 01:INF 8.60 .554 1992.0804.1400 308.60 421 .000]
042451 [XIMP= 54:TIMP= 64]
042452 [Horton parameters: Pw= 76.20; Fc= 13.20; DCAV= 4.14; F= .00]
042453 [Previous area IApex= 4.675LFPF=2.001LGP= 40.0MNF=250.0SFC= .0]
042454 [Impervious area IAlmp=1.571SLP= .501IM= 239.0MM= .013IC=1]
042455 [IARECLIP= 1.50 IARECPE= 6.00]
042456 [LID for Outlet W7]
042457 [Assumed trench 1.25m wide 0.4 deep, 169m long, porosity of 0.4 with 250mm perforated pipe]
042458 [Total Volume provided by LID = 30 m³]
042459 [Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5]
042460 [ROUTE RESERVOIR -> 5.0 02:INF 8.92 .574 1992.0804.1400 308.60 n/a .000]
042461 [overflow <- 5.0 03:INF-LID 4.39 .563 1992.0804.1400 308.60 n/a .000]
042462 [MStoUsed= .3029E+01 m³, TotDrVVol= .1218E+01 m³, N-Over= 60, TotDrVVol= 85 hrs]
042463 [CONTINUOUS STANDBY 5.0 01:INF 8.60 .554 1992.0804.1400 308.60 421 .000]
042464 [XIMP= 54:TIMP= 64]
042465 [Horton parameters: Pw= 76.20; Fc= 13.20; DCAV= 4.14; F= .00]
042466 [Previous area IApex= 4.675LFPF=2.001LGP= 40.0MNF=250.0SFC= .0]
042467 [Impervious area IAlmp=1.571SLP= .501IM= 239.0MM= .013IC=1]
042468 [IARECLIP= 1.50 IARECPE= 6.00]
042469 [LID for Outlet W8]
042470 [Assumed trench 1.25m wide 0.4 deep, 169m long, porosity of 0.4 with 250mm perforated pipe]
042471 [Total Volume provided by LID = 30 m³]
042472 [Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5]
042473 [ROUTE RESERVOIR -> 5.0 02:INF 8.92 .574 1992.0804.1400 308.60 n/a .000]
042474 [overflow <- 5.0 03:INF-LID 4.39 .563 1992.0804.1400 308.60 n/a .000]
042475 [MStoUsed= .3029E+01 m³, TotDrVVol= .1218E+01 m³, N-Over= 60, TotDrVVol= 85 hrs]
042476 [CONTINUOUS STANDBY 5.0 01:INF 8.60 .554 1992.0804.1400 308.60 421 .000]
042477 [XIMP= 54:TIMP= 64]
042478 [Horton parameters: Pw= 76.20; Fc= 13.20; DCAV= 4.14; F= .00]
042479 [Previous area IApex= 4.675LFPF=2.001LGP= 40.0MNF=250.0SFC= .0]
042480 [Impervious area IAlmp=1.571SLP= .501IM= 239.0MM= .013IC=1]
042481 [IARECLIP= 1.50 IARECPE= 6.00]
042482 [LID for Outlet W9]
042483 [Assumed trench 1.25m wide 0.4 deep, 169m long, porosity of 0.4 with 250mm perforated pipe]
042484 [Total Volume provided by LID = 30 m³]
042485 [Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5]
042486 [ROUTE RESERVOIR -> 5.0 02:INF 8.92 .574 1992.0804.1400 308.60 n/a .000]
042487 [overflow <- 5.0 03:INF-LID 4.39 .563 1992.0804.1400 308.60 n/a .000]
042488 [MStoUsed= .3029E+01 m³, TotDrVVol= .1218E+01 m³, N-Over= 60, TotDrVVol= 85 hrs]
042489 [CONTINUOUS STANDBY 5.0 01:INF 8.60 .554 1992.0804.1400 308.60 421 .000]
042490 [XIMP= 54:TIMP= 64]
042491 [Horton parameters: Pw= 76.20; Fc= 13.20; DCAV= 4.14; F= .00]
042492 [Previous area IApex= 4.675LFPF=2.001LGP= 40.0MNF=250.0SFC= .0]
042493 [Impervious area IAlmp=1.571SLP= .501IM= 239.0MM= .013IC=1]
042494 [IARECLIP= 1.50 IARECPE= 6.00]
042495 [LID for Outlet W10]
042496 [Assumed trench 1.25m wide 0.4 deep, 169m long, porosity of 0.4 with 250mm perforated pipe]
042497 [Total Volume provided by LID = 30 m³]
042498 [Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5]
042499 [ROUTE RESERVOIR -> 5.0 02:INF 8.92 .574 1992.0804.1400 308.60 n/a .000]
042500 [overflow <- 5.0 03:INF-LID 4.39 .563 1992.0804.1400 308.60 n/a .000]
042501 [MStoUsed= .3029E+01 m³, TotDrVVol= .1218E+01 m³, N-Over= 60, TotDrVVol= 85 hrs]
042502 [CONTINUOUS STANDBY 5.0 01:INF 8.60 .554 1992.0804.1400 308.60 421 .000]
042503 [XIMP= 54:TIMP= 64]
042504 [Horton parameters: Pw= 76.20; Fc= 13.20; DCAV= 4.14; F= .00]
042505 [Previous area IApex= 4.675LFPF=2.001LGP= 40.0MNF=250.0SFC= .0]
042506 [Impervious area IAlmp=1.571SLP= .501IM= 239.0MM= .013IC=1]
042507 [IARECLIP= 1.50 IARECPE= 6.00]
042508 [LID for Outlet W11]
042509 [Assumed trench 1.25m wide 0.4 deep, 169m long, porosity of 0.4 with 250mm perforated pipe]
042510 [Total Volume provided by LID = 30 m³]
042511 [Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5]
042512 [ROUTE RESERVOIR -> 5.0 02:INF 8.92 .574 1992.0804.1400 308.60 n/a .000]
042513 [overflow <- 5.0 03:INF-LID 4.39 .563 1992.0804.1400 308.60 n/a .000]
042514 [MStoUsed= .3029E+01 m³, TotDrVVol= .1218E+01 m³, N-Over= 60, TotDrVVol= 85 hrs]
042515 [CONTINUOUS STANDBY 5.0 01:INF 8.60 .554 1992.0804.1400 308.60 421 .000]
042516 [XIMP= 54:TIMP= 64]
042517 [Horton parameters: Pw= 76.20; Fc= 13.20; DCAV= 4.14; F= .00]
042518 [Previous area IApex= 4.675LFPF=2.001LGP= 40.0MNF=250.0SFC= .0]
042519 [Impervious area IAlmp=1.571SLP= .501IM= 239.0MM= .013IC=1]
042520 [IARECLIP= 1.50 IARECPE= 6.00]
042521 [LID for Outlet W12]
042522 [Assumed trench 1.25m wide 0.4 deep, 169m long, porosity of 0.4 with 250mm perforated pipe]
042523 [Total Volume provided by LID = 30 m³]
042524 [Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5]
042525 [ROUTE RESERVOIR -> 5.0 02:INF 8.92 .574 1992.0804.1400 308.60 n/a .000]
042526 [overflow <- 5.0 03:INF-LID 4.39 .563 1992.0804.1400 308.60 n/a .000]
042527 [MStoUsed= .3029E+01 m³, TotDrVVol= .1218E+01 m³, N-Over= 60, TotDrVVol= 85 hrs]
042528 [CONTINUOUS STANDBY 5.0 01:INF 8.60 .554 1992.0804.1400 308.60 421 .000]
042529 [XIMP= 54:TIMP= 64]
042530 [Horton parameters: Pw= 76.20; Fc= 13.20; DCAV= 4.14; F= .00]
042531 [Previous area IApex= 4.675LFPF=2.001LGP= 40.0MNF=250.0SFC= .0]
042532 [Impervious area IAlmp=1.571SLP= .501IM= 239.0MM= .013IC=1]
042533 [IARECLIP= 1.50 IARECPE= 6.00]
042534 [LID for Outlet W13]
042535 [Assumed trench 1.25m wide 0.4 deep, 169m long, porosity of 0.4 with 250mm perforated pipe]
042536 [Total Volume provided by LID = 30 m³]
042537 [Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5]
042538 [ROUTE RESERVOIR -> 5.0 02:INF 8.92 .574 1992.0804.1400 308.60 n/a .000]
042539 [overflow <- 5.0 03:INF-LID 4.39 .563 1992.0804.1400 308.60 n/a .000]
042540 [MStoUsed= .3029E+01 m³, TotDrVVol= .1218E+01 m³, N-Over= 60, TotDrVVol= 85 hrs]
042541 [CONTINUOUS STANDBY 5.0 01:INF 8.60 .554 1992.0804.1400 308.60 421 .000]
042542 [XIMP= 54:TIMP= 64]
042543 [Horton parameters: Pw= 76.20; Fc= 13.20; DCAV= 4.14; F= .00]
042544 [Previous area IApex= 4.675LFPF=2.001LGP= 40.0MNF=250.0SFC= .0]
042545 [Impervious area IAlmp=1.571SLP= .501IM= 239.0MM= .013IC=1]
042546 [IARECLIP= 1.50 IARECPE= 6.00]
042547 [LID for Outlet W14]
042548 [Assumed trench 1.25m wide 0.4 deep, 169m long, porosity of 0.4 with 250mm perforated pipe]
042549 [Total Volume provided by LID = 30 m³]
042550 [Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5]
042551 [ROUTE RESERVOIR -> 5.0 02:INF 8.92 .574 1992.0804.1400 308.60 n/a .000]
042552 [overflow <- 5.0 03:INF-LID 4.39 .563 1992.0804.1400 308.60 n/a .000]
042553 [MStoUsed= .3029E+01 m³, TotDrVVol= .1218E+01 m³, N-Over= 60, TotDrVVol= 85 hrs]
042554 [CONTINUOUS STANDBY 5.0 01:INF 8.60 .554 1992.0804.1400 308.60 421 .000]
042555 [XIMP= 54:TIMP= 64]
042556 [Horton parameters: Pw= 76.20; Fc= 13.20; DCAV= 4.14; F= .00]
042557 [Previous area IApex= 4.675LFPF=2.001LGP= 40.0MNF=250.0SFC= .0]
042558 [Impervious area IAlmp=1.571SLP= .501IM= 239.0MM= .013IC=1]
042559 [IARECLIP= 1.50 IARECPE= 6.00]
042560 [LID for Outlet W15]
042561 [Assumed trench 1.25m wide 0.4 deep, 169m long, porosity of 0.4 with 250mm perforated pipe]
042562 [Total Volume provided by LID = 30 m³]
042563 [Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5]
042564 [ROUTE RESERVOIR -> 5.0 02:INF 8.92 .574 1992.0804.1400 308.60 n/a .000]
042565 [overflow <- 5.0 03:INF-LID 4.39 .563 1992.0804.1400 308.60 n/a .000]
042566 [MStoUsed= .3029E+01 m³, TotDrVVol= .1218E+01 m³, N-Over= 60, TotDrVVol= 85 hrs]
042567 [CONTINUOUS STANDBY 5.0 01:INF 8.60 .554 1992.0804.1400 308.60 421 .000]
042568 [XIMP= 54:TIMP= 64]
042569 [Horton parameters: Pw= 76.20; Fc= 13.20; DCAV= 4.14; F= .00]
042570 [Previous area IApex= 4.675LFPF=2.001LGP= 40.0MNF=250.0SFC= .0]
042571 [Impervious area IAlmp=1.571SLP= .501IM= 239.0MM= .013IC=1]
042572 [IARECLIP= 1.50 IARECPE= 6.00]
042573 [LID for Outlet W16]
042574 [Assumed trench 1.25m wide 0.4 deep, 169m long, porosity of 0.4 with 250mm perforated pipe]
042575 [Total Volume provided by LID = 30 m³]
042576 [Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5]
042577 [ROUTE RESERVOIR -> 5.0 02:INF 8.92 .574 1992.0804.1400 308.60 n/a .000]
042578 [overflow <- 5.0 03:INF-LID 4.39 .563 1992.0804.1400 308.60 n/a .000]
042579 [MStoUsed= .3029E+01 m³, TotDrVVol= .1218E+01 m³, N-Over= 60, TotDrVVol= 85 hrs]
042580 [CONTINUOUS STANDBY 5.0 01:INF 8.60 .554 1992.0804.1400 308.60 421 .000]
042581 [XIMP= 54:TIMP= 64]
042582 [Horton parameters: Pw= 76.20; Fc= 13.20; DCAV= 4.14; F= .00]
042583 [Previous area IApex= 4.675LFPF=2.001LGP= 40.0MNF=250.0SFC= .0]
042584 [Impervious area IAlmp=1.571SLP= .501IM= 239.0MM= .013IC=1]
042585 [IARECLIP= 1.50 IARECPE= 6.00]
042586 [LID for Outlet W17]
042587 [Assumed trench 1.25m wide 0.4 deep, 169m long, porosity of 0.4 with 250mm perforated pipe]
042588 [Total Volume provided by LID = 30 m³]
042589 [Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5]
042590 [ROUTE RESERVOIR -> 5.0 02:INF 8.92 .574 1992.0804.1400 308.60 n/a .000]
042591 [overflow <- 5.0 03:INF-LID 4.39 .563 1992.0804.1400 308.60 n/a .000]
042592 [MStoUsed= .3029E+01 m³, TotDrVVol= .1218E+01 m³, N-Over= 60, TotDrVVol= 85 hrs]
042593 [CONTINUOUS STANDBY 5.0 01:INF 8.60 .554 1992.0804.1400 308.60 421 .000]
042594 [XIMP= 54:TIMP= 64]
042595 [Horton parameters: Pw= 76.20; Fc= 13.20; DCAV= 4.14; F= .00]
042596 [Previous area IApex= 4.675LFPF=2.001LGP= 40.0MNF=250.0SFC= .0]
042597 [Impervious area IAlmp=1.571SLP= .501IM= 239.0MM= .013IC=1]
042598 [IARECLIP= 1.50 IARECPE= 6.00]
042599 [LID for Outlet W18]
042600 [Assumed trench 1.25m wide 0.4 deep, 169m long, porosity of 0.4 with 250mm perforated pipe]
042601 [Total Volume provided by LID = 30 m³]
042602 [Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5]
042603 [ROUTE RESERVOIR -> 5.0 02:INF 8.92 .574 1992.0804.1400 308.60 n/a .000]
042604 [overflow <- 5.0 03:INF-LID 4.39 .563 1992.0804.1400 308.60 n/a .000]
042605 [MStoUsed= .3029E+01 m³, TotDrVVol= .1218E+01 m³, N-Over= 60, TotDrVVol= 85 hrs]
042606 [CONTINUOUS STANDBY 5.0 01:INF 8.60 .554 1992.0804.1400 308.60 421 .000]
042607 [XIMP= 54:TIMP= 64]
042608 [Horton parameters: Pw= 76.20; Fc= 13.20; DCAV= 4.14; F= .00]
042609 [Previous area IApex= 4.675LFPF=2.001LGP= 40.0MNF=250.0SFC= .0]
042610 [Impervious area IAlmp=1.571SLP= .501IM= 239.0MM= .013IC=1]
042611 [IARECLIP= 1.50 IARECPE= 6.00]
042612 [LID for Outlet W19]
042613 [Assumed trench 1.25m wide 0.4 deep, 169m long, porosity of 0.4 with 250mm perforated pipe]
042614 [Total Volume provided by LID = 30 m³]
042615 [Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5]
042616 [ROUTE RESERVOIR -> 5.0 02:INF 8.92 .574 1992.0804.1400 308.60 n/a .000]
042617 [overflow <- 5.0 03:INF-LID 4.39 .563 1992.0804.1400 3







05401 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
05402 64 43 9 1 0 0 0 0 0
05403 R0999.C0000
05404 COMPUTE API
05405 [APFIM= 50.00; APFKEY= 9000; APFKD= .9956]
05406 [APFMAX= 57.22; APFAYG= 21.28; APFMIN= 1.69]
05407
05408 # Barhaves Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITIONS
05409
05410 R0999.C0004 -----DTM=ID:INHYD-----AREAA-QFEARMS-TpeakDate\_hh:mm-----Rvm-R.C-----DMFMS
05411 # CONTINUOUS STANDBY 5.0 01M2 8.22 .210 1999.0627, 1100 170.72 .388 .000
05412 [XIMP= 54.71MP= 64]
05413 [Horton parameters: Fw= 76.20FC= 13.20;DCAY=4.14; Fw=.00]
05414 [Previous area: IArea= 4.67;SLFP=2.00;LGP= 40.1MNF=250;SCP= .0]
05415 [Impervious area: IAlmp= 1.57;SLFP= .50;LGI= 234.1MNI=.013;SCI= .0]
05416 [IARECimp= 1.50; IARECper= 6.00]
05417 # LID for Outlet W
05418 # Assumed trench 1.25m wide 0.4 deep, 1939m long, porosity of 0.4 with 250mm perforated pipe
05419 # Total Volume provided by LID = 344 m³
05420 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05421 R0999.C0005 -----DTM=ID:INHYD-----AREAA-QFEARMS-TpeakDate\_hh:mm-----Rvm-R.C-----DMFMS
05422 ROUTE RESERVOIR -----DTM=ID:INHYD-----AREAA-QFEARMS-TpeakDate\_hh:mm-----Rvm-R.C-----DMFMS
05423 out <= 5.0 02M2 8.22 .210 1999.0627, 1100 170.72 n/a .000
05424 overflow <= 5.0 03M2-LID 4.83 .002 1999.0531, 9130 170.72 n/a .000
05425 [MxStoUsed=.330E+01 m³, TotVol=5790E+00 m³, N-Ov= 50, TotDurOv= 56 hrs]
05426 R0999.C0006 -----DTM=ID:INHYD-----AREAA-QFEARMS-TpeakDate\_hh:mm-----Rvm-R.C-----DMFMS
05427 # CONTINUOUS STANDBY 5.0 01M2 8.22 .194 1999.0627, 1100 170.72 .388 .000
05428 [XIMP= 54.71MP= 64]
05429 [Horton parameters: Fw= 76.20FC= 13.20;DCAY=4.14; Fw=.00]
05430 [Previous area: IArea= 4.67;SLFP=2.00;LGP= 40.1MNF=250;SCP= .0]
05431 [Impervious area: IAlmp= 1.57;SLFP= .50;LGI= 234.1MNI=.013;SCI= .0]
05432 [IARECimp= 1.50; IARECper= 6.00]
05433 # LID for Outlet W
05434 # Assumed trench 1.25m wide 0.4 deep, 1939m long, porosity of 0.4 with 250mm perforated pipe
05435 # Total Volume provided by LID = 330 m³
05436 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05437 R0999.C0007 -----DTM=ID:INHYD-----AREAA-QFEARMS-TpeakDate\_hh:mm-----Rvm-R.C-----DMFMS
05438 ROUTE RESERVOIR -----DTM=ID:INHYD-----AREAA-QFEARMS-TpeakDate\_hh:mm-----Rvm-R.C-----DMFMS
05439 out <= 5.0 02M2 8.22 .194 1999.0627, 1100 170.72 n/a .000
05440 overflow <= 5.0 03M2-LID 4.83 .002 1999.0531, 9130 170.72 n/a .000
05441 [MxStoUsed=.330E+01 m³, TotVol=5790E+00 m³, N-Ov= 50, TotDurOv= 56 hrs]
05442 R0999.C0008 -----DTM=ID:INHYD-----AREAA-QFEARMS-TpeakDate\_hh:mm-----Rvm-R.C-----DMFMS
05443 # CONTINUOUS STANDBY 5.0 01M2 8.22 .233 1999.0627, 1100 170.72 .388 .000
05444 [XIMP= 54.71MP= 64]
05445 [Horton parameters: Fw= 76.20FC= 13.20;DCAY=4.14; Fw=.00]
05446 [Previous area: IArea= 4.67;SLFP=2.00;LGP= 40.1MNF=250;SCP= .0]
05447 [Impervious area: IAlmp= 1.57;SLFP= .50;LGI= 239.1MNI=.013;SCI= .0]
05448 [IARECimp= 1.50; IARECper= 6.00]
05449 # LID for Outlet W
05450 # Assumed trench 1.25m wide 0.4 deep, 1939m long, porosity of 0.4 with 250mm perforated pipe
05451 # Total Volume provided by LID = 303 m³
05452 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05453 R0999.C0009 -----DTM=ID:INHYD-----AREAA-QFEARMS-TpeakDate\_hh:mm-----Rvm-R.C-----DMFMS
05454 ROUTE RESERVOIR -----DTM=ID:INHYD-----AREAA-QFEARMS-TpeakDate\_hh:mm-----Rvm-R.C-----DMFMS
05455 out <= 5.0 02M2 8.22 .233 1999.0627, 1100 170.72 n/a .000
05456 overflow <= 5.0 03M2-LID 4.83 .002 1999.0531, 9130 170.72 n/a .000
05457 [MxStoUsed=.302E+01 m³, TotVol=5702E+00 m³, N-Ov= 57, TotDurOv= 61 hrs]
05458 R0999.C0010 -----DTM=ID:INHYD-----AREAA-QFEARMS-TpeakDate\_hh:mm-----Rvm-R.C-----DMFMS
05459 # CONTINUOUS STANDBY 5.0 01M2 8.22 .203 1999.0627, 1100 170.72 .388 .000
05460 [XIMP= 54.71MP= 64]
05461 [Horton parameters: Fw= 76.20FC= 13.20;DCAY=4.14; Fw=.00]
05462 [Previous area: IArea= 4.67;SLFP=2.00;LGP= 40.1MNF=250;SCP= .0]
05463 [Impervious area: IAlmp= 1.57;SLFP= .50;LGI= 239.1MNI=.013;SCI= .0]
05464 [IARECimp= 1.50; IARECper= 6.00]
05465 # LID for Outlet W
05466 # Assumed trench 1.25m wide 0.4 deep, 1939m long, porosity of 0.4 with 250mm perforated pipe
05467 # Total Volume provided by LID = 303 m³
05468 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
05469 R0999.C0011 -----DTM=ID:INHYD-----AREAA-QFEARMS-TpeakDate\_hh:mm-----Rvm-R.C-----DMFMS
05470 ROUTE RESERVOIR -----DTM=ID:INHYD-----AREAA-QFEARMS-TpeakDate\_hh:mm-----Rvm-R.C-----DMFMS
05471 out <= 5.0 02M2 8.22 .203 1999.0627, 1100 170.72 n/a .000
05472 overflow <= 5.0 03M2-LID 4.83 .002 1999.0531, 9130 170.72 n/a .000
05473 [MxStoUsed=.303E+01 m³, TotVol=5702E+00 m³, N-Ov= 62, TotDurOv= 61 hrs]
05474 R0999.C0012 -----DTM=ID:INHYD-----AREAA-QFEARMS-TpeakDate\_hh:mm-----Rvm-R.C-----DMFMS
05475 ADD HYD + 5.0 02M2 8.22 .194 1999.0627, 1100 170.72 n/a .000
05476 + 5.0 02M2 8.22 .194 1999.0627, 1100 170.72 n/a .000
05477 + 5.0 01M2-PH3 8.60 .203 1999.0627, 1100 170.72 n/a .000
05478 + 5.0 01M2-PH3 35.64 .840 1999.0627, 1100 170.72 n/a .000
05479 R0999.C0013 -----DTM=ID:INHYD-----AREAA-QFEARMS-TpeakDate\_hh:mm-----Rvm-R.C-----DMFMS
05480 ADD HYD + 5.0 02M2-LID 3.81 .208 1999.0627, 1100 170.72 n/a .000
05481 + 5.0 02M2-LID 4.83 .002 1999.0531, 9130 170.72 n/a .000
05482 + 5.0 02M2-LID 5.10 .231 1999.0627, 1100 170.72 n/a .000
05483 + 5.0 02M2-LID 4.00 .201 1999.0627, 1100 170.72 n/a .000
05484 + 5.0 01M2-PH3 16.30 .431 1999.0627, 1100 170.72 n/a .000
05485 + 5.0 01M2-PH3 35.64 .840 1999.0627, 1100 170.72 n/a .000
05486 # Barhaves Conservancy Development Phase 3 (WITH INFILTRATION) - POST DEVELOPMENT CONDITIONS
05487 # Set infiltration to 0 (CN = 99.99) for water balance analysis
05488 # CONTINUOUS STANDBY 5.0 01M2-W1 8.22 .348 1999.0627, 1100 260.60 .592 .000
05489 [XIMP= 54.71MP= 64]
05490 [LOGS= 2 ICM=100.0]
05491 [Previous area: IArea= 4.67;SLFP=2.00;LGP= 40.1MNF=250;SCP= .0]
05492 [Impervious area: IAlmp= 1.57;SLFP= .50;LGI= 244.1MNI=.013;SCI= .0]
05493 [IARECimp= 1.50; IARECper= 6.00]
05494 [SMIN= 1.39; SMAX= 9.24; SK= .030]
05495 R0999.C0015 -----DTM=ID:INHYD-----AREAA-QFEARMS-TpeakDate\_hh:mm-----Rvm-R.C-----DMFMS
05496 # CONTINUOUS STANDBY 5.0 01M2-W1 8.22 .386 1999.0627, 1100 260.60 .592 .000
05497 [XIMP= 54.71MP= 64]
05498 [LOGS= 2 ICM=100.0]
05499 [Previous area: IArea= 4.67;SLFP=2.00;LGP= 40.1MNF=250;SCP= .0]
05500 [Impervious area: IAlmp= 1.57;SLFP= .50;LGI= 239.1MNI=.013;SCI= .0]
05501 [IARECimp= 1.50; IARECper= 6.00]
05502 [SMIN= 1.39; SMAX= 9.24; SK= .030]
05503 R0999.C0016 -----DTM=ID:INHYD-----AREAA-QFEARMS-TpeakDate\_hh:mm-----Rvm-R.C-----DMFMS
05504 ADD HYD + 5.0 02M2-W1 8.22 .348 1999.0627, 1100 260.60 n/a .000
05505 + 5.0 02M2-W1 8.22 .348 1999.0627, 1100 260.60 n/a .000
05506 + 5.0 02M2-W1 9.30 .386 1999.0627, 1100 260.60 n/a .000
05507 + 5.0 01M2-PH3 8.60 .203 1999.0627, 1100 170.72 n/a .000
05508 + 5.0 01M2-PH3 35.64 .840 1999.0627, 1100 170.72 n/a .000
05509 # CONTINUOUS RAINFALL DATA
05510 \*\*\*\*\*
05511 \*\*\*\*\*
05512 \*\*\*\*\*
05513 \*\*\*\*\*
05514 \*\*\*\*\*
05515 \*\*\*\*\*
05516 \*\*\*\*\*
05517 \*\*\*\*\*
05518 \*\*\*\*\*
05519 \*\*\*\*\*
05520 \*\*\*\*\*
05521 \*\*\*\*\*
05522 \*\*\*\*\*
05523 R0999.C0018 -----DTM=ID:INHYD-----AREAA-QFEARMS-TpeakDate\_hh:mm-----Rvm-R.C-----DMFMS
05524 ADD HYD + 5.0 02M2-W1 8.22 .348 1999.0627, 1100 260.60 n/a .000
05525 + 5.0 02M2-W1 8.22 .348 1999.0627, 1100 260.60 n/a .000
05526 + 5.0 02M2-W1 9.30 .386 1999.0627, 1100 260.60 n/a .000
05527 + 5.0 01M2-PH3 8.60 .203 1999.0627, 1100 170.72 n/a .000
05528 + 5.0 01M2-PH3 35.64 .840 1999.0627, 1100 170.72 n/a .000
05529 \*\*\*\*\*
05530 \*\*\*\*\*
05531 \*\*\*\*\*
05532 \*\*\*\*\*
05533 \*\*\*\*\*
05534 \*\*\*\*\*
05535 \*\*\*\*\*
05536 \*\*\*\*\*
05537 \*\*\*\*\*
05538 \*\*\*\*\*
05539 \*\*\*\*\*
05540 R0999.C0001
05541 R0999.C0001
05542 START
05543 [TZRO= .00 hrs on 19990101]
05544 [MTOU= 2 (1-Imperial, 2-metric output)]
05545 [MTRM= 0]
05546 [MUN= .009]
05547
05548 # SWSHYMO Ver:5.02/Jan 2001 cBETA / INPUT DATA FILE
05549 # Project Name: Barhaves Conservancy Development
05550 # Date : 2021/Oct/19
05551 # Modeler : J.Burnett, P.Eng.
05552 # Company : J.F. Sabourin and Associates
05553 # License #: 23820-01
05554 # \*\*\*\*\*
05555 # \*\*\*\*\*
05556 # \*\*\*\*\*
05557 # \*\*\*\*\*
05558 R0999.C0002
05559 # HEAD ARE DATA
05560 [Filename= YOM\_1967\_2007\_123 ]
05561 [Start\_date= 1999.0101; End\_date= 1999.1231]
05562 [DT= 60;min; Length= 1640; hrs; WetHrs= 4193; PTO= 424.40]
05563 # Maximum average rainfall intensities over
05564 1 hr 2 hrs 3 hrs 6 hrs 12 hrs 24 hrs 36 hrs 48 hrs 72 hrs
05565 17.50 20.20 21.10 39.40 39.70 39.70 52.20 58.60 69.50 mm/hr
05566 199701 199707 199708 199709 199710 199711 199712 199801 199802 199803 199804 199805 199806 199807 199808 199809 199810 199811 199812 199901 199902 199903 199904 199905 199906 199907 199908 199909 199910 199911 199912 200001 200002 200003 200004 200005 200006 200007 200008 200009 200010 200011 200012 200101 200102 200103 200104 200105 200106 200107 200108 200109 200110 200111 200112 200201 200202 200203 200204 200205 200206 200207 200208 200209 200210 200211 200212 200301 200302 200303 200304 200305 200306 200307 200308 200309 200310 200311 200312 200401 200402 200403 200404 200405 200406 200407 200408 200409 200410 200411 200412 200501 200502 200503 200504 200505 200506 200507 200508 200509 200510 200511 200512 200601 200602 200603 200604 200605 200606 200607 200608 200609 200610 200611 200612 200701 200702 200703 200704 200705 200706 200707 200708 200709 200710 200711 200712 200801 200802 200803 200804 200805 200806 200807 200808 200809 200810 200811 200812 200901 200902 200903 200904 200905 200906 200907 200908 200909 200910 200911 200912 201001 201002 201003 201004 201005 201006 201007 201008 201009 201010 201011 201012 201101 201102 201103 201104 201105 201106 201107 201108 201109 201110 201111 201112 201201 201202 201203 201204 201205 201206 201207 201208 201209 201210 201211 201212 201301 201302 201303 201304 201305 201306 201307 201308 201309 201310 201311 201312 201401 201402 201403 201404 201405 201406 201407 201408 201409 201410 201411 201412 201501 201502 201503 201504 201505 201506 201507 201508 201509 201510 201511 201512 201601 201602 201603 201604 201605 201606 201607 201608 201609 201610 201611 201612 201701 201702 201703 201704 201705 201706 201707 201708 201709 201710 201711 201712 201801 201802 201803 201804 201805 201806 201807 201808 201809 201810 201811 201812 201901 201902 201903 201904 201905 201906 201907 201908 201909 201910 201911 201912 202001 202002 202003 202004 202005 202006 202007 202008 202009 202010 202011 202012 202101 202102 202103 202104 202105 202106 202107 202108 202109 202110 202111 202112 202201 202202 202203 202204 202205 202206 202207 202208 202209 202210 202211 202212 202301 202302 202303 202304 202305 202306 202307 202308 202309 202310 202311 202312 202401 202402 202403 202404 202405 202406 202407 202408 202409 202410 202411 202412 202501 202502 202503 202504 202505 202506 202507 202508 202509 202510 202511 202512 202601 202602 202603 202604 202605 202606 202607 202608 202609 202610 202611 202612 202701 202702 202703 202704 202705 202706 202707 202708 202709 202710 202711 202712 202801 202802 202803 202804 202805 202806 202807 202808 202809 202810 202811 202812 202901 202902 202903 202904 202905 202906 202907 202908 202909 202910 202911 202912 203001 203002 203003 203004 203005 203006 203007 203008 203009 203010 203011 203012 203101 203102 203103 203104 203105 203106 203107 203108 203109 203110 203111 203112 203201 203202 203203 203204 203205 203206 203207 203208 203209 203210 203211 203212 203301 203302 203303 203304 203305 203306 203307 203308 203309 203310 203311 203312 203401 203402 203403 203404 203405 203406 203407 203408 203409 203410 203411 203412 203501 203502 203503 203504 203505 203506 203507 203508 203509 203510 203511 203512 203601 203602 203603 203604 203605 203606 203607 203608 203609 203610 203611 203612 203701 203702 203703 203704 203705 203706 203707 203708 203709 203710 203711 203712 203801 203802 203803 203804 203805 203806 203807 203808 203809 203810 203811 203812 203901 203902 203903 203904 203905 203906 203907 203908 203909 203910 203911 203912 204001 204002 204003 204004 204005 204006 204007 204008 204009 204010 204011 204012 204101 204102 204103 204104 204105 204106 204107 204108 204109 204110 204111 204112 204201 204202 204203 204204 204205 204206 204207 204208 204209 204210 204211 204212 204301 204302 204303 204304 204305 204306 204307 204308 204309 204310 204311 204312 204401 204402 204403 204404 204405 204406 204407 204408 204409 204410 204411 204412 204501 204502 204503 204504 204505 204506 204507 204508 204509 204510 204511 204512 204601 204602 204603 204604 204605 204606 204607 204608 204609 204610 204611 204612 204701 204702 204703 204704 204705 204706 204707 204708 204709 204710 204711 204712 204801 204802 204803 204804 204805 204806 204807 204808 204809 204810 204811 204812 204901 204902 204903 204904 204905 204906 204907 204908 204909 204910 204911 204912 205001 205002 205003 205004 205005 205006 205007 205008 205009 205010 205011 205012 205101 205102 205103 205104 205105 205106 205107 205108 205109 205110 205111 205112 205201 205202 205203 205204 205205 205206 205207 205208 205209 205210 205211 205212 205301 205302 205303 205304 205305 205306 205307 205308 205309 205310 205311 205312 205401 205402 205403 205404 205405 205406 205407 205408 205409 205410 205411 205412 205501 205502 205503 205504 205505 205506 205507 205508 205509 205510 205511 205512 205601 205602 205603 205604 205605 205606 205607 205608 205609 205610 205611 205612 205701 205702 205703 205704 205705 205706 205707 205708 205709 205710 205711 205712 205801 205802 205803 205804 205805 205806 205807 205808 205809 205810 205811 205812 205901 205902 205903 205904 205905 205906 205907 205908 205909 205910 205911 205912 206001 206002 206003 206004 206005 206006 206007 206008 206009 206010 206011 206012 206101 206102 206103 206104 206105 206106 206107 206108 206109 206110 206111 206112 206201 206202 206203 206204 206205 206206 206207 206208 206209 206210 206211 206212 206301 206302 206303 206304 206305 206306 206307 206308 206309 206310 206311 206312 206401 206402 206403 206404 206405 206406 206407 206408 206409 206410 206411 206412 206501 206502 206503 206504 206505 206506 206507 206508 206509 206510 206511 206512 206601 206602 206603 206604 206605 206606 206607 206608 206609 206610 206611 206612 206701 206702 206703 206704 206705 206706 206707 206708 206709 206710 206711 206712 206801 206802 206803 206804 206805 206806 206807 206808 206809 206810 206811 206812 206901 206902 206903 206904 206905 206906 206907 206908 206909 206910 206911 206912 207001 207002 207003 207004 207005 207006 207007 207008 207009 207010 207011 207012 207101 207102 207103 207104 207105 207106 207107 207108 207109 207110 207111 207112 207201 207202 207203 207204 207205 207206 207207 207208 207209 207210 207211 207212 207301 207302 207303 207304 207305 207306 207307 207308 207309 207310 207311 207312 207401 207402 207403 207404 207405 207406 207407 207408 207409 207410 207411 207412 207501 207502 207503 207504 207505 207506 207507 207508 207509 207510 207511 207512 207601 207602 207603 207604 207605 207606 207607 207608 207609 207610 207611 207612



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06121 R0103:CO007-----DtnIn-ID:HYD-----AREAb-QFEARqns-TpeakDate_hh:mm-----RvMn-R-C-----DWFCms
06122 ROUTE RESERVOIR -> 5.0 02M4 8.22 .199 2003.0711.1700 228.03 n/a .000
06123 out <= 5.0 01M2-LID 4.53 .002 2003.0501.1400 228.03 n/a .000
06124 overflow <= 5.0 03M4-LID-Out 3.69 .189 2003.0711.1700 228.03 n/a .000
06125 Hmst00sedn-3030E-01 n3, TotDvVol=8410E+00 n3, N-Ovr= 47, TotDurOvr= 84.hrs)
06126 R0103:CO008-----DtnIn-ID:HYD-----AREAb-QFEARqns-TpeakDate_hh:mm-----RvMn-R-C-----DWFCms
06127 CONTINUOUS STANDHYD 5.0 01M4 8.60 .221 2003.0711.1700 228.03 .411 .000
06128 [XMP= 54:TMP=64]
06129 [Horton parameters: F= 76.20(F= 13.20;DCA=4.14; F= .0)]
06130 [Impervious area: IArea= 4.67;SIFP=2.00;IGP= 40;.IMP=250;SFC= .0]
06131 [Impervious area: IArea= 1.57;SIFP= .50;IWI= 257;.IMI=.01;SCI= .0]
06132 [IARECLMP= 1.50; IARECPE= 6.00]
06133 # LID for Outlet W3
06134 # Assumed trench 1.25m wide 0.4 deep, 163m long, porosity of 0.4 with 25mm perforated pipe
06135 # Total Volume provided by LID = 303 m3
06136 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
06137 R0103:CO009-----DtnIn-ID:HYD-----AREAb-QFEARqns-TpeakDate_hh:mm-----RvMn-R-C-----DWFCms
06138 ROUTE RESERVOIR -> 5.0 02M3 9.90 .221 2003.0711.1700 228.03 n/a .000
06139 out <= 5.0 01M2-LID 4.55 .002 2003.0501.2100 228.08 n/a .000
06140 overflow <= 5.0 03M4-LID-Out 5.35 .228 2003.0711.1700 228.03 n/a .000
06141 Hmst00sedn-3030E-01 n3, TotDvVol=1221E+01 n3, N-Ovr= 69, TotDurOvr= 120.hrs)
06142 R0103:CO010-----DtnIn-ID:HYD-----AREAb-QFEARqns-TpeakDate_hh:mm-----RvMn-R-C-----DWFCms
06143 CONTINUOUS STANDHYD 5.0 01M4 8.60 .201 2003.0711.1700 228.03 .411 .000
06144 [XMP= 54:TMP=64]
06145 [Horton parameters: F= 76.20(F= 13.20;DCA=4.14; F= .0)]
06146 [Impervious area: IArea= 4.67;SIFP=2.00;IGP= 40;.IMP=250;SFC= .0]
06147 [Impervious area: IArea= 1.57;SIFP= .50;IWI= 257;.IMI=.01;SCI= .0]
06148 [IARECLMP= 1.50; IARECPE= 6.00]
06149 # LID for Outlet W3
06150 # Assumed trench 1.25m wide 0.4 deep, 163m long, porosity of 0.4 with 25mm perforated pipe
06151 # Total Volume provided by LID = 303 m3
06152 # Soil infiltration rates assumed at 9mm/hr with a safety factor of 2.5
06153 R0103:CO011-----DtnIn-ID:HYD-----AREAb-QFEARqns-TpeakDate_hh:mm-----RvMn-R-C-----DWFCms
06154 ROUTE RESERVOIR -> 5.0 02M4 8.60 .201 2003.0711.1700 228.03 n/a .000
06155 out <= 5.0 02M-LID 4.37 .002 2003.0501.2100 228.08 n/a .000
06156 overflow <= 5.0 03M4-LID-Out 4.23 .198 2003.0711.1700 228.03 n/a .000
06157 Hmst00sedn-3030E-01 n3, TotDvVol=9555E+00 n3, N-Ovr= 51, TotDurOvr= 106.hrs)
06158 R0103:CO012-----DtnIn-ID:HYD-----AREAb-QFEARqns-TpeakDate_hh:mm-----RvMn-R-C-----DWFCms
06159 ADD HYD 5.0 02M1 8.92 .228 2003.0711.1700 228.03 n/a .000
06160 + 5.0 02M2 8.90 .231 2003.0711.1700 228.03 n/a .000
06161 + 5.0 02M3 9.90 .201 2003.0711.1700 228.03 n/a .000
06162 + 5.0 02M4 8.60 .201 2003.0711.1700 228.03 n/a .000
06163 SUM= 5.0 01:RCD-PH3 35.64 .832 2003.0711.1700 228.03 n/a .000
06164 R0103:CO013-----DtnIn-ID:HYD-----AREAb-QFEARqns-TpeakDate_hh:mm-----RvMn-R-C-----DWFCms
06165 ADD HYD 5.0 02M-LID-Out 4.11 .005 2003.0711.1700 228.03 n/a .000
06166 + 5.0 02M2-LID-Out 3.69 .189 2003.0711.1700 228.02 n/a .000
06167 + 5.0 02M3-LID-Out 5.35 .228 2003.0711.1700 228.03 n/a .000
06168 + 5.0 02M4-LID-Out 4.23 .198 2003.0711.1700 228.03 n/a .000
06169 SUM= 5.0 01:RCD-PH3-L1 17.39 .819 2003.0711.1700 228.03 n/a .000
06170 # Barhaven Conservancy Development Phase 3 (WITHOUT INFILTRATION) - POST DEVELOPMENT CONDITIONS
06171 # Set infiltration to 0 (CN = 99.99) for water balance analysis
06172 R0103:CO014-----DtnIn-ID:HYD-----AREAb-QFEARqns-TpeakDate_hh:mm-----RvMn-R-C-----DWFCms
06173 CONTINUOUS STANDHYD 5.0 01:INF-W1 8.92 .358 2003.0711.1700 358.61 .647 .000
06174 [XMP= 54:TMP=64]
06175 [LOGS= 2 :CN=100.0]
06176 [Impervious area: IArea= 4.67;SIFP=2.00;IGP= 40;.IMP=250;SFC= .0]
06177 [Impervious area: IArea= 1.57;SIFP= .50;IWI= 244;.IMI=.01;SCI= .0]
06178 [IARECLMP= 1.50; IARECPE= 6.00]
06179 [SMIN= 1.39; SMAX= 9.24; SW= .030]
06180 R0103:CO015-----DtnIn-ID:HYD-----AREAb-QFEARqns-TpeakDate_hh:mm-----RvMn-R-C-----DWFCms
06181 CONTINUOUS STANDHYD 5.0 01:INF-W2 8.22 .330 2003.0711.1700 358.61 .647 .000
06182 [XMP= 54:TMP=64]
06183 [LOGS= 2 :CN=100.0]
06184 [Impervious area: IArea= 4.67;SIFP=2.00;IGP= 40;.IMP=250;SFC= .0]
06185 [Impervious area: IArea= 1.57;SIFP= .50;IWI= 234;.IMI=.01;SCI= .0]
06186 [IARECLMP= 1.50; IARECPE= 6.00]
06187 [SMIN= 1.39; SMAX= 9.24; SW= .030]
06188 R0103:CO016-----DtnIn-ID:HYD-----AREAb-QFEARqns-TpeakDate_hh:mm-----RvMn-R-C-----DWFCms
06189 CONTINUOUS STANDHYD 5.0 01:INF-W3 9.90 .396 2003.0711.1700 358.61 .647 .000
06190 [XMP= 54:TMP=64]
06191 [LOGS= 2 :CN=100.0]
06192 [Impervious area: IArea= 4.67;SIFP=2.00;IGP= 40;.IMP=250;SFC= .0]
06193 [Impervious area: IArea= 1.57;SIFP= .50;IWI= 257;.IMI=.01;SCI= .0]
06194 [IARECLMP= 1.50; IARECPE= 6.00]
06195 [SMIN= 1.39; SMAX= 9.24; SW= .030]
06196 R0103:CO017-----DtnIn-ID:HYD-----AREAb-QFEARqns-TpeakDate_hh:mm-----RvMn-R-C-----DWFCms
06197 CONTINUOUS STANDHYD 5.0 01:INF-W4 8.60 .345 2003.0711.1700 358.61 .647 .000
06198 [XMP= 54:TMP=64]
06199 [LOGS= 2 :CN=100.0]
06200 [Impervious area: IArea= 4.67;SIFP=2.00;IGP= 40;.IMP=250;SFC= .0]
06201 [Impervious area: IArea= 1.57;SIFP= .50;IWI= 239;.IMI=.01;SCI= .0]
06202 [IARECLMP= 1.50; IARECPE= 6.00]
06203 [SMIN= 1.39; SMAX= 9.24; SW= .030]
06204 R0103:CO018-----DtnIn-ID:HYD-----AREAb-QFEARqns-TpeakDate_hh:mm-----RvMn-R-C-----DWFCms
06205 ADD HYD 5.0 02:INF-W1 8.92 .358 2003.0711.1700 358.61 n/a .000
06206 + 5.0 02:INF-W2 8.22 .330 2003.0711.1700 358.61 n/a .000
06207 + 5.0 02:INF-W3 9.90 .396 2003.0711.1700 358.61 n/a .000
06208 + 5.0 02:INF-W4 8.60 .345 2003.0711.1700 358.61 n/a .000
06209 SUM= 5.0 01:RCD-PH3 35.64 .832 2003.0711.1700 358.61 n/a .000
06210 #####
06211 # CONTINUOUS RAINFALL DATA
06212 #####
06213 R0103:CO002-----DtnIn-ID:HYD-----AREAb-QFEARqns-TpeakDate_hh:mm-----RvMn-R-C-----DWFCms
06214 FINISH
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06301 *** WARNING: Requested start date is less than start date in file.
06302 *** WARNING: Missing rainfall increments were set to 0.
06303 R0096:CO0004 CONTINUOUS STANDHYD
06304 *** NOTE: The pervious area has no runoff.
06305 R0096:CO0006 CONTINUOUS STANDHYD
06306 *** NOTE: The pervious area has no runoff.
06307 R0096:CO0008 CONTINUOUS STANDHYD
06308 *** NOTE: The pervious area has no runoff.
06309 R0096:CO0010 CONTINUOUS STANDHYD
06310 *** NOTE: The pervious area has no runoff.
06311 R0097:CO0002 READ AES DATA
06312 *** WARNING: Missing rainfall increments were set to 0.
06313 R0097:CO0004 CONTINUOUS STANDHYD
06314 *** NOTE: The pervious area has no runoff.
06315 R0097:CO0006 CONTINUOUS STANDHYD
06316 *** NOTE: The pervious area has no runoff.
06317 R0097:CO0008 CONTINUOUS STANDHYD
06318 *** NOTE: The pervious area has no runoff.
06319 R0097:CO0010 CONTINUOUS STANDHYD
06320 *** NOTE: The pervious area has no runoff.
06321 R0098:CO0002 READ AES DATA
06322 *** WARNING: Requested start date is less than start date in file.
06323 *** WARNING: Missing rainfall increments were set to 0.
06324 R0098:CO0004 CONTINUOUS STANDHYD
06325 *** NOTE: The pervious area has no runoff.
06326 R0098:CO0006 CONTINUOUS STANDHYD
06327 *** NOTE: The pervious area has no runoff.
06328 R0098:CO0008 CONTINUOUS STANDHYD
06329 *** NOTE: The pervious area has no runoff.
06330 R0098:CO0010 CONTINUOUS STANDHYD
06331 *** NOTE: The pervious area has no runoff.
06332 *** WARNING: Requested start date is less than start date in file.
06333 *** WARNING: Missing rainfall increments were set to 0.
06334 *** WARNING: Requested start date is less than start date in file.
06335 *** WARNING: Missing rainfall increments were set to 0.
06336 *** WARNING: Missing rainfall increments were set to 0.
06337 *** WARNING: Requested start date is less than start date in file.
06338 *** WARNING: Missing rainfall increments were set to 0.
06339 *** WARNING: Requested start date is less than start date in file.
06340 *** WARNING: Missing rainfall increments were set to 0.
06341 Simulation ended on 2021-10-19 at 10:04:29
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# Attachment B

## Water Budget Results



**Table B1: BCD Phase 3 - Pre Development Water Budget**

Year	Total Rainfall		Runoff (No Infiltration)		Evaporation		Runoff		Infiltration	
	(mm)	(m <sup>3</sup> )	(mm)	(m <sup>3</sup> )	(mm)	(m <sup>3</sup> )	(mm)	(m <sup>3</sup> )	(mm)	(m <sup>3</sup> )
1967	386.9	137,891	190.21	67,791	196.7	70,100	36.4	12,962	153.8	54,829
1968	592.8	211,274	257.40	91,737	335.4	119,537	38.2	13,618	219.2	78,119
1969	570.3	203,255	233.70	83,291	336.6	119,964	30.5	10,870	203.2	72,420
1970	558.9	199,192	222.47	79,288	336.4	119,904	29.9	10,649	192.6	68,639
1971	522.1	186,076	181.82	64,801	340.3	121,276	22.3	7,937	159.6	56,864
1972	784.3	279,525	375.41	133,796	408.9	145,728	71.4	25,447	304.0	108,349
1973	744.9	265,482	337.66	120,342	407.2	145,140	51.0	18,180	286.7	102,162
1974	386.2	137,642	119.81	42,700	266.4	94,941	13.4	4,758	106.5	37,942
1975	535.5	190,852	219.51	78,233	316.0	112,619	30.7	10,938	188.8	67,295
1976	493.2	175,776	170.05	60,606	323.2	115,171	19.7	7,007	150.4	53,599
1977	677.8	241,568	283.86	101,168	393.9	140,400	39.5	14,081	244.4	87,086
1978	641.4	228,595	269.84	96,171	371.6	132,424	29.6	10,560	240.2	85,611
1979	866.5	308,821	449.28	160,123	417.2	148,697	82.8	29,496	366.5	130,628
1980	622	221,681	254.15	90,579	367.9	131,102	32.8	11,686	221.4	78,893
1981	936.4	333,733	459.70	163,837	476.7	169,896	116.7	41,599	343.0	122,238
1982	596.1	212,450	228.69	81,505	367.4	130,945	26.0	9,263	202.7	72,242
1983	587.5	209,385	217.30	77,446	370.2	131,939	28.9	10,289	188.4	67,156
1984	459.4	163,730	207.21	73,850	252.2	89,881	27.6	9,830	179.6	64,020
1985	559.9	199,548	262.29	93,480	297.6	106,068	29.0	10,336	233.3	83,145
1986	849.4	302,726	418.06	148,997	431.3	153,730	88.5	31,556	329.5	117,441
1987	640.1	228,132	240.27	85,632	399.8	142,499	40.5	14,431	199.8	71,202
1988	643.8	229,450	255.71	91,135	388.1	138,315	37.6	13,390	218.1	77,745
1989	523.2	186,468	197.69	70,457	325.5	116,012	23.0	8,187	174.7	62,270
1990	727.8	259,388	311.89	111,158	415.9	148,230	48.0	17,097	263.9	94,061
1991	556	198,158	197.89	70,528	358.1	127,630	25.5	9,095	172.4	61,433
1992	732.8	261,170	326.37	116,318	406.4	144,852	55.2	19,680	271.2	96,638
1993	721.3	257,071	264.26	94,182	457.0	162,889	34.7	12,378	229.5	81,804
1994	540.2	192,527	227.40	81,045	312.8	111,482	34.1	12,146	193.3	68,899
1995	538.5	191,921	327.35	116,668	211.2	75,254	107.0	38,142	220.3	78,526
1996	512.2	182,548	195.06	69,519	317.1	113,029	25.5	9,095	169.5	60,424
1997	433.2	154,392	161.58	57,587	271.6	96,805	15.1	5,382	146.5	52,205
1998	440.3	156,923	163.10	58,129	277.2	98,794	17.7	6,315	145.4	51,813
1999	424.4	151,256	171.71	61,197	252.7	90,059	18.5	6,586	153.2	54,611
2000	535.9	190,995	214.65	76,501	321.3	114,494	31.8	11,319	182.9	65,182
2002	551.5	196,555	294.04	104,796	257.5	91,759	62.7	22,357	231.3	82,439
2003	554.6	197,659	251.88	89,770	302.7	107,889	43.2	15,379	208.7	74,391
Minimum	386.2	137,642	120	42700	196.7	70,100	13.4	4,758	106.5	37,942
Maximum	936.4	333,733	460	163837	476.7	169,896	116.7	41,599	366.5	130,628
Average	595.8	212,328	254	90677	341.3	121,651	40.7	14,501	213.7	76,176
Percentage	100.0%	100.0%	42.7%	42.7%	57.3%	57.3%	6.8%	6.8%	35.9%	35.9%

**Table B2: BCD Phase 3 - Post Development Water Budget - Without LIDs**

Year	Total Rainfall		Runoff (No Infiltration)		Evaporation		Runoff		Infiltration	
	(mm)	(m <sup>3</sup> )	(mm)	(m <sup>3</sup> )	(mm)	(m <sup>3</sup> )	(mm)	(m <sup>3</sup> )	(mm)	(m <sup>3</sup> )
1967	386.9	137,891	264.01	94,093	122.9	43,798	165.9	59,116	98.1	34,977
1968	592.8	211,274	378.65	134,951	214.2	76,323	247.5	88,213	131.1	46,738
1969	570.3	203,255	349.05	124,401	221.3	78,854	226.7	80,778	122.4	43,623
1970	558.9	199,192	341.01	121,536	217.9	77,656	230.7	82,211	110.3	39,325
1971	522.1	186,076	300.01	106,924	222.1	79,153	201.4	71,779	98.6	35,145
1972	784.3	279,525	527.33	187,940	257.0	91,584	345.7	123,190	181.7	64,751
1973	744.9	265,482	478.82	170,651	266.1	94,831	312.2	111,282	166.6	59,369
1974	386.2	137,642	211.02	75,208	175.2	62,434	143.3	51,086	67.7	24,121
1975	535.5	190,852	336.48	119,921	199.0	70,931	224.3	79,930	112.2	39,992
1976	493.2	175,776	279.75	99,703	213.5	76,074	184.8	65,845	95.0	33,858
1977	677.8	241,568	430.70	153,501	247.1	88,066	281.6	100,359	149.1	53,143
1978	641.4	228,595	413.06	147,215	228.3	81,380	273.5	97,483	139.5	49,732
1979	866.5	308,821	604.35	215,390	262.2	93,430	384.0	136,847	220.4	78,543
1980	622	221,681	393.13	140,112	228.9	81,569	255.1	90,907	138.1	49,205
1981	936.4	333,733	632.43	225,398	304.0	108,335	416.2	148,316	216.3	77,082
1982	596.1	212,450	372.35	132,706	223.8	79,745	246.6	87,878	125.8	44,828
1983	587.5	209,385	355.31	126,632	232.2	82,753	234.3	83,508	121.0	43,124
1984	459.4	163,730	303.36	108,118	156.0	55,613	192.8	68,728	110.5	39,389
1985	559.9	199,548	379.24	135,161	180.7	64,387	241.8	86,192	137.4	48,969
1986	849.4	302,726	579.81	206,644	269.6	96,082	363.5	129,544	216.3	77,100
1987	640.1	228,132	383.53	136,690	256.6	91,442	254.0	90,529	129.5	46,161
1988	643.8	229,450	390.26	139,089	253.5	90,362	261.2	93,099	129.0	45,990
1989	523.2	186,468	314.66	112,145	208.5	74,324	207.9	74,110	106.7	38,035
1990	727.8	259,388	456.65	162,750	271.2	96,638	293.1	104,457	163.6	58,293
1991	556	198,158	331.20	118,040	224.8	80,119	221.6	78,985	109.6	39,054
1992	732.8	261,170	471.31	167,975	261.5	93,195	308.6	109,985	162.7	57,990
1993	721.3	257,071	434.50	154,856	286.8	102,216	288.4	102,782	146.1	52,074
1994	540.2	192,527	341.46	121,696	198.7	70,831	220.0	78,390	121.5	43,306
1995	538.5	191,921	404.90	144,306	133.6	47,615	247.1	88,052	157.8	56,254
1996	512.2	182,548	312.66	111,432	199.5	71,116	205.1	73,108	107.5	38,324
1997	433.2	154,392	267.24	95,244	166.0	59,148	176.6	62,926	90.7	32,318
1998	440.3	156,923	260.60	92,878	179.7	64,045	170.7	60,845	89.9	32,033
1999	424.4	151,256	268.01	95,519	156.4	55,737	173.3	61,750	94.8	33,769
2000	535.9	190,995	325.68	116,072	210.2	74,922	212.5	75,731	113.2	40,341
2002	551.5	196,555	391.69	139,598	159.8	56,956	252.6	90,041	139.1	49,557
2003	554.6	197,659	358.61	127,809	196.0	69,851	228.0	81,270	130.6	46,539
Minimum	386.2	137,642	211	75208	122.9	43,798	143.3	51,086	67.7	24,121
Maximum	936.4	333,733	632	225398	304.0	108,335	416.2	148,316	220.4	78,543
Average	595.8	212,328	379	135064	216.8	77,264	247.0	88,035	132.0	47,029
Percentage	100.0%	100.0%	63.6%	63.6%	36.4%	36.4%	41.5%	41.5%	22.1%	22.1%

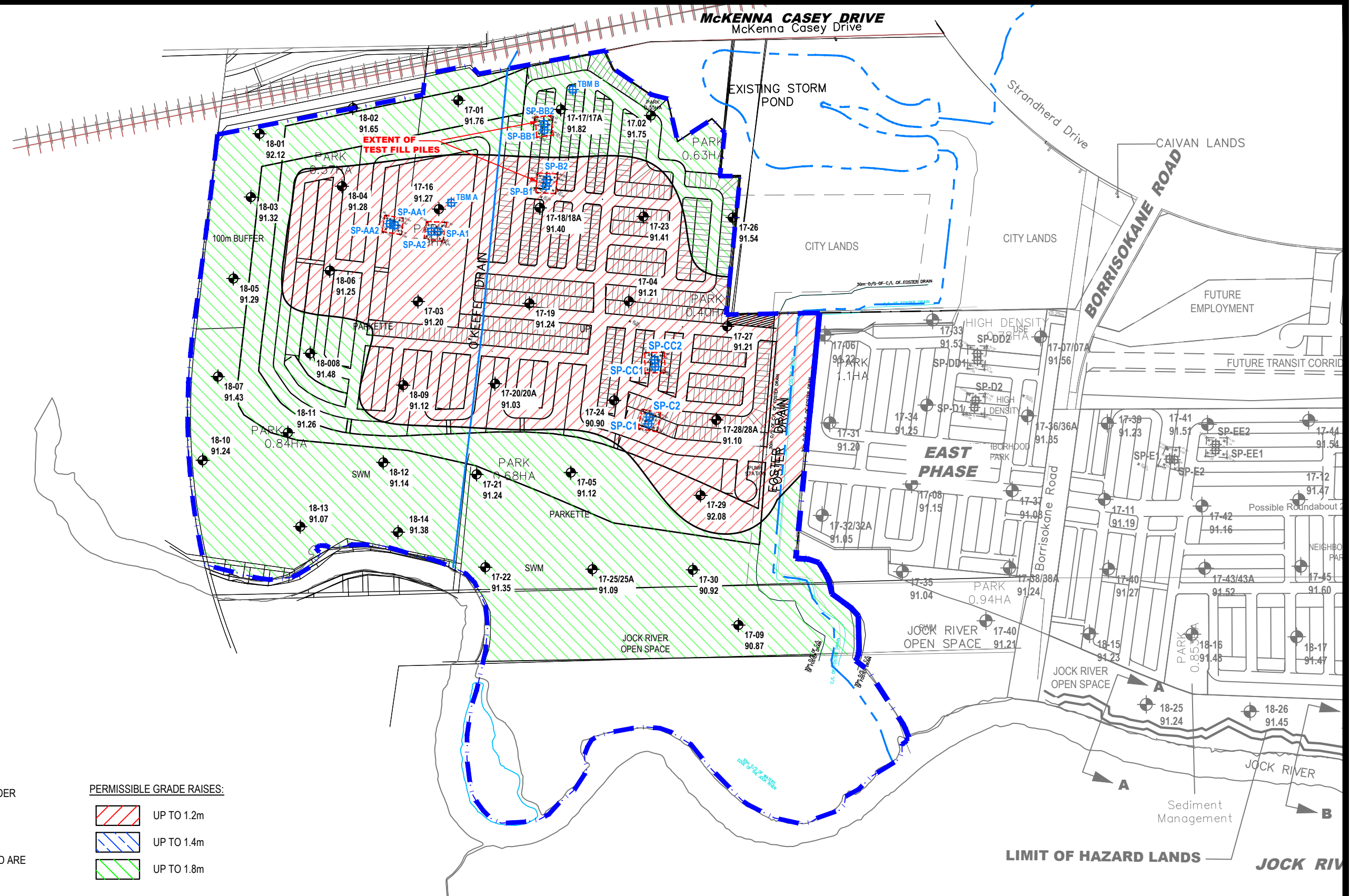
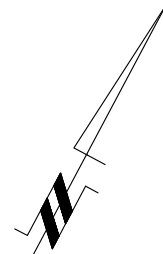
**Table B3: BCD Phase 3- Post Development Water Budget - With LIDs**

Year	Total Rainfall		Runoff (No Infiltration)		Evaporation		Runoff		Infiltration	
	(mm)	(m <sup>3</sup> )	(mm)	(m <sup>3</sup> )	(mm)	(m <sup>3</sup> )	(mm)	(m <sup>3</sup> )	(mm)	(m <sup>3</sup> )
1967	386.9	137,891	264.01	94,093	122.9	43,798	91.8	32,726	172.2	61,367
1968	592.8	211,274	378.65	134,951	214.2	76,323	118.5	42,225	260.2	92,726
1969	570.3	203,255	349.05	124,401	221.3	78,854	108.3	38,598	240.7	85,803
1970	558.9	199,192	341.01	121,536	217.9	77,656	111.8	39,860	229.2	81,676
1971	522.1	186,076	300.01	106,924	222.1	79,153	83.4	29,727	216.6	77,197
1972	784.3	279,525	527.33	187,940	257.0	91,584	197.5	70,374	329.9	117,566
1973	744.9	265,482	478.82	170,651	266.1	94,831	168.7	60,137	310.1	110,514
1974	386.2	137,642	211.02	75,208	175.2	62,434	51.6	18,405	159.4	56,803
1975	535.5	190,852	336.48	119,921	199.0	70,931	108.7	38,730	227.8	81,192
1976	493.2	175,776	279.75	99,703	213.5	76,074	75.8	27,010	204.0	72,692
1977	677.8	241,568	430.70	153,501	247.1	88,066	133.2	47,476	297.5	106,025
1978	641.4	228,595	413.06	147,215	228.3	81,380	132.2	47,100	280.9	100,114
1979	866.5	308,821	604.35	215,390	262.2	93,430	228.5	81,440	375.8	133,950
1980	622	221,681	393.13	140,112	228.9	81,569	121.7	43,387	271.4	96,724
1981	936.4	333,733	632.43	225,398	304.0	108,335	236.0	84,104	396.4	141,294
1982	596.1	212,450	372.35	132,706	223.8	79,745	101.9	36,320	270.4	96,386
1983	587.5	209,385	355.31	126,632	232.2	82,753	98.1	34,959	257.2	91,673
1984	459.4	163,730	303.36	108,118	156.0	55,613	98.3	35,039	205.0	73,078
1985	559.9	199,548	379.24	135,161	180.7	64,387	128.4	45,756	250.9	89,405
1986	849.4	302,726	579.81	206,644	269.6	96,082	198.6	70,768	381.2	135,877
1987	640.1	228,132	383.53	136,690	256.6	91,442	116.3	41,454	267.2	95,236
1988	643.8	229,450	390.26	139,089	253.5	90,362	126.7	45,139	263.6	93,950
1989	523.2	186,468	314.66	112,145	208.5	74,324	89.8	32,002	224.9	80,143
1990	727.8	259,388	456.65	162,750	271.2	96,638	140.6	50,118	316.0	112,632
1991	556	198,158	331.20	118,040	224.8	80,119	86.7	30,894	244.5	87,146
1992	732.8	261,170	471.31	167,975	261.5	93,195	159.4	56,813	311.9	111,162
1993	721.3	257,071	434.50	154,856	286.8	102,216	121.7	43,374	312.8	111,482
1994	540.2	192,527	341.46	121,696	198.7	70,831	111.4	39,701	230.1	81,995
1995	538.5	191,921	404.90	144,306	133.6	47,615	160.4	57,170	244.5	87,137
1996	512.2	182,548	312.66	111,432	199.5	71,116	87.7	31,241	225.0	80,191
1997	433.2	154,392	267.24	95,244	166.0	59,148	70.7	25,213	196.5	70,032
1998	440.3	156,923	260.60	92,878	179.7	64,045	78.1	27,827	182.5	65,050
1999	424.4	151,256	268.01	95,519	156.4	55,737	84.4	30,078	183.6	65,441
2000	535.9	190,995	325.68	116,072	210.2	74,922	105.1	37,464	220.6	78,609
2002	551.5	196,555	391.69	139,598	159.8	56,956	150.4	53,610	241.3	85,988
2003	554.6	197,659	358.61	127,809	196.0	69,851	111.3	39,654	247.3	88,154
Minimum	386.2	137,642	211	75208	122.9	43,798	51.6	18,405	159.4	56,803
Maximum	936.4	333,733	632	225398	304.0	108,335	236.0	84,104	396.4	141,294
Average	595.8	212,328	379	135064	216.8	77,264	122.0	43,497	256.9	91,567
Percentage	100.0%	100.0%	63.6%	63.6%	36.4%	36.4%	20.5%	20.5%	43.1%	43.1%

**Table B4- LID Infiltration Summary**

<b>LID</b>	<b>Area (ha)</b>	<b>Average Annual Infiltration Volume (m<sup>3</sup>/Yr)</b>	<b>Average Annual Infiltration Volume (mm/Yr)</b>
W1	8.92	11,749	132
W2	8.22	11,093	135
W3	9.9	11,080	112
W4	8.6	10,620	123
<b>Total/Average</b>	<b>35.64</b>	<b>44,543</b>	<b>125.5</b>

**APPENDIX E**  
**GEO TECHNICAL**



**LEGEND:**

APPROXIMATE BOREHOLE LOCATION (GOLDER ASSOCIATES, 04/2019)  
 91.07 GROUND SURFACE ELEVATION (m)  
 BOREHOLE LOCATIONS WERE SURVEYED BY OTHERS AND ARE REFERENCED TO A GEODETIC DATUM.

**PERMISSIBLE GRADE RAISES:**

UP TO 1.2m  
 UP TO 1.4m  
 UP TO 1.8m

**patersongroup**  
consulting engineers

154 Colonnade Road South  
Ottawa, Ontario K2E 7J5  
Tel: (613) 226-7381 Fax: (613) 226-6344

NO.	REVISIONS	DATE	INITIAL
1	UPDATED TO LATEST CONCEPTUAL PLAN	19/10/2021	OC

**CAIVAN COMMUNITIES**  
**GEOTECHNICAL INVESTIGATION**  
**PROP. RESIDENTIAL DEVELOPMENT - CONSERVANCY LANDS WEST**  
 OTTAWA, ONTARIO

Title: **PERMISSIBLE GRADE RAISE PLAN**

Scale:	1:5000	Date:	09/2019
Drawn by:	MPG	Report No.:	PG5036-2
Checked by:	SD	<b>PG5036-5</b>	Revision No.:
Approved by:	SD		